

Data-driven and physics-based interval modelling of power spectral density functions from limited data

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Abstract

In stochastic dynamics, ensuring the structural reliability of buildings and structures is of paramount importance, especially when subjected to environmental loads such as wind or earthquakes. To adequately address these loads and the uncertainties associated with them, it is often necessary to utilise advanced load models, frequently expressed using a power spectral density (PSD) function. The construction of these load models becomes challenging when only limited data is available and meaningful statistics cannot be reliably derived. To address this issue, safety bounds are commonly used in load models to account for uncertainties. Many PSD functions, such as the Clough-Penzien model, are described by parameters with a physical background and can therefore reflect the real case. The aim of this work is to expand these physical parameters in order to account for uncertainties. For this purpose, bootstrapping is used to derive more reliable statistics. By introducing a scaling parameter that allows for flexibility, bounds of the data set can be derived. Consequently, suitable PSD models are fitted to the derived bounds. The PSD function is thus represented by intervals for its physical properties instead of relying on discrete values. When applying such a bounded load model to a structure, advanced interval propagation schemes can be utilised to bound the failure probability.

Keywords: Power spectral density function, Random vibrations, Stochastic processes, Stochastic dynamics, Uncertainty quantification.

1. Introduction

The ever-increasing demands for safer and more robust structures have led researchers and engineers to explore new avenues in the assessment of structural reliability. Traditional design approaches that rely solely on deterministic methods can fail to recognise the profound impact of uncertainties that occur in real-world scenarios. Stochastic dynamics [1, 2, 3, 4] and structural reliability [5, 6] offer a useful approach to model and integrate loads and material properties probabilistically or imprecisely, allowing for a more comprehensive understanding of structural behaviour under random excitations, such as earthquakes or wind loads.

The power spectral density (PSD) function [7, 8] is a key tool in the study of stochastic dynamics and plays a crucial role in evaluating the response of structures subjected to random excitations. It provides a representation of a stochastic process in the frequency domain or for more realistic cases in the time-frequency domain [9, 10, 11], which result in so-called *evolutionary* PSD (EPSD) functions. It enables to understand the distribution of power across different frequencies. The PSD function provides a relationship between the time domain and the frequency domain and enables easier analysis of structures under stochastic loads. By applying the concept of the PSD function, engineers can transform the problem of evaluating the structural response to random loads into a simpler frequency domain problem. This transformation facilitates the identification of critical resonant frequencies and enables the design of structures with better resistance to vibrations caused by dynamic loads. Including the PSD function in structural reliability analysis allows for a more realistic representation of the loads. Real world dynamic loads, such as earthquakes, wind loads or ocean waves have random characteristics in terms of both amplitude and frequency content. The PSD function allows for capturing these statistical characteristics and take them into account in reliability assessment to ensure that structures are designed to withstand certain dynamic excitations. Despite its merits, working with the PSD function may present

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26 challenges, particularly when dealing with non-stationary processes or limited experimental
27 data. Addressing these challenges requires innovative techniques in signal processing and
28 statistical analysis, as well as advancements in data-driven approaches to estimate the PSD
29 function accurately.

30 In cases where the availability of data is limited, it is important construct robust models
31 for the PSD function, thus an adaptable approach becomes imperative. Three distinct
32 avenues can be identified for addressing this challenge: (i) a strictly data-driven methodology
33 without explicitly incorporating physical principles, (ii) a purely physics-based approach,
34 reliant solely on theoretical formulations without direct data influence and (iii) a synergistic
35 approach that combines data-driven and physics-based aspects. In this research, the third
36 approach is selected due to its potential to combine the strengths of data-driven techniques
37 with the physical principles of PSD functions and corresponding stochastic processes. This
38 strategy not only accommodates limited data scenarios, but also takes advantage of the
39 improved performance that can be achieved by incorporating available physical knowledge
40 into the modelling process. The aim is to provide a comprehensive framework that uses
41 the advantages of both data and physics-based knowledge to construct reliable and accurate
42 PSD models, thereby contributing to an understanding of the underlying system dynamics.

43 While stochastic dynamics and structural reliability offer a promising approach for de-
44 signing new structures, several challenges arise when dealing with real-world data, especially
45 in the context of estimating PSD functions and assessing structural reliability. Often, only
46 limited experimental data or historical records are available, leading to uncertainties es-
47 pecially in estimating a reliable PSD function. The lack of data can affect the accuracy
48 of PSD estimation and thus lead to incorrect reliability analysis. Measurement errors and
49 uncertainties are a critical aspect as they can significantly affect the accuracy and relia-
50 bility of experimental data used for analysis and design. These uncertainties arise from
51 various sources, such as equipment limitations, sensors which may calibrated inaccurately,
52 environmental conditions or simply due to the digitisation of data [12]. Understanding and
53 quantifying these uncertainties is critical to perform reliable probabilistic analyses. Some
54 general approaches in the field of uncertainty quantification have already been carried out.

55 These can be broadly divided into probabilistic approaches [13], interval approaches [14] or
56 imprecise probabilities [15]. More specifically, approaches for problems under limited data
57 can be tackled by [16, 17] or many more.

58 The main focus of many works is to establish reliable bounds for a given set of data
59 or parameters. Some approaches in this area have already been addressed. The bounding
60 of the failure probability based on different interval parameters of PSD models has been
61 carried out in [18]. A large set of accelerograms was utilised in [19] to determine different
62 representations of PSD function. In [20], a limited number of PSD functions are used to
63 determine an upper and lower bound using radial basis function networks. However, it is
64 crucial to question the reliability of such bounds, especially when dealing with limited data.
65 This paper addresses the problem of uncertain bounds. It aims to increase the credibility
66 of limited data approaches by addressing the reliability of the resulting bounds. On many
67 occasions, the available data is limited, thereby requiring an assessment of the accuracy of
68 the bounds. This approach attempts to address these concerns and introduce flexibility in
69 the definition of these bounds.

70 The goal of this work is to determine bounds for the physical parameters of an analytical
71 PSD function, such as the Kanai-Tajimi PSD [21, 22] model or the Clough-Penzien PSD
72 model [23]. This is carried out by a data-driven bootstrapping approach for the quantifi-
73 cation of uncertainties. The key aspect of this approach is the introduction of a scaling
74 parameter that allows the setting of bounds based on expert knowledge and statistical prop-
75 erties of the data set. This allows for the selection of more conservative or less conservative
76 bounds, providing some flexibility in the modelling of the bounds. To illustrate the practi-
77 cality of this method, consider the following scenario: Data have been collected from only
78 one monitoring station in an area where the construction of new buildings is planned. By
79 using the existing data from the measuring station, it is possible to define intervals for the
80 physical parameters. Consequently, best-case and worst-case scenarios can be created for
81 this location, enabling informed decision-making and better planning and including site-
82 specific information, such as the soil properties. Further, by fitting physical based models
83 to the data, uncertainties due to PSD estimators can be reduced.

84 This work is organised as follows: In Section 2 some preliminaries necessary for this
85 work will be introduced. The proposed procedure for developing a load model accounting
86 for uncertainties is illustrated in Section 3 for the stationary case and for the non-stationary
87 case, where both, the separable and non-separable EPSD will be utilised. Real data records
88 are utilised in Section 4 to derive the bounds and to show the methods feasibility and
89 flexibility for real world cases. The work concludes in Section 5 with some final remarks.

90 2. Preliminaries

91 In this section, a brief overview of the fundamental concepts essential for the context of
92 this work is provided.

93 2.1. Stochastic processes

94 The Wiener-Khintchine theorem (e.g. [3, 11, 7]) is an important relation in the field of
95 stochastic processes. It establishes a fundamental link between the power spectral density
96 (PSD) function $S_X(\omega)$ of a signal and its autocorrelation function $R_X(\tau)$ with τ as time lag.
97 The theorem states that the Fourier transform of the autocorrelation function of a stochastic
98 process is equal to the PSD function of that signal

$$S_X(\omega) = \frac{1}{2\pi} \int_{-\infty}^{\infty} R_X(\tau) e^{-i\omega\tau} d\tau, \quad (1)$$

99 while the inverse Fourier transform yields the vice versa result

$$R_X(\tau) = \int_{-\infty}^{\infty} S_X(\omega) e^{i\omega\tau} d\omega. \quad (2)$$

100 The theorem is particularly useful when dealing with random or stochastic signals where
101 conventional time-domain analysis does not provide sufficient insight. It allows to analyse the
102 frequency content of signals and to understand how their power is distributed over different
103 frequencies. By transforming the signal into the frequency domain, dominant frequency
104 components can be identified and the spectral properties of the signal can be investigated.
105 While the Wiener-Khintchine theorem establishes a theoretical relationship between the PSD
106 and autocorrelation function, PSD estimators play a crucial role in practical applications.

107 The theorem assumes that the signal is wide-sense stationary and has an infinite length
 108 in time, which is not fulfilled in real world applications. Further, the theorem holds for
 109 stationary processes only. Earthquakes, for instance, have a strongly transient character, so
 110 that other techniques have to be resorted to.

111 2.1.1. PSD and EPSPD estimation

112 In this section, PSD estimation for both stationary and non-stationary PSDs, often
 113 referred to as EPSPDs, is briefly described. The stationary PSD estimation can be computed
 114 using the periodogram, for instance, which is based on the discrete Fourier transform [8].
 115 The periodogram is given to be

$$\hat{S}_X(\omega_k) = \frac{1}{N_t} \left| \sum_{t=0}^{N_t-1} x_t e^{-\frac{i2\pi}{N_t} kt} \right|^2, \quad (3)$$

116 where \hat{S}_X denotes the PSD estimate, N_t is the number of points in time, x_t is the value of the
 117 t -th time instant and k is the integer frequency for $\omega_k = \frac{2\pi k}{T}$, where T is the total length of
 118 the time record. Other methods to estimate the stationary PSD are, for instance, Bartlett's
 119 method [24, 25] or Welch's method [26]. Since these methods work by segmenting and
 120 averaging the time signal, they usually provide smoother estimates than the periodogram.

