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To the Graduate Council:

I am submitting herewith a dissertation written by Sami Said Ghezawi entitled "Verification and validation of TRAF-NETSIM model through actual field observations in Amman-Jordan." I have examined the final electronic copy of this dissertation for form and content and recommend that it be accepted in partial fulfillment of the requirements for the degree of Doctor of Philosophy, with a major in Civil Engineering.

Steve Richards, Major Professor

We have read this dissertation and recommend its acceptance:

Arun Chatterjee, John Hungerford, Fred Wegmann

Accepted for the Council:

Carolyn R. Hodges

Vice Provost and Dean of the Graduate School

(Original signatures are on file with official student records.)

To the Graduate Council:

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Auphin H. Richards

Steve Richards, Major Professor

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the

Accepted for the Council:

uminke

Associate Vice Chancellor and Dean of The Graduate School

# VERIFICATION AND VALIDATION OF TRAF-NETSIM MODEL

THROUGH ACTUAL FIELD OBSERVATIONS IN AMMAN - JORDAN

A Dissertation Presented for the Doctor of Philosophy Degree The University of Tennessee, Knoxville

> SAMI SAID GHEZAWI December 1999

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# DEDICATION

This dissertation is dedicated to my wife and two daughters

Tammi, Natasha, & Jana

#### ACKNOWLEDGMENTS

There are many people to whom I am thankful for giving me this wonderful experience. First and far most all praise and thanks are due to God for his merciful divine direction throughout my study.

I am grateful to the faculty and staff in the Civil Engineering Department for their time and assistance in various situations throughout my stay at the University of Tennessee, Knoxville. I would like to particularly thank my Dissertation Chairman Dr. Stephen Richards and Committee members Dr. Fred Wegmann, Dr. Arun Chatterjee and Dr. John Hungerford for their valuable time, assistance, and encouragement. Their kind consideration and understanding have been an incentive for the completion of the dissertation. Sincere appreciation and gratitude are extended to Dr. Wegmann and Dr. Chatterjee for giving me the invaluable opportunity as a Graduate Teaching Associate while pursuing my doctorate work.

I wish to express my appreciation to friends and colleagues at The Municipality of Greater Amman. Special thanks are due to Nasser Obidat and Maher Tarrawneh for their help and assistance during the data collection phase of this research.

Lastly, the greatest debt is owed to my parents, Said M. Ghezawi and Betty Clark Ghezawi, who having raised me in a healthy environment, made me what I am today.

#### ABSTRACT

As urban traffic continues to increase in metropolitan cities around the globe, transportation engineers are constantly attempting to improve the utilization of existent transportation systems. Their objective is to achieve maximum efficiency of these systems, in terms of movement of persons, services, and goods in a safe and convenient manner. Although congestion problems have existed in some major cities for some time, it has become a significant issue until recent years. The substantial increase in automobile ownership to meet our changing lifestyles in the last few decades, coupled with a decline of new highway construction, has stretched many roadway networks beyond their design capacity. To evaluate different traffic management strategies and their effect on the behavior of an urban street system is a very complex process due to the interrelationships between its components. Therefore, engineers have to rely on mathematical, computerbased simulation models to accurately predict the behavior of the system over a period of time. One of the most effective tools of traffic management is the application of computer simulation models to represent the traffic system, in order to determine the effects of traffic management strategies on the system's operational performance. This performance can be stated in terms of Measures of Effectiveness (MOE) on specific traffic parameters such as average vehicle speed, average travel time, vehicle stops, maximum queue length and fuel consumption. These MOE's can provide the traffic engineer with valuable insight into the responsiveness of the traffic stream to different operational strategies.

Among the many computer simulation programs, the TRAF-NETSIM, an Integrated Traffic Network Simulation model, is probably one of the most widely used

v

and accepted traffic simulation models in The United States of America. TRAF-NETSIM is a very complex microscopic simulation model, which simulates the individual car movements stochastically. This research used TRAF-NETSIM Version 5.0 to determine the applicability and adaptability of this model to assess the traffic performance in Amman – Jordan, which was accomplished by the following steps:

- A typical street network in Amman Jordan, was selected and all the required input information to run NETSIM was collected from the field (The Test Network).
- Two Measures of Effectiveness, Travel Time and Route Delay Time, were measured concurrently during the collection of traffic related input data.
- The Test Network was used to collect the following traffic parameters needed to calibrate the NETSIM model.
  - Mean Start-Up Lost Time
  - Mean Queue Discharge Headway
  - Distribution of Start-Up Lost Time
  - Distribution of Queue Discharge Headway
- Calibration on TRAF-NETSIM, in which the simulated results were compared with the observed field values using both the default and calibrated parameters.
- A second street was selected in the same city to test the performance of the calibrated model (The Validation Network).

It was found that the TRAF-NETSIM model using the default traffic parameters did not adequately predict the traffic performance in the test network. However, after changing the embedded default parameters in TRAF-NETSIM with the measured values in the field, the simulated travel times and delay times, for weekdays other than Fridays, were similar to those observed for both street networks. Conversely, for Friday the model did not predict the measured travel time and delay time within a given accuracy for both the test and validation networks. It should be brought to the reader's attention that Friday is a holiday in Jordan and that the traffic on Friday is synonymous to Sunday traffic found in the United States of America.

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# CHAPTER I

## INTRODUCTION

## Background

The Hashemite Kingdom of Jordan is situated in the northwest corner of the Arabian Peninsula. Located in the heart of the Arab world, Jordan shares its borders with Syria on the north, the Kingdom of Saudi Arabia and Iraq on the east, Saudi Arabia on the south, and on the west it borders both Palestine and Israel (figure 1-1).

Jordan is approximately 91,862 square kilometers, which is about 35,468 square miles. In comparison, it is slightly smaller than the size of the State of Indiana, and is about 4/5 the size of the State of Tennessee. The population of Jordan according to the 1997 census is estimated at about 4,322,255. (According to the Jordanian Department of Statistics), this figure has more than doubled in less than two decades since the official figure of 2,132,997, given in 1979<sup>(1)</sup>. According to the United Nations Population Fund, Jordan's average population growth rate is approximately 3.3%. Thus Jordan ranks 6<sup>th</sup> in world countries with the fastest growing population. The population increase has been boosted by a high birth rate, along with and primarily, the migration of Jordanian citizens from Saudi Arabia and other Gulf countries during the 1990-1991 Gulf War. The majority of urbanized areas are located in the Northern and Central highlands. And according t 1996 figures, about 72% of the population live in urban areas and the reminder

28% in rural areas.



# Figure1-1



Amman, the capital of Jordan lies about 40 kilometers (about 25 miles) northeast of the Dead Sea. It is the largest city in terms of population and land area within Jordan. The city of Amman is a major commercial, economic, and cultural center of about 1,231,000 people. The population of "Greater Amman", which includes the major surrounding urbanized counties (Muhafazat) is estimated at about 1,940,500 according to the 1991 official figures<sup>(1)</sup>.

The city of Amman, which was originally built on seven hills, and had spread in recent years over another five, as well as, a large area of the surrounding country-side, giving the city it's characteristic roller - coaster appearance. The size of this city, which contains about one third of the country's overall population, and its associated automobile ownership, is a major cause of concern for both traffic engineers and city planners. According to official figures, the car ownership in Jordan has dramatically grown from about 22,000 in 1970 to about 362,800 in 1997, and this figure is expected to reach 380,000 vehicles by the end of 1999. <sup>(26, 27)</sup>

The rapid increase in population and car ownership has degraded the mobility and traffic performance in Amman. Like most urbanized areas, traffic congestion on the street network is becoming an ever-increasing problem, which the road user must deal with on a daily basis. Now, more than ever, transportation engineers are applying different traffic management strategies in order to ease traffic congestion. There is a well established roadway network connecting the suburban areas with downtown Amman, with approximately 120 traffic control signals, ranging from a simple fixed control to fully actuated traffic signals. In addition, there is a good public transit system serving the main

arterial streets comprising of mini buses, jitney service and taxi cabs which serves the large majority of the working force.

## **Statement of the Problem**

As urban traffic problems continue to increase in many metropolitan cities around the globe, traffic engineers and urban planners are increasingly challenged to insure a safe and efficient transportation system. The traffic engineer's responsibility goes beyond optimization of movement on a limited network to a complete and comprehensive evaluation of different strategies on a system wide basis.

The evaluation of different alternatives on the actual street system is a very complex process due to the interrelationships between its components, which are often time consuming, labor intensive, unsafe and sometimes unrealistic to implement on the road network. Therefore, to accurately predict the impact of various geometric and traffic control schemes, traffic engineers have relied on numerical, computer-based simulation programs that can be used to imitate the behavior of the system over time.

The recent surge in technology has made personal computers extremely powerful with massive computing capabilities at a very reasonable cost. In addition, the availability of programming languages, and advances in simulation methodologies have aided in the development of a wide variety of computer models. These models give the practicing traffic engineer a practical method of developing and evaluating solutions that could vary from changing signal timings on an isolated intersection, to looking at signal progression along arterial streets or within a network. The Handbook of Computer Models for Traffic Analysis, <sup>(2)</sup> lists some of the computer models that are available for traffic engineers and

planners, which can be used to solve different transportation management problems.

The majority of computer models have been developed in the United States of America. These models have been calibrated to best describe the characteristics of the user, including drivers and pedestrian, the different vehicle mix and their operating performance. Also, many field experiments have been performed in order to validate and further enhance the credibility of the computer simulation models. In order for traffic engineers in other countries around the world to use existing simulation models in their own cities, computer simulation programs must be fine-tuned or modified to accurately represent the local environment.

The transportation system is made-up of the following three parts: The human, the vehicle, and the roadway. The road user, including drivers and pedestrians, is a very important part of the street network. The capabilities, limitations, and performance of the road user have an effect on the type, frequency, and quickness, in which a person might respond to a stimulus. Social and cultural differences from one region to another effect the behavioral and performance characteristic of humans thus it is a vital input influencing the operation of a transportation system. Therefore, driver performance measures in Amman, Jordan such as: Gap acceptance, headway, and response to traffic signals will be different when compared to driver performance in the United States.

In order to use existing simulation programs in Amman, such performance measures must be determined in the field. Furthermore, the computer simulation model should be validated and calibrated to best replicate the local driving environment.

#### **Research Scope and Objective**

Traffic engineers have been applying empirical models such as the Highway Capacity Software (HCS), to evaluate the effect of different geometric and traffic control alternatives. In such models, the basic relationships among the different variables in the model have been developed by actual field measurements. However, within the last decade, the increasing traffic demand and its accompanying congestion have become apparent in most urbanized cities and hence, no longer restricted to isolated locations or within the central business district. Consequently, traffic engineers have found that such models can not adequately provide the insight needed to address traffic related problems on a system wide basis.

The recent development in computer technology has given the practicing traffic engineer a wide selection of computer models that can be used as a tool to help manage and hopefully alleviate the traffic problems. The Network Simulation Model (abbreviated NETSIM) is an example of a computer simulation model used by traffic engineers. Although, it was originally developed for the Federal Highway Administration (FHWA), NETSIM is a very widely used and accepted traffic network simulation model among different public and private agencies in the United States of America. The Traff-Netsim software, as well as a wide variety of traffic and transportation related software, can be purchased from The Center for Microcomputers in Transportation "McTrans", University of Florida, Transportation Research Center, 512 Weil Hall, P O Box 116585, Gainesville, Florida 32611.

NETSIM a very complex model, is a microscopic, urban street network program which simulates the individual car movements stochastically. However, to use NETSIM in

Amman-Jordan, it should be modified accordingly through field experiments, to accurately

replicate the Jordanian driving environment, which is the main objective of this research.

This will be accomplished by the following:

STEP 1: Identify a typical street network in Amman (Test Network), and collect all the required input information to run NETSIM.

A- Geometric input data:

- Link length
- Number of full lanes
- Number of turning lanes
- Length of turn bays
- Lane channelization
- Lane alignment

B- Traffic input data:

- Traffic volumes at entry nodes
- Turn movements for each link
- Traffic composition
- Bus routes
- Location of bus stations

C- Control input data:

- Type of traffic control devices (Traffic signal or Traffic sign)
- Mode of traffic signal (Fixed time or Actuated)
- Phase sequence
- Number of phases and their duration

STEP 2: Collect the following measures of effectiveness (MOE's) from the test network on specific links. These will be measured concurrently during the collection of traffic input data in step 1b above.

A- Travel Time: (sec/vehicle) defined as the average link travel time for a single vehicle. <sup>(3, 15, 16)</sup>

B- Delay Time: (sec/vehicle) defined as the average delay on a link for a single vehicle (computed as the difference between the total travel time and idealized travel time for link) <sup>(3, 15, 16)</sup>

STEP 3: Collect the following traffic parameters from the Test Network to calibrate the TRAF-NETSIM model.

A- Mean Start-Up Lost Time

B- Mean Queue Discharge Headway

C-Distribution of Start-Up Lost Time

D- Distribution of Queue Discharge Headway

## STEP 4: CALIBRATION OF TRAF-NETSIM:

Model calibration involves the comparison of the simulated results with the observed field data in which changes are made to the model's embedded default parameters collected from step 3 above. (Record types 140 to 150 inclusive)

STEP 5: Repeat step 1 for a new arterial street (Validation Network).

STEP 6: Repeat step 2 for the Validation Network.

## STEP 7: MODEL VALIDATION:

The purpose of the validation phase is to determine whether or not the calibrated model is transportable. Specifically, to test if the model can simulate traffic conditions at a second network (Validation Network) without changes to any of the field collected traffic parameters from step 3 above. The only change would be the input data directly related to the characteristics of the validation network collected from step 5.

STEP 8: Compare the output of the calibrated NETSIM with the appropriate MOE's measured from step 6 (travel time and delay time) on the validation network and present the findings.

