

Effects of Processing Variables on the Morphology and Microstructural Characteristics of TiO₂ Fibers Produced by Solution Blow Spinning

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A factorial design was used to evaluate the effects of processing variables on the morphology and microstructural characteristics of titanium dioxide (TiO₂) fibers produced by solution blow spinning (SBS). For this, tests were carried out varying TiO₂ precursor content, feed rate, air pressure, polymer, and solvent. The TTIP concentration and feed rate statistically influenced the average diameters of the PVC/TiO₂ system. The proper combination between polymer and solvent enables the obtaining of TiO₂ nanofibers with similar morphologies either using hydrophilic or hydrophobic polymer, however, fiber diameter is influenced by type of system (polymer/solvent) used. Only the anatase crystalline phase was found in the fibers with the PVC polymer and THF solvent, while two crystalline phases were obtained in the fibers with PVP and alcohol, anatase and rutile, indicating that the variation of the polymer and solvent influences the crystalline phases of the TiO₂ fibers studied.

Keywords: *Solution blow spinning, Titanium dioxide, Fibers, Factorial design.*

1. Introduction

The intense research aimed at the nanomaterials class makes their production techniques increasingly improved, thus improving the quality of the synthesized material. Advances in the development of materials imply improvements in processing techniques to achieve appropriate performance in their applications¹⁻⁴.

The solution blow spinning technique is a processing route to produce nanofibrous materials developed in the past decade⁵⁻⁷. It uses aerodynamic forces (pressure of a gas/air) and not electrostatic forces (electrical field difference), to produce nanofibers with high productivity and with nanometer and submicrometer diameters. It was adapted between 2012 and 2015 for the production of micrometer and submicrometer nanofibers from ceramic materials⁸⁻¹⁰. In this sense, in recent years, several studies have demonstrated the efficiency of the SBS technique in the production of nanofibers and submicrometric ceramic fibers, such as ferrites¹¹⁻¹³, SiO₂¹⁴⁻¹⁶, CeO₂¹⁷ and TiO₂¹⁸⁻²¹.

These studies also demonstrated that SBS is very influenced by processing variables, because the efficacy of the injection of the solution through the coaxial nozzle, the stretching of the polymeric solution by the high-pressure gas stream and the solvent evaporation is intimately dependent of type and amount precursor material, feed rate and air pressure. However, there is a scarcity of studies involving the influence of processing variables, such as feed rate,

gas pressure, precursor material concentration, and the characteristics of the polymer and solvent used when ceramic nanofibers are produced by SBS. Works address the influence of some of these variables in studies involving the production of polymeric nanofibers produced by SBS^{6,22}, while others have investigated such influence in electrospun ceramic nanofibers^{23,24}. The works involving SBS observed that low polymer concentrations (4 – 8% m/v) associated with high pressures (58 – 80 psi) produce smaller diameters (70 – 210 nm) fibers. Under these conditions, smooth surface morphology was also observed. However, there is a scarcity of studies on the influence of processing parameters on morphological and microstructural characteristics of ceramic fibers produced by SBS.

On the other hand, TiO₂ nanofibers have been produced by SBS for use in several applications, such as water treatment, decomposition of organic compounds and antimicrobial action¹⁷⁻²¹, and authors depicted that inadequate processing parameters values can affect or even impede the formation of the fibers. However, a systematic study on the influence of these parameters was already not presented in the literature.

Thus, in order to better understand the influence of processing parameters on the synthesis of TiO₂ nanofibers by SBS, this work aims to analyze the influence of the TiO₂ precursor content, feed rate, air pressure and polymer and solvent type on the morphology and microstructural characteristics of the fibers produced. For this, tests were carried out varying these factors, with the aid of an experimental design of type 2³.

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TiO₂ precursor content and the feed rate had statistically influence on the average diameters of the PVC/TiO₂ fibers and the proper combination between polymer and solvent enables obtaining TiO₂ nanofibers with similar morphologies either using hydrophilic or hydrophobic polymer.

