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Cyclic Triaxial Tests on Eastern Scheldt Sand

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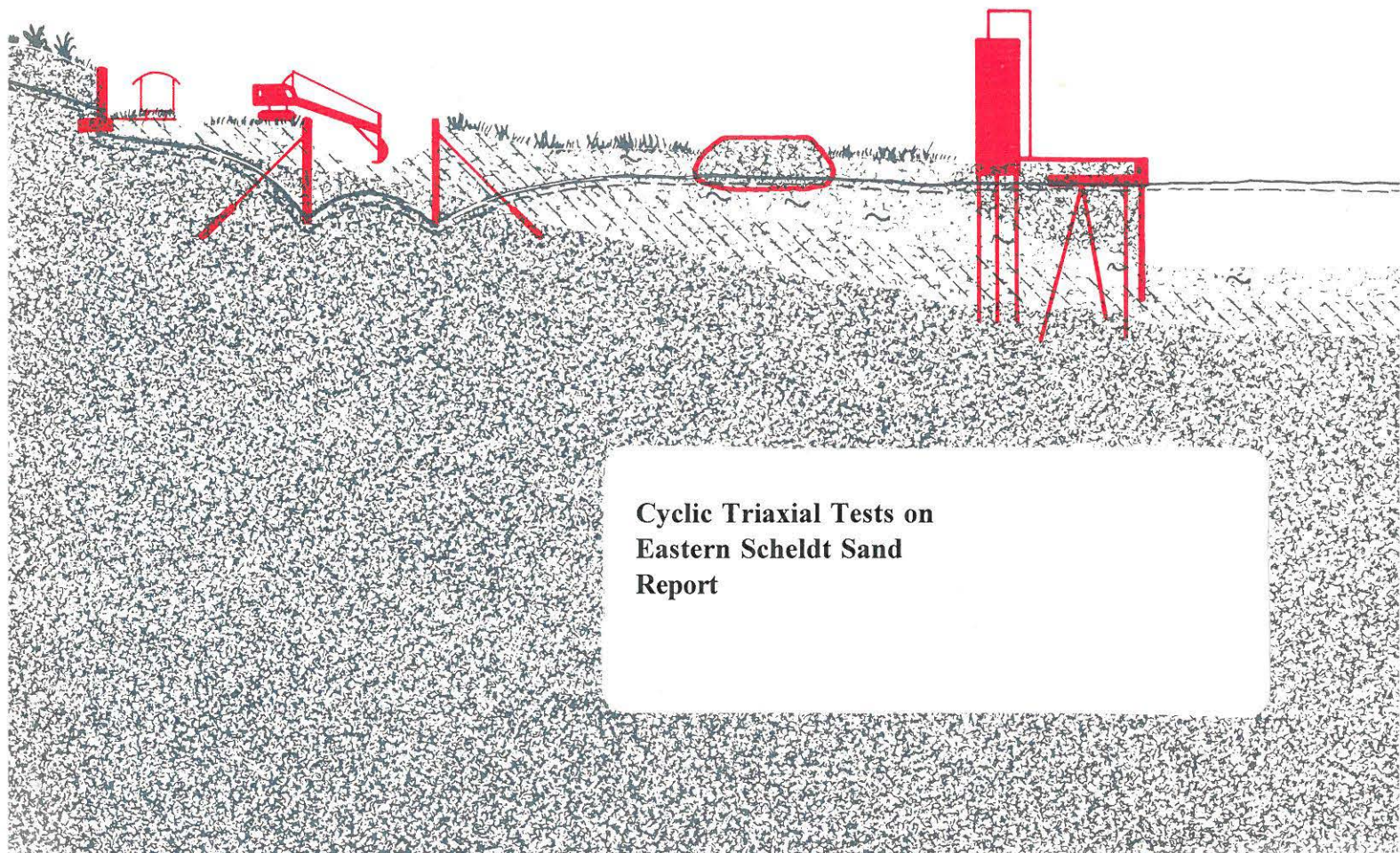
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**Cyclic Triaxial Tests on
Eastern Scheldt Sand
Report**

Aalborg Universitet

Geoteknikgruppen
Sohngaardsholmsvej 57
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**Cyclic Triaxial Tests on
Eastern Scheldt Sand
Report**

Cyclic Triaxial Tests on Eastern Scheldt Sand

Kim Parsberg Jakobsen

Aalborg University, Aalborg, Denmark

1 INTRODUCTION

For prediction of the behaviour of foundations subjected to cyclic loading, for instance earthquakes and repetitive environmental loading, it is common practice to perform numerous laboratory studies. During cyclic loading the pore pressure in the soil mass evidently changes and under disadvantageous conditions the pore pressure build-up will exceed a characteristic value and the soil may liquefy. In the absence of liquefaction excessive settlements may occur. In both cases the damage on foundations and structures can be far-reaching.

Various factors affect the liquefaction potential and settlements of soil (Seed and Lee, 1966; Lee and Seed, 1967):

- Grain size and grading
- Initial density
- Initial state of stress
- Overconsolidation and preshearing
- Load amplitude
- Number of cycles
- Drainage characteristic of the deposit

In the present study the effects of initial state of stress, load amplitude and number of cycles

have been considered with special reference to the development of pore pressure build-up. The study is accomplished by performing several undrained cyclic triaxial tests, starting from different initial states of stress and applying various load amplitudes.

All tests are performed on reconstituted medium dense specimens of Eastern Scheldt Sand. Soil properties, applied equipment and test procedures are described in the succeeding sections, concluding with a summary of the performed triaxial tests.

Information about hydraulic properties and static loading response of Eastern Scheldt Sand under drained and undrained condition can be found in Jakobsen (1998a), Jakobsen and Praastrup (1998) and Jakobsen (1998b), respectively.

2 EASTERN SCHELDT SAND

Eastern Scheldt Sand is a fine, well-sorted line shore quartz sand, with sub-rounded to rounded grains. The classification properties are summarised in Table 1. For information about grain size distributions refer to Jakobsen (1998a).

Table 1. Classification properties for Eastern Scheldt Sand.

| Property | Value |
|--|----------|
| Specific gravity, G_s | 2.650 |
| Maximum void ratio, e_{max} | 0.886 |
| Minimum void ratio, e_{min} | 0.591 |
| Maximum grain size, d_{100} | 0.500 mm |
| Mean grain size, d_{50} | 0.166 mm |
| Fines content | 1.3 % |
| Uniformity coefficient, $C_U = \frac{d_{60}}{d_{10}}$ | 1.52 |
| Curvature coefficient, $C = \frac{d_{30}^2}{d_{10}d_{60}}$ | 0.99 |

3 EQUIPMENT FOR CYCLIC TRIAXIAL TESTING

The cyclic tests are performed in a device based on the measuring principle of the Danish triaxial apparatus developed in the late sixties (Jacobsen, 1970). The measuring and control system have recently been brought up-to-date.

This renovation gives full digital control over the hydraulic actuator, allowing adjustment of axial load or displacement to be executed from the computer. In both cases the axial load and deformation are redirected to the comparator for fast and accurate control of the hydraulic system, generating any prescribed load or deformation. A schematic set-up of the cyclic triaxial apparatus is shown in Figure 1.

During the cyclic test axial load and deformation as well as pore and cell pressure are measured and transmitted to the computer for data processing. If drainage is allowed the volumetric changes can be measured by use of the backpressure system. A summary of the capabilities of the cyclic triaxial apparatus is given in Table 2.

Even though the measuring and control system are up-to-date it is important to avoid measuring errors due to false deformations of the devices. The problem is avoided by performing all the measurements as close to the specimen as possible. Thus, displacement transducers are mounted on the top and bottom pressure heads, the axial load is measured

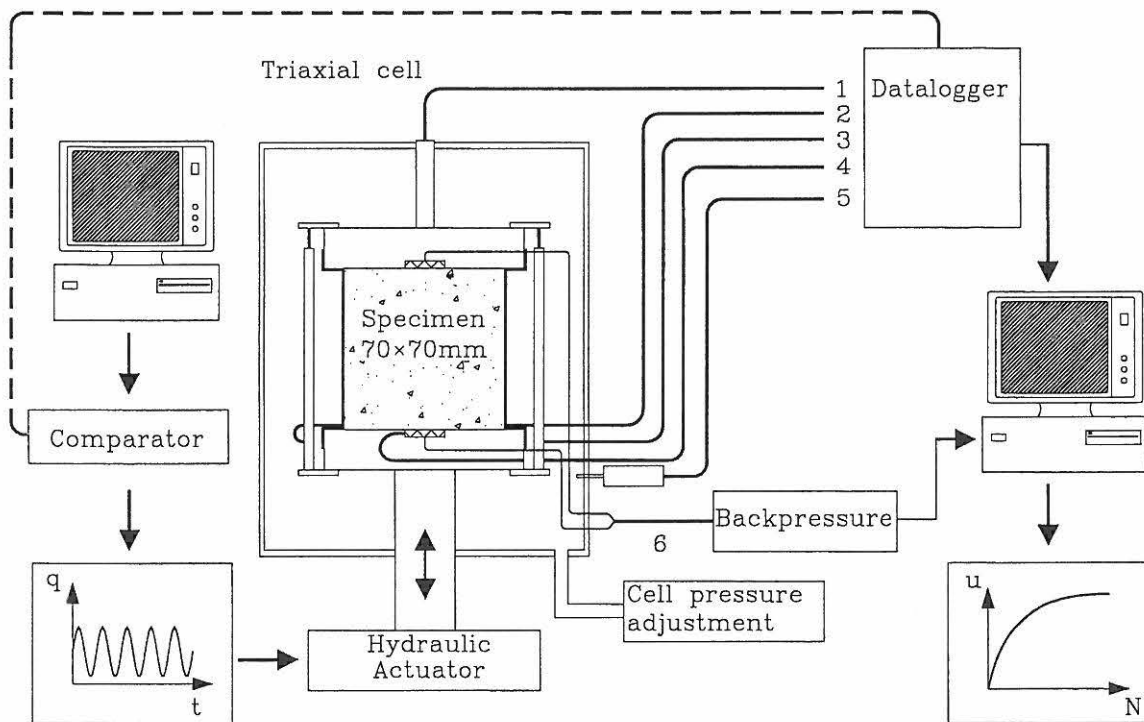


Figure 1. Schematic set-up of the cyclic triaxial apparatus. 1) axial load, 2-3) axial deformation, 4) pore pressure, 5) cell pressure and 6) volumetric change/backpressure.

inside the cell and the pore pressure is measured in the bottom pressure head beneath the porous filter.

Table 2. Capabilities of the cyclic triaxial apparatus.

| Subject | Value |
|----------------------------|--------------|
| Specimen height | 70-140 mm |
| Specimen diameter | 70 mm |
| Maximum axial deformation | 40 mm |
| Deformation rate | 6-10000 %ph. |
| Cyclic loading frequency | 0.01-10 Hz |
| Maximum confining pressure | 700 kPa |
| Maximum axial load | 20 kN |
| Maximum backpressure | 500 kPa |

4 SPECIMEN PREPARATION

In order to obtain homogeneous stress and strain states in the specimen during testing, all tests are performed on 70×70 mm specimens using lubricated end plates (Jacobsen, 1970; Rowe and Barden, 1964; Kirkpatrick, 1974).

The specimens are prepared by air pluviation in a split mould with an initial void ratio of 0.672 and a tolerance of ± 0.001 .

All the specimens are saturated by use of the backpressure technique, as a high degree of saturation is necessary for the achievement of reliable pore pressure measurements (see Jacobsen, 1998b). The degree of saturation is checked by measuring the pore pressure coefficient, B , expressing the ratio between the resulting change in pore pressure and the imposed change in the cell pressure (Skempton, 1954). The degree of saturation is found to be acceptable if B -values above 0.975 are obtained.

5 PERFORMED TRIAXIAL TESTS

After saturation the specimen is isotropically consolidated at a maximum loading rate of 5

kPa per minute to a predefined isotropic stress state, followed by an anisotropic drained consolidation until the desired initial state of stress is reached. A sinusoidal loading with a period of 10 seconds and constant load amplitude is afterwards applied. The confining pressure is kept constant throughout the test.

The test conditions in terms of initial void ratio, initial stress state and load amplitude for the performed tests are summarised in Table 3.

Table 3. Test conditions for performed cyclic triaxial tests.

| Test No. | e_0 [-] | p'_0 [kPa] | q_0 [kPa] | q_{cyc} [kPa] |
|----------|--------------|-----------------|----------------|--------------------|
| 9802.01 | 0.669 | 100.0 | 75.0 | 25.0 |
| 9802.02 | 0.673 | 100.0 | 75.0 | 50.0 |
| 9802.03 | 0.674 | 200.0 | 75.0 | 50.0 |
| 9802.04 | 0.672 | 100.0 | 43.3 | 28.6 |
| 9802.05 | 0.672 | 100.0 | 75.0 | 67.5 |
| 9802.06 | 0.670 | 200.0 | 75.0 | 67.5 |
| 9802.07 | 0.671 | 50.0 | 75.0 | 25.0 |
| 9802.08 | 0.674 | 200.0 | 75.0 | 100.0 |
| 9802.09 | 0.665 | 100.0 | 75.0 | 82.5 |
| 9802.10 | 0.669 | 99.5 | 150.0 | 22.5 |
| 9802.11 | 0.672 | 200.3 | 75.9 | 82.5 |
| 9802.14 | 0.673 | 50.0 | 75.0 | 11.3 |
| 9802.15 | 0.672 | 100.0 | 75.0 | 25.0 |
| 9802.16 | 0.671 | 50.0 | 75.0 | 25.0 |
| 9802.17 | 0.673 | 100.0 | 151.5 | 100.0 |
| 9802.18 | 0.671 | 30.0 | 55.0 | 36.3 |

Graphical presentations of the performed tests are furthermore given in Figures 2 and 3. Figure 2 shows the initial states of stress and the corresponding test numbers. To give an idea of the soil response upon loading the drained failure envelope (see Section 7), is also included. Figure 3 shows the cyclic load amplitude relative to the initial deviator stress (q_{cyc}/q_0) plotted as function of the initial deviatoric stress ratio (q_0/p'_0). For amplitude ratios above unity the tests progress into the extension region.

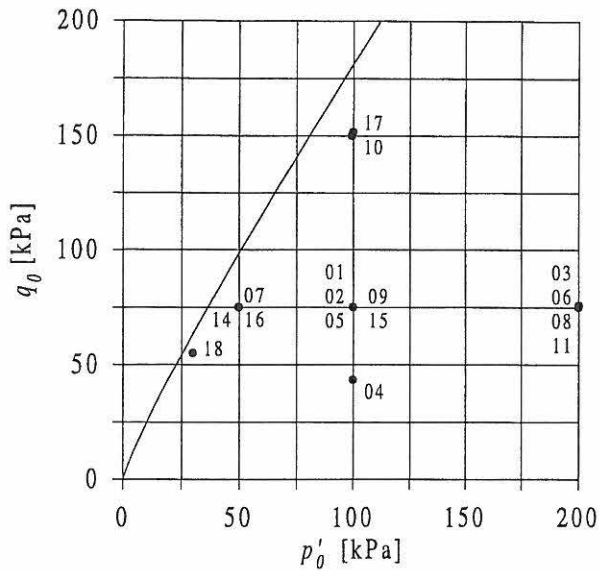


Figure 2. Initial stress states for performed cyclic triaxial tests.

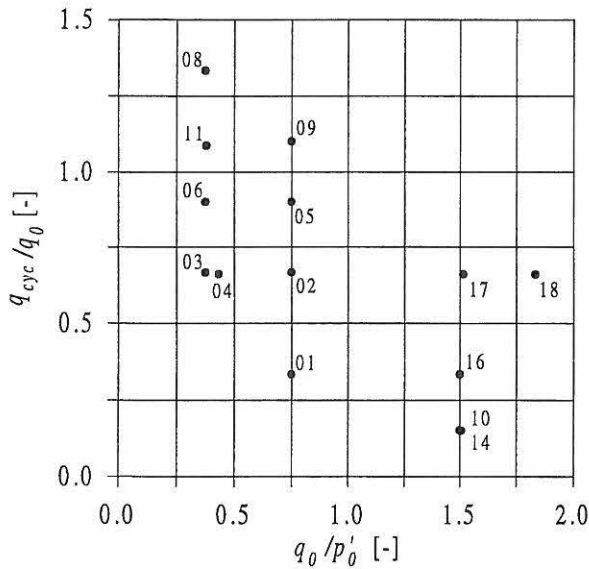


Figure 3. Cyclic load amplitude relative to initial deviator stress for performed cyclic triaxial tests.

6 PRESENTATION OF TEST RESULTS

The analysis of the test results is briefly discussed and parameters used for description of characteristic stress and strain states are defined.

During the triaxial test simultaneous values of axial displacement, volumetric change,

confining pressure, pore pressure and axial load are measured by the principles outlined in Section 3. As both the measured loads and displacements coincide with the principal axes of stresses and strains the analysis is straight forward.

The exact displacement field is established from the measured axial displacements and the volumetric change. From these quantities the radial displacement, u_2 is determined by the relation:

$$u_2 = \frac{D_0}{2} - \sqrt{\frac{V_0 - \Delta V}{\pi(H_0 - u_1)}} \quad (1)$$

u_1 being the average value of the measured axial displacements and $V_0 - \Delta V$ the current volume of the specimen. The relative deformation can afterwards be expressed by any suitable strain measure. In geotechnical engineering or geomechanics it is common practice to use the simple and linear engineering strain measure. This measure is, however found to be inconsistent with the used measuring techniques and may lead to erroneous results (Praastrup et al. 1998). It is therefore chosen to use the non-linear natural strain measure instead:

$$\varepsilon_1 = \ln\left(\frac{H_0}{H_0 - u_1}\right) \quad (2)$$

$$\varepsilon_2 = \varepsilon_3 = \ln\left(\frac{D_0}{D_0 - 2u_2}\right) \quad (3)$$

$$\varepsilon_v = \varepsilon_1 + 2\varepsilon_3 = \ln\left(\frac{V_0}{V_0 - \Delta V}\right) \quad (4)$$

The stresses are given as true stresses, expressing the ratio between current load and current area. The cross sectional area of the specimen is continuously corrected by:

$$A = \frac{\pi}{4}(D_0 - 2u_2)^2 = \frac{V_0 - \Delta V}{H_0 - u_1} \quad (5)$$

The test results are in general presented in terms of the deviatoric stress q and mean normal stress p' :

$$p' = \frac{1}{3}(\sigma'_1 + 2\sigma'_3) = \frac{1}{3}((\sigma_1 - u) + 2(\sigma_3 - u)) \quad (6)$$

$$q = (\sigma'_1 - \sigma'_3) \quad (7)$$

in which primes denote effective stresses.

Associated with these stress quantities are the volumetric and shear strain, ε_v and ε_q :

$$\varepsilon_v = \varepsilon_1 + 2\varepsilon_3 \quad (8)$$

$$\varepsilon_q = \frac{2}{3}(\varepsilon_1 - \varepsilon_3) = \varepsilon_1 - \frac{1}{3}\varepsilon_v \quad (9)$$

For description of the cyclic load and the development in stresses and strains during the cyclic loading step the following quantities are defined:

$$q_{cyc}(N) = \frac{1}{2}(q_{\max} - q_{\min}) \quad (10)$$

$$q_m(N) = \frac{1}{2}(q_{\max} + q_{\min}) \quad (11)$$

$$p'_m(N) = (\sigma_3 - u_p) + \frac{1}{3}q_m \quad (12)$$

The permanent pore pressure, u_p , is determined for $q = q_m$ after each load cycle. The development in pore pressure is furthermore described in term of the cyclic pore pressure given by:

$$u_{cyc}(N) = \frac{1}{2}(u_{\max} - u_{\min}) \quad (13)$$

The developments in strains are given in terms of cyclic axial strain, ε_{cyc} , and permanent or irrecoverable axial strain, ε_p , within each load cycle. The cyclic axial strain is calculated by:

$$\varepsilon_{cyc}(N) = \frac{1}{2}(\varepsilon_{\max} - \varepsilon_{\min}) \quad (14)$$

The permanent axial strain is taken at the same time as the permanent pore pressure.

7 SUMMARY OF TEST RESULTS

Results from the tests, outlined in Table 2, are shown in Enclosures 1-16 consisting of four pages each.

Page 1: Test conditions, test programme and results of isotropic and anisotropic consolidation.

Page 2: Results from undrained cyclic loading, including mean normal stress, mean deviator stress, permanent and cyclic pore pressure and permanent and cyclic axial strain for chosen cycles.

Page 3: Cyclic stress response in the $p' - q$ plane. The development in stresses are bounded by the drained failure envelopes in compression and extension (Jacobsen, 1989):

$$q_f = \frac{6 \sin \varphi_a}{3 - \sin \varphi_a} p' \left(1 + \frac{c_a \cot \varphi_a}{m p'} \right)^m \quad (15)$$

$$q_f = \frac{-6 \sin \varphi_a}{3 + \sin \varphi_a} p' \left(1 + \frac{c_a \cot \varphi_a}{m p'} \right)^m \quad (16)$$

The parameters $\varphi_a = 35.0^\circ$, $c_a = 46.2$ kPa and $m = 0.143$ are derived from static triaxial tests reported by Jacobsen and Praastrup (1998b). As no extension tests have been performed the friction angle is increased by 10 percent in the extension region.

Page 4: Development of deviator stress, pore pressure and axial strain quantities with number of cycles applied.

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9 NOTATION

| | | |
|---------------------|--------------------|---|
| A | [mm ²] | : area of specimen |
| B | [-] | : Skempton's pore pressure parameter |
| C | [-] | : curvature coefficient |
| C_U | [-] | : uniformity coefficient |
| c_a | [kPa] | : asymptotic cohesion for curved failure criteria |
| d | [mm] | : grain size |
| D_0 | [mm] | : initial diameter of specimen |
| e | [-] | : void ratio |
| e_0 | [-] | : initial void ratio |
| e_{max} | [-] | : maximum void ratio |
| e_{min} | [-] | : minimum void ratio |
| G_s | [-] | : specific gravity |
| H_0 | [mm] | : initial height of specimen |
| m | [-] | : curvature parameter for failure criteria |
| N | [-] | : number of cycles |
| p' | [kPa] | : mean normal stress (effective) |
| p'_0 | [kPa] | : initial mean normal stress (effective) |
| p'_m | [kPa] | : mean normal stress (effective) after N cycles |
| q | [kPa] | : deviator stress |
| q_m | [kPa] | : mean deviator stress |
| q_{cyc} | [kPa] | : cyclic deviator stress |
| u | [kPa] | : pore pressure |
| u_p | [kPa] | : permanent pore pressure after N cycles |
| u_{cyc} | [kPa] | : cyclic pore pressure after N cycles |
| u_i | [mm] | : principal displacements, $i=1..3$ |
| V_0 | [mm ³] | : initial volume of specimen |
| ε_{cyc} | [%] | : cyclic axial strain after N cycles |
| ε_p | [%] | : permanent axial strain after N cycles |
| ε_q | [%] | : triaxial shear strain |
| ε_v | [%] | : triaxial volumetric strain |
| ε_i | [%] | : principal strains, $i=1..3$ |
| σ'_3 | [kPa] | : confining pressure (effective) |
| σ'_i | [kPa] | : principal stresses (effective), $i=1..3$ |
| φ_a | [°] | : asymptotic friction angle for curved failure criteria |

Enclosures

| | | |
|--------------|------------------------------------|---------|
| Enclosure 1 | Cyclic Triaxial Test 9802.01 | 4 pages |
| Enclosure 2 | Cyclic Triaxial Test 9802.02 | 4 pages |
| Enclosure 3 | Cyclic Triaxial Test 9802.03 | 4 pages |
| Enclosure 4 | Cyclic Triaxial Test 9802.04 | 4 pages |
| Enclosure 5 | Cyclic Triaxial Test 9802.05 | 4 pages |
| Enclosure 6 | Cyclic Triaxial Test 9802.06 | 4 pages |
| Enclosure 7 | Cyclic Triaxial Test 9802.07 | 4 pages |
| Enclosure 8 | Cyclic Triaxial Test 9802.08 | 4 pages |
| Enclosure 9 | Cyclic Triaxial Test 9802.09 | 4 pages |
| Enclosure 10 | Cyclic Triaxial Test 9802.10 | 4 pages |
| Enclosure 11 | Cyclic Triaxial Test 9802.11 | 4 pages |
| Enclosure 12 | Cyclic Triaxial Test 9802.14 | 4 pages |
| Enclosure 13 | Cyclic Triaxial Test 9802.15 | 4 pages |
| Enclosure 14 | Cyclic Triaxial Test 9802.16 | 4 pages |
| Enclosure 15 | Cyclic Triaxial Test 9802.17 | 4 pages |
| Enclosure 16 | Cyclic Triaxial Test 9802.18 | 4 pages |

| | | | |
|--|---------------------------------|-------------------|----------|
| Description of soil Eastern Scheldt Sand | Cyclic Triaxial Apparatus | Sample properties | |
| Specimen preparation Air pluviation | Calibration file Cal9802.dat | Height | 71.50 mm |
| Saturation procedure CO ₂ / Backpressure | Date 1998-01-29 | Diameter | 69.70 mm |
| | | Void ratio | 0.669 |
| | | B-value | 0.996 |

| | | | |
|--------------|---|-------------|---------|
| Test program | Isotropic compression, σ'_3 : | 10.0 - 75.0 | kPa |
| | Loading rate: | 5.0 | kPa/min |
| | Anisotropic compression, q_m : | 75.0 | kPa |
| | Loading rate: | 3.0 | kPa/min |
| | <input checked="" type="checkbox"/> Applied drained | | |
| | <input type="checkbox"/> Applied undrained | | |
| | Cyclic loading, q_{cyc} : | 25.0 | kPa |
| | Period: | 10.0 | s |

| | | | |
|-----------------------|--------------|-------|-----|
| Isotropic compression | | | |
| Confining pressure | σ'_3 | 75.3 | kPa |
| Pore pressure | u | 199.8 | kPa |
| Axial strain | ϵ_1 | 0.12 | % |
| Volumetric strain | ϵ_v | 0.38 | % |
| Void ratio | e | 0.663 | |

| | | | |
|-------------------------|--------------|-------|-----|
| Anisotropic compression | | | |
| Confining pressure | σ'_3 | 75.0 | kPa |
| Axial pressure | σ'_1 | 149.9 | kPa |
| Deviator stress | q | 74.9 | kPa |
| Mean normal stress | p' | 100.0 | kPa |
| Pore pressure | u | 199.8 | kPa |
| Axial strain | ϵ_1 | 0.39 | % |
| Volumetric strain | ϵ_v | 0.52 | % |
| Void ratio | e | 0.660 | |

| | |
|--------------------|--------------------|
| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 1 |
| Evaluated: KPJ | Approved: KPJ |

| Cyclic loading | | | | | | |
|----------------|---------------|--------------|--------------|------------------|-------------------|-----------------------|
| N | p'_m kPa | q_m kPa | u_p kPa | u_{cyc} kPa | ϵ_p % | ϵ_{cyc} % |
| 1 | 93.9 | 74.0 | 5.9 | 3.9 | 0.11 | 0.06 |
| 3 | 91.4 | 74.0 | 8.1 | 4.8 | 0.14 | 0.01 |
| 5 | 90.4 | 74.0 | 9.2 | 5.0 | 0.15 | 0.01 |
| 10 | 88.4 | 74.0 | 11.2 | 5.0 | 0.17 | 0.01 |
| 25 | 86.2 | 73.9 | 13.6 | 5.1 | 0.21 | 0.01 |
| 50 | 83.9 | 73.9 | 15.8 | 5.0 | 0.24 | 0.01 |
| 75 | 82.6 | 73.9 | 17.0 | 4.9 | 0.27 | 0.01 |
| 100 | 82.1 | 73.9 | 17.7 | 4.9 | 0.29 | 0.01 |
| 150 | 80.2 | 73.9 | 19.5 | 4.6 | 0.30 | 0.01 |
| 200 | 80.8 | 73.9 | 18.9 | 5.2 | 0.31 | 0.01 |
| 300 | 79.7 | 73.8 | 20.1 | 4.7 | 0.35 | 0.00 |
| 400 | 79.5 | 73.8 | 20.2 | 4.7 | 0.36 | 0.00 |
| 500 | 79.8 | 73.8 | 20.0 | 4.7 | 0.37 | 0.00 |
| 750 | 81.0 | 73.8 | 18.6 | 5.1 | 0.38 | 0.00 |
| 1000 | 83.3 | 73.8 | 16.4 | 4.9 | 0.39 | 0.00 |
| 1250 | 86.1 | 73.8 | 13.5 | 5.1 | 0.40 | 0.00 |
| 1500 | 88.3 | 73.8 | 11.5 | 5.1 | 0.40 | 0.00 |
| 1750 | 90.0 | 73.8 | 9.8 | 5.1 | 0.41 | 0.00 |
| 2000 | 92.1 | 73.8 | 7.6 | 5.3 | 0.41 | 0.00 |
| 2250 | 95.4 | 73.8 | 4.6 | 5.6 | 0.42 | 0.00 |
| 2500 | 97.1 | 73.8 | 2.8 | 5.5 | 0.42 | 0.00 |
| 3000 | 100.5 | 73.8 | -0.9 | 5.6 | 0.43 | 0.00 |
| 3500 | 104.3 | 73.8 | -4.7 | 5.7 | 0.43 | 0.00 |
| 3900 | 108.1 | 73.8 | -8.8 | 5.8 | 0.43 | 0.00 |

Remarks:

Job: Ph.D. Project

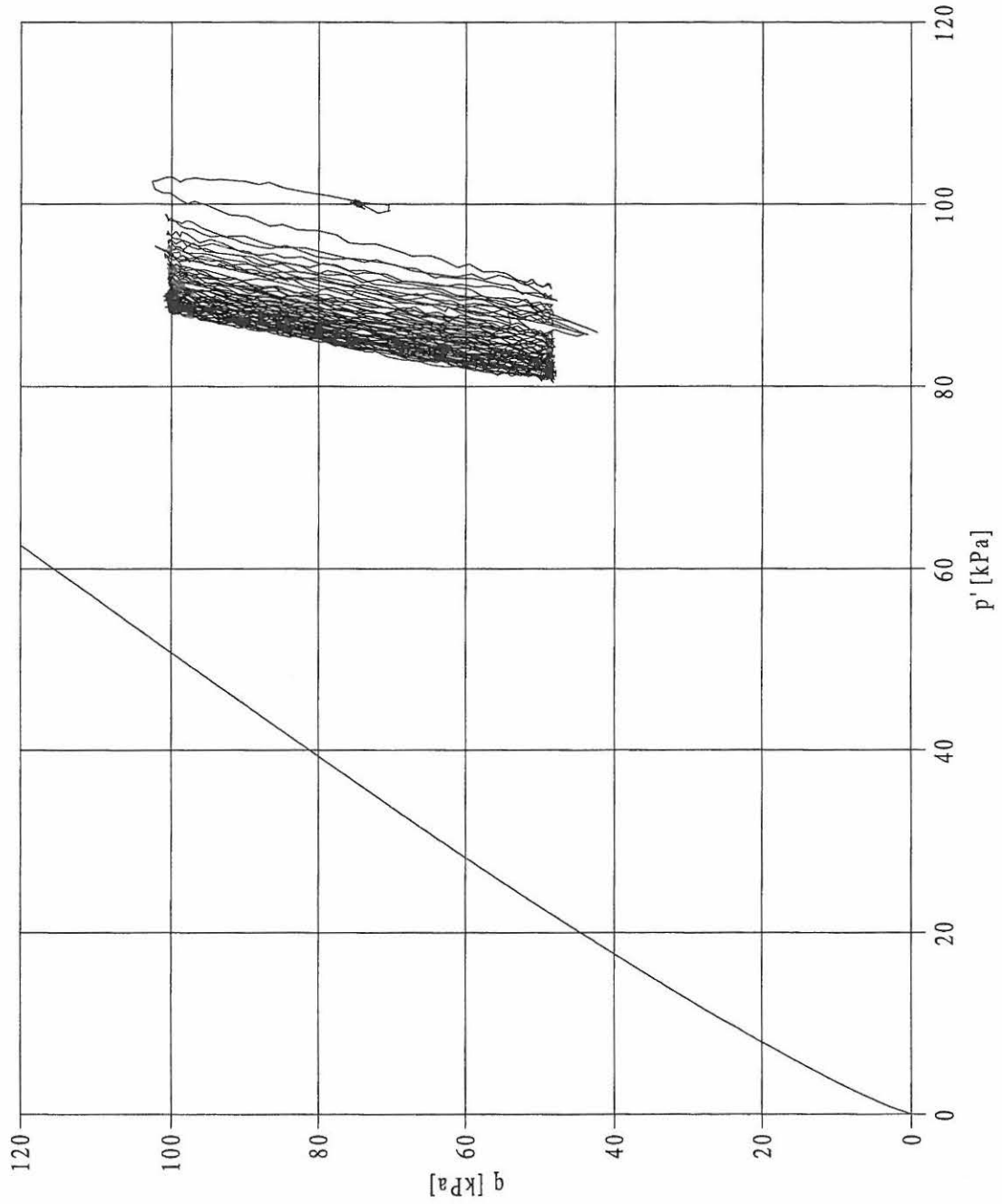
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Executed: KPJ

Enclosure No. 1

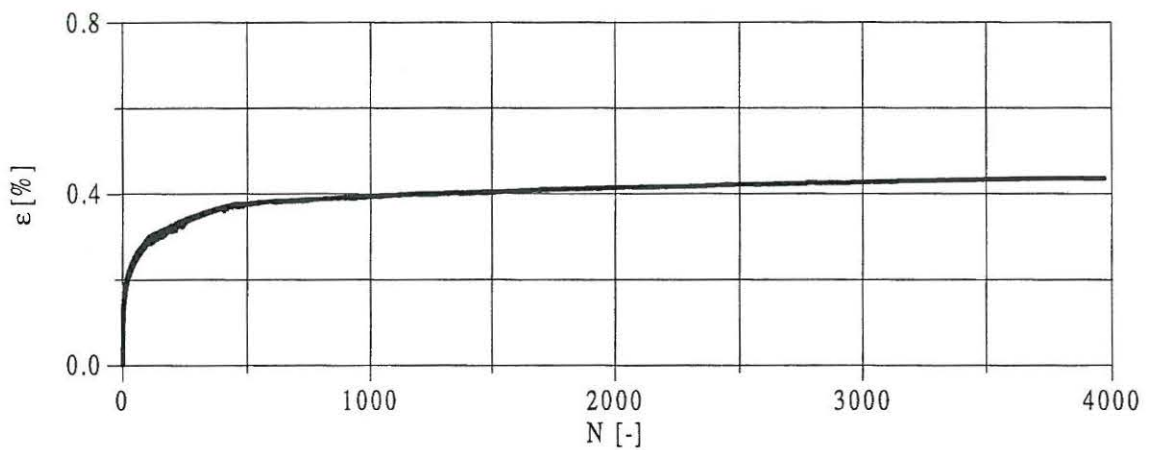
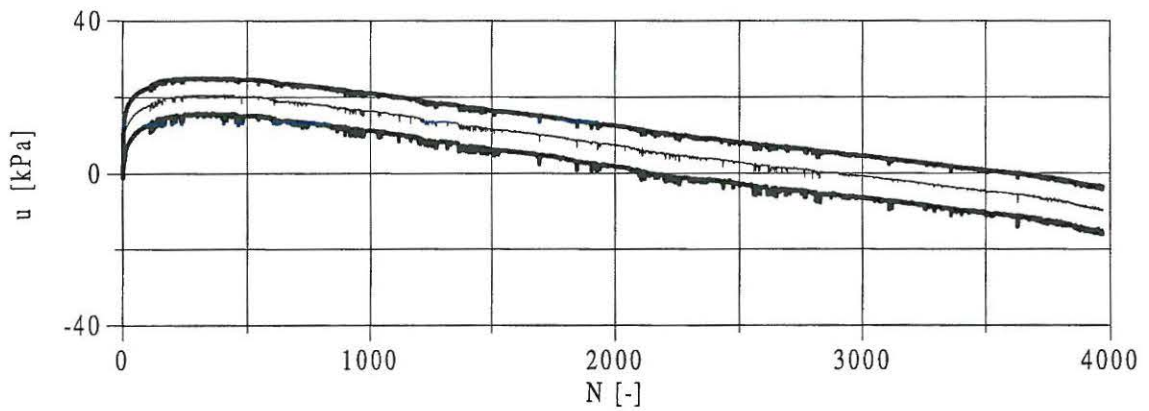
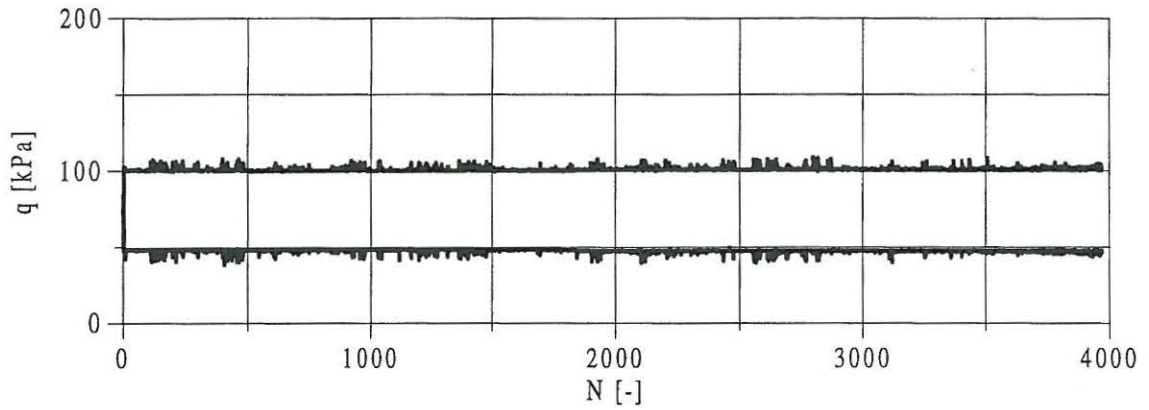
Evaluated: KPJ

Approved: KPJ



Remarks
Noise on load signal
Only cycle 1-500 plotted.

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| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 1 |
| Evaluated: KPJ | Approved: KPJ |



Remarks
Noise on load signal

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|----------------|--------------------|
| Job: | Aalborg University |
| Executed: KPJ | Enclosure No. 1 |
| Evaluated: KPJ | Approved: KPJ |

| | | | |
|--|---------------------------------|-------------------|----------|
| Description of soil Eastern Scheldt Sand | Cyclic Triaxial Apparatus | Sample properties | |
| Specimen preparation Air pluviation | Calibration file Cal9802.dat | Height | 71.50 mm |
| Saturation procedure CO ₂ / Backpressure | Date 1998-01-30 | Diameter | 69.70 mm |
| | | Void ratio | 0.673 |
| | | B-value | 0.980 |

| | | | |
|--------------|---|-------------|---------|
| Test program | Isotropic compression, σ'_3 : | 10.0 - 75.0 | kPa |
| | Loading rate: | 5.0 | kPa/min |
| | Anisotropic compression, q_m : | 75.0 | kPa |
| | Loading rate: | 3.0 | kPa/min |
| | <input checked="" type="checkbox"/> Applied drained | | |
| | <input type="checkbox"/> Applied undrained | | |
| | Cyclic loading, q_{cyc} : | 50.0 | kPa |
| | Period: | 10.0 | s |

| | | | |
|-----------------------|--------------|-------|-----|
| Isotropic compression | | | |
| Confining pressure | σ'_3 | 75.1 | kPa |
| Pore pressure | u | 300.0 | kPa |
| Axial strain | ϵ_1 | 0.15 | % |
| Volumetric strain | ϵ_v | 0.42 | % |
| Void ratio | e | 0.666 | |

| | | | |
|-------------------------|--------------|-------|-----|
| Anisotropic compression | | | |
| Confining pressure | σ'_3 | 75.0 | kPa |
| Axial pressure | σ'_1 | 149.7 | kPa |
| Deviator stress | q | 74.7 | kPa |
| Mean normal stress | p' | 99.9 | kPa |
| Pore pressure | u | 199.8 | kPa |
| Axial strain | ϵ_1 | 0.39 | % |
| Volumetric strain | ϵ_v | 0.57 | % |
| Void ratio | e | 0.664 | |

| | |
|--------------------|--------------------|
| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 2 |
| Evaluated: KPJ | Approved: KPJ |

| Cyclic loading | | | | | | |
|----------------|---------------|--------------|--------------|------------------|-------------------|-----------------------|
| N | P'_m kPa | q_m kPa | u_p kPa | u_{cyc} kPa | ϵ_p % | ϵ_{cyc} % |
| 1 | 86.3 | 74.6 | 13.4 | 6.7 | 0.20 | 0.11 |
| 3 | 82.8 | 74.5 | 17.0 | 7.6 | 0.26 | 0.03 |
| 5 | 81.1 | 74.5 | 18.6 | 7.7 | 0.30 | 0.02 |
| 10 | 78.6 | 74.4 | 21.2 | 7.8 | 0.36 | 0.02 |
| 25 | 75.9 | 74.3 | 23.9 | 7.7 | 0.47 | 0.02 |
| 50 | 73.8 | 74.3 | 26.0 | 7.6 | 0.58 | 0.02 |
| 75 | 73.0 | 74.2 | 26.9 | 7.4 | 0.65 | 0.01 |
| 100 | 72.1 | 74.2 | 27.6 | 7.3 | 0.70 | 0.01 |
| 150 | 71.2 | 74.1 | 28.6 | 7.3 | 0.78 | 0.01 |
| 200 | 70.7 | 74.1 | 29.1 | 7.2 | 0.83 | 0.01 |
| 300 | 70.0 | 74.0 | 30.0 | 7.2 | 0.91 | 0.01 |
| 400 | 69.5 | 74.0 | 30.4 | 7.0 | 0.97 | 0.01 |
| 500 | 69.9 | 73.9 | 30.3 | 7.0 | 1.01 | 0.01 |
| 750 | 69.0 | 73.8 | 31.1 | 7.0 | 1.08 | 0.00 |
| 1000 | 69.0 | 73.8 | 31.1 | 7.1 | 1.13 | 0.00 |
| 1250 | 69.1 | 73.8 | 31.2 | 6.9 | 1.17 | 0.00 |
| 1500 | 69.0 | 73.7 | 31.4 | 6.9 | 1.20 | 0.00 |
| 1750 | 67.9 | 73.7 | 32.6 | 6.9 | 1.23 | 0.00 |
| 2000 | 67.9 | 73.7 | 32.6 | 6.9 | 1.25 | 0.00 |

Remarks:

Job: Ph.D. Project

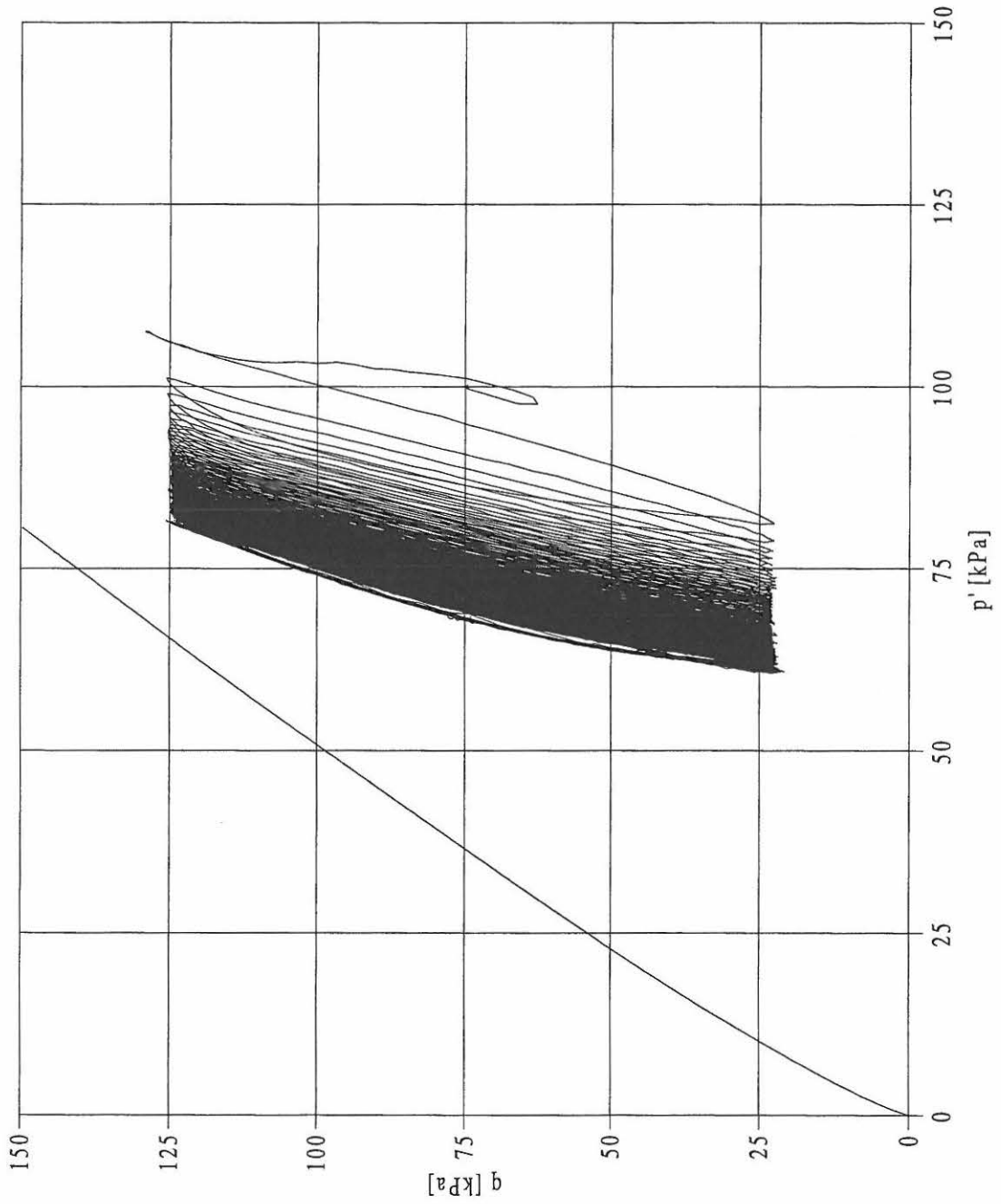
Aalborg University

Executed: KPJ

Enclosure No. 2

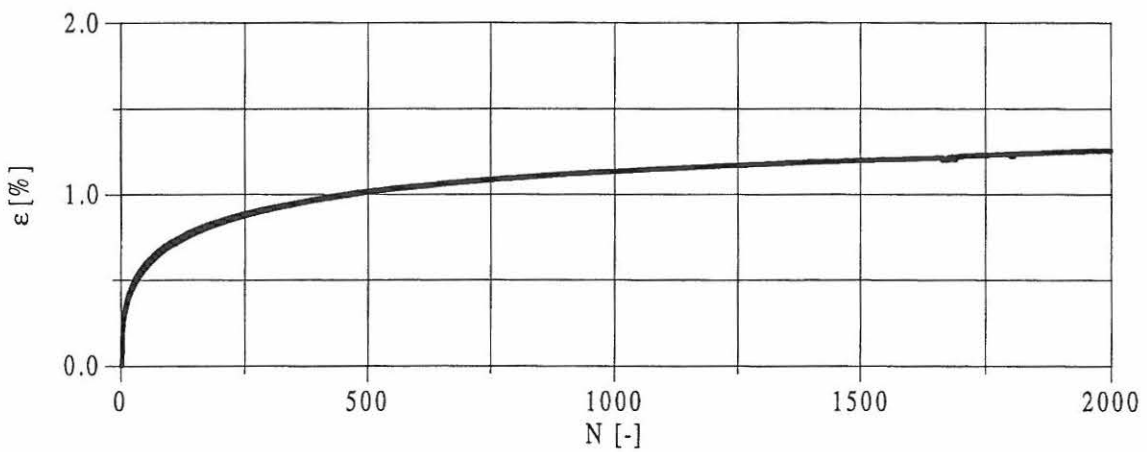
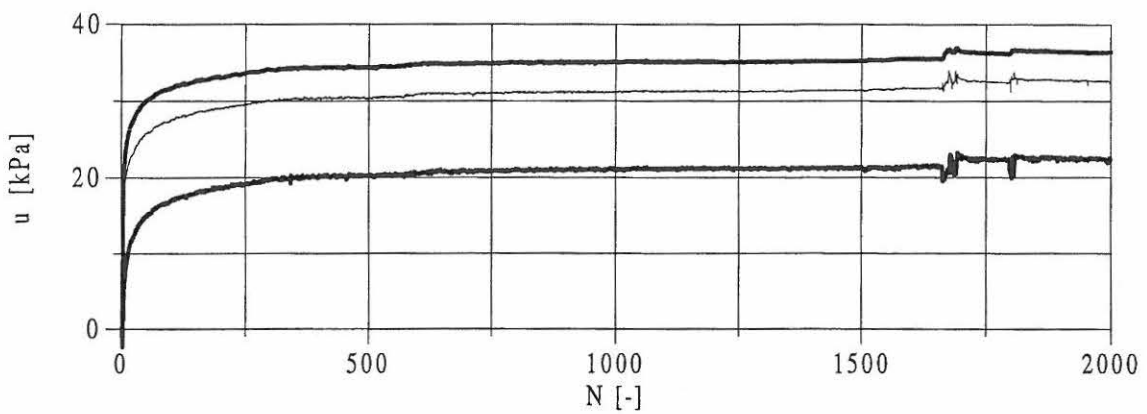
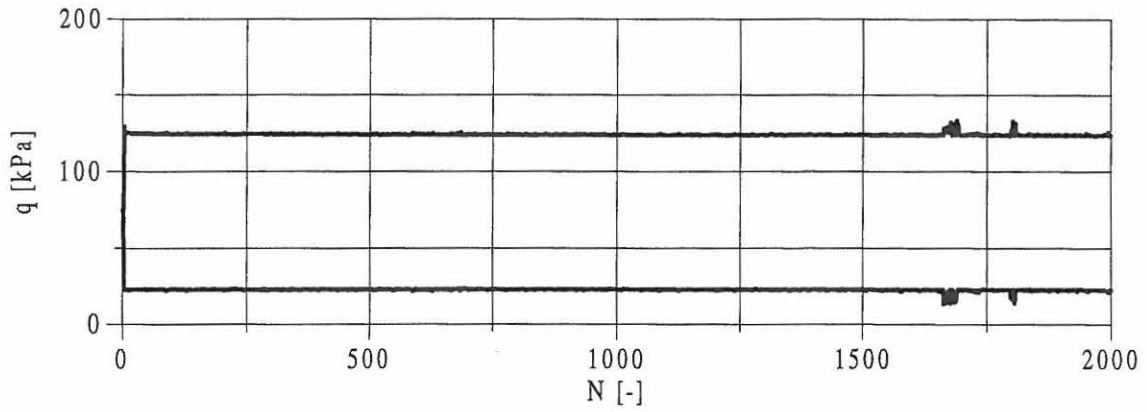
Evaluated: KPJ

Approved: KPJ



Remarks

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| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 2 |
| Evaluated: KPJ | Approved: KPJ |



Remarks

Job: Aalborg University
 Executed: KPJ
 Evaluated: KPJ
 Enclosure No. 2
 Approved: KPJ

| | | | |
|--|---------------------------------|-------------------|----------|
| Description of soil Eastern Scheldt Sand | Cyclic Triaxial Apparatus | Sample properties | |
| Specimen preparation Air pluviation | Calibration file Cal9802.dat | Height | 71.51 mm |
| Saturation procedure CO ₂ / Backpressure | Date 1998-01-31 | Diameter | 69.71 mm |
| | | Void ratio | 0.674 |
| | | B-value | 0.983 |

| | | | |
|--------------|---|--------------|---------|
| Test program | Isotropic compression, σ'_3 : | 10.0 - 175.0 | kPa |
| | Loading rate: | 5.0 | kPa/min |
| | Anisotropic compression, q_m : | 75.0 | kPa |
| | Loading rate: | 3.0 | kPa/min |
| | <input checked="" type="checkbox"/> Applied drained | | |
| | <input type="checkbox"/> Applied undrained | | |
| | Cyclic loading, q_{cyc} : | 50.0 | kPa |
| | Period: | 10.0 | s |

| | | | |
|-----------------------|--------------|-------|-----|
| Isotropic compression | | | |
| Confining pressure | σ'_3 | 175.2 | kPa |
| Pore pressure | u | 300.0 | kPa |
| Axial strain | ϵ_1 | 0.27 | % |
| Volumetric strain | ϵ_v | 0.73 | % |
| Void ratio | e | 0.661 | |

| | | | |
|-------------------------|--------------|-------|-----|
| Anisotropic compression | | | |
| Confining pressure | σ'_3 | 175.0 | kPa |
| Axial pressure | σ'_1 | 249.9 | kPa |
| Deviator stress | q | 74.9 | kPa |
| Mean normal stress | p' | 200.0 | kPa |
| Pore pressure | u | 300.0 | kPa |
| Axial strain | ϵ_1 | 0.40 | % |
| Volumetric strain | ϵ_v | 0.85 | % |
| Void ratio | e | 0.659 | |

| | |
|--------------------|--------------------|
| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 3 |
| Evaluated: KPJ | Approved: KPJ |

| Cyclic loading | | | | | | |
|----------------|---------------|--------------|--------------|------------------|-------------------|-----------------------|
| N | P'_m kPa | q_m kPa | u_p kPa | u_{cyc} kPa | ϵ_p % | ϵ_{cyc} % |
| 1 | 175.4 | 75.4 | 24.7 | 16.6 | 0.05 | 0.04 |
| 3 | 166.5 | 75.4 | 33.6 | 13.7 | 0.07 | 0.01 |
| 5 | 161.7 | 75.4 | 38.4 | 13.8 | 0.08 | 0.01 |
| 10 | 154.3 | 75.4 | 45.8 | 13.9 | 0.09 | 0.01 |
| 25 | 142.4 | 75.4 | 57.7 | 13.9 | 0.13 | 0.01 |
| 50 | 132.6 | 75.4 | 67.5 | 13.6 | 0.16 | 0.01 |
| 75 | 125.8 | 75.4 | 74.1 | 12.8 | 0.18 | 0.01 |
| 100 | 120.9 | 75.3 | 79.1 | 12.5 | 0.20 | 0.00 |
| 150 | 113.4 | 75.3 | 86.5 | 12.2 | 0.23 | 0.00 |
| 200 | 108.1 | 75.3 | 91.8 | 11.6 | 0.25 | 0.00 |
| 300 | 100.4 | 75.3 | 99.5 | 11.8 | 0.29 | 0.00 |
| 400 | 95.0 | 75.2 | 104.9 | 10.7 | 0.34 | 0.00 |
| 500 | 91.3 | 75.2 | 108.5 | 10.1 | 0.37 | 0.00 |
| 750 | 85.7 | 75.2 | 114.2 | 9.6 | 0.43 | 0.00 |
| 1000 | 82.8 | 75.1 | 117.2 | 9.2 | 0.49 | 0.00 |
| 1250 | 80.8 | 75.1 | 119.3 | 9.1 | 0.55 | 0.00 |
| 1500 | 80.0 | 75.0 | 120.2 | 8.9 | 0.58 | 0.00 |
| 1750 | 79.4 | 75.0 | 120.8 | 8.8 | 0.62 | 0.00 |
| 2000 | 79.3 | 75.0 | 121.0 | 8.6 | 0.64 | 0.00 |
| 2250 | 79.4 | 74.9 | 121.0 | 8.7 | 0.66 | 0.00 |
| 2500 | 79.4 | 74.9 | 121.0 | 8.6 | 0.67 | 0.00 |
| 3000 | 79.9 | 74.9 | 120.6 | 8.6 | 0.70 | 0.00 |
| 3500 | 80.3 | 74.9 | 120.2 | 8.7 | 0.71 | 0.00 |
| 4000 | 80.9 | 74.9 | 119.7 | 8.7 | 0.73 | 0.00 |

Remarks:

Job: Ph.D. Project

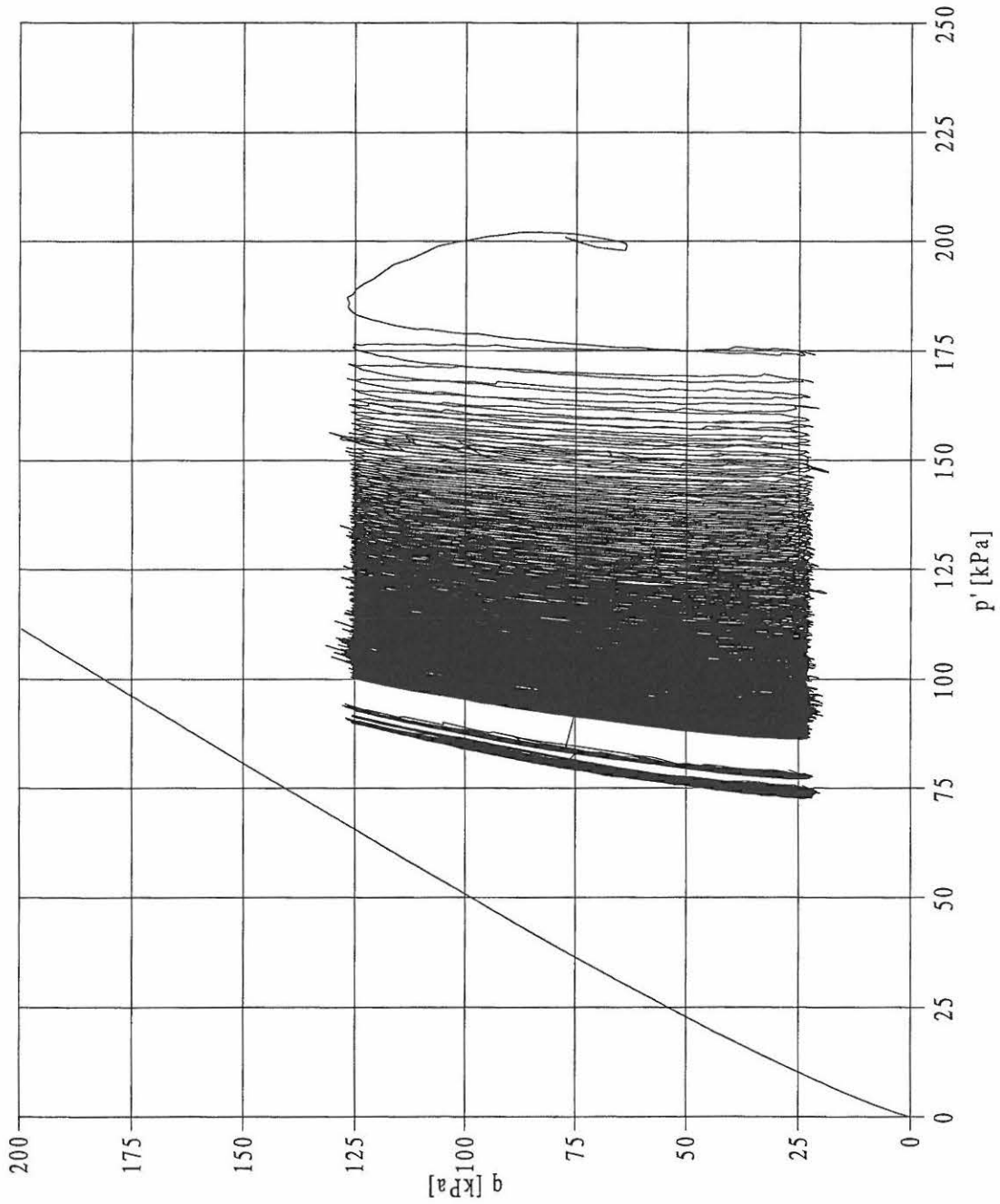
Aalborg University

Executed: KPJ

Enclosure No. 3

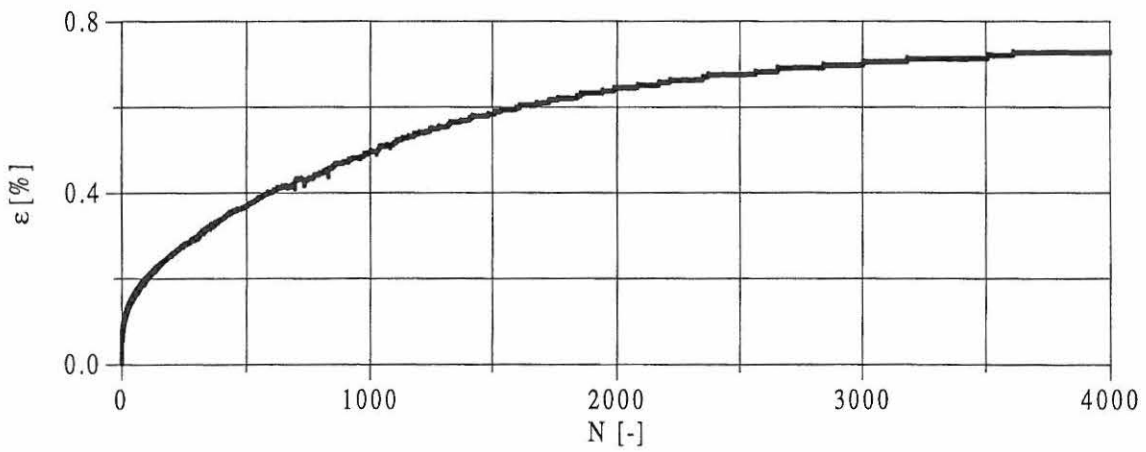
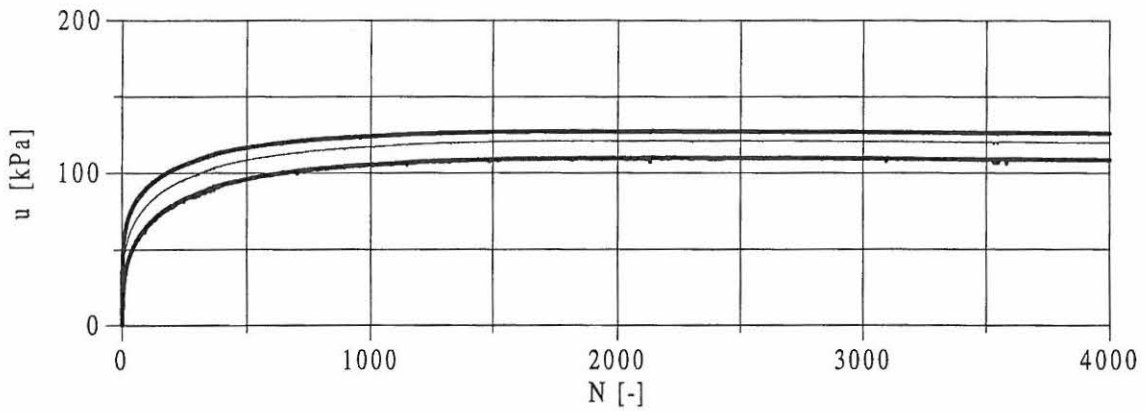
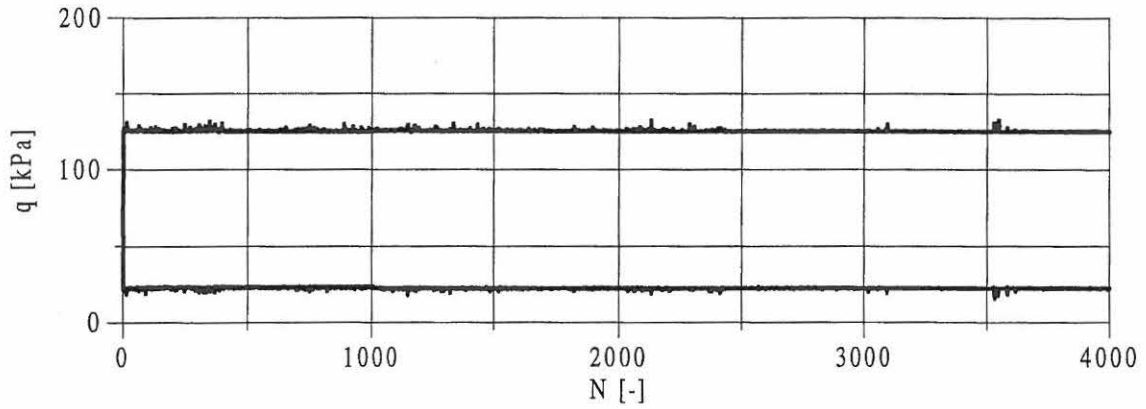
Evaluated: KPJ

Approved: KPJ



Remarks

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| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 3 |
| Evaluated: KPJ | Approved: KPJ |



Remarks

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|----------------|--------------------|
| Job: | Aalborg University |
| Executed: KPJ | Enclosure No. 3 |
| Evaluated: KPJ | Approved: KPJ |

| | | | |
|--|---------------------------------|-------------------|----------|
| Description of soil Eastern Scheldt Sand | Cyclic Triaxial Apparatus | Sample properties | |
| Specimen preparation Air pluviation | Calibration file Cal9802.dat | Height | 71.50 mm |
| Saturation procedure CO ₂ / Backpressure | Date 1998-02-01 | Diameter | 69.70 mm |
| | | Void ratio | 0.672 |
| | | B-value | 0.990 |

| | | | |
|--------------|---|-------------|---------|
| Test program | Isotropic compression, σ'_3 : | 10.0 - 85.6 | kPa |
| | Loading rate: | 5.0 | kPa/min |
| | Anisotropic compression, q_m : | 43.3 | kPa |
| | Loading rate: | 3.0 | kPa/min |
| | <input checked="" type="checkbox"/> Applied drained | | |
| | <input type="checkbox"/> Applied undrained | | |
| | Cyclic loading, q_{cyc} : | 28.6 | kPa |
| | Period: | 10.0 | s |

| | | | |
|-----------------------|--------------|-------|-----|
| Isotropic compression | | | |
| Confining pressure | σ'_3 | 85.6 | kPa |
| Pore pressure | u | 200.0 | kPa |
| Axial strain | ϵ_1 | 0.13 | % |
| Volumetric strain | ϵ_v | 0.42 | % |
| Void ratio | e | 0.665 | |

| | | | |
|-------------------------|--------------|-------|-----|
| Anisotropic compression | | | |
| Confining pressure | σ'_3 | 85.5 | kPa |
| Axial pressure | σ'_1 | 128.9 | kPa |
| Deviator stress | q | 43.4 | kPa |
| Mean normal stress | p' | 100.0 | kPa |
| Pore pressure | u | 200.0 | kPa |
| Axial strain | ϵ_1 | 0.21 | % |
| Volumetric strain | ϵ_v | 0.47 | % |
| Void ratio | e | 0.665 | |

| | |
|--------------------|--------------------|
| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 4 |
| Evaluated: KPJ | Approved: KPJ |

| Cyclic loading | | | | | | |
|----------------|---------------|--------------|--------------|------------------|-------------------|-----------------------|
| N | P'_m kPa | q_m kPa | u_p kPa | u_{cyc} kPa | ϵ_p % | ϵ_{cyc} % |
| 1 | 92.1 | 43.2 | 7.8 | 6.6 | 0.03 | 0.02 |
| 3 | 88.4 | 43.3 | 11.5 | 7.4 | 0.04 | 0.01 |
| 5 | 86.5 | 43.3 | 13.4 | 7.5 | 0.04 | 0.01 |
| 10 | 83.1 | 43.3 | 16.7 | 7.4 | 0.05 | 0.01 |
| 25 | 77.7 | 43.3 | 22.0 | 7.3 | 0.07 | 0.02 |
| 50 | 72.9 | 43.3 | 26.9 | 7.1 | 0.09 | 0.02 |
| 75 | 69.6 | 43.3 | 30.1 | 6.9 | 0.10 | 0.01 |
| 100 | 67.1 | 43.3 | 32.6 | 6.8 | 0.12 | 0.02 |
| 150 | 63.4 | 43.3 | 36.4 | 6.5 | 0.14 | 0.02 |
| 200 | 60.3 | 43.3 | 39.1 | 6.3 | 0.17 | 0.02 |
| 300 | 56.5 | 43.3 | 43.0 | 6.0 | 0.20 | 0.02 |
| 400 | 53.3 | 43.3 | 46.2 | 5.6 | 0.24 | 0.02 |
| 500 | 50.8 | 43.3 | 48.8 | 5.4 | 0.27 | 0.02 |
| 750 | 46.9 | 43.2 | 52.5 | 5.0 | 0.34 | 0.02 |
| 1000 | 45.2 | 43.2 | 54.4 | 4.7 | 0.40 | 0.02 |
| 1250 | 43.4 | 43.2 | 56.2 | 4.4 | 0.45 | 0.02 |
| 1500 | 41.9 | 43.1 | 57.6 | 4.3 | 0.49 | 0.02 |
| 1750 | 41.1 | 43.1 | 58.5 | 4.2 | 0.53 | 0.02 |
| 2000 | 40.7 | 43.1 | 58.9 | 4.2 | 0.56 | 0.02 |
| 2250 | 40.0 | 43.1 | 59.4 | 4.1 | 0.58 | 0.02 |
| 2500 | 39.5 | 43.1 | 59.9 | 4.0 | 0.61 | 0.02 |
| 3000 | 38.9 | 43.1 | 60.5 | 3.9 | 0.64 | 0.02 |
| 3500 | 39.1 | 43.1 | 60.2 | 3.9 | 0.67 | 0.02 |
| 4000 | 39.0 | 43.1 | 59.9 | 3.8 | 0.69 | 0.02 |

Remarks:

Job: Ph.D. Project

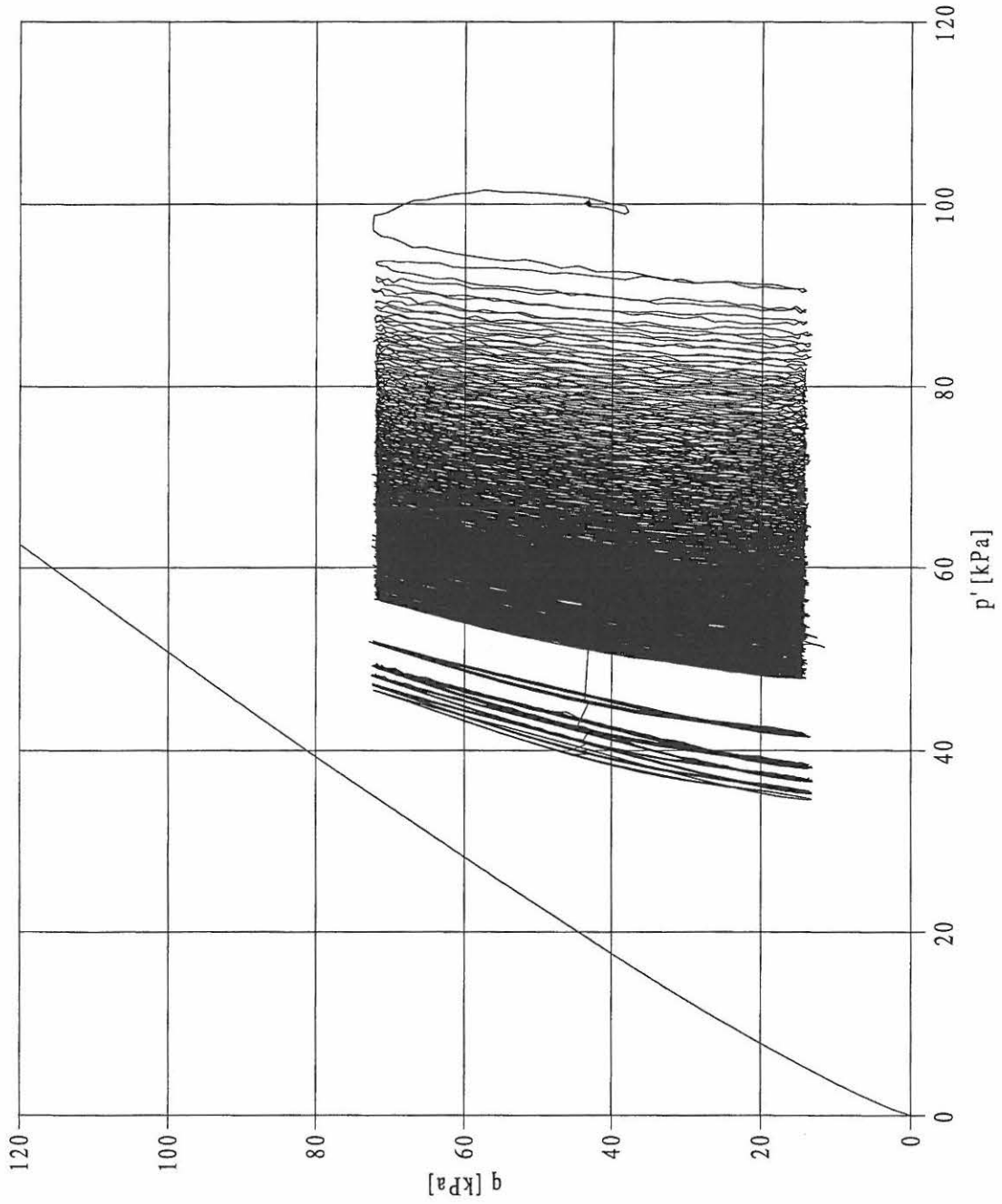
Aalborg University

Executed: KPJ

Enclosure No. 4

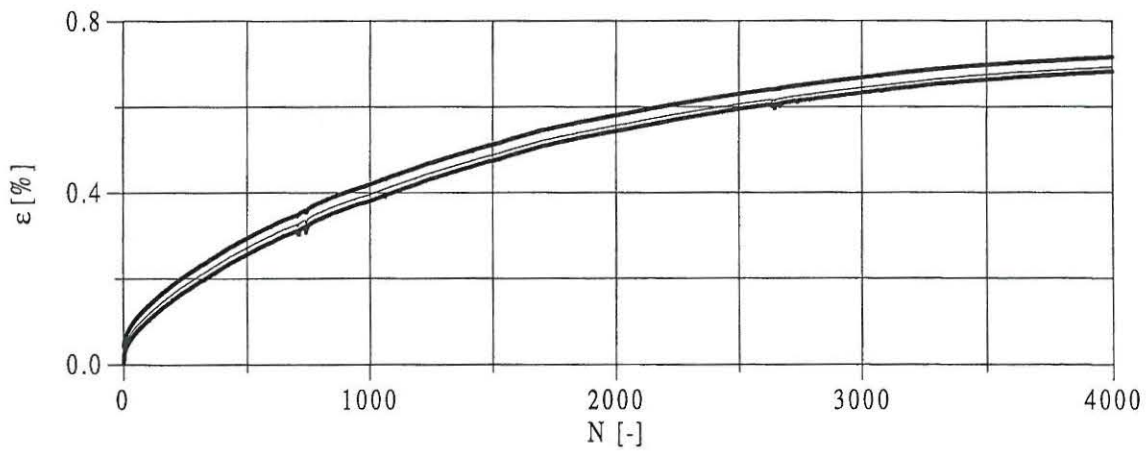
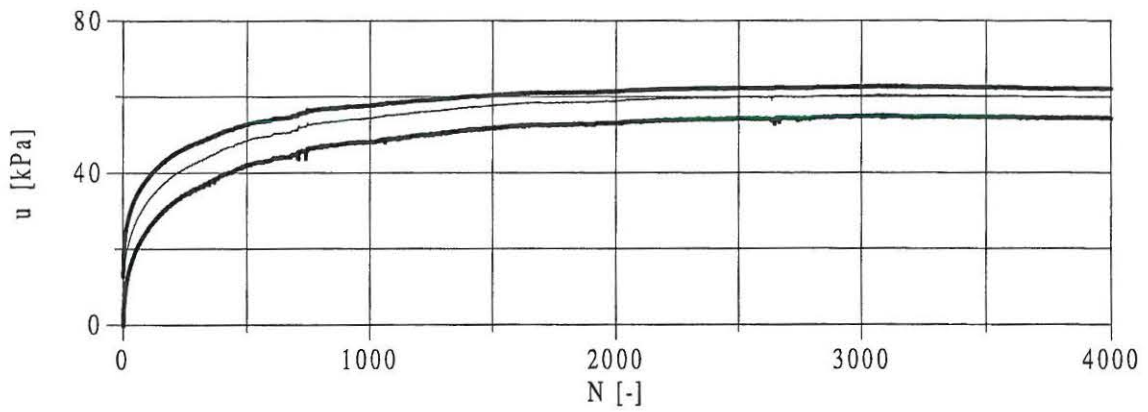
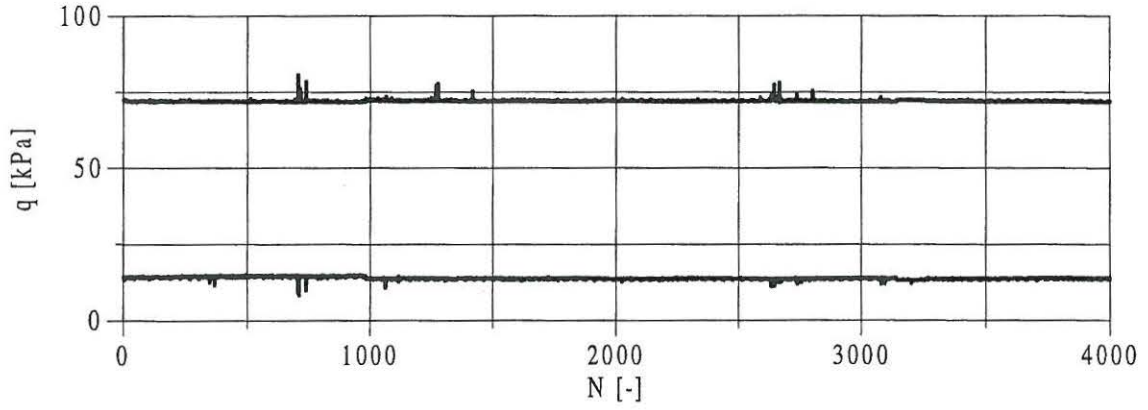
Evaluated: KPJ

Approved: KPJ



Remarks

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| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 4 |
| Evaluated: KPJ | Approved: KPJ |



Remarks

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| Job: | Aalborg University |
| Executed: KPJ | Enclosure No. 4 |
| Evaluated: KPJ | Approved: KPJ |

| | | | |
|--|---------------------------------|-------------------|----------|
| Description of soil Eastern Scheldt Sand | Cyclic Triaxial Apparatus | Sample properties | |
| Specimen preparation Air pluviation | Calibration file Cal9802.dat | Height | 71.50 mm |
| Saturation procedure CO ₂ / Backpressure | Date 1998-02-02 | Diameter | 69.70 mm |
| | | Void ratio | 0.672 |
| | | B-value | 0.977 |

| | | | |
|--------------|---|-------------|---------|
| Test program | Isotropic compression, σ'_3 : | 10.0 - 75.0 | kPa |
| | Loading rate: | 5.0 | kPa/min |
| | Anisotropic compression, q_m : | 75.0 | kPa |
| | Loading rate: | 3.0 | kPa/min |
| | <input checked="" type="checkbox"/> Applied drained | | |
| | <input type="checkbox"/> Applied undrained | | |
| | Cyclic loading, q_{cyc} : | 67.5 | kPa |
| | Period: | 10.0 | s |

| | | | |
|-----------------------|--------------|-------|-----|
| Isotropic compression | | | |
| Confining pressure | σ'_3 | 75.2 | kPa |
| Pore pressure | u | 200.0 | kPa |
| Axial strain | ϵ_1 | 0.11 | % |
| Volumetric strain | ϵ_v | 0.37 | % |
| Void ratio | e | 0.666 | |

| | | | |
|-------------------------|--------------|-------|-----|
| Anisotropic compression | | | |
| Confining pressure | σ'_3 | 74.9 | kPa |
| Axial pressure | σ'_1 | 150.0 | kPa |
| Deviator stress | q | 75.1 | kPa |
| Mean normal stress | p' | 100.0 | kPa |
| Pore pressure | u | 200.0 | kPa |
| Axial strain | ϵ_1 | 0.26 | % |
| Volumetric strain | ϵ_v | 0.47 | % |
| Void ratio | e | 0.664 | |

| | |
|--------------------|--------------------|
| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 5 |
| Evaluated: KPJ | Approved: KPJ |

| Cyclic loading | | | | | | |
|----------------|---------------|--------------|--------------|------------------|-------------------|-----------------------|
| N | P'_m kPa | q_m kPa | u_p kPa | u_{cyc} kPa | ϵ_p % | ϵ_{cyc} % |
| 1 | 78.6 | 75.0 | 21.1 | 11.4 | 0.23 | 0.14 |
| 3 | 73.0 | 74.9 | 26.7 | 8.8 | 0.32 | 0.05 |
| 5 | 70.7 | 74.8 | 29.3 | 8.8 | 0.39 | 0.05 |
| 10 | 66.9 | 74.8 | 32.8 | 8.5 | 0.50 | 0.05 |
| 25 | 63.8 | 74.6 | 36.0 | 8.1 | 0.71 | 0.05 |
| 50 | 62.5 | 74.4 | 37.3 | 8.0 | 0.92 | 0.04 |
| 75 | 61.3 | 74.4 | 38.4 | 7.9 | 1.06 | 0.04 |
| 100 | 61.0 | 74.3 | 38.7 | 7.8 | 1.17 | 0.04 |
| 150 | 59.3 | 74.1 | 40.4 | 7.8 | 1.33 | 0.04 |
| 200 | 60.1 | 74.0 | 39.7 | 7.8 | 1.46 | 0.04 |
| 300 | 57.9 | 73.9 | 41.8 | 8.1 | 1.65 | 0.05 |
| 400 | 59.0 | 73.8 | 40.6 | 7.7 | 1.81 | 0.04 |
| 500 | 58.6 | 73.7 | 41.0 | 7.7 | 1.93 | 0.04 |
| 750 | 58.2 | 73.5 | 41.3 | 7.7 | 2.15 | 0.04 |
| 1000 | 58.8 | 73.4 | 41.1 | 7.8 | 2.31 | 0.04 |
| 1250 | 58.4 | 73.3 | 41.4 | 7.9 | 2.43 | 0.04 |
| 1500 | 58.6 | 73.2 | 41.2 | 7.7 | 2.52 | 0.04 |
| 1750 | 58.4 | 73.2 | 41.3 | 7.9 | 2.60 | 0.04 |
| 2000 | 59.1 | 73.1 | 40.9 | 8.0 | 2.67 | 0.04 |
| 2250 | 58.8 | 73.0 | 41.1 | 7.8 | 2.72 | 0.04 |
| 2500 | 58.4 | 73.0 | 41.6 | 8.0 | 2.79 | 0.04 |
| 3000 | 57.8 | 72.9 | 41.8 | 8.1 | 2.89 | 0.04 |
| 3500 | 58.4 | 72.9 | 41.5 | 8.0 | 2.97 | 0.04 |
| 4000 | 57.6 | 72.8 | 41.9 | 8.1 | 3.04 | 0.04 |
| 4500 | 58.1 | 72.8 | 41.8 | 8.3 | 3.09 | 0.04 |
| 5000 | 57.7 | 72.7 | 42.3 | 8.1 | 3.16 | 0.04 |
| 5500 | 58.0 | 72.7 | 42.1 | 8.0 | 3.20 | 0.04 |
| 6000 | 55.9 | 72.6 | 44.3 | 8.2 | 3.25 | 0.04 |

Remarks:

Job: Ph.D. Project

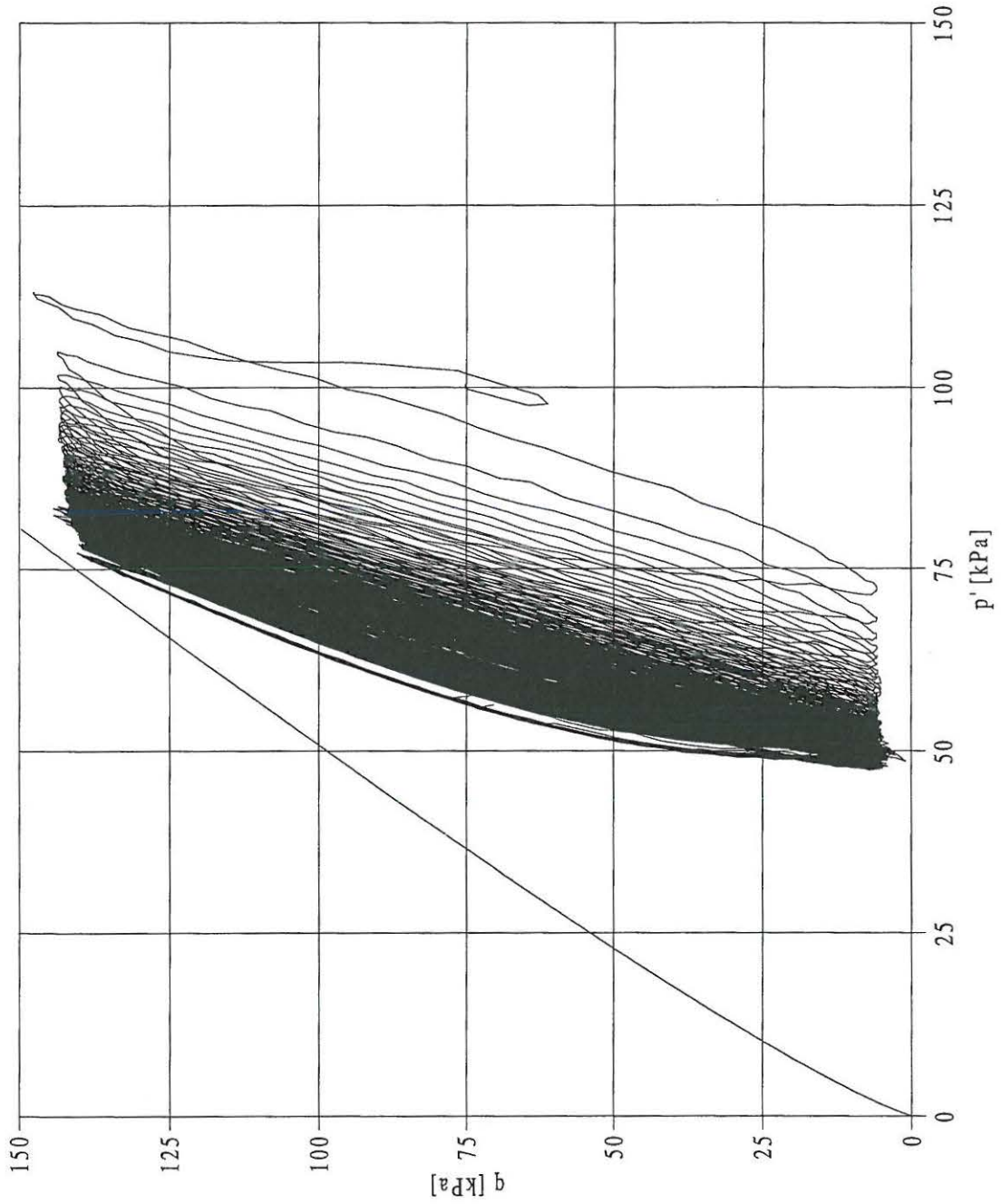
Aalborg University

Executed: KPJ

Enclosure No. 5

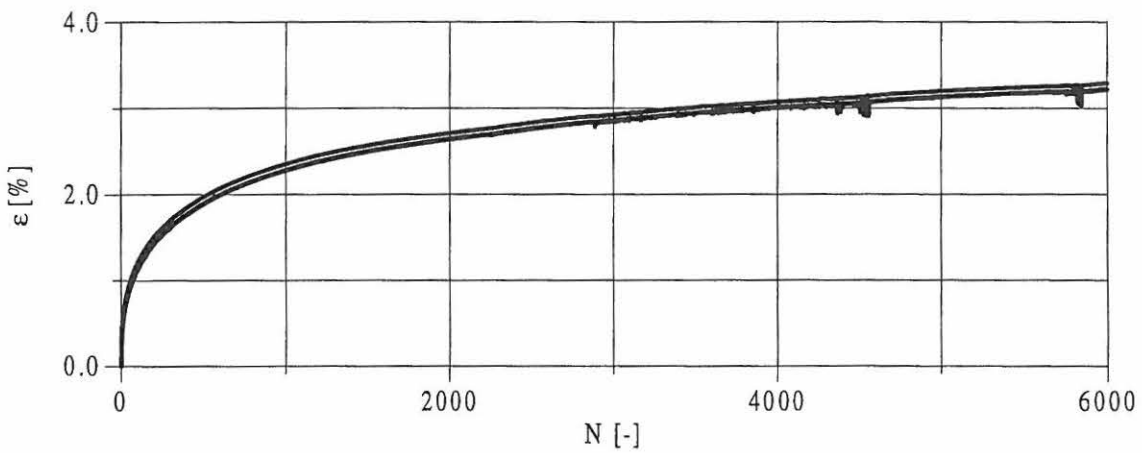
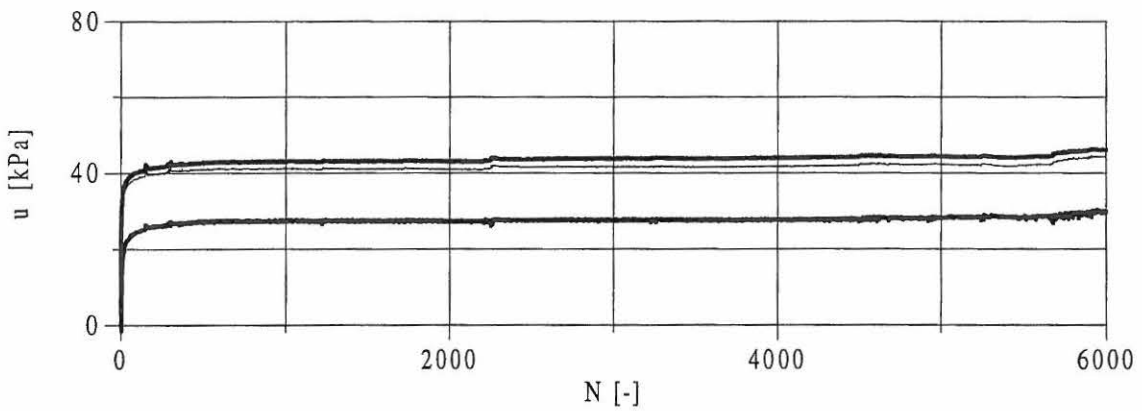
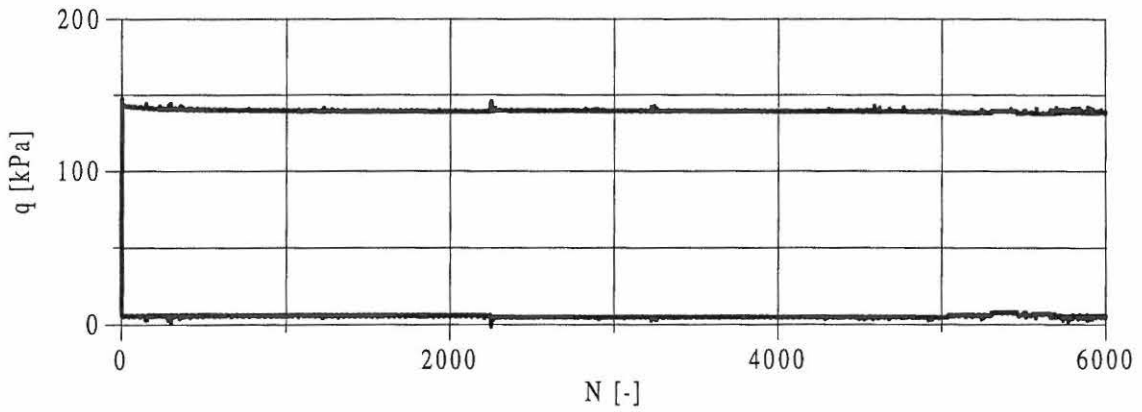
Evaluated: KPJ