## CHAPTER II

## LITERATURE REVIEW

## Introduction

Transportation engineers have been using computer models extensively in the last couple of decades to solve many transportation problems. Some of these models were developed to simulate traffic performance on different geometric configuration. For example, SOAP, which stands for Signal Operations Analysis Package, is a traffic signal optimization model. It can be used to evaluate present timing plans or as a design tool to determine the optimal signal-timing plan for any three or four legged intersection. SOAP was programmed and designed by the Transportation Research Center at the University of Florida. TEXAS, which is an acronym for Traffic EXperimental and Analytical Simulation, is mainly used to evaluate and analyze isolated intersection ranging from a simple uncontrolled intersection to a complex signalized intersection. Thus, it is not used to optimize signal-timing plans. However, it enables researchers to evaluate proposed designs in the safety of their office without the need to implement potentially dangerous and expensive field observations. TEXAS, as the name suggests was developed by The University of Texas' Center for Highway Research at Austin, Texas. PASSER II, which stands for Progression Analysis and Signal System Evaluation Routine, was created by Texas Transportation Institute at the University of Texas A&M. The model can be used by traffic engineers to determine the optimal cycle length for progression along a signalized

arterial. TRANSYT-7F, <u>TRA</u>ffic <u>Network StudY</u> <u>T</u>ool release #7 of the FHWA, and TRAF-NETSIM, Integrated <u>TRAF</u>ic <u>NET</u>work <u>SIM</u>ulation are both traffic network simulation models. TRANSYT-7F is used to optimize signal timings for both arterial streets and grid networks. It can simulate up to 50 intersections with a maximum of 250 directional links. Where as TRAF-NETSIM, a network analysis simulation program is developed primarily to aid traffic engineers to evaluate and analyze complex network strategies. It is particularly useful in the analysis of highly integrated and dynamically controlled traffic systems. NETSIM can simulate in great detail a maximum of 250 intersections with up to 500 unidirectional links. Table 2-1 compares the different features of TRAF-NETSIM release 5.0 with some of the widely used computer models discussed earlier. <sup>(2, 4,15, 16)</sup>

## Simulation

A computer simulation is the imitation of the physical system or traffic performance over a specified time. Simulation involves the creation of the real system, and the observation of that system over time to evaluate the operating characteristics of the actual system. Since the real-world system is very complex in nature and difficult to observe, numerical, simulation models have been developed and data generated from these models is used to estimate the measures of performance of the simulation model as if a real system were actually being observed.

## Applications in simulations:

In the past decade, the increase use of personal computers and the several programming languages have made computer simulation one of the most and widely used

|    | Table                    | 2-1             |                |    |
|----|--------------------------|-----------------|----------------|----|
| Ac | omparison of TRAF-NETSIM | 15.0 with other | computer model | ls |

|                    | SOAP   | TEXAS    | PASSER II | TRANST-7F | TRAF-          |
|--------------------|--------|----------|-----------|-----------|----------------|
|                    |        |          |           |           | NETSIM         |
| Macroscopic vs.    | Macro. | Micro.   | Macro.    | Macro.    | Micro.         |
| Microscopic        |        |          |           |           |                |
| Deterministic vs.  | Deter. | Deter. & | Deter.    | Deter.    | Deter. & Stoc. |
| Stochastic         |        | Stoc.    |           |           |                |
| Evaluation vs.     | Opt.   | Eva.     | Opt.      | Opt.      | Eva.           |
| Optimization       |        |          |           |           |                |
|                    |        |          |           |           |                |
| MODEL              |        |          |           |           |                |
| FEATURES           |        |          |           |           |                |
| Simulates Isolated | Yes    | Yes      | Yes       | Yes       | Yes            |
| Intersections      |        |          |           |           |                |
| Simulates Pre-     | Yes    | Yes      | Yes       | Yes       | Yes            |
| Timed Control      |        |          |           |           |                |
| Simulates          | No     | Yes      | No        | No        | Yes            |
| Actuated Control   |        |          |           |           |                |
| Simulates          | No     | No       | Yes       | Yes       | Yes            |
| Arterial           |        |          |           |           |                |
| Simulates          | No     | No       | No        | Yes       | Yes            |
| Networks           |        |          |           |           |                |
| Simulates Stop &   | No     | Yes      | No        | Yes       | Yes            |
| Yield conditions   |        |          |           |           |                |
| Simulates          | No     | No       | No        | No        | Yes            |
| saturated          |        |          |           |           |                |
| conditions         |        | <u> </u> |           |           |                |
| Simulates Buses    | No     | No       | No        | Yes       | Yes            |
| Simulatas Dadaina  | No     | Na       | No        | No        | Vee            |
| Simulates Parking  | NO     | INO      | INO       | INO       | ies            |
| Simulates          | No     | No       | No        | No        | Vec            |
| Pedestrians        | 140    | 140      | 110       | 140       | 1 05           |
| Simulates          | No     | No       | No        | No        | Yes            |
| Lane Closures      |        | 110      | 110       | 110       | 105            |
| Simulates Intra-   | No     | No       | No        | No        | Yes            |
| Link lane changing |        |          |           |           |                |
| Simulates          | No     | No       | No        | No        | Yes            |
| Shared turn lanes  |        |          |           |           |                |
| Simulates Urban    | No     | No       | No        | No        | Yes            |
| interchanges       |        |          |           |           |                |
| Simulates detailed | No     | No       | No        | No        | Yes            |
| maneuvers within   |        |          |           |           |                |
| an intersection    |        |          |           |           |                |

tools in traffic operations analysis. Simulation can be applied (put not limited to) the following situations:

- To gain knowledge of how an actual transportation system or a specific strategy is going to perform prior to its implementation on the existing street network. The actual development of new theories or systems such as the construction of a new highway, widening an existing roadway, or even implementing certain traffic regulations such as one-way streets, establishing of a high-occupancy vehicles (HOV) lanes, etc. All of which are, very costly, unsafe, and time-consuming to implement on the actual street network.

- The need to evaluate certain measures of effectiveness on an existing facility may cause unnecessary interruptions to the actual street network. For instance, the effect of different signal plans, speed limits, and access control strategies all can be evaluated in great detail without confusing or alarming drivers.

- To test alternative designs such as a Before-and-After study under identical traffic conditions. For example, the behavior of traffic flow in the real world involves many changeable factors and complex interactions between the driver, the vehicle, and the roadway itself. Therefore, it may be highly improbable to insure identical traffic flow behavior in the field to accurately assess a Before-and-After study. However, in a computer simulation it is very easy to reproduce similar traffic volumes, and traffic composition under similar traffic conditions to evaluate several alternative system designs, assuming the simulation model is capable of producing identical traffic steam.

## Different types of simulation models:

A model can be classified as being physical or mathematical. Physical models involves' the actual construction of a model. An example of a physical model might be the building of a bridge to a scale of 1:100. On the other hand, numerical, computerbased simulation model is a particular form of a mathematical model. It is a mathematical representation of the sequence of events over time comprising a certain process. The sequence of events is repeated several times to study the outcome. Because of the availability of digital computers and the ease in performing many computations at a very high speed, mathematical simulation models are incorporated into what is known today as computer simulation models.

Simulation models are further categorized as being static or dynamic, deterministic or stochastic, event scan or time scan, and microscopic or macroscopic in nature. A brief discussion is presented.

A static simulation model represents a system at a particular point in time. Where as a dynamic simulation model represents the way in which a system changes over time? The simulation of a bank from 9:00 a.m. to 2:00 p.m. is an example of a dynamic simulation.

Simulation models that have no laws of chance incorporated into the models are classified as deterministic. Deterministic models have no randomness what so ever. An example of such models is if all the vehicles arrived at an intersection exactly 10 seconds apart. A stochastic or probabilistic model is used in the simulation of traffic systems whose state is affected by the laws of chance. The randomness in stochastic models is introduced by a random number generator; While the distribution functions describe the

relative frequencies of possible outcomes, they can be considered only as statistical estimates to the true characteristics of the model.

Simulation models are further classified as being either event scan or time scan models. With event scan models the process being analyzed is updated upon each event that occurs. On the other hand, time scan models update the process under consideration at constant time intervals. For example, in a time-scan model the position and status of vehicles in a queue at a single-pump gas station could be calculated at specified time intervals (i.e. at one second intervals), or it could be calculated each time a vehicle enters or leaves the gas station.

Furthermore simulation models are either microscopic or macroscopic in nature. Macroscopic simulation models represent traffic in terms of aggregate measures on each section of the street. Macroscopic models simulate vehicle in-groups (platoons) and report measures of effectiveness collectively. In a microscopic simulation models each vehicle is handled as a distinct entity. It is moved and monitored through the street network based on time-scan principle. This means that each movement of all the vehicles on the street network and every variable control (traffic lights) and event are updated, for example every 1 second interval. Table 2-2 summarizes the three main characteristics of traffic flow at both the macroscopic and microscopic levels.

In general, microscopic simulation models are believed to be more realistic in their description of the process being simulated. However, they normally require much more detailed information about the system being modeled in the form of input data requirements and their execution time will be substantially longer given the same computer hardware and street network.

| TRAFFIC        | MICROSCOPIC      | MACROSCOPIC           |
|----------------|------------------|-----------------------|
| CHARACTERISTIC | LEVEL            | LEVEL                 |
|                | INDIVIDUAL UNITS | GROUPS OF UNITS       |
| Speed          | Individual Speed | Average Speed         |
| <b>•</b>       | mph or km/h      | mph or km/h           |
| Flow           | Time Headway     | Flow Rates            |
|                | (seconds)        | vehicle / hr / lane   |
| Density        | Distance Headway | Density               |
|                | Spacing (feet)   | Vehicle / mile / lane |

Table 2-2 Characteristics of Traffic Flow

In summary, simulation is a very powerful tool and should be resorted to when the system under consideration is too complex to be analyzed analytically. An analytical approach to problem solving involves the use of a well-established equation to yield the answer directly. However, the increased use of simulation studies and the corresponding lack of experience on the part of some users can lead to a sort of pseudo-simulation. Researchers and decision-makers should not be misled or even fooled by the vast pile of computer printouts, and accept them as absolute truth. In fact the simulation output should be viewed with a certain amount of skepticism until it has been validated. "GIGO" or "Garbage-In Garbage-out" is a basic concept in the computer science world, which also applies to computer simulation programs.

#### Studies using NETSIM

Transportation engineers have applied NETSIM to a wide spectrum of traffic related issues. These have ranged from evaluating signal timings on an isolated intersection, to studying different traffic signal control schemes and geometric designs for an arterial or street network. The following abstracts are some of the published literature by transportation engineers that have used NETSIM to compare different design alternatives or to actual field verification of the models estimated output parameters.

Nemeth and Mekemson, 1983<sup>(7)</sup>, have applied both SOAP, a macroscopic, optimization model and NETSIM, which is a microscopic, simulation model in the analysis of a signalized intersection. They looked at three hypothetical cases. The first two involved the intersection of two two-lane highways controlled by a pre-timed and traffic-actuated two-phase traffic signal respectively. The third case involved a two four-lane intersection with left-turn bays controlled by a pre-timed multi-phase signal. In each of the above cases, about 80 different combinations of traffic volumes and left-turn percentages were analyzed. The two measures of effectiveness selected by Nemeth and Mekemson were delay and fuel consumption. The study indicated that for the first two cases, the pattern of average delay under various volumes was similar with higher values produced by NETSIM. This increase can be related to travel-time delay due to vehicles traveling along both approach and departure links as simulated by NETSIM. For the pre-timed multi-phase intersection (case3), NETSIM and SOAP produced delays that are very similar. However, NETSIM delays were larger at high traffic volumes. Due to the fact that both NETSIM and SOAP defines fuel consumption differently, the authors looked at the differences between NETSIM fuel consumption and SOAP excess fuel consumption. The report indicated that after differences in definitions had been taken into consideration, both SOAP and NETSIM fuel-consumption values were similar in all three cases. However, in their study, no grades, parking activity, different vehicle composition, or pedestrian conflicts were assumed.

Grantz and Mekemson 1990<sup>(8)</sup>, compares the macroscopically flow profiles produced by TRANSYT-7F model to the microscopically flow profiles generated by TRAF-

NETSIM. In comparing the flow profiles it appears that TRAF-NETSIM is modeling aggressive, higher speed drivers more than TRANSYT-7F. On the other hand, it seems that TRANSYT-7F is emphasizing the non-aggressive drivers trailing the platoon more than TRAF-NETSIM. However, authors point out that due to the stochastic nature of TRAF-NETSIM in assigning free flow speeds for individual vehicles. And the recognition that the version of TRAF-NETSIM used in their study did not permit vehicle lane changing to allow movement around a slower moving vehicle as the main causes of the free flow differences.

Labrum 1981 <sup>(9)</sup> describes Utah's experience with NETSIM in analyzing different traffic control problems for single intersections, arterial, and street networks. They tested the model generated traffic volumes to actual field observations on a network consisting of two intersecting arterial streets in the SALT LAKE suburban area. The study indicates that there was no significant difference in vehicle volumes at the 10% level. However, Utah's DOT has found NETSIM to be a very useful tool for engineers and have recommended it for solving a wide spectrum of problems.

Hurely and Radwan<sup>(10)</sup> wrote on the experience gained while using NETSIM by undergraduate, graduate, and faculty members at Virginia Polytechnic Institute (VPI). However, most of their research focused on determining the signal timing requirements for minimizing fuel consumption rates for isolated signalized intersection with fixed control.

Davis and Ryan<sup>(11)</sup>, describes two cases in 1979 of user experience with NETSIM (version of Netsim supplied by the FHWA in 1978). The first case, an isolated Tintersection with semi-actuated control was analyzed by NETSIM, and the simulated results where compared to actual field observations. In this study, the only MOE compared was that of queue length at the start of the green interval. NETSIM was run for 30-minutes using two

15-minute periods, each with a different seed for the random number generator. The study shows that the average queue lengths seems to be similar and that queues estimated by NETSIM were shorter than what was observed in the field. However, the variance was larger in the observed queue lengths than in NETSIM. It should be mentioned that this study used the default value of 2.1 sec/vehicle for queue discharge headway and a free flow speed of 30 mph for each link. Also, the findings were limited to only one study period with no trucks or buses present.