2. Experimental

2.1. Materials

Titanium (IV) isopropoxide (TTIP, ≥97.0%, Sigma-Aldrich, Brazil), Polyvinyl chloride (PVC, M_w = 50,360 g/mol, Norvics SP 100) and Polyvinylpyrrolidone (PVP, M_w ≈ 1300,000 g/mol, Sigma-Aldrich, Brazil) were used as titania precursor and spinning agents, respectively. Tetrahydrofuran (THF, 99.9%, Proquimios) and ethanol (EtOH, 99.5%, Synth, Brazil) were used as solvents. Hydrochloric acid (HCl, 36.5%, Nuclear) and acetic acid (HAc, 99.9%, VWR Chemicals) were used to stabilize the solutions.

2.2. Experimental design

A Factorial design 2³ with a central point, was used to estimate the main effects and interactions of three processing parameters on the average diameter of the fibers. Two replications were performed on the study. The studied parameters were: TTIP concentration, air pressure and feed rate for the two systems used. The two systems used were PVC as polymer, THF as solvent and TTIP as precursor, PVC/TiO₂; and PVP as polymer, ethanol as solvent and TTIP as precursor, PVP/TiO₂. The codified levels and factors applied in the experimental design are shown in Table 1. In both systems, the experiments were carried out in random order. The experimental project matrix is shown in Tables 2 and 3.

The mathematical model (Equation 1) was evaluated by analysis of variance (ANOVA) and only the significant effects were used in the model²⁵. The significance level used was 5% ($\alpha = 0.05$).

Table 1. Coded and uncoded factors and levels of 2³ Experimental design of PVC/TiO₂ and PVP/TiO₂ fibers.

Factors				Codified Levels		
				-1	0	+1
PVC/TiO ₂ Fibers	X ₁	TTIP concentration	% v/v	4.0	8.0	12.0
	X ₂	Air pressure	psi	30.0	50.0	70.0
	X ₃	Feed rate	ml.h ⁻¹	4.4	7.2	10.0
PVP/TiO ₂ Fibers	X ₁	TTIP concentration	% v/v	4.0	8.0	12.0
	X ₂	Air pressure	psi	50.0	60.0	70.0
	X ₃	Feed rate	ml.h ⁻¹	4.4	7.2	10.0

Table 2. 2³ Experimental design matrix of PVC/TiO₂ fibers.

Experiments	TTIP concentration (% v/v)	Air pressure (psi)	Feed rate (ml h ⁻¹)
1	4.0	30.0	4.4
2	12.0	30.0	4.4
3	4.0	70.0	4.4
4	12.0	70.0	4.4
5	4.0	30.0	10.0
6	12.0	30.0	10.0
7	4.0	70.0	10.0
8	12.0	70.0	10.0
9	8.0	50.0	7.2
10	8.0	50.0	7.2
11	8.0	50.0	7.2

Table 3. 2³ Experimental design matrix of PVP/TiO₂ fibers.

Experiments	TTIP concentration (% v/v)	Air pressure (psi)	Feed rate (ml h ⁻¹)
1	4.0	50.0	4.4
2	12.0	50.0	4.4
3	4.0	70.0	4.4
4	12.0	70.0	4.4
5	4.0	50.0	10.0
6	12.0	50.0	10.0
7	4.0	70.0	10.0
8	12.0	70.0	10.0
9	8.0	60.0	7.2
10	8.0	60.0	7.2
11	8.0	60.0	7.2

$$y = \mu + \sum_i^k xi + \sum_{i<j}^k xixj + \varepsilon_{ij} \quad (1)$$

where y is the response variable, μ is the mean of the model, x are the independent variables, and ε is the random error component.

2.3. Preparation of precursor solutions

For the production of PVC/TiO₂ fibers, TTIP (according to the amounts defined in the experimental design, Table 1 and 2, in % v/v) was dissolved in a mixture of THF (10 mL) and HCl (200 μ L) under stirring for 1h. Then, PVC was added in the solution at a concentration of 10% (w/v). The solution was kept under constant stirring for 1h, until the polymer was completely dissolved.