Approved: KPJ



Remarks

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| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 5 |
| Evaluated: KPJ | Approved: KPJ |



Remarks

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| Job: | Aalborg University |
| Executed: KPJ | Enclosure No. 5 |
| Evaluated: KPJ | Approved: KPJ |

| | | | |
|--|---------------------------------|-------------------|----------|
| Description of soil Eastern Scheldt Sand | Cyclic Triaxial Apparatus | Sample properties | |
| Specimen preparation Air pluviation | Calibration file Cal9802.dat | Height | 71.47 mm |
| Saturation procedure CO ₂ / Backpressure | Date 1998-02-03 | Diameter | 69.67 mm |
| | | Void ratio | 0.670 |
| | | B-value | 0.986 |

| | | | |
|--------------|---|--------------|---------|
| Test program | Isotropic compression, σ_3 : | 10.0 - 175.0 | kPa |
| | Loading rate: | 5.0 | kPa/min |
| | Anisotropic compression, q_m : | 75.0 | kPa |
| | Loading rate: | 3.0 | kPa/min |
| | <input checked="" type="checkbox"/> Applied drained | | |
| | <input type="checkbox"/> Applied undrained | | |
| | Cyclic loading, q_{cyc} : | 67.5 | kPa |
| | Period: | 10.0 | s |

| | | | |
|-----------------------|--------------|-------|-----|
| Isotropic compression | | | |
| Confining pressure | σ_3 | 175.3 | kPa |
| Pore pressure | u | 200.0 | kPa |
| Axial strain | ϵ_1 | 0.18 | % |
| Volumetric strain | ϵ_v | 0.60 | % |
| Void ratio | e | 0.660 | |

| | | | |
|-------------------------|--------------|-------|-----|
| Anisotropic compression | | | |
| Confining pressure | σ_3 | 175.0 | kPa |
| Axial pressure | σ_1 | 250.4 | kPa |
| Deviator stress | q | 75.4 | kPa |
| Mean normal stress | p' | 200.1 | kPa |
| Pore pressure | u | 200.0 | kPa |
| Axial strain | ϵ_1 | 0.27 | % |
| Volumetric strain | ϵ_v | 0.67 | % |
| Void ratio | e | 0.659 | |

| | |
|--------------------|--------------------|
| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 6 |
| Evaluated: KPJ | Approved: KPJ |

| Cyclic loading | | | | | | |
|----------------|---------------|--------------|--------------|------------------|-------------------|-----------------------|
| N | P'_m kPa | q_m kPa | u_p kPa | u_{cyc} kPa | ϵ_p % | ϵ_{cyc} % |
| 1 | 170.8 | 75.1 | 29.3 | 19.9 | 0.06 | 0.04 |
| 3 | 158.0 | 75.1 | 42.1 | 16.0 | 0.08 | 0.02 |
| 5 | 150.0 | 75.1 | 50.0 | 16.1 | 0.09 | 0.02 |
| 10 | 137.0 | 75.1 | 62.8 | 16.0 | 0.12 | 0.03 |
| 25 | 116.2 | 75.1 | 83.7 | 14.7 | 0.17 | 0.03 |
| 50 | 98.1 | 75.0 | 102.0 | 13.1 | 0.26 | 0.03 |
| 75 | 88.4 | 74.9 | 111.8 | 11.8 | 0.36 | 0.03 |
| 100 | 82.6 | 74.8 | 117.6 | 11.0 | 0.44 | 0.03 |
| 150 | 76.5 | 74.7 | 123.8 | 10.2 | 0.59 | 0.03 |
| 200 | 73.1 | 74.6 | 127.0 | 9.8 | 0.71 | 0.03 |
| 300 | 70.4 | 74.5 | 129.9 | 9.2 | 0.89 | 0.03 |
| 400 | 68.5 | 74.4 | 131.6 | 9.0 | 1.02 | 0.03 |
| 500 | 67.9 | 74.3 | 132.4 | 9.0 | 1.13 | 0.03 |
| 750 | 67.1 | 74.1 | 133.4 | 8.7 | 1.32 | 0.03 |
| 1000 | 66.6 | 74.0 | 133.9 | 8.6 | 1.44 | 0.02 |
| 1250 | 66.1 | 73.9 | 134.5 | 8.7 | 1.55 | 0.02 |
| 1500 | 66.1 | 73.9 | 134.5 | 8.6 | 1.63 | 0.02 |
| 1750 | 66.2 | 73.8 | 134.6 | 8.8 | 1.69 | 0.02 |
| 2000 | 66.4 | 73.8 | 134.6 | 8.7 | 1.74 | 0.02 |
| 2250 | 65.5 | 73.8 | 135.1 | 8.7 | 1.78 | 0.02 |
| 2500 | 65.3 | 73.7 | 135.2 | 8.7 | 1.82 | 0.02 |
| 3000 | 64.9 | 73.7 | 135.4 | 8.8 | 1.87 | 0.02 |
| 3500 | 64.7 | 73.7 | 135.7 | 8.9 | 1.91 | 0.02 |
| 4000 | 63.8 | 73.7 | 136.2 | 9.0 | 1.95 | 0.02 |
| 4500 | 63.1 | 73.7 | 136.8 | 9.0 | 1.98 | 0.02 |
| 5000 | 62.5 | 73.7 | 137.3 | 9.1 | 2.00 | 0.02 |
| 5500 | 61.3 | 73.7 | 138.2 | 9.0 | 2.03 | 0.02 |
| 6000 | 59.4 | 73.6 | 140.2 | 9.1 | 2.05 | 0.02 |

Remarks:

Job: Ph.D. Project

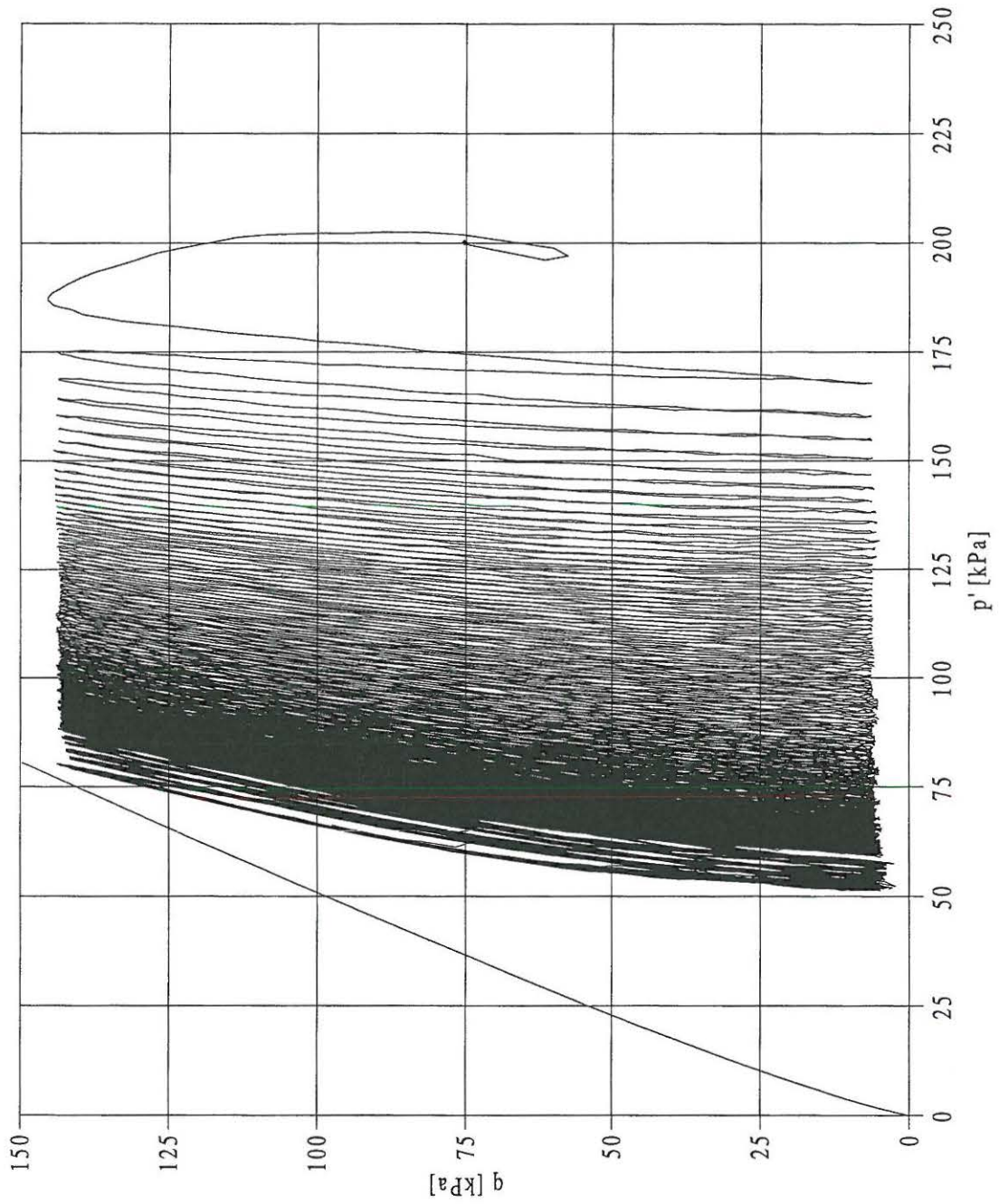
Aalborg University

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Enclosure No. 6

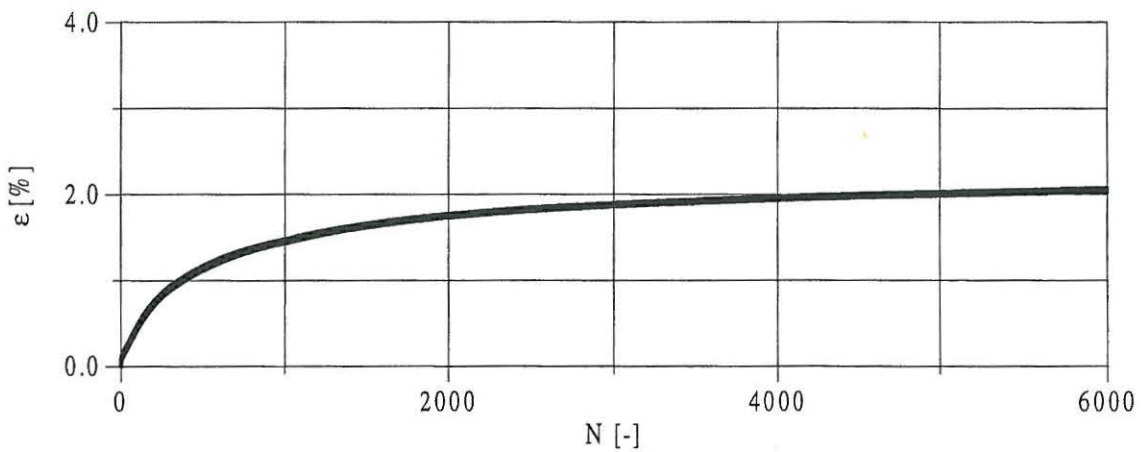
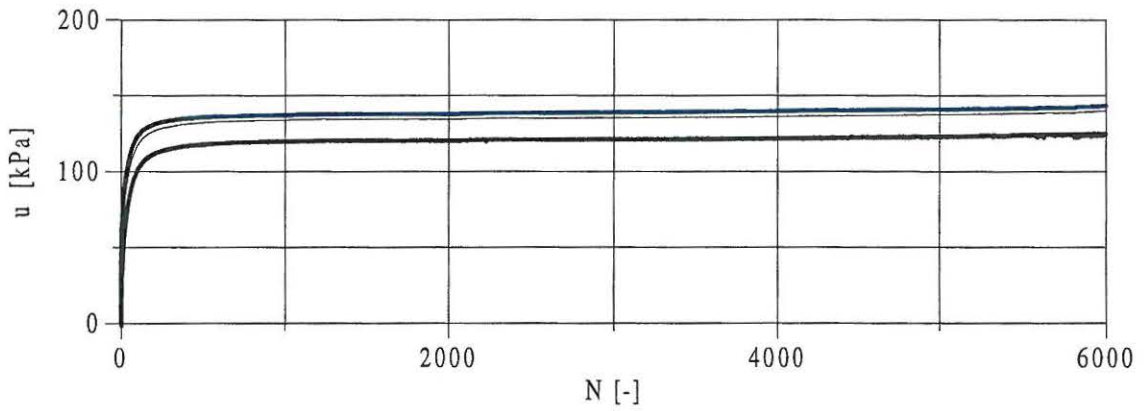
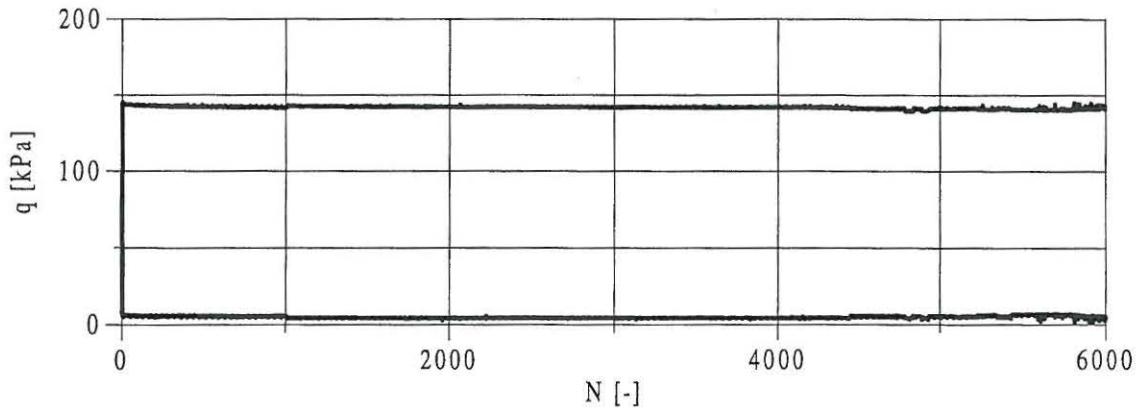
Evaluated: KPJ

Approved: KPJ



Remarks

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| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 6 |
| Evaluated: KPJ | Approved: KPJ |



Remarks

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| Job: | Aalborg University |
| Executed: KPJ | Enclosure No. 6 |
| Evaluated: KPJ | Approved: KPJ |

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|--|---------------------------------|-------------------|----------|
| Description of soil Eastern Scheldt Sand | Cyclic Triaxial Apparatus | Sample properties | |
| Specimen preparation Air pluviation | Calibration file Cal9802.dat | Height | 71.48 mm |
| Saturation procedure CO ₂ / Backpressure | Date 1998-02-04 | Diameter | 69.68 mm |
| | | Void ratio | 0.671 |
| | | B-value | 0.980 |

| | | | |
|--------------|---|-------------|---------|
| Test program | Isotropic compression, σ'_3 : | 10.0 - 25.0 | kPa |
| | Loading rate: | 5.0 | kPa/min |
| | Anisotropic compression, q_m : | 75.0 | kPa |
| | Loading rate: | 3.0 | kPa/min |
| | <input checked="" type="checkbox"/> Applied drained | | |
| | <input type="checkbox"/> Applied undrained | | |
| | Cyclic loading, q_{cyc} : | 25.0 | kPa |
| Period: | 10.0 | s | |

| | | | |
|-----------------------|--------------|-------|-----|
| Isotropic compression | | | |
| Confining pressure | σ'_3 | 25.1 | kPa |
| Pore pressure | u | 200.0 | kPa |
| Axial strain | ϵ_1 | 0.06 | % |
| Volumetric strain | ϵ_v | 0.11 | % |
| Void ratio | e | 0.670 | |

| | | | |
|-------------------------|--------------|-------|-----|
| Anisotropic compression | | | |
| Confining pressure | σ'_3 | 25.0 | kPa |
| Axial pressure | σ'_1 | 100.4 | kPa |
| Deviator stress | q | 75.4 | kPa |
| Mean normal stress | p' | 50.1 | kPa |
| Pore pressure | u | 200.0 | kPa |
| Axial strain | ϵ_1 | 0.82 | % |
| Volumetric strain | ϵ_v | 0.18 | % |
| Void ratio | e | 0.668 | |

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| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 7 |
| Evaluated: KPJ | Approved: KPJ |

| Cyclic loading | | | | | | |
|----------------|---------------|--------------|--------------|------------------|-------------------|-----------------------|
| N | P'_m kPa | q_m kPa | u_p kPa | u_{cyc} kPa | ϵ_p % | ϵ_{cyc} % |
| 1 | 56.0 | 75.3 | -6.0 | 4.5 | 0.11 | 0.06 |
| 3 | 57.0 | 75.3 | -7.0 | 2.2 | 0.14 | 0.01 |
| 5 | 57.3 | 75.2 | -7.2 | 2.2 | 0.16 | 0.01 |
| 10 | 57.7 | 75.2 | -7.7 | 2.2 | 0.20 | 0.01 |
| 25 | 58.0 | 75.1 | -8.0 | 2.3 | 0.25 | 0.01 |
| 50 | 58.1 | 75.1 | -8.2 | 2.4 | 0.29 | 0.01 |
| 75 | 58.1 | 75.1 | -8.1 | 2.4 | 0.31 | 0.01 |
| 100 | 58.1 | 75.1 | -8.1 | 2.4 | 0.33 | 0.01 |
| 150 | 58.3 | 75.0 | -8.3 | 2.4 | 0.36 | 0.01 |
| 200 | 58.4 | 74.9 | -8.4 | 2.4 | 0.38 | 0.01 |
| 300 | 58.6 | 74.9 | -8.6 | 2.4 | 0.40 | 0.01 |
| 400 | 58.8 | 74.9 | -8.8 | 2.5 | 0.41 | 0.01 |
| 500 | 59.2 | 74.9 | -9.0 | 2.5 | 0.42 | 0.01 |
| 750 | 60.2 | 74.9 | -9.8 | 2.6 | 0.44 | 0.01 |
| 1000 | 61.1 | 74.9 | -10.5 | 2.6 | 0.46 | 0.01 |
| 1250 | 62.4 | 74.9 | -11.6 | 2.7 | 0.47 | 0.01 |
| 1500 | 63.3 | 74.9 | -12.4 | 2.7 | 0.47 | 0.01 |
| 1750 | 63.7 | 74.9 | -12.6 | 2.7 | 0.48 | 0.01 |
| 2000 | 64.5 | 74.9 | -13.4 | 2.8 | 0.49 | 0.01 |
| 2250 | 65.3 | 74.9 | -14.0 | 2.8 | 0.49 | 0.01 |
| 2500 | 66.0 | 74.9 | -14.6 | 2.8 | 0.49 | 0.01 |
| 3000 | 65.7 | 74.9 | -15.0 | 2.9 | 0.50 | 0.01 |
| 3500 | 66.7 | 74.9 | -15.9 | 3.0 | 0.50 | 0.01 |
| 4000 | 66.9 | 74.9 | -16.2 | 3.0 | 0.50 | 0.01 |

Remarks:

Job: Ph.D. Project

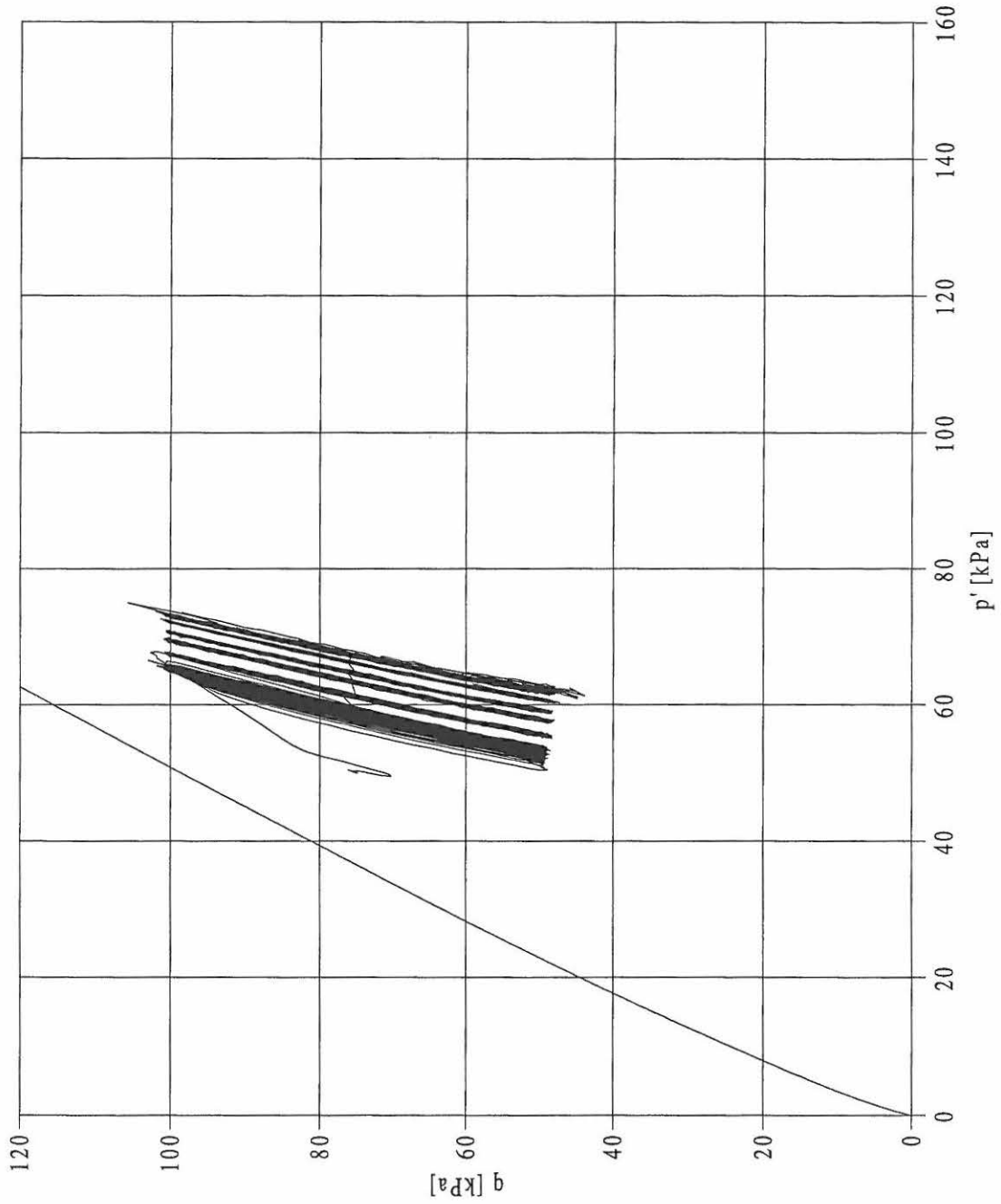
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Enclosure No. 7

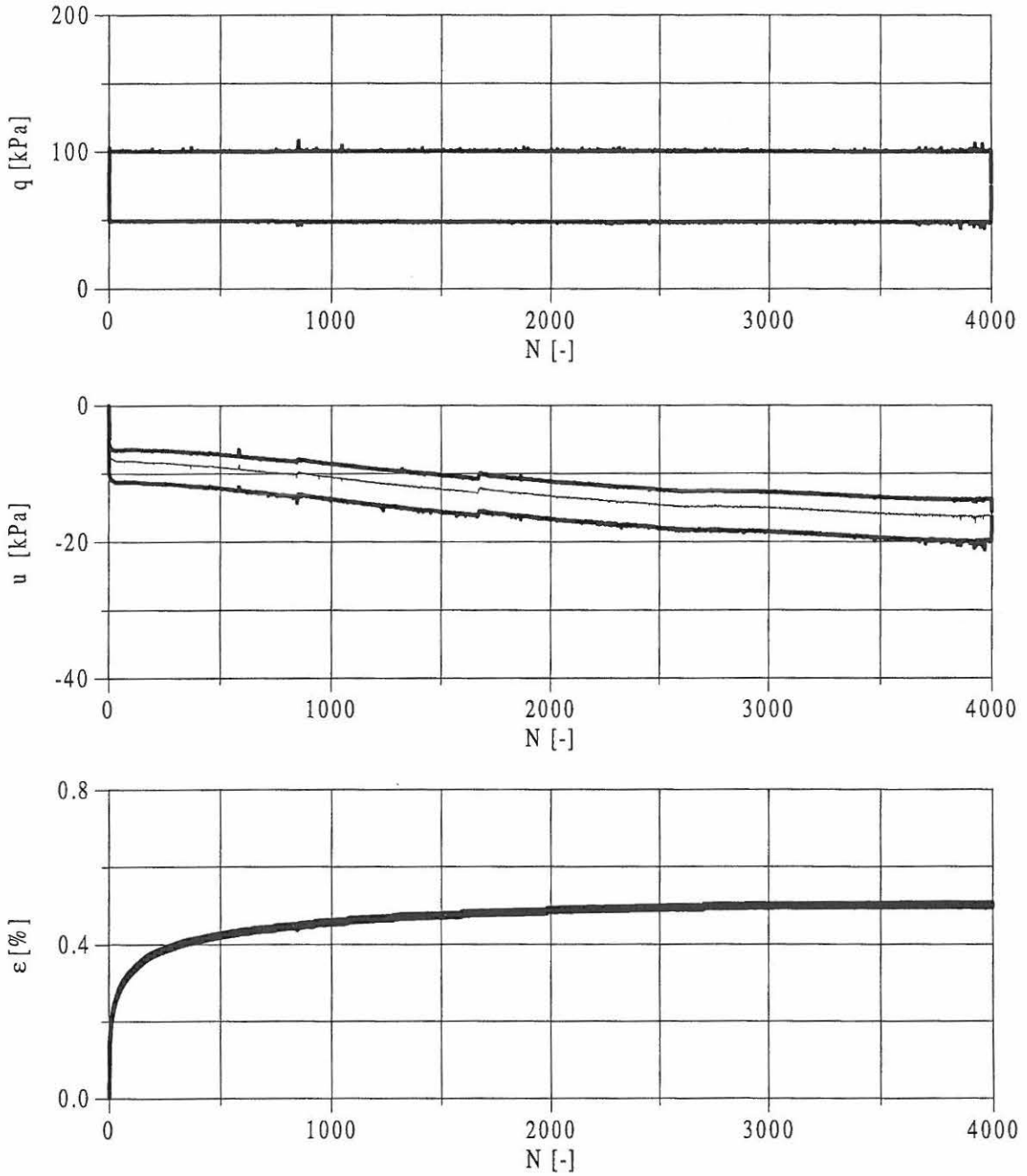
Evaluated: KPJ

Approved: KPJ



Remarks

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| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 7 |
| Evaluated: KPJ | Approved: KPJ |



