# POLITECNICO DI TORINO Repository ISTITUZIONALE

Experimental validation of machine-learning based spectral-spatial power evolution shaping using Raman amplifiers

### Original

Experimental validation of machine-learning based spectral-spatial power evolution shaping using Raman amplifiers / Soltani, Mehran; Da Ros, Francesco; Carena, Andrea; Zibar, Darko. - In: OPTICS EXPRESS. - ISSN 1094-4087. - ELETTRONICO. - 30:25(2022), pp. 45958-45969. [10.1364/OE.475873]

Availability:

This version is available at: 11583/2984837 since: 2024-01-04T16:48:49Z

Publisher:

Optica Publishing Group

Published

DOI:10.1364/OE.475873

Terms of use:

This article is made available under terms and conditions as specified in the corresponding bibliographic description in the repository

### Publisher copyright

Optica Publishing Group (formely OSA) postprint versione editoriale con OAPA (OA Publishing Agreement)

© 2022 Optica Publishing Group. Users may use, reuse, and build upon the article, or use the article for text or data mining, so long as such uses are for non-commercial purposes and appropriate attribution is maintained. All other rights are reserved.

(Article begins on next page)

# **Experimental validation of machine-learning** based spectral-spatial power evolution shaping using Raman amplifiers

MEHRAN SOLTANI, 1,\* D FRANCESCO DA ROS, 1 D ANDREA CARENA.<sup>2</sup> D AND DARKO ZIBAR<sup>1</sup>

Abstract: We experimentally validate a real-time machine learning framework, capable of controlling the pump power values of Raman amplifiers to shape the signal power evolution in two-dimensions (2D): frequency and fiber distance. In our setup, power values of four first-order counter-propagating pumps are optimized to achieve the desired 2D power profile. The pump power optimization framework includes a convolutional neural network (CNN) followed by differential evolution (DE) technique, applied online to the amplifier setup to automatically achieve the target 2D power profiles. The results on achievable 2D profiles show that the framework is able to guarantee very low maximum absolute error (MAE) (<0.5 dB) between the obtained and the target 2D profiles. Moreover, the framework is tested in a multi-objective design scenario where the goal is to achieve the 2D profiles with flat gain levels at the end of the span, jointly with minimum spectral excursion over the entire fiber length. In this case, the experimental results assert that for 2D profiles with the target flat gain levels, the DE obtains less than 1 dB maximum gain deviation, when the setup is not physically limited in the pump power values. The simulation results also prove that with enough pump power available, better gain deviation (less than 0.6 dB) for higher target gain levels is achievable.

© 2022 Optica Publishing Group under the terms of the Optica Open Access Publishing Agreement

#### Introduction

Distributed Raman amplifiers (DRAs) present several advantages over the erbium doped fiber amplifiers (EDFAs) including lower noise figure (NF), and flexibility in power evolution design by adjusting the pump power and wavelength values [1,2]. Due to multi-pumping scheme, DRAs are also a practical solution to amplify a broad range of wavelengths beyond the C-band and increase the available transmission capacity [3]. One approach in designing Raman amplifiers is to optimize the pump power and wavelength values to obtain a desired signal power evolution shape, jointly in spectral and spatial (fiber distance) domains. Shaping the signal power evolution in frequency and distance is a beneficial way to approach some of the long-term goals in optical communication systems such as signal-to-noise (SNR) maximization and nonlinearity mitigation [4,5]. As an example, a flat two-dimensional (2D) profile in frequency and distance, resembling a lossless link, minimizes the accumulated amplified spontaneous emission (ASE) noise at the end of the fiber [4,6,7]. This flat 2D profile is also a requirement for the transmission based on Nonlinear Fourier Transform (NFT) [8,9]. Another example is a 2D symmetric power profile with respect to the middle point in distance. A symmetric 2D profile can be utilized to mitigate the nonlinear impairments using optical phase conjugation (OPC) systems [5,10,11].

Power profiles in a 2D space are mostly addressed by heuristic tuning of the Raman pump power and wavelength values, where the pump power values are adjusted based on experience and

 $<sup>^{</sup>I}$ Department of Electrical and Photonics Engineering, Technical University of Denmark (DTU), DK-2800 Kgs. Lyngby, Denmark

<sup>&</sup>lt;sup>2</sup>Dipartimento di Elettronica e Telecomunicazioni (DET), Politecnico di Torino, Corso Duca degli Abruzzi, 24 - 10129, Torino, Italy

<sup>\*</sup>msolt@fotonik.dtu.dk

without applying an intelligent optimization framework [4,12–14]. The heuristic optimization of the parameters in a practical setup requires simplifying the optimization problem which can be challenging when the dimensionality of the problem to solve, i.e. the number of parameters to optimize, increases. This approach will be time consuming and also less accurate in case the goal is to design several 2D target profiles with different cost functions using the same Raman amplifier setup under test. In [15,16], we presented and numerically validated an online machine learning framework to automatically optimize the Raman pump power values to design power profiles of practical interest, jointly in frequency and fiber distance domains. The proposed approach consists of a convolution neural network (CNN) [15], trained as an inverse system model, followed by a differential evolution (DE) [16] technique. Numerical results shown that the resulting framework has the flexibility to design different 2D profiles with specific objectives by optimizing the pump power values.

