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Experimental research on the effect of graphite on heat transfer performance of a latent heat storage system

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Phase change materials (PCMs) provide a good resolution for the latent heat storage system which can be used in many application fields such as solar energy utilization and waste heat recovery. This study aims to experimentally investigate the impact of graphite powder on the thermal characteristics and heat transfer performance of paraffin with ceresin (PC) as a PCM, using water as the heat transfer fluid. Experimental tests were conducted to analyze the heat transfer performance of PC and the influence of graphite powder on its thermal characteristics. Different masses of graphite powder were employed to assess their effects on the heating rate and the time required for PC to reach its melting temperature. The experimental results revealed that the addition of graphite powder improved the heating rate of both PC and water, attributed to its high thermal conductivity. Furthermore, the time for PC to reach the melting temperature was decreased with varying amounts of graphite powder, achieving a maximum reduction of 17.2% with the addition of 40 g of graphite powder. However, the effectiveness of graphite powder in enhancing heat transfer efficiency was found to be limited, with the optimal promotion effect observed at around 40 g of graphite powder for 500 g of PC. The findings of this investigation provide valuable insights for the design of phase change energy storage systems, with potential applications including heat pump drying units, greenhouse energy storage in modern agriculture, and solar energy storage utilization technology. The theoretical basis established can contribute to the development and optimization of PCM-based systems in diverse practical scenarios.

KEYWORDS

heat storage technology, phase change materials, paraffin, graphite powder, heat transfer efficiency

1 Introduction

Thermal energy is one of the most important forms of energy in the existing energy structure (Curry et al., 2023). Thermal storage technology can address the contradiction between the timing and intensity of thermal energy supply and demand, effectively reducing energy waste caused by the time difference in energy supply and demand. Therefore, thermal storage technology has broad application prospects in many fields such as heating and air conditioning energy saving, solar energy utilization, and waste heat recovery in industrial and civil buildings.

There are many ways to store thermal energy, including chemical energy storage (Jayaprabakar et al., 2023), sensible energy storage (Paul et al., 2022) and latent energy storage (Lu et al., 2023). Among them, the latent heat storage has a high density and an

isothermal heat storage and release process, which is easy to control and operate, making it the main heat storage method (Waseem Aftab et al., 2021). Latent energy storage based on phase change materials (PCMs), such as paraffins, salt hydrates and metallics, has been widely studied in the application of solar engineering, heat pump, spacecraft thermal control, industrial waste heat storage, and so on (Zhang et al., 2021; Matos and Pala, 2023). Paraffin is a by-product of refined petroleum separated from the wax fraction of crude oil. Industrial grade paraffin is often used as a phase change heat storage material, which has the advantages of high latent heat, low melting vapor pressure, good chemical stability, self-nucleation, no phase separation and corrosion (Lu et al., 2021a). However, pure paraffin suffers from problems such as low thermal conductivity, limiting its utilization (Rahmalina and Abdu RahmanIsmail, 2022). In order to improve the thermal conductivity of paraffin, researchers mainly focus on the improvement of heat storage equipment, such as using fins (Sheikholeslami and Jafaryar, 2023), honeycombs (Sheikholeslami, 2022), porous media (Mohammadreza Naghdi Bazneshin et al., 2023), or adding metal powder (Gao et al., 2023), metal mesh (Homlakorn et al., 2023), graphite (Liu et al., 2023), and so on.

