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Numerical Simulation of Parallel RLC Model Using Different Fractional Derivative Operators

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Abstract- In the current study, the theory of fractional calculus is applied to the electric parallel RLC circuit. The aim of this article is to alter the concept of a parallel RLC circuit by applying various fractional derivative operators. A fractional RLC circuit was investigated via Caputo, Caputo-Fabrizio, and Atangana-Baleanu derivatives. The Laplace transform technique was applied to resolve the system of governing differential equations. The results for the various orders are compared to each other. When the fractional order derivative tends to be one, the system's performance is found to be very slow due to a decrease in damping capacity.

Keywords- Fractional calculus, RLC circuit, Caputo fractional derivative, Caputo-Fabrizio fractional derivative, Atangana-Baleanu fractional derivative.

I. Introduction

Many research fields use fractional calculus, including automatic control, medical applications, civil engineering, time series, and long memory effect modeling [1-8]. The most commonly used definitions of fractional calculus are the Riemann-Liouville and Caputo derivatives with fractional orders, but they have a singularity [9]. Caputo-Fabrizio overcame this problem by devising a new fractional derivative based on the exponential function with no singularity. [10, 11]. The mathematical properties of Fabrizio were developed by Atangana [12]. Atangana-Baleanu introduced another definition of Caputo-Fabrizio based on the Mittag-Leffler function into the fractional derivative, which many researchers have used in their articles [13, 14].

A resistance, capacitor, and inductor (RCL) circuits are found in almost every electrical device. The responses of a parallel RCL circuit will be analyzed using various fractional derivative operators.

In this paper, we will compare the performance of fractional RLC circuits based on Caputo, Caputo-Fabrizio, and Atangana-Baleanu fractional derivatives. It is organized as follows: basic information is explained in the next section. In section 3, we present the mathematical model that represents the various currents in a fractional parallel RLC circuit. Section 4 discusses case studies. Finally, section 5 summarizes this paper's contribution.

II. Basic Information

This section contains various fractional calculus definitions and properties.

2.1 Riemann-Liouville integral operator

The Riemann-Liouville integral operator of order $\alpha \geq 0$ of the function is defined by

$$J_a^\alpha v(t) = \int_a^t \frac{(t-s)^{\alpha-1} v(s)}{\Gamma(\alpha)} ds \quad (1)$$

Where $\Gamma(\alpha)$ is the gamma function. As special case, when $\alpha = 0$, we can write $J_0^\alpha = J^\alpha$

2.2 Caputo fractional derivative

The Caputo fractional derivative of order α of the function $v(t)$ is defined by [21]

$$D_a^\alpha v(t) = J_a^{m-\alpha} \frac{d^m}{dt^m} v(t) = \int_0^t \frac{(t-s)^{m-\alpha-1} v'(s)}{\Gamma(m-\alpha)} ds \quad (2)$$

When $\alpha = 0$ we write ${}_0^{\alpha}D = D^\alpha$

The Laplace transform of (2) is defined by

$$L[D^\alpha v(s)] = s^\alpha v(s) - \sum_{k=0}^{n-1} s^{\alpha-k-1} v^{(k)}(0) \quad (3)$$

When $n = [R(\alpha)] + 1$. From this expression we have two special cases

$$L[D^\alpha v(t)] = s^\alpha v(s) - s^{\alpha-1} v(0), \quad 0 < \alpha \leq 1 \quad (4)$$

$$L[D^\alpha v(t)] = s^\alpha v(s) - s^{\alpha-1} v(0) - s^{\alpha-2} v'(0), \quad 1 < \alpha \leq 2 \quad (5)$$

2.3 Caputo - Fabrizio fractional operator

The Caputo- Fabrizio fractional derivative is defined by [10, 11]

$${}^{cf}_0 D_t^\alpha v(t) = \frac{M(\alpha)}{1-\alpha} \int_0^t v'(s) e^{-\alpha \frac{t-s}{1-\alpha}} ds \quad (6)$$