In [17], we presented a Raman amplifier setup and experimentally verified the performance of the CNN model and the CNN-assisted DE framework to design a data-set of achievable 2D power profiles. This amplifier setup utilizes four first order counter-propagating pumps and the target data-set is generated by applying random pump power values to the setup and measuring their resulting 2D power profile. For each target 2D profile in the data-set, the pump power values are optimized aiming to minimize the maximum absolute error (MAE) between the target and designed 2D profile. First, the CNN prediction on the target 2D profiles is investigated, which results in low MAE on average (0.37 dB), while showing high MAE(>1 dB) for roughly 2% of the profiles. To improve the CNN accuracy on 2D profiles with high MAE, the CNN-assisted DE is applied to perform online optimization on the Raman amplifier setup, resulting in less than 0.5 dB for all of the selected high-error 2D profiles.

In this paper, we extend [17] by providing more details on the experimental validation of the CNN model and the CNN-assisted DE framework for designing achievable 2D profiles. Additionally, in this work we experimentally test the DE framework in a scenario where the target is to shape the 2D signal power evolution to jointly satisfy multiple spatial-spectral objectives, rather than designing a specific achievable 2D profile shape. In particular, we consider two cost functions as the objectives and perform an online optimization of the pump power values to minimize these cost functions using the Raman amplifier setup. The two cost functions are: 1) the maximum deviation from a spectrally flat-gain profile at the end of the fiber (over the full C-band), and 2) the maximum spectral power excursion along the fiber distance. This is a multi-objective optimization problem with non-differentiable cost functions with respect to the free parameters, which is challenging to be solved with gradient-based neural network (NN) approaches presented in [18]. Our approach in this scenario is to use only the DE framework without involving the CNN. The proposed DE framework provides less than 1 dB gain deviation and spectral power excursion when enough pump power value is provided in the amplifier setup. Additionally, the simulation results also assert that the DE is able to achieve less than 0.6 dB gain deviation when the amplifier setup is not limited by the upper-bound pump power values.

The paper is organized as follows. Section 2 presents the experimental Raman amplifier setup used to validate the proposed machine learning-based power optimization framework. In Section 3, the proposed framework is discussed in more details with particular emphasis to the online application. Section 4 presents and compares the experimental results of the DE and the CNN-assisted DE frameworks. Finally, section 5 concludes the paper.

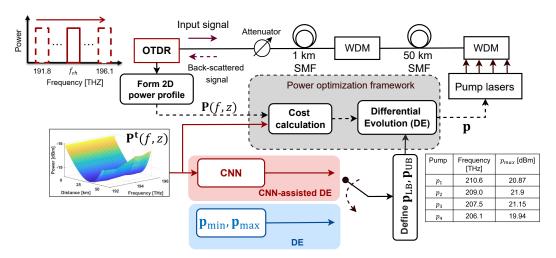
#### 2. Experimental setup

The experimental setup for verifying the proposed machine learning-based framework to optimize the Raman pump power values is depicted in Fig. 1. We consider a span of standard single-mode fiber (SSMF) with 50 km length and the Raman pump module of four counter-propagating lasers. Pump wavelengths are fixed (shown with their maximum available power value  $p_{max}$  in the table

inset in Fig. 1), and able to amplify the entire C-band. The goal is to optimize the Raman pump powers values  $\mathbf{p} = [p_1, p_2, p_3, p_4]$  to achieve the targeted 2D profile  $\mathbf{P}^{\mathbf{t}}(f, z)$ , defined in both spectral (f) and spatial (z) domains. In Raman amplification, the relation between the signal and pump power evolution over the fiber distance is described by a well-known set of non-linear ordinary differential equations [1]:

$$\begin{split} \frac{dP_{s,i}}{dz} &= -\alpha_s P_{s,i} + C_R(f_{s,i}, f_{p,j})[P_{p,j}^+ + P_{p,j}^-]P_{s,i}, \\ &\pm \frac{dP_{p,j}^\pm}{dz} = -\alpha_p P_{p,j}^\pm - (\frac{f_{p,j}}{f_{s,i}})C_R(f_{s,i}, f_{p,j})P_{s,i}P_{p,j}^\pm. \end{split} \tag{1}$$

where  $P_s$  is the signal power,  $P_{p,j}^+$  and  $P_{p,j}^-$  are respectively the co- and counter-propagating pump powers (we only have considered counter-propagating pumps in the setup),  $\alpha_s$  and  $\alpha_p$  represent the signal and the pumps attenuation coefficients measured in  $m^{-1}$ ,  $f_{s,i}$  and  $f_{p,j}$  are the signal and the pump frequencies, and  $C_R$  is the Raman gain efficiency, measured in 1/W/m. In these equations, i identifies the signal channel index for  $i = \{1, \ldots, n_{ch}\}$ , and j identifies the pump index for  $j = \{1, \ldots, n_p\}$ , with  $n_p = 4$  in the proposed setup.



