

# The study of viscoelastic behavior of blood vessels

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## Summary

Tissues belonging to cardiovascular system show a viscoelastic behavior, due to superposition of an elastic and a viscous component, so that, the transmission of mechanical energy across the system is split in two parts: one can be stored into tissues and can be retrieved due to elasticity, while the second part is dissipated due to viscosity.

This paper aims at an introductory explanation of the possibilities offered by the fractional calculus in the analysis of the viscoelastic behavior of cardiovascular system.

## Viscoelasticity of arteries

Arteries show a viscoelastic behavior, so that energy transmitted is both stored and dissipated due to elastic and viscous components of arterial walls [1-7]. The knowledge of that behavior and the knowledge of the elastic and viscous components may be of paramount importance in the study of physiopathological mechanisms of degenerative disease affecting cardiovascular systems.

The first relevant studies published about this topic examined the static and dynamic viscoelastic behavior of the dog's arteries [1,2] published a milestone study examining the viscoelasticity of the dog's arteries by means of the analysis of the correlation between radius and pressure at various frequencies. He observed a significant increase in the value of the dynamic elastic (Young's) modulus based on the frequency of the pulse wave, and on the muscular component of the arterial wall. In particular, since the Young's modulus is given as [3]:

$$E = \frac{\Delta p}{\Delta R_e} \frac{2(1-s^2)R_e R_i^2}{(R_e^2 - R_i^2)}, \quad (1)$$

where  $\Delta R_e$  is the variation of external radius induced by the pressure variation  $\Delta p$ , while  $R_i$  is the internal radius, and  $s$  is the Poisson's ratio, e.g. the ratio of the transverse to the axial strain. The Young's modulus of equation (1) may be split into an elastic and a viscous component [2], respectively  $E_c$  and  $E_s$ , given by

$$\begin{aligned} E_c &= E \cos \alpha \\ E_s &= E \sin \alpha \\ &= \eta \omega \end{aligned}$$

$\alpha$  being the phase between pressure change and external radius dilatation,  $\eta$  the viscosity, and  $\omega$  the pulsation, e.g.,  $2\pi$  times the frequency  $\nu$ .

Simulation of the mechanical behavior of arteries is performed using mathematical modeling involving springs (representing elasticity) and dashpots (representing viscosity) in series and in parallel. In a spring, the relationship between stress  $\sigma$  and strain  $\varepsilon$  is given by the equation

$$\frac{\sigma}{\varepsilon} = E,$$

while in a dashpot the relationship is

$$\sigma = \eta \partial_t \varepsilon,$$

the symbol  $\partial_t$  denoting the time derivative. The main combinations of spring and dashpot are the Maxwell model (a spring and a dashpot in series) and the Voigt model (a spring and a dashpot in parallel) [5].

The Maxwell model, with spring  $S$  and dashpot  $D$  in series is characterized by a total stress equal to the stress in both elements, which must be the same, so that  $\sigma = \sigma_S = \sigma_D$ , while total strain is given by the sum of individual strains, to get  $\varepsilon = \varepsilon_S + \varepsilon_D$ , and the time variation of the strain is

$$\partial_t \varepsilon = \left( \frac{1}{E} \partial_t + \frac{\sigma}{\eta} \right) \sigma(t),$$

being of course  $\partial_t \sigma = \partial_t \sigma_S = \partial_t \sigma_D$ .

In the Voigt model, instead, total stress is given by the sum of the individual ones, e.g.,  $\sigma = \sigma_S + \sigma_D$ , and a total strain is  $\varepsilon = \varepsilon_S = \varepsilon_D$ , so that the stress can be written in the form:

$$\sigma(t) = (\eta \partial_t + E) \varepsilon(t).$$

A further model, called the standard linear solid (SLS) model [6], combines a Maxwell model with a spring in parallel. If the Young's modulus of the spring in parallel is  $E_P$ , and the Young's modulus of the spring in the Maxwell model is  $E_M$ , then the equation governing the standard linear solid model is

$$\partial_t \varepsilon(t) = \frac{E_M}{\eta(E_P + E_M)} \left[ \left( \frac{\eta}{E_M} \partial_t + 1 \right) \sigma(t) - E_P \varepsilon(t) \right]. \quad (2)$$

## Fractional calculus

Fractional calculus is a branch of mathematical analysis which studies the fractional derivation and integration of given functions. In first approximation, it can be used when two or more physical effects are superposing and therefore, both are to be taken into accounts.

A simple way to explain how fractional calculus [8] may arise can be evolved knowing that the  $n$ -th derivative of a function  $y(t) = t^m$  is  $y^{(n)}(t) = \partial_t^n y^m = m(m-1) \cdots (m-n+1) y^{m-n}$ , hence we can write

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$$\partial_t^n y^m = \frac{m!}{(m-n)!} y^{m-n} = \frac{\Gamma(m+1)}{\Gamma(m-n+1)} y^{m-n} \quad (3)$$

where  $\Gamma(m+1) = m!$  is the Euler Gamma function,  $m!$  denoting the factorial of  $m$ , e.g., the product  $m(m-1)\dots 1$ . We can then infer

$$\begin{aligned} \Gamma(m+1) &= m(m-1)\dots(m-n-1)(m-n)! \\ &= m(m-1)\dots(m-n-1)\Gamma(m-n+1). \end{aligned}$$

