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Fluid mud induced by periodic tidal advection and fine-grained sediment settling in the Yangtze estuary

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This study presents *in-situ* observations of fluid mud in the Yangtze Estuary via a bottom tripod. Six occurrences of periodic fluid muds (F1-F6) were observed at high slack water, with suspended sediment concentration (SSC) exceeding 10 kg/ m³. The thickness of the fluid mud varied across the six occurrences, reaching a maximum of 0.32m. Notably, temperature and salinity anomalies were observed within the fluid mud. The formation of fluid mud was found to be influenced by turbulence, with turbulence kinetic energy (TKE) below $5 \times 10^{-4} \text{ m}^2/\text{s}^2$ favoring settling as the primary cause of formation. The critical shear stress (τ_{cw}) for fluid mud formation was estimated to be approximately 0.09 Pa. The formation of fluid muds during early tidal cycles was attributed to liquefaction and bed erosion resulting from strong waves. However, in most cases, the wave energy was insufficient for erosion, suggesting that advection played a role in sediment supply during the subsequent tide cycles. The increased cross-channel current velocity during flood facilitated the lateral transport of a significant amount of eroded sediment from shallow water into the channel. Due to its short duration, the fluid mud layer was entrained by the current before consolidation. Enhanced turbulence led to the breakdown of fluid mud at the early ebb. The critical $au_{\rm cw}$ for fluid mud breakdown depended on the density and duration of the fluid mud, with a maximum value of up to 0.70 Pa. The absence of the fluid mud layer during low slack water and neap tide was associated with a reduction in advection and tidal pumping, disrupting the original sediment balance between supply and demand. These data provide valuable insights into the formation and breakdown of fluid mud, contributing to estuarine hydrodynamic modeling studies and enhancing the understanding of estuary dynamics.

KEYWORDS

fluid mud, bed shear stress, advection, tidal pumping, Yangtze estuary

1 Introduction

Fluid mud is a common, highly concentrated suspension primarily composed of silt and clay, frequently found in the estuarine turbidity maximum (ETM), particularly in the near-bed layer (McAnally et al., 2007; van Rijn, 2016). Within the ETM, the collision process of suspended sediment results in sediment aggregation and floc formation, increasing the settling velocity of suspended sediment and ultimately leading to the formation of fluid mud (Winterwerp, 2002). The suspended sediment concentration (SSC) within fluid mud typically ranges from 10 to >100 kg/m³ (Ross and Mehta, 1989; Winterwerp, 1999), so this study considers the occurrence of fluid mud when the SSC exceeds 10 kg/m³. The thickness of fluid mud can vary, reaching several meters depending on sediment supply and settling time (Azhikodan and Yokoyama, 2018). Fluid mud strongly inhibits turbulence and reduces entrainment due to its high SSC, resulting in the SSC-induced stratification of the water column (Trowbridge and Kineke, 1994; Egan et al., 2020). Consequently, fluid mud has a high deposition rate, leading to siltation in waterways and harbors, affecting ship navigation (Wurpts, 2005). Dredging these sediments requires significant resources to maintain navigational depth in the channel (Dai et al., 2013).

The formation and evolution of fluid mud are primarily governed by two factors: sediment source and hydrodynamics. First, the formation of fluid mud requires sufficient sediment to maintain high SSC (Ge et al., 2020). Second, the hydrodynamics must facilitate the aggregation and retention of suspended sediment near the bed. In fact, due to processes such as consolidation, erosion, and entrainment, fluid mud exhibits strong spatial and temporal variability (Mehta, 1991; Wehr and Malcherek, 2012). Particularly, consolidation plays a crucial role in the evolution of fluid mud, as it gradually solidifies to form a new bed in the absence of external disturbances. Given its importance, there have been a few numerical efforts to incorporate consolidation in the simulation of fluid mud (e.g., Winterwerp, 1999). Moreover, in estuaries and coastal oceans, strong tidal currents have the ability to erode and entrain fluid mud into the upper water column (Becker et al., 2018; Wu et al., 2022).