Compared with other methods, adding thermal conductive materials, such as graphite, is a relatively simple, economical, and feasible method to improve the thermal conductivity of paraffin. Graphite has good thermal conductivity and can quickly conduct heat. Therefore, when graphite powder is added to paraffin, it can accelerate the melting rate of paraffin and improve thermal uniformity, avoiding local overheating or solidification (Dhandayuthabani et al., 2020). For the investigation of graphite, mass ratio is an important focus. It is found that when it comes to the case of 95 mass% of composite PCM, a reduction of 13.3% in the melting time is obtained (Zheng et al., 2018). In the study of Zeng et al. (Zheng et al., 2018), when 3.0 mass% graphite was added, the super cooling degree could be alleviated to 62.6°C with the latent heat of 185.7 J/g. The production method of paraffin and graphite composition is another research content. In the study of Yang et al. (2022), paraffin wax and graphite powder were compressed into a shape-stabilized phase material. By testing the pressure and density of the mixture, they found that the maximum density of the mixture was 1.07 g/cm³. In the investigation of Dong et al. (2022), a novel strategy was developed by constructing graphite sheets with high orientation inside the phase change composites following compression induction. Highly efficient heat transfer could be obtained through the channels provide by the highly oriented graphite sheets. In the study of Yang et al. (2023), a 3D porous graphite foam was prepared by a pressing and drying method, which was used as the thermal conductive skelton and shape stabilizer of phase change materials. They found that the mixture had an ultrahigh thermal conductivity of 19.27 W/(m·K), which was about 76 times higher than that of pure paraffin.

To further improve heat exchange efficiency, combinations of graphite and other additives attract much attention. In an air conditioning system, tetradecane combined with graphite achieved a 30% reduction in CO₂ emission and compressor size (Aljehani et al., 2018). In the study of Liu et al. (2022), expanded graphite (EG)/paraffin (PA)/silica (SiO₂) composite materials were fabricated, with a thermal conductivity of 2.053 W/(m·K), which was 8.5 times higher than that of pure paraffin wax. In the energy storage system, combination of wood and graphite is utilized to improve the stabilization, with a conductivity of 65 W/(m·K) (Huang et al., 2017). In the investigation of Wang et al.

(2020), microstructure of graphite was approved to greatly enhance the thermal conductivity of paraffin phase change materials, mainly due to the synergetic effects induced by the intrinsic high thermal conductivity of graphite and the high anisotropy degree of graphite sheets in the paraffin matrix. However, graphite powder can agglomerate in molten paraffin wax and settle. To solve this problem, Gorbacheva et al. (2021) utilized hydrophobic nano-sized silicon dioxide as a stabilizer. They found that at the concentration of 3 vol. %, silica nanoparticles formed a percolation structure, which was capable to prevent the sedimentation of graphite particles introduced into the mixture. Through environmental scanning electron microscope (ESEM) technology, graphite particle was found to disperse homogeneously in composite PCMs (Lu et al., 2021b). After repeated melting and solidification cycles during the stability tests, the properties of paraffin-graphite phase change materials were demonstrated to remain unchanged (Chakraborty et al., 2022). Moreover, better stability and dynamic characteristics were also found in the composite PCM amended expansive soil under combined effect of alternating load and wet and dry cycles (Liu et al., 2023).

Graphite powder has a promoting effect on the phase change heat transfer process of paraffin, but the relationship between the amount of graphite powder added and the heat transfer enhancement is still unclear. As a result, in this investigation, we chose the paraffin with ceresin (PC) as the research object and experimentally studied the influence of different mass of graphite powder on the heat transfer performance of pure PC. Heat load was supplied by an electric heater. PC absorbs heat and melts, then transfers the heat to the circulating water. Temperature variation of PC material and water are compared with different mass of graphite powder.

2 Experimental setup and experimental procedures

2.1 Experimental set-up

The schematic of the test system is shown in Figure 1. The experimental apparatus includes heating system, water circulation system, data acquisition system and the thermal storage system. In the heating system, the heat load is provided by a thin film heater with the size of 100 mm \times 30 mm \times 6 mm. During the experiment, the heater is attached directly on the bottom of the organic glass box, and adjusted by altering the DC power output voltage imposed on it. The water circulation system consists of a pump, water pipe, and a flowmeter. The outer diameter of the pipe is 19 mm. The outer surface of the water pipe is covered with a foam insulation layer, with the thickness of 15 mm. The flow rate of water is 100.0 mL/min. In the data acquisition system, the temperature of fluid is measured using T-type thermocouples with the accuracy of ±0.5°C. Agilent Keysight DAQ970A is utilized to monitor and record the temperature at a time interval of every 2 minutes. In the thermal storage system, an organic glass box is utilized, with the size of $200 \text{ mm} \times 100 \text{ mm} \times 100 \text{ mm}$. The outside of the glass box is covered by a layer of foam insulation, with the thickness of 30 mm. The interior of the box is filled with phase change material, and for this study, paraffin with ceresin (PC) is chosen as the research object. PC type is No. 48 semi-refined paraffin wax with the melting point of 48°C-50°C. For the graphite powder, the particle size is 74 µm and





