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Regadío Carretero, A., Sánchez Prieto, S. & Esteban, L. 2019, "Filtering of pulses from particle detectors by means of Singular Value Decomposition (SVD)", Nuclear Instruments and Methods in Physics Research Section A: Accelerators, Spectrometers, Detectors and Associated Equipment, vol. 922, pp. 257-264.

Available at <https://doi.org/10.1016/j.nima.2019.01.028>

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Filtering of pulses from particle detectors by means of Singular Value Decomposition (SVD)

Alberto Regadío^{a,*}, Sebastián Sánchez-Prieto^b, Luis Esteban^c

^a*Electronic Technology Area, Instituto Nacional de Técnica Aeroespacial, 28850 Torrejón de Ardoz, Spain*

^b*Department of Computer Engineering, Space Research Group, Universidad de Alcalá, 28805 Alcalá de Henares, Spain*

^c*Universidad Antonio de Nebrija, C/Pirineos, 55 28040 Madrid, Spain*

Abstract

This paper presents a novel methodology to filter pulses coming from particle detectors. It is based on variable-in-time convolutions in which one of the operands is the input pulse and the other is a vector that changes with every convolution step. This is equivalent to multiply every incoming pulse by a filtering matrix. The coefficients of this matrix are computed by applying a Singular Value Decomposition (SVD) factorization over a set of training pulses. A detailed explanation of this SVD-filtering methodology, a noise filtering analysis, simulations and filtering of pulses coming from a neutron monitor were carried out to verify its feasibility.

Keywords: Digital pulse processing, Pulse filtering, Noise, Dimensionality reduction, SVD

1. Introduction

The indirect or direct interaction of particles with the appropriate particle detector produces a charge build up or if accelerated, pulses of current. These pulses are converted to voltage by means of trans-impedance amplifiers and fed into subsequent processing stages. These voltage pulses carry useful information about the incident particles such as type, energy or angle of impact [1]. These outgoing pulses are always mixed with noise, limiting the accuracy of the measurement.

In particle detection systems the dominating noise is generated both in the detector and in the detector readout electronics, specially in the analog front-end. The readout electronics is typically implemented with discrete analog components (resistors, diodes, field-effect transistors, etc.) and by hence affected by parasitic effects. This noise causes the masking of information present in the signal.

Part of the noise is the result of fundamental physical processes and quantities such as the discrete nature of electric charge and therefore it cannot be avoided [1]. However, its effects can be reduced by using proper

*Corresponding Author

Email addresses: regadioca@inta.es (Alberto Regadío), sebastian.sanchez@uah.es (Sebastián Sánchez-Prieto), lesteban@nebrija.es (Luis Esteban)

28 noise filtering strategies. A key to successful noise filtering is to accurately model the noise that appears in
29 the system. This noise model enables the design of filters that maximize the Signal-to-Noise Ratio (SNR).

30 Filtering of detector pulses is crucial in most nuclear pulse processing applications. A generic pulse
31 filter attenuates or even removes a certain frequency interval of frequency components from a pulse. These
32 frequency components are typically noise though there are situations in which a filter is used to remove some
33 part of the pulse as well.

34 With the development of integrated circuits, digital electronics has also been used for particle detectors,
35 even replacing the use of analog electronics in some detection stages such as shaping. The use of digital
36 electronics provides many advantages, for instance, the inclusion of several stages in a single integrated
37 circuit, lower volume and consumption or reconfigurability when implemented in Field Programmable Gate
38 Arrays (FPGAs). However, this change could increase the complexity of particle detector backends and
39 increase the number of noise sources that appear due to the new elements added such as Analog to Digital
40 Converters (ADC) [2].

41 The two digital systems commonly used in particle detection systems are filters and pulse shapers. There
42 are two types of digital filters, Finite Impulse Response (FIR) and Infinite Impulse Response (IIR). The FIR
43 filtering of any pulse can be analyzed from the perspective of the convolution of a vector, which represents
44 the filter. In this paper, the convolution is replaced by a multiplication matrix which is denominated
45 filtering matrix. As exposed in Section 2, the multiplication by a filtering matrix is equivalent to making a
46 convolution in which one of the elements is the input pulse and the other is a value that changes with every
47 convolution step. To achieve an optimal filtering it is necessary to find out the matrix entries that optimize
48 the SNR.

49 Singular Value Decomposition (SVD) is a non-parametric factorization of real (or complex) matrices.
50 SVD is explained in more detail in Section 3. It has been already used in areas related to particle spectroscopy
51 such as histogram creation [3] and pulse unfolding [4]. In [3] SVD is also used for filtering but, unlike
52 the proposed method of this article, it obtains all the SVD values of the pulses at the same time (an
53 autofiltering) without distinguishing between training pulses and real pulses. It has also been used to unfold
54 entire histograms [5, 6]. In this work, the elements of the filtering matrix are obtained using the method
55 explained in Section 4. This method is suitable for real-time implementation using either hardware or
56 software. Finally, a filtering noise analysis is explained in Section 5 and the results of applying this method
57 on pulses are explained in Section 6.

58 **2. Convolution as a matrix multiplication**

59 As stated in Section 1, the result of filtering a digital input pulse $\mathbf{x} = x[n]$ with a Finite Response Filter
60 (FIR) in time-domain can be represented by a convolution. This operation, in turn, can be represented

61 as a matrix multiplication whose impulse response $\mathbf{m} = m[n]$ is a Toeplitz matrix [7] (i.e. its descending
 62 diagonals from left to right are constant). For example, the convolution of \mathbf{x} and \mathbf{m} can be rewritten as

$$\mathbf{y} = \mathbf{m} * \mathbf{x} = \mathbf{M}\mathbf{x} = \begin{pmatrix} M_1 & 0 & \dots & 0 & 0 \\ M_2 & M_1 & \dots & \vdots & \vdots \\ M_3 & M_2 & \dots & 0 & 0 \\ \vdots & M_3 & \dots & M_1 & 0 \\ M_{l-1} & \vdots & \dots & M_2 & M_1 \\ M_l & M_{l-1} & \ddots & \vdots & M_2 \\ 0 & M_l & \dots & M_{l-2} & \vdots \\ 0 & 0 & \dots & M_{l-1} & M_{l-2} \\ \vdots & \vdots & \vdots & M_l & M_{l-1} \\ 0 & 0 & 0 & \dots & M_l \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \\ \vdots \\ x_n \end{pmatrix} \quad (1)$$