For the production of PVP/TiO₂ fibers two solutions were prepared and then mixed together. For the first solution, TTIP (according to the amounts defined in the experimental design, Table 1 and 2, in % v/v) was dissolved in a mixture of ethanol (10 mL) and acetic acid (50 μ L) under stirring for 15 min, until complete dissolution. For the second solution PVP, 10% (w/v) was added in 10 ml of ethanol and stirred for 1h, until complete dissolution. Then, the second solution was added dropwise to the first and mixed under vigorous stirring for 30 min before spinning.

2.4. Fiber production

The spinning process was conducted immediately after the preparation of the precursor solutions by applying a conventional solution blow spinning (SBS) apparatus, which consists of a pressurized air source, injection pump, SBS concentric nozzle and collecting chamber. The set of coaxial nozzles used was previously described²¹. The external annular area of the nozzle was of 0.07 mm² and the inner-tube has an internal diameter of 0.7 mm. The feed rate and air pressure were determined according to the experimental design. Fibers were collected in a chamber placed at 200 mm (work distance) from the concentric nozzle. The as-spun fibers were calcined in a muffle furnace (air atmosphere, at heating rate of 5 °C/min) for 2 h at 600 °C to remove the solvent and the polymer.

2.5. Fibers characterization

Fibers morphologies were assessed on gold-sputtered samples using a scanning electron microscopy by scanning electron microscopy (SEM) (LEO, 1430) (20 kV). For each samples the diameters were measured by ImageJ (National Institute of Health, USA) of at least 100 individual fibers per sample across two different sites spun fiber.

Samples were also analyzed by transmission electron microscopy, TEM, (FEI Tecnai, G2 F20) at operation voltage of 200 kV. The crystalline structure of calcined solution blow spun titania fibers were characterized by X-ray diffraction, XRD (Shimadzu, XRD-6000) with Cu K α radiation source ($\lambda = 1.5418 \text{ \AA}$) at 40 kV, 30 mA, 0.02° per minute from 20 < 2 θ < 70°, and graphite monochromator. The crystallite size “D” was determined using Scherrer Equation (2).

$$D = \frac{K\lambda}{\beta \cos\theta} \quad (2)$$

where K is the Scherrer constant; λ is the wavelength of the X-ray radiation; FWHM is the full width at half maximum; and θ , is the diffraction angle.

3. Results and Discussion

Figure 1 shows SEM representative micrographs of the PVC/TiO₂ and PVP/TiO₂ fibers obtained at different processing conditions. The general morphology obtained is characterized by fibers with a smooth appearance, conjoined fibers, some regions with an accumulation of material forming beads and fibers with a circular cross-section. According to Santos et al¹⁹, the conjoined fibers are due to the incomplete evaporation of solvents. The beads are formed due to the instability of the solution resulting from the low viscosity of the solution or high surface tensions and/or low solvent evaporation rates^{6,26,27}. Fibers produced with ethanol and PVP showed a more uniform and smooth appearance when compared to fibers prepared with THF and PVC.

MET micrographs (Figure 2) display that in both systems the fibers are constituted by small particles, with an average diameter of approximately 30 nm (SD = 6 nm) and 51 nm (SD = 12 nm), for the PVC/TiO₂ and PVP/TiO₂ systems, respectively. According to the t-test ($p < 0.001$), there is a statistically significant difference in the mean diameters. The lower particle size of PVC/TiO₂ could be related to the pH of the solution, the basicity of the medium caused by THF do not enhanced anatase crystal growth such as in mediums with a higher acidity. However, study²¹ that produced TiO₂ fibers by SBS using PVP as spinning aid obtained fibers composed by particles with similar size, at around 55nm.

Table 4 shows the coefficient of determination (R^2) and F-test of the average fiber diameters for the experimental design studied. The coefficient of determination (R^2) quantifies the quality of the adjustment, as it provides a measure of the proportion of variation explained by the regression equation in relation to the total variation of responses, ranging from 0 to 100%^{28,29}.