The second case reported by Davis and Ryan, dealt with the comparison of average delay per vehicle calculated by Webster's Technique and NETSIM on a hypothetical fourlegged intersection, with fixed time control. The study shows that the simulated average delay by NETSIM was similar or less than those computed by Webster's technique until volumes approached capacity at which NETSIM predicted higher values.

Yagar and Case, 1974 <sup>(12)</sup>, have studied and applied UTCS-1 the forerunner of NETSIM on a network in Toronto, Canada. The network consisted of an arterial street with its intersecting links. The floating-vehicle technique was used to collect field observations on travel time and speed on each link along the arterial. The study concludes that the "UTCS-1 appears to predict traffic speeds quite accurately", and that the simulated results seems to be similar when using a different seed number for the random number generator.

Robert Ferlis and Richard Worrall, <sup>(25)</sup> have applied the UTCS-1 network simulation model to three different experiments to suggest potential uses of the model as an aid to traffic engineers. The first experiment, the validation of the simulation model is presented to illustrate the high degree of conformity and reliability of the model's ability to simulate actual traffic conditions on a street network. The second experiment, the arterial

demonstration describes how the UTCS-1 can be used by researchers as a design tool to aid in the evaluation of different design schemes. The third experiment is the San Jose experiment which demonstrates the adaptability of the simulation model to different traffic conditions from those used in the validation network in Washington, D.C. Validation of the UTCS-1 Model:

The UTCS-1 network simulation model was originally calibrated for a grid network located in downtown Washington DC. The model's ability to predict traffic conditions was accomplished by setting up aerial and ground-based time-lapse photography to aid in the collection of a comprehensive set of field data which was used in the comparison of two sets of model runs, the a.m. peak and the a.m. off-peak traffic conditions. The simulation model was run three times (replications) with common sets of inputs for both the a.m. peak and a.m. off-peak conditions in order to minimize the influence of the model's stochastic variations on the data set. The simulation model was run for 32 minutes of real time for each replication. The results of the validation exercise is presented in Table 2-3, in which field measured and simulated values for different MOE's are compared.

As can be seen from the table, in the a.m. peak conditions the simulated MOE's where similar to the field observed values (all within a 2% difference) with the exception of average speed, the difference between field and simulated values was around 2.4%. However, the study indicates that the differences between field and simulated MOE's where not statistically significant at the 5 percent level. In the a.m. off peak traffic conditions, the differences are more obvious. It appears that the model had considerable underestimation during that period. The study indicates that the simulated values produced by the model where significantly different at the 1 percent level. The authors suggest that the model
| CHARACTERSTIC         | FIELD          | RUN 1<br>SIMU- D<br>LATED | DIFFER- %<br>ENCE        | RUN 2<br>SIMU- DIFFER- %<br>LATED ENCE | RUN 3<br>SIMU- DIFFER- %<br>LATED ENCE |
|-----------------------|----------------|---------------------------|--------------------------|--|--|
| Total Link Output vph |                |                           |                          |  |  |
| Peak<br>Off peak      | 36108<br>27433 | <b>36345</b><br>27731     | 237 0.7<br>298 1.1       | 36399 291 0.8<br>27930 497 1.8         | 36.345 237 0.7<br>27.731 298 1.1       |
| Vehicles in Network   |                |                           |                          |  |  |
| Peak<br>Off peak      | 328.4<br>276.4 | 327.9<br>246.3            | -0.5 -0.2<br>-30.1 -10.9 | 332.0 3.6 1.1<br>243.3 -33.1 -12.0     | 329.5 1.1 0.3<br>238.7 -37.7 -13.6     |
| Vehicle minutes       |                |                           |                          |  |  |
| Peak<br>Off peak      | 10506<br>8841  | 10502<br>7891             | -4 0.0<br>-950 -10.7     | 10616 110 1.0<br>7781 -1060 -12.0      | 10539 33 0.3<br>7634 -1207 -13.7       |
| Vehicle miles         |                |                           |                          |  |  |
| Peak<br>Off peak      | 1701<br>1285   | 1705<br>1293              | 4 0.2<br>8 0.6           | 1710 9 0.5<br>1302 17 1.3              | 1710 9 0.5<br>1306 21 1.6              |
| Total Delay veh min   |                |                           |                          |  |  |
| Peak<br>Off peak      | 6475<br>5806   | 6455<br>4831              | -20 -0.3<br>-975 -16.8   | 6561 86 1.3<br>4700 -1106 -19.0        | 6483 8 0.1<br>4541 -1265 -21.8         |
| Average travel time   |                |                           |                          |  |  |
| Peak<br>Off peak      | 5.4<br>6.4     | 5.5<br>6.0                | 0.1 1.9<br>0.4 -6.3      | 5.4 0.0 0.0<br>5.2 -1.2 -18.8          | 5.4 0.0 0.0<br>5.1 -1.3 -20.3          |
| Average speed mph     |                |                           |                          |  |  |
| Peak<br>Off peak      | 16.43<br>15.35 | 16.08<br>16.48            | -0.35 -2.1<br>1.13 7.4   | 15.99 -0.44 -2.7<br>16.88 1.53 10.0    | 16.03 -0.40 -2.4<br>16.71 1.36 8.9     |

# Table 2-3Comparison between field and simulated MOE's

seemed to impede traffic flow less than necessary in order to reproduce the field data in the off-peak traffic conditions.

The second experiment conduced by the authors was to demonstrate the possible use of the model as an aid in iterative design. The network chosen for the study was an arterial 1.1miles long in Washington, DC. Actual traffic volumes, geometry, and signal timing data were also used in this experiment. The study examined and compared selected MOE's of different design strategies to the existing arterial traffic conditions. They have looked at reversible lanes, eliminating some left turns, construction of additional lane, and different traffic signal designs. In summary, the second experiment illustrated the ability of the UTCS-1 network simulation model as a tool to aid traffic engineers in evaluating different transportation management schemes.

The third experiment chosen by the authors was to examine the different signal timing plans produced by SIGOP and TRANSYT to a street network in San Jose, California. The results of this study suggests that the signal timing produced by TRANSYT showed consistently lower delay and higher average speeds than the equivalent settings produced by SIGOP.

In conclusion, the following remarks can be drawn from the above literature:

- NETSIM is used as a tool by researchers and practitioners to evaluate a wide range of transportation related problems. Most of the studies evaluated the performance of isolated, hypothetical intersections without considering the effect of grade, different vehicle mix, or pedestrian conflicts.
- It appears that NETSIM produces higher delays and more models aggressive higher speed drivers when compared to SOAP and TRANSYT-7F respectively.

- NETSIM's simulated travel-time and speed seem to be similar to actual field conditions.
- In the original validation of the UTCS-1, the forerunner of NETSIM, actual field data was collected and compared to simulated values. The model was run three times with different random number seeds in order to reduce the variability from one simulation run to the next. It was shown that the model was able to produce similar values under peak conditions. However, the model produced considerable underestimation on some of the selected measures of effectiveness during the off peak period.
- Transportation engineers can use traffic simulation programs to gain added insight at traffic performance under a very wide range of design concepts.
- It appears that NETSIM is one of the most widely used and accepted traffic simulation models among the profession.

## **TRAF-NETSIM Model**

As the world's population reaches approximately 6 billion, global over crowding may be the most pressing issue we face as we enter the new millennium. Transportation engineers throughout the world are constantly trying to alleviate progressively greater congestion levels and traffic delays in our major metropolitan areas. Previously, traffic engineers would simply widen the existing facilities or even construct new highways to reduce traffic congestion. However, due to the increasing environmental concerns, construction cost, and right-of-way restrictions, transportation engineers must use different transportation system management (TSM) strategies in order to optimize the efficiency of the existing road network in order to harmonize the traffic congestion problems we encounter on a daily basis. To evaluate the effect of different TSM

strategies on trip patterns, transportation engineers have to examine a large portion of the street network in which a trip maker may use in order to reach his/her destination. This can be accomplished if there is a comprehensive traffic simulation model that simulates the behavior of traffic progressing along different types of street segments. For example, a person may first travel along a two lane rural road, and then a four lane divided highway or a signalized arterial and finally back to a two lane urban road, in order to reach their destination. To accomplish this idea of a single integrated simulation model, The Federal Highway Administration (FHWA) has been pursuing several simulation programs since the mid 1970's which have lead to the evolution of a system of simulation models known as TRAF.

TRAF (for integrated TRAFfic simulation models) is basically a group of simulation models which are integrated together to represent the aggregate traffic environment. Each traffic simulation model in TRAF is designed to represent traffic behavior on a particular street network. For instance, TRAF can simulate the traffic flow on an arterial street or a two-lane roadway each with a desired level of simulation detail. As can be seen from Table 2-4, TRAF consists of three microscopic and two macroscopic simulation programs.

The naming of these models is made up of a prefix and a suffix. The prefix in an indication of the type of network being simulated and the suffix shows the level of simulation detail. For example, the prefix NET, FRE and ROAD, stands for network, freeways, and two-lane road respectively. Where as the suffixes SIM and FLO shows if the simulation is microscopic or macroscopic in nature.

## Table 2-4 TRAF family of models

| TRAF                   | MICROSCOPIC | MACROSCOPIC  |
|------------------------|-------------|--------------|
| Surface Street Network | NetSim      | NetFlo 1 & 2 |
| Freeway Network        | FreSim      | FreFlo       |
| Two Lane Roads         | RoadSim     |              |

A brief description of the TRAF models is presented in the following section from TRAF user reference guide<sup>(16)</sup>.

## FRESIM:

The FRESIM simulation model is the newest addition to the TRAF family of models. It is a microscopic, time-scanning freeway simulation program. FRESIM model is capable of simulating with great detail a wide variety of design features and operational characteristics, which includes the following:

- Simulation of freeway with up to 5 through lanes
- Auxiliary lanes, lane additions, and lane drops
- Ramp metering
- Driver reaction to warning signs and geometric changes

## ROADSIM:

ROADSIM is a microscopic traffic simulation program that simulates traffic flow along a two lane rural road. Because it is of a microscopic detail each vehicle is handled as an individual entity and is moved along the traffic stream once every second of simulation clock time.

#### NETFLO:

NETFLO 1 and NETFLO 2 (also called NETFLO level 1 or level 2) are two macroscopic traffic simulation models of urban traffic. Each vehicle is modeled explicitly and its behavioral attributes such as its' free flow speed, queue discharge headway and turn movements are simulated in a stochastic (probabilistic) manner. In addition, nearly all traffic conditions encountered in an urbanized environment can be realistically simulated with either NETFLO level 1 or level 2 models. However, since those models represent the traffic condition at a macroscopic level of simulation detail, each vehicle is moved whenever an event occurs (event scan), and that vehicle is moved downstream as possible in a single motion. Macroscopic level implies that no Car-following logic is being considered by either of these traffic simulation programs. The main difference in NETFLO 1 and NETFLO 2 is that NETFLO 2 does not simulate carpools. In addition buses are treated at a lower level of simulation detail. It should be mentioned that NETFLO 2's logic adapted from TRANSYT (TRAffic Network Study Tool). However, NETFLO 2 differs from TRANSYT in its ability to handle more than one cycle length along with time varying traffic flow conditions. Also data inputs were simplified to match that of the TRAF family of models. But the main difference is that TRANSYT is used for optimizing the traffic signal plan on both arterial and grid networks, where as the TRAF family of model's are mainly used for the evaluation and analysis of different traffic control strategies. Instead of optimizing signal timings, it optimizes the utilization of transportation resources to improve the movement of people and goods in an efficient and safe manner.

#### FREFLO:

The FREFLO model is also a macroscopic simulation program, which simulates the traffic environment in terms of aggregate measures of freeways (Highways). The aggregate measures for each freeway section includes entry and exit flow rates, density, and space-mean-speeds. Furthermore, it can accommodate three types of vehicles such as buses, carpools and passenger cars, which includes trucks. High Occupancy Lanes (HOV) can be modeled explicitly as well as merging and diverging of traffic on a highway segment.

#### NETSIM:

Finally, the last model in the family of TRAF is NETSIM, which stands for <u>NET</u>work <u>SIM</u>ulation. It is a FORTRAN-based microscopic, stochastic simulation program, which models in great detail, a wide range of traffic operations in a network of surface streets. This program formally known as the UTCS-1 network simulation model was originally designed to assist in the development and evaluation of complex urban street control strategies. Ever since the introduction of the UTCS-1 model researchers have been extensively applying this simulation program to a wide variety of problem areas and it is undoubtedly the most widely used network simulation program. It's wide application can range from evaluation of traffic performance on a single isolated intersection to a very complex urban network that might have special HOV lanes oneway and two-way streets, and a full range of fixed-time and vehicle-actuated traffic signal control strategies.

Since the release of the UTCS-1 by the FHWA in 1971, which has evolved into NETSIM, it has been subsequently updated in 1973 and 1978. Netsim's name was later

changed to TRAF-NETSIM when it was integrated in to the TRAF family of models in the 1980's. And as part of TRAF, NETSIM has undergone major enhancements in the past few years, thus improving its capabilities to simulate a wide variety of transportation system management (TSM) strategies. These enhancements include the addition of actuated control logic, the ability to produce identical traffic streams, and conditional turning- movement <sup>(5)</sup>. These features are briefly described in the following:

1- Actuated Signal Logic:

TRAF-NETSIM has been updated to allow the simulation of a wide range of traffic actuated control signals. These include isolated traffic actuated signals, actuated coordination of traffic signals (free actuated mode), volume-density controllers, and semi-actuated traffic signals. Phase operations for TRAF-NETSIM actuated signals is based on the National Electrical Manufactures Association (NEMA) or type - 170 traffic controllers. In addition, this new traffic actuated signal logic allows for two types of detector groups. Each group has three different detector characteristics. The only limitation is that the total number of detectors on any link may not exceed 10. In addition detectors can be passage or presence. In passage operation, a constant 0.3 seconds pulse is generated whenever a vehicle is detected, regardless of the length of time the vehicle spends over the sensor. In presence operation, the length of the pulse generated is equivalent to the length of time a vehicle spends over the sensor. Additional traffic actuated control features have been added to TRAF-NETSIM V. 5.0 which is used by this research. The new features are left-turn extensions, lag left - turn hold, conditional service, and simultaneous gap out all of which adds to the credibility and realism of the simulation program.