**Fig. 1.** The experimental setup and the block diagram of the processes used to optimize the pump powers values for designing a 2D target power profile  $\mathbf{P}^{\mathbf{t}}(f,z)$ .

To experimentally measure the signal power evolution  $P_s$  over the spectrum and along the fiber distance, a frequency-tunable optical time-domain reflectometer (OTDR) is used. The signal bandwidth of the OTDR covers the C-band between 191.8 THz and 196.1 THz, equivalent to  $n_{ch} = 44$  channels with 100 GHz spacing. The OTDR is connected to the fiber span with three elements in between: a tunable attenuator employed to control the signal power flow into the OTDR, a 1 km SMF link to cover the dead-zone of the OTDR, and a wavelength division multiplexer (WDM), utilized to filter out the pump waves in the range between 203.9 THz and 211.1 THz, such that they do not enter the OTDR. Another WDM coupler is placed at the end of the fiber link to combine the signal and the pumps.

The OTDR introduces a low power signal (-12 dBm) into each of the channels and measures their back-scattered signal, sequentially. Overall attenuator and WDM loss is 4 dB resulting in almost -16 dBm input signal power to the 50 km fiber. To reduce the impact of noise on the measurements and have a clear trace for each channel, the signal pulse width is set to 3  $\mu s$  and the distance resolution of the OTDR to 8.2 m. The OTDR measures the signal

power evolution for all channels ( $P_{s,i}$ ), and we post-process the measured signal by applying a Savitzky-Golay smoothing filter [19] with window size w = 19 (equivalent to  $19 \times 8.2 = 155.8$  m) and polynomial order n = 2 in distance to reduce the signal fluctuations. According to the numerical results reported in [15,16], a distance resolution of 500 m is sufficient for the CNN training and evaluation. Therefore, the smoothed traces are down-sampled in distance direction using a linear interpolation to achieve 500 m resolution, and a 2D power profile  $\mathbf{P}(f,z)$  of size  $44 \times 100$  is formed.  $\mathbf{P}(f,z)$  is used as the input to the cost calculation block, where its MAE value with respect to the pre-defined target 2D profile  $\mathbf{P}^{\mathbf{t}}(f,z)$  is calculated. After the cost calculation, the power optimization framework updates the pump powers accordingly and applies a new set of pump powers to the setup, aiming to reduce the MAE in the following iteration (see Section 3 for the framework description). The process of applying pump powers, recording the resulting 2D profile, and the cost calculation continues until a convergence criteria such as a minimum cost value without considerable variation in pump power values or a maximum number of DE iterations is achieved.

#### 3. Raman pump power optimization framework

The proposed pump power optimization framework, shown in Fig. 1, consists of an evolutionary optimization algorithm, known as differential evolution (DE) [20]. The main goal of the DE is to optimize the pump power values to achieve the target 2D power evolution profile  $\mathbf{P}^{\mathbf{t}}(f,z)$ in the span. This framework is evaluated numerically in [16] using the synthetic data to find the optimum pump powers values for 2D profiles of practical interest. The DE can be used to perform optimization in an online closed-loop process by applying pump power values to the setup, evaluating their resulting cost, and updating them aiming to reduce the cost in the next iteration. If the DE optimization starts with a randomly selected population of individuals (as the initial candidate solutions), it will be more time consuming and also prone to local minimum in case the individuals in the initial population are not in the vicinity of the solution. Additionally, if the number of parameters to be optimized is high, the volume of the space to explore increases, and consequently, the DE can converge to different local minimum points each time it starts to run. For a target 2D profile  $P^{t}(f,z)$ , it is shown in [16] that a CNN-based inverse model initialization improves the DE performance in terms of its finally achieved cost value, the speed of the convergence and also the certainty in converging to the same optimum point every time the DE starts to run. The CNN model, which consists of four CNN layers followed by two fully-connected hidden layers, is trained to learn the mapping between the 2D profiles and their corresponding pump powers values using a data-set. The data-set is generated by applying randomly selected pump powers values to the amplifier setup and measuring their resulting 2D power evolution profile.

