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OREGON STATE UNIVERSITY

**Backscattering Programs for  
Spherical Targets**

by  
Richard K. Johnson  
Lawrence Flax  
David Standley

Office of Naval Research  
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April 1979

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number)  The programs presented compute the acoustical reflectivity of a sphere in a fluid medium and differ in the allowed physical properties of the spheres. The principal outputs of the programs are plots of reflectivity, $R^2$ , as a function of size-frequency, $ka$ . The reflectivity is defined as $R^2 = \frac{\sigma_b}{a^2/4}$ , where $\sigma_b$ is the backscattering cross-section of the sphere, and $a^2/4$ is the backscattering cross-section of a completely reflecting sphere of radius $a$ . The variable $k$ is the wavenumber in the medium. These plots may be considered		

as dimensionless representations of target strength vs. frequency. The conversions are  $TS = 10 \log (R^2 a^2 / 4)$  and  $f = cka / 2\pi a$  with (a) in meters, (c) in meters per second and (f) in kHz. This relation for frequency is such that the product of frequency in kHz and radius in mm is 240 when  $ka = 1$ . These programs have been used primarily for low contrast cases at relatively low values of  $ka$  (less than 10). Some adjustments to the tolerance parameters may be necessary for other cases.

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BACKSCATTERING PROGRAMS FOR  
SPHERICAL TARGETS\*

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Reference 79-7  
April 1979

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Dean

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\*Supported by the Office of Naval Research

## Introduction

These programs compute the acoustical reflectivity of a sphere in a fluid medium. The programs differ in the allowed physical properties of the spheres. The principal outputs of the programs are plots of reflectivity,  $R^2$ , as a function of size-frequency,  $ka$ . The reflectivity is defined as

$$R^2 = \frac{\sigma_b}{a^2/4},$$

where  $\sigma_b$  is the backscattering cross-section of the sphere, and  $a^2/4$  is the backscattering cross-section of a completely reflecting sphere of radius  $a$ . The variable  $k$  is the wavenumber in the medium.

These plots may be considered as dimensionless representations of target strength vs. frequency. The conversions are

$$TS = 10 \log (R^2 a^2/4) \text{ and}$$

$$f = cka/2\pi a$$

with  $a$  in meters,  $c$  in meters per second and  $f$  in kHz. This relation for frequency is such that the product of frequency in kHz and radius in mm is 240 when  $ka = 1$ .

These programs have been used primarily for low contrast cases (with  $g$  and  $h$  near one) at relatively low values of  $ka$  (less than 10). Some adjustments to the tolerance parameters may be necessary for other cases.

## Program Variables

### Input Parameters

Name	Symbol	Meaning
AB1	$\beta_C$	compressional attenuation in sphere (dB/wavelength)
AB2	$\beta_S$	shear attenuation in sphere (dB/wavelength)
DRATIO	$g$	density of sphere/density of medium
PRATIO	$h$	compressional speed in sphere/speed in medium
SRATIO	$s$	shear speed in sphere/speed in medium
Z	$ka$	size-frequency parameter

### Output Parameters

G	R	reflectivity or form function
G2	$R^2$	reflectivity squared

## Fluid Sphere

The program SPHERF is a simplified version of SPHERE. It calculates  $R^2$  for a sphere which differs from the fluid medium only in density and compressional sound speed.

### Bibliography

Anderson, V.C., 1950. Sound scattering from a fluid sphere. J. Acoust. Soc. Am. 22, 426-431.

Johnson, R.K., 1977. Sound scattering from a fluid sphere revisited. J. Acoust. Soc. Am. 61, 375-377.

```

0001      PROGRAM SPHERF
C*****
C SPHERF
C   COMPUTES BACK SCATTERING FORM FUNCTION FOR A FLUID SPHERE
C   WRITTEN BY LARRY FLAX,NRL
C   MODIFIED BY R K JOHNSON AND D STANDLEY
C
C*****
0002      DIMENSION ZZ(1000),IE(10),GG(1000)
0003      COMPLEX CI,TEMP,SUM,F
0004      DATA NO/2HN /,D/0.1/,EPS/0.0005/
C---PLOT COMMON, ETC.
0005      COMMON /PLT/P(14),IROT,ISIZE,NXCH,NYCH,XFMT,YFMT,XLAB,YLAB
0006      DIMENSION XFMT(2),YFMT(2),XLAB(10),YLAB(10),PLID(3)
0007      DIMENSION DATLBL(10),PRL(3),DRL(3)
0008      EQUIVALENCE (DATLBL,PLID(3))
0009      DATA PLID/'SPHE','RF'  ','  ''  //
0010      DATA P/7.,8.,2.,2.,0.,0.,0.,0.,0.,0.,1.,10.,1.,10./
0011      DATA XFMT/'(F4,','1)'  ','  ',YFMT/'(F5,','0)'  '//,NXCH/4/,NYCH/5/
0012      DATA PENUP/1/,PENDWN/0/
0013      DATA PRL/'H = ','2*'  '//,DRL/'G = ','2*'  '//
0014      DATA XLAB/' KA ','9*'  '//
0015      DATA YLAB/' R ('','DB)' ','8*'  '//
0016      INTEGER PENUP, PENDWN

C-----
C   GET ACOUSTIC PROPERTIES AND KA RANGE
C
0017      1  CALL DATMSG
0018      CALL DTMSG(DATLBL)          !FOR PLOT
0019      TYPE 100
0020      ACCEPT 101, DRATIO, PRATIO  !G,H
0021      20  TYPE 102
0022      ACCEPT 101, ZFROM,ZTO,ZSTEP
0023      IEND=(ZTO-ZFROM)/ZSTEP+1.5
0024      IF(IEND .LE. 1000)GO TO 30
0026      TYPE 110
0027      GO TO 20
0028      30  TYPE 103
0029      ACCEPT 104, ITYP
0030      IF(ITYP.EQ.NO)GO TO 50
0032      TYPE 105
0033      50  CONTINUE
0034      CI=(0.,1.)
0035      G2LM=1000.          !SET G2L MINIMUM ARBITRARILY HIGH
C*****  START LOOP
0036      DO 80 IZ=1,IEND
0037      Z=FLOAT(IZ-1)*ZSTEP+ZFROM
0038      ZL=Z/PRATIO
0039      TE1=0.
0040      TE2=0.
0041      TEMP=(0.,0.)
0042      CALL SBESJ(Z,0,BJ,D,IE(1))
0043      CALL SBESJ(ZL,0,BJL,D,IE(2))
0044      CALL SBESY(Z,0,BY,IE(3))
0045      DO 6 K=1,50
0046      L=K-1
0047      X=(2*L+1)*(-1)**L
0048      CALL SBESJ(Z,K,BJ1,D,IE(4)) !SPHERICAL BESSEL FUNCTIONS
0049      CALL SBESJ(ZL,K,BJL1,D,IE(5))
0050      CALL SBESY(Z,K,BY1,IE(6))
0051      DO 80 ICK=1,6
0052      IF(IE(ICK).EQ.0)GO TO 80
0054      TYPE 106,ICK,IE(ICK)
0055      80  IE(ICK) = 0

```

```

0056      BJP=BJ*L/Z-BJ1          !FIRST DERIVATIVES
0057      BJPL=BJL*L/ZL-BJL1
0058      BYP=BY*L/Z-BY1
0059      E2=ZL*BJPL/BJL
0060      AN=E2/DRATIO
0061      R=BJ*AN-Z*BJP
0062      S=BY*AN-Z*BYP
0063      U=R*R+S*S
0064      SUM=(X/U)*(CI*R*R-R*S)
0065      TEMP=SUM+TEMP
0066      T=REAL(TEMP)
0067      T1=AIMAG(TEMP)
0068      QE1=ABS((T-TE1)/T)
0069      QE2=ABS((T1-TE2)/T1)
C.....INCLUDE MORE MODES UNTIL CHANGE IS LESS THAN EPS
0070      IF(QE1.LE.EPS.AND.QE2.LE.EPS)GO TO 13
0072      TE1=T
0073      TE2=T1
0074      BJ = BJ1                !BESSEL OUTPUT FOR NEXT ITERATION
0075      BJL = BJL1
0076      BY = BY1
0077      6 CONTINUE
0078      13 F = 2. * TEMP / Z    !FORM FUNCTION
0079      F1=REAL(F)
0080      F2=AIMAG(F)
C.....MODULUS=SQRT(BACKSCATTERING/GEOMETRIC CROSS-SECTION)
0081      G2=F1*F1+F2*F2
0082      G=SQRT(G2)
0083      ZZ(IZ)=ALOG10(Z)
0084      G2L=10.*ALOG10(G2)
0085      IF(ITYP.NE.NO)TYPE 107,Z,L,G,G2L
0087      GG(IZ)=G2L
0088      IF(G2L.LT.G2LM)G2LM=G2L    !SEARCH FOR MINIMUM VALUE OF G2L
0090      800 CONTINUE

C-----
C      PLOTTING ROUTINE:
C
0091      TYPE 108,G2LM
0092      ACCEPT 101, YS
0093      IF(YS.GE.0)GO TO 1
0095      ZLOGS=ALOG10(ZFROM)
0096      ZLOGE=ALOG10(ZTO)
0097      MIN = INT((SIGN(ABS(ZLOGS)+0.96,ZLOGS)))
0098      IF(MIN .GT. 0)MIN = MIN - 1
0100      XMIN = 10. ** MIN
0101      MAX = INT((SIGN(ABS(ZLOGE)+0.96,ZLOGE)))
0102      IF(MAX .LT. 0)MAX = MAX + 1
0104      XMAX = 10. ** MAX
0105      P(1) = 7.                !X LENGTH
0106      P(2) = 8.                !Y LENGTH
0107      P(3) = 2.
0108      P(4) = 2.
0109      P(5) = XMIN
0110      P(6) = XMAX
0111      P(7) = YS                !YMIN
0112      P(8) = YS + 80.         !YMAX
0113      P(9) = P(5)            !XO
0114      P(10) = YS             !YO
0115      CALL AXIS(3)           !DRAW AXES
0116      ENCODE(6,109,DRL(2))DRATIO
0117      ENCODE(6,109,PRL(2))PRATIO
0118      CALL PLOTXY(P(5),P(8),PENUP,0)    !GO TO (XMIN,YMAX)
0119      CALL PLOT(5,IX,IY)
0120      IX = IX + 200