the purity is 99%. There are five temperature measurement points in this experiment. T1 is temperature of the water tank outlet. T2 and T3 are temperature of the water inlet/outlet of the glass box. T4 and T5 are the temperature of the PC material inside the glass box. Detailed positions of the heater and the temperature measurement points inside the box are shown in Figure 2.

2.2 Experimental procedures

There are two sections in this investigation. In part one, the heat transfer performance of pure PC material is studied. The electric

heating film provides heat to the system, which is then transferred to the PC material inside the acrylic box through conductive heat transfer on the wall. As the PC is heated, its temperature increases until reaching the melting point and gradually melts from solid to liquid. The high-temperature PC then transfers heat to the water through the pipe wall, achieving the purpose of heating the water. By measuring the temperature changes of water, the heat transfer efficiency of the system can be calculated.

Then in part two, graphite powder with different masses is added into the pure PC material, in order to compare the influence of graphite powder on the heat transfer efficiency. Before the start of the experiment, weigh different masses of graphite powder using an electronic scale, place it into fully melted PC material and stir evenly. Then start the experiment after the mixed material is naturally cooled to the room temperature. All the experimental steps are the same as in part one. Five cases are performed using the graphite powder of 10 g, 20 g, 30 g, 40 g and 50 g respectively.

2.3 Data reduction and uncertainty analysis

The heat transfer efficiency can be obtained by:

$$\eta = \frac{Q_{PC}}{Q} \tag{1}$$

Where Q_{PC} is the heat transferred to PC material and Q is the heat load supplied by the electric heater.

The heat transferred to PC material can be calculated as:

$$Q_{\rm PC} = c_{\rm PC} m_{\rm PC} \Delta T_{\rm PC} + m_{\rm PC} h_{\rm PC} \tag{2}$$

Where $c_{\rm PC}$ is specific heat capacity, which is taken as 2.0 J/(g.°C) in this experiment; $m_{\rm PC}$ is the quality of PC material, g; $\Delta T_{\rm PC}$ is the temperature difference during the heating process, °C. In this study, $\Delta T_{\rm PC}$ is taken as $\frac{1}{2} [(T4_{max} - T4_{min}) + (T5_{max} - T5_{min})]$. $h_{\rm PC}$ is the latent heat of PC material, which is taken as 200 J/g in this experiment.

According to the standard of evaluation and expression of uncertainty in measurement (JJF 1059-2012), the uncertainty of temperature u(T) can be described as in Eq. 3:

$$u(T) = a / k \tag{3}$$

Where *a* is the accuracy of the T-type thermocouples. *k* is the coverage factor, depending on the assumed probability distribution of the measured data. In this study, *k* is $\sqrt{6}$ based on the assumption of triangular distribution of the measured temperature.

Standard uncertainty of Q_{PC} can be calculated as in Eq. 4:

$$\frac{\Delta Q_{PC}}{Q_{PC}} = \sqrt{\left(\frac{1}{2} \frac{u(T4)}{T4}\right)^2 \times 2 + \left(\frac{1}{2} \frac{u(T5)}{T5}\right)^2 \times 2} = 0.58\%$$
(4)

Heat load supplied to the whole system can be calculated by multiplying the current I and the voltage U, as shown in Eq. 5.

$$Q = IU \tag{5}$$

Standard uncertainty of the heat load can be calculated as in Eq. 6:

$$\frac{\Delta Q}{Q} = \sqrt{\left(\frac{\delta U'}{U}\right) + \left(\frac{\delta I'}{I}\right)} = \sqrt{\left(\frac{0.5\% \times 250}{220}\right)^2 + \left(\frac{0.5\% \times 3.0}{0.91}\right)^2} = 1.74\%$$
(6)

Where the accuracy grade of the ammeter and the voltmeter is $\delta = 0.5\%$. When the heat load is set to be 200W, the corresponding voltage and current values are U = 220V and I = 0.91A respectively. The ranges of the voltmeter and ammeter are U' = 250 V and I' = 3.0A respectively.