TRAF-NETSIM simulation program can handle up to 100 traffic actuated control signals, with a maximum of five approaches could be specified for each signalized intersection. Additional traffic actuated control features have been added to NETSIM Version 5.0 used in this research. The new features are left-turn extensions, lag left-turn hold, conditional service, and simultaneous gap out all of which adds to the degree of conformity, reliability and realism of the simulation program.

2- Identical Traffic Streams: (ITS)

The TRAF-NETSIM simulation program uses a number of stochastic processes such as random sampling from discrete and continuous distributions to represent the traffic environment adequately. However, due to this highly attractive probabilistic nature of Netsim, the simulation output generally contains a great deal of variability from one simulation run to the next. This output variability is normally more obvious in TRAF-NETSIM due to the microscopicity of the model. <sup>(6,18,19,24)</sup> More importantly, the presence of high variability in simulation output can have a negative effect concerning the reliability and realism of the simulation model. Since the older versions of Netsim model used only one random number seed as a basis for all stochastic decisions including the determination of driver and vehicle characteristics, the traffic engineer had no control over the traffic stream and its operational and behavioral performance from one run to the next. This means that one cannot test different control strategies or alternative designs with the certainty that the changes in the output are due solely to the control variables and not to the random variations which is a characteristic of all stochastic simulation models.

Due to the limitations discussed above, and to increase the credibility and statistical validity of the simulation results, an added feature was implemented in TRAF-

NETSIM which allows the modeler to simulate the traffic stream exhibiting the same routing patterns, driver-vehicle characteristics through a series of simulation runs. To accomplish the identical traffic stream movement a unique random number seed is generated for each vehicle entering the network, which in turn is used for all stochastic decision's associated with that vehicle. This vehicle specific random seed; hereafter referred to as the 'base seed' is used to determine driver type, vehicle type, turn decisions and other behavioral and operational decisions.

TRAF-NETSIM employs two random number seeds specified by the user in entries 11 and 12 on card type 2. <sup>(16)</sup> The first random number seed is the 'base seed' and it is used to generate the traffic movement for a given simulation run. The second random number seed is the 'common seed' and it is used for all time-dependent stochastic decisions (i.e. accepting available gaps for turns, determining location and duration of events, and so on and so forth).

Based on the above, one can conclude that there are two possible scenarios in performing traffic simulation experiments with TRAF-NETSIM. The first is when the researcher is interested in comparing different system designs or operating strategies. The other is when the researcher is trying to determine the performance characteristics of an individual system, each of which are discussed below.

In the case of comparing alternatives, the user wishes to minimize the variance in the traffic performance measures of effectiveness which are due to variations in the traffic movement encountered from one simulation run to the next. This can be accomplished by keeping the same value for the base and common seeds for alternative designs in different runs, hence, the same driver/vehicle mix and routing pattern will be

simulated. Thus, the difference in the calculated MOE's between alternative simulation runs will be due solely to the differences in effectiveness on the control strategy or system design, as long as the same turn percentages, and traffic volumes are used. By employing the identical traffic stream feature in this manner, the user can compare alternative designs with the assurance that the same traffic stream in employed for all cases.

In the second case, the researcher is trying to determine the performance characteristics of an individual system. In this case, the user is interested in performing independent replications. Independent replications in simulation experiments refers to the execution of the simulation model several times for a given set of identical input data, except that the random number seed will differ from one simulation to the next. Here, the user uses a different random number 'base seed' for each simulation run and does not change any other input data. Thus, the set of independent replications would reflect the differences in the measures of effectiveness that might be observed between the traffic stream on one weekday morning to that of another. Based on the above, this research will evaluate different MOE's on the selected street networks based upon independent replications. It should be mentioned that the ability to perform independent replications in a true statistical sense was not possible with the previous versions of Netsim, because only one random seed was used for all stochastic decisions throughout the simulation program.

Finally, if the user wishes to change only the common random number seed from one simulation run to the next, the output of such runs will reflect differences due to time-dependent stochastic processes. That is, the user can simulate with traffic stream

exhibiting identical routing and driver/vehicle characteristics, but in a different traffic environment. According to A. Rathi and A. Santiago<sup>(19)</sup>, such a simulation run will generate statistics that are of no practical use in analyzing the simulation results.

3- Conditional Turning Movements:

The conditional turning movement feature is designed to constrain vehicles from making a series of unrealistic turns. For example, the user may want to restrain certain vehicles from making a series of consecutive right turns. Depending on the type of network simulated, TRAF-NETSIM users may apply conditional turning movement on certain links to restrain vehicles from going around the block.

In addition to the three major enhancements mentioned above, four new modifications to the simulation program have been made to the TRAF-NETSIM logic used in this research.

These enhancements will help to model traffic behavior more realistically and are briefly described here.

1- Intra-Link Lane Changing:

Prior to TRAF-NETSIM V. 5.0, vehicles were only allowed to change traffic lanes when they entered a new segment of a roadway. This logic is unrealistic in the real world since drivers may change lanes at any point on a link. In this new version, vehicles will know their next turn movement and will try to change into an appropriate lane for that turn movement as they travel along the network. The decision to make a lane change is based on parameters such as duration of a lane change, deceleration rates during lane changes, unacceptable headway, and cooperation of drivers to vehicles trying to perform

a lane change. All of which can be altered by the traffic engineer if he or she feels that the default values are unrealistic.

2- Shared Turn Lanes:

Shared turn logic was added to TRAF-NETSIM to further enhance its capabilities when simulating the traffic stream. Previous versions of Netsim would not allow the left most or right most lanes to service more than one turn movement. For example, a left most lane on a link approaching an intersection could only allow for either a left-turn movement or a through movement. As of TRAF-NETSIM v. 5.0, a left most turn lane can accommodate both through and left turn traffic which might be the case in many signalized intersections. Five new channelization codes where added to netsim's logic to allow all possible lane configurations to be modeled and thus improving the reliability and credibility of the simulation program.

3- Urban Interchanges:

With the added enhancement of Intra-link lane changing phenomena discussed earlier, Traf-Netsim can now simulate the behavior of traffic when performing weaving and merging maneuvers. Furthermore, this new feature gives Traf-Netsim the capability to simulate multilevel urban interchanges. This allows for more realistic presentation of multilevel interchanges using the newly developed computer animation graphics system, which will be discussed later in this chapter. In addition, the graphic capability of presenting curved links and grade separation has also been added to Traf-Netsim model. 4- Intersection Simulation "Micronodes":

Traf-Netsim has the ability to model intersections in great detail. In this version, left-turn vehicles will proceed into the intersection and will wait in the middle of the

intersection until there is a gap long enough to permit a left turn movement. In all the previous models, left turns would stop and wait at the stop line until an appropriate gap for left turn was available in opposing traffic. In addition, this new intersection logic allows for the simulation of vehicle blockage, which may be present within an intersection. Up to 20 intersections can be simulated as Micronodes.

#### The Logic Underlying NETSIM Model

TRAF-NETSIM is a microscopic stochastic simulation program which models the individual vehicular behavior in response to a wide range of traffic conditions encountered in most cities around the globe. In order to truly understand how TRAF-NETSIM works internally, a brief description of the model has been summarized and is presented below. <sup>(2,4,15,16)</sup>

Every simulation program developed describes some process that extends over time. While there are several ways of representing the passage of time, the TRAF-NETSIM model uses an interval scanning approach, which is driven by an internal clock. In TRAF-NETSIM, all system elements that vary with time are updated either at the end or during a 'one second' interval. For example, the active indications displayed by the traffic signal are updated at the end of each second. Since vehicles in the system are moved during each second if such movement is permissible. Vehicles are actually moved during the one-second interval in accordance to the car-following rules and gapacceptance process.

Vehicles enter the traffic network at entry links, at a uniform rate, and are proportional to the input volume. Upon entering the network, a right-turn vehicle and a

left-turn vehicle are assigned to the right-most lane and left-most lane respectively. Whereas a through vehicle is assigned to the lane that has the least number of vehicles. Upon entering a lane, each vehicle reacts according to the car-following rules. If the vehicle is a leader, and acceleration rate is applied to the vehicle until it reaches a freeflow speed.

Subsequent vehicles in the traffic stream will accelerate to the free flow speed similarly while maintaining a safe stopping distance between one another. The mean freeflow speed and acceleration rates for each vehicle type are user specified or impeded as defaults. The TRAF-NETSIM program can accommodate four vehicle fleet components such as automobiles, trucks, buses and carpools, each with a different acceleration, speed, vehicle length, headway, and occupancy. All of which can be modified by the user in order to reflect certain operating characteristics for a specified vehicle fleet. Even within the same vehicle fleet, say automobiles; drivers may behave somewhat differently to the same stimuli. TRAF-NETSIM manages to represent such a highly variable environment by modeling traffic stochastically, using statistical and probabilistic techniques. For example, Table 2-5 presents default values used by NETSIM for different driver types ranging from aggressive drivers to very timid drivers.

Columns 1 through 10 in Table 2-5, represents 10 different driver types and the values in each column are percentages obtained from a decile distribution. These percentages are multiplied to the mean values (user input) to reflect a specific type of driver. As each vehicle enters the network, a random number between 1 and 10 inclusive is tagged to that vehicle. This number is used to extract the proper element of the distribution representing the vehicle's driver characteristics.

| DRIVER TYPE  | 1   | 2   | 3   | 4   | 5   | 6   | 7   | 8   | 9   | 10  |
|--|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| % multiplier of<br>mean free-flow<br>speed         | 75  | 81  | 91  | 94  | 97  | 100 | 107 | 111 | 117 | 127 |
| % multiplier of<br>mean start-up lost<br>time      | 218 | 140 | 125 | 118 | 102 | 86  | 78  | 63  | 47  | 23  |
| % multiplier of<br>mean queue<br>discharge headway | 170 | 120 | 120 | 110 | 110 | 110 | 90  | 70  | 70  | 50  |

Table 2-5 Default values used by NETSIM

For example, suppose the traffic engineer specifies a mean Free-Flow speed of 60 Km/h, a mean Start-Up Lost-Time of 2.5 seconds, and a mean Queue Discharge Headway of 2.0 seconds and TRAF-NETSIM assigns a random number of 9 to a vehicle as it enters a specified link. This vehicle will have a free flow speed of 70.2 Km/h (1.17\*60), a start-up lost time of 1.18 seconds (0.47\*2.5), and a queue discharge headway of 1.40 seconds (0.70\*2.0), representing what one might call an aggressive driver. When another vehicle enters the same link, and if its random number is 4, it will have a free-flow speed of 56.4 Km/h (0.94\*60), a start-up lost time of 2.95 seconds (1.18\*2.5), and a queue discharge headway of 2.20 seconds (1.10\*2.0). Therefore, even if similar vehicles are on the same link, they may have different operating characteristics representing a wide spectrum of human behavior.

Another example of how Netsim works is to explain what happens when a lead vehicle approaches a traffic signal. The simulation program keeps track of the time and position of each vehicle in the network. Depending on the traffic signal indication facing the vehicle as it travels downstream, one of the following scenarios will occur. First, if the signal indication is red, the vehicle will reduce its speed at a deceleration rate of one foot/second<sup>2</sup> until its speed has dropped 10 percent. Then a deceleration rate of 7 feet/second<sup>2</sup> is applied until the vehicle comes to a complete stop.

The second scenario is if the traffic signal indication turns from green to yellow, the vehicle may either proceed through the intersection or stop. If the position of the vehicle is at a distance closer than the calculated safe stopping distance from the stop line, the vehicle will travel through the intersection without stopping. However, if the vehicle's position is at a distance greater than its safe stopping distance, the vehicle will stop at the stop line.

The last scenario is if the traffic signal is green, the vehicle will continue traveling along its path without stopping.

One of the objectives of this research project is to observe and collect the start-up lost time and queue discharge headway encountered by vehicles as the signal turns from red to green. This is discussed in great depth in the methodology chapter (Chapter 3). The way NETSIM discharges vehicles when the traffic signal indication turns from red to green is shown in Figure 2-1.



Figure 2-1 Vehicles Discharging from a Traffic Signal

As can be seen from figure 2-1, the first vehicle in queue will have a delay equal to the start up lost time, then it will accelerate at a specified rate until it reaches a free flow speed. The second vehicle in the queue will have a start-up lost time equal to the mean headway plus 0.5 seconds. The third vehicle in the queue will have a start-up lost time equal to the mean headway plus 0.2 seconds. The fourth and subsequent vehicles will leave the stop line at a rate equal to the mean headway.

Similar simulation logic is applied in great detail to all vehicles traversing the network as they perform different driving tasks. Such as approaching a stop sign, yield sign, or even how a lead vehicle may react to a lane obstruction due to a bus loading or unloading in its travel path.

TRAF-NETSIM model uses a number of stochastic processes such as random sampling from discrete distributions to represent the traffic environment in the real world. Many behavioral and operational decisions such as free flow speeds, acceleration rates, and gap acceptance are represented in the model as random processes. The way TRAF-NETSIM generates random numbers is presented below:

Random number generation in TRAF-NETSIM is based on linear recursive procedure. This implies that the initial random number seed forms the basis for all stochastic decisions in the model. Using a multiplicative congruence technique, the internal logic of the model will generate a sequence of random numbers by calculating the next random number from the last random number, given the initial random number seed. In the current TRAF-NETSIM model the initial value of the random number seed in user defined or default. The user is asked to provide an odd number of up to eight digits ending in 1, 3, 7, or 9. The selection of an odd number (except 5) will guarantee a full

period for the random numbers. That is, the simulation internal logic procedure will randomly generate, non-negative integer numbers between 10,001 and 99,999,999 before any number is repeated in the simulation of random processes.