121 As stochastic processes often have an inherent non-stationary character (e.g. earthquakes
 122 have a short term transient behaviour), the estimation of the EPSPD will result in a more
 123 reliable and more realistic representation. The EPSPD is a transformation from time domain
 124 to time-frequency domain and accounts for temporal changes in the frequency content of
 125 the process. Various methods for estimating the EPSPD are available, including but not
 126 limited to the short-time Fourier transform, the Priestley method [9], and Wavelet-based
 127 methods [27, 28]. However, in this work, the recently developed multi-taper S-transform
 128 (MTST) [29, 30] will be utilised as it yields results in a good resolution and is able to reduce
 129 the estimation variance. The MTST estimation is given to be

$$\hat{S}_X(\omega, t) = \frac{1}{M} \sum_{m=0}^{M-1} s_m^*(\omega, t) s_m^T(\omega, t), \quad (4)$$

130 where the S-transform $s_m(\omega, t)$ and its complex conjugate $s_m(\omega, t)^*$ of a non-stationary
 131 stochastic process $U(t)$ is

$$s_m(\omega, t) = \sum_{k=-\infty}^{\infty} \Psi_m(\omega, k\Delta t - t)U(k\Delta t)e^{-i2\pi\omega k\Delta t}\Delta t. \quad (5)$$

132 In this equation, the orthogonal time-frequency Hermite windows $\Psi_0(\omega, t)$ for the zeroth-
 133 order is

$$\Psi_0(\omega, t) = \pi^{-0.25}\sqrt{w(\omega)}e^{-0.5w^2(\omega)t^2}, \quad (6)$$

134 while $\Psi_1(\omega, t)$ for the first-order yields

$$\Psi_1(\omega, t) = \sqrt{2}\pi^{-0.25}w^{1.5}(\omega)te^{-0.5w^2(\omega)t^2}, \quad (7)$$

135 and any higher order $\Psi_m(\omega, t)$ for $m > 1$ is

$$\Psi_m(\omega, t) = \sqrt{\frac{2}{m}}w(\omega)t\Psi_{m-1}(\omega, t) - \sqrt{\frac{m-1}{m}}\Psi_{m-2}(\omega, t). \quad (8)$$

136 2.1.2. Stochastic process generation

137 For the generation of stochastic processes used in simulations, the spectral representation
 138 method (SRM) [31] can be utilised. The method requires an analytical or estimated expres-
 139 sion of a PSD function $S(\omega)$ and yields a stochastic process X_t in time domain, carrying the
 140 spectral characteristics of the underlying PSD function. SRM reads as follows

$$X_t = \sqrt{2} \sum_{n=0}^{N_\omega-1} (2S(\omega_n)\Delta\omega)^{1/2} \cos(\omega_n t + \varphi_n), \quad (9)$$

141 where $n = 0, 1, \dots, N_\omega - 1$, N_ω as the number of frequency components, $\Delta\omega$ as frequency
 142 discretisation, $\omega_n = n\Delta\omega$ as frequency coordinates, the φ_n 's describe independent random
 143 phase angles in the range $[0, 2\pi]$ and t is the time vector.

144 Equivalently, non-stationary stochastic processes can be generated based on an underly-
 145 ing EPSD function $S(\omega, t)$ by an extension of SRM to its non-stationary case [32]. In this
 146 case, the stationary PSD function $S(\omega_n)$ is replaced by its non-stationary equivalent $S(\omega, t)$

$$X_t = \sqrt{2} \sum_{n=0}^{N_\omega-1} (2S(\omega_n, t)\Delta\omega)^{1/2} \cos(\omega_n t + \varphi_n). \quad (10)$$

147 2.2. *Bootstrap sampling*

148 Bootstrap sampling is a resampling technique widely employed in statistics and machine
149 learning to address the challenge of estimating the sampling distribution of a statistic or
150 making inferences about a population based on a single sample, see for instance [33]. It
151 has since become a fundamental tool in data analysis. The basic idea behind bootstrap
152 sampling involves generating numerous “pseudo-samples” from the original samples by ran-
153 domly selecting data points from it with replacement. Each pseudo-sample may contain
154 duplicate observations and omit others, effectively mimicking the randomness of drawing
155 samples from the population. By calculating the statistic of interest (e.g., mean, median,
156 confidence interval) for each of these pseudo-samples and examining the distribution of these
157 bootstrap statistics, analysts can make robust inferences about the population or assess the
158 variability of their estimates. Bootstrap sampling is particularly advantageous because it
159 does not rely heavily on assumptions about the population’s distribution and can be applied
160 to various statistical problems, offering a versatile tool for data analysis.

161 3. Method development

162 To enhance the statistical robustness of the limited PSD functions, a bootstrapping ap-
163 proach applied to individual frequencies was employed. This method involved generating
164 pseudo-samples, often referred to as bootstrap samples, through random sampling with re-
165 placement. These pseudo-samples simulate multiple instances of the original data, allowing
166 for a more comprehensive assessment of the variability in spectral estimates. By applying
167 bootstrapping independently to each frequency component in the PSD functions, more reli-
168 able estimates of statistical quantities, such as mean and standard deviation, for instance,
169 can be obtained. This resampling technique offers a powerful means of assessing the vari-
170 ability of spectral estimates, particularly in regions where the only limited data is available.
171 The resulting bootstrapped statistics, based on these pseudo-samples, not only provide a
172 comprehensive understanding of the central tendencies and uncertainties associated with
173 each frequency but also enable the computation of more reliable maximum and minimum

174 spectra. This method effectively mitigates problems associated with limited data sets, which
 175 contributes to the overall robustness of the spectral analysis, enhancing the credibility of
 176 the findings.

177 The bootstrap sampled minimum spectrum S_{\min}^{BS} and maximum spectrum S_{\max}^{BS} are

$$S_{\min}^{BS}(\omega_n) = \min(S_i^{BS}(\omega_n)) \forall i \in N_{BS} \quad (11)$$

178 and

$$S_{\max}^{BS}(\omega_n) = \max(S_i^{BS}(\omega_n)) \forall i \in N_{BS}, \quad (12)$$

179 with N_{BS} as number of bootstrap samples. Similarly, the standard deviation of the bootstrap
 180 samples will be determined from all bootstrap samples

$$\sigma_{\min}^{BS}(\omega_n) = \sqrt{\frac{1}{N_{BS} - 1} \sum_{i=1}^{N_{BS}} (S_i^{BS}(\omega_n) - S_{\min}^{BS}(\omega_n))^2} \quad (13)$$

181 and

$$\sigma_{\max}^{BS}(\omega_n) = \sqrt{\frac{1}{N_{BS} - 1} \sum_{i=1}^{N_{BS}} (S_i^{BS}(\omega_n) - S_{\max}^{BS}(\omega_n))^2}. \quad (14)$$

182 By introducing a scaling factor λ , the *augmented* bounds result in

$$\underline{S}^{aug}(\omega_n) = S_{\min}^{BS}(\omega_n) - \lambda \sigma_{\min}^{BS}(\omega_n) \quad (15)$$

183 and

$$\overline{S}^{aug}(\omega_n) = S_{\max}^{BS}(\omega_n) + \lambda \sigma_{\max}^{BS}(\omega_n). \quad (16)$$

184 The equations presented here demonstrate the procedure for PSD functions. When using
 185 EPSD functions, the same approach can be used, whereby the respective functions are ex-
 186 tended by the time parameter. The scaling factor $\lambda \in \mathbb{R}$ has to be determined by the analyst
 187 and shall be selected properly, in the optimal scenario with the integration of expert knowl-
 188 edge. Some suggestions on how to choose λ are given in Section 3.1. Handling the bounds
 189 in such a way offers several advantages: flexibility, case-dependent adjustment, iterative ap-
 190 proach. If the scaling factor λ is chosen too large, negative values in the augmented bounds

191 can occur. Since spectral densities are non-negative by nature, those can simply be set to
 192 zero.

193 Separate upper and lower bound optimisations are performed to fit a PSD model S^{model}
 194 and its corresponding set of parameters $\boldsymbol{\theta}$ to the augmented bounds determined by boot-
 195 strapping. The objective function for the optimisation is specified by the least squares
 196 solution between the augmented bounds and the chosen model. The optimisation for the
 197 lower bounds in the stationary case reads

$$f(\underline{\boldsymbol{\theta}}) = \min_{\underline{\boldsymbol{\theta}}} \sum_{n=1}^{N_\omega} (\underline{S}^{aug}(\omega_n) - S^{model}(\omega_n, \underline{\boldsymbol{\theta}}))^2, \quad (17)$$

198 while the upper bound can be optimised via

$$f(\overline{\boldsymbol{\theta}}) = \min_{\overline{\boldsymbol{\theta}}} \sum_{n=1}^{N_\omega} (\overline{S}^{aug}(\omega_n) - S^{model}(\omega_n, \overline{\boldsymbol{\theta}}))^2. \quad (18)$$

199 In case a more realistic EPSDs is utilised, the optimisation for the lower bound yields

$$f(\underline{\boldsymbol{\theta}}) = \min_{\underline{\boldsymbol{\theta}}} \sum_{n=1}^{N_\omega} \sum_{m=1}^{N_t} (\underline{S}^{aug}(\omega_n, t_m) - S^{model}(\omega_n, t_m, \underline{\boldsymbol{\theta}}))^2, \quad (19)$$

200 whereas the upper bound can be optimised by

$$f(\overline{\boldsymbol{\theta}}) = \min_{\overline{\boldsymbol{\theta}}} \sum_{n=1}^{N_\omega} \sum_{m=1}^{N_t} (\overline{S}^{aug}(\omega_n, t_m) - S^{model}(\omega_n, t_m, \overline{\boldsymbol{\theta}}))^2. \quad (20)$$

201 In these equations $\underline{\boldsymbol{\theta}}$ and $\overline{\boldsymbol{\theta}}$ represents the particular set of parameters needed for the specific
 202 model. Once the model and the corresponding parameters are fitted to the augmented
 203 bounds, interval parameters result which can be used to sample individual PSD functions
 204 in subsequent simulations. Thus, the best-case or worst-case scenario can be determined
 205 within the framework of a reliability analysis.

206 3.1. Selection of the scaling parameter λ

207 The scaling parameter plays a pivotal role in enhancing the adaptability of models for
 208 bounding purposes. However, it is crucial to exercise caution when selecting its value, as ar-
 209 bitrary choices may lead to undesirable consequences. An excessively high scaling parameter

210 can result in unreasonably large bounds, thereby increasing the failure probability beyond
211 acceptable limits, which contradicts the intended outcome. Conversely, an inadequately
212 small parameter fails to adequately quantify or incorporate uncertainties into the model. To
213 address this challenge, this study explores a potential solution to establish an appropriate
214 scaling parameter by examining the characteristics of generated stochastic processes. This
215 approach aims to provide deeper insights into the scaling parameter’s properties prior to
216 conducting simulations.