For instance, let define the following normalized low-pass FIR filter whose impulse response in the z -domain is

$$m(z) = \frac{1}{3} (1 + z^{-1} + z^{-2}) \quad (2)$$

Consequently, the associated matrix to filter a pulse of length $l = 6$ is

$$\mathbf{M} = \frac{1}{3} \begin{pmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ 1 & 1 & 0 & 0 & 0 & 0 \\ 1 & 1 & 1 & 0 & 0 & 0 \\ 0 & 1 & 1 & 1 & 0 & 0 \\ 0 & 0 & 1 & 1 & 1 & 0 \\ 0 & 0 & 0 & 1 & 1 & 1 \end{pmatrix} \quad (3)$$

63 In the case that \mathbf{M} was not a Toeplitz matrix but a generic matrix, \mathbf{M} will actually be a variable-in-time
 64 convolution. It implies that the convolution coefficients (i.e. the filter) are changing for every \mathbf{x} element,
 65 which is useful to improve the filtering results. In this paper, a novel procedure to obtain an efficient \mathbf{M}
 66 against noise using SVD decomposition is proposed. Thi method is explained in Sections 3 and 4.

67 3. Singular Value Decomposition

68 **The** SVD algorithm is a non-parametric (also called *blind*) factorization of real (or complex) matrices.
 69 Additional information about SVD and its implementation can be found in [7]. In this paper, only real
 70 numbers are used. Whether we apply SVD to an arbitrary matrix $\mathbf{X} \in \mathbb{R}^{l \times n}$, we obtain

$$\mathbf{X} = \mathbf{U}\mathbf{S}\mathbf{V}^\top \quad (4)$$

71 where, for $n < l$, $\mathbf{U} \in \mathbb{R}^{n \times n}$, $\mathbf{S} \in \mathbb{R}^{n \times n}$ and $\mathbf{V}^\top \in \mathbb{R}^{n \times l}$.

72 In this decomposition, \mathbf{U} is an orthogonal matrix (i.e. whose transpose \mathbf{U}^\top is also its inverse \mathbf{U}^{-1}),
73 \mathbf{S} is the diagonal matrix of eigenvalues and \mathbf{V} (which is also orthogonal) contains the eigenvectors of the
74 decomposition (that is a basis for \mathbf{X}).

75 In contrast to other blind factorization methods such as Non-Negative Matrix Factorization (NNMF)
76 or Sparse Component Analysis (SCA), the use of SVD has the advantage that the obtained eigenvalues
77 are ordered in relation to their significance [7] with respect to \mathbf{X} . These eigenvalues provide a basis of n
78 dimensions. According to [3] the most significant dimensions considered are the signal and the lowest noise
79 and therefore they can be removed.

80 This filter mitigates any type of noise including white, brownian or $1/f$ following the same procedure
81 described above.

82 The variability of the pulses, both in height and shape, is learned by the filter in the same way than a
83 neural network. In fact, the SVD method is equivalent to using an autoencoder neural network with a linear
84 hidden unit [8]. The difference is that the main components of SVD are represented on an orthogonal basis
85 while those of the neural network do not have to be necessary orthogonal.

86 4. Procedure

87 It is known that the value of a vector (actually a tensor) can be expressed in terms of a basis and its
88 components and that it is independent from the chosen reference system. Keeping this in mind, the main
89 idea of this algorithm is to calculate an alternative basis (of reduced dimensions) using training pulses and fit
90 the incoming pulses in it using a change of basis (multiplying by \mathbf{V}). As a result of the fitting of the incoming
91 pulses in the alternative basis a series of components have to be obtained. Afterwards, these components
92 are transformed to the original basis again (by multiplying by \mathbf{V}^{-1}) in order to obtain the filtered incoming
93 pulses.

94 For this purpose, let \mathbf{X}_t be a set of n different training pulses of length equal to l clock cycles (dimensions)
95 each, $\mathbf{X}_t \in \mathbb{R}^{n \times l}$. These pulses can be obtained from a real detector or can be generated automatically
96 without noise (the difference in results is explained in Section 6). In order to obtain \mathbf{V} , when $n < l$, the
97 value of \mathbf{X}_t is factorized using SVD (4)

$$\mathbf{X}_t = \mathbf{U}\mathbf{S}\mathbf{V}^\top = \mathbf{H}_t\mathbf{V}^\top \quad (5)$$

98 where $\mathbf{H}_t \in \mathbb{R}^{n \times n}$ are the components of the training pulses and $\mathbf{V} \in \mathbb{R}^{l \times n}$ are their basis. \mathbf{H}_t is not
99 used for this algorithm. If $n > l$, \mathbf{V} it must be replaced by \mathbf{U} and vice versa. However, in this work, it is

100 assumed that a sufficient number of samples is taken from the pulses to filter them correctly compared to
 101 the number of training pulses and therefore $n < l$.

102 On the other hand, a number of k digital pulses coming from detectors of length l each are embedded
 103 into a matrix \mathbf{X} . These pulses contain noise that can be reduced if they are analyzed according to the
 104 previously obtained basis \mathbf{V} . Thus, whenever a new pulse ($k = 1$) or a set of new k pulses are detected,
 105 their components are obtained by applying $\mathbf{H} = \mathbf{U}\mathbf{S}$ on Eq. (4). It yields

$$\mathbf{H} = \mathbf{V}^\top \mathbf{X} \quad (6)$$

106 where $\mathbf{H} \in \mathbb{R}^{n \times k}$ are the components of the test pulses according to the \mathbf{V} basis.

107 In order to clear up the pulse, the first s eigenvectors of the diagonal matrix \mathbf{S} are chosen and the others
 108 are set to zero. Since $\mathbf{U}\mathbf{S} = \mathbf{H}$, this is equivalent to keep the first s rows of \mathbf{H} and set the others to zero.
 109 The result of this operation is represented by $\mathbf{H}_s \in \mathbb{R}^{n \times k}$ matrix

$$\mathbf{H}_s = \begin{pmatrix} H_{11} & H_{12} & \dots & H_{1k} \\ H_{21} & H_{22} & \dots & H_{2k} \\ \vdots & \vdots & \ddots & \vdots \\ H_{s1} & H_{s2} & \dots & H_{sk} \\ 0 & 0 & \dots & 0 \\ \vdots & \vdots & \vdots & \vdots \end{pmatrix} \quad (7)$$

110 Finally, to obtain the filtered pulse \mathbf{Y}

$$\mathbf{Y} = \mathbf{V}\mathbf{H}_s \quad (8)$$

111 where $\mathbf{Y} \in \mathbb{R}^{l \times k}$.