So, the uncertainty of heat transfer efficiency can be obtained as in Eq. 7:

$$\frac{\Delta\eta}{\eta} = \sqrt{\left(\frac{\Delta Q_{PC}}{Q_{PC}}\right)^2 + \left(\frac{\Delta Q}{Q}\right)^2} = 1.83\%$$
(7)







3 Results and analysis

3.1 Pure PC material

Figure 3 shows the temperature variation of the pure PC material. At the beginning of the experiment, 10 min prior, the system temperature is relatively low, and the PC is in a solid state. From the 8th minute onwards, the temperature starts to rise rapidly. Due to the closer proximity of temperature measurement point T4 to the heating film, the heating rate and amplitude of T4 are higher than that of T5. The time it takes for T4 and T5 to reach the melting point is 12.6 min and 18.0 min, respectively. Then heat is stored in the form of latent heat. The PC material has a relatively low thermal conductivity, so before the phase transition occurs, heat is primarily transferred through conduction, while after melting, it is



mainly transferred through convection. Therefore, after the 12th minute, the growth rate of T4 and T5 is much higher than that in the conduction period of the experiment.

Figure 4 shows the temperature variation of the circulating water. Within the first 2 minutes after the start of the experiment, the temperature of the circulating water almost remains constant. As can also be seen from Figure 3, the temperature of the PC material remains almost unchanged during this initial two-minute period, indicating that the heat transferred to the water during this stage can be neglected. By the end of the experiment, the temperature of the circulating water is raised by a total of 1.1° C. From this result, it can be concluded that the heating efficiency will not be very high if only pure PC material is used.

3.2 PC with graphite powder

In this section of the experiment, different masses of graphite powder are added into the PC material to investigate the effect of graphite powder on the heat transfer performance of pure PC material. Temperature variation of PC material and the water are studied.

3.2.1 Temperature variation of PC

Figure 5, Figure 6, Figure 7, Figure 8, Figure 9 show the temperature variation of PC material with graphite powder of 10 g-50 g respectively. When a small amount of graphite powder is added (10 g and 20 g, Figure 5, Figure 6), the promotion of heat transfer process by graphite powder is not very significant, and there is not much change in the temperature inside the PC material. The time it takes for T4 and T5 to reach the melting point remains essentially unchanged.

Figure 7 shows the temperature variation of PC material with graphite powder of 30 g. When adding 30 g of graphite powder, T5 shows a significant improvement and the heating rate rapidly



Temperature variation of T4 and T5 with 20 g of graphite powder.



increases from the 10th minute, nearly 2 minutes earlier than that without graphite powder added. The time it takes for T4 and T5 to reach the melting temperature shorten from 12.6 min and 18.0 min to 12.3 min and 17.2 min, respectively, with a reduction of 2.38% and 4.44%.

Figure 8, Figure 9 show the temperature variation of PC material with graphite powder of 40 g and 50 g. When enough graphite powder is added, the heat transfer performance of both T4 and T5 are greatly improved. The temperature value increases significantly, and the time required for rapid heating to begin is reduced to 8 min, which is nearly 4 min shorter than that without graphite powder adding. For the case of adding 40 g of graphite powder, the time it takes for T4 and T5 to reach the melting point



FIGURE 8

Temperature variation of T4 and T5 with 40 g of graphite powder.



shorten from 12.6 min and 18.0 min to 11.0 min and 14.9 min, respectively, with a reduction of 12.7% and 17.2%.