Table 4. Correlation coefficient, % explained variation and F test of the average fiber diameters for the experimental design studied.

Variation source	AD_PVC/TiO ₂	AD_PVP/TiO ₂
Correlation Coefficient (R)	0.77	0.45
Coefficient of determination (R^2) (%)	88.08	67.36
F _{calculated}	5.66	1.66
F _{tabulated}	2.76	2.76
F _{calculated} /F _{tabulated}	2.05	0.60

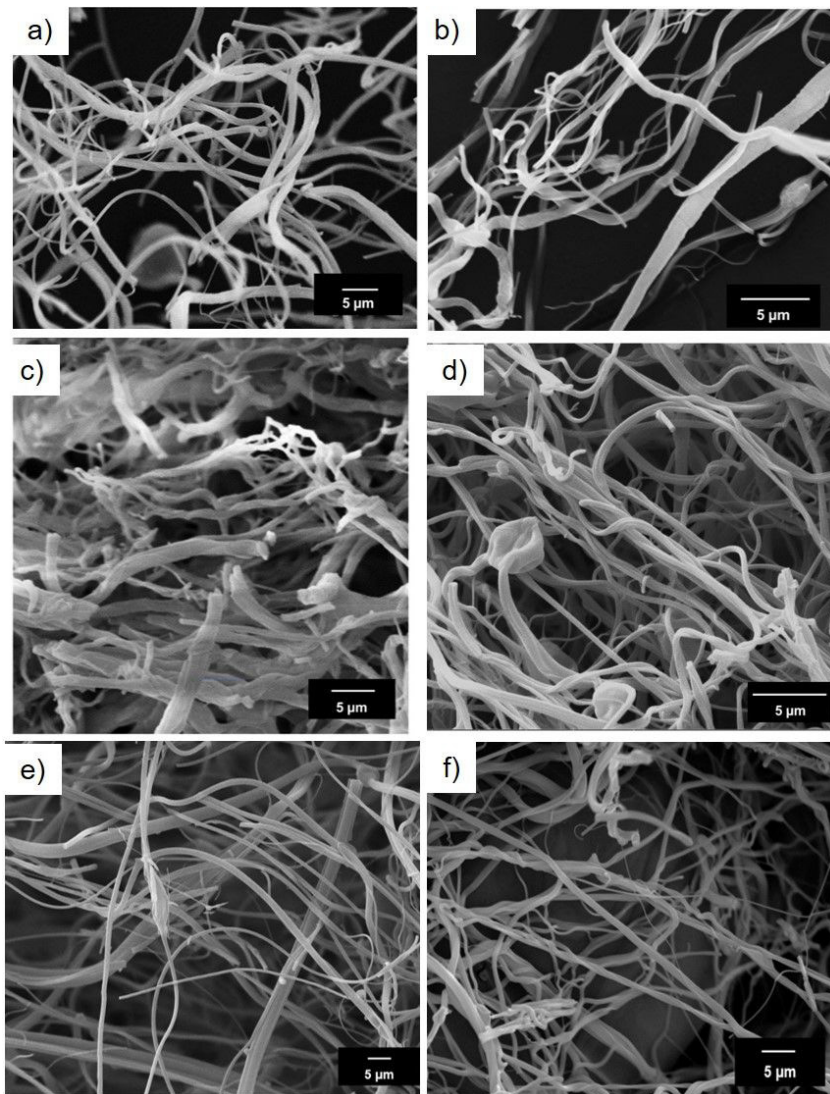


Figure 1. SEM images of fibers obtained from different processing conditions: PVC/TiO₂ fibers (a) 12%TTIP-30psi-4.4ml.h⁻¹, (b) 12%TTIP-70psi-10ml.h⁻¹ and (c) 8%TTIP-50psi-7.2ml.h⁻¹; PVP/TiO₂ fibers (d) 12%TTIP-50psi-4.4ml.h⁻¹, (e) 12%TTIP-70psi-4.4ml.h⁻¹ and (f) 4%TTIP-50psi-10ml.h⁻¹.