112 Logically, $\mathbf{H}_n = \mathbf{H}$ and implies that $\mathbf{Y} = \mathbf{V}\mathbf{V}^\top \mathbf{X}$ as explained in Section 5.3.

113 Distinguishing between training and real pulses implies a significant improvement of the results. To sum
 114 up, a scheme of the filtering performed in this section is shown in Fig. 1. Note that with this filtering
 115 scheme, both a single pulse (case $k = 1$) or a set of k pulses in parallel can be filtered. In the next section,
 116 the efficiency of this filtering approach against noise is analyzed.

117 5. Noise filtering analysis

118 The objective of this analysis is to calculate how the SVD-filtering improves the SNR compared to other
 119 FIR filters. As stated in Section 2, these FIR filters are modeled as Toeplitz matrices. The noise filtering
 120 study is carried out in time-domain in a similar way to [9–11] for analog shaping. In these works, the
 121 assumption that an average number of delta functions (white noise) and step functions (brownian noise) are

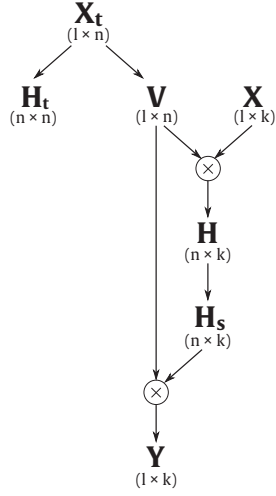


Figure 1: Diagram of the SVD-filtering.

122 produced in the input circuit by the noise sources is made. Both indices are inversely proportional to the
 123 SNR. In accordance with [11], white and brownian noise are represented by F_v and F_i respectively and they
 124 are equal to:

$$F_i = \frac{1}{S^2} \int_0^\infty W^2(t) dt \quad (9)$$

$$F_v = \frac{1}{S^2} \int_0^\infty \left(\frac{dW}{dt} \right)^2 dt \quad (10)$$

125 where S is the signal amplitude (in case of filters, it is assumed that $S = 1$ because it is not need it to
 126 amplify the signal, just to filter it). $W(t)$ represents the residual effect of a single unit noise element. $W(t)$
 127 can be determined analytically because the filter is known. For time-invariant pulse shaping, $W(t)$ is the
 128 system's impulse response for a short input pulse with the peak output signal normalized to unity. For
 129 time-variant systems (e.g. gated integrators), $W(t)$ can be also calculated with the method described in [9].
 130 The impact of more general noise types such as those outlined in [12] are beyond of the scope of this paper.

131 Eq. (9, 10) are applicable to both analog and digital shapers taking into account that integrals and
 132 derivatives must be changed to summations and subtractions in the digital shapers also the residual effect
 133 must be discretized

$$F_i = \frac{1}{S^2} \sum_{n=0}^{\infty} (W[n])^2 \Delta t \quad (11)$$

$$F_v = \frac{1}{S^2} \sum_{n=0}^{\infty} \left(\frac{W[n] - W[n-1]}{\Delta t} \right)^2 \Delta t \quad (12)$$

134 where Δt is the clock period of the discrete filter.

135 In the same way that the cited works and in order to quantify how the SVD-filtering improves the SNR
 136 compared to more traditional FIR filters, these two last formulas were adapted to replace $W[n]$ by \mathbf{M} .

137 5.1. Response to white noise

138 As it is pointed out by [9], a unit of white noise (also called delta noise in the cited reference) can be
 139 modeled as a discrete Dirac delta function. In discrete signal processing, this function can be represented by
 140 $\delta = (1 \ 0 \ 0 \ \dots)^\top$. However, when an unit of white noise modifies a pulse, it can happen along all the pulse
 141 duration. For this reason, let us also define δ_i as δ delayed i cycles, where i can take any discrete value from
 142 0 to the length of the pulse l . The impact of white noise in the pulse measurement is the mean value of all
 143 of these probabilities. Therefore

$$F_v = \frac{1}{l} \sum_{i=0}^l \sum_{j=0}^k (M_{ij} \delta_i)^2 \quad (13)$$

144 where M_{ij} are the entries of \mathbf{M} .

This equation can be simplified as

$$F_v = \frac{1}{l} \sum_{i=0}^l \sum_{j=0}^k (M_{ij})^2 \quad (14)$$

Lets compare this last equation with (12) using the FIR filter defined in (2). Using (12) and normalizing
 $S = 1$ and $\Delta t = 1$ the white noise index is obtained as

$$F_v = 3 \left(\frac{1}{3} \right)^2 = \frac{1}{3}$$

On the other hand, using Eq. (14) with the matrix (2) associated to the example filter for input signals
 of length $l = 6$, the same result is obtained:

$$F_v = \frac{1}{6} \sum_{i=0}^5 \sum_{j=0}^5 \begin{pmatrix} \frac{1}{3^2} & 0 & 0 & 0 & 0 & 0 \\ \frac{1}{3^2} & \frac{1}{3^2} & 0 & 0 & 0 & 0 \\ \frac{1}{3^2} & \frac{1}{3^2} & \frac{1}{3^2} & 0 & 0 & 0 \\ 0 & \frac{1}{3^2} & \frac{1}{3^2} & \frac{1}{3^2} & 0 & 0 \\ 0 & 0 & \frac{1}{3^2} & \frac{1}{3^2} & \frac{1}{3^2} & 0 \\ 0 & 0 & 0 & \frac{1}{3^2} & \frac{1}{3^2} & \frac{1}{3^2} \end{pmatrix} = \frac{1}{3}$$

145 5.2. Response to brownian noise

146 As pointed out by [9], an unit of brownian noise (also called step noise in the cited reference) can be
 147 modeled as a step signal.

148 Thus, this function can be modeled simply as $\mathbf{u} = (1 \ 1 \ 1 \ 1 \ \dots)^\top$. Thereby, to calculate F_i , we have to
 149 divide the effect of filters on brownian noise by l in the same way than F_v

$$F_i = \sum_{i=0}^l \left(\sum_{j=0}^k M_{ij} \right)^2 \quad (15)$$

150 Note that, unlike white noise and assuming that the number of events multiplied by the length of the pulse
 151 is small compared to the total past time, we can consider that all brownian noise pulse turned up before the
 152 pulse is captured. For this reason, delaying \mathbf{u} has no sense because it gives the same result and therefore no
 153 mean is worked out for this equation.