#### **Input Requirements:**

TRAF-NETSIM, a microscopic stochastic simulation program, which simulates the traffic behavior and traffic control conditions of a network over a period of time, is a very data intensive program. And in light of the complexity of NETSIM'S capabilities, the developers of TRAF have strive to make the task of input data as simple as possible. They have provided a TRAF support program called TRAFEdit to ease the task of data entry. TRAFEdit is an interactive, menu-driven, micro computer based data program which allows the users to create an input data file or modify an existing input data file for the TRAF family. TRAFEdit has two component editors for data entry. The first is the "smart edit" editor, which is designed to facilitate the creation on new data sets. It is particularly useful for unfamiliar users on Netsim because it provides information about the entry fields on individual cards and will disallow many illegal entries. The second is the "Quick edit" editor, which is designed to ease the task of data "debugging" or modification changes which are required when developing an input data set.

In order to simulate the traffic behavior on a street network a detailed representation of the traffic environment must be specified by the user. Specifically, the following input data are required to run TRAF-NETSIM:

1. The Topology of the roadway system is represented in the form of nodes and unidirectional links. Nodes may represent intersections or where geometric changes

in the roadway occur (e.g. added lanes, change of grade, etc.). In addition, traffic generators; such as off street parking lots and minor streets may be represented by special purpose nodes referred to as 'sink or source' nodes. Each link represents one directional segment of a roadway or as an approach to a node.

- 2. Geometric information for each roadway segment (link). The user must specify for each link the following:
  - Number of traffic lanes.
  - Link length.
  - Number and length of left or right turn pockets.
  - Percent grade.
  - Mean start-up lost time and queue discharge headway.
  - Free-flow speed.
  - Pedestrian volumes.
  - Lane channelization.
  - Down stream node number receiving through or turning traffic.
  - Lane alignment.
- 3. Control input data for each intersection (node). For each node the type of traffic

control device should be specified in great detail. Here, the user specifies if the intersection is under sign control (Stop or Yield sign) or signal control (Pre-timed or actuated). If the intersection is under signal control additional information such as phase sequence, number of phases, duration of phases, offsets, type and location of detectors, and so on and so forth may be required to run Netsim.

4. Traffic input data. The user must specify traffic demand at entry links and source nodes in the form of flow rates (VPH). Traffic composition in terms of percent of trucks, percent of passenger cars, and percent of carpools. And surface-street turning movements at each intersection coded in terms of percent of traffic or actual flow rates.

- 5. Duration of simulation. TRAF-NETSIM allows for the simulation of traffic and traffic control strategies which may change over a period of time. The user may specify up to 19 time periods to accommodate conditions which not only differ from one location to another, but which may also change with time.
- 6. As an option, Pedestrian volumes at intersection, bus routes, bus volumes and location of bus stops may also be specified.

In addition to the input requirement just mentioned, there is a wide range of traffic parameters which may be modified by the user, specially if calibration of the simulation model is necessary, in order to more accurately represent the microscopic behavioral characteristics of the traffic environment under study. These include vehicle type specifications, vehicle responses to events in the traffic stream, characteristics of vehicle flow, and duration of certain events effecting the traffic flow.

#### Measures of Effectiveness Available from TRAF-NETSIM

After the creation of the required input data and the execution of the model, TRAF-NETSIM will produce a comprehensive set of statistical tabulations describing the different measures of effectiveness. These MOE's are on a link specific basis, aggregated over each sub-network, or specified over the entire network. In addition, TRAF-NETSIM could produce a cumulative output that provides data accumulated since the beginning of simulation excluding statistics gathered during worm-up or initialization period. Table 2-6 shows the various statistical outputs available from TRAF-NETSIM.

In addition to the intensive data output produced by TRAF-NETSIM in a statistical tabular format, an interactive computer graphics system which provides the

# Table 2-6

## Various MOE's available from TRAF-NETSIM

| LINK SPECIFIC MEASURES           | NETWORK-WIDE MEASURES                 |
|----------------------------------|---------------------------------------|
| Vehicle Miles or Kilometers      | Vehicle Miles or Kilometers           |
| Venicie Trips                    | Merring Time (uchicle hour)           |
| Woving Time (venicie-minutes)    | Moving Time (venicle-nour)            |
| Delay Time (vehicle-minutes)     | Delay Time (venicle-nour)             |
| Total Travel Time                | Total Travel Time                     |
| (vehicle-minutes)                | (vehicle-hour)                        |
| Moving/Total Time (percent)      | Moving/Total Time (percent)           |
| Total Time (minutes/ km or mile) | Total Time (minutes/mile or km)       |
| Delay Time (minutes/ km or mile) | Delay Time (minutes/mile or km)       |
| Total Travel Time                | Total Travel Time                     |
| (seconds/vehicle)                | (minutes/vehicle-trip)                |
| Delay Time (seconds/vehicle)     | Delay Time (minutes/vehicle-<br>trip) |
| Queue Time (seconds/vehicle)     | Stopped Delay Time                    |
|                                  | (minutes/vehicle-trips)               |
| Stop Time (seconds/vehicle)      | Stop Percentage                       |
| Percent Stops                    | Average Speed (mph or km/h)           |
| Average Volume (vph)             | Network Occupancy (vehicles)          |
| Average Speed (mph or km/h)      | Phase Failure                         |
| Average Occupancy (vehicles)     |                                       |
| Queue Length by lane (vehicles)  |                                       |
| Number of Lane Changes           |                                       |
| (vehicles)                       |                                       |
| Phase Failure                    |                                       |

users with means of analyzing and evaluating simulation results graphically has been added as a support program to the TRAF family of models. GTRAF version 5.0, which was developed for the Federal Highway Administration of the U.S. Department of Transportation was designed as an interactive graphics display program for a traffic simulation model known as TRAF-NETSIM version 5.0. GTRAF is subdivided into two parts: SNETG and ANETG. SNETG is used to present "static" displays in a graphical format while ANETG is used to presents "dynamic" or animated displays. Figure 2-2 shows the hierarchy of the logical structure of the GTRAF program.

GTRAF, a microcomputer-based interactive program is a very useful feature, which has been added as a support tool to graphically display the wealth of information produced by TRAF-NETSIM. This graphics program provides transportation engineers with a highly effective capability of reviewing the input data and analyzing the results generated by TRAF-NETSIM. In addition, it aides researchers in presenting their findings or recommendations to policy makers in a graphical or animated format which is an efficient, and somewhat entertaining way to gain insight into the specific traffic strategies being analyzed.

This research has relied on the animated feature in GTRAF to check the geometric input data (number of lanes, turning bays, etc.), the traffic input data (traffic volumes), and the traffic control input data (signal timings, phase sequence), to the actual data observed in the field.

In summary, TRAF\_NETSIM produces a vast amount of simulation output in the form of statistical tables, and it will be very time consuming and would require considerable skills to manually convert these statistical data presented by NETSIM into



Figure 2-2 Hierarchy of the Logical Structure of GTRAF

graphical information. In addition, there are some professionals who are reluctant to accept the idea that a computer simulation can actually describe the complex process of traffic flow at an acceptable level of accuracy and reliability. The GTRAF graphics software was designed to specifically demonstrate TRAF-NETSIM'S ability to realistically represent the traffic environment, thus increasing the validity and credibility of the simulation program.

## **Microcomputer Version of TRAF-NETSIM Model**

The TRAF-NETSIM computer program is written in FORTRAN language and was originally indented for mainframe computers. However as part of the maintenance and support activity for the TRAF simulation software, a microcomputer version of the TRAF-NETSIM simulation program has also been developed. This microcomputer version of TRAF-NETSIM requires an IBM XT, AT, with a 386 microprocessor (or compatible) with 640 kilobytes of conventional memory, a 25 megabytes of free hard disk and a monitor. To be able to view graphic outputs, a VGA (Video graphic adapter) color monitor is required along with at least 8 megabytes of extended memory (8 megabytes of RAM). Simulation time varies depending on the size of the network being simulated, the traffic volumes specified, and the hardware available on the computer running TRAF-NETSIM.

## CHAPTER III

## **RESEARCH METHODOLOGY**

## Introduction

During the past decade, transportation engineers have been utilizing computer-based simulation programs to aid in the design and evaluation of a wide range of transportation management strategies. TRAF-NETSIM, a microscopic computer simulation program, which simulates the behavior of traffic flow stochastically, is probably one of the most widely used and accepted traffic simulation model in the United States of America. The methodology utilized in this research used the TRAF-NETSIM version 5.0<sup>(16)</sup>, which is part of the TRAF family of models, to determine the adaptability and applicability of this model in predicting the traffic flow performance in Amman, Jordan. This was accomplished by measuring specific traffic parameters from an actual street segment, collecting all the required input data from the street network, comparing the simulated output with specific field measurements, calibrating the model, and validating the calibrated model in a second street network.

#### **Analytical Analysis**

A wide range of embedded, default traffic parameters in TRAF-NETSIM model reflects drivers' performance and traffic conditions that exist in The United States of America. Some of these parameters were expected to be different in Jordan and if so,

modified accordingly to better represent the local driving environment. These include driver

and vehicle response to changes in the traffic environment and characteristics of vehicle

flow.

The following is a list of the calibration parameters that are embedded within the

## TRAF-NETSIM model.

- 1. Mean value of start-up lost time for the first vehicle.
- 2. Mean queue discharge headway.
- 3. Desired free flow speed.
- 4. Distribution for start up lost time.
- 5. Distribution for queue discharge headway.
- 6. Distribution of free flow speed.
- 7. Left-turn jumper probabilities.
- 8. Maximum allowable turning speeds.
- 9. Lane switching acceptable lag.
- 10. Probability of a vehicle joining a spillback.
- 11. Left turn lagger turn probability.
- 12. Effective length of vehicle type.
- 13. Acceptable gap in near-side cross traffic for vehicles at a stop sign.
- 14. Additional time for far-side cross traffic for vehicles at a stop sign.
- 15. Amber phase response.
- 16. Acceptable gaps in oncoming traffic for left-turners.
- 17. Acceptable gaps in oncoming traffic for right-turners.
- 18. Delay due to pedestrian conflicts.
- 19. Distribution for short-term event duration.

As can be seen, there is a wide variety of embedded default parameters used

internally by NETSIM, some of which may, or may not be applicable to the local

environment being simulated. In addition, some of the parameters are more important than

other parameters, since they may have a greater impact on the selected MOE'S. To identify

which parameters meet the above criteria a detailed look at each embedded parameter is

presented.

1. Mean value of start-up lost time for 1st vehicle:

The new version of TRAF-NETSIM (release 5.0) has modified the default value of start-up lost time from 2.5 seconds to 2.0 seconds according to a recent study conducted in Maryland and published by NCHRP. <sup>(16)</sup> The start-up lost time value is the delay experienced by lead vehicles in a standing queue when the traffic signal changes from red to green. Start-up lost time is a representation of how fast or slow a driver may react to a given stimulus. This value will be measured in the field to determine the appropriate value needed to accurately calibrate the model.

## 2. Mean queue discharge headway:

The new version of TRAF-NETSIM release 5.0 has also modified the default value of mean queue discharge headway from 2.2 seconds to 1.8 seconds according to the latest study conducted in Maryland and published by NCHRP. <sup>(16)</sup> By definition, it is the time-gap between vehicles discharging from a standing queue. This value is a representation of how aggressive drivers may react as they move up to the stop line. This value will be measured in the field to determine the appropriate value needed to calibrate the NETSIM model.

#### 3. Desired free flow speed:

As each vehicle enters an approach (link), it is assigned an unimpeded free-flow speed. This is obtained by multiplying the specified unimpeded mean free-flow speed for that link by a percentage. The default used by NETSIM is 30 mph (48 km/h). The desired free flow speed does influence the travel time and delay values on a particular link.

Therefore, this parameter will be modified according to the posted speed limit on the selected street network in Amman, Jordan.

4. Distribution for start up lost time:

The first vehicle in the queue will incur some start-up lost time. This is calculated by multiplying the free-flow speed by a percent obtained from the following decile distribution.

| Driver<br>Characteristic<br>K | 1   | 2   | 3   | 4   | 5   | 6  | 7  | 8  | 9  | 10 |
|-------------------------------|-----|-----|-----|-----|-----|----|----|----|----|----|
| Link Type 1                   | 218 | 140 | 125 | 118 | 102 | 86 | 78 | 63 | 47 | 23 |
| Link Type 2                   | 258 | 190 | 143 | 114 | 95  | 76 | 57 | 38 | 29 | 0  |

For example, as a vehicle enters a link it will be assigned a random number from 1 to 10 inclusive. Assuming that this number is 7 with a start-up lost time of 2.0 seconds. Then the start-up lost time of this vehicle would be 2.0 \* 0.78 or 1.56 seconds. This decile distribution will be changed to reflect the local driving environment.

## 5. Distribution for queue discharge headway:

As each queued vehicle moves up to the stop line, it is assigned a delay until discharged, reflecting the queue discharge headway. This is calculated by multiplying the mean queue discharge headway by a percent obtained from the following decile distribution.

| Driver<br>Characteristic<br>K | 1   | 2   | 3   | 4   | 5   | 6   | 7  | 8  | 9  | 10 |
|-------------------------------|-----|-----|-----|-----|-----|-----|----|----|----|----|
| Link Type 1                   | 170 | 120 | 120 | 110 | 100 | 100 | 90 | 70 | 70 | 50 |
| Link Type 2                   | 180 | 140 | 120 | 110 | 100 | 90  | 80 | 70 | 60 | 50 |

For example, as a vehicle enters a link it will be assigned a random number from 1 to 10 inclusive. Assuming that this number is 7 and the specified mean queue discharge headway is 1.8 seconds. Then the discharge headway for this vehicle would be 1.8 \* 0.9 or 1.62 seconds. This decile distribution will be change to reflect the local driving environment.