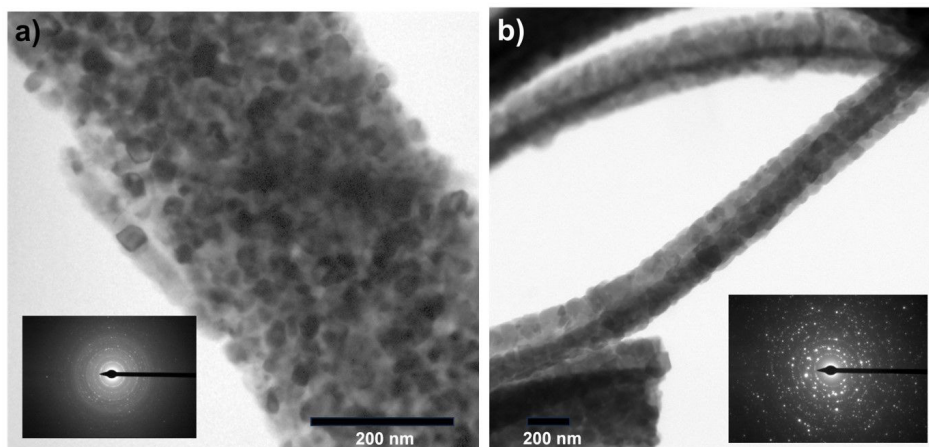


Figure 2. TEM images and selected area electron diffraction pattern (SAED) of fibers: (a) PVC/TiO₂ and (b) PVP/TiO₂.

Based on Table 4, the statistical significance analysis showed that the coefficient of determination (R^2) of the experimental results for PVC/TiO₂ fibers for the mean diameter was satisfactory, with a value greater than 88.08%. Thus, the mathematical model presented has more than 88% of the variations obtained explained by the model. For PVP/TiO₂ fibers the value of the coefficient of determination (R^2) was greater than 67.36%, with more than 67% of the variations obtained explained by the model.

The F-test is used as the criterion to evaluate the statistical significance of the regression coefficients of the determined parameters and shows a ratio between the $F_{\text{calculated}}$ and the $F_{\text{tabulated}}$, whenever this relation is greater than 1, the regression is statistically significant, that is, there is a relationship between the independent and dependent variables²⁸. However, according to Table 4, the F-test was greater than 1 only for PVC/TiO₂ fibers, indicating that there was a relationship between the independent and dependent variables studied.

The model is described in a reduced equation, considering only the significant coefficients, wherein TTIP concentration, air pressure, and feed rate are coded by X1, X2, and X3, respectively (Equations 3 and 4):

$$AD_{PVC/TiO_2} = (535.81 \pm 35.23) - (191.13X_1) - (102.12X_3) + 41.31 \quad (3)$$

$$AD_{PVP/TiO_2} = (539.59 \pm 31.61) + (85.87X_1 * X_2) + 37.66 \quad (4)$$

where AD is the average diameter.

Equation 3 suggests that the TTIP concentration and feed rate exhibit a direct relationship with the average diameter of the fibers of the system PVC/TiO₂. The increase in the TTIP concentration and feed rate will decrease average diameter of PVC/TiO₂ system. On the other hand, Equation 4 suggests that increasing the average diameter of fibers is due interaction between TTIP concentration and air pressure. These results indicate that processing parameters had different influences on fiber diameter according to the type of polymer and solvent used.

Moreover, according to equations the pressure had no statistical influence on the diameters of fibers of the system with a high volatile solvent (THF), however, on the system with low volatile solvent the pressure influenced the diameter in conjunction with TTIP amount.

Figure 3 shows the response surfaces obtained from the mathematical model (Equation 3) obtained for PVC/TiO₂ system. It was observed that higher TTIP concentration contributes positively to lower values of fiber diameter. Smaller fiber diameters were obtained with the use of higher feed rates (10psi) and higher TTIP concentration (12%) The fiber diameter is affected by the feed rate. The rate becomes ideal when it is equivalent to the rate of the jet that carries the solution, causing the fiber diameter to be reduced and to have a narrow distribution⁶. This ideal value is mainly affected by the viscosity of the solution, which depends on the molecular weight and concentration of the solution material, such as polymer, solvent and TTIP sources.