Following the previous example, lets compare this last equation with (11) using the FIR filter defined in
 (2). If we feed this filter with \mathbf{u} , the output pulse is $(\frac{1}{2} \frac{2}{3} 1 1 1 1)$. Using (11) and normalizing $S = 1$ and
 $\Delta t = 1$. The brownian noise index is obtained

$$F_i = \frac{1}{2^2} + \frac{2}{2^2} + 1 + 1 + 1 + 1 = 4.556$$

On the other hand, using Eq. (15) with the matrix (2) associated to the example filter for input signals
 of length $l = 6$, we obtain the same result

$$F_i = \sum_{i=0}^l \left(\frac{1}{3} \begin{pmatrix} \begin{pmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ 1 & 1 & 0 & 0 & 0 & 0 \\ 1 & 1 & 1 & 0 & 0 & 0 \\ 0 & 1 & 1 & 1 & 0 & 0 \\ 0 & 0 & 1 & 1 & 1 & 0 \\ 0 & 0 & 0 & 1 & 1 & 1 \end{pmatrix} \begin{pmatrix} 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \end{pmatrix} \right)^2 = 4.556$$

154 Using (14, 15) it is observed that, as explained in [9], the effect of white noise is inversely proportional
 155 to the length of the pulse l whereas brownian noise is proportional to l .

156 Unfortunately, when $s < n$ the filtering operation is not linear, there is not a matrix \mathbf{M} from which to
 157 calculate F_i nor F_v but they have to be calculated in three steps (6, 7, 8). Next section, is focused on the
 158 analysis of the case when $s = n$ (that is $\mathbf{H}_s = \mathbf{H}_n$, which is the only case where the filtering operation is
 159 linear, to calculate the noise indexes (see Section 6.1) and then calculate the effect on noise of varying s .

160 5.3. Particular case for $\mathbf{H} = \mathbf{H}_n$

As stated in Section 4, when all the eigenvalues are taken to filter the signal, that is $\mathbf{H} = \mathbf{H}_n$, Eq. (8)
 is rearranged as

$$\mathbf{Y} = \mathbf{V}\mathbf{V}^T \mathbf{X} \quad (16)$$

161 The key to analyze the impact of noise is to find out what represents $\mathbf{V}\mathbf{V}^T$. It is known that \mathbf{V} is an
 162 orthogonal matrix i.e. $\mathbf{V}^T = \mathbf{V}^{-1}$ but it is also known that \mathbf{V} is not (always) symmetric. Therefore, it can
 163 be concluded that \mathbf{V}^T is the Moore-Penrose pseudoinverse [13, 14] of the orthogonal matrix \mathbf{V} .

Pseudoinverse matrices have specific properties depending of their dimension. Let define $\mathbf{I}_L = \mathbf{V}^\top \mathbf{V}$ and $\mathbf{I}_R = \mathbf{V}\mathbf{V}^\top$ where, as stated in (5), $\mathbf{V} \in \mathbb{R}^{l \times n}$. Then,

$$\mathbf{I}_L = \mathbf{I} \Leftrightarrow n < l \quad (17)$$

$$\mathbf{I}_R = \mathbf{I} \Leftrightarrow n > l \quad (18)$$

$$\mathbf{I}_L = \mathbf{I}_R = \mathbf{I} \Leftrightarrow n = l \quad (19)$$

164 where \mathbf{I} is the identity matrix.

165 Then, according to Eq. (16), when $n > l$, $\mathbf{V}\mathbf{V}^\top = \mathbf{I}$ and the system does not filter at all. This is also
166 applicable when $s < n$, i.e. following the steps (6, 7, 8).

167 From all of this it can be concluded that SVD-filtering only works when $n > l$ because, otherwise, in Eq.
168 (4), $\mathbf{U} \in \mathbb{R}^{n \times l}$, $\mathbf{S} \in \mathbb{R}^{l \times l}$ and $\mathbf{V}^\top \in \mathbb{R}^{l \times l}$. Therefore, \mathbf{V} is orthogonal and symmetric and $\mathbf{V}\mathbf{V}^\top = \mathbf{V}^\top \mathbf{V} = \mathbf{I}$.
169 In conclusion, the constraint $n < l$ is mandatory for the filter to work.

170 A property of \mathbf{I}_R and \mathbf{I}_L is that $\mathbf{I}_R^2 = \mathbf{I}_R$ and $\mathbf{I}_L^2 = \mathbf{I}_L$ hence the same output is obtained whether we
171 apply the filter once or several times in cascade. This is also applicable when we filter \mathbf{X} is filtered when
172 $s < n$.

173 In the case of white noise, when $\mathbf{H} = \mathbf{H}_s$, \mathbf{M} value of Eq. (14) is replaced by $\mathbf{V}\mathbf{V}^\top$. Elaborating this
174 equation, it yields

$$F_v = \frac{1}{l} \sum_{\text{entries}} \mathbf{V}^\top \mathbf{V} \quad (20)$$

175 where *entries* are every entry of the matrix $\mathbf{V}^\top \mathbf{V}$.

According to (17), when $n < l$, which is mandatory as stated before, $\mathbf{V}^\top \mathbf{V} = \mathbf{I}$, this identity matrix has
dimensions $n \times n$. Therefore,

$$F_v = \frac{n}{l} \quad (21)$$

176 In case of brownian noise, when $\mathbf{H} = \mathbf{H}_n$, Eq. (15) leads up to

$$F_i = \frac{1}{l} \sum_{\text{entries}} \mathbf{V}\mathbf{V}^\top \quad (22)$$

177 In this case, the product $\mathbf{V}\mathbf{V}^\top \in \mathbb{R}^{l \times l}$.

178 With these two indexes it can be concluded that, since $n < l$, F_i is greater than F_v . In addition, in the
179 same way that common filters and shapers [9, 12], the effect of white noise is inversely proportional to the
180 length of the pulse l whereas brownian noise is proportional to l . In the next section, these assumptions are
181 verified.

182 **6. Results**

183 A set of simulations and tests to check the SVD-filtering in a real environment has been performed with
 184 the aim of checking that it works efficiently.

185 The SVD-filter is designed to work on acquisition chains at the output of the preamplifier or at the
 186 output of the shaping stage because at this point there is still noise left: in Section 6.1, it was placed at
 187 the output of the shaping stage to highlight the shape of the shaper, especially how flat is the output of
 188 the trapezoidal shaper (although its height varies). This flatness can help to the pulse height analyzer to
 189 measure the height of the pulse. In Section 6.2, it was placed at the output of the preamplifier, which is a
 190 more realistic scenario.