Where $M(\alpha)$ is a normalization function such that $M(0) = M(1) = 1$

The Laplace transform of (6) is defined by

$$L[{}^{cf}_0 D_t^\alpha v(t)] = \frac{sv(s) - v(0)}{s + \alpha(1-s)} \quad (7)$$

2.4 Atangana – Baleanu fractional operator

The Atangana – Baleanu fractional derivative is defined by [15-20]

$${}^{ABC}_a D_t^\alpha v(t) = \frac{M(\alpha)}{1-\alpha} \int_a^t v'(s) E_\alpha \left(-\alpha \frac{(t-s)^\alpha}{1-\alpha} \right) ds \quad (8)$$

The Laplace transform of (8) is defined by

$$L[{}^{ABC}_a D_t^\alpha v(t)] = \frac{M(\alpha)}{1-\alpha} \frac{s^\alpha v(s) - s^{\alpha-1} v(0)}{s^\alpha + \frac{\alpha}{1-\alpha}} \quad (9)$$

III. Mathematical Model

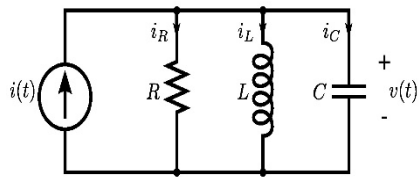


Figure 1. Parallel RLC circuit.

Consider the circuit shown in figure 1, which includes a resistor, capacitor and inductor connected in parallel, with $i_L(0) = i_o$ representing the initial inductor current, $v_c(0) = v_o$ indicating the initial capacitor, and $i_s(t)$ showing the current source [27].

Where i_R is the resistor current, i_L is the inductor current, i_c is the capacitor current and $v(t)$ is the voltage source of the circuit in figure 1.

The governing mathematical equation of the circuit is

$$CD_t^\beta v(t) + \frac{1}{L}j^\alpha V(t) + \frac{1}{R}V(t) + i_0 = i_s(t) \quad (10)$$

Since α and β are the voltage and current parameters of a fractional order inductor and capacitor, respectively [26]. From equation 10, using the Caputo fractional operator in the Laplace domain, the voltage of the capacitor may be represented as

$$v_{c1}(s) = \frac{s^{\alpha+\beta-1}v_c(o) + \frac{1}{C}s^\alpha I_s(s) - \frac{1}{C}I_0s^{\alpha-1}}{s^{\alpha+\beta} + \frac{1}{RC}s^\alpha + \frac{1}{LC}} \quad (11)$$

In the Laplace domain, the voltage of the capacitor using the Caputo-Fabrizio fractional operator can be expressed as

$$v_{c2}(s) = \frac{s + \beta(1 - s) \left(I_s - \frac{I_0}{s} \right) + C v_c(0)}{Cs + (s + \beta(1 - s)) \left(\frac{1}{L}s^{-\alpha} + \frac{1}{R} \right)} \quad (12)$$

In the Laplace domain, the voltage of the capacitor can be represented as using the Atangana – Baleanu operator

$$v_{c3}(s) = \frac{CM(\beta)s^{\beta-1}v_c(0) + (s^\beta - \beta s^\beta + \beta) \left(I_s(s) - \frac{I_0}{s} \right)}{CM(\beta)s^\beta + (s^\beta - \beta s^\beta + \beta) \left(\frac{1}{L}s^{-\alpha} + \frac{1}{R} \right)} \quad (13)$$

IV Case Study

In this section we will discuss an example to describe the under damping (namely figures 2, 3, 4, 6, 7, 8 and 9), over damping (e.g., figures 6, 10 and 11) and critical damping response (figure 12). The model's parameters were chosen as $I_s(t) = 4u_o(t)$, $i_L(0) = 0$, $v_c(0) = 0$, $R = 60 \Omega$, $L = 200 \text{ mH}$, $C = 120 \text{ mF}$.