```



```
0121      CALL STRING(IX,IY,28,PLID,0,2)                !LABEL THE PLOT
0122      CALL STRING(IX,IY-60,10,DRL,0,2)
0123      CALL STRING(IX,IY-120,10,PRL,0,2)
0124      CALL PLOTXY(P(5),P(7),PENUP,0)
0125      DO 600 I=1, IEND
0126          YY = GG(I)
0127          XXX = ZZ(I)
0128          IF(I .EQ. 1)CALL PLOTXY(XXX, YY, PENUP, 0) !GO TO FIRST POINT
0130 600    CALL PLOTXY(XXX, YY, PENDWN, 0)
0131      CALL PLWAIT
0132      CALL PLOT(2,1885)
0133      CALL PLOT(3)
0134      CALL PLWAIT
0135      GO TO 1
0136 100    FORMAT(' ENTER DRATIO, PRATIO ... [G,H] : ', $)
0137 101    FORMAT (3F10.4)
0138 102    FORMAT(' ENTER ZFROM, ZTO, ZSTEP : ', $)
0139 103    FORMAT(' TYPE RESULTS?(Y/N) ', $)
0140 104    FORMAT(A2)
0141 105    FORMAT ('          KA          MODE          MODULUS          2OLOG '//)
0142 106    FORMAT(' REQ PREC NOT ACHIEVED. ROUTINE #',I2,' ER=',I2)
0143 107    FORMAT(F10.3,I8,F14.4,F11.1)
0144 108    FORMAT('OPLOT:GIVE START OF Y SCALE (MAX VALUE=',F5.1,') : ', $)
0145 109    FORMAT(F6.3)
0146 110    FORMAT(' TOO MANY INCREMENTS ... TRY AGAIN'//)
0147      END
*
```

G = 1.040

H = 1.020

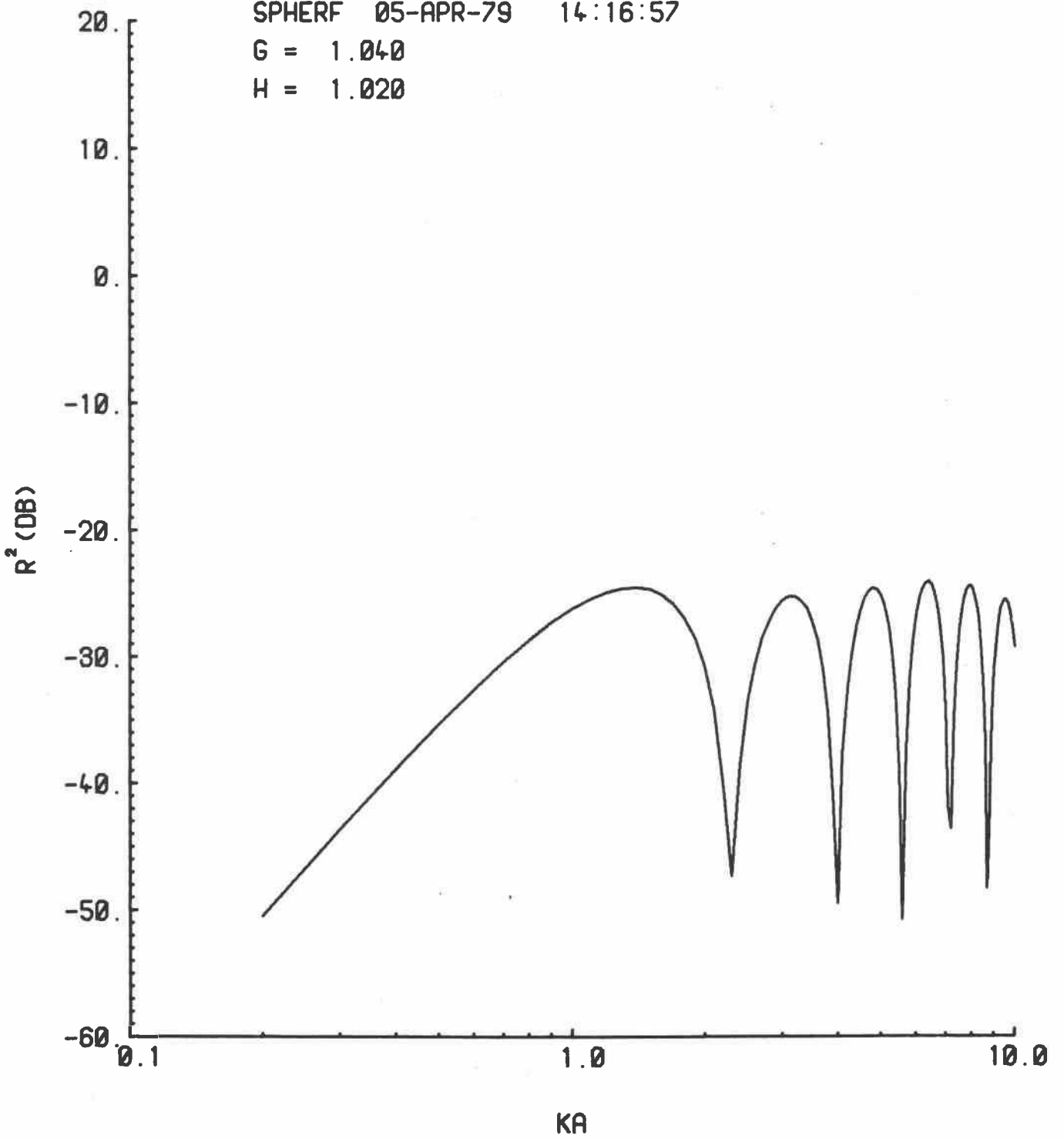


Fig. 1 Output plot from SPHERF.

## Elastic Sphere

The program SPHERE calculates  $R^2$  for a elastic sphere in a fluid medium.  
The original version of this program was written by Larry Flax.