191 *6.1. Results with simulated pulses and noise*

192 In this test, a set of triangular, trapezoidal and cusp-like pulses of random heights and without noise were
 193 created (\mathbf{X}^*). Then, white, brownian and $1/f$ noises were added to these pulses to yield \mathbf{X} . These pulses
 194 were filtered using the SVD-filtering method to verify how the SNR was improved. The detection chain
 195 scheme was detector→shaper→filter, consequently \mathbf{X} are the pulses at the output of the shaper. Despite
 196 that the brownian noise is generated mainly at the detector, we suppose that both noise types are generated
 197 before the filtering for comparison purposes.

198 Two examples of filtering using SVD-filtering are shown in Figure 2 and 3. The length of all the pulses of
 199 these two figures are $l = 100$ and the number of learning pulses were $n = 3$. For all cases, \mathbf{H} was transformed
 200 to \mathbf{H}_1 . However, for this concrete experiment, similar results were obtained with both \mathbf{H} and \mathbf{H}_1 .

201 The noise indexes F_v and F_i defined on (21) and (22), respectively are listed on Table 1. In this Table,
 202 the noise indexes for a generic low-pass filter were also added for comparison purposes. The transfer function
 203 of this filter in the z -domain is

$$h(z) = \frac{1}{5} (1 + z^{-1} + z^{-2} + z^{-3} + z^{-4}) \quad (23)$$

204 For this filter, the filtering matrix is not an orthogonal matrix but a Toeplitz matrix, as explained in
 205 Section 2. Therefore, to calculate the noise indexes, Eq. (14, 15) had to be used instead of (21, 22).

Table 1: Noise indexes value for the tests shapers and for a generic FIR low-pass filter for $s = k$.

Shaper	F_v	F_i
Triangular	0.030	0.748
Trapezoidal	0.030	0.840
Cusp-like	0.030	0.694
Low-pass	0.196	0.972

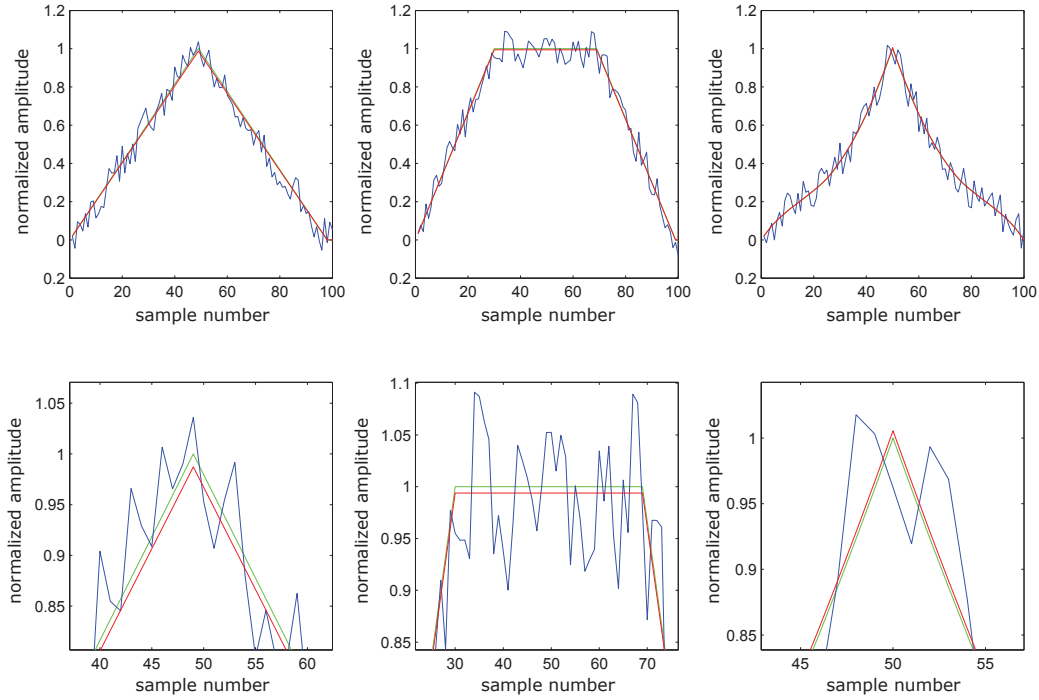


Figure 2: Example of white noise filtering for a triangular, trapezoidal and cusp-like pulse. The green pulse is the original one without noise \mathbf{X}^* whose amplitude is equal to 1, the blue pulse is the input with noise \mathbf{X} and the red pulse is the filtered one \mathbf{Y} . The panels below show a detailed view of the peak of the above panels.

206 When $s < n$, F_v remains constant but F_i changes. These changes are illustrated in Figure 4. It can be seen
 207 that F_i oscillates around the values given in Table 1 because F_i is proportional to the squared area of the
 208 pulse.

209 It can be observed that F_v is lowered to a constant value n/l , which is independent of the pulse shape, as
 210 predicted in (21), whereas F_i indicates that the brownian noise is harder to filter using this method. The
 211 low-pass filter gives worse results in both indexes than the other filters.

212 These two indexes support the assessment that the SVD-filtering filters noise in a more efficient way than
 213 FIR filters. However, when the pulses from the particle detector are processed using Pulse Height Analysis
 214 (PHA), a more realistic way to obtain the system resolution is to measure the relative error Δ of each pulse
 215 \mathbf{x} contained in \mathbf{X} , defined as

$$\Delta = \text{mean} \left(\frac{|\max(\mathbf{x}) - \max(\mathbf{x}^*)|}{\max(\mathbf{x}^*)} \right) \quad (24)$$

216 where *mean* stands for the mean value of every pulse contained in \mathbf{X} . In the case of trapezoidal shaping, the
 217 maximum value of the pulse is the mean value of its plateau. To calculate this mean value, the number of
 218 filtered pulses were $k = 200$. Using this method instead of the one explained in Section 5 we obtain similar