## 6. Distribution of free flow speed

As each vehicle enters an approach (link), it is assigned a free flow speed. This is obtained by multiplying the unimpeded free-flow speed by a percent obtained from the following decile distribution.

| Driver                                | 1  | 2  | 3  | 4  | 5  | 6   | 7   | 8   | 9   | 10  |
|---------------------------------------|----|----|----|----|----|-----|-----|-----|-----|-----|
| Characteristic<br>K                   |    |    |    |    |    |     |     |     |     |     |
| % Multiplier<br>of Free-Flow<br>Speed | 75 | 81 | 91 | 94 | 97 | 100 | 107 | 111 | 117 | 127 |

For example, as a vehicle enters a link, it will be assigned a random number from 1 to 10 inclusive. Assuming that this number is 7 and a free flow speed of 30 mph was entered by the user. Then the free flow speed of this vehicle would be 30 \* 1.07 or 32.1 mph. This decile distribution seems to be reasonable and will remain the same.

#### 7. Left-turn jumper probabilities:

A left turn jumper is a vehicle that is first in queue when the signal changes from red to green, and executes the left-turn maneuver (immediately) before the on-coming queues can

discharge. This is applicable only when there is a permitted left turn and will not be applicable in Amman since all left-turns at signalized intersections have a protected phase. This embedded value will not be applicable.

## 8. Maximum allowable turning speeds:

A moving vehicle unimpeded by others must slow as they approach an intersection if they are to negotiate a right or left turning maneuver. The embedded default speeds applied deterministically are 13 fps (4 m/s) and 22 fps (7 m/s) for right and left turners respectively. This parameter will not have a great impact on travel time or delay on the arterial street. Therefore it will not be changed.

## 9. Lane switching acceptable lag:

A vehicle cannot switch lanes unless an acceptable lag is available in the target lane. The embedded default applied deterministically is 3.1 seconds. This parameter might have a significant effect on travel times and delay. However, it is difficult to measure in the field due to the limited resources available to the analyst.

#### 10. Probability of a vehicle joining a spill-back:

A vehicle, which faces a spillback condition on its receiving link at the time it is about to discharge, must decide whether to discharge or wait until the spillback ahead dissipates. The probability of a vehicle joining a spillback comprised of I vehicles is shown below:

| Ι           | 1   | 2  | 3  | 4  |
|-------------|-----|----|----|----|
| Probability | 100 | 81 | 69 | 40 |

These probabilities seems reasonable, therefore will not be changed.

11. Left turn lagger turn probability:

A left turn lagger is a queued vehicle that executes a left-turn across opposing traffic during a NO GO interval immediately following a left-turn GO (and AMBER) interval. If a left-turner is at the stop line within 2 seconds after the start of the NO GO interval, the probability that he will execute the turn movement is stored in LTLAGP(1); if within 4 seconds, in LTLAPG(2); if within 5 seconds, in LTLAGP(3). The embedded default values are:

> LTLAGP(1) = 97% LTLAGP(2) = 77% LTLAGP(3) = 37%

These probabilities seem reasonable and if modified slightly will not significantly effect the travel times and delay at the main arterial street. Therefore these values will not be changed.

12. Effective length of vehicle type:

The effective length of vehicles includes the vehicle length plus an inter-vehicle spacing of 3-ft (1m). The embedded default values are:

| Ι | Fleet<br>Component | Length              |
|---|--------------------|---------------------|
| 1 | Auto               | 20 feet (6 meters)  |
| 2 | Truck              | 37 feet (11 meters) |
| 3 | Carpool            | 20 feet (6 meters)  |
| 4 | Bus                | 50 feet (15 meters) |

These values seem reasonable since the traffic fleet in the United States and Jordan are

similar. (There are American cars, German cars, and Japanese cars etc.) However, a 5th fleet will be added since Amman has both Mini buses (20 to 25 seats) and large buses operating as public transit vehicles on the proposed network.

13. Acceptable gap in near-side cross traffic for vehicles at a stop sign:

A vehicle at a stop-line facing a STOP sign cannot discharge until an acceptable gap is available in the nearside cross street. The nearside cross street is always the approach to the left of the STOP sign approach. The acceptable gap (in tenths of a second) is based upon driver characteristic code I, and is chosen from a decile distribution. The embedded default values are:

| Driver Characteristic I | 1  | 2  | 3  | 4  | 5  | 6  | 7  | 8  | 9  | 10 |
|-------------------------|----|----|----|----|----|----|----|----|----|----|
| Acceptable Gaps         | 56 | 50 | 46 | 42 | 39 | 37 | 34 | 30 | 26 | 20 |

14. Additional time for far-side cross traffic for vehicles at a stop sign:

Time in addition to acceptable gap required for vehicles to cross the far side cross street at a STOP sign. The far side cross street is always the approach to the right of the STOP sign approach. The additional time (in tenths of a second) required to cross the far side cross street depends on the total number of lanes to be crossed, and is chosen from a decile distribution.

The embedded default values are:

| Total lanes to clear the intersection | 1  | 2  | 3  | 4  | 5  | 6  | 7  | 8  | 9  | 10 |
|---------------------------------------|----|----|----|----|----|----|----|----|----|----|
| Additional time                       | 12 | 21 | 26 | 31 | 35 | 39 | 42 | 46 | 49 | 51 |

Acceptable gaps at stop signs will not be changed because the proposed study period is the afternoon peak, and the majority of vehicles will be turning into the side streets, as opposite to turning into the main street. This is true for both of the proposed networks, since there are residential neighborhoods at both sides of the main arterial street.

## 15. Amber phase response:

The response of a lead-moving vehicle in a lane that has no queue at the instant the signal turns amber, is expressed in terms of an acceptable deceleration rate. The embedded default values, in ft/sec<sup>2</sup> are:

| Driver Characteristic K | 1  | 2  | 3  | 4  | 5 | 6 | 7 | 8 | 9 | 10 |
|-------------------------|----|----|----|----|---|---|---|---|---|----|
| Acceptable              | 21 | 18 | 15 | 12 | 9 | 7 | 6 | 5 | 4 | 4  |
| Deceleration            |    |    |    |    |   |   |   |   |   |    |

This parameter will not be changed since it will be difficult to observe due the limited resources and equipment available for the analyst.

16. Acceptable gaps in oncoming traffic for left-turners:

Acceptable gaps for left-turning vehicles in the oncoming traffic. The embedded

default values, in tenths of a second, are:

| Driver Characteristic K | 1  | 2  | 3  | 4  | 5  | 6  | 7  | 8  | 9  | 10 |
|-------------------------|----|----|----|----|----|----|----|----|----|----|
| Acceptable Gaps         | 78 | 66 | 60 | 54 | 48 | 45 | 42 | 39 | 36 | 27 |

This parameter will not apply since all left-turners in the proposed network will have their own signal phase indication.

17. Acceptable gaps in oncoming traffic for right-turners:

Acceptable gaps in oncoming traffic for right-turners to complete a RTOR maneuver. The embedded default values, in tenths of a second, are:

| Driver Characteristic 10<br>+ K | 11  | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 |
|---------------------------------|-----|----|----|----|----|----|----|----|----|----|
| Acceptable Gaps                 | 100 | 88 | 80 | 72 | 64 | 60 | 56 | 52 | 48 | 36 |

This parameter will not be applied since RTOR is prohibited in Jordan.

18. Delay due to pedestrian conflicts:

The amount of pedestrian conflict is determined by the intensity of the pedestrian flow and the elapsed time since the beginning of the green phase. There are two kinds of conflicts defined by a statistical decile distribution, along with the duration of vehicle delay, in seconds. The embedded default values are:

| I                  | 1  | 2  | 3  | 4  | 5  | 6  | 7  | 8  | 9  | 10 |
|--------------------|----|----|----|----|----|----|----|----|----|----|
| Weak Interaction   | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 1  | 2  | 6  |
| 10 + I             | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 |
| Strong Interaction | 0  | 0  | 0  | 1  | 2  | 3  | 4  | 5  | 8  | 15 |

Here, I reflect a random number between 1 and 10, inclusive. The time between strong and weak interaction is expressed in terms of the elapsed time since the beginning of green. At the beginning of the phase, strong interaction prevails. However, for the rest of that phase, weak interaction is in effect. The embedded default values for the duration of a strong pedestrian interaction are:

| Light Pedestrian Flow    | 0 seconds  |
|--------------------------|------------|
| Moderate Pedestrian Flow | 10 seconds |
| Heavy Pedestrian Flow    | 25 seconds |

The proposed network has very few, if any pedestrian crossing at the signalized intersection. Therefore these values will not be changed.

## 19. Distribution for short term event duration:

The duration of a short-term event is assigned by multiplying the specified duration (Record Type 54), for that link, by a percentage extracted from a decile distribution. A short-term event is applicable only if vehicles are illegally parked, standing, or stopping in lane 1 (Curb lane). The embedded default duration of short-term event, in percent are:

| I                     | 1  | 2  | 3  | 4  | 5  | 6  | 7   | 8   | 9   | 10  |
|-----------------------|----|----|----|----|----|----|-----|-----|-----|-----|
| % Multiplier of short | 10 | 20 | 30 | 40 | 50 | 70 | 100 | 130 | 180 | 370 |
| term event duration   |    |    |    |    |    |    |     |     |     |     |

Here, I reflect a random number between 1 and 10, inclusive. This parameter seems reasonable and will not be changed.

A brief description of the traffic parameters embedded into TRAF-NETSIM model has been presented. These parameters are treated in the model as default values representing traffic conditions that may be applicable in the absence of actual field values. This research will measure the following five traffic parameters in the field under normal driving conditions. These values will be used to calibrate the TRAF-NETSIM model to best represent the Jordanian driving environment.

1. Mean value of start-up lost time for 1st vehicle.
- 2. Mean queue discharge headway.
- 3. Desired free flow speed.
- 4. Distribution for start up lost time.
- 5. Distribution for queue discharge headway.

In order to reach the desired goals and objectives of this research mentioned in chapter I, several steps where taken and are presented in the following:

### **Network Selection**

The first task taken by this research was to identify two arterial streets in Amman -Jordan. The first arterial street was used in the evaluation and calibration of TRAF-NETSIM; the second arterial street was used in the validation of the calibrated model.

After studying and touring the streets of Amman for several days, two main arterial streets that contained both signalized and unsignalized intersections were chosen for the purpose of this research. To assure the successfulness of this project and to insure that the two arterial streets were typical streets representing traffic conditions in Amman-Jordan, the following guidelines were established to facilitate in the selection of the study sites.

- The study sites had to be within the city limits due to the willingness of The Greater Amman's Traffic Engineering Department to assist in supplying the traffic signal timings.
- 2. The street network should contain intersections that are controlled by stop signs, pre-timed and/or actuated signals, and signals with different cycle lengths.
- The street network should be traveled by a variety of automobiles such as:
  Private and public automobiles, trucks, and buses.

- 4. The street network should not contain any abnormal traffic conditions such as road maintenance, detours, or special events.
- The site should contain near-by buildings to permit for the appropriate camera setup used in the collection of all traffic input data required to run the TRAF-NETSIM simulation model.

It should be mentioned that the last criteria presented above, was related to the accuracy of the data collection technique utilized by this research. The exact location and procedural information will be discussed in more detail later in the chapter.

The first arterial street network (presented in Figure 3-1), here after referred to as the Test Network, is a 4 lane divided arterial. The major arterial street name is Mecca Street, which contains three fully actuated signalized intersections and is approximately 2500 meters long (1.562 miles).

The second arterial street network (shown in Figure 3-2), here after referred to as the Validation Network, is a 4 lane divided arterial. The major arterial name is Al-Shareef Nasser Bin Jameel Street, (or Safeway Street) which contains four actuated signalized intersections and is approximately 1500 meters long (0.937 miles).

The Test Network was utilized in the following manner:

- 1. Evaluate and test the TRAF-NETSIM model using the embedded default values.
- 2. Collect the five traffic parameters to replace the TRAF-NETSIM'S embedded default values.
- Evaluate and test the calibrated model using the parameters obtained from 2 above.



FIGURE 3-1: Test Network (Plan View)



FIGURE 3-2: Validation Network (Plan View)

The Validation Network was utilized in the following manner:

 Model Validation, the purpose of this step is to determine whether of not the calibrated model can accurately simulate traffic conditions in the Validation Network.

### Measures of Effectiveness (MOE's)

TRAF-NETSIM, a microscopic simulation program, that simulates the traffic system and predicts the effects of different traffic engineering and transportation systems management strategies on the system's operational performance, expressed in terms of measures of effectiveness. These MOE's are calculated for each specific link or for the network as a whole and are presented by the model in a statistical tabulation format. The specific measures of effectiveness selected for the evaluation of driver performance in Amman, Jordan were as follows:

1. Link Travel Time:

Travel Time is defined as the average travel time for a single vehicle on a specific link expressed in terms of seconds per vehicle.

2. Delay Time (Route Delay Time):

Delay Time is defined as the average delay time for a single vehicle on a specific link expressed in terms of seconds per vehicle.

Figure 3-3 shows the relationship between Travel Time, Moving Time, and Delay Time for vehicles travelling along a link.



Figure 3-3 Relationship between Travel Time and Delay Time

A vehicle traveling from node 1 to node 2 would enter the link at time T1 and would exit the link at time T2. Therefore the travel time for this vehicle would simply be the difference between entry time and exit time. This is expressed as:

Travel Time = T2 - T1

Assuming that there is no impedance on the road, then the vehicle would enter the link at time T1 and would exit the link at time T3, while traveling along the link at the vehicle's free flow speed. Therefore, this travel time would represent the fastest travel time possible, for this vehicle, as it travels along the link. This time is referred to Ideal Travel Time and it is expressed as:

Delay time is the time spent on the link by a vehicle in excess of its' Ideal Travel Time. This is expressed as:

Delay Time = T2 - T3

These measures of effectiveness were selected because they are good indications of the system's performance and most importantly are relatively easy to observe in the field.