To experimentally validate the pump power optimization framework, two DE population initialization approaches are proposed as shown in Fig. 1. In the first approach, so-called CNN-assisted DE in Fig. 1, the target 2D profile  $\mathbf{P}^{\mathbf{t}}(f,z)$  is used as the input to CNN model, where a set of pump powers values  $\mathbf{p}'$  are predicted as the initial solution. These values are then used to define the pump power lower-bound and upper-bound values  $\mathbf{p}_{LB}$  and  $\mathbf{p}_{UB}$ , respectively. The  $\mathbf{p}_{LB}$  and  $\mathbf{p}_{UB}$  are specified according to the deviation of the first-order pump values in [16] by considering  $\mathbf{p}_{LB} = \mathbf{p}' - 0.5 \cdot \mathbf{p}'$  and  $\mathbf{p}_{UB} = \mathbf{p}' + 0.5 \cdot \mathbf{p}'$ . In the second experimental approach, we have proposed the DE with random initialization, so-called DE in Fig. 1. In this approach, the CNN is not involved and each element of  $\mathbf{p}_{LB}$  and  $\mathbf{p}_{UB}$  are defined without any prior knowledge and basically are the minimum  $p_{min} = -5$  dBm and maximum  $p_{max}$  pump powers values (provided in the table inset in Fig. 1), respectively. To provide intuition on how the CNN improves the DE initialization, the performance of the DE and the CNN-assisted DE is compared in terms of their MAE in designing a data-set of achievable target 2D profiles in the proposed amplifier setup.

#### 4. Experimental results

#### 4.1. Designing achievable 2D profiles

In this section, we investigate and compare the performance of the CNN-assisted DE and the DE on predicting the pump power values for a test data-set of achievable target 2D profiles. This data-set consists of 500 set of pump powers and their resulting measured 2D profiles. For each test 2D profile the goal is to predict the pump power values aiming to minimize the error between the true and the predicted pump power values, or the MAE between the target 2D profile and the resulting 2D profile in the span. Both CNN-based and random initialization approaches are used and compared in terms of convergence speed and resulting MAE. We start with the validation of the CNN-assisted DE framework, which its first step is to train and evaluate the CNN model. Regarding this, 4400 2D profiles are generated in total, divided into two sets for train and validation with the size of 4100 and 300 2D profiles, respectively.

Once the CNN is trained, the test 2D profiles are used as the input to the model and the  $R^2$  score is calculated to evaluate the correlation between the true and the predicted pump power values. The  $R^2$  score takes the values between 0 and 1 where the highest value indicates a perfect prediction. The  $R^2$  score attained for each pump is reported in Table 1. According to this results, in general, the CNN has good performance on predicting all four pump power values with more accurate prediction for  $p_3$  and  $p_4$ , compared to the  $p_1$  and  $p_2$ . The lower accuracy of  $p_1$  and  $p_2$  (compared to  $p_3$  and  $p_4$ ) is mainly because of their less impact on the signal power evolution shape as the peak of their corresponding Raman gain efficiency lies slightly outside the signal bandwidth (between 191.8 THz and 196.1 THz).

Table 1. R<sup>2</sup> test scores for the CNN model prediction.

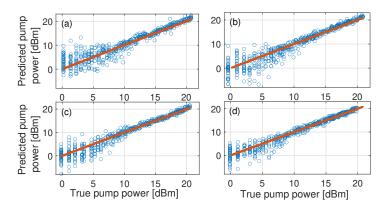
Pump	$p_1$	$p_2$	$p_3$	$p_4$
$R^2$	0.86	0.87	0.91	0.93

Additionally, a scatter plot of the true and the predicted pump power values is shown in Fig. 2(a)-(d) for all four pump values  $p_1$ ,  $p_2$ ,  $p_3$ ,  $p_4$ , respectively. Based on this figure, the correlation between the true and the predicted pump power values is low for low ranges of pump power values which is because of the low impact of the low pump power values on the signal power evolution shape. As the pump power values increase, they become more influential on the signal power profile, and the prediction accuracy increases, accordingly.

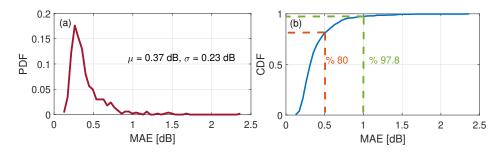
A more rigorous and meaningful approach to evaluate the CNN prediction performance is to apply the predicted pump power values to the experimental amplifier setup, measure the designed 2D profile and calculate the MAE between the targeted 2D profile and the resulting one. Fig. 3(a) and (b) show the probability density function (PDF) and the cumulative density function (CDF) of the MAE for all test profiles, respectively. For the test 2D profiles, the CNN achieves the MAE with mean  $\mu = 0.37$  dB, and standard deviation  $\sigma = 0.23$  dB. According to the CDF results, 80% of the test 2D profiles have MAE lower than 0.5 dB, and 97.8% of them result in MAE values lower than 1 dB.

According to Fig. 3, the CNN obtains statistically low MAE values, while only for eleven 2D profiles ( $\approx 2.2\%$  of all 500 test 2D profiles), it results in a MAE higher than 1 dB. Selecting this 2D profiles with the error higher than 1 dB, we apply the CNN-assisted DE approach to improve the prediction results in real-time on the experimental setup with a limit of maximum 100 iterations.