Extreme weather condition is known to favor the formation of fluid mud (Wright and Friedrichs, 2006). During storm events, the combined forces of strong waves and tidal currents can erode the bed, resuspend and retain sediment near the bed, ultimately resulting in the formation of a fluid sediment layer. This particular form of fluid mud is commonly known as wavesupported fluid mud and is frequently observed on the continental shelf and in estuarine subaqueous deltas (*e.g.*, Hale and Ogston, 2015; Liu et al., 2022; Tang et al., 2023). Prolonged wave action can lead to an increase in excess pore pressure within the bed, resulting in a decrease in bed strength and localized liquefaction (Jeng, 2013; Anderson et al., 2017). In estuarine areas, winds and waves erode shoals and tidal flats, causing the resuspended sediment to converge in the channel under the action of tidal currents, ultimately forming fluid mud in the channel (Wan et al., 2014; Li W. et al., 2023). However, observations of fluid mud during storms are limited. Particularly, ship-based observations are impractical due to the difficulty of ship operations in strong waves and the potential for large measurement errors. Nevertheless, bottom tripod observations using acoustic and optical instruments enable long-term, *in-situ* observations regardless of weather conditions, although they do have limitations in space coverage.

On the other hand, fluid mud can also form under calm weather conditions. In fact, settling-induced fluid mud is a prominent type of fluid mud found in estuaries (Li et al., 2004). Suspended sediment in the water column gradually settles to form fluid mud during periods of weak hydrodynamics, such as slack water. This phenomenon is more prevalent in estuaries characterized by high SSC, including the Jiaojiang (Li L. et al., 2023), Severn (Manning et al., 2010), Weser (Becker et al., 2013), and Yangtze estuaries (Wu et al., 2022). The flocculation of suspended sediment is crucial for fluid mud formation, as it facilitates the rapid settling of sediment during slack water periods.

This study utilized field observations to examine the dynamics of fluid mud formation and evolution in the South Passage of the Yangtze Estuary. By analyzing *in-situ* data, we identified the presence of fluid mud during winter storms and elucidated the mechanisms behind its formation and breakdown through the examination of shear stress, liquefaction, erosion, and turbulence parameters. Additionally, we investigate the influence of advection and tidal pumping on the fluid mud process and present a schematic diagram illustrating the various modes of fluid mud formation in the Yangtze Estuary.

2 Study area

Our study area is located at the Yangtze estuary (Figure 1A). The Yangtze estuary is the fourth largest globally in terms of average annual sediment transport, and the runoff brings a huge amount of fine-grained sediments to the estuary (Milliman and Farnsworth, 2011). Its runoff has significant wet and dry season variations, with the wet season being approximately 2.5 times that of the dry season (Figure 1C). The Yangtze estuary is subjected to East Asian monsoon and is significantly affected by winter storms during the dry season, of which the maximum wind speeds can exceed 30 m/s.

In terms of hydrodynamics, the Yangtze estuary is dominated by irregular semidiurnal tides, with an average tidal range of 2.66 m, and a maximum tidal range of 4.62 m (Chen et al., 1988). Due to shallow water constituents, tidal asymmetry is pronounced in the water level and velocity, with ebb tide dominating. The duration of ebb is generally greater than 7 hours. Waves in the Yangtze estuary are primarily wind waves. The wave climate is highly correlated with local winds, with significant seasonal variations. The average wave height in winter (up to 1.4-2.7 m) is larger than that in spring and summer (1.1-2.1 m).



FIGURE 1

(A) The general location of the study area (dashed red box); (B) the monitoring station (red square) and the study area (Yangtze Estuary); (C) a twoyear time series of water discharge at Datong Hydrological Station in Yangtze River (Data source: http://www.cjh.com.cn/), the period of field observation is denoted by the gray shading.

3 Methods

3.1 Field observation

The observation station was located in the South Passage, near the mouth bar (Figure 1B). The observational period was between December 22 and December 31, 2018, during the transition from spring to neap tide. The observation consisted of a bottom-mounted tripod and a surface wave buoy (Figure 2). The configurations of instruments are briefly introduced below and the details are summarized in Table 1. Near-bed field water samples were collected at 1-hour intervals during the tidal cycle on December 24 and December 30, and three bed sediment samples (S1-S3) were collected during slack tide, as indicated in Figure 3A. S1 and S2 were collected prior to the winter storm event, and S3 was collected after the winter storm.

On the tripod, two Optical Backscatter Sensors (OBSs) (OBS-3A, D&A Instrument Co.) were deployed at the heights of 0.27 mab (meters above the bed) and 0.75 mab. These OBSs measured near bottom turbidity, temperature, and salinity at 1 Hz frequency with burst mode (Table 1). A downward-looking Acoustic Backscatter Sensor (ABS, Aquatec Group Limited) with four channels (0.5, 1, 2,



Position	Instrument	Height (mab)	Duration /Interval/Sampling frequency	Parameters	
Tripod	OBS	0.27	20 s/5 min /1 IIn	optical turbidity, temperature, salinity	
	OBS	0.75	50 \$/5 mm/1 mz		
	ABS	1.44	30 s/10 min/8 Hz	sediment concentration (0.02 m resolutio	
	ADV	0.42	512 c/10 min /16 Hz	current velocity, pressure	
	ADV	0.9	512 \$/10 mm/16 mz		
Виоу	Meteorological module	Surface	1 hour/10 min/4 Hz	wind, wave, air pressure	
	ADP	Surface	30 s/5min/1 Hz	current velocity profile	

TABLE 1 Deployment information for instruments in the tripod and wave buoy.