We obtained the following time response for the RLC circuit based on different values of α and β by using FORTRAN code for finding the inverse Laplace transform for equations (11, 12 and 13).

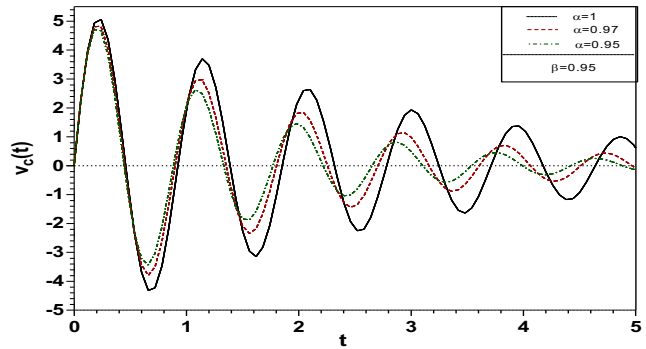


Figure 2. Numerical results for RLC circuit based on Caputo fractional operator; for $\alpha = 0.95, 0.97$ and 1 with $\beta = 0.95$.

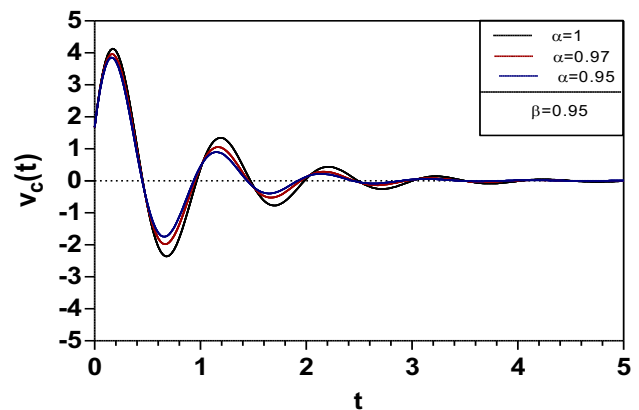


Figure 3. Numerical results for RLC circuit based on Caputo-Fabrizio fractional operator; for $\alpha = 0.95, 0.97$ and 1 with $\beta = 0.95$.

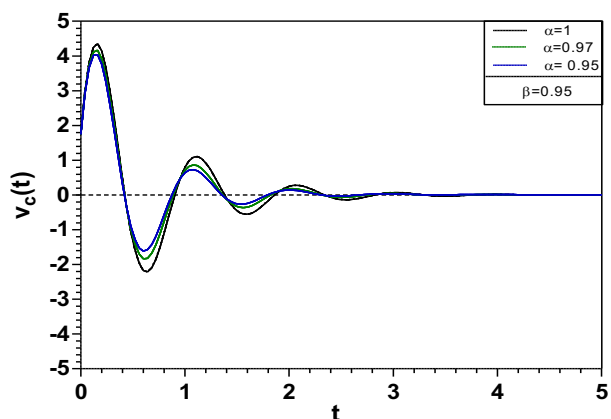


Figure 4. Numerical results for RLC circuit based on Atangana – Baleanu fractional operator; for $\alpha = 0.95, 0.97$ and 1 with $\beta = 0.95$.

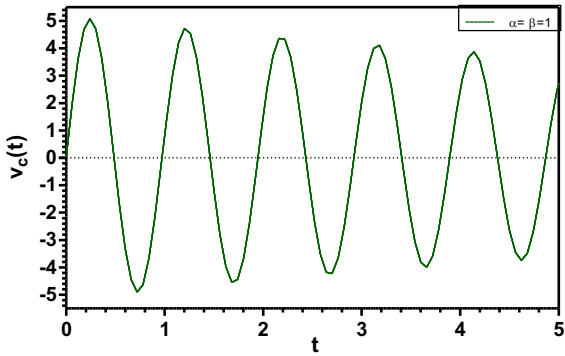


Figure 5. Numerical results for RLC circuit in the classical case; for $\alpha = \beta = 1$.