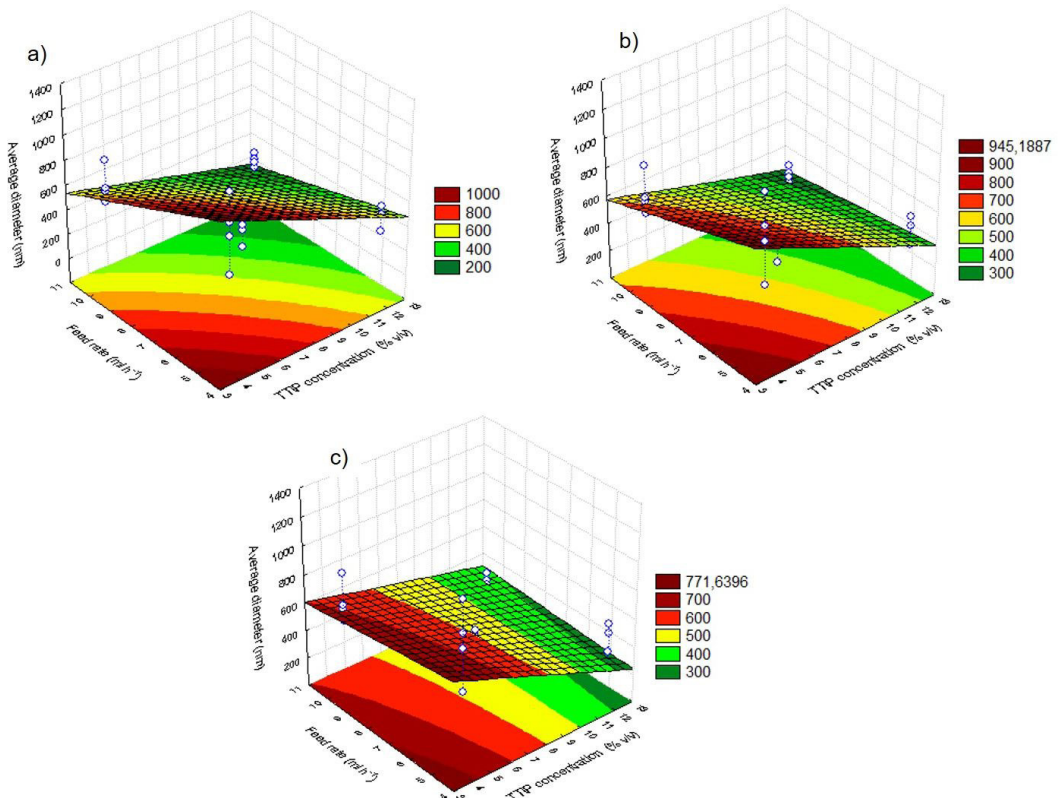


Figure 3. Response surface plots of PVC/TiO₂ fibers setting air pressure at: (a) 30 psi, (b) 50 psi and (c) 70 psi.

Based on Figure 4, produced for PVP/TiO₂ system (Equation 4), it was observed that smaller fiber diameters are obtained with the use of lower pressure together with a lower concentration of TTIP. According to Oliveira et al.⁶, at higher air pressures, there is an increase in the solvent evaporation rate and results in a decrease in diameter. This occurs because the airflow surrounding the surface of the jet exiting the nozzle does not allow an accumulation of solvent molecules immediately above the jet surface, therefore promoting a high evaporation rate. However, Oliveira et al.⁶ used SBS without a heated apparatus (work distance and collected chamber), such as used in this work. Previous work^{10,11,21}, that the used heated work distances and collected chambers, demonstrated that SBS is more efficient with auxiliary heating when producing ceramic fibers.