4 Hz) was deployed at 1.44 mab to acquire high resolution vertical profiles (0.02 m) of SSC. Two Acoustic Doppler Velocities (ADVs) was mounted at the height of 0.42 mab and 0.9 mab. These ADVs measured high-frequency current velocity and pressure at 16 Hz with burst mode (Table 1).

On the wave buoy, a meteorological module was installed to obtain wind speed and direction, air temperature and pressure, and wave parameters such as significant wave height (H_s) , wave period (T) and wave direction. In addition, a downward-looking Acoustic Doppler Profiler was mounted on the buoy to obtain current velocity profile of the water column.

OBS turbidities were converted to SSCs based on the regression curves (Figure 4). ABS calibration was conducted with the recursive algorithmic method: the sediment sound-absorption coefficient was acquired by referring to SSCs from OBS, and ABS SSC profiles were then obtained by recursive algorithmic (see details in Wu et al. (2022). The grain size distributions of bed sediment and field water samples were obtained with a laser diffraction particle size analyzer (range $0.02-2000 \mu m$, Malvern MasterSizer 2000).

3.3 Current velocities

3.2 SSC calibration and grain size

In order to obtain field SSCs, the method described in Wu et al. (2022) was adopted to calibrate OBS turbidity versus SSC; and the

First, the ADV velocity data were quality controlled: data records with good signal-to-noise ratio (>20) or high correlation coefficient (>0.7) were labelled as effective. Then, the near bottom mean velocity was acquired by averaging over each burst which has



FIGURE 3

(A) Time-depth distribution of SSC (only show data within 1 m), three bed sediment samples were collected at S1-S3, black solid line indicates seabed variations; (B) current velocity (black line) and turbulent kinetic energy (TKE, red line) calculated from ADV at 0.75 mab; (C) estimated bed shear stress by current (τ_{cr} , blue line), wave (τ_{wr} , red line) and combined wave-current action (τ_{cwr} , dotted line). Light gray shading represents the winter storm event, dark gray shading represents the presence of fluid mud (F1-F6).



over 70% effective data. The mean velocity in the upper water column was acquired from ADP with similar approach.

3.4 Liquefaction degree

Klammler et al. (2021) defined a dimensionless liquefaction parameter (liquefaction degree *L*):

$$L = \begin{cases} \lim_{z \to 0^{-}} \frac{-\gamma_w \sigma_z}{(\gamma_s - \gamma_w)z}, \sigma_z > 0, \\ 0, \sigma_z \le 0 \end{cases}$$
(1)

where σ_z is wave induced vertical effective stress (unit m) and γ_w and γ_s are specific weights of seawater and saturated sediment, respectively. The limit of *z* approaching 0⁻ is due to the fact that liquefaction occurs below the surface of the bed. If σ_z is negative, it will have a compressive effect on the sediment and stabilize the bed (L = 0). Positive σ_z values enhance sediment buoyancy and raise the risk of bed instability (L > 0). $L \ge 1$ is indicative of a fully liquefied bed (*i.e.*, a fluid state). When 0 < L < 1, the low critical bed shear stresses result in an increased likelihood of bed instability and erosion, even though the bed is not fully liquefied.

The wave induced vertical effective stress (σ_z) can be expressed as:

$$\sigma_z = \operatorname{Re}\left\{\sum_m a_m S(z) \exp[i(k_m x - \omega_m t + \epsilon_m)]\right\},\tag{2}$$

where a_m and e_m are the amplitude and phase of surface waves with different wave number (k_m) and frequency (ω_m) , which can be derived from ADV-measured pressure via Fourier analysis. S(z)varies with depth and is a function of bed properties such as porosity, horizontal and vertical hydraulic conductivities, degree of saturation, shear modulus, Poisson ratio, density and elastic modulus of fluid, the absolute pore pressure for average water depth, and vertical thickness of the sediment bed above some assumed rigid impermeable bedrock. For more details, please refer to Klammler et al., 2020).

Once σ_z exceeds the reduced gravity of sediment (gravity force minus buoyancy force), sediment instability (or bed failure) can take place; and the failure depth is the deepest location where sediment instability can occur, *i.e.*, the depth where σ_z just balances with the reduced gravity.