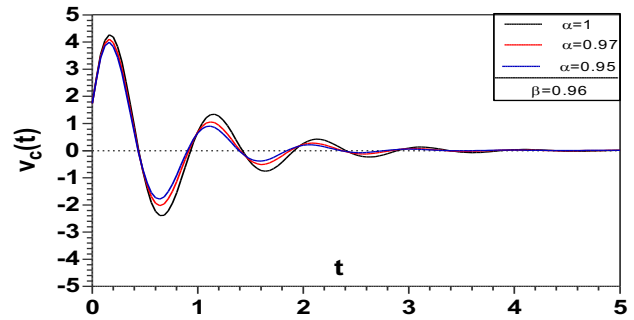


Figure8. Numerical results for RLC circuit based on Caputo-Fabrizio fractional operator; for $\alpha = 0.95, 0.97$ and 1 with $\beta=0.96$.

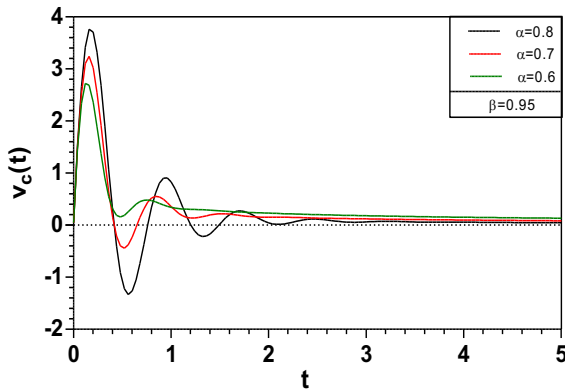


Figure 6. Numerical results for RLC circuit based on Caputo fractional operator; for $\alpha = 0.6, 0.7$ and 0.8 with $\beta = 0.95$.

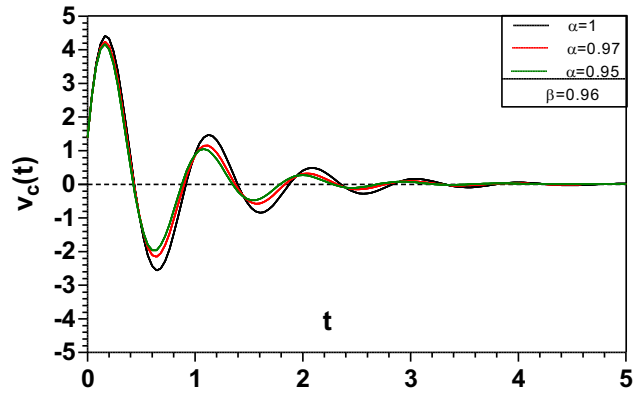


Figure 9. Numerical results for RLC circuit based on Atangana- Baleanu fractional operator; for $\alpha = 0.95, 0.97$ and 1 with $\beta = 0.95$.

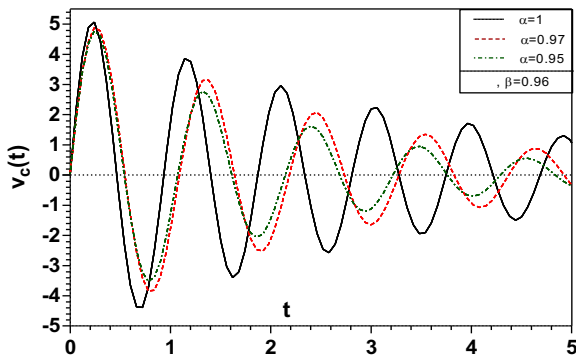


Figure7. Numerical results for RLC circuit based on Caputo fractional operator; for $\alpha = 0.95, 0.97$ and 1 with $\beta=0.96$.