### Bibliography

- Neubauer, W.G., Vogt, R.H., and L.R. Dragonette, 1974. Acoustic reflection from elastic spheres. I. Steady-state signals. J. Acoust. Soc. Am. 55, 1123-1129.
- Faran Jr., J.J., 1951. Sound Scattering by solid cylinders and spheres. J. Acoust. Soc. Am. 23, 405.
- Hampton, L.D. and C.M. McKinney, 1961. Experimental study of the scattering of acoustic energy from solid metal spheres in water. J. Acoust. Soc. Am. 33, 694.
- Hickling, R., 1962. Analysis of echoes from solid elastic sphere in water. J. Acoust. Soc. Am. 34, 1582.
- Rudgers, A.J., 1967. Techniques for numerically evaluating the formulas describing monostatic reflections of acoustic waves by elastic spheres. NRL Rep. 6551

```

0001      PROGRAM SPHERE
C*****
C SPHERE
C   COMPUTES BACK SCATTERING FORM FUNCTION FOR AN ELASTIC SPHERE
C   WRITTEN BY LARRY FLAX,NRL
C   MODIFIED BY R K JOHNSON, T KEFFER, AND D STANDLEY
C
C*****
0002      DIMENSION ZZ(500),IE(10),GG(500),A(3,3)
0003      COMPLEX CI,TEMP,SUM,F
0004      REAL LM1,LP1
0005      DATA NO/2HN /,D/0.1/,EPS/0.001/
C---PLOT COMMON, ETC.
0006      COMMON /PLT/P(14),IROT,ISIZE,NXCH,NYCH,XFMT,YFMT,XLAB,YLAB
0007      DIMENSION XFMT(2),YFMT(2),XLAB(10),YLAB(10),PLID(3)
0008      DIMENSION DATLBL(10),PRL(3),DRL(3),SRL(3)
0009      EQUIVALENCE (DATLBL,PLID(3))
0010      DATA PLID/'SPHE','RE ','/'
0011      DATA P/7.,8.,2.,2.,0.,0.,0.,0.,0.,0.,1.,10.,1.,10./
0012      DATA XFMT/'(F4.,'1) ','/,'YFMT/'(F5.,'0) ','/,'NXCH/4/,'NYCH/5/
0013      DATA PENUP/1/,PENDWN/0/
0014      DATA PRL/'H = ','2*' /,'DRL/'G = ','2*' /
0015      DATA XLAB/' KA ','9*' /,'SRL/'S = ','2*' /
0016      DATA YLAB/' R (','DB) ','8*' /
0017      INTEGER PENUP, PENDWN
C-----
C   GET ACOUSTIC PROPERTIES AND KA RANGE
C
0018      1   CALL DATMSG
0019      CALL DTMSG(DATLBL)           !FOR PLOT
0020      TYPE 100
0021      ACCEPT 101,DRATIO,PRATIO,SRATIO           !G,H,S
0022      20  TYPE 102
0023      ACCEPT 101, ZFROM,ZTO,ZSTEP
0024      IEND=(ZTO-ZFROM)/ZSTEP+1.5
0025      IF(IEND .LE. 500)GO TO 30
0027      TYPE 110
0028      GO TO 20
0029      30  TYPE 103
0030      ACCEPT 104, ITYP
0031      IF(ITYP.EQ.NO)GO TO 40
0033      TYPE 105
0034      40  C=SRATIO**2/(PRATIO**2-2.*SRATIO**2)   !POISSON'S RATIO
0035      50  CONTINUE
0036      CI=(0.,1.)
0037      G2LM=1000.           !SET G2L MINIMUM ARBITRARILY HIGH
C***** START LOOP
0038      DO 800 IZ=1,IEND
0039      Z=FLOAT(IZ-1)*ZSTEP+ZFROM
0040      ZL=Z/PRATIO
0041      ZS=Z/SRATIO
0042      TE1=0.
0043      TE2=0.
0044      TEMP=(0.,0.)
0045      CALL SBESJ(Z,0,BJ,D,IE(1))
0046      CALL SBESJ(ZL,0,BJL,D,IE(2))
0047      CALL SBESY(Z,0,BY,IE(3))
0048      CALL SBESJ(ZS,0,BJS,D,IE(4))
0049      DO 6 K=1,50
0050      L=K-1
0051      X=(2*L+1)*(1-2*MOD(L,2))
0052      CALL SBESJ(Z,K,BJ1,D,IE(5)) !SPHERICAL BESSEL FUNCTIONS
0053      CALL SBESJ(ZL,K,BJL1,D,IE(6))
0054      CALL SBESJ(ZS,K,BJS1,D,IE(7))

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```

0055     CALL SBESY(Z,K,BY1,IE(8))
0056     DO 80 ICK=1,8
0057     IF(IE(ICK).EQ.0)GO TO 80
0059     TYPE 106,ICK,IE(ICK)
0060     80 IE(ICK) = 0
0061     BJP=BJ*L/Z-BJ1           !FIRST DERIVATIVES
0062     BJPL=BJL*L/ZL-BJL1
0063     BJPS=BJS*L/ZS-BJS1
0064     BYP=BY*L/Z-BY1
0065     ZS2=ZS*ZS           !SECOND DERIVATIVES
0066     LM1=FLOAT(L*(L-1))
0067     LP1=FLOAT(L*(L+1))
0068     BJPPL=(LM1/(ZL*ZL)-1.)*BJL+2.*BJL1/ZL
0069     BJPPS=(LM1/ZS2-1.)*BJS+2.*BJS1/ZS
0070     A(1,1)=(BJL-2.*C*BJPPL)/(1.+2.*C)
0071     A(1,3)=-2.*LP1*(ZS*BJPS-BJS)/ZS2
0072     A(2,1)=ZL*BJPL
0073     A(2,3)=LP1*BJS
0074     A(3,1)=2.*(ZL*BJPL-BJL)
0075     A(3,3)=ZS2*BJPPS+FLOAT((L+2)*(L-1))*BJS
0076     E1=A(2,1)*A(3,3)-A(3,1)*A(2,3)
0077     E=A(1,1)*A(3,3)-A(1,3)*A(3,1)
0078     E2=E1/E
0079     AN=E2/DRATIO
0080     R=BJ*AN-Z*BJP
0081     S=BY*AN-Z*BYP
0082     U=R*R+S*S
0083     SUM=(X/U)*(CI*R*R-R*S)
0084     TEMP=SUM+TEMP
0085     T=REAL(TEMP)
0086     T1=AIMAG(TEMP)
0087     QE1=ABS((T-TE1)/T)
0088     QE2=ABS((T1-TE2)/T1)
C.....INCLUDE MORE MODES UNTIL CHANGE IS LESS THAN EPS
0089     IF(QE1.LE.EPS.AND.QE2.LE.EPS)GO TO 13
0091     TE1=T
0092     TE2=T1
0093     BJ = BJ1           !BESSEL OUTPUT FOR NEXT ITERATION
0094     BJL = BJL1
0095     BJS = BJS1
0096     BY = BY1
0097     6 CONTINUE
0098     13 F = 2. * TEMP / Z           !FORM FUNCTION
0099     F1=REAL(F)
0100     F2=AIMAG(F)
C.....MODULUS=SQRT(BACKSCATTERING/GEOMETRIC CROSS-SECTION)
0101     G2=F1*F1+F2*F2
0102     G=SQRT(G2)
0103     ZZ(IZ)=ALOG10(Z)
0104     G2L=10.*ALOG10(G2)
0105     IF(ITYP.NE.NO)TYPE 107,Z,L,G,G2L
0107     GG(IZ)=G2L
0108     IF(G2L.LT.G2LM)G2LM=G2L           !SEARCH FOR MINIMUM VALUE OF G2L
0110     800 CONTINUE
C-----
C PLOTTING ROUTINE:
C
0111     TYPE 108,G2LM
0112     ACCEPT 101, YS
0113     IF(YS.GE.0)GO TO 1
0115     ZLOGS=ALOG10(ZFROM)
0116     ZLOGE=ALOG10(ZTO)
0117     MIN = INT((SIGN(ABS(ZLOGS)+0.96,ZLOGS)))
0118     IF(MIN .GT. 0)MIN = MIN - 1

```

```

0120      XMIN = 10. ** MIN
0121      MAX = INT((SIGN(ABS(ZLOGE)+0.96,ZLOGE)))
0122      IF(MAX .LT. 0)MAX = MAX + 1
0124      XMAX = 10. ** MAX
0125      P(1) = 7.                !X LENGTH
0126      P(2) = 8.                !Y LENGTH
0127      P(3) = 2.
0128      P(4) = 2.
0129      P(5) = XMIN
0130      P(6) = XMAX
0131      P(7) = YS                !YMIN
0132      P(8) = YS + 80.         !YMAX
0133      P(9) = P(5)            !X0
0134      P(10) = YS             !Y0
0135      CALL AXIS(3)           !DRAW AXES
0136      ENCODE(6,109,DRL(2))DRATIO
0137      ENCODE(6,109,PRL(2))PRATIO
0138      ENCODE(6,109,SRL(2))SRATIO
0139      CALL PLOTXY(P(5),P(8),PENUP,0)           !GO TO (XMIN,YMAX)
0140      CALL PLOT(5,IX,IY)
0141      IX = IX + 200
0142      CALL STRING(IX,IY,28,PLID,0,2)           !LABEL THE PLOT
0143      CALL STRING(IX,IY-60,10,DRL,0,2)
0144      CALL STRING(IX,IY-120,10,PRL,0,2)
0145      CALL STRING(IX,IY-180,10,SRL,0,2)
0146      CALL PLOTXY(P(5),P(7),PENUP,0)
0147 599  DO 600 I=1, IEND
0148      YY = GG(I)
0149      XXX = ZZ(I)
0150      IF(I .EQ. 1)CALL PLOTXY(XXX, YY, PENUP, 0) !GO TO FIRST POINT
0152 600  CALL PLOTXY(XXX, YY, PENDWN, 0)
0153      CALL PLWAIT
0154      CALL PLOT(2,1885)
0155      CALL PLOT(3)
0156      CALL PLWAIT
0157      GO TO 1
0158 100  FORMAT(' ENTER DRATIO, PRATIO, SRATIO ... [G,H,S] : ',%)
0159 101  FORMAT(3F10.4)
0160 102  FORMAT(' ENTER ZFROM, ZTO, ZSTEP : ',%)
0161 103  FORMAT(' TYPE RESULTS?(Y/N) ',%)
0162 104  FORMAT(A2)
0163 105  FORMAT('/'          KA          MODE          MODULUS          2OLOG '//)
0164 106  FORMAT(' REQ PREC NOT ACHIEVED. ROUTINE #',I2,' ER=',I2)
0165 107  FORMAT(F10.3,I8,F14.4,F11.1)
0166 108  FORMAT('O PLOT:GIVE START OF Y SCALE (MAX VALUE=',F5.1,') : ',%)
0167 109  FORMAT(F6.3)
0168 110  FORMAT(' TOO MANY INCREMENTS ... TRY AGAIN'//)
0169      END
*
```