To provide an intuition regarding the CNN impact on the DE initialization, another set of experiments for the proposed eleven 2D profiles is performed using DE. For each one of these selected 2D profiles, indexed from 1 to 11, the MAE is shown in Fig. 4(a) for the CNN, the

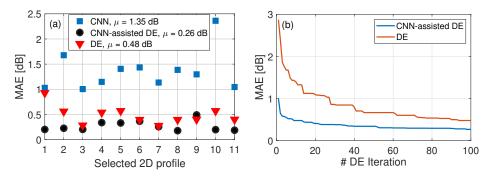


**Fig. 2.** The scatter plot of the true versus predicted pump power values using the CNN model on test data. Each blue dot corresponds to a test 2D profile and the orange solid line represents the ideal prediction. (a)  $p_1$ , (b)  $p_2$ , (c)  $p_3$ , (d)  $p_4$ .



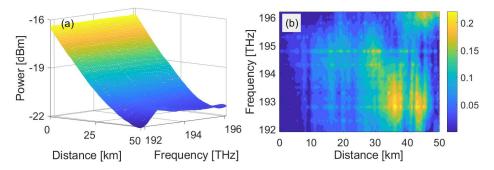
**Fig. 3.** The CNN model performance on test profiles. (a) PDF of the MAE, (b) CDF of the MAE.

CNN-assisted DE and the DE scenarios. The resulting error using CNN-assisted DE for all eleven 2D profiles is less than 0.5 dB. Figure 4(a) also asserts that the CNN-assisted DE results are considerably better than the CNN and the DE results. In addition, the average MAE evolution for all eleven 2D profiles over the number of DE iterations is shown in Fig. 4(b) for the CNN-assisted DE and DE scenarios. This plot shows that the DE initialized with the CNN converges faster and to a point with lower MAE.



**Fig. 4.** (a) The MAE for the CNN model, the CNN-assisted DE and the DE approaches for the eleven selected 2D profiles with high MAE. (b) The average value of the MAE over the selected 2D profiles for each DE iteration using the CNN-assisted DE and the DE scenarios.

Moreover, a visual representation of the CNN-assisted DE framework result (10th selected 2D profile in Fig. 4) is shown in Fig. 5, providing the target 2D profile Fig. 5(a) and the resulting heatmap of its absolute error with the predicted 2D profile over the frequency and fiber distance Fig. 5(b). For this case, the resulting MAE value between the target and the predicted 2D profile is 0.22 dB.



**Fig. 5.** CNN-assisted DE result for the 10th selected 2D profile in Fig. 4(a). (a) Target 2D profile, (b) Heatmap of the absolute error (in dB) between the target and the predicted 2D profiles over the frequency and distance domains.

#### 4.2. Designing objective-based 2D profiles

In this section we approach a different design scenario where the target is not to minimize the MAE between a target 2D profile and the designed 2D profile, but to achieve a 2D profile which fulfills multiple desired spectral-spatial objectives. In the following scenario, the specific objective is designing 2D profiles with a desired flat gain level at the end of the span, meanwhile, minimizing the spectral excursion in the entire span. This is a multi-objective optimization problem which is quite complex to solve, and we experimentally prove that it can be approached with the DE, applied real-time to the amplifier setup. It is worth noting that the CNN-assisted in Fig. 1 is not applicable since there is no 2D target profile  $\mathbf{P}^{\mathbf{t}}(f,z)$  to be used as the input to the CNN model. Only the DE can be used effectively for this design scenario, therefore, we define two cost functions for this purpose. The first objective is to have a spectrally flat 2D power evolution in distance. For this objective, the first cost function  $J_0(\mathbf{p})$ , referred to as the maximum spectral power excursion, which is aimed to be minimized, is formulated as the following:

$$J_0(\mathbf{p}) = \max_{z} [\max_{f} (\mathbf{P}(f, z|\mathbf{p})) - \min_{f} (\mathbf{P}(f, z|\mathbf{p}))].$$
 (2)

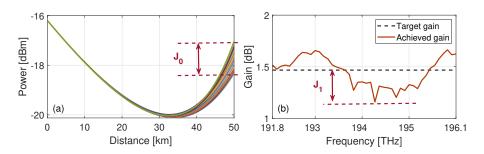
Minimizing  $J_0(\mathbf{p})$  results in achieving a 2D profile which has the minimum spectral excursion over the entire span. To provide a visual intuition on  $J_0$  value, Fig. 6(a) shows a sample power evolution profile for all channels over the distance, and the maximum spectral excursion as  $J_0$  is specified, which for this specific case, occurs at the end of the span.