Remarks

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|----------------|--------------------|
| Job: | Aalborg University |
| Executed: KPJ | Enclosure No. 7 |
| Evaluated: KPJ | Approved: KPJ |

| | | | |
|--|---------------------------------|-------------------|----------|
| Description of soil Eastern Scheldt Sand | Cyclic Triaxial Apparatus | Sample properties | |
| Specimen preparation Air pluviation | Calibration file Cal9802.dat | Height | 71.52 mm |
| Saturation procedure CO ₂ / Backpressure | Date 1998-02-05 | Diameter | 69.72 mm |
| | | Void ratio | 0.674 |
| | | B-value | 0.990 |

| | | | |
|--------------|---|--------------|---------|
| Test program | Isotropic compression, σ'_3 : | 10.0 - 175.0 | kPa |
| | Loading rate: | 5.0 | kPa/min |
| | Anisotropic compression, q_m : | 75.0 | kPa |
| | Loading rate: | 3.0 | kPa/min |
| | <input checked="" type="checkbox"/> Applied drained | | |
| | <input type="checkbox"/> Applied undrained | | |
| | Cyclic loading, q_{cyc} : | 100.0 | kPa |
| | Period: | 10.0 | s |

| | | | |
|-----------------------|--------------|-------|-----|
| Isotropic compression | | | |
| Confining pressure | σ'_3 | 175.1 | kPa |
| Pore pressure | u | 200.0 | kPa |
| Axial strain | ϵ_1 | 0.20 | % |
| Volumetric strain | ϵ_v | 0.66 | % |
| Void ratio | e | 0.663 | |

| | | | |
|-------------------------|--------------|-------|-----|
| Anisotropic compression | | | |
| Confining pressure | σ'_3 | 175.0 | kPa |
| Axial pressure | σ'_1 | 249.7 | kPa |
| Deviator stress | q | 74.7 | kPa |
| Mean normal stress | p' | 199.9 | kPa |
| Pore pressure | u | 200.0 | kPa |
| Axial strain | ϵ_1 | 0.31 | % |
| Volumetric strain | ϵ_v | 0.75 | % |
| Void ratio | e | 0.662 | |

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| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 8 |
| Evaluated: KPJ | Approved: KPJ |

| Cyclic loading | | | | | | |
|----------------|---------------|--------------|--------------|------------------|-------------------|-----------------------|
| N | P'_m kPa | q_m kPa | u_p kPa | u_{cyc} kPa | ϵ_p % | ϵ_{cyc} % |
| 1 | 141.8 | 74.7 | 58.0 | 30.6 | 0.11 | 0.09 |
| 3 | 114.8 | 74.6 | 84.9 | 16.6 | 0.19 | 0.05 |
| 5 | 98.6 | 74.6 | 101.2 | 16.2 | 0.26 | 0.06 |
| 10 | 73.8 | 74.4 | 125.9 | 15.3 | 0.42 | 0.08 |
| 25 | 34.2 | 73.9 | 165.5 | 24.7 | 1.13 | 0.82 |
| 50 | 29.2 | 68.9 | 173.0 | 29.6 | 7.39 | 3.66 |

Remarks:

Job: Ph.D. Project

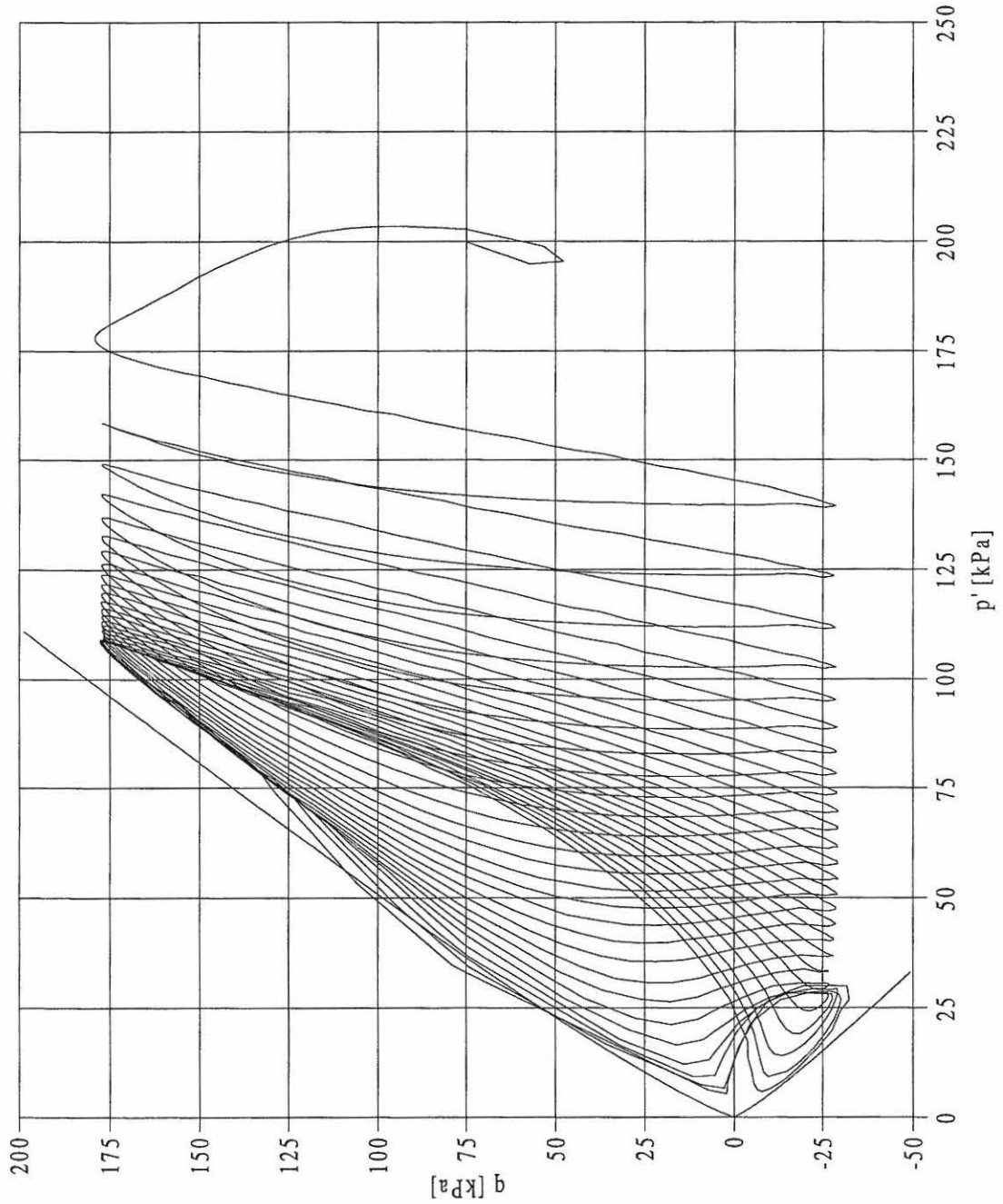
Aalborg University

Executed: KPJ

Enclosure No. 8

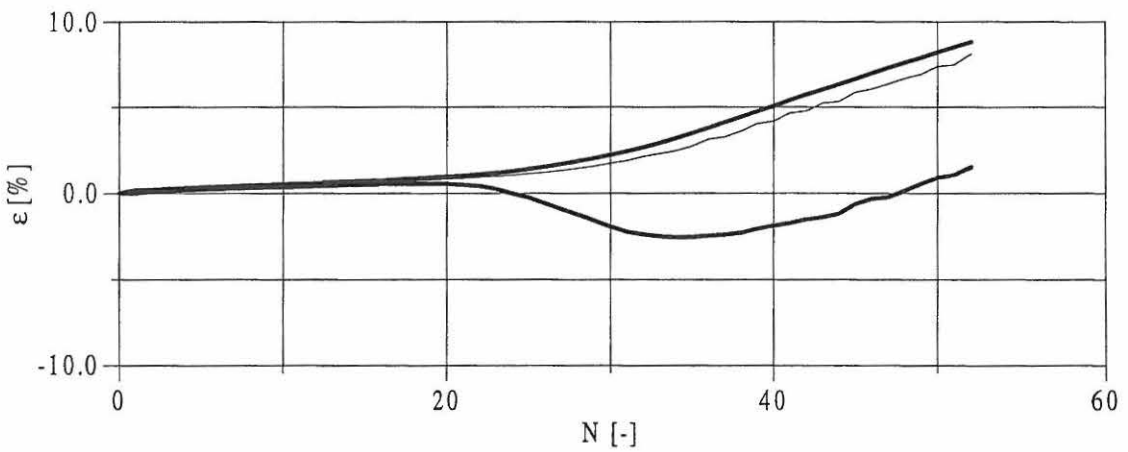
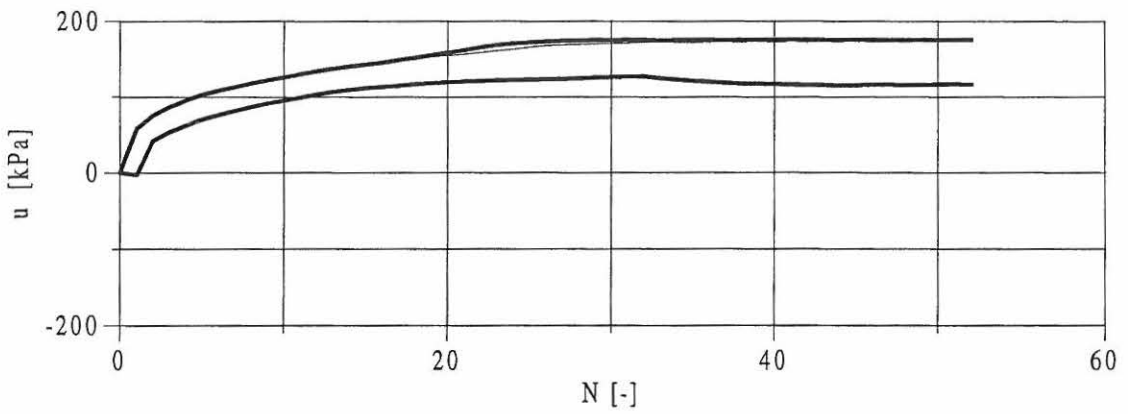
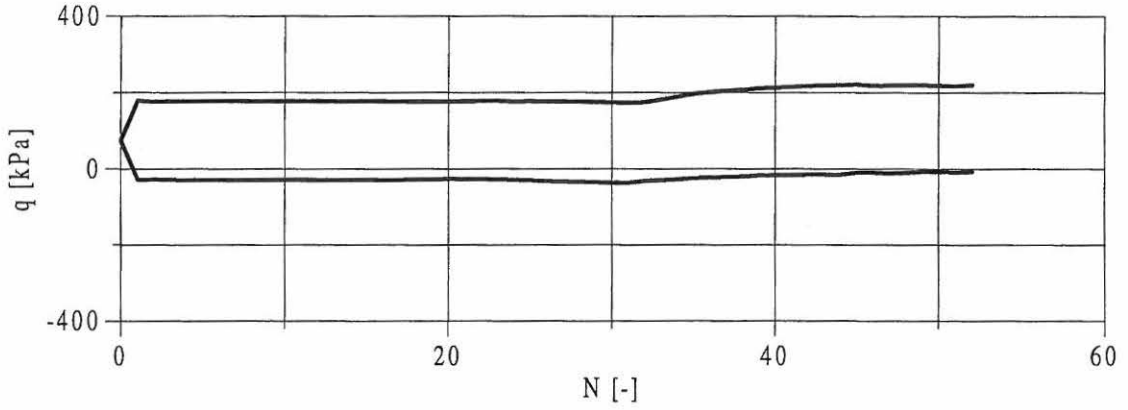
Evaluated: KPJ

Approved: KPJ



Remarks

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| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 8 |
| Evaluated: KPJ | Approved: KPJ |



Remarks

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| Job: | Aalborg University |
| Executed: KPJ | Enclosure No. 8 |
| Evaluated: KPJ | Approved: KPJ |

| | | | |
|--|---------------------------------|-------------------|----------|
| Description of soil Eastern Scheldt Sand | Cyclic Triaxial Apparatus | Sample properties | |
| Specimen preparation Air pluviation | Calibration file Cal9802.dat | Height | 71.43 mm |
| Saturation procedure CO ₂ / Backpressure | Date 1998-02-05 | Diameter | 69.63 mm |
| | | Void ratio | 0.666 |
| | | B-value | 0.993 |

| | | | |
|--------------|---|-------------|---------|
| Test program | Isotropic compression, σ'_3 : | 10.0 - 75.0 | kPa |
| | Loading rate: | 5.0 | kPa/min |
| | Anisotropic compression, q_m : | 75.0 | kPa |
| | Loading rate: | 3.0 | kPa/min |
| | <input checked="" type="checkbox"/> Applied drained | | |
| | <input type="checkbox"/> Applied undrained | | |
| | Cyclic loading, q_{cyc} : | 82.5 | kPa |
| | Period: | 10.0 | s |

| | | | |
|-----------------------|--------------|-------|-----|
| Isotropic compression | | | |
| Confining pressure | σ'_3 | 74.2 | kPa |
| Pore pressure | u | 201.3 | kPa |
| Axial strain | ϵ_1 | 0.01 | % |
| Volumetric strain | ϵ_v | 0.01 | % |
| Void ratio | e | 0.666 | |

| | | | |
|-------------------------|--------------|-------|-----|
| Anisotropic compression | | | |
| Confining pressure | σ'_3 | 73.6 | kPa |
| Axial pressure | σ'_1 | 149.1 | kPa |
| Deviator stress | q | 75.5 | kPa |
| Mean normal stress | p' | 98.8 | kPa |
| Pore pressure | u | 201.3 | kPa |
| Axial strain | ϵ_1 | 0.08 | % |
| Volumetric strain | ϵ_v | 0.06 | % |
| Void ratio | e | 0.665 | |

Remarks: Sample preconsolidated before test ($\sigma'_3 \approx 75$ kPa, $\sigma'_1 \approx 110$ kPa)

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| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 9 |
| Evaluated: KPJ | Approved: KPJ |

| Cyclic loading | | | | | | |
|----------------|---------------|--------------|--------------|------------------|-------------------|-----------------------|
| N | P'_m kPa | q_m kPa | u_p kPa | u_{cyc} kPa | ϵ_p % | ϵ_{cyc} % |
| 1 | 73.8 | 75.2 | 24.7 | 14.7 | 0.32 | 0.21 |
| 3 | 65.8 | 75.1 | 32.6 | 11.7 | 0.47 | 0.08 |
| 5 | 62.0 | 75.0 | 36.5 | 11.1 | 0.58 | 0.08 |
| 10 | 58.2 | 74.9 | 40.2 | 10.6 | 0.74 | 0.09 |
| 25 | 54.1 | 74.6 | 44.1 | 9.5 | 1.15 | 0.09 |
| 50 | 52.9 | 74.3 | 45.4 | 8.6 | 1.58 | 0.08 |
| 75 | 52.2 | 74.0 | 45.9 | 8.2 | 1.89 | 0.08 |
| 100 | 52.1 | 73.9 | 46.0 | 7.9 | 2.14 | 0.08 |
| 150 | 52.5 | 73.6 | 45.6 | 7.4 | 2.51 | 0.08 |
| 200 | 52.1 | 73.3 | 45.9 | 7.5 | 2.80 | 0.07 |
| 300 | 51.8 | 73.0 | 46.2 | 7.6 | 3.28 | 0.07 |
| 400 | 51.8 | 72.7 | 46.0 | 7.7 | 3.65 | 0.07 |
| 500 | 51.5 | 72.5 | 46.3 | 7.8 | 3.97 | 0.07 |
| 750 | 50.6 | 71.9 | 47.1 | 7.9 | 4.68 | 0.07 |
| 1000 | 50.1 | 71.5 | 47.6 | 8.1 | 5.23 | 0.07 |
| 1250 | 50.7 | 71.1 | 47.0 | 8.3 | 5.68 | 0.06 |
| 1500 | 50.7 | 70.8 | 47.0 | 8.5 | 6.08 | 0.06 |
| 1750 | 51.0 | 70.6 | 46.8 | 8.5 | 6.41 | 0.06 |
| 2000 | 51.0 | 70.3 | 46.8 | 8.8 | 6.70 | 0.06 |

Remarks:

Job: Ph.D. Project

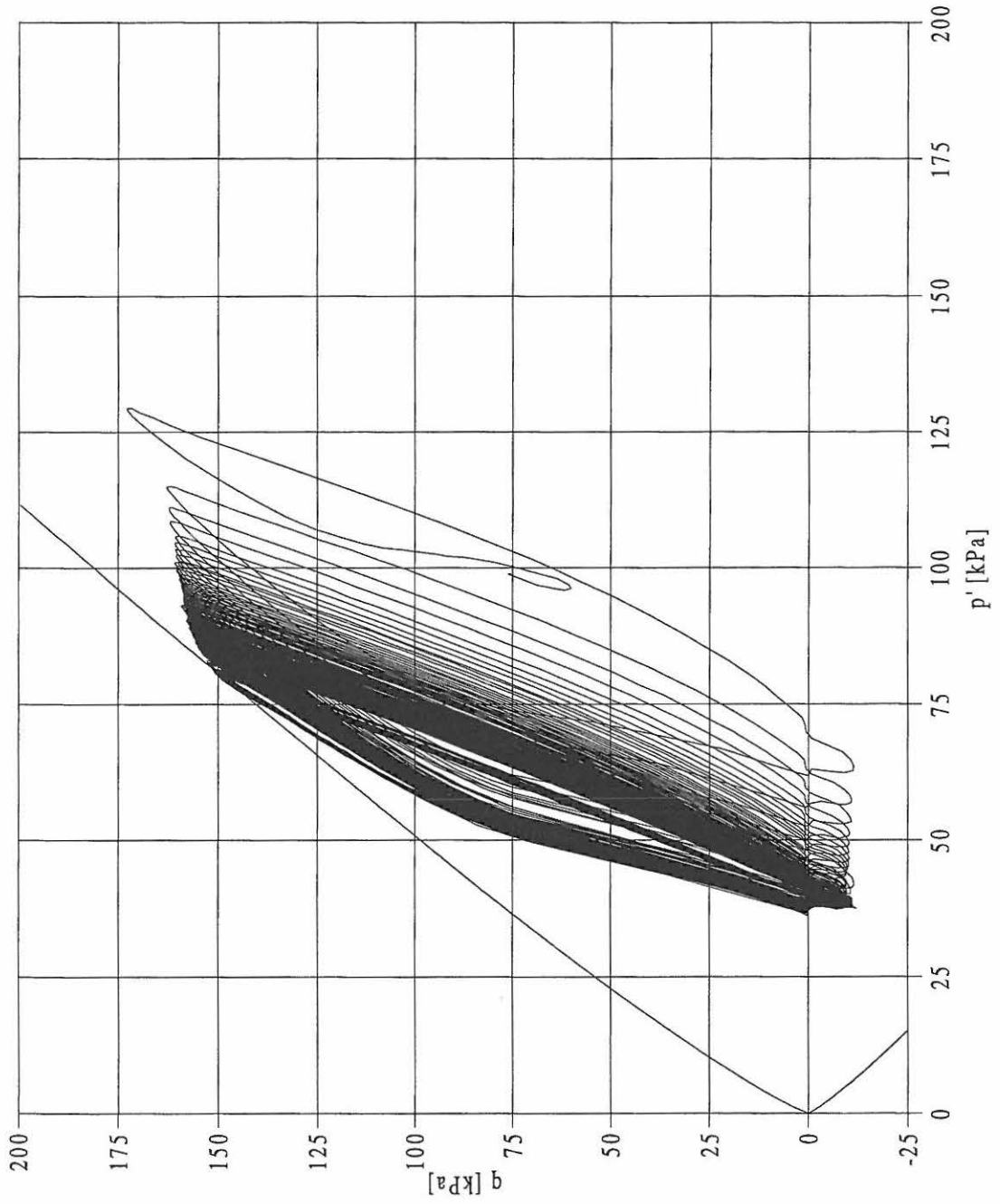
Aalborg University

Executed: KPJ

Enclosure No. 9

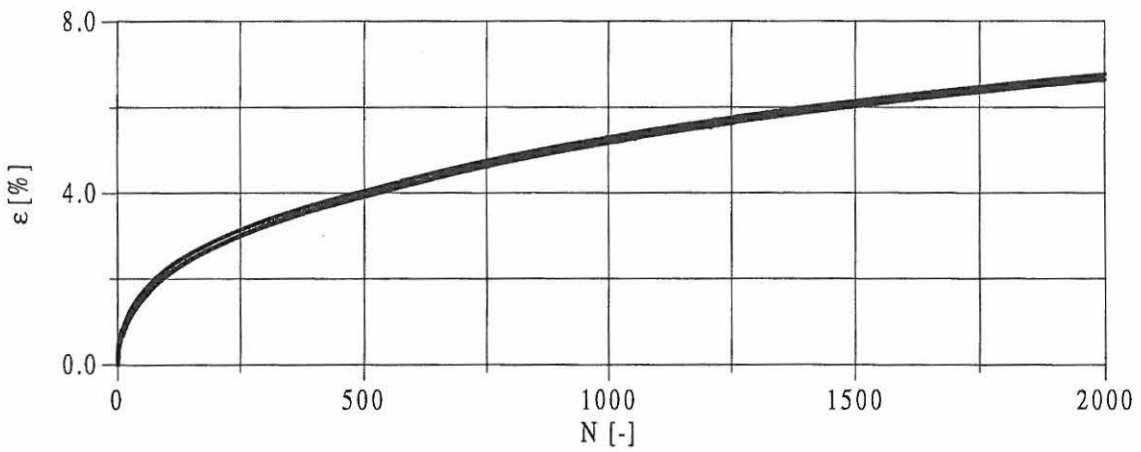
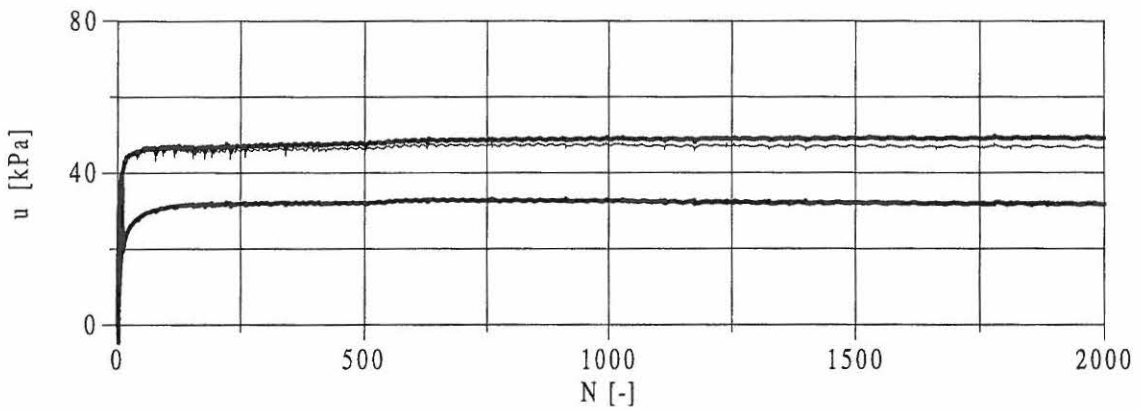
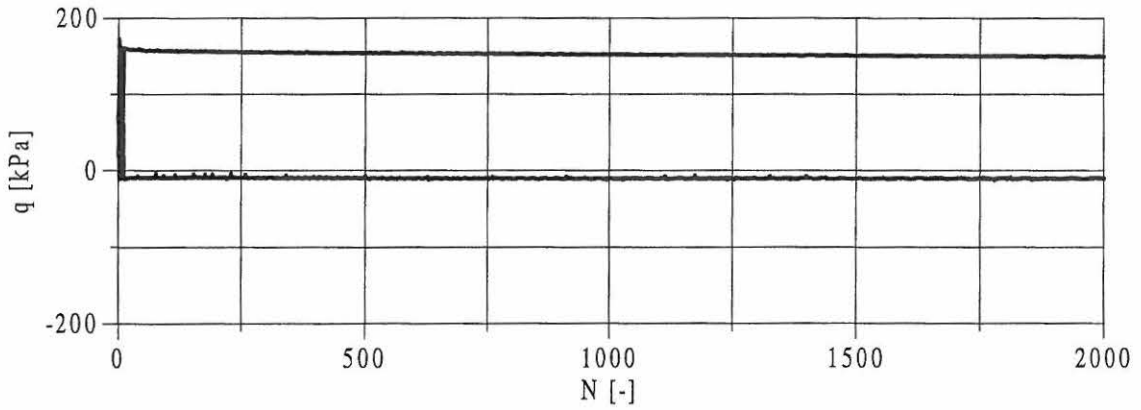
Evaluated: KPJ

Approved: KPJ



Remarks

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| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 9 |
| Evaluated: KPJ | Approved: KPJ |



Remarks

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| Job: | Aalborg University |
| Executed: KPJ | Enclosure No. 9 |
| Evaluated: KPJ | Approved: KPJ |

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|--|----------------------------------|-------------------|----------|
| Description of soil Eastern Scheldt Sand | Cyclic Triaxial Apparatus | Sample properties | |
| Specimen preparation Air pluviation | Calibration file Cal98021.dat | Height | 71.45 mm |
| Saturation procedure CO ₂ / Backpressure | Date 1998-02-06 | Diameter | 69.65 mm |
| | | Void ratio | 0.669 |
| | | B-value | 0.990 |

| | | | |
|--------------|---|-------------|---------|
| Test program | Isotropic compression, σ'_3 : | 10.0 - 49.5 | kPa |
| | Loading rate: | 5.0 | kPa/min |
| | Anisotropic compression, q_m : | 150.0 | kPa |
| | Loading rate: | 3.0 | kPa/min |
| | <input checked="" type="checkbox"/> Applied drained | | |
| | <input type="checkbox"/> Applied undrained | | |
| | Cyclic loading, q_{cyc} : | 22.5 | kPa |
| | Period: | 10.0 | s |

| | | | |
|-----------------------|--------------|-------|-----|
| Isotropic compression | | | |
| Confining pressure | σ'_3 | 49.4 | kPa |
| Pore pressure | u | 200.0 | kPa |
| Axial strain | ϵ_1 | 0.09 | % |
| Volumetric strain | ϵ_v | 0.26 | % |
| Void ratio | e | 0.665 | |

| | | | |
|-------------------------|--------------|-------|-----|
| Anisotropic compression | | | |
| Confining pressure | σ'_3 | 49.4 | kPa |
| Axial pressure | σ'_1 | 199.7 | kPa |
| Deviator stress | q | 150.3 | kPa |
| Mean normal stress | p' | 99.6 | kPa |
| Pore pressure | u | 199.9 | kPa |
| Axial strain | ϵ_1 | 1.22 | % |
| Volumetric strain | ϵ_v | 0.26 | % |
| Void ratio | e | 0.665 | |

| | |
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| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 10 |
| Evaluated: KPJ | Approved: KPJ |

| Cyclic loading | | | | | | |
|----------------|---------------|--------------|--------------|------------------|-------------------|-----------------------|
| N | p'_m kPa | q_m kPa | u_p kPa | u_{cyc} kPa | ϵ_p % | ϵ_{cyc} % |
| 1 | 105.7 | 150.3 | -6.1 | 4.8 | 0.04 | 0.02 |
| 3 | 106.8 | 150.3 | -7.3 | 2.5 | 0.06 | 0.01 |
| 5 | 107.3 | 150.2 | -7.6 | 2.5 | 0.07 | 0.01 |
| 10 | 108.0 | 150.2 | -8.3 | 2.6 | 0.09 | 0.00 |
| 25 | 108.2 | 150.2 | -8.6 | 2.6 | 0.11 | 0.00 |
| 50 | 108.6 | 150.2 | -9.1 | 2.6 | 0.13 | 0.00 |
| 75 | 108.6 | 150.1 | -8.9 | 2.6 | 0.14 | 0.00 |
| 100 | 108.6 | 150.1 | -9.0 | 2.6 | 0.15 | 0.00 |
| 150 | 108.7 | 150.1 | -9.2 | 2.6 | 0.16 | 0.00 |
| 200 | 109.1 | 150.1 | -9.3 | 2.6 | 0.17 | 0.00 |
| 300 | 109.5 | 150.1 | -9.7 | 2.6 | 0.19 | 0.00 |
| 400 | 109.7 | 150.1 | -9.9 | 2.6 | 0.19 | 0.00 |
| 500 | 110.1 | 150.0 | -10.3 | 2.7 | 0.20 | 0.00 |
| 750 | 111.0 | 150.0 | -11.2 | 2.7 | 0.21 | 0.00 |
| 1000 | 112.0 | 150.0 | -12.0 | 2.7 | 0.22 | 0.00 |
| 1250 | 113.1 | 150.0 | -12.9 | 2.7 | 0.23 | 0.00 |
| 1500 | 113.9 | 149.9 | -13.7 | 2.8 | 0.23 | 0.00 |
| 1750 | 114.8 | 149.9 | -14.4 | 2.7 | 0.24 | 0.00 |
| 2000 | 115.7 | 149.9 | -15.2 | 2.8 | 0.24 | 0.00 |
| 2250 | 116.6 | 149.9 | -16.0 | 2.8 | 0.24 | 0.00 |
| 2500 | 117.4 | 149.9 | -16.8 | 2.8 | 0.24 | 0.00 |
| 3000 | 118.9 | 149.9 | -18.1 | 2.9 | 0.25 | 0.00 |
| 3500 | 120.4 | 149.9 | -19.6 | 2.9 | 0.25 | 0.00 |

Remarks:

Job: Ph.D. Project

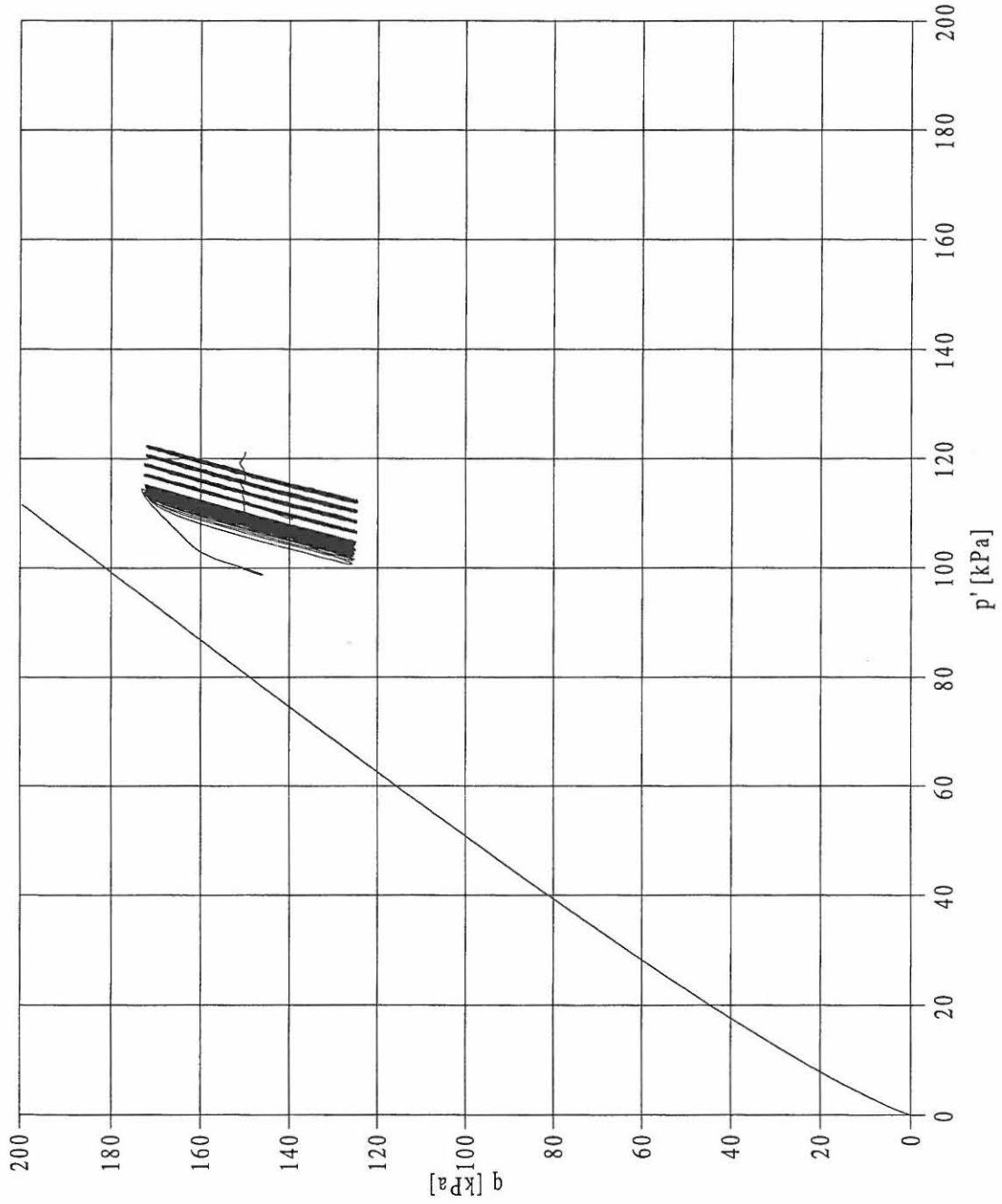
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Enclosure No. 10

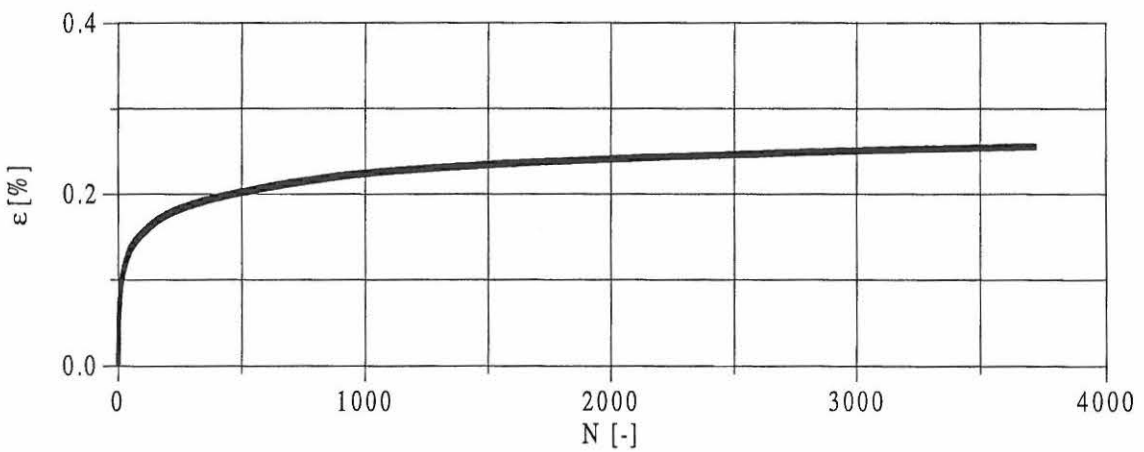
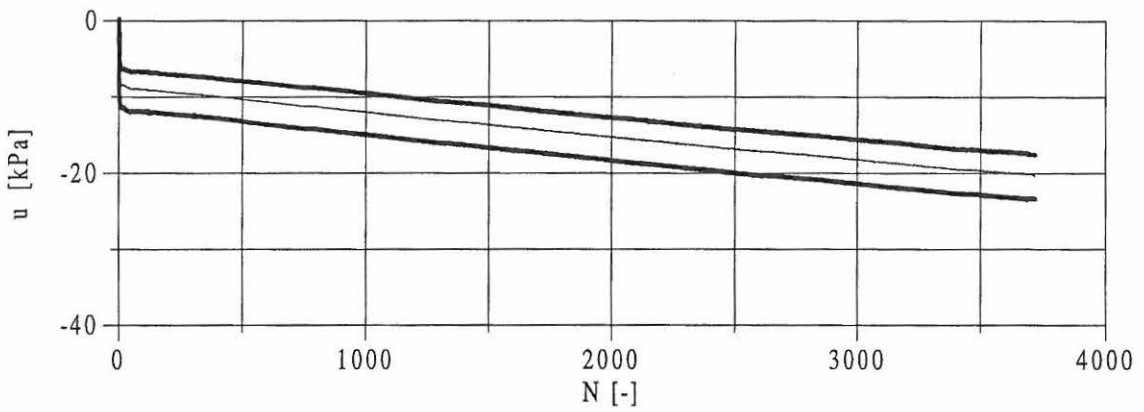
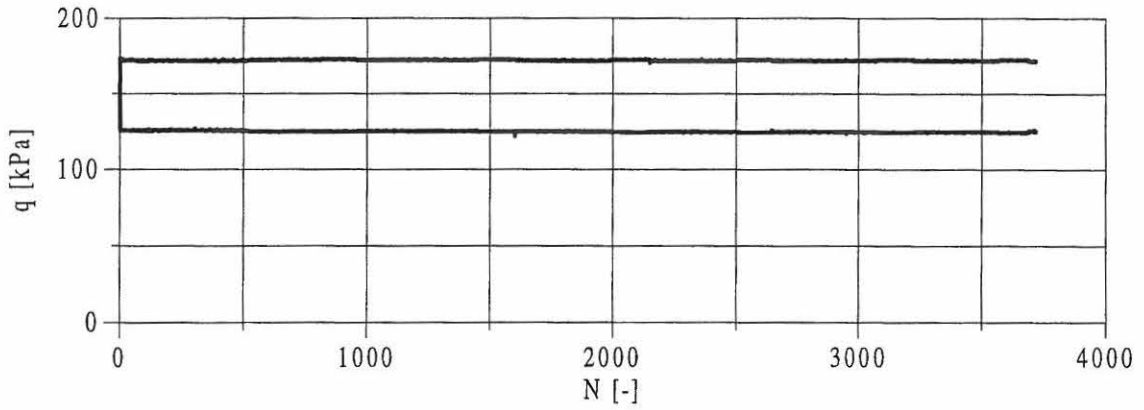
Evaluated: KPJ

Approved: KPJ



Remarks

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| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 10 |
| Evaluated: KPJ | Approved: KPJ |



Remarks

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| Job: | Aalborg University |
| Executed: KPJ | Enclosure No. 10 |
| Evaluated: KPJ | Approved: KPJ |

| | | | |
|--|----------------------------------|-------------------|----------|
| Description of soil Eastern Scheldt Sand | Cyclic Triaxial Apparatus | Sample properties | |
| Specimen preparation Air pluviation | Calibration file Cal98022.dat | Height | 71.50 mm |
| Saturation procedure CO ₂ / Backpressure | Date 1998-02-08 | Diameter | 69.70 mm |
| | | Void ratio | 0.672 |
| | | B-value | 0.997 |

| | | | |
|--------------|---|--------------|---------|
| Test program | Isotropic compression, σ'_3 : | 10.0 - 175.0 | kPa |
| | Loading rate: | 5.0 | kPa/min |
| | Anisotropic compression, q_m : | 75.9 | kPa |
| | Loading rate: | 3.0 | kPa/min |
| | <input checked="" type="checkbox"/> Applied drained | | |
| | <input type="checkbox"/> Applied undrained | | |
| | Cyclic loading, q_{cyc} : | 82.5 | kPa |
| | Period: | 10.0 | s |

| | | | |
|-----------------------|--------------|-------|-----|
| Isotropic compression | | | |
| Confining pressure | σ'_3 | 175.0 | kPa |
| Pore pressure | u | 200.0 | kPa |
| Axial strain | ϵ_1 | 0.19 | % |
| Volumetric strain | ϵ_v | 0.68 | % |
| Void ratio | e | 0.661 | |

| | | | |
|-------------------------|--------------|-------|-----|
| Anisotropic compression | | | |
| Confining pressure | σ'_3 | 175.0 | kPa |
| Axial pressure | σ'_1 | 250.8 | kPa |
| Deviator stress | q | 75.8 | kPa |
| Mean normal stress | p' | 200.3 | kPa |
| Pore pressure | u | 200.0 | kPa |
| Axial strain | ϵ_1 | 0.28 | % |
| Volumetric strain | ϵ_v | 0.76 | % |
| Void ratio | e | 0.659 | |

| | |
|--------------------|--------------------|
| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 11 |
| Evaluated: KPJ | Approved: KPJ |

| Cyclic loading | | | | | | |
|----------------|---------------|--------------|--------------|------------------|-------------------|-----------------------|
| N | P'_m kPa | q_m kPa | u_p kPa | u_{cyc} kPa | ϵ_p % | ϵ_{cyc} % |
| 1 | 161.6 | 75.7 | 38.5 | 22.4 | 0.07 | 0.06 |
| 3 | 142.6 | 75.6 | 57.6 | 17.3 | 0.11 | 0.04 |
| 5 | 130.3 | 75.6 | 69.9 | 16.8 | 0.14 | 0.04 |
| 10 | 108.5 | 75.6 | 91.6 | 15.4 | 0.21 | 0.05 |
| 25 | 74.0 | 75.3 | 126.1 | 11.8 | 0.50 | 0.06 |
| 50 | 58.0 | 75.0 | 142.0 | 10.0 | 0.99 | 0.07 |
| 75 | 53.5 | 74.7 | 146.3 | 9.7 | 1.36 | 0.08 |
| 100 | 51.6 | 74.5 | 148.3 | 9.2 | 1.66 | 0.08 |
| 150 | 49.7 | 74.1 | 150.0 | 8.9 | 2.15 | 0.08 |
| 200 | 47.7 | 73.8 | 152.0 | 8.8 | 2.57 | 0.08 |
| 300 | 46.1 | 73.2 | 153.4 | 8.5 | 3.26 | 0.08 |
| 400 | 45.7 | 72.8 | 153.8 | 8.7 | 3.81 | 0.08 |
| 500 | 45.4 | 72.5 | 154.1 | 8.7 | 4.26 | 0.08 |
| 750 | 44.2 | 71.7 | 155.0 | 8.9 | 5.20 | 0.08 |
| 1000 | 43.8 | 71.2 | 155.3 | 9.0 | 5.93 | 0.07 |
| 1250 | 43.4 | 70.7 | 155.5 | 9.2 | 6.53 | 0.07 |
| 1500 | 42.7 | 70.3 | 156.0 | 9.3 | 7.07 | 0.07 |
| 1750 | 42.2 | 70.0 | 156.4 | 9.4 | 7.53 | 0.07 |
| 2000 | 41.8 | 69.7 | 156.6 | 9.5 | 7.95 | 0.07 |
| 2250 | 41.0 | 69.4 | 157.2 | 9.5 | 8.36 | 0.07 |
| 2500 | 40.6 | 69.1 | 157.5 | 9.6 | 8.73 | 0.07 |

Remarks:

Job: Ph.D. Project

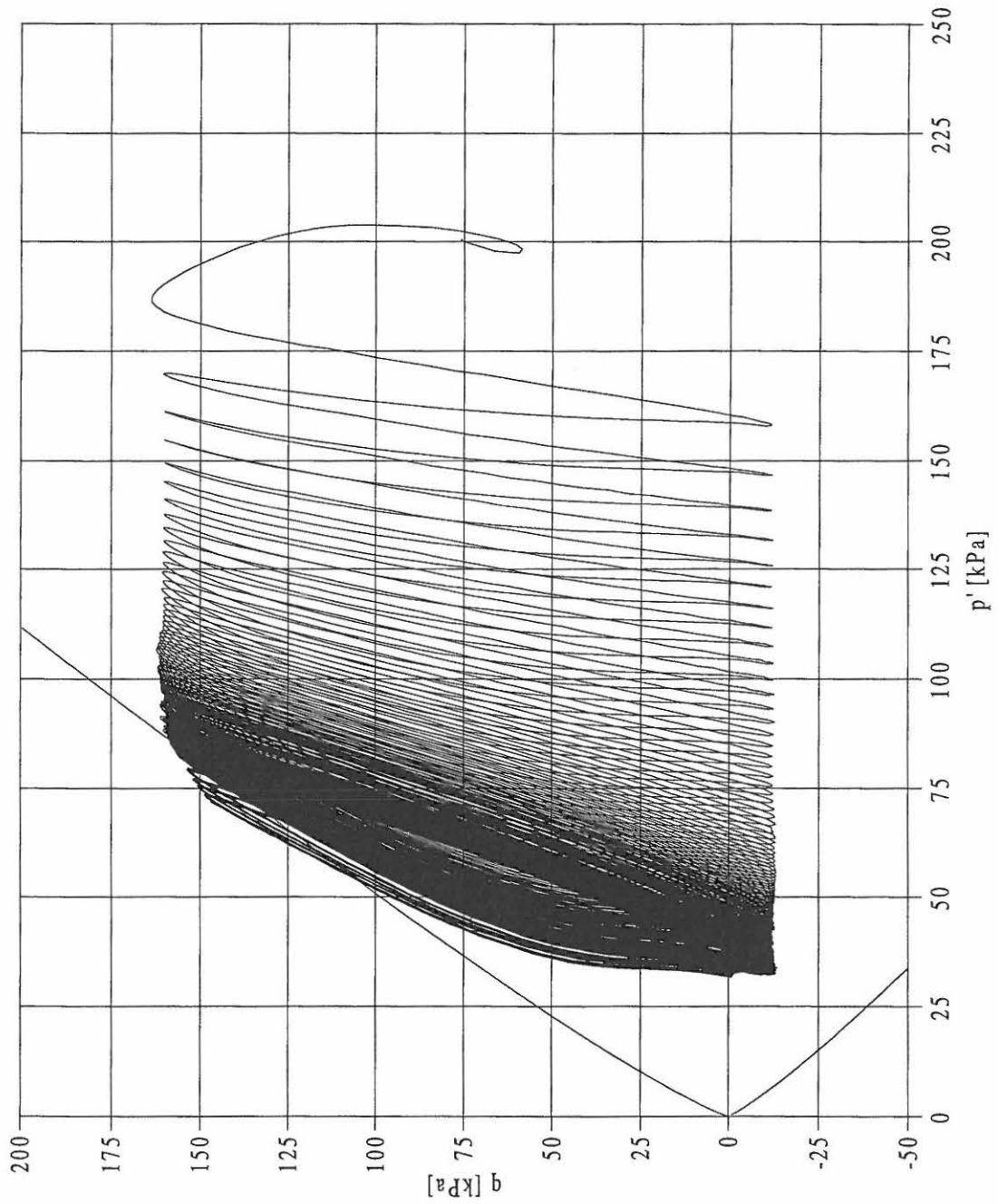
Aalborg University

Executed: KPJ

Enclosure No. 11

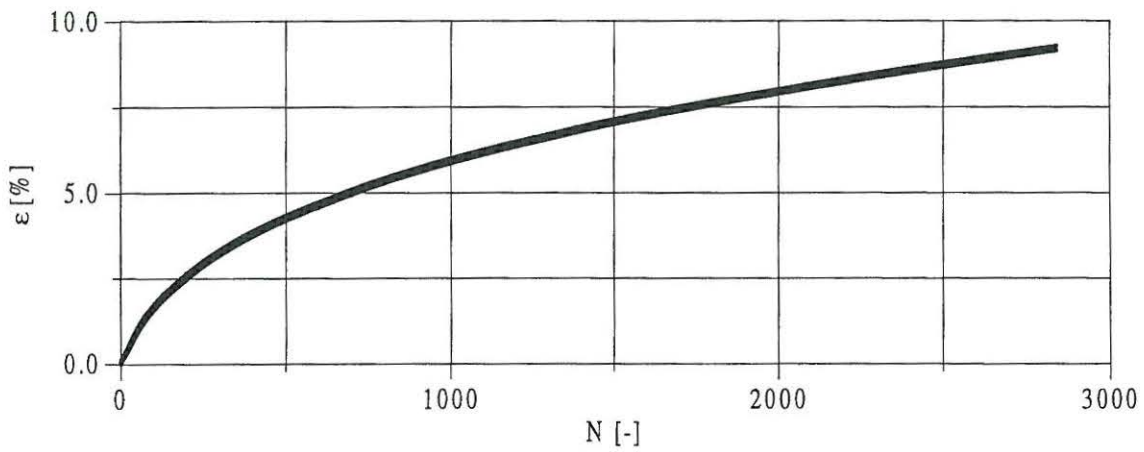
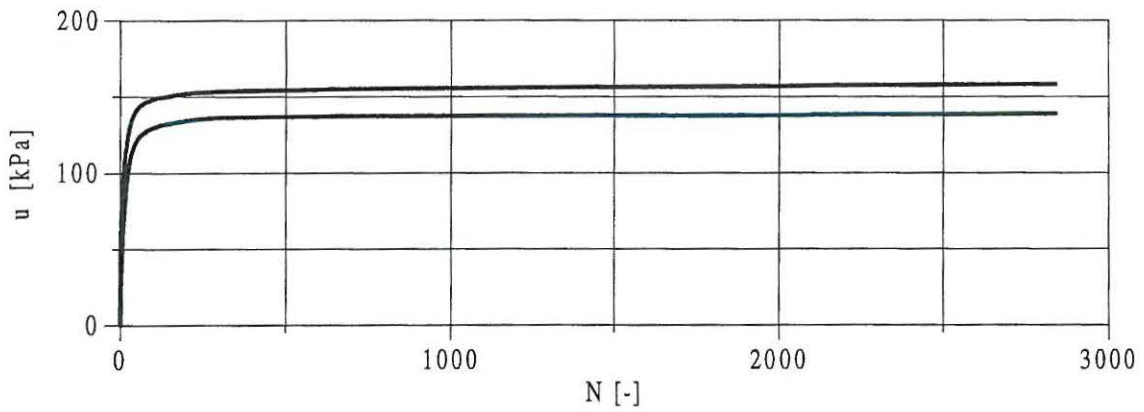
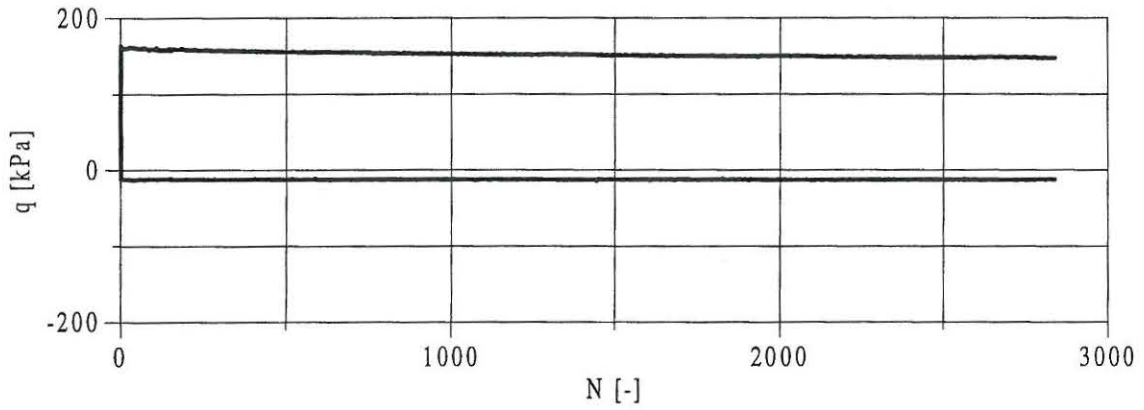
Evaluated: KPJ

Approved: KPJ



Remarks

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| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 11 |
| Evaluated: KPJ | Approved: KPJ |



Remarks

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|----------------|--------------------|
| Job: | Aalborg University |
| Executed: KPJ | Enclosure No. 11 |
| Evaluated: KPJ | Approved: KPJ |

| | | | |
|--|----------------------------------|-------------------|----------|
| Description of soil Eastern Scheldt Sand | Cyclic Triaxial Apparatus | Sample properties | |
| Specimen preparation Air pluviation | Calibration file Ca198023.dat | Height | 71.50 mm |
| Saturation procedure CO ₂ / Backpressure | Date 1998-02-09 | Diameter | 69.70 mm |
| | | Void ratio | 0.673 |
| | | B-value | 0.990 |

| | | | |
|--------------|---|-------------|---------|
| Test program | Isotropic compression, σ'_3 : | 10.0 - 25.0 | kPa |
| | Loading rate: | 5.0 | kPa/min |
| | Anisotropic compression, q_m : | 75.0 | kPa |
| | Loading rate: | 3.0 | kPa/min |
| | <input checked="" type="checkbox"/> Applied drained | | |
| | <input type="checkbox"/> Applied undrained | | |
| | Cyclic loading, q_{cyc} : | 11.3 | kPa |
| Period: | 10.0 | s | |

| | | | |
|-----------------------|--------------|-------|-----|
| Isotropic compression | | | |
| Confining pressure | σ'_3 | 25.0 | kPa |
| Pore pressure | u | 300.3 | kPa |
| Axial strain | ϵ_1 | 0.03 | % |
| Volumetric strain | ϵ_v | 0.11 | % |
| Void ratio | e | 0.671 | |

| | | | |
|-------------------------|--------------|-------|-----|
| Anisotropic compression | | | |
| Confining pressure | σ'_3 | 25.0 | kPa |
| Axial pressure | σ'_1 | 99.9 | kPa |
| Deviator stress | q | 74.9 | kPa |
| Mean normal stress | p' | 50.0 | kPa |
| Pore pressure | u | 300.0 | kPa |
| Axial strain | ϵ_1 | 0.72 | % |
| Volumetric strain | ϵ_v | 0.16 | % |
| Void ratio | e | 0.670 | |

| | |
|--------------------|--------------------|
| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 12 |
| Evaluated: KPJ | Approved: KPJ |

| Cyclic loading | | | | | | |
|----------------|---------------|--------------|--------------|------------------|-------------------|-----------------------|
| N | P'_m kPa | q_m kPa | u_p kPa | u_{cyc} kPa | ϵ_p % | ϵ_{cyc} % |
| 1 | 53.0 | 74.9 | -2.9 | 2.3 | 0.04 | 0.02 |
| 3 | 53.4 | 74.9 | -3.3 | 1.3 | 0.05 | 0.00 |
| 5 | 53.5 | 74.9 | -3.4 | 1.2 | 0.06 | 0.00 |
| 10 | 53.5 | 74.9 | -3.6 | 1.2 | 0.07 | 0.00 |
| 25 | 53.7 | 74.9 | -3.6 | 1.3 | 0.10 | 0.00 |
| 50 | 53.7 | 74.8 | -3.7 | 1.3 | 0.11 | 0.00 |
| 75 | 53.8 | 74.8 | -3.7 | 1.3 | 0.12 | 0.00 |
| 100 | 53.8 | 74.8 | -3.8 | 1.3 | 0.13 | 0.00 |
| 150 | 54.2 | 74.8 | -4.0 | 1.4 | 0.14 | 0.00 |
| 200 | 54.6 | 74.8 | -4.3 | 1.3 | 0.15 | 0.00 |
| 300 | 55.1 | 74.8 | -4.8 | 1.3 | 0.16 | 0.00 |
| 400 | 55.8 | 74.8 | -5.4 | 1.4 | 0.17 | 0.00 |
| 500 | 56.3 | 74.8 | -6.0 | 1.4 | 0.17 | 0.00 |
| 750 | 58.1 | 74.8 | -7.7 | 0.0 | 0.18 | 0.00 |
| 1000 | 60.0 | 74.8 | -9.6 | 1.5 | 0.19 | 0.00 |
| 1250 | 61.0 | 74.8 | -11.3 | 1.7 | 0.19 | 0.00 |
| 1500 | 62.4 | 74.8 | -12.7 | 1.7 | 0.19 | 0.00 |
| 1750 | 63.8 | 74.8 | -14.5 | 1.8 | 0.20 | 0.00 |
| 2000 | 65.0 | 74.8 | -15.5 | 1.7 | 0.20 | 0.00 |
| 2250 | 66.0 | 74.8 | -16.6 | 1.8 | 0.20 | 0.00 |
| 2500 | 67.0 | 74.8 | -17.7 | 1.8 | 0.20 | 0.00 |
| 3000 | 72.6 | 74.4 | -18.4 | 1.9 | 0.21 | 0.00 |
| 3500 | 73.7 | 74.4 | -20.0 | 1.8 | 0.21 | 0.00 |
| 4000 | 76.0 | 74.4 | -21.8 | 1.9 | 0.21 | 0.00 |

Remarks:

Job: Ph.D. Project

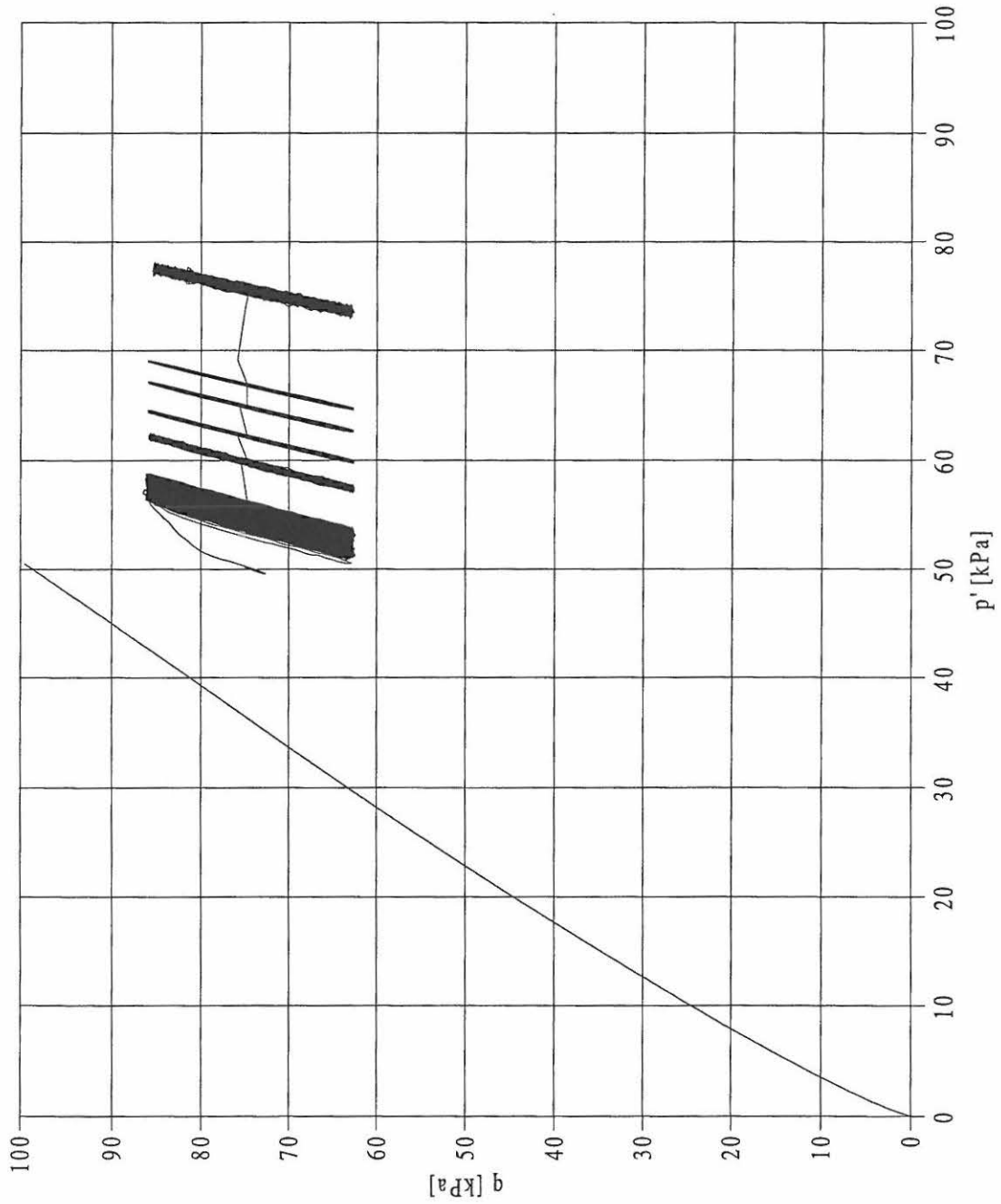
Aalborg University

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Enclosure No. 12

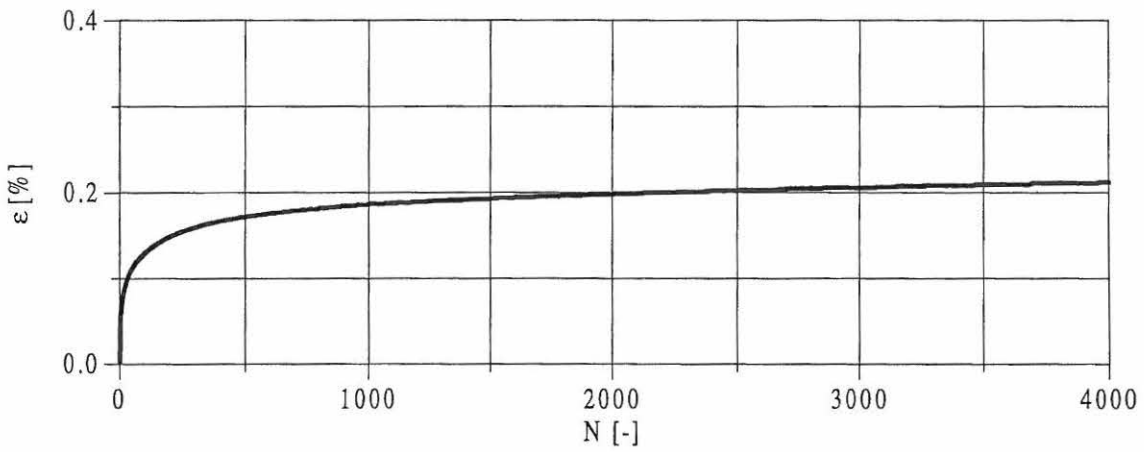
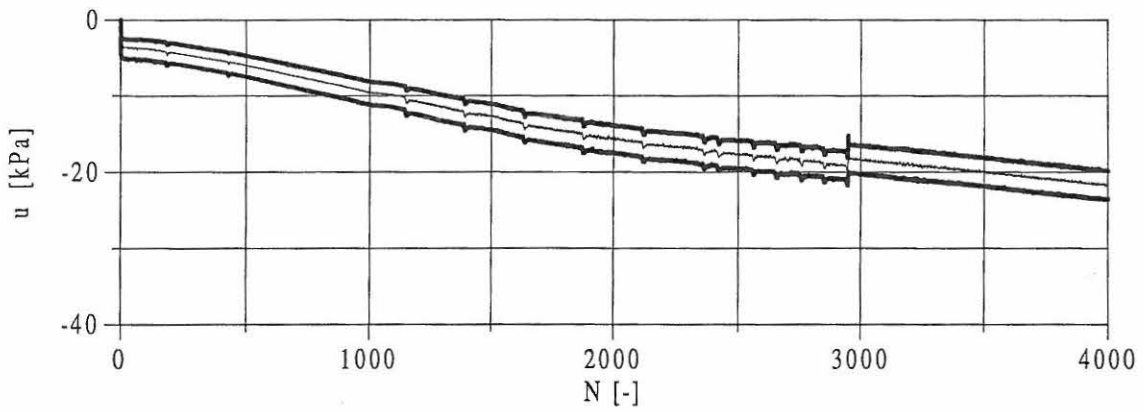
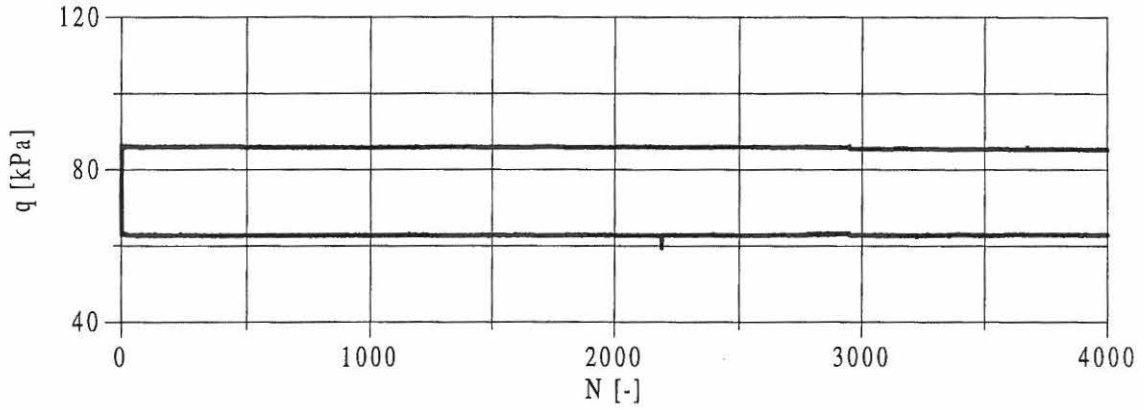
Evaluated: KPJ

Approved: KPJ



Remarks

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|--------------------|--------------------|
| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 12 |
| Evaluated: KPJ | Approved: KPJ |



Remarks

Job: Aalborg University
 Executed: KPJ
 Evaluated: KPJ
 Enclosure No. 12
 Approved: KPJ

| | | | |
|--|----------------------------------|-------------------|----------|
| Description of soil Eastern Scheldt Sand | Cyclic Triaxial Apparatus | Sample properties | |
| Specimen preparation Air pluviation | Calibration file Cal98023.dat | Height | 71.50 mm |
| Saturation procedure CO ₂ / Backpressure | Date 1998-03-05 | Diameter | 69.70 mm |
| | | Void ratio | 0.672 |
| | | B-value | 0.983 |

| | | | |
|--------------|---|-------------|---------|
| Test program | Isotropic compression, σ'_3 : | 10.0 - 75.0 | kPa |
| | Loading rate: | 5.0 | kPa/min |
| | Anisotropic compression, q_m : | 75.0 | kPa |
| | Loading rate: | 3.0 | kPa/min |
| | <input checked="" type="checkbox"/> Applied drained | | |
| | <input type="checkbox"/> Applied undrained | | |
| | Cyclic loading, q_{cyc} : | 25.0 | kPa |
| Period: | 10.0 | s | |

| | | | |
|-----------------------|--------------|-------|-----|
| Isotropic compression | | | |
| Confining pressure | σ'_3 | 75.0 | kPa |
| Pore pressure | u | 299.6 | kPa |
| Axial strain | ϵ_1 | 0.14 | % |
| Volumetric strain | ϵ_v | 0.30 | % |
| Void ratio | e | 0.667 | |

| | | | |
|-------------------------|--------------|-------|-----|
| Anisotropic compression | | | |
| Confining pressure | σ'_3 | 75.0 | kPa |
| Axial pressure | σ'_1 | 150.4 | kPa |
| Deviator stress | q | 75.4 | kPa |
| Mean normal stress | p' | 100.1 | kPa |
| Pore pressure | u | 299.6 | kPa |
| Axial strain | ϵ_1 | 0.35 | % |
| Volumetric strain | ϵ_v | 0.40 | % |
| Void ratio | e | 0.665 | |

| | |
|--------------------|--------------------|
| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 13 |
| Evaluated: KPJ | Approved: KPJ |

| Cyclic loading | | | | | | |
|----------------|---------------|--------------|--------------|------------------|-------------------|-----------------------|
| N | P'_m kPa | q_m kPa | u_p kPa | u_{cyc} kPa | ϵ_p % | ϵ_{cyc} % |
| 1 | 93.0 | 75.5 | 6.9 | 4.2 | 0.09 | 0.05 |
| 3 | 90.9 | 75.4 | 9.1 | 4.3 | 0.11 | 0.01 |
| 5 | 89.7 | 75.4 | 10.3 | 4.4 | 0.13 | 0.01 |
| 10 | 88.4 | 75.4 | 11.6 | 4.6 | 0.15 | 0.01 |
| 25 | 86.1 | 75.4 | 14.1 | 4.6 | 0.18 | 0.01 |
| 50 | 84.3 | 75.4 | 15.6 | 4.5 | 0.20 | 0.01 |
| 75 | 83.6 | 75.4 | 16.4 | 4.5 | 0.22 | 0.00 |
| 100 | 83.4 | 75.3 | 16.8 | 4.4 | 0.23 | 0.00 |
| 150 | 83.2 | 75.3 | 16.9 | 4.5 | 0.25 | 0.00 |
| 200 | 82.8 | 75.3 | 17.1 | 4.5 | 0.27 | 0.00 |
| 300 | 83.6 | 75.3 | 16.4 | 4.5 | 0.30 | 0.00 |
| 400 | 84.6 | 75.3 | 15.4 | 4.5 | 0.31 | 0.00 |
| 500 | 86.1 | 75.3 | 14.1 | 4.5 | 0.32 | 0.00 |
| 750 | 91.0 | 75.2 | 9.8 | 4.6 | 0.34 | 0.00 |
| 1000 | 95.3 | 75.1 | 5.9 | 4.8 | 0.36 | 0.00 |
| 1250 | 97.9 | 75.2 | 2.9 | 5.0 | 0.37 | 0.00 |
| 1500 | 102.0 | 75.1 | -0.8 | 5.0 | 0.38 | 0.00 |
| 1750 | 104.5 | 75.1 | -3.5 | 5.2 | 0.38 | 0.00 |
| 2000 | 107.2 | 75.1 | -6.2 | 5.2 | 0.39 | 0.00 |
| 2250 | 109.9 | 75.1 | -8.7 | 5.4 | 0.39 | 0.00 |
| 2500 | 112.1 | 75.1 | -10.9 | 5.3 | 0.40 | 0.00 |
| 3000 | 113.8 | 75.2 | -13.3 | 5.5 | 0.40 | 0.00 |
| 3500 | 116.3 | 75.2 | -15.9 | 5.6 | 0.41 | 0.00 |
| 4000 | 117.2 | 75.2 | -17.2 | 5.6 | 0.42 | 0.00 |
| 4500 | 118.2 | 75.2 | -18.2 | 5.6 | 0.42 | 0.00 |
| 5000 | 119.1 | 75.2 | -19.0 | 5.7 | 0.43 | 0.00 |

Remarks:

Job: Ph.D. Project

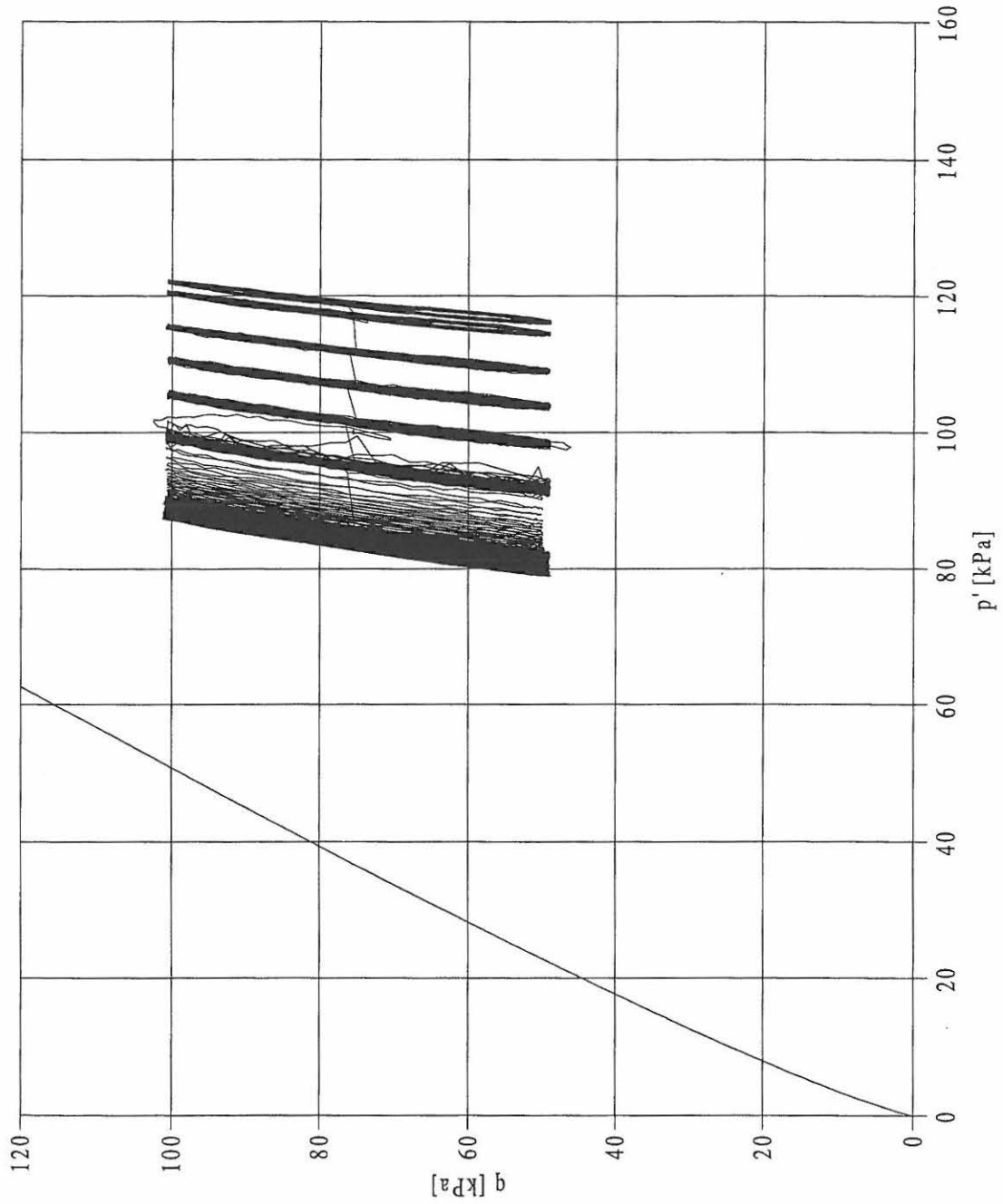
Aalborg University

Executed: KPJ

Enclosure No. 13

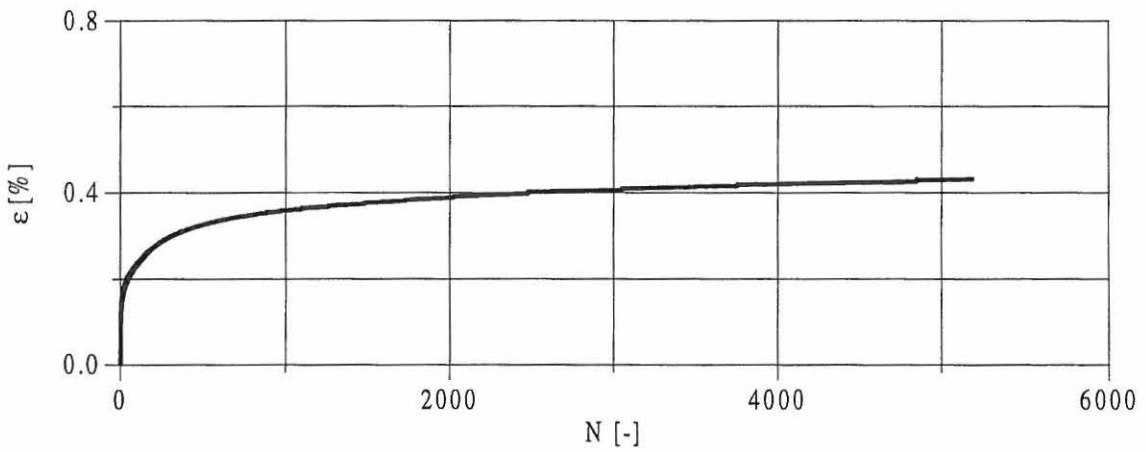
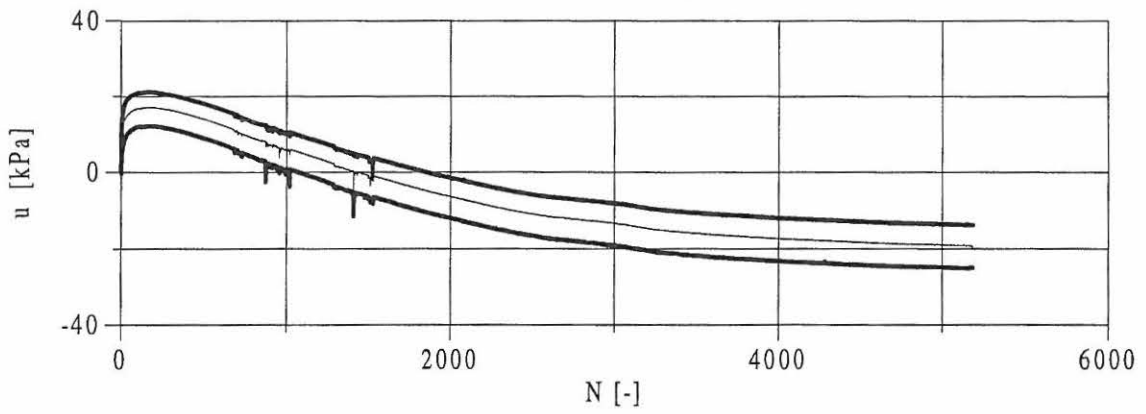
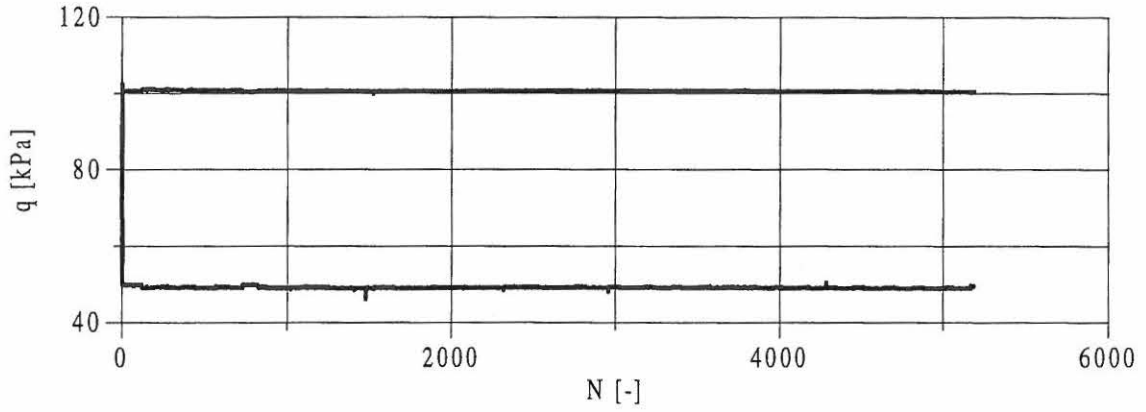
Evaluated: KPJ

Approved: KPJ



Remarks

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| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 13 |
| Evaluated: KPJ | Approved: KPJ |



Remarks

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|----------------|--------------------|
| Job: | Aalborg University |
| Executed: KPJ | Enclosure No. 13 |
| Evaluated: KPJ | Approved: KPJ |

| | | | |
|--|----------------------------------|-------------------|----------|
| Description of soil Eastern Scheldt Sand | Cyclic Triaxial Apparatus | Sample properties | |
| Specimen preparation Air pluviation | Calibration file Cal98023.dat | Height | 71.47 mm |
| Saturation procedure CO ₂ / Backpressure | Date 1998-03-06 | Diameter | 69.67 mm |
| | | Void ratio | 0.671 |
| | | B-value | 0.977 |

| | | | |
|--------------|---|-------------|---------|
| Test program | Isotropic compression, σ'_3 : | 10.0 - 25.0 | kPa |
| | Loading rate: | 5.0 | kPa/min |
| | Anisotropic compression, q_m : | 75.0 | kPa |
| | Loading rate: | 3.0 | kPa/min |
| | <input checked="" type="checkbox"/> Applied drained | | |
| | <input type="checkbox"/> Applied undrained | | |
| | Cyclic loading, q_{cyc} : | 25.0 | kPa |
| Period: | 10.0 | s | |

| | | | |
|-----------------------|--------------|-------|-----|
| Isotropic compression | | | |
| Confining pressure | σ'_3 | 24.9 | kPa |
| Pore pressure | u | 299.9 | kPa |
| Axial strain | ϵ_1 | 0.00 | % |
| Volumetric strain | ϵ_v | 0.01 | % |
| Void ratio | e | 0.671 | |

| | | | |
|-------------------------|--------------|-------|-----|
| Anisotropic compression | | | |
| Confining pressure | σ'_3 | 25.0 | kPa |
| Axial pressure | σ'_1 | 100.4 | kPa |
| Deviator stress | q | 75.4 | kPa |
| Mean normal stress | p' | 50.1 | kPa |
| Pore pressure | u | 299.9 | kPa |
| Axial strain | ϵ_1 | 0.59 | % |
| Volumetric strain | ϵ_v | -0.05 | % |
| Void ratio | e | 0.672 | |

| | |
|--------------------|--------------------|
| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 14 |
| Evaluated: KPJ | Approved: KPJ |

| Cyclic loading | | | | | | |
|----------------|---------------|--------------|--------------|------------------|-------------------|-----------------------|
| N | P'_m kPa | q_m kPa | u_p kPa | u_{cyc} kPa | ϵ_p % | ϵ_{cyc} % |
| 1 | 56.0 | 75.4 | -5.8 | 5.0 | 0.10 | 0.05 |
| 3 | 57.1 | 75.4 | -6.9 | 2.5 | 0.13 | 0.01 |
| 5 | 57.4 | 75.4 | -7.3 | 2.5 | 0.15 | 0.01 |
| 10 | 57.8 | 75.4 | -7.7 | 2.5 | 0.18 | 0.01 |
| 25 | 58.2 | 75.3 | -8.1 | 2.6 | 0.22 | 0.01 |
| 50 | 58.3 | 75.3 | -8.2 | 2.6 | 0.26 | 0.01 |
| 75 | 58.2 | 75.3 | -8.1 | 2.6 | 0.28 | 0.01 |
| 100 | 58.3 | 75.3 | -8.1 | 2.6 | 0.29 | 0.01 |
| 150 | 58.2 | 75.2 | -8.2 | 2.7 | 0.32 | 0.01 |
| 200 | 58.2 | 75.2 | -8.2 | 2.6 | 0.34 | 0.01 |
| 300 | 58.2 | 75.2 | -8.1 | 2.7 | 0.36 | 0.01 |
| 400 | 58.1 | 75.2 | -8.0 | 2.7 | 0.38 | 0.01 |
| 500 | 58.3 | 75.2 | -8.1 | 2.7 | 0.40 | 0.01 |
| 750 | 58.2 | 75.2 | -8.0 | 2.7 | 0.42 | 0.01 |
| 1000 | 58.3 | 75.1 | -7.9 | 2.6 | 0.45 | 0.01 |
| 1250 | 58.4 | 75.1 | -7.8 | 2.6 | 0.46 | 0.01 |
| 1500 | 58.4 | 75.1 | -7.6 | 2.6 | 0.48 | 0.01 |
| 1750 | 58.3 | 75.0 | -7.3 | 2.6 | 0.50 | 0.01 |
| 2000 | 58.0 | 75.0 | -7.0 | 2.5 | 0.51 | 0.01 |
| 2250 | 57.9 | 75.0 | -6.8 | 2.5 | 0.52 | 0.01 |
| 2500 | 57.7 | 75.0 | -6.5 | 2.5 | 0.54 | 0.01 |
| 3000 | 56.9 | 75.0 | -6.0 | 2.5 | 0.56 | 0.01 |
| 3500 | 56.5 | 75.0 | -5.6 | 2.5 | 0.58 | 0.01 |
| 4000 | 56.7 | 74.9 | -5.7 | 2.5 | 0.60 | 0.01 |
| 4500 | 56.6 | 75.0 | -5.7 | 2.6 | 0.61 | 0.01 |
| 5000 | 56.9 | 74.9 | -6.0 | 2.6 | 0.62 | 0.01 |
| 5500 | 57.3 | 74.9 | -6.4 | 2.6 | 0.62 | 0.01 |
| 6000 | 58.1 | 74.9 | -7.2 | 2.6 | 0.63 | 0.01 |
| 7000 | 59.5 | 74.9 | -8.8 | 2.8 | 0.63 | 0.01 |
| 8000 | 61.3 | 74.9 | -10.5 | 2.9 | 0.64 | 0.01 |
| 9000 | 62.6 | 74.9 | -11.9 | 3.0 | 0.64 | 0.01 |
| 10000 | 64.5 | 74.9 | -13.5 | 3.1 | 0.64 | 0.01 |
| 12000 | 67.7 | 74.9 | -16.5 | 3.3 | 0.64 | 0.01 |
| 14000 | 70.8 | 74.9 | -19.3 | 3.4 | 0.65 | 0.01 |
| 16000 | 72.3 | 74.9 | -21.1 | 3.6 | 0.65 | 0.01 |
| 18000 | 71.3 | 74.9 | -20.4 | 3.4 | 0.64 | 0.01 |
| 20000 | 74.9 | 74.9 | -23.4 | 3.7 | 0.64 | 0.01 |

Job: Ph.D. Project

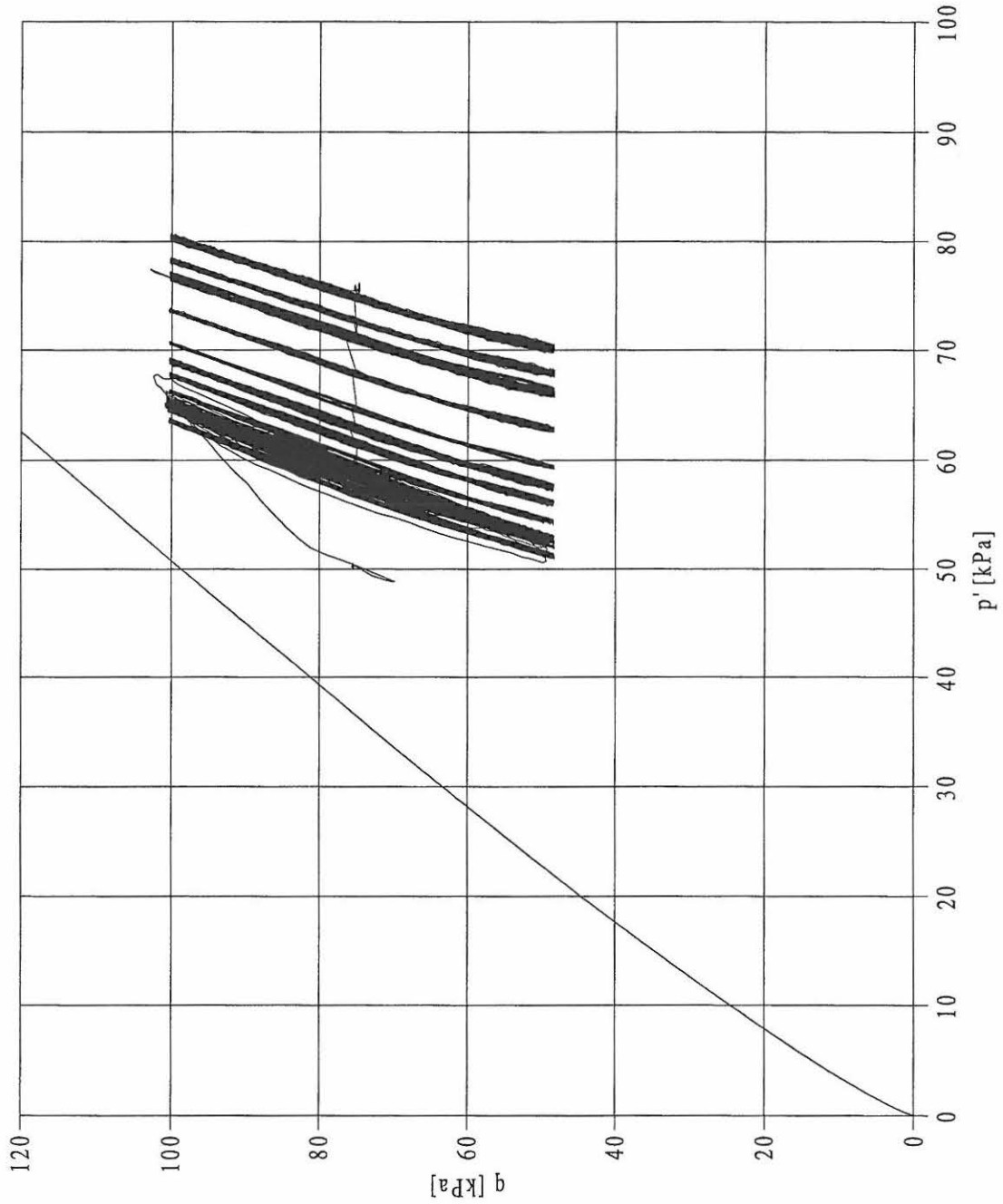
Aalborg University

Executed: KPJ

Enclosure No. 14

Evaluated: KPJ

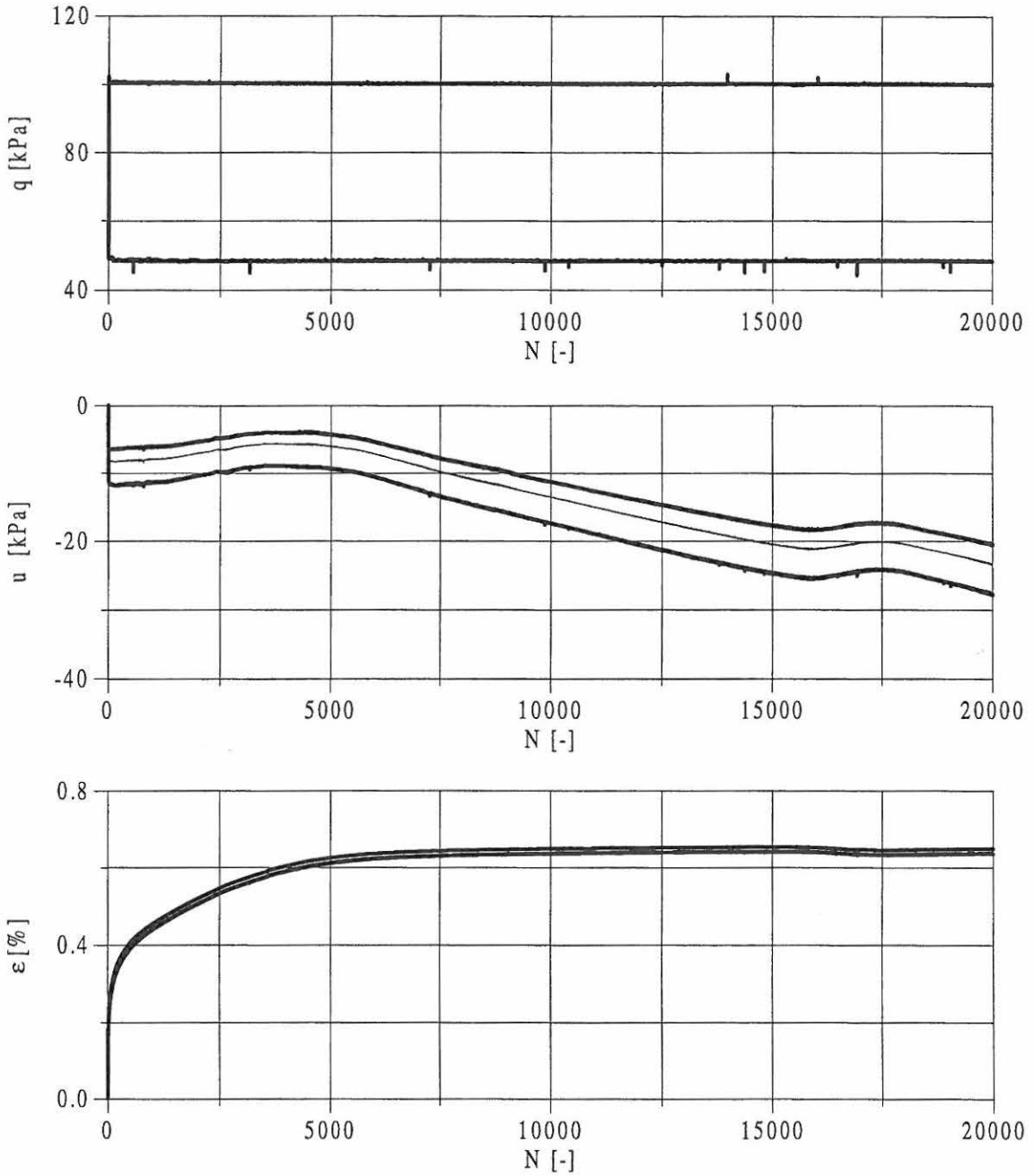
Approved: KPJ



Remarks

Job: Ph.D. Project
Executed: KPJ
Evaluated: KPJ

Aalborg University
Enclosure No. 14
Approved: KPJ



Remarks

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|----------------|--------------------|
| Job: | Aalborg University |
| Executed: KPJ | Enclosure No. 14 |
| Evaluated: KPJ | Approved: KPJ |