SPHERE 05-APR-79 14:08:49

G = 1.040

H = 1.020

S = 0.010

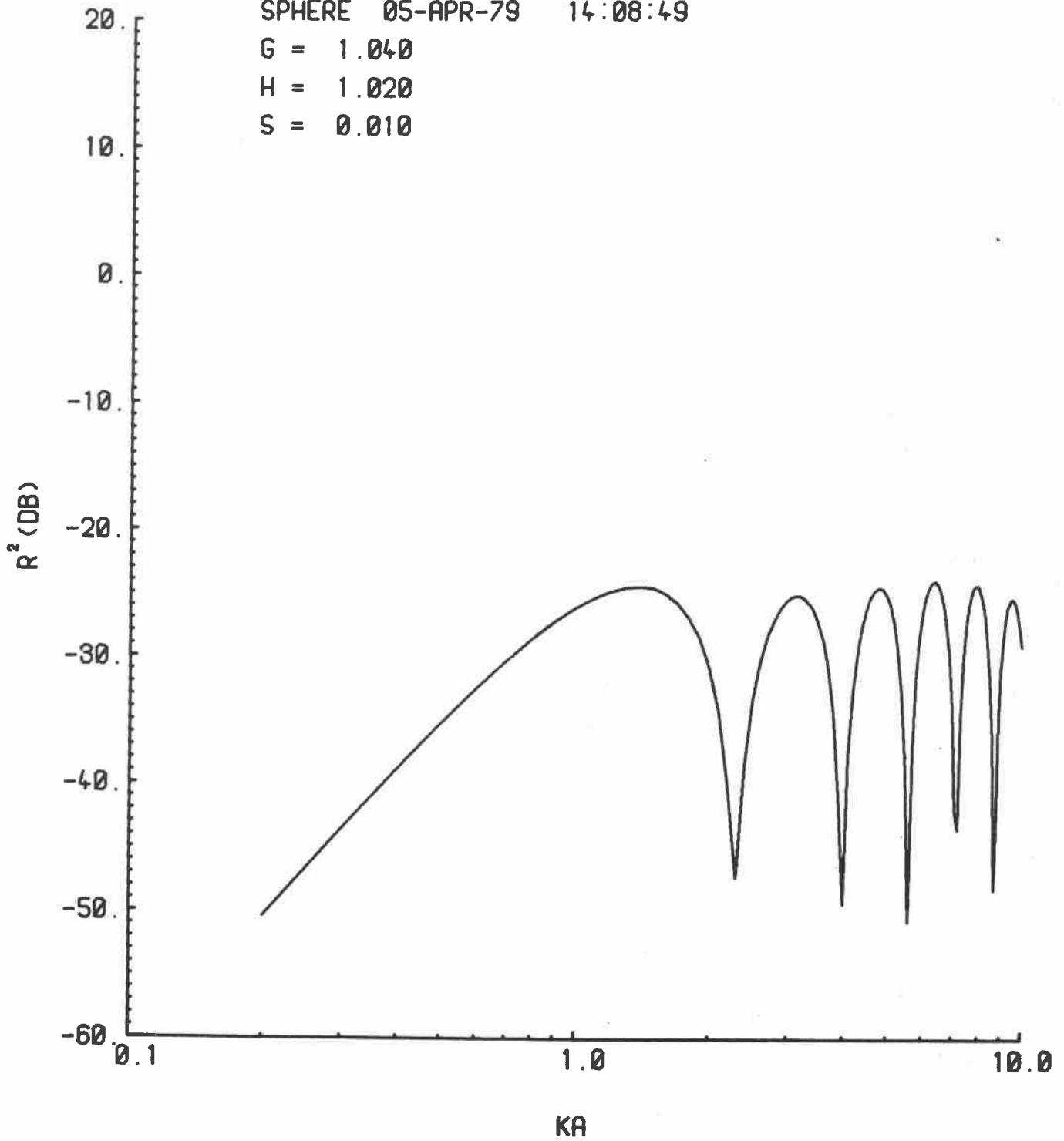


Fig. 2 Output plot from SPHERE for a case with very low shear speed.

SPHERE 05-FEB-79 12:03:00

G = 1.040

H = 1.020

S = 0.050

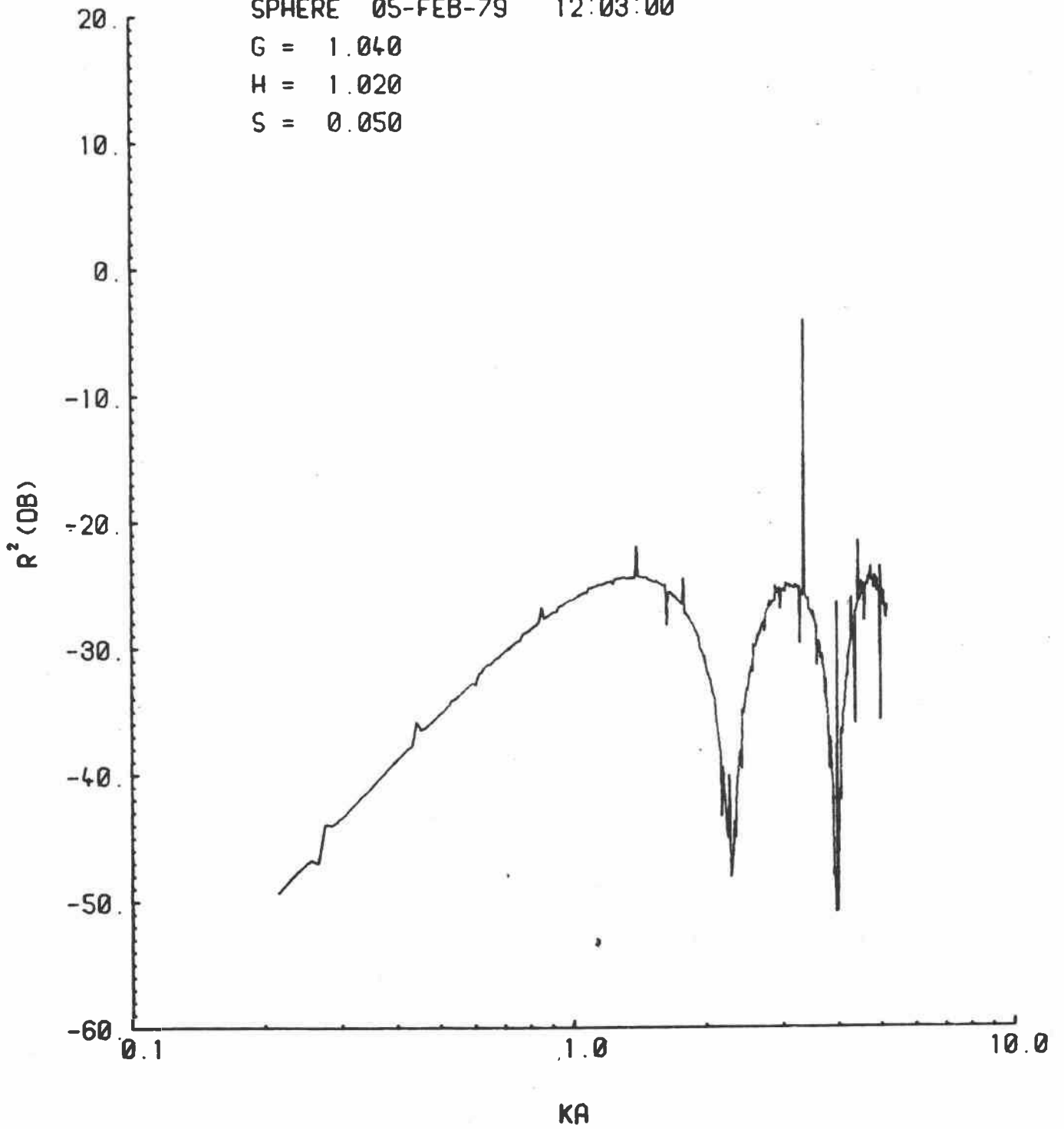


Fig. 3 Output plot from SPHERE for a case with moderate shear speed.



## Viscoelastic Sphere

The program ABSPHR calculates  $R^2$  for a viscoelastic (absorbing) sphere in a fluid medium. The original version of this program was supplied by Tokahi Hasegawa.