The second objective is to achieve a spectral flat target gain level such as  $\mathbf{g}^t(f)$  at the end of the span. Approaching this objective, the cost function  $J_1(\mathbf{p})$  is defined as the maximum absolute deviation between the achieved gain  $\hat{\mathbf{g}}(f, \mathbf{p})$  and the target gain level  $\mathbf{g}^t(f)$  at the end of the fiber, formulated as:

$$J_1(\mathbf{p}) = \max_{f} |\hat{\mathbf{g}}(f, \mathbf{p}) - \mathbf{g}^t(f)|. \tag{3}$$

where L is the span length, and the on-off gain  $\hat{\mathbf{g}}(f, \mathbf{p})$  is defined as:

$$\hat{\mathbf{g}}(f, \mathbf{p}) = \mathbf{P}(f, z = L|\mathbf{p}) - \mathbf{P}(f, z = L|\mathbf{p}_{off}). \tag{4}$$



**Fig. 6.** (a) Spatial representation of  $J_0$ , (b) Spectral representation of  $J_1$ .

where  $\mathbf{P}(f, z|\mathbf{p}_{off})$  is the 2D power profile when all pumps are turned off. In Fig. 6(b), a target gain level is targeted and the  $J_1$  value is specified according to a sample 2D profile's achieved gain at the end of the fiber.

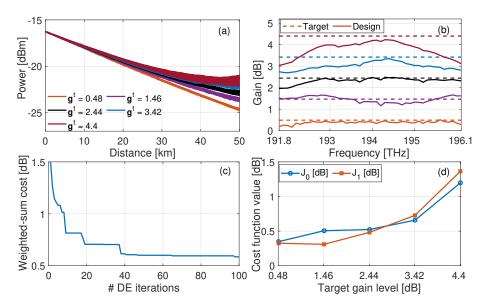
Considering the above-mentioned objectives, we define the multi-objective optimization problem aiming to minimize both  $J_0(\mathbf{p})$  and  $J_1(\mathbf{p})$ , simultaneously, and find the optimal set of pump power values  $\mathbf{p}^*$ . To make the optimization process simpler and also to be able to control the impact of each objective on the final result, we make an approximation by converting the multi-objective optimization into a classical weighted-sum as proposed in [16]. Approaching this, each objective is multiplied by a weight, defined as a hyper-parameter, and it is added to the other objectives as the following:

$$\begin{aligned} \mathbf{p}^* &= \arg\min[m_0 J_0(\mathbf{p}) + m_1 J_1(\mathbf{p})], \\ \mathbf{p} & \\ \text{such that } \mathbf{p}_{LB} \leq \mathbf{p}_{pump} \leq \mathbf{p}_{UB}, \ m_0, m_1 > 0, \ m_0 + m_1 = 1. \end{aligned} \tag{5}$$

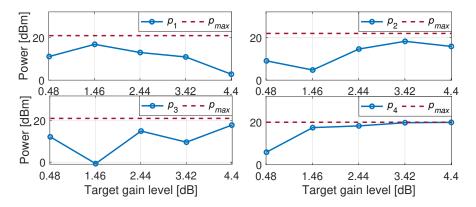
where  $m_0$  and  $m_1$  are the weights used to control the impact of  $J_0$  and  $J_1$  on the optimal point. In our analyses, we set  $m_0 = m_1 = 1/2$ , giving  $J_0$  and  $J_1$  the same impact. Five 2D profiles with different flat gain levels are designed by solving the Eq. (5). The maximum possible gain level provided by the pumps at the end of the fiber, when all of the pumps are operating at their maximum available power, is equal to  $g_{max} = 4.9$  dB. Considering this, we target five equally-spaced gain levels starting with 0.48 dB and ending with 4.4 dB. In Fig. 7(a), the resulting five power evolution profiles with different flat target gains  $\mathbf{g}^t$  are shown over the distance, with their corresponding spectral gain versus the target gain level, depicted in Fig. 7(b). Additionally, the average of the cost value for all five profiles at each DE iteration is calculated and shown in Fig. 7(c), demonstrating that the average cost does not significantly improve after 40 iterations.

Moreover, the cost values of  $J_0$  and  $J_1$  over the different target gain levels are illustrated in Fig. 7(d), showing less than 1 dB error for target gain levels up to 4 dB. Both  $J_0$  and  $J_1$  increase noticeably when the target gain level reaches higher than 4 dB. This phenomenon is mainly because of the limited pump power provided by the pumps in the setup depicted in Fig. 1, rather than the failure of the proposed power optimization framework. As the target gain level increases, the experimental amplifier setup physically limits the performance of the DE framework in achieving low cost 2D profiles by providing low upper-bound pump power  $\mathbf{p}_{UB}$  values. Regarding this, we have shown the resulting power values of all four pumps for different target gain levels by applying the DE framework in Fig. 8. In particular, it is shown that the power value of pump  $p_4$ , with increasing the target gain level, has an increasing trend towards its maximum value 19.94 dBm. In case the pumps, especially  $p_4$ , provide enough power value and they do not limit the optimization process, the DE would be able to design target gain levels more accurately.