### Field Study

The field study was a major step in this research project. The TRAF-NETSIM simulation program is very data intensive and requires detailed information to accurately represent the traffic environment being analyzed. The simulation program requires information concerning the geometric representations for each roadway segment, traffic volumes and turn movements at each intersection, and type of traffic control being used along with its duration.

The Municipality of Amman did not have detailed maps or traffic volumes for the selected sites. Therefore, a local surveying firm was hired to map the selected sites, which were needed to accurately code the network into TRAF-NETSIM. In addition a local video camera crew was hired to video tape all the traffic volumes at main intersections in order to produce traffic counts, turning percentages and traffic composition needed to execute accurately the TRAF-NETSIM model.

### Video Study

As mentioned earlier, a local video camera crew equipped with the state of the art equipment was hired to setup and record the traffic activities for both the Test Network and Validation Network. These tapes were later used to gather detailed information on traffic counts, turn percentages, and traffic composition through out the study period.

### Test Network:

In order to capture all of the traffic activities along the Test Network (Figure 3-1), a total of seven video cameras were setup strategically on the roofs of three buildings. Each of the buildings were close to the three signalized intersections and were elevated adequately to permit the video lens to capture all turning movements at the signalized intersections. Figure 3-4 shows the approximate locations of the buildings along with the number of video cameras and their respective angle of view. Due to social and cultural circumstances in Amman, Jordan, the official public holiday of each week, is Friday. In addition, the majority of government agencies work from 8:00 AM until 2:00 PM. The data-collection phase started on Saturday, May 10, 1997 and continued for a total of seven days until Friday, May 16, 1997. The video cameras recorded traffic volumes continuously for a period of 2 hours, from 12:30 PM until 2:30 PM of every day. At the end of seven days of video filming, a total of 49 videos each 2 hours long were collected. The videotapes were at a later date viewed by the researcher with the help of an associate, in order to retrieve traffic volumes; turning percentages and vehicle classifications along the Test Network. This phase of data viewing and recording took an extensive amount of time, since all of the videotapes were viewed several times, in order to capture all the traffic activities.



FIGURE 3-4: Building locations and number of video cameras for Test Network

#### Validation Network:

In order to video tape all the required traffic volumes from the Validation Network (Figure 3-2), a total of five video cameras were setup strategically on top of two buildings. Each building was close to two signalized intersections and their elevation allowed the video camera lens to record all the traffic volumes and turning movements, within the arterial. Figure 3-5 presents the approximate locations of the buildings, along with the number of video cameras and their prospective views. The data-collection phase for the validation network started on Saturday, June 27, 1998 and proceeded for seven days until Friday, July 3, 1998. The camera operators recorded traffic volumes continuously for a period of 2 hours from 12:30 P.M. until 2:30 P.M. of every day. At the conclusion of seven days of video filming, a total of 35 videos, each 2 hours long, had been compiled. The videotapes were at a later date viewed by the researcher and colleague, in order to recover traffic volumes, turning percentages, and vehicle classifications along the Validation Network. This phase of data viewing and recording also required an extended period of time, since each videotape had to be viewed multiple times, to capture all the traffic activities.

Prior to filming on both the Test and Validation Networks, the owners of all the selected buildings were informed by the researcher on the scope of this project. After which, permission for the filming crew to setup and access a power supply for our video cameras was granted. Each video camera was equipped with a supplementary battery, in the event of probable local power failures. In addition, all the video camera's internal clocks were calibrated to the closest minute, so that all the data collection would start at the same time.



FIGURE 3-5: Building locations and number of video cameras for Validation Network

Furthermore, to avoid any interruptions from police officers questioning the purpose of our activities, official permits for filming were obtained. This necessitated that the researcher, along with the Head of the Municipality of Amman's Traffic Department, contacted the Traffic Police Authority and informed them on the scope, location and duration of each phase of video filming, previous to the scheduled collection date.

### **Floating Car Study**

The specific measures of effectiveness selected for the evaluation of driver performance were Average Travel Time and Average Delay Time of vehicles along the arterial street. The first measure of effectiveness, The Average Travel Time, was measured in the field, in accordance to the Test Car Technique presented in the Manual of Transportation Engineering Studies<sup>(13)</sup>. A Travel Time study measures the time required to transverse a given section of the roadway. Historically, there are two driving strategies used to obtain representative travel times. The first is the "floating car" method, in which the driver attempts to approximate the average speed by passing as many vehicles, as pass the driver. The second the "average speed" method, in which the driver travels at a speed that in his opinion, is representative of the speed of the traffic at every point. In other words the driver attempts to "go with the flow" as he travels along the roadway. The latter method was chosen for this research, since it had shown by previous tests excellent correlation with actual average travel times <sup>(14)</sup>. The researcher along with a colleague, each drove their car measuring travel times between designated points along the arterial street. In order to compare the field measured and computer simulated Travel Times under similar traffic-volume conditions, the data collection was performed

simultaneously during the video camera procedure outlined in the video study above for both the Test and Validation networks. A 9-lap memory stopwatch was used to keep track of the travel times between intersection along the arterial. The driver would start the stopwatch at the beginning of the test site and would press the lap button at successive control points along the route. The driver would then record the lap times on a designated worksheet at the end of each run. The test runs started at different time points in the signal cycle, to avoid having all trips be a first in the platoon placement. The number of runs recorded on the Test Network was 7 runs per direction (WB, EB) and on the Validation Network ranged from 8 to 10 runs per direction of travel (NB, SB) per recording day. The statistical analysis of the Travel Time Study is presented in the next chapter.

### **Calibration Parameters**

A brief description of the traffic parameters embedded into TRAF-NETSIM model was presented in the Analytical Analysis section. These embedded parameters are treated in the model as default values representing traffic conditions that may be applicable in the absence of actual field values. This research will measure the Mean Discharge Headway and the Mean Start-Up lost time along with their respective distributions in the field under normal driving conditions. These modified or calibrated traffic parameters will replace the default values in TRAF-NETSIM in order to calibrate the simulation model.

### 1. Mean Discharge Headway (Saturation Headway)

In order to collect Average Discharge Headway's at intersections a Saturation Flow

study using a stopwatch was performed. This study was accomplished by observing vehicle's discharging from a link when the signal turns from red to green. The observer situated on the rooftop of a three-story building located near an approach to a signalized intersection measured Discharge Headway's of passenger cars. This assured a clear view of the approach being observed, the stop line, and the signal indication. In addition, it made the observer extremely inconspicuous, thereby minimizing any disturbance in the natural behavior of traffic flow. The observer started the stop watch when the rear axle of the third vehicle in a queue, that had been stationary while waiting for the green phase crossed the stop line, and stopped the stop watch when the rear axle of the seventh, eighth, or ninth vehicle in queue, crossed the stop line (which was the last vehicle in the stopped queue at the instant the signal turned green). This study was performed mid-week during the month of April on Monday the 28<sup>th</sup>, Tuesday the 29<sup>th</sup>, and Wednesday the 30<sup>th</sup>, 1997. This study followed the procedure for studying saturation flow with a stopwatch outlined in both the Manual of Transportation Engineering Studies, and Traffic Engineering Handbook. <sup>(13,14)</sup> The statistical analysis for the mean discharge headway is presented in the next chapter.

#### 2. Mean Start-Up Lost Time

Start-up lost time by definition is that time that occurs between the instant the green signal indication starts and the queue begins moving efficiently. Therefore, Start-up lost time for the first vehicle in queue when the signal turns to green can be computed by subtracting the difference in time between the start of the green phase and the passing of the rear axle of the first vehicle in queue. This study was performed simultaneously during the measurement of the Mean Discharge Headway discussed above. The observer measured the

Start-up lost time for the first vehicle by starting the stopwatch when the signal turned from green to red and stopped the stopwatch when the rear axle of the same vehicle crossed the stop line. The statistical analysis of the Start-Up Lost Time study along with its distribution is presented in the next chapter. It should be mentioned that this study followed the procedure for Start-Up Lost Time Studies as outlined in the Manual of Transportation Engineering Studies.<sup>(13)</sup> The statistical inquiry of this study is discussed in the Statistical Analysis Chapter.

#### **Simulation Study**

The TRAF-NETSIM model, which simulates the behavior of individual drivervehicle combinations in an urban street network, is a microscopic, stochastic simulation program. The simulation output produced by TRAF-NETSIM contains a great deal of variability from one simulation run to the next. This variability is present in the model due to the highly attractive probabilistic nature in TRAF-NETSIM and tends to be more apparent in microscopic simulation programs. To reduce the variability in the model's generated output, which can have a negative effect concerning the reliability and realism of the simulation model, a new feature was added to the TRAF-NETSIM model that allows the users to simulate with traffic streams exhibiting the same routing patterns and driver-vehicle combinations. This new feature, the Identical Traffic Streams, which was discussed in depth in chapter II, allowed the user to specify two random numbers seeds to control all stochastic decisions. The first random number seed is the "base seed" and is used to generate the traffic movement for a given simulation run. The second random number seed is the 'common

seed' and is used for all time-dependent stochastic decisions (i.e. accepting available gaps for turns, determining location and duration of events, etc.).

In order to reduce the variance between simulation runs, this research will use multiple independent replications. Independent replications in simulation experiments refers to the execution of the simulation model several times for a given set of identical input data, except the random number seed is changed between runs <sup>(19)</sup>. This research will use a set of identical random numbers for the "base seed" for each simulation run and will not change any other input data. This variance reduction technique is known as the Common Random Numbers (CRN) reduction procedure in simulation experiments' <sup>(18,28)</sup>. It should be emphasized that the reason for making several runs in TRAF-NETSIM is to increase the probability that the mean of the runs is accurately representative of the mean of the distribution, thus obtaining more reliable results. <sup>(15)</sup> However, other issues concerning the statistical aspects of simulation experiments have not been answered. This research will attempt to resolve issues of concerns such as:

- How many simulation runs should be made?
- How long should each simulation run be?
- How long should the initialization period be?

In order to get meaningful simulation results with a desired level of accuracy these questions will be addressed in the Statistical Analysis presented in the next chapter.

### Input Data

TRAF-NETSIM, a microscopic stochastic simulation program, which simulates the traffic behavior and traffic control conditions of a network over a period of time, is a

very data intensive program. In order to simulate the traffic behavior on both the Test Network and the Validation Network, a detailed representation of the traffic environment had to be specified. Specifically, the following input data were required to run TRAF-NETSIM model.

1- The Topology of the Network.

The topology of both arterial streets in the form of nodes and uni-directional links was specified. Nodes represented intersections or where geometric changes in the roadway occurred (e.g. added lanes, change of grade, etc.). In addition, each link represented one directional segment of a roadway or as an approach to a node. Figures 3-6 and 3-7 shows both the Test and Validation Street Networks respectively, in the form of Link-Node diagrams.

2- Geometric' for each roadway segment (link).

The following was specified for each link through out the arterial street network:

- Number of traffic lanes.
- Link length.
- Number and length of left or right turn pockets.
- Percent grade.
- Mean start-up lost time, queue discharge headway, and free-flow speed.
- Lane channelization.
- Down stream node number receiving through or turning traffic.
- Lane alignment.



FIGURE 3-6: Test Network in the form of Link-Node diagram





3. Control input data for each intersection (node).

For each node the type of traffic control device was specified in great detail. Both arterial street networks had intersections controlled by stop signs and actuated traffic signals. For those intersections under traffic signal control, additional information such as phase sequence, number of phases, duration of phases, offsets, type and location of detectors, and so forth and so on, was required to run TRAF-NETSIM. The test and validation networks had three and four fully actuated traffic signals respectively. The Amman Traffic Engineering Department supplied signal timings for all the signalized intersections on both arterial streets. Tables 3-1 and 3-2 shows the signal timing on both the test and validation networks.

## 4. Traffic Volumes.

This research collected all the required traffic volume data using video cameras located at advantage points to capture the traffic volumes through out the arterial street. The traffic demand at entry links and source nodes were defined in the form of flow rates (VPH); surface street turning movements at each intersection were also coded in terms of percent of traffic. In addition, traffic composition in terms of percent of trucks, and percent of passenger cars were also coded into the TRAF-NETSIM simulation model for both street networks. Tables 3-3 and 3-4 shows a summary of total traffic volumes expressed in VPH during the first (12:30 - 13:30) and second hour (13:30 - 14:30) of data collection on both the test and validation networks.