### Bibliography

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- Hasegawa, T., Kitagawa, Y., and Y. Watanabe, 1977. Sound reflection from an absorbing sphere. *J. Acoust. Soc. Am.*, 62, 1298-1300.
- Vogt, R.H., Flax, L., Dragonette, L.R., and W.G. Neubauer, 1975. Monostatic reflection of a plane wave from an absorbing sphere. *J. Acoust. Soc. Am.* 57, 558-561.

```

0001      PROGRAM ABSPHR
C*****
C ABSPHR
C
C ACOUSTIC BACK SCATTERING FROM AN ABSORBING SPHERE:
C REFLECTION FORM FUNCTION VS KA
C
C THIS PROGRAM CALCULATES THE REFLECTION FORM FUNCTION FOR AN
C ABSORBING ELASTIC SPHERE BASED ON TAKAHI HASEGAWA, YOSHIKO
C KITAGAWA AND YUMIKO WATANABE. SOUND REFLECTION FROM AN
C ABSORBING SPHERE. J.ACOUST. SOC. AM.62, 1298-1300. 1977.
C
C MODIFIED BY R K JOHNSON AND D STANDLEY
C*****
0002      COMPLEX X1,X2,JN,JB,A,B,G,D,C,E,H,F,HN,PH,CN
0003      COMPLEX D1C,D2C,TC,P5C,DENSC,X3
0004      REAL K1A, K2A
0005      DIMENSION XX(500),YP(500),JN(50),JB(50),SJ(50)
0006      DIMENSION SN(50),ALP(50),BET(50),DJN(50),DJB(50)
0007      DATA YES/'YES'//, EPS/0.001/,PX/54.5757/
C---PLOT COMMON, ETC.
0008      COMMON /PLT/P(14),IROT,ISIZE,NXCH,NYCH,XFMT,YFMT,XLAB,YLAB
0009      DIMENSION XFMT(2),YFMT(2),XLAB(10),YLAB(10),PLID(3)
0010      DIMENSION DATLBL(10),AB1L(3),AB2L(3),PRL(3),DRL(3),SRL(3)
0011      EQUIVALENCE (DATLBL,PLID(3))
0012      DATA PLID/'ABSP','HR' '//
0013      DATA P/7.,8.,2.,2.,0.,0.,0.,0.,0.,0.,1.,10.,1.,10./
0014      DATA XFMT/'(F4.','1)' '//,YFMT/'(F5.','0)' '//,NXCH/4/,NYCH/5/
0015      DATA PENUP/1/, PENDWN/0/
0016      DATA AB1L(1)/'AB1='//,AB2L(1)/'AB2='//,DRL(1)/'G = '//
0017      DATA PRL(1)/'H = '//,SRL(1)/'S = '//
0018      DATA XLAB/' KA ','9*' //
0019      DATA YLAB/' R ('','DB) ','8*' //
0020      INTEGER PENUP, PENDWN
0021      1 CALL DATMSG
0022      CALL DTMSG(DATLBL) !FOR PLOT
C-----
C GET OPTION
C 1) CALCULATE AND SAVE RESULTS ON FILE FOR LATER PLOTTING
C 2) CALCULATE AND PLOT RESULTS
C 3) READ RESULTS FILE AND PLOT
C
0023      TYPE 104
0024      ACCEPT 105, IOPT
0025      IF(IOPT.EQ. 3)GO TO 410
0027      2 TYPE 902
0028      ACCEPT 100,AB1,AB2
0029      TYPE 906
0030      ACCEPT 100,DRATIO,PRATIO,SRATIO !G,H,S
0031      CC1 = 1. / PRATIO
0032      CC2 = 1. / SRATIO
0033      9 TYPE 907
0034      ACCEPT 100, ZFROM, ZTO, ZSTEP
0035      IF(ZSTEP.EQ. 0.0)ZSTEP = 0.25
0037      IMAX = IFIX( (ZTO - ZFROM) / ZSTEP + 1.0001)
0038      IF(IMAX.LE. 500)GO TO 10
0040      TYPE 114
0041      GO TO 9
0042      10 YM = 1000. !LARGE MINIMUM
0043      IHDR = 0
0044      ET = SECNDS(0.) !ELAPSED TIME
C***** START LOOP
0045      DO 30 I=1,IMAX
0046      XX(I) = ZFROM + ZSTEP * FLOAT(I-1)

```

```

0047      X = XX(I)
0048      K1A = CC1 * X
0049      K2A = CC2 * X
0050      AL1 = -AB1 * K1A / PX
0051      AL2 = -AB2 * K2A / PX
0052      X1 = CMPLX(K1A,AL1)
0053      X2 = CMPLX(K2A,AL2)
0054      NM = IFIX(X + 5.0)
0055      IF(X .LE. 3.41)NM = 7
0057      IF(X .LE. 2.20)NM = 6
0059      IF(X .LE. 1.83)NM = 5
0061      IF(X .LE. 1.12)NM = 4
0063      IF(X .LE. 0.5)NM = 3
0065      NNM = NM+ 3
0066      IF(AIMAG(X1) .EQ. 0.)GO TO 21
0068      CALL CSBSJ(X1, JN, NNM, IER)
0069      IF(IER .EQ. 0)GO TO 3
0071      TYPE 905, IER, NNM, X1
0072      GO TO 3
0073 21    CALL SJBES(NNM, REAL(X1), DJN)
0074      DO 211 IC = 1, NNM
0075 211   JN(IC) = CMPLX(DJN(IC), 0.)
0076 3     IF(AIMAG(X2) .EQ. 0.)GO TO 22
0078     CALL CSBSJ(X2, JB, NNM, IER)
0079     IF(IER .EQ. 0)GO TO 4
0081     TYPE 905, IER, NNM, X2
0082     GO TO 4
0083 22    CALL SJBES(NNM, REAL(X2), DJB)
0084     DO 221 IC= 1, NNM
0085 221   JB(IC) = CMPLX(DJB(IC), 0.)
0086 4     CALL SJBES(NNM, X, SJ)
0087     CALL SNBES(NNM, X, SN)
0088 25    PJJ = 0.
0089     PNN = 0.
0090     DO 20 N=1,NM
0091     T = FLOAT(N - 1)
0092     N1 = N
0093     N2 = N + 1
0094     TC = CMPLX(T,0.)
0095     A = TC * JN(N1) - X1 * JN(N2)
0096     B = A - JN(N1)
0097     D1C = CMPLX(1.,0.)
0098     D2C = CMPLX(2.,0.)
0099     G = (X2**2 / D2C - TC * (TC - D1C)) * JN(N1) - D2C * X1 * JN(N2)
0100     A = A / B
0101     D = G / B
0102     C = D2C * TC * (TC + D1C) * JB(N1)
0103     E = (D2C * TC * TC - X2**2 - D2C) * JB(N1) + D2C * X2 * JB(N2)
0104     H = D2C * TC * (TC+D1C) * ((D1C-TC) * JB(N1) + X2 * JB(N2))
0105     B = C / E
0106     E = H / E
0107     P5C = CMPLX(.5,0.)
0108     DENSC = CMPLX(DRATIO,0.)
0109     F = P5C * (A - B) * X2**2 / ((D - E) * DENSC)
0110     PJ = T * SJ(N1) - X * SJ(N2)
0111     PN = T * SN(N1) - X * SN(N2)
0112     HN = CMPLX(SJ(N1), -SN(N1))
0113     PH = CMPLX(PJ, -PN)
0114     CN = (CMPLX(PJ,0.)-F*CMPLX(SJ(N1),0.))/(F*HN-PH)
0115     ALP(N1) = REAL(CN)
0116     BET(N1) = AIMAG(CN)
0117     N5 = N - 1
0118     YN = (2. * FLOAT(N5) + 1.) * (-1.)**N5
0119     PJJ = PJJ + YN * BET(N)

```

```

!X IS KA
!COMPRESSIONAL
!SHEAR
!COMPLEX COM. WAVE NUMBER
!COMPLEX SHEAR WAVE NUMBER
!NUMBER OF MODES TO CALCULATE
!FASTER IF NOT CPLX
!ADD UP REAL AND IMAGINARY MODES