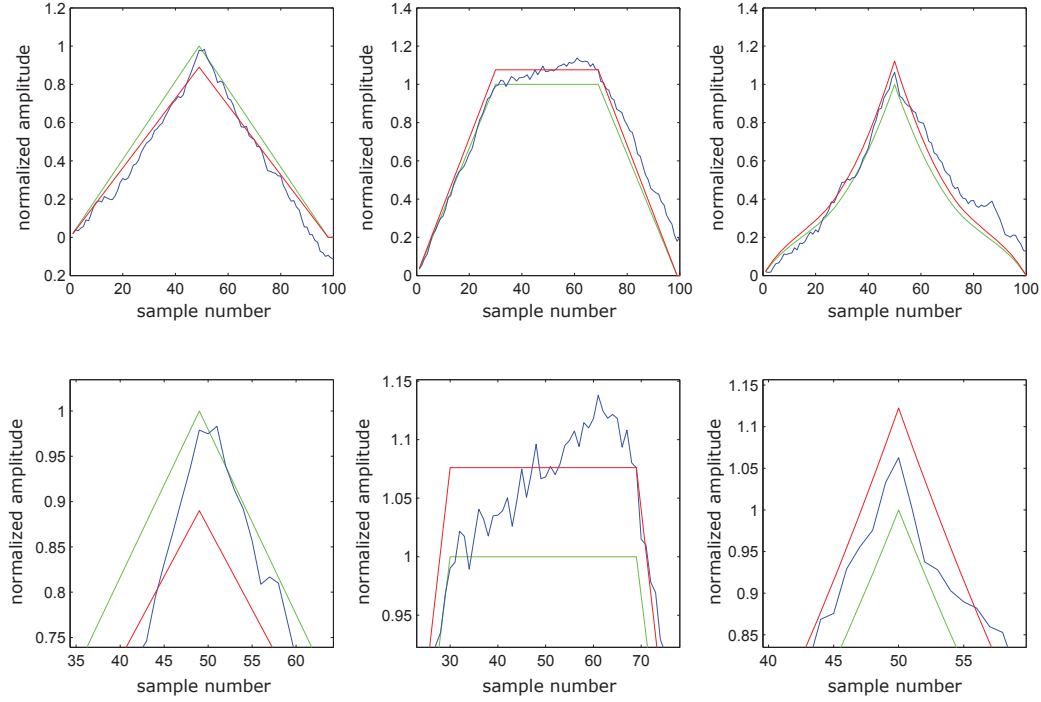


Figure 3: Example of brownian noise filtering for a triangular, trapezoidal and cusp-like pulse. The green pulse is the original one without noise \mathbf{X}^* whose amplitude is equal to 1, the blue pulse is the input with noise \mathbf{X} and the red pulse is the filtered one \mathbf{Y} . The panels below show a detailed view of the peak of the above panels.

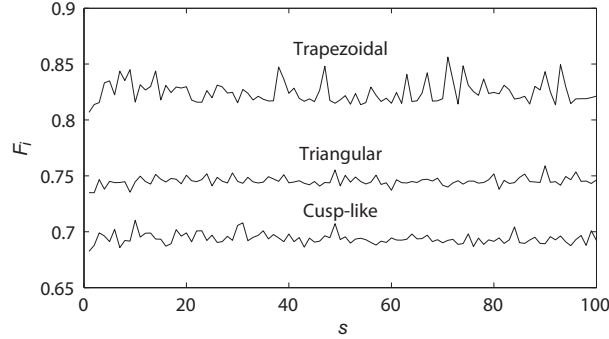


Figure 4: F_i vs s for trapezoidal (upper line), triangular, and cusp-like (lower line) for $l = 100$.

219 results. They are shown in Figure 5, 6 and 7 for white, $1/f$ and brownian noise, respectively. The straight
 220 lines indicate pulses with $l = 100$ whereas the dotted lines indicate pulses with $l = 10$. The \mathbf{V} matrices were
 221 calculated using $n = 1$, $n = 10$ and $n = 100$ training pulses (in red, green and blue, respectively). These
 222 figures also includes the low-pass filtering (depicted in black for comparison) defined in Eq. (23).

223 The blue ($n = 100$) dotted ($l = 10$) line does not appear in these figures because n is greater than l and,
 224 according to $\mathbf{V}\mathbf{V}^T = \mathbf{I}$ it is not possible. The black dotted line is not depicted in any figure because the

225 filter of (23) lowers the height of the pulses with length ($l = 10$). In fact, the error value defined in (24) is
 226 approximately one order of magnitude higher than the others.

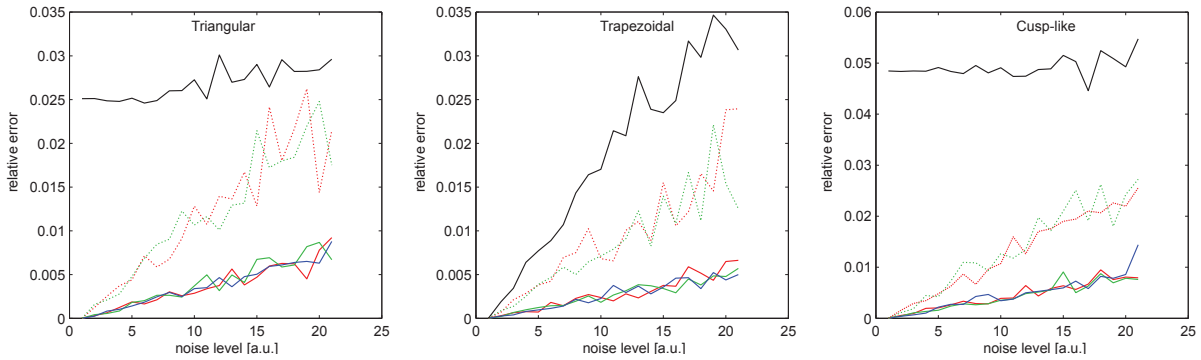


Figure 5: Level of white noise (in arbitrary units) vs. relative error (in percentage) for triangular, trapezoidal and cusp-like pulses.

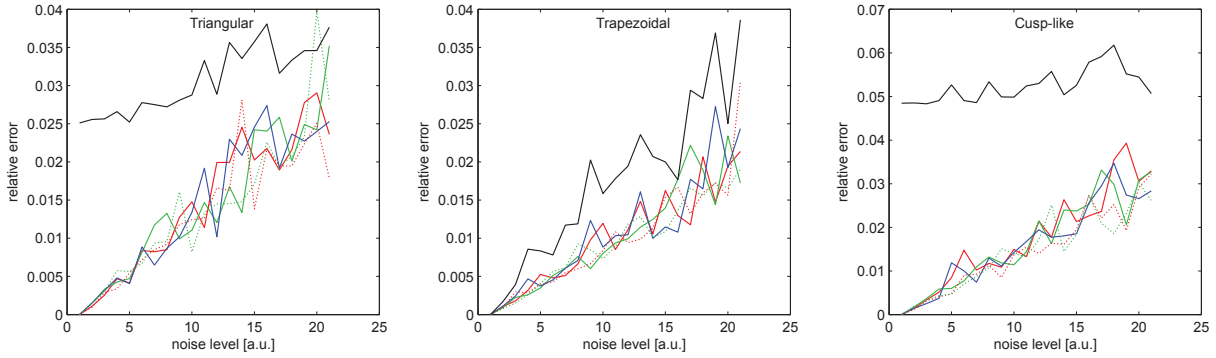


Figure 6: Level of $1/f$ noise (in arbitrary units) vs. relative error (in percentage) for triangular, trapezoidal and cusp-like pulses.