| | | | |
|--|----------------------------------|-------------------|----------|
| Description of soil Eastern Scheldt Sand | Cyclic Triaxial Apparatus | Sample properties | |
| Specimen preparation Air pluviation | Calibration file Cal98023.dat | Height | 71.50 mm |
| Saturation procedure CO ₂ / Backpressure | Date 1998-03-09 | Diameter | 69.70 mm |
| | | Void ratio | 0.673 |
| | | B-value | 0.997 |

| | | | |
|--------------|---|-------------|---------|
| Test program | Isotropic compression, σ'_3 : | 10.0 - 49.5 | kPa |
| | Loading rate: | 5.0 | kPa/min |
| | Anisotropic compression, q_m : | 151.5 | kPa |
| | Loading rate: | 3.0 | kPa/min |
| | <input checked="" type="checkbox"/> Applied drained | | |
| | <input type="checkbox"/> Applied undrained | | |
| | Cyclic loading, q_{cyc} : | 100.0 | kPa |
| | Period: | 10.0 | s |

| | | | |
|-----------------------|--------------|-------|-----|
| Isotropic compression | | | |
| Confining pressure | σ'_3 | 49.4 | kPa |
| Pore pressure | u | 299.2 | kPa |
| Axial strain | ϵ_1 | 0.06 | % |
| Volumetric strain | ϵ_v | 0.13 | % |
| Void ratio | e | 0.671 | |

| | | | |
|-------------------------|--------------|-------|-----|
| Anisotropic compression | | | |
| Confining pressure | σ'_3 | 49.5 | kPa |
| Axial pressure | σ'_1 | 200.6 | kPa |
| Deviator stress | q | 151.1 | kPa |
| Mean normal stress | p' | 99.9 | kPa |
| Pore pressure | u | 299.2 | kPa |
| Axial strain | ϵ_1 | 1.11 | % |
| Volumetric strain | ϵ_v | 0.19 | % |
| Void ratio | e | 0.670 | |

| | |
|--------------------|--------------------|
| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 15 |
| Evaluated: KPJ | Approved: KPJ |

| Cyclic loading | | | | | | |
|----------------|---------------|--------------|--------------|------------------|-------------------|-----------------------|
| N | P'_m kPa | q_m kPa | u_p kPa | u_{cyc} kPa | ϵ_p % | ϵ_{cyc} % |
| 1 | 109.2 | 150.4 | -9.5 | 19.3 | 0.30 | 0.17 |
| 3 | 113.8 | 150.2 | -14.1 | 13.0 | 0.45 | 0.06 |
| 5 | 115.3 | 150.1 | -15.9 | 11.8 | 0.54 | 0.05 |
| 10 | 117.5 | 149.8 | -18.0 | 10.9 | 0.69 | 0.04 |
| 25 | 119.7 | 149.5 | -20.4 | 10.7 | 0.91 | 0.04 |
| 50 | 120.8 | 149.2 | -21.4 | 11.0 | 1.11 | 0.04 |
| 75 | 121.1 | 149.0 | -21.8 | 11.2 | 1.23 | 0.04 |
| 100 | 121.1 | 148.9 | -22.0 | 11.3 | 1.33 | 0.04 |
| 150 | 121.4 | 148.6 | -22.2 | 11.4 | 1.46 | 0.03 |
| 200 | 121.8 | 148.5 | -22.4 | 11.5 | 1.55 | 0.03 |
| 300 | 121.5 | 148.3 | -22.3 | 11.6 | 1.69 | 0.03 |
| 400 | 121.6 | 148.1 | -22.3 | 11.6 | 1.78 | 0.03 |
| 500 | 121.5 | 148.0 | -22.2 | 11.7 | 1.86 | 0.03 |
| 750 | 121.6 | 147.8 | -22.2 | 11.8 | 1.99 | 0.03 |
| 1000 | 121.8 | 147.7 | -22.4 | 11.8 | 2.08 | 0.03 |
| 1250 | 121.7 | 147.6 | -22.3 | 11.9 | 2.14 | 0.03 |
| 1500 | 122.1 | 147.5 | -22.6 | 11.9 | 2.19 | 0.02 |
| 1750 | 122.2 | 147.4 | -22.8 | 12.0 | 2.23 | 0.02 |
| 2000 | 122.5 | 147.4 | -23.0 | 12.1 | 2.26 | 0.02 |
| 2250 | 122.3 | 147.4 | -23.0 | 12.1 | 2.29 | 0.02 |
| 2500 | 122.0 | 147.3 | -22.9 | 12.3 | 2.31 | 0.02 |
| 3000 | 121.7 | 147.3 | -22.9 | 12.3 | 2.34 | 0.02 |
| 3500 | 121.8 | 147.3 | -23.0 | 12.4 | 2.37 | 0.02 |
| 4000 | 123.9 | 147.3 | -25.4 | 12.4 | 2.40 | 0.02 |

Remarks:

Job: Ph.D. Project

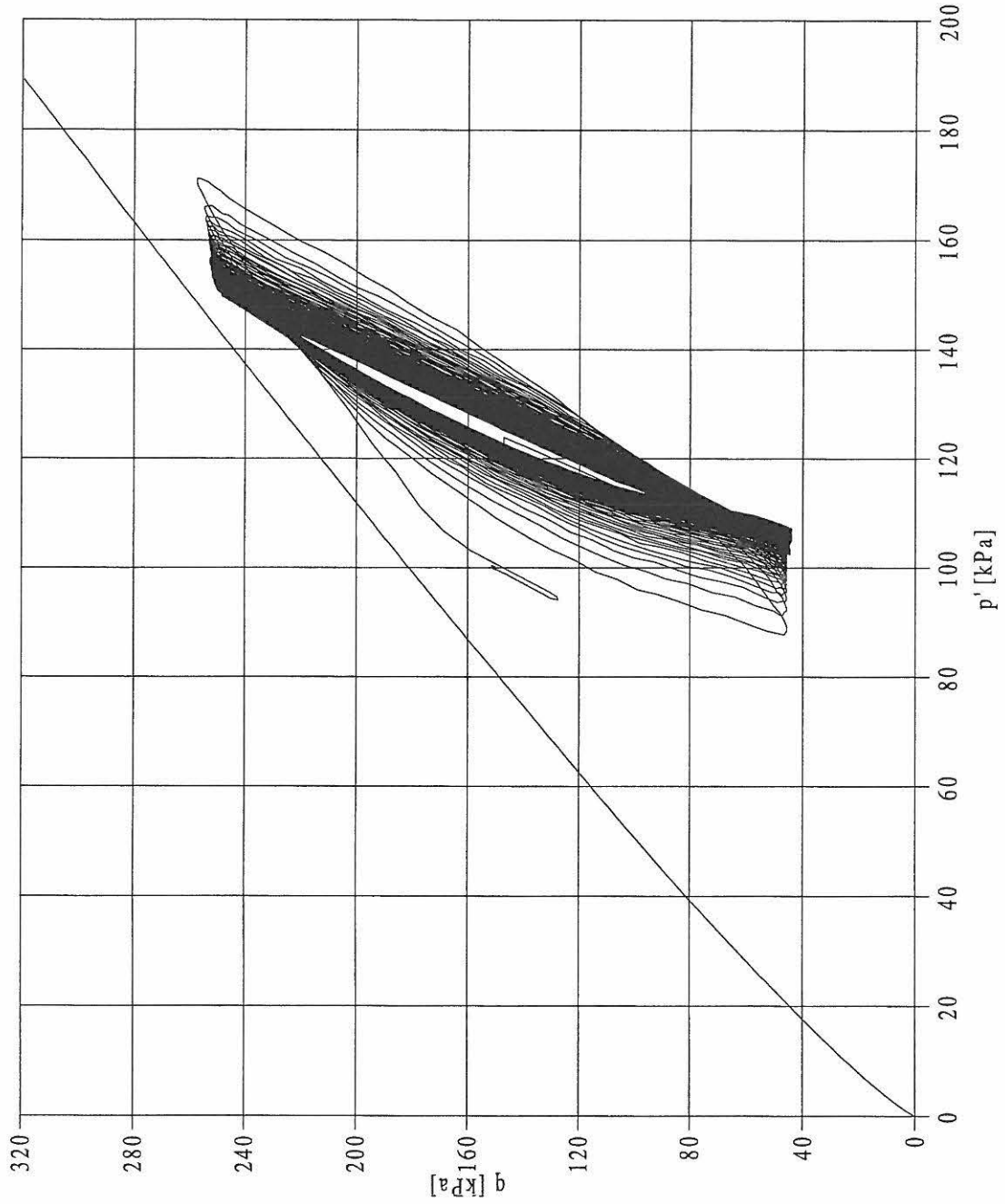
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Enclosure No. 15

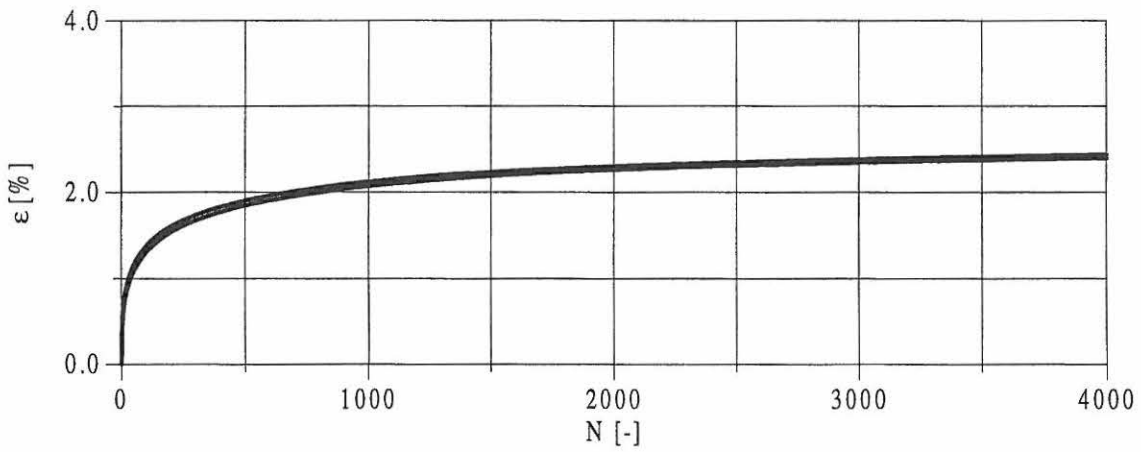
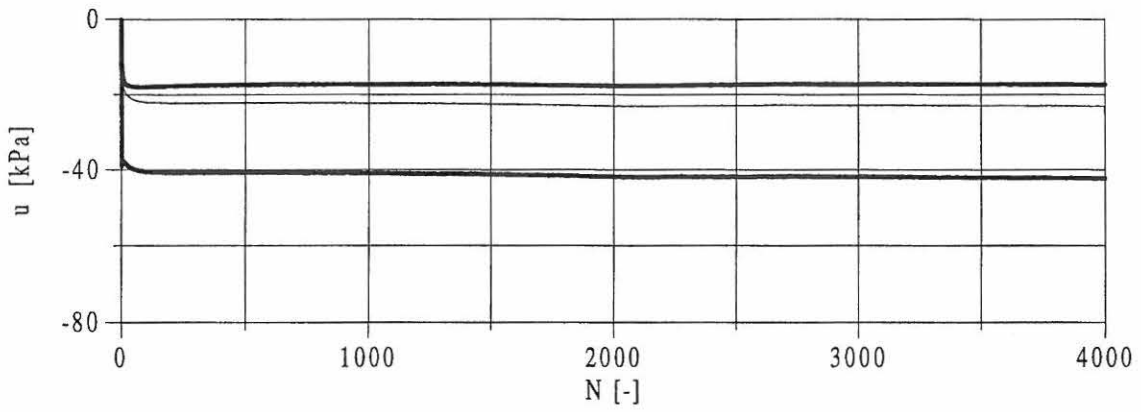
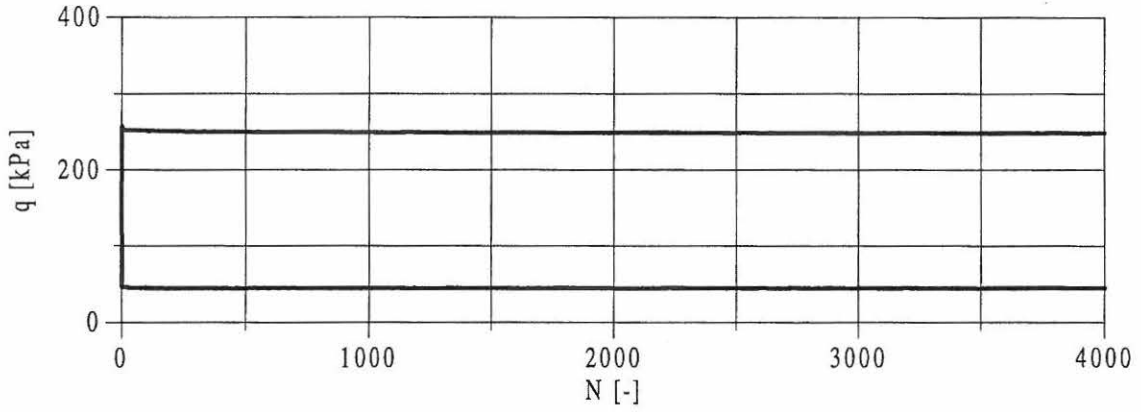
Evaluated: KPJ

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| Job: Ph.D. Project | Aalborg University |
| Executed: KPJ | Enclosure No. 15 |
| Evaluated: KPJ | Approved: KPJ |



Remarks

Job: Aalborg University
Executed: KPJ
Evaluated: KPJ
Enclosure No. 17
Approved: KPJ

| | | | |
|--|----------------------------------|-------------------|----------|
| Description of soil Eastern Scheldt Sand | Cyclic Triaxial Apparatus | Sample properties | |
| Specimen preparation Air pluviation | Calibration file Cal98023.dat | Height | 71.47 mm |
| Saturation procedure CO ₂ / Backpressure | Date 1998-03-10 | Diameter | 69.67 mm |
| | | Void ratio | 0.671 |
| | | B-value | 0.997 |

| | | | |
|--------------|---|-------------|---------|
| Test program | Isotropic compression, σ'_3 : | 10.0 - 11.7 | kPa |
| | Loading rate: | 5.0 | kPa/min |
| | Anisotropic compression, q_m : | 55.0 | kPa |
| | Loading rate: | 3.0 | kPa/min |
| | <input checked="" type="checkbox"/> Applied drained | | |
| | <input type="checkbox"/> Applied undrained | | |
| | Cyclic loading, q_{cyc} : | 36.3 | kPa |
| | Period: | 10.0 | s |

| | | | |
|-----------------------|--------------|-------|-----|
| Isotropic compression | | | |
| Confining pressure | σ'_3 | 11.7 | kPa |
| Pore pressure | u | 299.9 | kPa |
| Axial strain | ϵ_1 | 0.00 | % |
| Volumetric strain | ϵ_v | 0.01 | % |
| Void ratio | e | 0.671 | |

| | | | |
|-------------------------|--------------|-------|-----|
| Anisotropic compression | | | |
| Confining pressure | σ'_3 | 11.6 | kPa |
| Axial pressure | σ'_1 | 66.3 | kPa |
| Deviator stress | q | 54.7 | kPa |
| Mean normal stress | p' | 29.8 | kPa |
| Pore pressure | u | 299.8 | kPa |
| Axial strain | ϵ_1 | 1.22 | % |
| Volumetric strain | ϵ_v | -0.35 | % |
| Void ratio | e | 0.677 | |

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| Evaluated: KPJ | Approved: KPJ |

| Cyclic loading | | | | | | |
|----------------|---------------|--------------|--------------|------------------|-------------------|-----------------------|
| N | P'_m kPa | q_m kPa | u_p kPa | u_{cyc} kPa | ϵ_p % | ϵ_{cyc} % |
| 1 | 31.3 | 54.6 | -1.4 | 6.8 | 0.19 | 0.11 |
| 3 | 33.0 | 54.5 | -3.2 | 5.2 | 0.32 | 0.04 |
| 5 | 33.7 | 54.5 | -4.0 | 4.6 | 0.39 | 0.03 |
| 10 | 34.9 | 54.4 | -5.2 | 3.8 | 0.51 | 0.03 |
| 25 | 36.0 | 54.3 | -6.3 | 3.3 | 0.68 | 0.02 |
| 50 | 36.7 | 54.2 | -7.0 | 3.2 | 0.83 | 0.02 |
| 75 | 36.8 | 54.2 | -7.2 | 3.2 | 0.93 | 0.02 |
| 100 | 36.8 | 54.1 | -7.3 | 3.2 | 1.00 | 0.01 |
| 150 | 36.7 | 54.1 | -7.1 | 3.2 | 1.11 | 0.01 |
| 200 | 36.6 | 54.0 | -7.1 | 3.1 | 1.20 | 0.01 |
| 300 | 36.0 | 53.9 | -6.6 | 3.1 | 1.36 | 0.01 |
| 400 | 36.0 | 53.9 | -6.8 | 3.1 | 1.48 | 0.01 |
| 500 | 35.9 | 53.8 | -6.9 | 3.1 | 1.58 | 0.01 |
| 750 | 35.5 | 53.7 | -6.6 | 3.0 | 1.79 | 0.01 |
| 1000 | 35.2 | 53.6 | -6.1 | 3.1 | 1.99 | 0.01 |
| 1250 | 35.1 | 53.5 | -6.0 | 3.2 | 2.16 | 0.01 |
| 1500 | 34.9 | 53.4 | -5.7 | 3.2 | 2.30 | 0.01 |
| 1750 | 35.2 | 53.3 | -5.6 | 3.2 | 2.40 | 0.01 |
| 2000 | 35.2 | 53.3 | -5.6 | 3.2 | 2.49 | 0.00 |
| 2250 | 35.4 | 53.2 | -5.7 | 3.2 | 2.56 | 0.00 |
| 2500 | 35.7 | 53.2 | -5.7 | 3.3 | 2.63 | 0.00 |
| 3000 | 35.2 | 53.1 | -5.4 | 3.3 | 2.73 | 0.00 |
| 3500 | 35.0 | 53.1 | -5.2 | 3.2 | 2.82 | 0.00 |
| 4000 | 34.7 | 53.1 | -5.0 | 3.3 | 2.89 | 0.00 |
| 4500 | 34.5 | 53.0 | -4.9 | 3.2 | 2.96 | 0.00 |
| 5000 | 33.9 | 53.0 | -4.5 | 3.2 | 3.02 | 0.00 |
| 5500 | 33.7 | 53.0 | -4.3 | 3.2 | 3.08 | 0.00 |
| 6000 | 33.6 | 52.9 | -4.2 | 3.2 | 3.13 | 0.00 |

Remarks:

Job: Ph.D. Project

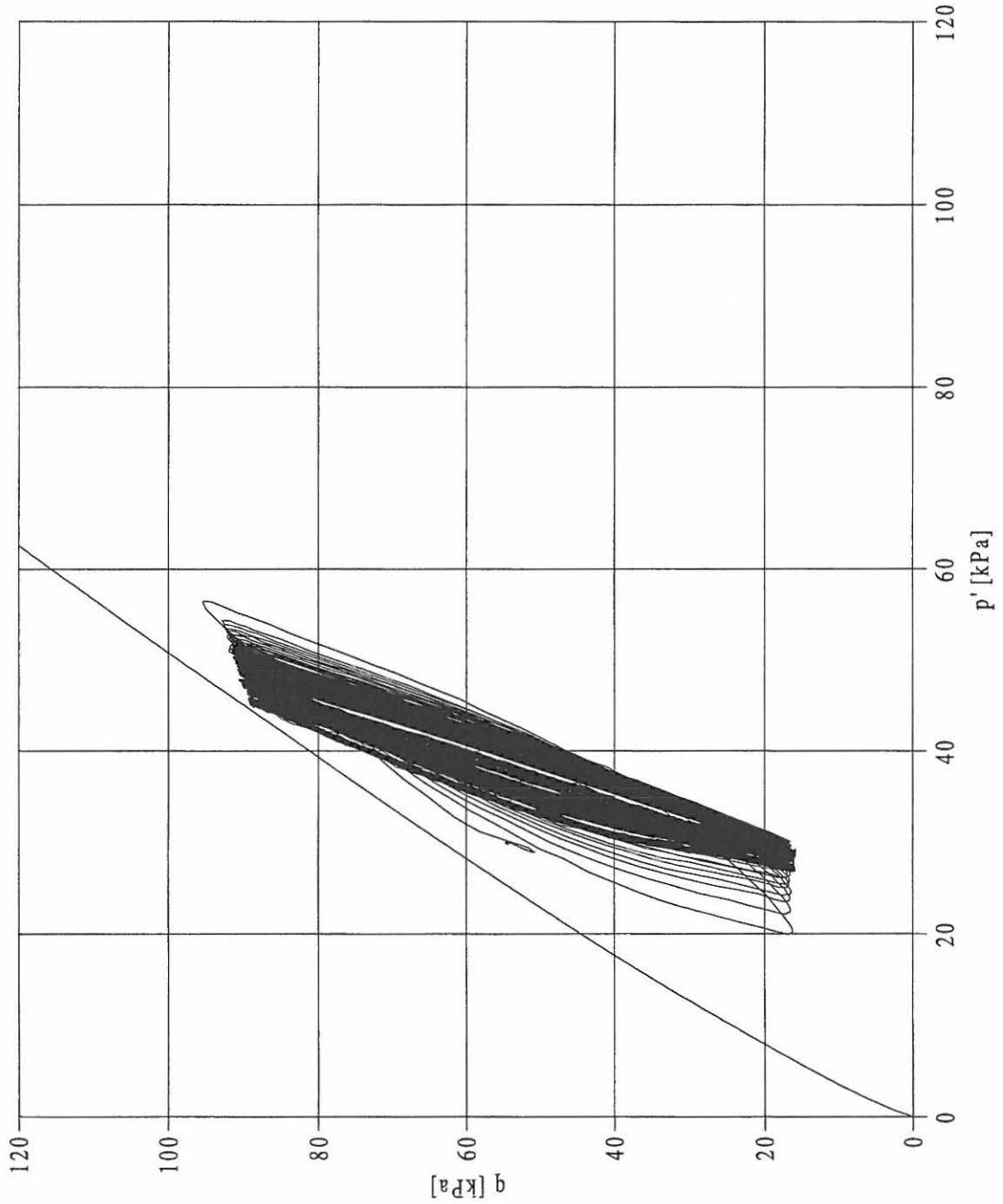
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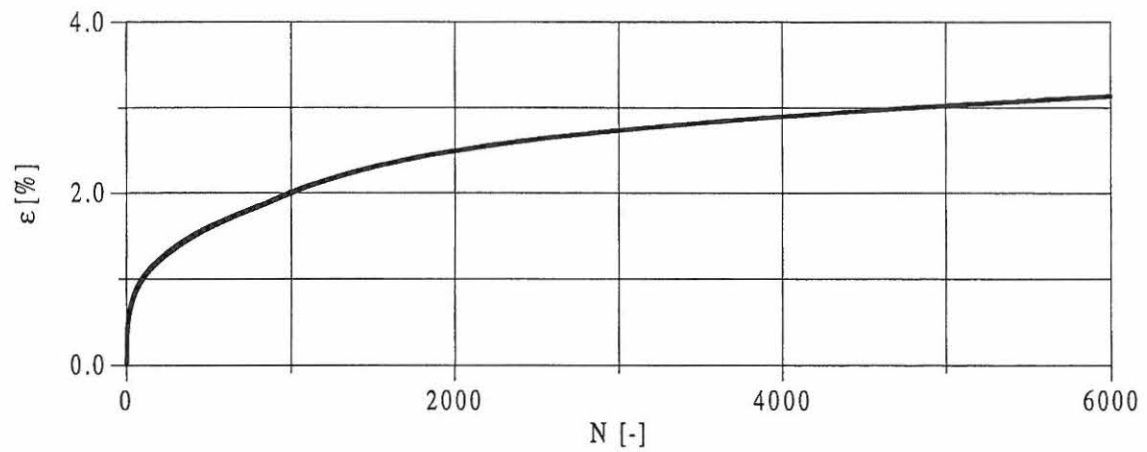
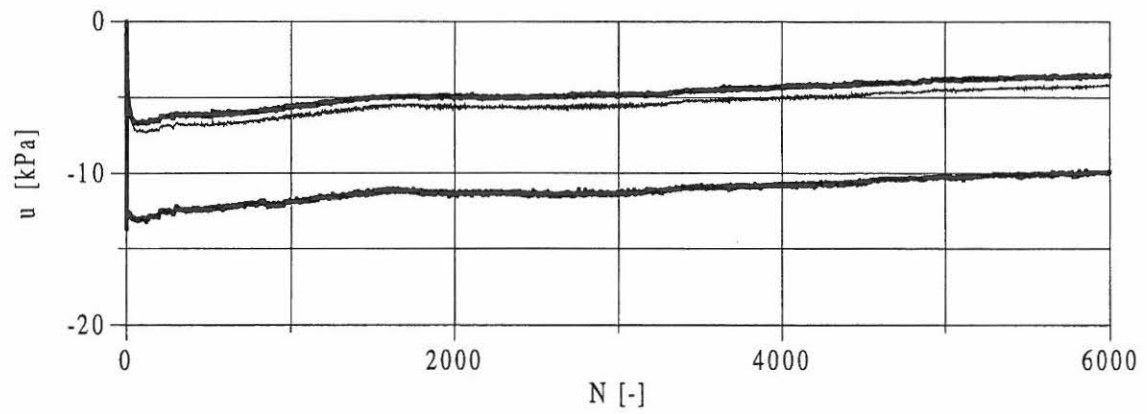
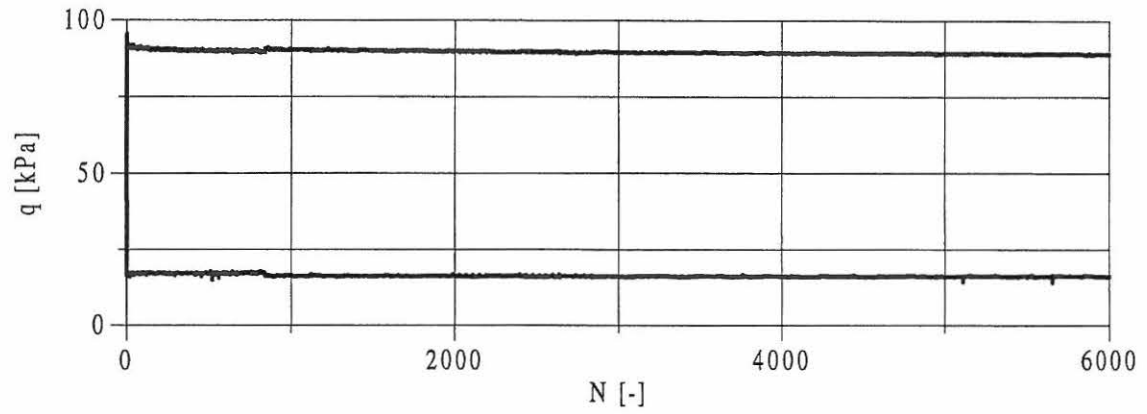
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