```

```

0120          PNN = PNN + YN * ALP(N)
C.....TEST FOR CONVERGENCE
0121          T1 = ABS(YN * BET(N)) / PJJ
0122          T2 = ABS(YN * ALP(N)) / PNN
0123          IF(ABS(T1) .LT. EPS .AND. ABS(T2) .LT. EPS)GO TO 201
0125  20    CONTINUE
0126          N = N - 1
0127          IF(NM+2 .GT. NNM)GO TO 200
0129          NM = NM + 1
0130          GO TO 25
0131  200    TYPE 113,X,NNM,NM
0132  201    YP(I) = 2.0 * SQRT(PJJ**2 + PNN**2) / X !CONVERT TO FORM FUNCTION
0133          YPL = 20. * ALOG10(YP(I))
0134          IF(YPL .LT. YM)YM = YPL
C.....TYPEOUT OPTION
0136          ISW = IPEEK('177570)          !READ CONSOLE SWITCHES
0137          IF(ISW .LT. 0)GO TO 30          !NORMAL
0139          IF(ISW .EQ. 0)GO TO 291        !EXIT LOOP IF SWITCHES=0
0141          IF(IHDR .EQ. 0)TYPE 110
0143          IHDR = 1                      !TYPEOUT IF SWITCHES +
0144          DT = SECNDS(ET)
0145          TYPE 111, X, YP(I), 20.*ALOG10(YP(I)), NNM,NM, X1, X2, DT
0146          ET = SECNDS(0.)
0147          GO TO 30
0148  291    IMAX = I
0149          GO TO 31
0150  30    CONTINUE
0151  31    TYPE 102, (XX(I), YP(I),20.*ALOG10(YP(I)),I=1,IMAX)
C-----
C CHECK OPTIONS
C
0152          GO TO(400,450,410),IOPT
0153  400    TYPE 106                          !OUTPUT FILE
0154          CALL ASSIGN(1,-1,'NEW')
0155          WRITE(1,107)AB1,AB2,DRATIO,PRATIO,SRATIO,YM,IMAX
0156          WRITE(1,108)(XX(I),YP(I),I=1,IMAX)
0157          CALL CLOSE(1)
0158          CALL EXIT
0159  410    TYPE 112                          !INPUT FILE
0160          CALL ASSIGN(1,-1,'RDO')
0161          READ(1,107)AB1,AB2,DRATIO,PRATIO,SRATIO,YM,IMAX
0162          READ(1,108)(XX(I),YP(I),I=1,IMAX)
0163          CALL CLOSE(1)
0164          ZFROM = XX(1)
0165          ZTO = XX(IMAX)
C-----
C PLOTTING ROUTINE:
C
0166  450    TYPE 109,YM
0167          ACCEPT 904, YS
0168          ZLOGS=ALOG10(ZFROM)
0169          ZLOGE=ALOG10(ZTO)
0170          MIN = INT((SIGN(ABS(ZLOGS)+0.96,ZLOGS)))
0171          IF(MIN .GT. 0)MIN = MIN - 1
0173          XMIN = 10. ** MIN
0174          MAX = INT((SIGN(ABS(ZLOGE)+0.96,ZLOGE)))
0175          IF(MAX .LT. 0)MAX = MAX + 1
0177          XMAX = 10. ** MAX
0178          P(1) = 7.                      !X LENGTH
0179          P(2) = 8.                      !Y LENGTH
0180          P(3) = 2.
0181          P(4) = 2.
0182          P(5) = XMIN
0183          P(6) = XMAX

```

```

0184      P(7) = YS                !YMIN
0185      P(8) = YS + 80.         !YMAX
0186      P(9) = P(5)             !X0
0187      P(10) = YS              !Y0
0188      CALL AXIS(3)            !DRAW AXES
0189      ENCODE(6,103,AB1L(2))AB1
0190      ENCODE(6,103,AB2L(2))AB2
0191      ENCODE(6,103,DRL(2))DRATIO
0192      ENCODE(6,103,PRL(2))PRATIO
0193      ENCODE(6,103,SRL(2))SRATIO
0194      CALL PLOTXY(P(5),P(8),PENUP,0)      !GO TO (XMIN,YMAX)
0195      CALL PLOT(5,IX,IY)
0196      IX = IX + 200
0197      CALL STRING(IX,IY,28,PLID,0,2)      !LABEL THE PLOT
0198      CALL STRING(IX,IY-60,10,AB1L,0,2)
0199      CALL STRING(IX,IY-120,10,AB2L,0,2)
0200      CALL STRING(IX,IY-180,10,DRL,0,2)
0201      CALL STRING(IX,IY-240,10,PRL,0,2)
0202      CALL STRING(IX,IY-300,10,SRL,0,2)
0203      CALL PLOTXY(P(5),P(7),PENUP,0)
0204      DO 600 I=1, IMAX          !PLOT THE POINTS
0205          YY = 20. * ALOG10(YP(I))
0206          XXX = ALOG10(XX(I))
0207          IF(I .EQ. 1)CALL PLOTXY(XXX, YY, PENUP, 0) !GO TO FIRST POINT
0209 600    CALL PLOTXY(XXX, YY, PENDWN, 0)
0210          CALL PLWAIT
0211          CALL PLOT(2,1885)
0212          CALL PLOT(3)
0213          CALL PLWAIT
0214 999    GO TO 1
0215 100    FORMAT(8F10.5)
0216 102    FORMAT(/3(5X,'KA',6X,'YP',6X,'20LOG'),/,3(2X,F7.3,F8.4,2X,F7.1))
0217 103    FORMAT(F6.3)
0218 104    FORMAT(' OPTION: 1)CALC&SAVE RESULTS, 2)CALC&PLOT, 3)READ ',
1          'RESULTS&PLOT : ',*)
0219 105    FORMAT(I2)
0220 106    FORMAT('OUTPUT FILE ',*)
0221 107    FORMAT(6E15.5,I6)
0222 108    FORMAT(6E15.5)
0223 109    FORMAT('PLOT:GIVE START OF Y SCALE (MAX VALUE=',F6.1,') :',*)
0224 110    FORMAT(/3X,'KA',6X,'YP',4X,'20LOG',3X,'MODE',5X,'X1R',7X,'X1I',
1          7X,'X2R',7X,'X2I',5X,'SECONDS'/)
0225 111    FORMAT(F7.3,F8.4,F7.1,I4,I3,2X,4(1PE10.3),2X,0PF4.0)
0226 112    FORMAT(' INPUT FILE ',*)
0227 113    FORMAT(' YP DID NOT CONVERGE AT X = ',F5.2,
1          ' NNM = ',I3,' NM = ',I3)
0228 114    FORMAT(' TOO MANY INCREMENTS ... TRY AGAIN')
0229 902    FORMAT(' ENTER AB1, AB2 : ',*)
0230 904    FORMAT(2F10.5)
0231 905    FORMAT('OCSBSJ ERROR #',I4,2X,'MODE=',I3,2X,2E16.7)
0232 906    FORMAT(' ENTER DRATIO, PRATIO, SRATIO ... [G,H,S] : ',*)
0233 907    FORMAT(' ENTER ZFROM, ZTO, ZSTEP : ',*)
0234      END

```

\*

ABSPPHR 05-FEB-79 16:02:53

AB1 = 0.000

AB2 = 0.040

G = 1.040

H = 1.020

S = 0.050

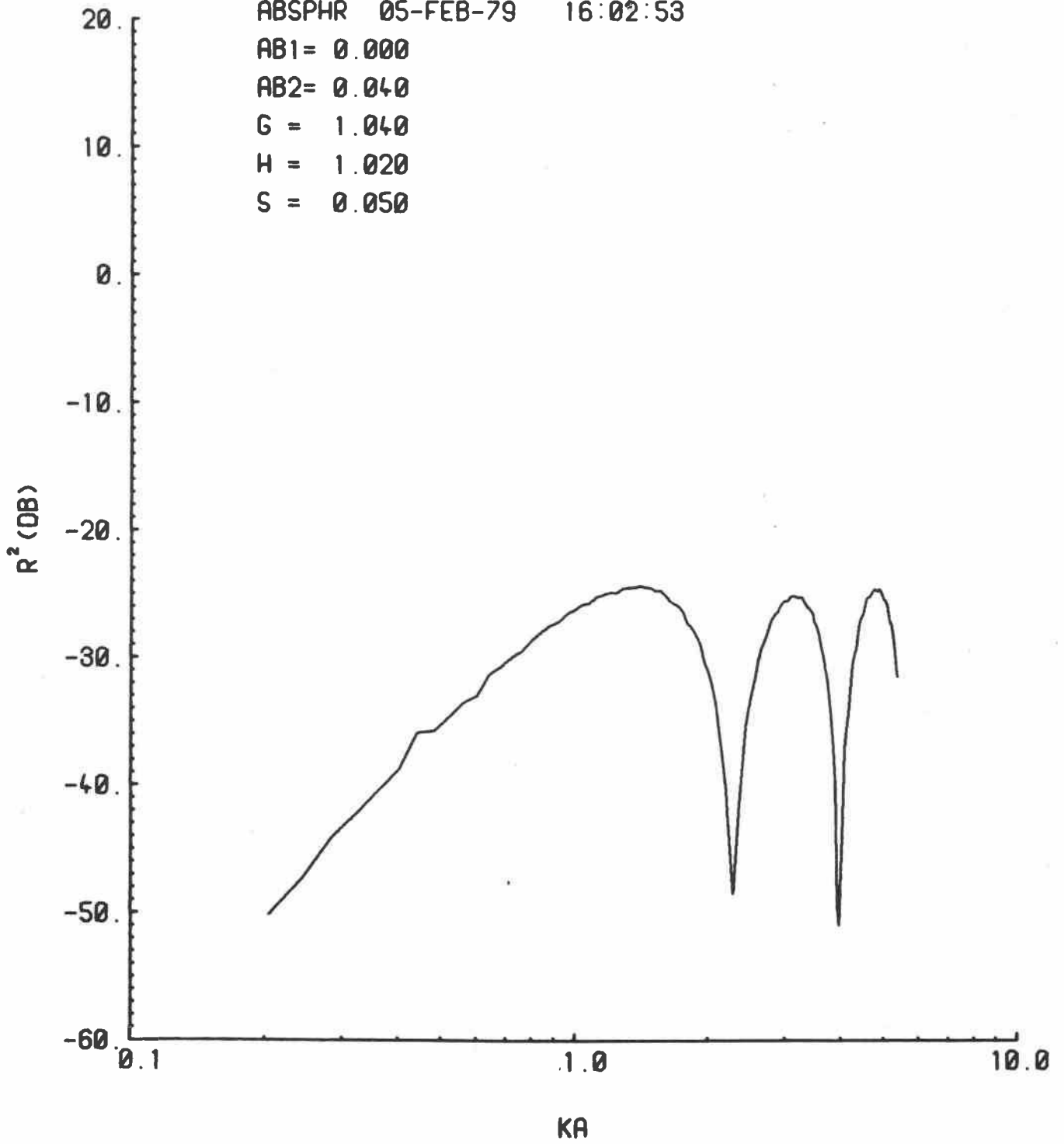


Fig. 4 Output from ABSPPHR for a case with shear attenuation.