217 To address the challenge of determining a suitable scaling parameter, the study pro-
218 poses an approach that involves a comprehensive examination of the stochastic processes
219 generated within the model. Through a comprehensive examination of these processes, a
220 deeper understanding of the scaling parameter’s behaviour and characteristics is sought.
221 This understanding is crucial in ensuring that the chosen scaling parameter aligns with the
222 desired level of uncertainty representation. Furthermore, the possibility of comparing the
223 scaling parameter with established seismic metrics like peak ground acceleration (PGA) is
224 investigated. This comparison allows to leverage existing knowledge of the statistical prop-
225 erties of the stochastic processes from which the model is derived and to assess the scaling
226 parameter’s appropriateness in the context of specific ground motions occurring within the
227 study area. Such an integrative approach enhances the ability to make informed decisions
228 regarding the scaling parameter’s value, ultimately leading to more robust and accurate
229 simulations.

230 *3.2. Artificial examples*

231 The procedure is illustrated covering different cases with artificially generated data, in
232 particular for a stationary PSD model, a non-separable EPSD model and a separable EPSD
233 model. Each of the three limited data sets was generated using an analytical PSD/EPSD
234 model to reflect the underlying physics. From this, artificial stochastic processes were gener-
235 ated using SRM (Eq. 9 or Eq. 10). These were considered as “recorded data”, at least for the
236 artificial examples, and transformed into the frequency domain (Eq. 3) or time-frequency
237 domain (Eq. 4) via the corresponding estimators. Based on these resulting ensemble of

238 PSD/EPD functions, the previously described approach will be illustrated. Further, these
 239 examples serve for comparison and validation if the feasible parameters were found. In all
 240 cases, a number of 10,000 bootstrap samples were generated based on the limited data set
 241 to obtain reliable statistics.

242 3.2.1. Stationary power spectral density function

243 In the stationary case two typical models used are the Kanai-Tajimi PSD model [21, 22]
 244 and the Clough-Penzien PSD model [23]. The Kanai-Tajimi PSD model reads as

$$S^{KT}(\omega, \boldsymbol{\theta}^{KT}) = S_0 \cdot \frac{\omega_g^4 + 4\zeta_g^2 \omega_g^2 \omega^2}{(\omega_g^2 - \omega^2)^2 + 4\zeta_g^2 \omega_g^2 \omega^2}, \quad (21)$$

245 with $\boldsymbol{\theta}^{KT} = [S_0, \omega_g, \zeta_g]$. The Kanai-Tajimi PSD model passes a white noise process through
 246 a linear soil filter determined by the natural frequency ω_g and damping ζ_g , respectively,
 247 while S_0 determines the spectral intensity, see for instance [34]. A drawback of the Kanai-
 248 Tajimi PSD model is that velocity and displacement are not defined for frequencies which
 249 tend to zero, i.e. $\omega \rightarrow 0$. To overcome this issue, the Clough-Penzien model was defined by
 250 expressing the Kanai-Tajimi PSD function with an additional filter determined by frequency
 251 ω_f and damping ζ_f

$$S^{CP}(\omega, \boldsymbol{\theta}^{CP}) = S_0 \cdot \frac{\omega^4}{(\omega_f^2 - \omega^2)^2 + 4\zeta_f^2 \omega_f^2 \omega^2} \cdot \frac{\omega_g^4 + 4\zeta_g^2 \omega_g^2 \omega^2}{(\omega_g^2 - \omega^2)^2 + 4\zeta_g^2 \omega_g^2 \omega^2}, \quad (22)$$

252 with $\boldsymbol{\theta}^{CP} = [S_0, \omega_g, \zeta_g, \omega_f, \zeta_f]$, see [23, 34] for instance.

253 In this example, the Clough-Penzien PSD model will be utilised due to its realistic
 254 behaviour. Three stochastic processes are generated based on the Clough-Penzien PSD
 255 model utilising the parameters $S_0 = 1$, $\omega_f = 0.5\pi$, $\zeta_f = 0.6$, $\omega_g = 5\pi$ and $\zeta_g = 0.6$, which are
 256 adopted from [35], while the upper cut-off frequency is set to $\omega_u = 80$ rad/s. The resulting
 257 ensemble of PSDs is depicted in Fig. 1.

258 The augmented bounds are derived using Eqs. 15 and 16 with scaling parameter $\lambda = 1.5$.
 259 The specific optimisation problems to be solved for lower and upper bound are

$$f(\underline{\boldsymbol{\theta}}^{CP}) = \min_{\underline{\boldsymbol{\theta}}^{CP}} \sum_{n=1}^{N_\omega} (\underline{S}^{aug}(\omega_n) - S^{CP}(\omega_n, \underline{\boldsymbol{\theta}}^{CP}))^2 \quad (23)$$

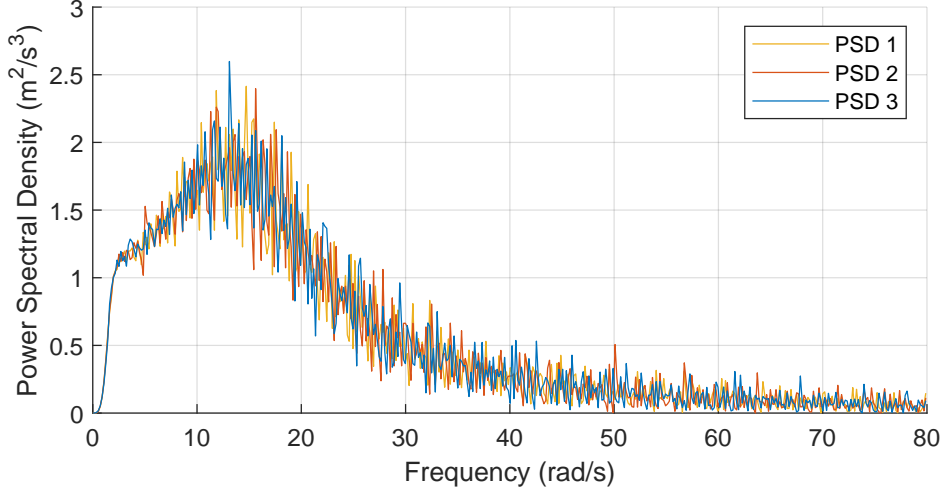


Figure 1: Ensemble of the Clough-Penzien PSDs.

Table 1: Identified parameters for the Clough-Penzien PSD model.

	S_0	ω_f	ζ_f	ω_g	ζ_g
$S^{CP}(\omega, \underline{\theta}^{CP})$	0.7517	1.7680	0.4809	13.9162	0.5666
$S^{CP}(\omega, \bar{\theta}^{CP})$	1.2407	1.3413	0.7552	16.7373	0.6270

260 and

$$f(\bar{\theta}^{CP}) = \min_{\bar{\theta}^{CP}} \sum_{n=1}^{N_\omega} \left(\bar{S}^{aug}(\omega_n) - S^{CP}(\omega_n, \bar{\theta}^{CP}) \right)^2. \quad (24)$$

261 An example of this procedure is depicted in Fig. 2, while the fitted parameters are given in
 262 Table 1. The corresponding objective function values are $f(\underline{\theta}^{CP}) = 7.6833$ and $f(\bar{\theta}^{CP}) =$
 263 9.4891. The relatively high values can be explained by the highly variant PSD functions
 264 in Fig. 2. The resulting bounds deliver very smooth results, while the derived augmented
 265 bounds are relatively variant. The general shape is captured well by the optimised bounds.

266

267 3.2.2. Non-separable evolutionary power spectral density function

268 An example for a non-separable EPSD function is given in [36], for instance, which is
 269 used in a generalised form in this work

$$S^{non-sep}(\omega, t, \theta^{non-sep}) = S_0 \left(\frac{\omega}{\omega_g} \right)^2 e^{ct} t^2 \exp \left(- \left(\frac{\omega}{\omega_g} \right)^2 t \right). \quad (25)$$

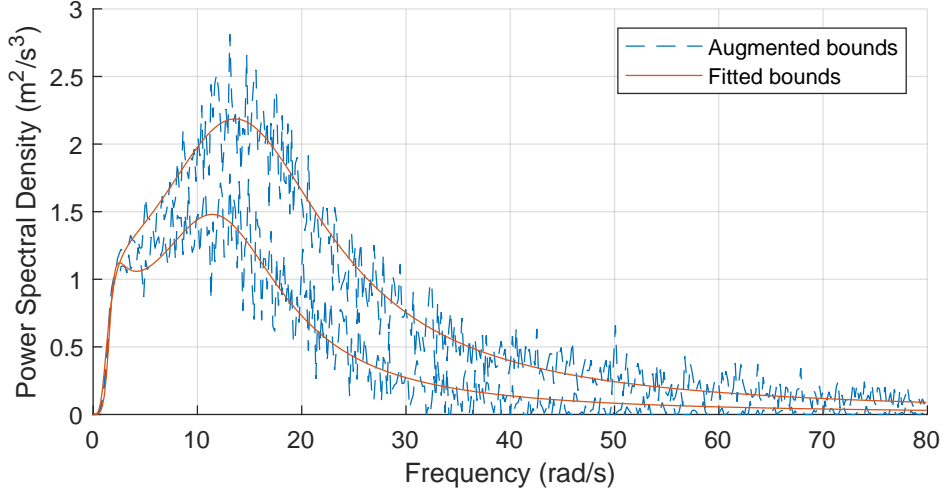


Figure 2: Example of the Clough-Penzien model fitted to the augmented bounds with scaling parameter $\lambda = 1.5$.

270 This model can be described by the parameters $\boldsymbol{\theta}^{non-sep} = [S_0, c, \omega_g]$. For generating the
 271 ensemble of EPSDs, the parameters $S_0 = 1$, $c = -0.15$ and $\omega_g = 5\pi$ are utilised.