Indeed, the Gamma function is a generalization of the factorial, and is defined for any possible value of a complex variable  $z$ , based on its definition

$$\begin{aligned} \Gamma(z+1) &= \int_0^{+\infty} t^z e^{-t} dt \\ &= -t^z e^{-t} \Big|_0^{+\infty} + z \int_0^{+\infty} t^{z-1} e^{-t} dt \\ &= z\Gamma(z). \end{aligned}$$

Starting from these premises, the Swiss mathematician Leonhard Euler, in 1730 noted that the definition in equation (3) allows to calculate a derivative of fractional order. Using the value  $n = \frac{1}{2}$ , Euler obtained

$$\begin{aligned} \partial_t^{1/2} y &= \frac{\Gamma(1+1)}{\Gamma(1-\frac{1}{2}+1)} y^{1-1/2} \\ &= \frac{\Gamma(2)}{\Gamma(\frac{3}{2})} \sqrt{y} \\ &= \frac{1}{\sqrt{\pi}} \sqrt{y} \\ &= 2 \sqrt{\frac{y}{\pi}}. \end{aligned}$$

Using the same Euler's procedure, one may then calculate a derivative of any order, like for example, the derivative of  $y^\pi$  of order  $\epsilon$ , as follows

$$\begin{aligned} \partial_t^\epsilon y^\pi &= \frac{\Gamma(\pi+1)}{\Gamma(\pi-\epsilon+1)} y^{\pi-\epsilon} \\ &= \int_0^{+\infty} t^\pi e^{-t} dt \left( \int_0^{+\infty} t^{\pi-\epsilon} e^{-t} dt \right)^{-1} y^{\pi-\epsilon}. \end{aligned}$$

More generally, we can use the definition of fractional derivative of order  $\alpha$  of a function  $f(t)$  due to Riemann-Liouville as

$$\partial_t^\alpha f(t) = \frac{1}{\Gamma(1-\alpha)} \partial_t \int_0^t \frac{1}{(t-\tau)^\alpha} f(\tau) d\tau. \quad (4)$$

The same reasoning may lead to definition of integrals of non-integer order, since - based on the Riemann-Liouville definition of  $n$ -th order integration - we can write, for an integer  $n$  and for an integrable function  $f(t)$ :

$$\int_0^t \dots \int_0^t f(\tau) d\tau = \frac{1}{(n+1)!} \int_0^t (t-\tau)^{n-1} f(\tau) d\tau \triangleq J^n f(t),$$

and generalizing the integral to a fractional order  $\varphi$  we obtain:

$$J^\varphi f(t) = \frac{1}{\Gamma(\varphi)} \int_0^t (t-\tau)^{\varphi-1} f(\tau) d\tau,$$

which allows us to integrate  $f(t)$  a non-integer number of times [8-10].

### Applications of fractional calculus for the study of viscoelasticity of arteries

The analysis of viscoelastic behavior of bodies by means of the fractional calculus starts from the possibility to define the fractional derivative of strain, from which one gets the stress in the equivalent forms:

$$\begin{aligned} \sigma(t) &= \eta \theta^\lambda \partial_t^{1-\lambda} \varepsilon(t) \\ &= E \theta^\mu \partial_t^\mu \varepsilon(t) \end{aligned}$$

where  $\theta = \eta/E$  is the time constant, while  $-1 \leq \lambda \leq 0$ , and  $0 \leq \mu \leq 1$ : an element with these characteristics is defined a spring-pot [11], since it possesses the properties of both a spring and a dashpot.

Taking the Laplace transform of equation (2), Craiem and co-workers [12] used the complex Young's modulus  $E^*(s)$  in the frequency domain, given by

$$\begin{aligned} E^*(s) &= \frac{\sigma(s)}{\varepsilon(s)} \\ &= (E_p + E_M) \left[ s + \frac{E_p E_M}{\eta(E_p + E_M)} \right] \left( s + \frac{E_M}{\eta} \right)^{-1}, \end{aligned}$$

to get, from equation (2), the fractional differential equation ruling the spring-pot in the form

$$\partial_t^\alpha \varepsilon(t) = \frac{E_M}{\eta(E_p + E_M)} \left[ \left( \frac{\eta}{E_M} \partial_t^\alpha + 1 \right) \sigma(t) - E_p \varepsilon(t) \right] \quad (5)$$

for which the stress-strain relationship is

$$\sigma(t) = \eta \partial_t^\alpha \varepsilon(t),$$

whereas the fractional version of the complex Young's modulus is

$$E^*(s) = (E_p + E_M) \left[ s^\alpha + \frac{E_p E_M}{\eta(E_p + E_M)} \right] \left( s^\alpha + \frac{E_M}{\eta} \right)^{-1}.$$

Using this mathematical framework, in which the spring-pot substituted the dashpot of a standard linear solid model, it was then possible to validate the experimental results using some segments of the human ascending aorta from donors died not for atherosclerosis-related causes [11], to obtain the values of  $E_p$ ,  $E_M$ ,  $\eta$  and  $\alpha$  at two different experimental levels of stress.

Many other possibilities of simulation are potentially useful in the study of the healthy as well as the pathological behavior of the human blood vessels: the elastic modulus exerts a significant effect on the blood transport along the various tissues and organs. Hence, one would expect that fractional calculus would be of paramount importance in the study, for example, of the blood vessels when, for any cause, the elastic components of the walls suddenly change along an artery: this is the case, for example, of the connection in the renal arteries after a renal transplant [13], or when stress is increased due to physiological or pathological factors [14-16].

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