3.5 Shear stress

The Reynolds stress method (RS), the turbulent kinetic energy method (TKE), the modified turbulent kinetic energy method (TKEw), and the turbulent inertial dissipation method (ID) are the four mainstream methods for calculating the bed shear stress induced by current (Kim et al., 2000). The specific equations are shown in Table 2, and the results of the four methods are averaged to obtain the final current shear stresses (τ_c).

The bed shear stress induced by wave (τ_w) can be expressed as follows (Soulsby, 1995),

$$\tau_w = \frac{1}{2}\rho f_w u_w^2 \tag{3}$$

$$f_{w} = \begin{cases} \exp\left(-7.30 + 5.61(A_{k})^{-0.109}\right), A_{k} > 100\\ \exp\left(-8.82 + 7.02(A_{k})^{-0.078}\right), 0.2 < A_{k} \le 100 \end{cases}$$
(4)
0.3, $A_{k} \le 100$

TABLE 2 The equations of calculating current shear stress (τ_c).

Method	Equation			
RS	$\tau_c = \rho\left(-\overline{u'w'}\right)$			
TKE	$\tau_c = 0.19 \rho \left(\overline{u^{'2}} + \overline{v^{'2}} + \overline{w^{'2}} \right)$			
TKEw	$ au_c = 0.9 ho \left(\overline{w^{'2}} ight)$			
ID	$\tau_{c} = \rho u_{*}^{2}, \ u_{*} = \left(\frac{2\pi\kappa z}{\bar{u}}\right)^{1/3} \left(\frac{P_{w}(f)f^{5/3}}{\alpha}\right)^{1/2}$			

p is fluid density, u', v' and w' are turbulence fluctuations in east, north and vertical directions, P_w (f) is the spectral density of the vertical turbulence component, κ is the von Karman constant ($\kappa = 0.4$), α is the Kolmogorov constant ($\alpha = \sim 0.69$), \overline{u} is the average current velocity, u is the friction velocity.

where f_w is the wave friction factor, u_w is the wave orbital velocity, $A_k = A_w/k_s$, $A_w = u_w T/2$ is the semi-orbital excursion, k_s is the Nikuradse roughness ($k_s = 2.5D_{50}$, D_{50} is the median grain size).

Based on the current and wave shear stress, combined wave and current shear stress can be calculated by Eq. (4) (Soulsby, 1995).

$$\tau_{cw} = \tau_c \left[1 + 1.2 \left(\frac{\tau_w}{\tau_c + \tau_w} \right)^{3.2} \right]$$
(5)

3.6 Suspended sediment flux

Following Dyer (1997), the net suspended sediment flux (*F*) can be expressed as:

$$F = \frac{1}{T} \int_{0}^{T} \int_{0}^{H} (U \cdot c) dz dt$$

= $\underbrace{c_{0} \ u_{0}H_{0}}_{F_{1}} + \underbrace{c_{0} \ \overline{u_{t}H_{t}}}_{F_{2}} + \underbrace{u_{0} \ \overline{H_{t}C_{t}}}_{F_{3}} + \underbrace{H_{0} \ \overline{u_{t}C_{t}}}_{F_{4}} + \underbrace{\overline{c_{t}u_{t}H_{t}}}_{F_{5}} + \underbrace{H_{0} \ \langle \overline{u_{d}}\overline{c_{d}} \rangle}_{F_{6}} (6)$
+ $\underbrace{H_{0} \ \langle \overline{u_{dt}c_{dt}} \rangle}_{F_{7}}$

where *T* is the tidal period, *H* is the water depth, *u* is the current velocity, *c* is the SSC. The subscript 0 denotes the spatial and temporal mean value, the subscript *t* denotes the vertically averaged tidal variation, the subscript *d* denotes the deviations from the vertical means, and the subscript *dt* denotes the temporal deviations from the tidally averaged deviations from the vertical means. *H*_t denotes the tidal variation in depth. Angled brackets (< >) and overbars ([¬]) denote the means over the depth and the tidal cycle, respectively. The terms F_{3} - F_{5} in Eq. (6) are tidal pumping terms and the tidal pumping induced sediment transport flux can be expressed as F_{tp} = F_3 + F_4 + F_5 .