272 The specific optimisation problems to be solved for lower and upper bound with a scaling
 273 parameter of $\lambda = 2$ are

$$f(\underline{\boldsymbol{\theta}}^{non-sep}) = \min_{\underline{\boldsymbol{\theta}}^{non-sep}} \sum_{n=1}^{N_\omega} \sum_{m=1}^{N_t} (\underline{S}^{aug}(\omega_n, t_m) - S^{non-sep}(\omega_n, t_m, \underline{\boldsymbol{\theta}}^{non-sep}))^2 \quad (26)$$

274 and

$$f(\overline{\boldsymbol{\theta}}^{non-sep}) = \min_{\overline{\boldsymbol{\theta}}^{non-sep}} \sum_{n=1}^{N_\omega} \sum_{m=1}^{N_t} (\overline{S}^{aug}(\omega_n, t_m) - S^{non-sep}(\omega_n, t_m, \overline{\boldsymbol{\theta}}^{non-sep}))^2. \quad (27)$$

275 An example of this procedure is depicted in Fig. 3, while the corresponding optimised
 276 parameters are given in Table 2. Although it may appear that the optimised bounds closely
 277 resemble the augmented bounds, this is challenged by the notably high objective function
 278 values of $f(\underline{\boldsymbol{\theta}}^{non-sep}) = 200.8499$ and $f(\overline{\boldsymbol{\theta}}^{non-sep}) = 4406.5$. Despite these values, these
 279 bounds can still be considered for further analysis. The optimised bounds rely on the shape
 280 of the estimated EPSDs, which can exhibit a strong non-smooth behaviour, resulting in high
 281 objective values. However, the objective is to obtain approximate EPSD bounds that can
 282 be effectively utilised in simulations, thus those bounds are reasonable.

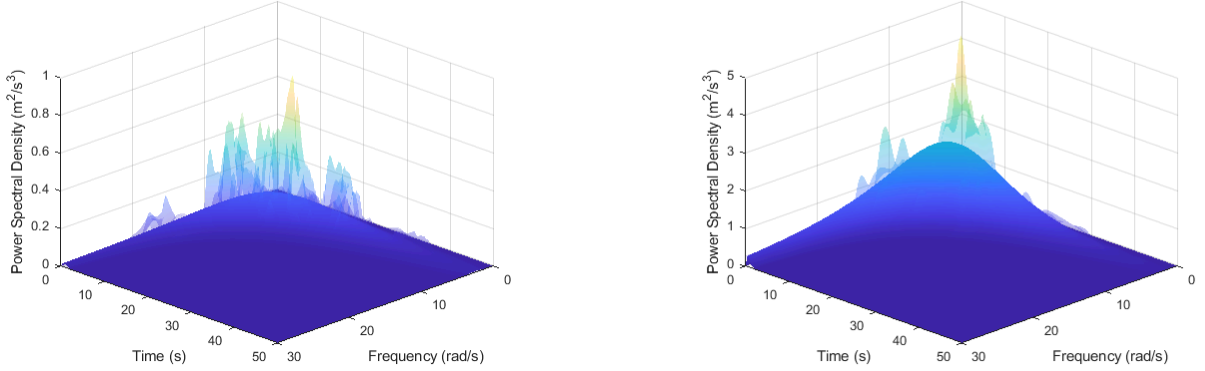


Figure 3: Comparison of augmented bounds and derived lower bound (left) and upper bound (right) for the non-separable EPSD model. The transparent representation shows the augmented bounds, the non-transparent ones are the fitted EPSDs. For both a scaling parameter of $\lambda = 2$ was utilised.

Table 2: Identified parameters for the non-separable EPSD model.

	S_0	c	ω_g
$S^{non-sep}(\omega, t, \underline{\theta}^{non-sep})$	0.1086	-0.1106	18.1903
$S^{non-sep}(\omega, t, \overline{\theta}^{non-sep})$	2.1590	-0.1508	15.6480

283 3.2.3. Separable evolutionary power spectral density function

284 A separable EPSD consists of a stationary PSD model, such as the Clough-Penzien
 285 model, and a time-modulating function, which will be multiplied with each other. The
 286 resulting separable EPSD function yields

$$S^{sep}(\omega, t) = S^{stationary}(\omega)g(t)^2. \quad (28)$$

287 The separable EPSD may offer more flexibility as the number of parameters in this specific
 288 case is higher than in the previous example. Further, this model can be adapted to different
 289 data sets or scenarios by replacing either the stationary PSD model $S^{stationary}$ or the time-
 290 modulating function $g(t)$. In the following example, the Clough-Penzien PSD described
 291 above (Section 3.2.1) will be utilised in combination with the time-modulating function

$$g_1(t) = k(e^{-at} - e^{-bt}), \quad (29)$$

292 with k as the scaling factor and a and b as shape parameters. The parameters utilised here
 293 are $k = 4$, $a = 0.25$ and $b = 0.5$. For reference, other time-modulating functions can be
 294 found Appendix A.

295 The resulting separable EPSP for this example yields

$$S^{sep}(\omega, t, \boldsymbol{\theta}^{sep}) = S^{CP}(\omega, \boldsymbol{\theta}^{CP}) g_1(t, \boldsymbol{\theta}^t)^2, \quad (30)$$

296 with $\boldsymbol{\theta}^{CP} = [S_0, \omega_g, \zeta_g, \omega_f, \zeta_f]$, $\boldsymbol{\theta}^t = [k, a, b]$ and thus $\boldsymbol{\theta}^{sep} = [\boldsymbol{\theta}^{CP}, \boldsymbol{\theta}^t]$. The derivation of the
 297 bounds is carried out with a scaling factor of $\lambda = 2$. The optimisation problems are thus

$$f(\underline{\boldsymbol{\theta}}^{sep}) = \min_{\underline{\boldsymbol{\theta}}^{sep}} \sum_{n=1}^{N_\omega} \sum_{m=1}^{N_t} (\underline{S}^{aug}(\omega_n, t_m) - S^{sep}(\omega_n, t_m, \underline{\boldsymbol{\theta}}^{sep}))^2 \quad (31)$$

298 and

$$f(\overline{\boldsymbol{\theta}}^{sep}) = \min_{\overline{\boldsymbol{\theta}}^{sep}} \sum_{n=1}^{N_\omega} \sum_{m=1}^{N_t} (\overline{S}^{aug}(\omega_n, t_m) - S^{sep}(\omega_n, t_m, \overline{\boldsymbol{\theta}}^{sep}))^2. \quad (32)$$

299 The resulting bounds are depicted in Fig. 4, while the corresponding parameters are given
 in Table 3. The objective function values are $f(\underline{\boldsymbol{\theta}}^{sep}) = 491.5593$ and $f(\overline{\boldsymbol{\theta}}^{sep}) = 7329.4$.

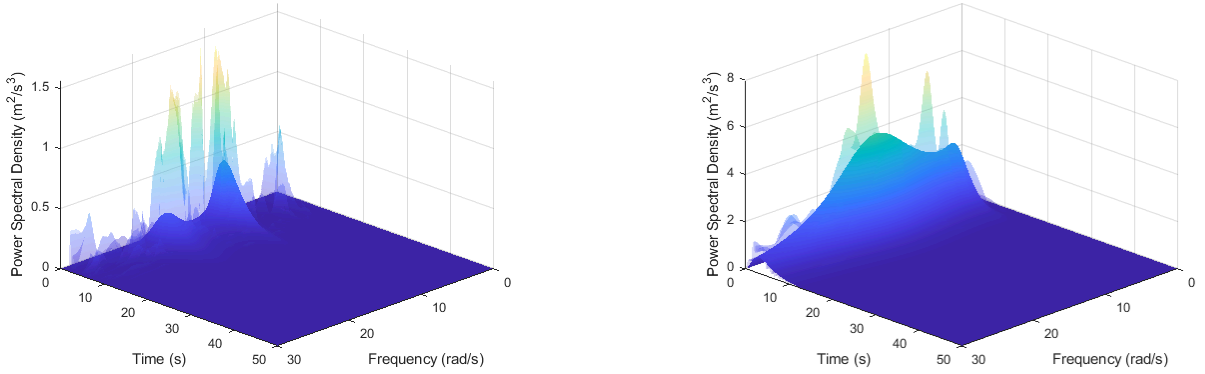


Figure 4: Comparison of augmented bounds and derived lower bound (left) and upper bound (right) for the separable EPSP model. The transparent representation shows the augmented bounds, the non-transparent ones are the fitted EPSPs. For both a scaling parameter of $\lambda = 2$ was utilised.

300 Here again, the derived bounds seem not to match well with the augmented bounds and
 301 again quite high objective values can be obtained. However, as before it can be argued that
 302 those bounds rely on the EPSP estimates, which are hardly ever smooth. Thus, although
 303 obtaining high objective values, the derived bounds can be used for further analysis.
 304

Table 3: Identified parameters for the separable EPSD model.

	S_0	ω_f	ζ_f	ω_g	ζ_g	k	a	b
$S^{sep}(\omega, t, \underline{\theta}^{sep})$	6.3859	9.5180	0.0702	17.7419	0.1057	10.8965	0.2593	0.2574
$S^{sep}(\omega, t, \bar{\theta}^{sep})$	7.7352	2.1889	0.4689	15.7403	0.4450	33.0126	0.3176	0.3299

3.3. Discussion on derived bounds

It is important to note that the parameters identified for the upper bound may not necessarily represent the uppermost values within their respective intervals. This observation is particularly pertinent in the context of specific models, such as the Clough-Penzien PSD model. In certain scenarios, increasing these parameters may unexpectedly lead to a reduction in the size of the PSD function itself. This counterintuitive behaviour can be attributed to the complex mathematical relationships inherent to the model, where higher parameter values may result in a more restricted or focused PSD function, rather than an expansion of its bounds.

An issue that arose during this investigation involved the generation of samples within predefined parameter bounds, some of which occasionally extended beyond these bounds, refer to Fig. 5. While this may initially seem counterintuitive, it's crucial to emphasise that the primary objective is to establish bounds for the underlying physical parameters, rather than strictly constraining the raw data itself. The focus lies in bounding the values associated with the physical characteristics of the system under examination.

In summary, the issue of samples occasionally exceeding parameter bounds aligns with the overarching goal of bounding the physical attributes of the system. Furthermore, it underscores the complexity of specific models, where adjusting parameter values may yield unexpected outcomes. Understanding and addressing these intricacies are essential for achieving accurate and meaningful results in the simulations.