## Real Spherical Bessel Functions

SBESJ

This procedure evaluates the spherical Bessel function of the first kind,  $j_n(x)$ , for real arguments. The method used for computation depends on the argument and the order.

For orders 0 and 1, the exact relations are

$$\begin{aligned}j_0(x) &= \sin(x)/x \\j_1(x) &= \sin(x)/x^2 - \cos(x)/x.\end{aligned}\tag{1}$$

For higher orders and small arguments, the procedure uses the series approximations

$$j_n(x) = \frac{x^n}{1 \cdot 3 \cdot 5 \cdots (2n + 1)}.\tag{2}$$

This approximation is acceptable only when

$$x^2/D < 2n,$$

where  $D$  is the required accuracy of the procedure.

For all other cases, the procedure uses the recurrence relation

$$j_{n+1}(x) = \frac{2n+1}{x} j_n(x) - j_{n-1}(x).\tag{3}$$

This relation can be used either to ascend to higher orders or to descend to lower orders.

Ascending recurrence is used for  $x > 2n$  since, in this case, the error in  $j_n(x)$  will not be increased in  $j_{n+1}(x)$ .

For the remaining case ( $x < 2n$ ), the procedure uses Miller's device, which is a decreasing recurrence technique. This method uses the approximation  $\hat{j}_m(x) = 0$  and  $\hat{j}_{m-1}(x) = 1$  for some  $m \geq n$ , then uses decreasing recurrence to calculate  $\hat{j}_i(x)$  for  $0 \leq i < m - 1$ . A scale factor  $P$  is calculated from

$j_0(x)/\hat{j}_0(x)$ , where  $j_0(x)$  is determined from equation (1). The correct value  $j_n(x)$  is the  $P^*j_n(x)$ . This sequence is repeated for higher values of  $m$  until successive values for  $j_n(x)$  differ by less than  $D$ .

#### SBESY

This procedure evaluates the spherical Bessel function of the second kind (also called the spherical Neumann function),  $y_n(x)$  or  $n_n(x)$ , for real arguments. The method is ascending recurrence and presents no computational problems.

These programs were written by Richard Johnson and Thomas Keffer.

#### Bibliography

Abramowitz, M. and I.A. Stegun, 1970. Handbook of Mathematical Functions (U.S. Government Printing Office) 435-478.





```

0020      42 BJ=SIN(X)/X
0021      RETURN
0022      43 BJ=SIN(X)/(X*X)-COS(X)/X
0023      RETURN
      C
      C      IF X IS VERY SMALL USE ASCENDING SERIES
0024      49 IF(X*X/D-FLOAT(2*N))300,50,50
      C
      C      IF X IS LARGE, USE INCREASING RECURRENCE
      C
0025      50      IF(X-FLOAT(2*N))60,210,210
      C
      C      IF X IS MIDDLIN, USE DECREASING RECURRENCE
      C
0026      60 MA=X+8.
0027      MB=N+IFIX(X)/4+2
0028      MZERO=MAXO(MA,MB)
      C
      C      SET UPPER LIMIT OF M
      C
0029      MMAX=NTEST
0030      DO 190 M=MZERO,MMAX,3
0031      FM1=1.
0032      FM=.0
0033      DO 160 K=1,M-1
0034      MK=M-K
0035      BMK=FLOAT(2*MK+1)*FM1/X-FM
0036      FM=FM1
0037      FM1=BMK
0038      IF(MK-N-1)160,140,160
0039      140 BJ=BMK
0040      160      CONTINUE
      C
      C      SCALE FACTOR
      C
0041      P=SIN(X)/(X*BMK)
0042      BJ=P*BJ
0043      IF(ABS(BJ-BPREV)-ABS(D*BJ))200,200,190
0044      190 BPREV=BJ
0045      IER=3
0046      200 RETURN
      C
      C      INCREASING RECURRENCE
      C
0047      210 BJA=SIN(X)/X
0048      BJB=SIN(X)/(X*X)-COS(X)/X
0049      K=1
0050      220 T=FLOAT(2*K+1)/X
0051      BJC=T*BJB-BJA
0052      K=K+1
0053      IF (K-N) 230,240,230
0054      230 BJA=BJB
0055      BJB=BJC
0056      GO TO 220
0057      240 BJ=BJC
0058      RETURN
      C
      C      ASCENDING SERIES:
0059      300 BJ=1.0
0060      DO 350 IFAC=1,N
0061      BJ=BJ*X/(FLOAT(2*IFAC+1))
0062      350 CONTINUE
0063      RETURN
0064      END

```

```

C
C .....
C
C     SUBROUTINE SBESY
C
C     PURPOSE
C       COMPUTE THE Y SPHERICAL BESSEL FUNCTION FOR A GIVEN
C       ARGUMENT AND ORDER
C
C     USAGE
C       CALL BESY(X,N,BY,IER)
C
C     DESCRIPTION OF PARAMETERS
C       X -THE ARGUMENT OF THE Y BESSEL FUNCTION DESIRED
C       N -THE ORDER OF THE Y BESSEL FUNCTION DESIRED
C       BY -THE RESULTANT Y BESSEL FUNCTION
C       IER-RESULTANT ERROR CODE WHERE
C         IER=0  NO ERROR
C         IER=1  N IS NEGATIVE
C         IER=2  X IS NEGATIVE OR ZERO
C         IER=3  BY HAS EXCEEDED MAGNITUDE OF 10**36
C
C     REMARKS
C       X MUST BE GREATER THAN ZERO
C       N MUST BE GREATER THAN OR EQUAL TO ZERO
C
C     SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
C       NONE
C
C     METHOD
C       RECURRENCE RELATION AND TRIG FORMULAE AS DESCRIBED
C       BY H.A. ANTOSIEWICZ IN HANDBOOK OF MATHEMATICAL
C       FUNCTIONS, PP. 438-439. THIS CODE PATTERNED AFTER
C       THAT FOR BESY.
C
C .....
0001  SUBROUTINE SBESY(X,N,BY,IER)
C
C     CHECK FOR ERRORS IN N AND X
0002      IF(N)180,10,10
0003      10 IER=0
0004      IF(X)190,190,20
C
C     EVALUATE Y0 AND Y1.
0005      20 Y0=-COS(X)/X
0006      Y1=-COS(X)/(X*X)-SIN(X)/X
C
C     CHECK IF ONLY Y0 OR Y1 IS DESIRED
0007      90 IF(N-1)100,100,130
C
C     RETURN EITHER Y0 OR Y1 AS REQUIRED
0008      100 IF(N)110,120,110
0009      110 BY=Y1
0010      GO TO 170
0011      120 BY=Y0
0012      GO TO 170
C
C     PERFORM RECURRENCE OPERATIONS TO FIND YN(X)

```

```
0013 130 YA=Y0
0014     YB=Y1
0015     K=1
0016 140 T=FLOAT(2*K+1)/X
0017     YC=T*YB-YA
0018     IF (ABS(YC)-1.0E36)145,145,141
0019 141 IER=3
0020     RETURN
0021 145 K=K+1
0022     IF (K-N)150,160,150
0023 150 YA=YB
0024     YB=YC
0025     GO TO 140
0026 160 BY=YC
0027 170 RETURN
0028 180 IER=1
0029     RETURN
0030 190 IER=2
0031     RETURN
0032     END
*
```

## Complex Spherical Bessel Functions

### CSBSJ

This procedure evaluates the spherical Bessel of the first kind,  $j_n(Z)$ , for complex arguments by means of a modified continued fraction technique. This technique is far more effective than upward or downward recursion methods.

The spherical Bessel function of order  $n$  can be expressed in terms of smaller orders as

$$j_n(Z) = \frac{j_n(Z)}{j_{n-1}(Z)} * \frac{j_{n-1}(Z)}{j_{n-2}(Z)} * \dots * \frac{j_1(Z)}{j_0(Z)} * j_0(Z), \quad (1)$$

and  $j_0(Z) = \sin(Z)/Z$ .