To confirm this statement, we have performed a set of simulations to analyze the amplifier setup in Fig. 1. In the simulations, the set of equations in Eq. (1) is solved numerically using



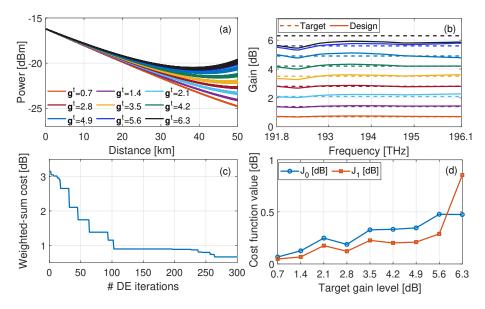
**Fig. 7.** DE results of pump power optimization by solving Eq. (5) with different target gain levels. (a) Spatial representation of the resulting power evolution profiles over the distance. (b) Spectral representation of target and designed gain levels at span end. (c) The average cost value over the five 2D profiles for each DE iteration. (d)  $J_0$  and  $J_1$  values achieved for different target gain levels.



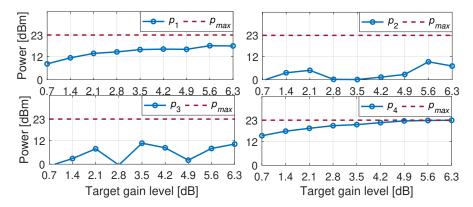
**Fig. 8.** Resulting pump power values in the experimental analyses for different target gain levels.

GNPy library [21] with the same setup configuration as proposed by Fig. 1, except that each pump in the simulations provides a higher power value, up to 23 dBm. In addition, since the range of space to explore with the new pump power ranges has higher volume compared to the experimental analyses, we set the number of the DE iterations to 300 (higher than 100 iterations in the experimental analyses).

In the simulation analyses, we use the same weight values ( $m_0 = m_1 = 1/2$ ). Nine 2D profiles with equally-spaced targeted gain levels starting from 0.7 dB and ending with 6.3 dB (slightly higher than 60% merit of Raman pumping as proposed in [22]) are generated by applying the DE to solve Eq. (5) In Fig. 9(a) the power evolution of the designed 2D profiles with their corresponding flat target gains  $\mathbf{g}^t$  are shown. The corresponding target gain level and the designed spectral gain levels of each 2D profile is demonstrated in Fig. 9(b). Moreover, the average cost over the nine 2D profiles for each DE iteration is calculated and shown in Fig. 9(c), which asserts that no considerable accuracy improvement after 260 iterations is obtained. Additionally, Fig. 9(d) shows that the resulting cost values are less than 0.6 dB for target gains levels less than 5.6 dB. For all cases with different target gain levels, the obtained pump power values are shown in Fig. 10. It is illustrated that for the case with the highest target gain level (6.3 dB), the power value of the pump  $p_4$  reaches its upper-bound 23 dB value and does not allow the DE to improve further. This results confirm that in case the amplifier setup is provided with pumps with higher upper-bound power values, high target gains can be achieved accurately using the DE framework.



**Fig. 9.** Simulation results of pump power optimization by solving Eq. (5) with different target gain levels. (a) Spatial representation of the resulting power evolution profiles over the distance. (b) Spectral representation of target and designed gain levels at span end. (c) Average cost value over the five 2D profiles for each DE iteration. (d)  $J_0$  and  $J_1$  values achieved for different target gain levels.



**Fig. 10.** Resulting pump power values in the simulation analyses for different target gain levels.

## 5. Conclusion

The DE and the CNN-assisted DE frameworks are experimentally validated for designing 2D power evolution profiles using Raman amplifiers. For test 2D profiles, the CNN model achieves less than 0.4 dB MAE on average while it is inaccurate for 2.2% of the 2D profiles in the test data-set. Addressing these profiles, CNN-assisted DE is applied to fine-tune the pump powers values, showing more than 1 dB improvement in average over the CNN results. In a second designing scenario, the DE framework is employed to design 2D profiles with two different objectives: 1) flat gain levels and, 2) minimum spectral power deviation. The results assert that the proposed frameworks can be effectively used to design 2D profiles, by online tuning of the pump power values in an amplifier setup under test.

**Funding.** European Research Council (ERC-CoG FRECOM grant no. 771878); Villum Fonden (OPTIC-AI grant no. 29334); Ministero dell'Università e della Ricerca (PRIN 2017, project FIRST).

**Disclosures.** The authors declare no conflicts of interest.

**Data availability.** Data underlying the results presented in this paper are not publicly available at this time but may be obtained from the authors upon reasonable request.