In some cases the objective function values seem extremely high. In addition, the shapes of the augmented bounds compared to the ones derived through minimisation and optimising the parameters of the physical model often exhibits large differences due to the non-smoothness of the estimated PSD functions. Both issues can be explained very easily.

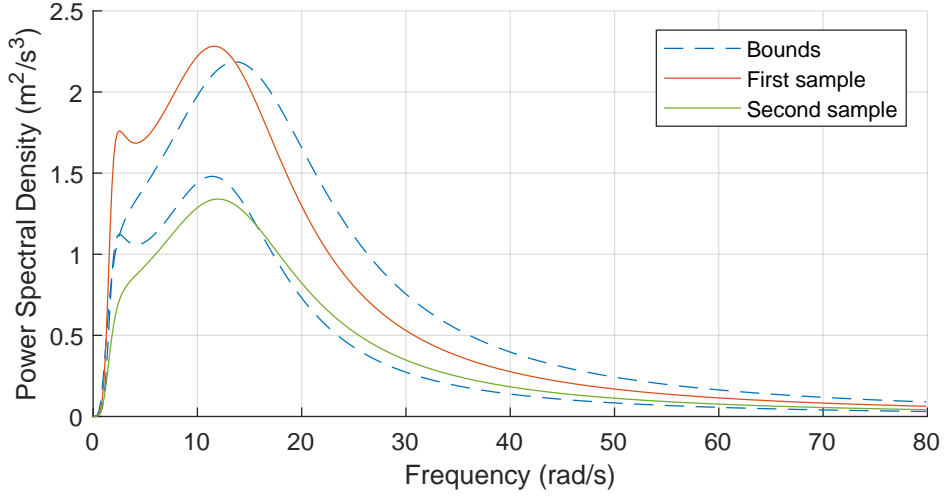


Figure 5: Example of generated samples which intersect the derived bounds.

329 The estimated PSDs and EPSDs have an immensely spiky behaviour, i.e. they often jump
 330 between high and low values between two frequency / time-frequency points. The fitted
 331 function, however, is smooth. By using the least squares as the objective function, this
 332 makes it impossible, nor desirable, to fit the function to the data perfectly. The function
 333 acts like a smoother of the data. Thus, it is logical that there are always high differences
 334 between the extreme value jumps. In the averaged sense, however, the fitted function adapts
 335 well. To overcome this issue, other PSD estimators may be used. For the stationary case
 336 Bartlett's method [24, 25] or Welch's method [26], as mentioned in Section 1, might be
 337 suitable, which usually result in a much smoother representation of the PSD and thus also
 338 most likely in a lower objective function.

339 However, the goal was to find, and specifically bound the respective parameters in order
 340 to capture the uncertainties induced by the limited data and the EPSD estimation process.
 341 For all cases, the PSD model and both EPSD models, bounded parameters can be derived.
 342 However, the parameters θ utilised for generating the underlying ensembles are not always
 343 bounded by the derived interval parameter sets θ^I , however, this is also not a significant
 344 issue as the interaction of various parameters can influence these and thus deviate signifi-
 345 cantly from the original parameters. The objective was to identify parameters capable of
 346 characterising both the upper and lower bound of the spectral densities, and this objective

347 has been successfully accomplished.

348 It's important to consider that in certain instances, it can be advantageous to pre-process
349 the data appropriately. Too many spectral densities close to 0 in a large range, especially
350 in the EPSD, can lead to undesired results and negatively influence the fitting. Large areas
351 with spectral densities close to 0 also push the value of the objective function down very
352 quickly, so that the optimisation algorithm quickly lies in a local minimum. Therefore, it is
353 advisable to reduce the data set to the range where high spectral densities are obtained, i.e.
354 the important range, and to cut off the parts where those densities are very close to zero (for
355 example $S(\omega, t) \leq 10^{-5}$). This has the advantage that only the relevant spectral densities
356 are considered in the fitting. Overall, this procedure has no disadvantages compared to
357 fitting the entire range, since the determined parameters will be entered into an analytical
358 function and the cut-off ranges can thus easily be included in the analytical function again.

359 **4. Application to real data records**

360 Within this section, the proposed method is put into practice using real data records to
361 demonstrate its applicability in real-world scenarios. The examples given in Section 3.2.1-
362 3.2.3 are merely illustrative of the proposed method, as artificially generated data are always
363 constructed in some way and therefore reflect reality only to a certain extent. For the sake of
364 brevity, only the resulting bounds and their corresponding parameters are presented for each
365 of the three types of PSD functions, i.e. the stationary PSD function, the non-stationary
366 non-separable EPSD function and the non-stationary separable EPSD function.

367 In this work, gradient-based optimisation algorithms are used to improve the efficiency
368 and convergence of optimisation tasks. These algorithms use gradient information to itera-
369 tively adjust parameters and thus facilitate the fast determination of optimal solutions. The
370 approach is particularly effective for smooth and continuous objective functions.

371 The data set used in this work is the well-known El Centro earthquake, see for in-
372 stance [37]. The data set consists of two records in time domain, i.e. the record in north-
373 south direction and the record east-west direction, which are transformed to the frequency

Table 4: Identified parameters for the Clough-Penzien PSD model fitted to the stationary El Centro data estimated with the periodogram.

		S_0	ω_f	ζ_f	ω_g	ζ_g
$\lambda = 0$	$S^{CP}(\omega, \underline{\theta}^{CP})$	0.0006	1.9286	0.5510	12.9481	0.6291
	$S^{CP}(\omega, \overline{\theta}^{CP})$	0.0016	1.0148	0.8452	12.6517	0.5864
$\lambda = 1$	$S^{CP}(\omega, \underline{\theta}^{CP})$	0.0004	2.0145	0.5514	11.5749	0.7840
	$S^{CP}(\omega, \overline{\theta}^{CP})$	0.0021	0.9164	0.8761	12.6874	0.5749
$\lambda = 2$	$S^{CP}(\omega, \underline{\theta}^{CP})$	0.0003	2.0461	0.5315	11.3969	0.7883
	$S^{CP}(\omega, \overline{\theta}^{CP})$	0.0027	0.8679	0.8912	12.7090	0.5681

domain by Eq. 3 for the stationary case and by Eq. 4 for the non-stationary case, respectively. The ensembles are depicted in Fig. 6.

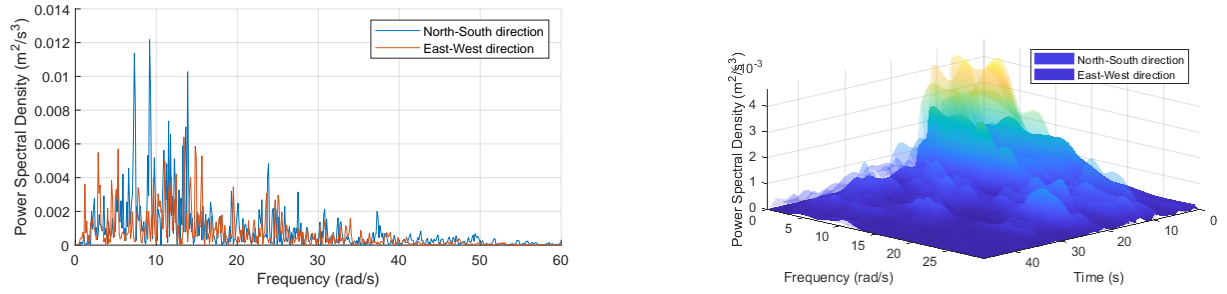


Figure 6: Ensemble of the PSDs and EPSDs of the El Centro earthquake.

The derivation of the bounds and their corresponding parameters for the estimated PSDs, i.e. for the stationary case, is described briefly in the following. The Clough-Penzien PSD model (Eq. 22) is utilised for fitting. The scaling parameter to obtain the augmented bounds is chosen to be $\lambda \in \{0, 1, 2\}$. The parameters derived by the proposed approach are given in Table 4, while the corresponding bounds are depicted in Fig. 7. The objective function values for the resulting bounds are given in Table 5.

For a more realistic representation, the non-separable EPSPD function in Eq. 25 is fitted to the augmented bounds of the El Centro EPSPD functions, again with scaling parameter $\lambda \in \{0, 1, 2\}$. The results for $\lambda = 0$ can be obtain in Fig. 8, while the identified bounded

Table 5: Objective function values for the resulting bounds of the stationary case.

	$S^{CP}(\omega, \underline{\theta}^{CP})$	$S^{CP}(\omega, \bar{\theta}^{CP})$
$\lambda = 0$	1.0593e-04	4.4814e-04
$\lambda = 1$	8.5038e-05	9.9150e-04
$\lambda = 2$	5.8963e-05	0.0018

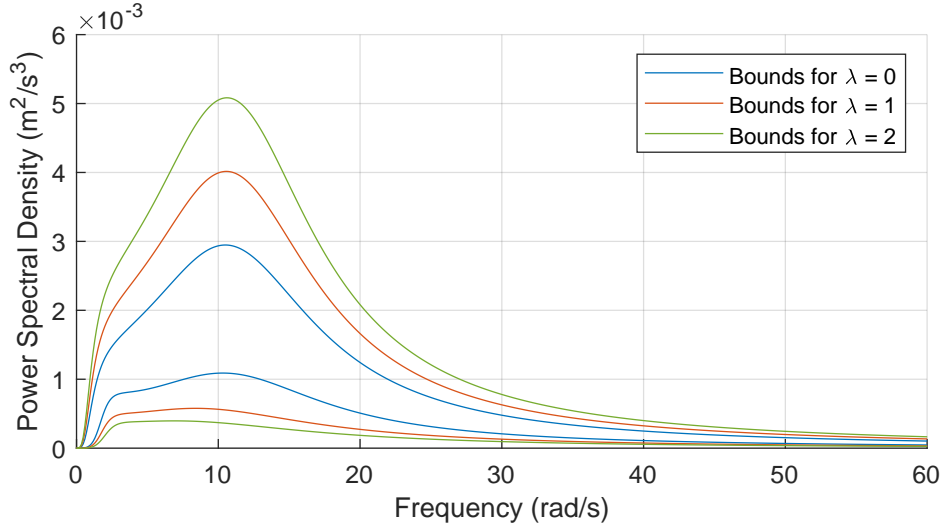


Figure 7: Comparison of the derived bounds for the El Centro data with the Clough-Penzien PSD model with $\lambda = \{0, 1, 2\}$.