4 Results

4.1 Temporal variation of observations

The time series of observed meteorological and hydrodynamical data are shown in Figure 5. During the observational period, winds were predominantly northerly, with an average wind speed of 8.34 m/

s and a maximum wind speed of 12.60 m/s (Figure 5A). The mean depth of the observation station was 7.65 m. The tidal water level was mostly semidiurnal but with diurnal inequality and the maximum tidal range reached 4.20 m (Figure 5B). The significant wave height correlated with wind speed (Figure 5B) and the wave direction was almost identical to the wind direction (Figure 5C), indicating that the waves were dominated by wind waves. The near bottom current was reciprocating flow, which was northwestward/southeastward during flood/ebb tide (Figure 5D). The maximum flood and ebb velocities at 0.75 mab were 1.15 m/s and 0.76 m/s, respectively. The minimum current velocity (*i.e.*, slack water) occurred approximately 80 min after high or low water. Semidiurnal variations were also significant in the temperature, salinity, and SSC time series (Figures 5E–G). The peak of near-bed SSC occurred during slack water, implying that settling led to the aggregation of suspended sediment.

There were two events with wind speeds exceeding 10 m/s (December 23rd 3:00-6:00 and 26th 4:00-29th 16:00), and accompanied by large waves, which H_s reached a maximum of 1.02 m. The windy weather was short-lived on December 23rd, with wind speed exceeding 10m/s for only four hours, and didn't result in significant changes in near-bed water characteristics (temperature, salinity and SSC). A very distinct winter storm event occurred between December 26th and 29th (light gray shade in Figure 5) with H_s consistently greater than 0.4 m. The winter storm event occurred in the intermediate tide, which was accompanied by a rise in air pressure and a drop in near-bed water temperature of approximate 3 °C (Figures 5A, E), and resulted in a high SSC near the bed, with maximum values exceeding 20 kg/m³ (Figure 5G). Salinity minima near the bed in winter storm event (~7 PSU) (Figure 5F).

4.2 Characteristics of periodic fluid mud

A total of 6 fluid mud events were detected during the observation, when the near bottom SSC exceeded 10 kg/m³ (labeled F1-F6 in Figure 3A). A closer examination revealed that these events took place during certain phase of the tide. They always formed at high slack water and existed for 1-2 hours before they disappeared during the following ebb tide. The fluid mud thickness is the height difference between the top (contours with SSC of 10 kg/m³) and bottom (sea bed measured by ABS) of the fluid mud layer. The maximum thickness of fluid mud was small (only 0.18 m) for F1 and F2 and approximately 0.30 m for F3-F6 (Table 3). The maximum SSC and density at 0.27 mab in F1 and F2 were also lower than those in F3-F6; and the maximum density at 0.27 mab in F3-F6 were generally greater than 1025 kg/m³. The duration of fluid mud event was relatively short in F1, F2, and F4 (c.a. 1 hour), while it reached approximately 2 hours in F3, F5, and F6.

During F3-F6, salinity anomalies due to fluid mud were clearly evident (Figure 5F), especially at 0.27 mab; and up to 1 PSU decrease was observed. Moreover, the vertical gradient of salinity reversed during these events and salinity was lower at 0.27 mab than at 0.75 mab. Given the conductivity of sediment is significantly lower than that of water, the decrease in salinity can be attributed to high SSCs (Traykovski et al., 2004). In addition, temperature



Time series of meteorological, hydrodynamic and water characteristics. (A) wind (black vector) and air pressure (P_{air} , red line); (B) significant wave height (H_{sr} , black line) and water depth (red line); (C) wave period (T_{pr} , black line) and wave direction (red dots); (D–G) current velocity, temperature, salinity and suspended sediment concentration (SSC) at 0.75 mab (black line) and 0.27 mab (red line). Light gray shading represents winter storm event, dark gray shading represents the presence of fluid mud (F1-F6).

anomalies occurred simultaneously with salinity anomalies, which may also be attributed to fluid mud. A similar, but less obvious, situation was also found in F1 and F2 (see section 5.2 for detailed discussion).

4.3 Formation and breakdown of fluid mud

All 6 fluid mud events occurred during periods of high slack water (Figure 3B). In all cases, the bottom velocity was less than

0.15 m/s ($\nu_{0.75f}$ in Table 3), and TKE was less than $5 \times 10^{-4} \text{ m}^2/\text{s}^2$ (Figure 3B) at the moment of fluid mud formation. Therefore, the weak hydrodynamic favored the settling of suspended sediment. Moreover, the *in-situ* floc particle size in the South Passage of Yangtze estuary can reach 80 µm during slack water, and the settling velocity is approximately 1 mm/s (Lu et al., 2020), which also facilitates the formation of fluid mud in a short period of time. Bed shear stress (τ_{cw}) was mainly contributed by tidal-induced shear stress (τ_{c}) rather than wave-induced shear stress (τ_{w}). Although τ_{w} increased significantly during the winter storm, τ_{cw}