In the present work higher pressures will increase the volume of air (cold) in the work distance and difficult the evaporation process. While at low pressures, the heating of the air/solvents and the evaporation are more effectively. The evaporation process causes the coalescence of the particles and polymer and the decrease of fibers diameters.

In the Pareto Charts, effect bars that exceed the line $p\text{-value} = 0.05$ (for 95% confidence) are considered significant. Based on Figure 5 it was observed that the TTIP concentration and feed rate had a significant influence on the average diameter of the fibers of the PVC/TiO₂ system. In Figure 6, it was observed that only the interaction of the effects of TTIP concentration and air pressure, in the investigated range of values, was statistically significant at a significance level of 5% in the PVP/TiO₂ system.

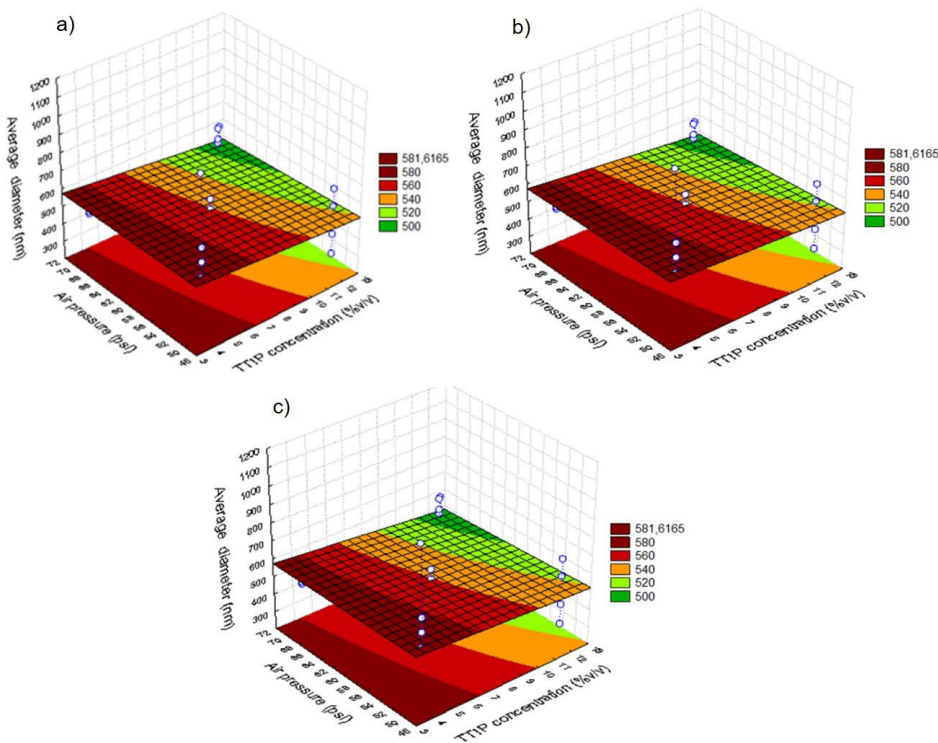


Figure 4. Response surface plots of PVP/TiO₂ fibers setting feed rate at.: (a) 4.4 mL/h, (b) 7.2 mL/h and (c) 10.0 mL/h.

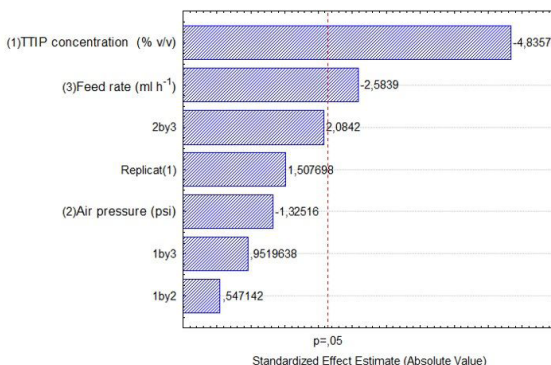


Figure 5. Pareto chart with 5% significance level of PVC/TiO₂ system.