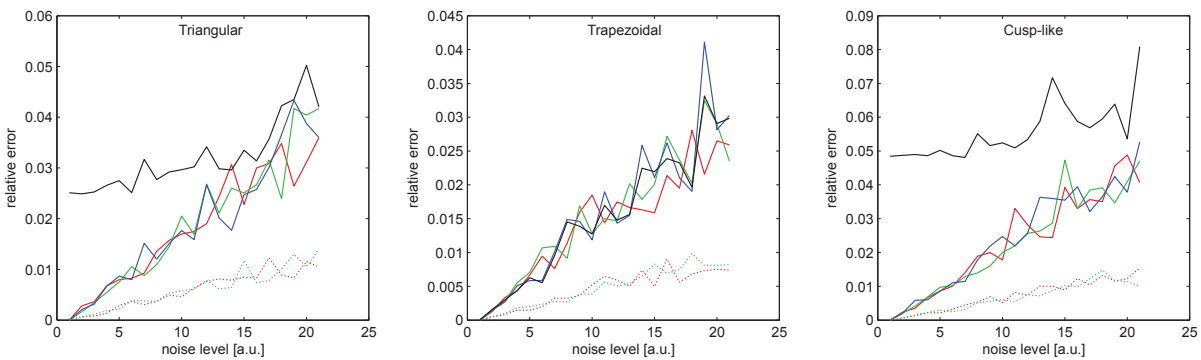


Figure 7: Level of brownian noise (in arbitrary units) vs. relative error (in percentage) for triangular, trapezoidal and cusp-like pulses.

227 These figures confirm that the pulse length is inversely proportional to the white noise effect, proportional
228 to the brownian noise effect and independent from the $1/f$ noise effect, in accordance with Section 5 and
229 [9, 11, 12]. Likewise, it can be seen that brownian noise has more impact on the SVD-filtering than white
230 noise, which were predicted by Eq. (21, 22).

231 It can be seen that this method filters the noise efficiently. In fact, when a high noise level is present,
232 the key issue is to establish a correct threshold algorithm such as the one presented in [15, 16].

233 6.2. Results with pulses from a neutron monitor

234 Finally, a test to check the proposed filtering was performed. The main objective of this test was to
235 obtain similar results to those obtained in the experiments done without SVD filtering.

236 This test was performed in the Castilla-La Mancha Neutron Monitor (CaLMa) located in Guadalajara,
237 Spain. This instrument consists of 15 proportional gas counter tubes. More information about features,
238 setup and results of this instrument can be found in [17]. In both the cited experiment and the present test,
239 an LND206 tube connected to a Canberra ACHNA98 preamplifier was used.

240 The raw data fed out from the preamplifier was digitized using a Data Acquisition system (DAQ) at
241 sampling period of $T_s = 20$ ns and storing it in a PC. Pulses stored in a text file can be used multiple times
242 without recapturing new data. In addition, it ensures that possible changes in the obtained results during
243 the test are exclusively due to digital pulse processing. The total raw data length was of 46105 pulses \times
244 1002 samples per pulse (i.e. $l = 1002$) captured during over 5 hours (from 10:20 UTC to 15:23 UTC on
245 November, 16th 2018). To separate the input pulses, a trigger threshold of 1 V without any previous digital
246 filtering was used.

247 A difference with the previous test is that the training pulses are obtained from the same source than the
248 test pulses. Thus, a conclusion obtained from this is that the more noise the training signal has, the more
249 pulses are required to reduce the noise, the larger is \mathbf{V} , and therefore more computing time is necessary
250 when processing a pulse. For this reason, a trade-off between learning pulses and computation time was
251 carried out and finally $n = 100$ and $s = 10$ were used. In Figure 9, the output of one pulse processed with
252 the SVD-filter compared to raw pulses and a low-pass FIR filter are shown. Note from this figure that
253 the low-pass filtering can remove the high frequency components which prevents the peak from reaching its
254 maximum. Therefore, altering the histogram.

255 In Figure 9, the output of six pulses processed with the same SVD-filter are shown. We can see that,
256 regardless of the shape of the pulses, the pulses are correctly filtered.

257 Since Eq. (24) cannot be used to evaluate the obtained results, because the value of \mathbf{X}^* is not known,
258 the filter quality was measured using the Full Width at Half Maximum (FWHM) which is defined as the
259 width of the distribution at a level that is just half the maximum value of the peak divided by the location
260 of the peak maximum [1].

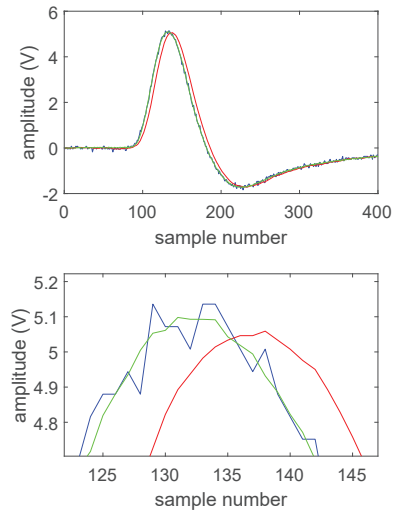


Figure 8: Example of pulse filtering. The blue pulse is the original unfiltered, the red pulse is the same pulse filtered with a low-pass filter such as (23) with order 10, the green pulse is the pulse filtered with the SVD method setting $s = 10$. The bottom panel shows a detailed view of the one above.

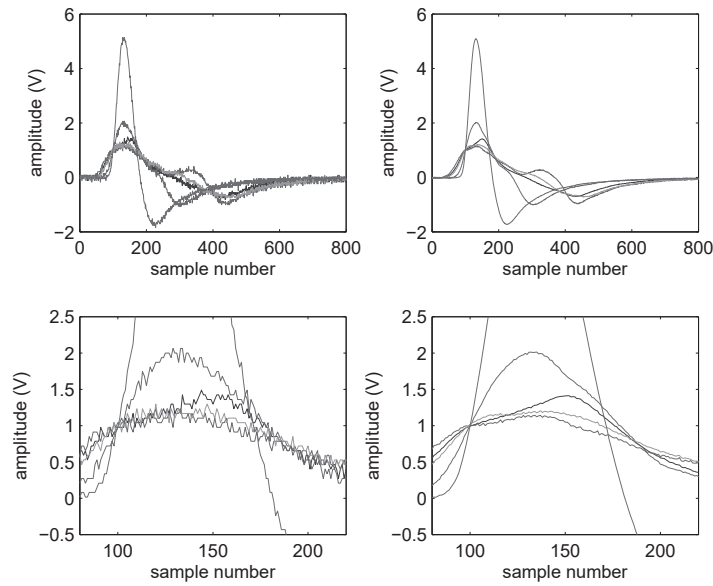


Figure 9: Example of pulse filtering on the neutron monitor. Left: Pulses from the neutron monitor without filtering. Right: Pulses filtered with the SVD-filter.