TABLE 3 The maximum thickness (h_{max}), maximum SSC at 0.27 mab (SSC_{max0.27}), maximum density at 0.27 mab (density) and duration of the six fluid mud events (F1-F6); the current velocity at 0.75 mab ($v_{0.75f}$) and the bed shear stress (τ_{cwf}) at the moment of fluid mud formation; the bed shear stress at the moment of fluid mud breakdown (τ_{cwb}).

fluid mud event	h _{max} (m)	SSC _{max0.27} (kg/m ³)	density (kg/m ³)	duration (min)	v _{0.75f} (m/s)	τ _{cwf} (Pa)	τ _{cwb} (Pa)
F1	0.18	6.01	1017	70	0.03	0.09	0.24
F2	0.18	7.23	1017	50	0.04	0.07	0.16
F3	0.32	34.5	1032	130	0.06	0.07	0.46
F4	0.26	21.23	1025	40	0.12	0.07	0.24
F5	0.30	34.13	1027	120	0.03	0.07	0.36
F6	0.30	35.67	1033	120	0.15	0.09	0.45

was weak and less than 0.3 Pa during the presence of fluid mud (Figure 3C). According to τ_{cwf} in Table 3, the critical shear stress for fluid mud formation was approximately 0.09 Pa.

The breakdown of fluid mud occurred at relatively high current velocity in the ebb tide, when the bottom velocity exceeded 0.2 m/s (Figure 3B). At this time, TKE was greater than $2 \times 10^{-3} \text{ m}^2/\text{s}^2$, four times greater than that at the moment of fluid mud formation, suggesting that sediment entrainment due to enhanced turbulence led to the breakdown of fluid mud. It is worth noting that TKE during ebb tide was much larger than that during flood tide, which favored the sediment entrainment. The τ_{cw} was all greater than 0.15 Pa at the breakdown of fluid muds (τ_{cwb} in Table 3). However, the critical τ_{cw} for fluid mud breakdown varied among these events, which was less than 0.25 Pa in F1, F2, and F4 but reached 0.46 Pa in F3. In fact, the critical τ_{cw} depends on the consolidation of fluid mud which is a function of the density and the duration of the fluid mud (Winterwerp, 1999).

5 Discussions

5.1 Sediment sources of fluid mud

5.1.1 Local resuspension

The liquefaction degree (*L*), which is a dimensionless liquefaction parameter based on the vertical effective stress (Klammler et al., 2021), generally exceeded 0.25 during the winter storm event (Figure 6A). *L* was larger than 1 only at the maximum H_s and the failure depth caused by liquefaction was 0.047 m, which was comparable to the erosion depth (0.04 m) of the bed before F1 (Figure 3A). Despite the low τ_{cw} (< 1 Pa), the bed was eroded by 0.08 m right before F2, indicating that liquefied bed was more susceptible to erosion.

Compared to the bed sediment sample S1, S2 has an increased fine-grained component, which is consistent with the sediment in the water sample (Figures 6B, C). The increase in fine-grained



FIGURE 6

(A) liquefaction degree, L (blue bar) and failure (or liquefaction) depth (red dashed line), black line denote the peak of L for the local maxima of each 1-h interval, $L \ge 1$ represents the presence of the liquefaction event, light gray shading represents winter storm event, dark gray shading represents the presence of fluid mud; (B, C) Grain size distribution of water samples (averaged) and bed sediment samples (S1-S3) collected from the observation field.

sediments on the seabed also ensures that eroded sediments can serve as a source of fluid mud (Hale and Ogston, 2015). The grain size distribution from S2 to S3 revealed a transition in the bed sediment from a bimodal distribution to a single-peaked distribution (Figure 6C), which implies these bed sediments were highly active. Thus, locally resuspended sediments due to bed erosion provide a source for F1 and F2 events.

5.1.2 Erosion in shallow water

In contrast to F1, L was smaller than 1 and the seabed elevation did not change significantly during the tidal cycles of F3-F6. However, the thickness of fluid mud during F3-F6 was larger than that in F1, suggesting an additional sediment source. Apart from local resuspension within the channel, shallow waters are more susceptible to erosion during storms. According to the liquefaction equation in Klammler et al. (2020), the failure depth due to liquefaction could be up to 0.2 m in shallow water with an average water depth of only 2 m, which is comparable to the thickness of intertidal flats erosion during storms observed by previous authors (*e.g.* Li et al., 2004; Shi et al., 2021). Waveeroded intertidal flats in the storm also contributes to the sediment supply of fluid mud.