Figure 10 shows the time needed to reach the melting temperature of PC material with and without graphite powder added for the positions of T4 and T5 respectively. The results indicate the same trend that when the mass of graphite powder is below 30 g, the time required to reach the melting point decreases slightly; when the mass is 40 g or more, the time to reach the melting point rapidly decreases and remains relatively stable. Additionally, when the mass of graphite power is more than 40 g, the temperature results almost remain unchanged, seen in Figure 8, Figure 9. Based on the results of temperature and time, we can come to a conclusion

that for 500 g of pure PC material, the maximum amount of graphite powder required for promoting heat transfer is around 40 g.

3.2.2 Temperature variation of circulating water

In this section, we investigate the temperature variation of circulating water with different mass of graphite powder added into the pure PC material. Figure 11 shows the temperature comparison results. It can be observed that as the quality of graphite powder increases, the outlet temperature of the circulating water, T3, continuously increases from 15.7° C to 16.2° C. The temperature difference between the inlet and outlet, i.e. T2 and T3, has increased from 1.1° C to 1.6° C.

3.3 Heat transfer efficiency

In this section, the heat transfer efficiency is studied to investigate the influence of graphite powder, which can be obtained from Eqs 1, 2, 5. The total time is 20 min. The temperature difference change of paraffin is taken as the average of T4 and T5. Figure 12 shows the comparison results of η with and without graphite powder added. As the mass of graphite powder increases, the heat transfer efficiency improves slightly but remains essentially unchanged. This can also be observed from the temperature curves, where the addition of graphite powder has a minor impact on the temperature difference of the paraffin before and after the experiment, but has a significant impact on the heating rate.

All of the above results show that when the quality of phase change materials remains constant, there is a maximum limit to the amount of graphite powder that can be added to enhance heat transfer efficiency and accelerate the melting of phase change materials. The practical implications of our findings highlight the potential for thermal conductive materials, such as graphite, in heat storage systems to improve heat transfer performance, thereby providing valuable insights for designers.

4 Conclusion

In this investigation, we experimentally studied the effect of graphite powder on the heat transfer process of PC material. 500 g of PC was chosen, with 10 g–50 g graphite powder added in five experiments. Water was adopted as the circulation fluid. Temperature variation of PC and water were recorded. Heat transfer efficiency and heating rate of PC were compared with and without graphite powder added. In conclusion, this study provides valuable insights into the thermal performance of latent heat storage system, which are described as follows:

(1) Graphite powder has excellent thermal conductivity. When it is added to PC material, it can enhance the thermal conductivity of PC, thereby reducing the time it takes to reach the melting temperature and increasing the melting rate of the PC. In this experiment, for 500 g of PC, a maximum reduction of 17.2% in the time needed to reach the melting temperature is obtained with 40 g of graphite powder.



Comparison of time needed to reach the melting temperature with and without graphite powder: (A) T4; (B) T5.





- (2) The effect of graphite powder on improving heat transfer efficiency is limited. In this experiment, 500 g of PC material has the highest heating rate and amplitude when the graphite powder addition is 40 g.
- (3) Graphite powder promotes the melting rate of PC material. For the enhancement of heat transfer efficiency, the effect is not significant due to the small change of temperature difference of PC at the beginning and end of the experiment.

Findings of this experimental study could be utilized to enhance heat transfer efficiency in applications such as heat pump drying unit, greenhouse energy storage in modern agriculture, solar energy storage utilization technology, and so on. In this investigation, particle size of the graphite powder was not considered. However, it is known that when paraffin wax is completely melted into a liquid state, during the convective heat transfer process, the graphite powder particles contribute to the enhancement of heat transfer by inducing turbulent disturbances. Thus, we suggest more detailed investigations on graphite powder such as particle size and microstructure, in order to obtain a deeper understanding about the mechanism of graphite powder enhancing paraffin heat transfer.

Data availability statement

The original contributions presented in the study are included in the article/Supplementary Material, further inquiries can be directed to the corresponding author.

Author contributions

YZ: Conceptualization, Funding acquisition, Project administration, Resources, Supervision, Validation, Visualization, Writing–review and editing. GL: Data curation, Software, Writing–original draft. XZ: Formal Analysis, Methodology, Validation, Writing–original draft. HW: Investigation, Validation, Writing–review and editing.

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Conflict of interest

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