Each of the ratios in (1) is found by a modified continued fraction method. Now

$$\frac{j_i(Z)}{j_{i-1}(Z)} = \frac{j_{i+1/2}(Z)}{j_{i-1/2}(Z)} \quad (2)$$

by definition. From Abramowitz and Stegun<sup>2</sup>,

$$\frac{j_i(Z)}{j_{i-1}(Z)} = \frac{1}{a_0} \frac{1}{a_1} \frac{1}{a_2} \dots \quad (3)$$

where  $a_k = 2(i + k)/Z$ .

The inverse of this ratio can be rewritten as

$$\frac{j_{i-1}(Z)}{j_i(Z)} = \frac{N_0 * N_1 * N_2 * \dots}{D_0 * D_1 * \dots} \quad (4)$$

where  $N_k = A_k - 1/N_{k-1}$ ,  $N_0 = A_0$

and  $D_k = A_{k+1} - 1/D_{k-1}$ ,  $D_0 = A_1$ .

In the algorithm, the computation of (4) is continued until  $N_k/D_{k-1} - 1 < \epsilon$ , where  $\epsilon$  is the allowable error.

This program was written by David Standley.

### Bibliography

Abramowitz, M. and I.A. Stegun, 1970. Handbook of Mathematical Functions (U.S. Government Printing Office) 435-478.

Lentz, W.J., 1973. A new method of computing spherical Bessel functions of complex argument with tables. U.S. Army Electronics Command Technical Report ECOM-5509.

0001

SUBROUTINE CSBSJ(X, JJ, M, IER)

\*\*\*\*\*  
 C 12-FEB-79 CHECK FOR XR=0. BEFORE ALOG IS TAKEN  
 C 8-DEC-78 STOP ITERATIONS WHEN (RATIO-1)<EPS  
 C 26-OCT-78 OPTIMIZE FOR SPEED  
 C 4-AUG-78  
 C D. STANDLEY  
 C  
 C COMPUTE COMPLEX SPHERICAL BESSEL FUNCTIONS BY USE OF CONTINUED FRACTIONS.  
 C SEE: "A METHOD OF COMPUTING SPHERICAL BESSEL FUNCTIONS OF COMPLEX  
 C ARGUMENT WITH TABLES" BY W. J. LENTZ  
 C-----

C SUBROUTINE CSBSJ(X, JJ, M, IER)

C DESCRIPTION OF PARAMETERS

C X -THE ARGUMENT OF THE J SPHERICAL BESSEL FUNCTION DESIRED  
 C X IS COMPLEX  
 C JJ -THE RESULTANT J SPHERICAL BESSEL FUNCTION  
 C JJ IS THE ARRAY OF M ORDERS  
 C JJ IS COMPLEX  
 C M -THE ORDER OF THE BESSEL FUNCTION DESIRED  
 C IER -ERROR CODE WHERE:  
 C IER=0 NO ERROR  
 C IER .LT. 0 UNDERFLOW OCCURRED AT ORDER (-IER)  
 C IER=2 IMAGINARY PART OF X IS >80. OR <-80.  
 C IER=3 ORDER > 49  
 C

C THE ACCURACY IS 5 TO 6 SIGNIFICANT FIGURES  
 C

\*\*\*\*\*

0002 COMPLEX X, A, SBES, QUO(50), NUMN, NUMN1, DENN, DENN1, JJ(50)  
 0003 COMPLEX ONE,TWO,TWODX,CSX,RATIO  
 0004 A(N) = TWODX \* CMPLX(V+FLOAT(N-1), ZERO)  
 0005 C1 = 1.  
 0006 EPSR = 1.E-5  
 0007 EPSI = 1.E-3  
 0008 ZERO = 0.  
 0009 ONE = (1.,0.)  
 0010 TWO = (2.,0.)  
 0011 IF(M .GT. 49)GO TO 514 !ORDER TOO BIG  
 0013 XR = REAL(X)  
 0014 XI = AIMAG(X)  
 0015 CSX = CSIN(X)  
 0016 VV = FLOAT(M)  
 0017 IXR = 0  
 0018 ICSR = 0  
 0019 IF(ABS(XI) .GT. 80.)GO TO 513 !OVERFLOW CONDITION!  
 0021 IF(XR .EQ. ZERO)GO TO 4  
 0023 ICSR = IFIX(ALOG10(ABS(REAL(CSX))))  
 0024 IXR = IFIX(ALOG10(ABS(XR)))  
 0025 4 ICSI = 0  
 0026 IXI = 0  
 0027 IF(XI .EQ. ZERO)GO TO 5  
 0029 ICSI = IFIX(ALOG10(ABS(AIMAG(CSX))))  
 0030 IXI = IFIX(ALOG10(ABS(XI)))  
 0031 5 V = VV + 1.5  
 0032 IF(VV .EQ. ZERO)GO TO 501 !CALCULATE DIRECTLY  
 0034 TWODX = TWO / X

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 C CALCULATE THE RATIO OF J(V-1)/J(V)  
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0035 DO 500 IV = 1, IFIX(VV) !GET NECESSARY RATIOS  
 0036 V = V - 1.  
 0037 L = IFIX(V - 0.5)

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0038     NUMNM1 = A(1)
0039     DENNM1 =A(2)
0040     QUO(L) = NUMNM1
0041     N = 1
0042  10    N = N + 1
0043     NUMN = A(N) - ONE / NUMNM1
0044     DENN = A(N+1) - ONE / DENNM1
0045     RATIO = NUMN / DENNM1
0046     IF(ABS(REAL(RATIO))-C1) .GT. EPSR)GO TO 11 !CHECK FOR CONVERGENCE
0048     IF(ABS(AIMAG(RATIO)) .LT. EPSI)GO TO 500 !STOP THE FRACTION
0050  11    QUO(L) = QUO(L) * RATIO !CONTINUE THE FRACTION
0051     NUMNM1 = NUMN
0052     DENNM1 = DENN
0053     GO TO 10
0054  500   CONTINUE

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C  CALCULATE EACH ORDER

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0055  501   DO 600 I=1, M+1
0056         SBES = ONE
0057         N = I - 1
0058         IF(N .EQ. 0)GO TO 510
0060         DO 502 J= 1, N
0061  502   SBES = SBES * ONE / QUO(J)

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C  FROM HERE TO 510 CHECK FOR UNDERFLOW

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0062     IF(REAL(SBES) .EQ. ZERO)GO TO 512
0064     ISR = IFIX(ALOG10(ABS(REAL(SBES))))
0065     ISI = 0
0066     IF(XI .EQ. ZERO)GO TO 504
0068  503   ISI = IFIX(ALOG10(ABS(AIMAG(SBES))))
0069  504   IF((ISR+ICSR) .GT. -36 .AND. (ISR+ICSR-IXR) .GT. -36)GO TO 505
0071         GO TO 512 !REAL UNDERFLOW
0072  505   IF((ISI+ICSI) .GT. -36 .AND. (ISI+ICSI-IXI) .GT. -36)GO TO 510
0074         GO TO 512 !IMAG. UNDERFLOW

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C  HERE COMES THE ANSWER

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0075  510   SBES = SBES * CSX / X
0076  600   JJ(I) = SBES
0077         IER = 0 !NORMAL RETURN
0078         RETURN
0079  512   IER = - N !UNDERFLOW AT ORDER N
0080         RETURN
0081  513   IER = 2 !OVERFLOW
0082         RETURN
0083  514   IER = 3 !ORDER TOO BIG
0084         END

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## Physical Notes

The reflectivity of a fluid sphere generally increases as its density and sound speed contrasts increase. The reflectivity increases most dramatically when the values for the sphere are less than those for the medium.

For the elastic sphere, a shear speed which is very small with respect to the compressional speed of the sphere and the medium will lead to a reflectivity which is indistinguishable from the corresponding fluid case. Apparently the impedance contrast in this case is such that little or no energy is converted to shear.

The elastic sphere program produces strange results for targets with high shear speed. Many of these cases can be ruled out physically since the shear speed of a substance must be less than  $0.7 \times$  its compressional speed. For cases with moderate shear speeds, the results are similar to those for a fluid sphere but spikey. It is probably necessary to include the effects of attenuation in order to get valid results.

For cases with very small attenuation, the viscoelastic sphere program produces results which are indistinguishable from the corresponding elastic cases. A moderate amount of shear attenuation will smooth out the spikiness caused by a moderate shear speed. Moderate values of compressional attenuation will raise the level of the curve; large values will also decrease the depth of the dips.

## Computational Notes

These programs and subroutines have explicit parameters that are used to test for convergence. In order to reduce execution times, these parameters have been set relatively high. The values were selected on the basis of the output plots, so the relative accuracy may be only about one percent.

The output plots are generated by means of an in-house developed plotting package. The output sections of the programs can be easily modified to work with other locally available plotting software.