5.2 Advection

The time derivative of SSC is attributed to both advection and local resuspension/deposition (Li et al., 2018). With a onedimensional box model, Li et al. (2021) confirmed that sediment advection dominates over local sediment resuspension in the South Passage of the Yangtze estuary. Indeed, during F3-F6, the influence of wave-induced local resuspension decreased, while the thickness of fluid mud increased, suggesting that advection was the primary sediment source.

In fact, lateral advection in estuaries has an important influence on sediment distribution in the channel-shoal system (Scully et al., 2009; Zhou et al., 2021); and the lateral exchange of sediment between the channel and the adjacent tidal flats was known to be significant (Wang et al., 2010; Zhu et al., 2016). Numerous studies have demonstrated the impact of storm winds and waves on lateral circulation in estuaries (e.g., Chen et al., 2009; Li and Li, 2011; Green and Coco, 2014). On one hand, wind-driven lateral circulation was found to have a strong impact on the lateral distribution of SSCs (Gong et al., 2023). On the other hand, wave-induced erosion of tidal flats can effectively increase SSC over the shoal, and the lateral differences of SSC-induced density can contribute to the crosschannel baroclinic pressure gradient force, enhancing bottom currents from shoal to channel. Such process favors the formation of fluid mud by adding fine sediment to the estuarine pool (Green and Coco, 2014; Zhang et al., 2021).

A comprehensive field investigation on how lateral advection contributes to fluid mud formation requires multiple stations along the cross-channel direction, given its spatially varying nature. Nevertheless, even though this study has only one station, the available data can still provide us some hints about the role of lateral advection in fluid mud formation. Time-averaged vertical profiles of current velocity during the winter storm were compared with those during normal weather conditions (Figures 7A-D). During flood tide, the along-channel current was weaker in the surface and bottom but stronger in the middle water column during the winter storm (Figure 7A). Nevertheless, the storm-driven crosschannel current was significantly stronger in the middle water column, indicating enhanced lateral flow (Figure 7C). Meanwhile, stormy weather can result in significant erosion of sediments from shoal and tidal flats (Li et al., 2001). Therefore, lateral transport of sediment can be greatly enhanced during flood. These sediments can serve as an essential source for the formation of fluid mud during high slack water once they entered the channel. In contrast, winter storm resulted in a clear decrease in current velocities during ebb, particularly in the near-bottom layer (Figures 6D, 7B). Consequently, the lateral transport was inhibited and the insufficient sediment supply prevented the formation of fluid mud during low slack tide. Moreover, the wave direction gradually changed from northeast (cross-channel) to northwest (alongchannel) during the storm (Figure 5C). This could also affect the lateral circulation via wave-current interaction (Gong et al., 2023), modulating fluid mud formation.

5.3 Tidal pumping

Aggregation of sediments is essential to the formation of fluid mud. In estuaries, a number of effects can lead to sediment aggregation, such as advection, tidal pumping and estuarine circulation. Among them, tidal pumping is widely acknowledged as a primary mechanism responsible for the formation and maintenance of the ETM (Dyer, 1997; Yu et al., 2014). The presence of estuarine fluid mud is typically observed within the ETM (Nichols, 1984; Schrottke et al., 2006), suggesting that tidal pumping plays a role in the formation of the fluid mud layer. Tidal pumping induces sediment convergence within the ETM, ensuring a continuous supply for the formation of fluid mud (Wu et al., 2022).

The depth-integrated sediment transport were analyzed with the decomposition method described in Dyer (1997), and tidal pumping term of each tidal cycle are shown in Figure 8. The tidal pumping flux during the tidal cycle of F3, F5, and F6, which had a thick fluid mud layer, was considerably higher compared to that during peak spring tide and normal weather (December 25). In the case of fluid mud event F4 with weak tidal pumping, there was a reduction in fluid mud thickness, indicating the limited contribution of tidal pumping to fluid mud formation. A continuous sediment supply is necessary to sustain the dynamic equilibrium between fluid mud formation and breakdown (Becker et al., 2018).

In general, weak hydrodynamics during neap tide make it more likely for fluid mud to form and sustain (Uncles et al., 2006; Ge et al., 2020). Adequate sediment supply is a necessary condition for fluid mud formation (Kineke et al., 1996), but the reduction in tidal pumping flux can disrupt the balance between supply and demand, resulting in insufficient sediment to form the fluid mud layer during neap tide (Wu et al., 2022).