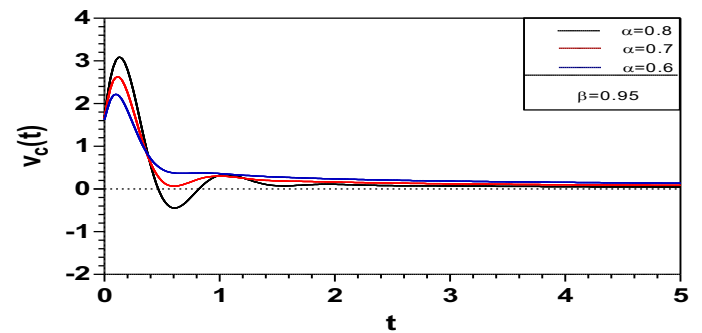


Figure10. Numerical results for RLC circuit based on Caputo-Fabrizio fractional operator; for $\alpha = 0.6, 0.7$ and 0.8 with $\beta = 0.95$.

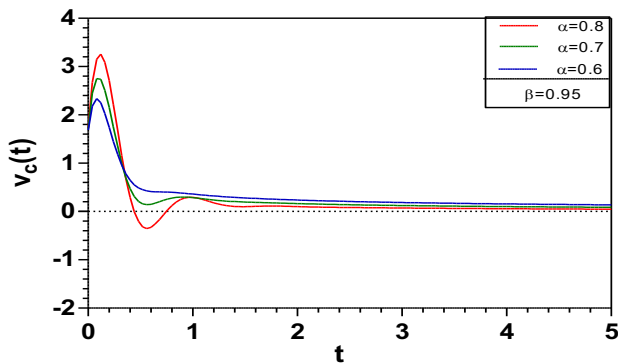


Figure 11. Numerical results for RLC circuit based on Atangana- Baleanu fractional operator; for $\alpha = 0.6, 0.7$ and 0.8 with $\beta = 0.95$.

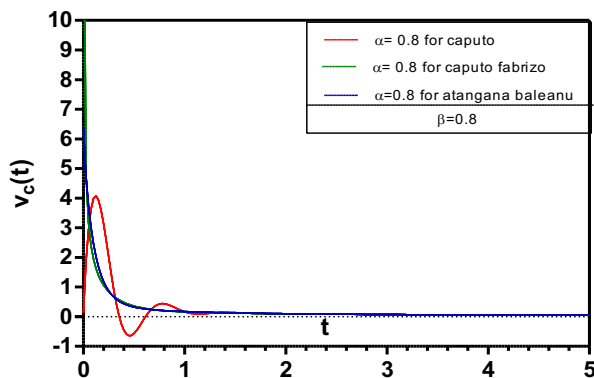


Figure 12. Numerical results for RLC circuit based on Caputo, Caputo Fabrizio and Atangana- Baleanu fractional operators; for $\alpha = \beta = 0.8$.

Conclusions

The mathematical solutions of a fractional RLC circuit were studied using Caputo, Fabrizio, and Atangana-Baleanu fractional derivatives with various values of α and β .

For all fractional operators, decreasing the fractional inductance operator (α) reduces the amplitude of the oscillation while increasing its damping capacity.

We note that from the figures, the transition between damping cases may be achieved by changing the values of fractional parameters α and β . The under damping case was obtained (from α and β which equals 0.95 to 1), over damping response (its α value between 0.6 and 0.7 and β equals 0.95) and critical damping behavior at α and β equal 0.8.

Overshoot is the divergence between the output signal and its maximum value; the greater the gap, the lower the system's performance.

As indicated in all previous figures, the responses of this system are extremely slow due to decreasing damping capacity, as illustrated in figure 5, which represents a classical case. The Caputo operator, as shown in figures (2, 6, 7 and 12), causes the system to be slow with a large overshoot. The Caputo-Fabrizio operator, as indicated in figures (3, 8, 10 and 12) and Atangana- Baleanu, as illustrated in figures (4, 9, 11 and 12), compares the response of these models with Caputo- Fabrizio and Atangana- Baleanu are very quick with a relatively modest

overshoot. As a result, the caputo operator is unsuitable for usage in this model.

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