Table 6: Identified parameters for the non-separable EPSD model fitted to the El Centro data.

		S_0	c	ω_g
$\lambda = 0$	$S^{non-sep}(\omega, t, \underline{\theta}^{non-sep})$	0.002	-0.1875	25.2118
	$S^{non-sep}(\omega, t, \overline{\theta}^{non-sep})$	0.0035	-0.2003	23.7434
$\lambda = 1$	$S^{non-sep}(\omega, t, \underline{\theta}^{non-sep})$	0.0012	-0.1826	26.6382
	$S^{non-sep}(\omega, t, \overline{\theta}^{non-sep})$	0.0044	-0.2007	23.4602
$\lambda = 2$	$S^{non-sep}(\omega, t, \underline{\theta}^{non-sep})$	0.0007	-0.1778	27.3245
	$S^{non-sep}(\omega, t, \overline{\theta}^{non-sep})$	0.0053	-0.201	23.2628

385 parameters are given in Table 6 and corresponding objective function values in Table 7.

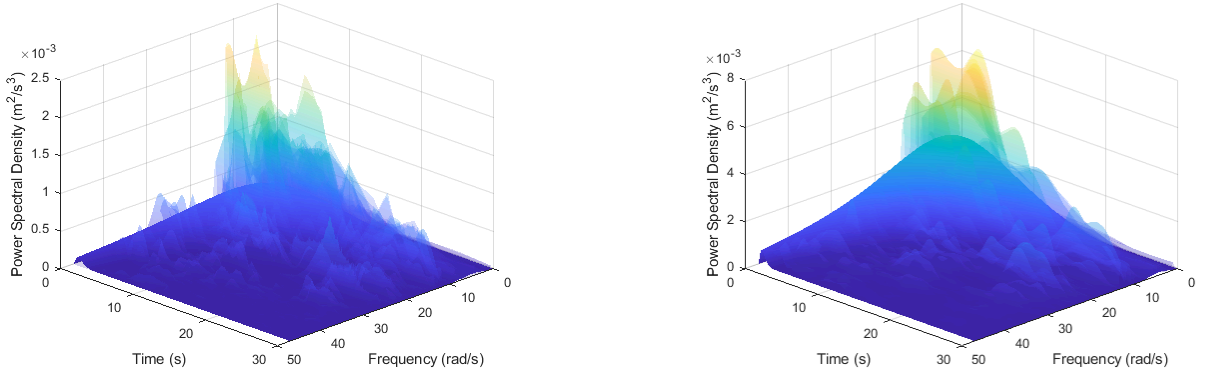


Figure 8: Comparison of augmented bounds and derived lower bound (left) and upper bound (right) for the non-separable EPSD model. The transparent representation shows the augmented bounds, the non-transparent ones are the fitted EPSDs. For both a scaling parameter of $\lambda = 0$ was utilised.

386 To also illustrate the flexibility of the separable EPSD, the fitting of the augmented
 387 EPSD bounds of the El Centro earthquake is illustrated for the same case, again with
 388 scaling parameter $\lambda \in \{0, 1, 2\}$. The respective bounds for $\lambda = 0$ are depicted in Fig. 9, the
 389 corresponding parameters are given in Table 8 and the objective function values are given
 390 in Table 9.

Table 7: Objective function values for the resulting bounds of the non-separable case.

	$S^{non-sep}(\omega, t, \underline{\boldsymbol{\theta}}^{non-sep})$	$S^{non-sep}(\omega, t, \overline{\boldsymbol{\theta}}^{non-sep})$
$\lambda = 0$	0.0536	0.1262
$\lambda = 1$	0.0354	0.2169
$\lambda = 2$	0.027	0.3388

Table 8: Identified parameters for the separable EPSD model fitted to the El Centro data.

		S_0	ω_f	ζ_f	ω_g	ζ_g	k	a	b
$\lambda = 0$	$S^{sep}(\omega, t, \underline{\boldsymbol{\theta}}^{sep})$	1.1687	1.4511	0.7412	12.5965	0.5936	3.5507	0.1907	0.1867
	$S^{sep}(\omega, t, \overline{\boldsymbol{\theta}}^{sep})$	1.0449	0.6871	1.7915	11.6559	0.6725	0.043	0.0403	1.4999
$\lambda = 1$	$S^{sep}(\omega, t, \underline{\boldsymbol{\theta}}^{sep})$	1.4939	1.8465	0.4303	13.8734	0.4555	5.969	0.1903	0.1889
	$S^{sep}(\omega, t, \overline{\boldsymbol{\theta}}^{sep})$	1.0072	0.8368	1.7974	10.9627	0.7089	0.0518	0.0403	1.5
$\lambda = 2$	$S^{sep}(\omega, t, \underline{\boldsymbol{\theta}}^{sep})$	1.0825	1.8953	0.304	13.5149	0.3557	3.1845	0.1921	0.1898
	$S^{sep}(\omega, t, \overline{\boldsymbol{\theta}}^{sep})$	1.0353	0.9821	1.7989	10.3706	0.7338	0.0588	0.0404	1.5

Table 9: Objective function values for the resulting bounds of the separable case.

	$S^{sep}(\omega, t, \underline{\boldsymbol{\theta}}^{sep})$	$S^{sep}(\omega, t, \overline{\boldsymbol{\theta}}^{sep})$
$\lambda = 0$	0.0467	0.0686
$\lambda = 1$	0.0313	0.1286
$\lambda = 2$	0.0245	0.2146

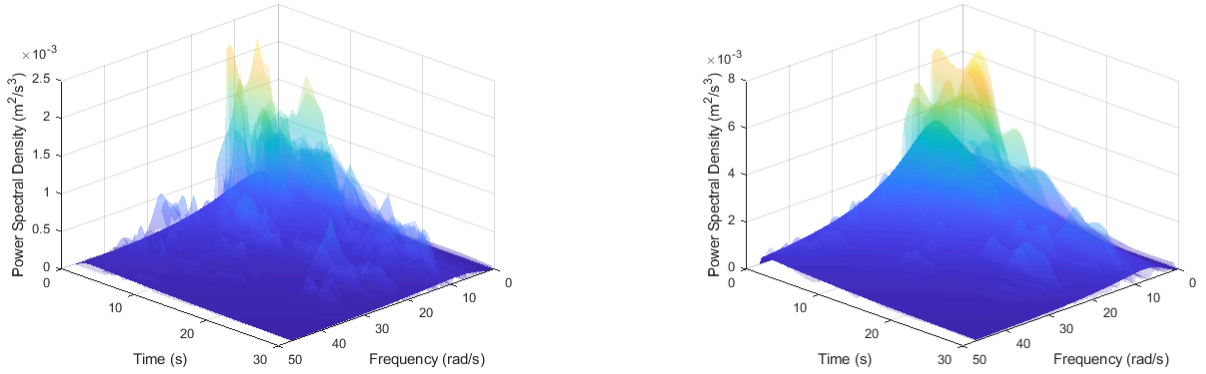


Figure 9: Comparison of augmented bounds and derived lower bound (left) and upper bound (right) for the separable EPSD model. The transparent representation shows the augmented bounds, the non-transparent ones are the fitted EPSDs. For both a scaling parameter of $\lambda = 0$ was utilised.

391 4.1. Comparison with imprecise power spectral density

392 In the pursuit of solving complex problems and achieving desired outcomes, it is often
 393 imperative to evaluate and compare different methods or approaches. This section aims into
 394 a comprehensive comparison of the proposed method with the imprecise PSD, proposed by
 395 some of the authors of this work. The imprecise PSD is an approach to bound a limited set
 396 of PSD functions in order to capture the uncertainties. The approach is described briefly
 397 in Appendix B, while the reader is referred to [20] for a detailed overview. The comparison
 398 of both methods will result in valuable insights into their respective efficiency, and suitability
 399 for specific scenarios. Through a critical analysis of their principles, implementation, and
 400 real-world performance, this examination seeks to assist decision-makers and analysts in
 401 making informed choices when choosing between these two approaches. The comparison is
 402 made for illustrative purposes and for the stationary case only, since the imprecise PSD is
 403 currently available for the stationary case only. As data set, the stationary PSDs determined
 404 from the El Centro earthquake will be utilised, see Fig. 6.

405 The proposed method is employed alongside the fitting of the Clough-Penzien PSD func-
 406 tion with scaling parameter $\lambda \in \{4, 5, 6\}$. This is compared directly to the imprecise PSD,
 407 where $N_B = 8$ basis functions are utilised to derive the bounds. As it can be seen from

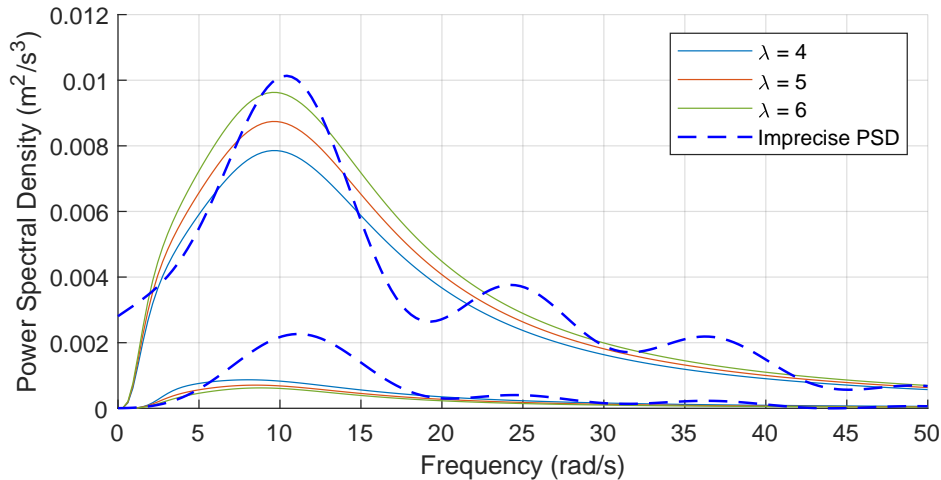


Figure 10: Comparison of the fitted Clough-Penzien spectrum with scaling parameter $\lambda \in \{4, 5, 6\}$ and the imprecise PSD with $N_B = 8$.