5.4 Schematic diagram of storm-induced fluid mud formation in the Yangtze Estuary

A schematic diagram of fluid mud formation under storm condition in the Yangtze Estuary is shown in Figure 9. During storm events, sediments in shallow waters such as intertidal flats can be significantly eroded. The resuspended sediments can be more easily transported to the channel by the enhanced lateral component of flood current. Meanwhile, tidal pumping can facilitate the convergence of sediment flux in the longitudinal direction. The combined effects of lateral advection and tidal pumping lead to high concentration of suspended sediment which settles rapidly to the bed during high slack water, resulting in the formation of fluid mud. The disappearance of fluid mud during the following ebb tide is related to the enhanced bottom shear stress and reduced lateral sediment supply. This fluid mud mode differs from wave-induced fluid mud on the shelf, which is formed by bed liquefaction and sediment resuspension (e.g. Hale and Ogston, 2015).



Tidal pumping induced sediment transport flux (F_{tp}) of each tidal cycle during observation and maximum thickness of fluid mud events F1-F6. Light gray shading represents the time of winter storm event.



6 Conclusions

A bottom tripod and a wave buoy were deployed during 9 days spring-neap tidal cycle observation. An evident winter storm event occurred during the intermediate tide, characterized by rising air pressure and a decrease in water temperature. The bottom water temperature dropped by approximately 3 °C. Periodic occurrences of fluid mud (F1-F6) were observed with SSC exceeding 10 kg/m³ within the winter storm event. These fluid muds formed during periods of high slack water when hydrodynamics was weak. The thickness of fluid mud varies between the different fluid mud occurrences. Fluid muds F1/F2 have a low thickness, while F3-F6 exhibit a higher thickness, with a maximum of 0.32 m. Temperature and salinity anomalies were observed within the fluid mud occurrences, particularly for F3-F6.

The formation and disappearance of fluid mud during slack water are primarily controlled by settling and entrainment processes. During high slack water, weak hydrodynamic with low TKE favor settling of suspended sediment, resulting in the formation of fluid mud. The in-suit floc particle size can reach up to 80 µm and the settling velocity is approximately 1 mm/s, ensuring rapid settling of sediments. The critical shear stress (τ_{cw}) for fluid mud formation is estimated to be approximately 0.09 Pa. Fluid mud is present for a short duration (maximum 130 minutes), leading to its entrainment before consolidation occurs. The breakdown of fluid mud took place at early ebb tide, when the velocity at 0.75 mab exceeded 0.2 m/s. Turbulence enhanced and the τ_{cw} exceeded 0.15 Pa during the breakdown of fluid mud. However, the critical τ_{cw} for fluid mud breakdown was not constant, and varied depending on the consolidation of fluid mud, which is in relation to the density and duration of the fluid mud. The critical $\tau_{\rm cw}$ was only 0.16 and 0.24 in F1/F2/F4, and reached a maximum of 0.70 Pa in F3.

Liquefaction and bed erosion caused by strong waves provided a source of material for the formation of fluid muds F1 and F2. However, in most cases, the waves did not reach the level of bed erosion, as observed during the F3-F6 period. Advection served as the primary source of material in F3-F6. The cross-channel current velocity significantly increases in the middle layer of the water column during flood tide, indicating an enhancement in lateral transport. During stormy weather, substantial amounts of sediment are eroded from shoals and tidal flats and transported into the channel through lateral transport. Current velocities and sediment transport by advection are reduced during ebb in the winter storm, which further results in the absence of fluid mud formation during low slack water.

Tide pumping is also a contributing factor in the maintenance of periodic fluid mud during the winter storm, as it continuously supplies sediment for fluid mud formation. The thickness of fluid mud was large during the tidal cycle of F3/F5/F6 when tidal pumping flux was large. The absence of the fluid mud layer during neap tide resulted from a reduction in both tidal pumping flux and lateral transport after the winter storm event, which disrupted the original sediment balance between supply and demand.

Data availability statement

The raw data supporting the conclusions of this article will be made available by the authors, without undue reservation.

Author contributions

HW: Conceptualization, Data curation, Formal Analysis, Investigation, Methodology, Visualization, Writing – original draft. JT: Data curation, Methodology, Writing – review & editing. WL: Data curation, Methodology, Writing – review & editing. FX: Methodology, Writing – review & editing. HY: Methodology, Writing – review & editing. FZ: Conceptualization, Formal Analysis, Resources, Supervision, Writing – review & editing. YW: Conceptualization, Formal Analysis, Resources, Supervision, Writing – review & editing.

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Conflict of interest

The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

The reviewer, JC, declared a past co-authorship with the author, YW.

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