#### References

- 1. C. Headley and G. P. Agrawal, Raman Amplification in Fiber Optical Communication Systems (Academic, 2005).
- W. S. Pelouch, "Raman amplification: An enabling technology for long-haul coherent transmission systems," J. Lightwave Technol. 34(1), 6–19 (2016).
- 3. U. C. de Moura, M. A. Iqbal, M. Kamalian, L. Krzczanowicz, F. Da Ros, A. M. R. Brusin, A. Carena, W. Forysiak, S. Turitsyn, and D. Zibar, "Multi-band programmable gain Raman amplifier," J. Lightwave Technol. **39**(2), 429–438 (2021).
- J. D. Ania-Castañón, V. Karalekas, P. Harper, and S. K. Turitsyn, "Simultaneous spatial and spectral transparency in ultralong fiber lasers," Phys. Rev. Lett. 101(12), 123903 (2008).
- M. Tan, M. A. Ai-Khateeb, M. A. Iqbal, and A. D. Ellis, "Distributed Raman amplification for combating optical nonlinearities in fibre transmission," in 2018 Conference on Lasers and Electro-Optics Pacific Rim (CLEO-PR), (IEEE, 2018), pp. 1–2.
- J. D. Ania-Castanon, "Quasi-lossless transmission using second-order Raman amplification and fibre Bragg gratings," Opt. Express 12(19), 4372–4377 (2004).
- 7. J. Bouteiller, K. Brar, and C. Headley, "Quasi-constant signal power transmission," 2002 28TH European Conference on Optical Communication 3, 1–2 (2002).
- L. F. Mollenauer and K. Smith, "Demonstration of soliton transmission over more than 4000 km in fiber with loss periodically compensated by Raman gain," Opt. Lett. 13(8), 675–677 (1988).
- S. T. Le, J. E. Prilepsky, P. Rosa, J. D. Ania-Castañón, and S. K. Turitsyn, "Nonlinear inverse synthesis for optical links with distributed Raman amplification," J. Lightwave Technol. 34(8), 1778–1786 (2016).
- 10. I. Phillips, M. Tan, M. Stephens, M. E. McCarthy, E. Giacoumidis, S. Sygletos, P. Rosa, S. Fabbri, S. T. Le, T. Kanesan, S. K. Turitsyn, N. J. Doran, P. Harper, and A. D. Ellis, "Exceeding the nonlinear-Shannon limit using

- Raman laser based amplification and optical phase conjugation," in *Optical Fiber Communication Conference*, (Optical Society of America, 2014), p. M3C.1.
- 11. M. Tan, P. Rosa, T. T. Nguyen, M. A. Z. Al-Khateeb, M. A. Iqbal, T. Xu, F. Wen, J. D. Ania-Castañón, and A. D. Ellis, "Distributed Raman amplification for fiber nonlinearity compensation in a mid-link optical phase conjugation system," Sensors 22(3), 758 (2022).
- T. Ellingham, J. Ania-Castanon, R. Ibbotson, X. Chen, L. Zhang, and S. Turitsyn, "Quasi-lossless optical links for broad-band transmission and data processing," IEEE Photonics Technol. Lett. 18(1), 268–270 (2006).
- P. Rosa, G. Rizzelli, M. Tan, P. Harper, and J. D. Ania-Castañón, "Characterisation of random DFB Raman laser amplifier for WDM transmission," Opt. Express 23(22), 28634–28639 (2015).
- A. E. Bednyakova, M. Fedoruk, P. Harper, and S. Turitsyn, "Hybrid gain-flattened and reduced power excursion scheme for distributed Raman amplification," Opt. Express 21(24), 29140–29144 (2013).
- M. Soltani, F. D. Ros, A. Carena, and D. Zibar, "Inverse design of a Raman amplifier in frequency and distance domains using convolutional neural networks," Opt. Lett. 46(11), 2650–2653 (2021).
- M. Soltani, F. Da Ros, A. Carena, and D. Zibar, "Spectral and spatial power evolution design with machine learning-enabled Raman amplification," J. Lightwave Technol. 40(12), 3546–3556 (2022).
- M. Soltani, F. D. Ros, A. Carena, and D. Zibar, "Experimental validation of spectral-spatial power evolution design using Raman amplifiers," accepted for ECOC (2022).
- 18. U. C. de Moura, F. D. Ros, A. M. R. Brusin, A. Carena, and D. Zibar, "Experimental characterization of Raman amplifier optimization through inverse system design," J. Lightwave Technol. 39(4), 1162–1170 (2021).
- A. Savitzky and M. J. E. Golay, "Smoothing and differentiation of data by simplified least squares procedures," Anal. Chem. 36(8), 1627–1639 (1964).
- 20. T. Eltaeib and A. Mahmood, "Differential evolution: A survey and analysis," Appl. Sci. 8(10), 1945 (2018).
- A. Ferrari, M. Filer, K. Balasubramanian, Y. Yin, E. Le Rouzic, J. Kundrat, G. Grammel, G. Galimberti, and V. Curri, "GNPy: an open source application for physical layer aware open optical networks," J. Opt. Commun. Netw. 12(6), C31–C40 (2020).
- V. Curri and A. Carena, "Merit of Raman pumping in uniform and uncompensated links supporting NyWDM transmission," J. Lightwave Technol. 34(2), 554–565 (2016).