Table 10: Energy of the bounded PSDs derived by the Clough-Penzien PSD function and the imprecise PSD.

	Lower bound	Upper bound
$\lambda = 4$	0.0518	0.5049
$\lambda = 5$	0.0407	0.5610
$\lambda = 6$	0.0343	0.6171
Imprecise PSD	0.0879	0.5837

408 Fig. 10, both methods yield approximately similar results. One important difference in both
409 methods is, that the proposed method is a model fitting approach, while the imprecise PSD
410 is a data-driven bounding approach of a set of PSD functions. Thus, it is reasonable to
411 choose a larger λ for a meaningful comparison, than in the previous sections. The model
412 derived by the proposed approach is thus more conservative compared to Section 4. In addi-
413 tion, the proposed method delivers much smoother results, due to the fitting process, while
414 the imprecise PSD results in more oscillating bounds, given by the fact that it is a bounding
415 approach. However, qualitatively, similar bounds can be obtained, depending on the choice
416 of λ . This fact is supported by the energy of the bounded PSDs, see Table 10. The energy
417 is computed by summing up all individual PSD values for each frequency.

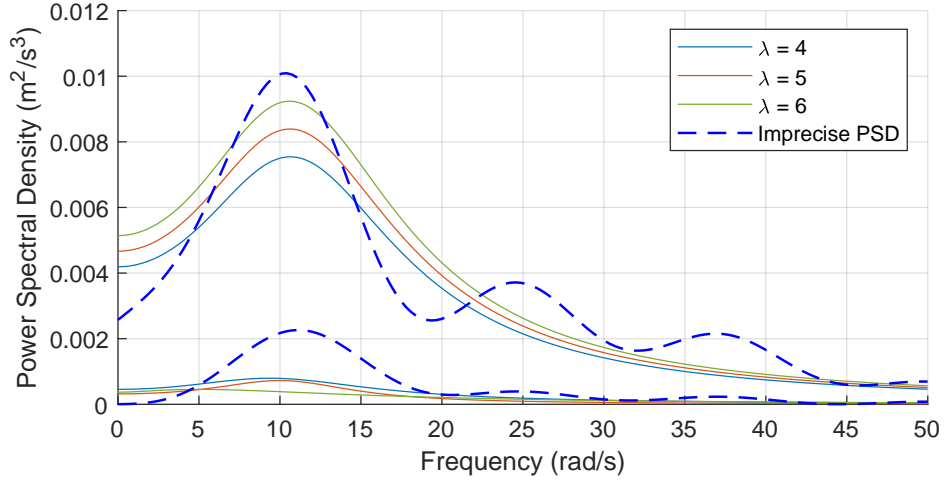


Figure 11: Comparison of the fitted Kanai-Tajimi spectrum with scaling parameter $\lambda \in \{4, 5, 6\}$ and the imprecise PSD with $N_B = 8$.

Table 11: Energy of the bounded PSDs derived by the Kanai-Tajimi PSD function and the imprecise PSD.

	Lower bound	Upper bound
$\lambda = 4$	0.0499	0.5013
$\lambda = 5$	0.0365	0.5572
$\lambda = 6$	0.0336	0.6131
Imprecise PSD	0.0879	0.5837

418 In a second comparison, the Kanai-Tajimi PSD function (Eq. 21) will be utilised to
419 derived the bounds of the El Centro PSD estimates with the proposed method. The bounds
420 are derived by using a scaling parameter of $\lambda \in \{4, 5, 6\}$. Again, the imprecise PSD bounds
421 with $N_B = 8$ are utilised for a comparison. As it can be obtained from Fig. 11, the bounds
422 of the Kanai-Tajimi PSD fit are very smooth, naturally for an analytical model. However,
423 small but neglectable differences can be obtained, mostly due to the oscillating nature of
424 the imprecise PSD. In general, a reasonably accurate approximation can be achieved, which
425 is supported by the determined energy in Table 11.

426 5. Conclusions

427 This study has introduced a robust methodology for the determination of interval pa-
428 rameters within physically derived stationary and evolutionary PSDs models. The resulting
429 bounded parameters offer a pivotal foundation for the assessment of upper and lower fail-
430 ure probabilities as an integral part of structural reliability evaluations. Importantly, this
431 approach is not limited to the PSD/EPD models utilised in this work. It can be used
432 with a wide range of models, making it flexible for different cases. Although this method
433 is fast and efficient at optimising parameter bounds, a significant challenge is choosing the
434 right model to match the data accurately. Since optimising the bounds is fast, it is worth
435 considering using multiple models and picking the best-fitting one. In this work, primarily
436 gradient-based optimisation algorithms have been utilised, which yielded in satisfactory re-
437 sults. However, it is essential to acknowledge that optimisation problems of this nature often
438 entail numerous local minima. Although no issues has been identified in this work, exploring
439 alternative classes of optimisation methods, such as particle swarm optimisation, may prove
440 advantageous, particularly when dealing with real-world data. Furthermore, the selection of
441 an appropriately scaling parameter is of paramount importance. An excessively large scaling
442 parameter can, depending on the specific characteristics of the system under investigation,
443 lead to a bounded failure probability of $p_f = [0, 1]$. While this outcome is theoretically cor-
444 rect, it lacks meaningful information and falls short of aligning with the intended objectives
445 of the proposed approach. Hence, the reasonable choice of the scaling parameter remains
446 a pivotal consideration in the methodology, which ensures the practicality and relevance
447 of the resulting failure probability assessments. An open issue is the efficient propagation
448 of derived bounds through a system under investigation. Classical double-loop approaches
449 may yield good results, however, for this class of problems advantageous solutions may be
450 required. Future developments will focus on such an efficient propagation method of the
451 bounds to obtain a bounded failure probability.

452 **CRedit author statement**

453 **Marco Behrendt:** Methodology, Formal analysis, Visualization, Validation, Software,
454 Writing - Original Draft. **Chao Dang:** Conceptualization, Methodology, Validation, Writ-
455 ing - Review & Editing. **Michael Beer:** Project administration, Supervision, Conceptual-
456 ization, Funding acquisition, Writing - Review & Editing.

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459 **Appendix A. Time-modulating functions**

460 There are several time-modulating functions available in the literature, which may fit
461 better to the problem at hand. See for instance [38, 39]. In contrast to the continuous
462 time-modulating function given in Eq. 29, these envelope functions are piecewise-defined:

$$g_2(t) = \begin{cases} \left(0.8 + 0.2\frac{t}{t_a}\right) & \text{for } t < t_a \\ 1 & \text{for } t_a \leq t \leq t_b \\ \left(\frac{t_b}{t}\right)^{\frac{2}{3}} & \text{for } t > t_b \end{cases} \quad (\text{A.1})$$

$$g_3(t) = \begin{cases} \left(\frac{t}{t_a}\right)^2 & \text{for } t < t_a \\ 1 & \text{for } t_a \leq t < t_b \\ \exp(-\alpha(t - t_b)) & \text{for } t \geq t_b \end{cases} \quad (\text{A.2})$$

463 **Appendix B. Imprecise power spectral density function**

464 The imprecise PSD function will be described in the following briefly. For a detailed
465 overview refer to [20].

466 A set of radial basis functions

$$\phi_i(x) = e^{-\left(\|x - c_i\| \cdot b_{\phi_i}\right)^2} \quad (\text{B.1})$$

467 constitute a radial basis function network

$$y(x) = \sum_{i=1}^{N_B} w_i \phi_i(\|x - c_i\| \cdot b_{\phi_i}) + b_0 \quad x \in \mathbb{R}^{N_\omega}. \quad (\text{B.2})$$

468 Such a network will be used to determine the bounded PSD model, the imprecise PSD.
 469 Therefore, the so-called basis power spectrum S_{basis} is computed, which can be, for instance
 470 the midpoint spectrum

$$S_{basis}(\omega_n) = \frac{1}{2} (S_{max}(\omega_n) + S_{min}(\omega_n)). \quad (\text{B.3})$$

471 With the resulting basis power spectrum a first approximation of the ensemble of PSD
 472 functions is derived, while the weights and bias can be obtained. To identify an upper and
 473 lower bound, the expression in Eq. B.2 will be reformulated

$$\begin{aligned} \underline{S}_{opt}(\omega_n; w^{low}) &= \sum_{i=1}^{N_B} w_i^{low} \phi_i + b_0, \\ \overline{S}_{opt}(\omega_n; w^{up}) &= \sum_{i=1}^{N_B} w_i^{up} \phi_i + b_0, \end{aligned} \quad (\text{B.4})$$

474 to modify the weights as part of an optimisation

$$\begin{aligned} \min \quad & \left\| \overline{S}_{opt}(\omega_n; w^{up}) - \underline{S}_{opt}(\omega_n; w^{low}) \right\| \\ \text{s.t.} \quad & \overline{S}_{opt}(\omega_n; w^{up}) \geq S_{max}(\omega_n) \\ & \underline{S}_{opt}(\omega_n; w^{low}) \leq S_{min}(\omega_n) \\ & \underline{S}_{opt}(\omega_n; w^{low}) \geq 0 \\ & w^{low} \leq w^{up}. \end{aligned} \quad (\text{B.5})$$

475 Thus, an upper bound \overline{S}_{opt} and lower bound \underline{S}_{opt} can be obtained.

476 References

- 477 [1] Y.-K. Lin, G.-Q. Cai, Probabilistic Structural Dynamics: Advanced Theory and Applications, McGraw-
 478 Hill New York, 1995.
- 479 [2] A. K. Chopra, Dynamics of Structures: Theory and Applications to Earthquake Engineering, Prentice-
 480 Hall, 1995.