261 In Figure 10, an example of histogram is shown. To evaluate the results, in all the tests the FWHM
 262 of the pulse height histograms were similar for three cases: (a) pulses unfiltered; (b) pulses filtered with

263 a low-pass filter whose response function in z -domain is (23); (c) filtered pulse using SVD-filtering. The
 264 obtained FWHM was 0.0370, 0.0340 and 0.0375, respectively. We can observe that the FWHM obtained
 265 with SVD-filtering is slightly lower than that of unprocessed pulses. On the contrary, as it was advanced,
 266 the low-pass filter reduces the height of the pulse, lowering its FWHM.

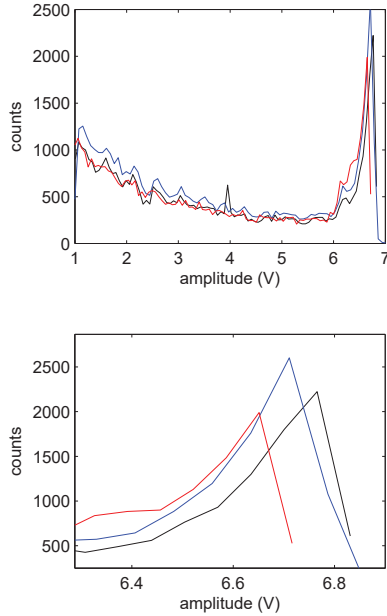


Figure 10: Histogram obtained using different filtering methods. The blue pulse is the original one unfiltered, the red pulse is the same pulse filtered with a low-pass filter of order 10, the green pulse is the pulse filtered with the SVD method setting $s = 800$. The panel below show a detailed view of the peaks.

267 Additional experiments showed that as s decreases, the filtered pulses (Fig. 9) are smoother. However,
 268 a decrease in the FWHM value begins to be noticed. Thus, it can be concluded that a good filtering not
 269 always implies a significant reduction of the FWHM. Moreover, for this concrete experiment, oscillations on
 270 the FWHM were detected for small variations of either s and l .

271 To finish, it has been seen from the observations that this method does not work properly with pile-up
 272 pulses. This fact has been addressed also in previous works such as [3].

273 7. Conclusions and future work

274 A novel filtering technique has been presented in this article. This technique is a time-variant convolution
 275 calculated using matrices. These matrices are obtained from SVD and provides a filtering quality that often
 276 improves that of traditional filters. This method filters noise as traditional filters do, that is, the length of

277 the pulse is proportional to the brownian noise and inversely proportional to the white noise. Despite being
278 less susceptible to white noise, it is more susceptible to brownian noise. Simulation and tests with pulses
279 coming from a neutron monitor were performed to evaluate its performance. The constraint of this method
280 is that the number of pulses to calculate the \mathbf{V} used to filter pulses must be lower than the length in cycles of
281 a single pulse. Besides, when the pulses used to calculate \mathbf{V} are noisy, additional training pulses are needed,
282 increasing the computation time. Noise indexes measurement supports the assessment that the SVD-filtering
283 filters noise in more an efficient way than FIR filters. Furthermore, practical tests demonstrate that lowering
284 the value of s (number of eigenvalues) improves the FWHM. With all this, this method is relatively easy to
285 implement (just matrix multiplication and a threshold mechanism are necessary) and therefore suitable for
286 particle detection spectroscopy.

287 As future work, alternative linear and non-linear techniques will be implemented to substitute the SVD
288 factorization method used to find out the basis.

289 Acknowledgments

290 This work has been supported by the Spanish Administration as part of the project with Ref. ESP2017-
291 88436-R. The authors thank the CaLMa Team for technical support and for providing the CaLMa facility.

292 Bibliography

293 References

- 294 [1] M. Nakhostin, Signal Processing for Radiation Detectors, Wiley (2018).
- 295 [2] V. T. Jordanov, K. V. Jordanova, IEEE International Conference on Advancements in Nuclear Instrumentation Measure-
296 ment Methods and their Applications (2011) 1.
- 297 [3] D. Yan et al., Journal of Low Temperature Physics 184 (2016) 397.
- 298 [4] A. Hëker, V. Kartvelishvili, Nuclear Instruments and Methods in Physics Research A 372 (1996) 469.
- 299 [5] I. Sandberg, et al., IEEE Transaction on Nuclear Science 59 (2012) 1105.
- 300 [6] V. Maget, et al., IEEE Transaction on Nuclear Science 61 (2012) 1687.
- 301 [7] G. H. Golub, C. F. Van Loan, Matrix Computations 4th ed, The John Hopkins University Press (2013).
- 302 [8] G. D. Clifford, HST582J/6.555J/16.456J Biomedical Signal and Image Processing (2005) 43.
- 303 [9] F. S. Goulding, Nuclear Instruments and Methods 100 (1972) 493.
- 304 [10] F. S. Goulding, Nuclear Instruments and Methods 485 (2002) 653.
- 305 [11] C. Patrignani et al. (Particle Data Group), Chin. Phys. C, 40, 100001 (2016) 477.
- 306 [12] A. Regadío, J. Tabero, S. Sánchez-Prieto, Nuclear Instruments and Methods in Physics Research A 811 (2016) 25.
- 307 [13] E. H. Moore, Bulletin of the American Mathematical Society 26.9 (1920) 394.
- 308 [14] R. Penrose, Proceedings of the Cambridge Philosophical Society 51 (1955) 406.
- 309 [15] V. T. Jordanov, D. L. Hall, M. Kastner, IEEE Nuclear Science Symposium Conference 1 (2002) 140.
- 310 [16] H. Kim, et al., Nuclear Instruments and Methods in Physics Research A 602 (2009) 618.
- 311 [17] J. Medina, et al., Nucl. Instrum. Methods Phys. Res. A 727 (2013) 97.