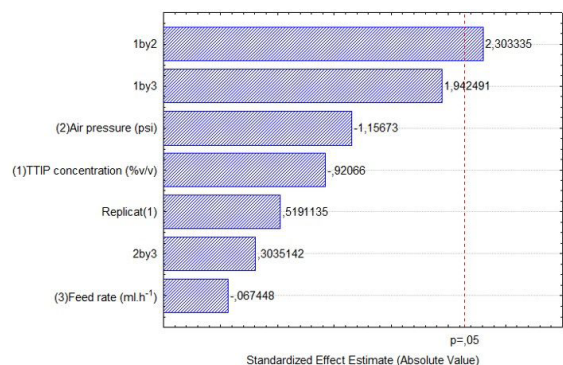


Figure 6. Pareto chart with 5% significance level of PVP/TiO₂ system.

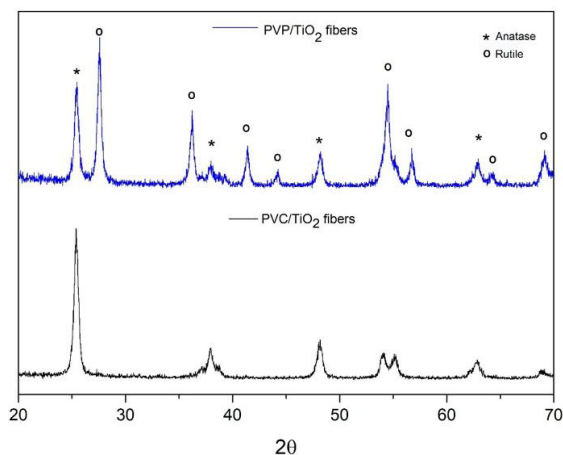


Figure 7. XRD patterns PVC/TiO₂ and PVP/TiO₂ fibers.

Anatase was the unique polymorph found in PVC/TiO₂ system containing tetrahydrofuran as the solvent and hydrochloric acid. Tetrahydrofuran is a polar aprotic solvent with a high basicity character and forms strong complexes³³. The strength of hydrochloric acid is limited (“leveled”) by solvent basicity¹⁹. This behavior may justify obtaining only anatase at the PVC/TiO₂ system, at the studied temperatures. The basicity of THF displaced the transition temperature of anatase-to-rutile transformation to higher temperatures, even when PVC decomposed releasing a high amount of hydrochloric acid. Zhou et al.³² synthesized hierarchical structures TiO₂ with different microstructures in nitric, hydrochloric and acetic acid via a surfactant-free and single-step solvothermal route. They observed that the acid medium affected the microstructure of TiO₂, precursors containing HCl as the acid medium have a tendency to form rutile while anatase was formed when using acetic or nitric acid, and the amount of HCl in the system contributed to the formation of rutile. Thus, as the amount of HCl used in this work was small (200 μl), there was no formation of rutile.

Furthermore, Costa et al.²¹ had suggested that the polymer crystallinity may influence the phase crystallization by increasing it. PVC and PVP are amorphous and semicrystalline polymers, respectively. PVC hinders the crystallization of TiO₂ and the formation of crystalline phases, consequently retarding the formation of the rutile phase. While PVP, is a semi-crystalline polymer, the crystallization effect is more accelerated and potentializes anatase-to-rutile phase transformation.

4. Conclusions

The TTIP concentration and feed rate statistically influenced the average diameters of the PVC/TiO₂ system. The smallest average diameter values were obtained using 12% of TTIP concentration and 10 psi of feed rate. The studied variables, TTIP concentration, air pressure and feed rate did not show any statistical influence on the average diameter of the PVP/TiO₂ system. The proper combination between polymer and solvent enables the obtaining of TiO₂ nanofibers with similar morphologies either using hydrophilic

or hydrophobic polymer. Only the anatase crystalline phase was found in the fibers with the PVC polymer and THF solvent, while two crystalline phases were obtained in the fibers with PVP and alcohol, anatase and rutile, indicating that the variation of the polymer and solvent has an effect on the crystalline phases of the TiO₂ fibers studied.

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