- 481 [3] J. Li, J. Chen, Stochastic Dynamics of Structures, John Wiley & Sons, 2009.
- 482 [4] M. Grigoriu, Stochastic Calculus: Applications in Science and Engineering, Springer, 2002. doi:<https://doi.org/10.1007/978-0-8176-8228-6>.
- 483
- 484 [5] L. D. Lutes, S. Sarkani, Random Vibrations: Analysis of Structural and Mechanical Systems, Butterworth-Heinemann, 2004.
- 485
- 486 [6] C. Wang, Structural Reliability and Time-Dependent Reliability, Springer Series in Reliability Engineering, Springer International Publishing, Cham, 2021. URL: <http://link.springer.com/10.1007/978-3-030-62505-4>. doi:10.1007/978-3-030-62505-4.
- 487
- 488
- 489 [7] D. E. Newland, An Introduction to Random Vibrations, Spectral & Wavelet Analysis, Courier Corporation, 2012.
- 490
- 491 [8] R. A. Muller, G. J. MacDonald, Ice ages and astronomical causes: data, spectral analysis and mechanisms, Springer Science & Business Media, 2002.
- 492
- 493 [9] M. B. Priestley, Evolutionary spectra and non-stationary processes, Journal of the Royal Statistical Society. Series B (Methodological) 27 (1965) 204–237.
- 494
- 495 [10] M. Priestley, Power spectral analysis of non-stationary random processes, Journal of Sound and Vibration 6 (1967) 86–97. doi:[https://doi.org/10.1016/0022-460X\(67\)90160-5](https://doi.org/10.1016/0022-460X(67)90160-5).
- 496
- 497 [11] M. Priestley, Spectral Analysis and Time Series, Probability and mathematical statistics : A series of monographs and textbooks, Academic Press, 1982.
- 498
- 499 [12] E. Nikolaidis, D. M. Ghiocel, S. Singhal, Engineering Design Reliability Handbook, 1 ed., CRC press, 2004. doi:<https://doi.org/10.1201/9780203483930>.
- 500
- 501 [13] M. Grigoriu, Stochastic systems: Uncertainty Quantification and Propagation, Springer Science & Business Media, 2012. doi:<https://doi.org/10.1007/978-1-4471-2327-9>.
- 502
- 503 [14] M. G. R. Faes, D. Moens, Recent trends in the modeling and quantification of non-probabilistic uncertainty, Archives of Computational Methods in Engineering 27 (2020) 633–671. URL: <https://link.springer.com/article/10.1007/s11831-019-09327-x>. doi:<https://doi.org/10.1007/s11831-019-09327-x>.
- 504
- 505
- 506
- 507 [15] M. Beer, S. Ferson, V. Kreinovich, Imprecise probabilities in engineering analyses, Mechanical Systems and Signal Processing 37 (2013) 4 – 29. doi:10.1016/j.ymssp.2013.01.024.
- 508
- 509 [16] R. Rocchetta, Q. Gao, M. Petkovic, Soft-constrained interval predictor models and epistemic reliability intervals: A new tool for uncertainty quantification with limited experimental data, Mechanical Systems and Signal Processing 161 (2021) 107973. URL: <https://www.sciencedirect.com/science/article/pii/S088832702100368X>. doi:<https://doi.org/10.1016/j.ymssp.2021.107973>.
- 510
- 511
- 512
- 513 [17] A. Gray, A. Wimbush, M. de Angelis, P. Hristov, D. Calleja, E. Miralles-Dolz, R. Rocchetta, From inference to design: A comprehensive framework for uncertainty quantification in engineering with
- 514

- 515 limited information, *Mechanical Systems and Signal Processing* 165 (2022) 108210. URL: <https://www.sciencedirect.com/science/article/pii/S0888327021005859>. doi:<https://doi.org/10.1016/j.ymsp.2021.108210>.
- 516
- 517
- 518 [18] M. G. R. Faes, M. A. Valdebenito, D. Moens, M. Beer, Bounding the first excursion probability of linear structures subjected to imprecise stochastic loading, *Computers & Structures* 239 (2020) 106320. URL: <https://www.sciencedirect.com/science/article/pii/S0045794920301231>. doi:<https://doi.org/10.1016/j.compstruc.2020.106320>.
- 519
- 520
- 521
- 522 [19] G. Muscolino, F. Genovese, A. Sofi, Reliability Bounds for Structural Systems Subjected to a Set of Recorded Accelerograms Leading to Imprecise Seismic Power Spectrum, *ASCE-ASME Journal of Risk and Uncertainty in Engineering Systems, Part A: Civil Engineering* 8 (2022) 04022009. doi:10.1061/AJRUA6.0001215.
- 523
- 524
- 525
- 526 [20] M. Behrendt, M. G. R. Faes, M. A. Valdebenito, M. Beer, Estimation of an imprecise power spectral density function with optimised bounds from scarce data for epistemic uncertainty quantification, *Mechanical Systems and Signal Processing* 189 (2023) 110072. URL: <https://www.sciencedirect.com/science/article/pii/S0888327022011402>. doi:<https://doi.org/10.1016/j.ymsp.2022.110072>.
- 527
- 528
- 529
- 530 [21] K. Kanai, Semi-empirical formula for the seismic characteristics of the ground, *Bulletin of the Earthquake Research Institute* 35 (1957) 309–325.
- 531
- 532 [22] H. Tajimi, A statistical method of determining the maximum response of a building structure during an earthquake, in: *Proceedings of the 2nd world conference of earthquake engineering*, volume 11, 1960, pp. 781–797.
- 533
- 534
- 535 [23] R. W. Clough, J. Penzien, *Dynamics of structures*, McGraw-Hill, 1975.
- 536 [24] M. S. Bartlett, Smoothing periodograms from time-series with continuous spectra, *Nature* 161 (1948) 686–687.
- 537
- 538 [25] M. S. Bartlett, Periodogram analysis and continuous spectra, *Biometrika* 37 (1950) 1–16. URL: <https://doi.org/10.1093/biomet/37.1-2.1>. doi:10.1093/biomet/37.1-2.1. arXiv:<https://academic.oup.com/biomet/article-pdf/37/1-2/1/486591/37-1-2-1.pdf>.
- 539
- 540
- 541 [26] P. Welch, The use of fast Fourier transform for the estimation of power spectra: A method based on time averaging over short, modified periodograms, *IEEE Transactions on Audio and Electroacoustics* 15 (1967) 70–73. doi:10.1109/TAU.1967.1161901.
- 542
- 543
- 544 [27] P. D. Spanos, G. Failla, Evolutionary spectra estimation using wavelets, *Journal of Engineering Mechanics* 130 (2004) 952–960. doi:10.1061/(ASCE)0733-9399(2004)130:8(952).
- 545
- 546 [28] D. E. Newland, Ridge and Phase Identification in the Frequency Analysis of Transient Signals by Harmonic Wavelets, *Journal of Vibration and Acoustics* 121 (1999) 149–155. URL: <https://doi.org/10.1115/1.2893957>. doi:10.1115/1.2893957.
- 547
- 548

- 549 [29] Z. Huang, Y.-L. Xu, T. Tao, Multi-taper S-transform method for evolutionary spectrum estimation, *Mechanical Systems and Signal Processing* 168 (2022) 108667. URL: <https://www.sciencedirect.com/science/article/pii/S0888327021009912>. doi:<https://doi.org/10.1016/j.ymsp.2021.108667>.
- 550
551
- 552 [30] Z. Huang, Y.-L. Xu, A Multi-Taper S-Transform Method for Spectral Estimation of Stationary Processes, *IEEE Transactions on Signal Processing* 69 (2021) 1452–1467. doi:10.1109/TSP.2021.3057488.
- 553
- 554 [31] M. Shinozuka, G. Deodatis, Simulation of stochastic processes by spectral representation, *Applied Mechanics Reviews* 44 (1991) 191–204. doi:10.1115/1.3119501.
- 555
- 556 [32] J. Liang, S. R. Chaudhuri, M. Shinozuka, Simulation of nonstationary stochastic processes by spectral representation, *Journal of Engineering Mechanics* 133 (2007) 616–627.
- 557
- 558 [33] R. J. Tibshirani, B. Efron, An introduction to the bootstrap, *Monographs on statistics and applied probability* 57 (1993).
- 559
- 560 [34] A. Zerva, *Spatial Variation of Seismic Ground Motions: Modeling and Engineering Applications*, CRC Press, 2009.
- 561
- 562 [35] G. Deodatis, Non-stationary stochastic vector processes: seismic ground motion applications, *Probabilistic Engineering Mechanics* 11 (1996) 149–167. URL: <https://www.sciencedirect.com/science/article/pii/0266892096000070>. doi:[https://doi.org/10.1016/0266-8920\(96\)00007-0](https://doi.org/10.1016/0266-8920(96)00007-0).
- 563
564
- 565 [36] P. Spanos, I. Kougiumtzoglou, Harmonic wavelets based statistical linearization for response evolutionary power spectrum determination, *Probabilistic Engineering Mechanics* 27 (2012) 57 – 68. URL: <http://www.sciencedirect.com/science/article/pii/S0266892011000294>. doi:<https://doi.org/10.1016/j.probingmech.2011.05.008>, the IUTAM Symposium on Nonlinear Stochastic Dynamics and Control.
- 566
567
568
- 569
- 570 [37] C. A. Goulet, T. Kishida, T. D. Ancheta, C. H. Cramer, R. B. Darragh, W. J. Silva, Y. M. Hashash, J. Harmon, G. A. Parker, J. P. Stewart, R. R. Youngs, PEER NGA-East database, *Earthquake Spectra* 37 (2021) 1331–1353. URL: <https://doi.org/10.1177/87552930211015695>. doi:10.1177/87552930211015695. arXiv:<https://doi.org/10.1177/87552930211015695>.
- 571
572
573
- 574 [38] P. D. Spanos, J. Tezcan, P. Tratskas, Stochastic processes evolutionary spectrum estimation via harmonic wavelets, *Computer Methods in Applied Mechanics and Engineering* 194 (2005) 1367–1383. URL: <https://www.sciencedirect.com/science/article/pii/S0045782504003974>. doi:<https://doi.org/10.1016/j.cma.2004.06.039>, special Issue on Computational Methods in Stochastic Mechanics and Reliability Analysis.
- 575
576
577
- 578
- 579 [39] M. Shields, G. Deodatis, Estimation of evolutionary spectra for simulation of non-stationary and non-gaussian stochastic processes, *Computers & Structures* 126 (2013) 149–163. URL: <https://www.sciencedirect.com/science/article/pii/S0045794913000552>. doi:<https://doi.org/10.1016/j.compstruc.2013.02.007>, Uncertainty Quantification in structural analysis and design: To commemo-
- 580
581
582

583 rate Professor Gerhart I. Schueller for his life-time contribution in the area of computational stochastic
584 mechanics.