## TABLE 3-1

# Signal Timing for the Test Network

|                               |           |      | TEST NETV | WORK ( MECO | CA STREE         | Г)       |            |         |
|-------------------------------|-----------|------|-----------|-------------|------------------|----------|------------|---------|
|                               |           |      | JABER IN  | FERSECTION  | (NODE 10         | 0)       |            |         |
| Phase                         | From node |      | To node   |             | Stage Tim        | es (sec) | Amber      | All Red |
|                               |           | Left | Through   | Right       | Min.             | Max.     | Time (sec) | (sec)   |
| Α                             | 225       | 102  | 103       |             | 7.0              | 30.0     | 3.0        | 1.0     |
| В                             | 225       |      | 103       |             | 7.0              | 25.0     | 3.0        | 1.0     |
|                               | 103       |      | 104       | -           |                  |          |            |         |
| С                             | 102       | 103  |           | 104         | 7.0              | 17.0     | 3.0        | 1.0     |
|                               | ·         |      | KILO INT  | ERSECTION ( | NODE 200         | )        |            |         |
| Phase                         | From node |      | To node   |             | Stage Tin        | ne (sec) | Amber      | All Red |
|                               |           | Left | Through   | Right       | Min.             | Max.     | Time (sec) | (sec)   |
| Α                             | 201       | 212  | 210       | 122         | 6.0              | 25.0     | 3.0        | 1.0     |
| В                             | 335       | 202  | 122       | 201         | 6.0              | 30.0     | 3.0        | 1.0     |
| С                             | 202       | 122  | 201       | 212         | 6.0              | 20.0     | 3.0        | 1.0     |
| D                             | 122       | 201  | 212       | 202         | 6.0              | 35.0     | 3.0        | 1.0     |
| RABIA INTERSECTION (NODE 300) |           |      |           |             |                  |          |            |         |
| Phase                         | From node |      | To node   |             | Stage Time (sec) |          | Amber      | All Red |
|                               |           | Left | Through   | Right       | Min.             | Max.     | Time (sec) | (sec)   |
| Α                             | 308       | 302  | 331       | 303         | 7.0              | 30.0     | 3.0        | 1.0     |
| В                             | 302       | 331  | 303       | 308         | 7.0              | 20.0     | 3.0        | 1.0     |
| С                             | 224       | 303  | 308       | 302         | 7.0              | 30.0     | 3.0        | 1.0     |
| D                             | 303       | 308  | 302       | 331         | 7.0              | 20.0     | 3.0        | 1.0     |
|                               |           |      |           |             |                  |          |            |         |

# TABLE 3-2

# Signal Timing for the Validation Network

|                                 |           | VALI | DATION NI | ETWORK ( SA | FEWAY     | STREET)   |            |         |
|---------------------------------|-----------|------|-----------|-------------|-----------|-----------|------------|---------|
|                                 |           | А    | BU ANZ 1  | INTERSECTI  | ON (NODE  | E 100)    |            |         |
| Phase                           | From node |      | To node   |             | Stage Tir | nes (sec) | Amber      | All Red |
|                                 |           | Left | Through   | Right       | Min.      | Max.      | Time (sec) | (sec)   |
| Α                               | 104       |      | 200       |             | 7.0       | 30.0      | 3.0        | 1.0     |
|                                 | 200       |      | 104       | 101         |           |           |            |         |
| В                               | 101       | 200  |           | 104         | 7.0       | 25.0      | 3.0        | 1.0     |
| С                               | 104       | 101  | 200       |             | 5.0       | 20.0      | 3.0        | 1.0     |
|                                 | <u> </u>  | A    | BU ANZ 2  | INTERSECTIO | ON (NODE  | 200)      |            |         |
| Phase                           | From node |      | To node   |             | Stage Ti  | me (sec)  | Amber      | All Red |
|                                 |           | Left | Through   | Right       | Min.      | Max.      | Time (sec) | (sec)   |
| Α                               | 220       |      | 100       |             | 7.0       | 30.0      | 3.0        | 1.0     |
|                                 | 100       |      | 220       |             |           |           |            |         |
| В                               | 202       | 100  | 201       | 220         | 7.0       | 25.0      | 3.0        | 1.0     |
| С                               | 220       | 202  |           |             | 5.0       | 20.0      | 3.0        | 1.0     |
|                                 | 100       | 201  |           |             |           |           |            |         |
|                                 |           | EM   | IBASEDOR  | INTERSECT   | ION (NOE  | DE 300)   |            |         |
| Phase                           | From node |      | To node   |             | Stage Ti  | me (sec)  | Amber      | All Red |
|                                 |           | Left | Through   | Right       | Min.      | Max.      | Time (sec) | (sec)   |
| Α                               | 310       | 301  | 400       | 302         | 5.0       | 10.0      | 3.0        | 1.0     |
| В                               | 310       | -    | 400       | 302         | 5.0       | 80.0      | 3.0        | 1.0     |
|                                 | 400       |      | 310       | 301         |           |           |            |         |
| С                               | 400       | 302  | 310       | 301         | 5.0       | 30.0      | 3.0        | 1.0     |
| D                               | 302       | 310  | 301       | 400         | 5.0       | 15.0      | 3.0        | 1.0     |
| SAFEWAY INTERSECTION (NODE 400) |           |      |           |             |           |           |            |         |
| Phase                           | From node |      | To node   |             | Stage T   | ime (sec) | Amber      | All Red |
|                                 |           | Left | Through   | Right       | Min.      | Max.      | Time (sec) | (sec)   |
| Α                               | 300       | 401  | 403       |             | 5.0       | 40.0      | 3.0        | 1.0     |
| В                               | 300       |      | 403       |             | 5.0       | 50.0      | 3.0        | 1.0     |
|                                 | 403       |      | 300       |             |           |           |            |         |
| C                               | 401       | 403  |           | 300         | 5.0       | 45.0      | 3.0        | 1.0     |
|                                 |           |      |           |             |           |           |            |         |

|                           |                  |                                  |            | ESTIMA      | TED A    | 10         | EAS               | TWEST      | DBC | CTON | 1000       |             |            |              |      |             |            |          |            |           | ſ   |
|---------------------------|------------------|----------------------------------|------------|-------------|----------|------------|-------------------|------------|-----|------|------------|-------------|------------|--------------|------|-------------|------------|----------|------------|-----------|-----|
|                           |                  | SATURD                           | AY         |             | SUNDAY   |            |                   | MONDAY     |     |      | THESTAY    |             |            | VELVICO      | T AN |             | A COCO     | ,        | ľ          |           | Ī   |
| <b>IABER INTERSECTION</b> |                  | HdV                              |            |             | Hdv      |            |                   | Hd         | T   |      | APH<br>VPH |             |            | VBU          |      |             | HURSUA     |          |            | RIDAY     | T   |
| NODE 100                  | -                | T                                | R          | -           | +        | œ          | _                 | -          | α   | ~    | -          | a           | ~          | Ē            | ٥    | -           |            |          | -          | Η,        | -   |
| FROM SOUTH 1ST H          | 225              |                                  | 164        | 242         |          | 850        | 575               |            | 841 | 547  |            | 197         | 88         |              | 888  | 513         |            | 872      | 298        | -         | 뜅   |
| HONZ                      | 200              |                                  | 922        | 8           |          | 876        | 619               |            | 878 | 619  |            | 885         | 900        |              | 861  | <b>5</b> 82 |            | 8        | 342        |           | 778 |
| FROM EAST 1ST HI          |                  | 67.2                             |            | 1024        | 172      |            | ₫<br>870          | 780        |     | 020  | 159        |             | 971        | 725          |      | 1107        | 808        |          | 693        | 368       |     |
| HONZ                      |                  |                                  |            | 1197        | 895      |            | 1225              | 910        |     | 112  | 867        |             | 1213       | 926          |      | 1305        | 818        | _        | 988<br>988 | 432       |     |
| HOM WEST 1SI H            | ~                | 55                               | 244        |             | 944      | 221        |                   | 973        | 290 |      | 877        | 252         |            | 929          | 259  |             | 1067       | 335      |            | 427       | 61  |
| HONE                      | 8                | 1001                             | 326        |             | 1009     | 302        |                   | 1025       | 20  |      | 1069       | 282         |            | 9 <b>9</b> 5 | 297  |             | 1079       | 80       |            | 5         | 155 |
| PERCENT TRUCKS            |                  | 1% to 2%                         |            |             | 1% 10.2% |            |                   | 1% to 2%   |     |      | 1% to 2%   |             |            | 1%           |      |             | % to 2%    |          |            | 19        |     |
| KILO INTERSECTION         |                  |                                  |            |             |          |            |                   |            |     |      |            |             |            |              |      |             |            |          |            |           |     |
| YODE 200                  |                  | F                                | æ          | -           | ۲        | ď          | ر                 | -4         | œ   |      | +          | α           |            |              | a    | _           | F          | ۵        | -          | ۲         | 0   |
| FROM NORTH 1ST HI         | 234              | 494                              | 522        | <b>8</b> 09 | 417      | 386        | 669               | 433        | 580 | 809  | 397        | <b>2</b> 02 | 624        | 405          | 476  | 803         | 474        | 553      | 113        | 2AA       | ž,  |
| 2ND H                     | 8 721            | 516                              | 527        | <b>9</b> 80 | 521      | 557        | 753               | 539        | 584 | 732  | 497        | 19          | 502        | 504          | 578  | 824         |            | 302      | 2 9        | 9 9 9     |     |
| FROM SOUTH 1ST HI         | 1 258            | 239                              | 2          | 233         | 436      | 8          | 289               | 508        | 8   | 271  | 520        | 82          | 239        | 515          | 8    | 248         | 22         | 52       | ₽Ę         | 282       | 64  |
| HONZ                      | 320              | 886                              | 8          | 8           | 800      | 2          | 88                | 909        | ន   | 284  | 569        | 8           | 284        | 598          | 68   | 277         | 617        | 8        | 202        | 414       | 5 2 |
| FROM EAST 1ST HI          | 8<br>2<br>2<br>2 | 873                              | 287        | 4           | 8        | 208        | 225               | 920        | 357 | 399  | 855        | <b>296</b>  | 458        | 858          | 290  | 443         | 8          | ŝ        | 283        | \$32<br>4 | 9   |
| HONZ                      | R 49/            | /96                              | ŝ          | 242         | 1120     | 291        | 576               | 1082       | æ   | 570  | 1083       | 381         | 570        | 1099         | 320  | 601         | 1125       | 316      | 373        | 213       | ę   |
| FROM WEST 1ST HI          | 1197             | 5                                | 8          | <b>6</b> 83 | 673      | 3          | 1322              | 835        | 8   | 1214 | 762        | 7           | 1261       | 715          | 83   | 1247        | 827        | 8        | 89         | 452       | 5   |
| HONZ                      |                  | 633                              | 3          | 1376        | 282      | 8          | 1419              | 848        | 8   | 1355 | 818        | 8           | 1367       | 818          | 65   | 1456        | 840        | 72       | 819        | 1084      | 6   |
| PERCENT TRUCKS            |                  | 1% 10 2%                         |            |             | 1% to 2% |            |                   | 3%         |     |      | % to 3%    |             | -          | % to 2%      |      | -           | % to 2%    |          |            | 1%        |     |
| <b>PABIA INTERSECTION</b> |                  |                                  |            |             |          | •          |                   |            |     |      |            | ·           |            |              |      |             |            |          |            |           |     |
| KODE 300                  | ۲<br>            | н                                | æ          |             | -        | æ          |                   | F          | α   |      | F          | α           | -          | ۲            | 0    | -           | ۰          | 4        | -          | ,         | 1   |
| FROM NORTH 1ST HE         | 46               | 353                              | ŝ          | 213         | 327      | 32         | 228               | 398        | ŧ   | 186  | 393        | 75          | 202        | 398          | 4    | 201         | 385        | 2 9      | 12         | 240       | r S |
| HONZ                      | 22               | 433                              | 8          | 8           | 379      | 4          | 237               | 370        | 2   | 208  | 366        | 51          | 224        | 387          | 4    | 224         | 439        | 2        | 143        | 247       | 3 8 |
| IROM SOUTH IST HI         | 197              | 20                               | Ŧ          | 172         | 88       | 133<br>133 | 229               | 900<br>900 | 141 | 83   | 334        | ŝ           | 217        | 314          | 148  | 185         | 344        | 8        | 19         | 226       | 8   |
|                           | 12               | 474                              | 2          | 8           | 1        |            |                   | 8          | 16  | 8    | 442        | 133         | 312        | 352          | 148  | 233         | \$         | 150      | 271        | 230       | 77  |
|                           |                  | 90<br>10<br>10<br>10<br>10<br>10 | 1          | 224         | 210      | <u> </u>   | 8                 | 949<br>949 | 246 | 8    | 58         | 218         | 512        | 825          | 540  | 620         | 928        | 286      | 344        | 173       | 131 |
| BOM WEST 181 ME           | ő                | 767                              | 5          | Ş           | 101      |            |                   | 100        |     |      | 1001       |             | 8          | 10/4         | 816  | 2           | 186        | 100      | 32         | R         | 147 |
| HONZ                      | 388              | 848                              | 1 <u>8</u> | 286         | 143      | 35         | 3.5               | 8          | 81  | 5 S  | 80         |             | 908<br>978 | 114          | 124  | 311         | <b>2</b> 8 | <u>8</u> | ₹<br>1     | 442       | 79  |
| PERCENT TRUCKS            |                  | *                                |            |             | 1% to 2% |            |                   | % to 2%    |     |      | 20         |             | 2          | 101          | 8    | 502         | 10         |          | 17         | 280       | 8   |
|                           |                  |                                  |            |             |          |            |                   |            |     |      | 2          |             | -          | e 7 01 e     | -    | -           | ¥ 20 5%    |          |            | ž         |     |
|                           | z                |                                  |            |             |          | 1          |                   |            |     |      | 4.<br>+    |             |            |              | *    |             |            |          |            |           |     |
|                           | ¢                |                                  |            |             | ŧ        |            | ц<br>Зорг<br>Сорг |            |     |      | NODE       |             |            | Τ            | NODE |             |            |          |            |           |     |
|                           | ۲<br>ک           | ~                                |            |             | ł        | Ī          | 3                 |            |     | Ī    | 22         |             |            | Ĩ            | ĝ    |             | •          |          |            |           | _   |
|                           | \$               |                                  |            |             |          |            | ••                |            |     | 1    | •          |             |            | ı            |      | _           |            |          |            |           | _   |
|                           |                  |                                  |            |             |          |            |                   |            |     |      |            |             |            |              |      |             |            |          |            |           |     |

TABLE 3-3 Tebular Summary of Vehicle Countis Test Network (Meoca

|                                |                  |                      |                  |                | ESTIMA       | TED A        | 10         | BR FA        | STAMEST      |            | NOILO        | - 36 m                 |          |                  |                |   |              |                          |                |               |             | I          |
|--------------------------------|------------------|----------------------|------------------|----------------|--------------|--------------|------------|--------------|--------------|------------|--------------|------------------------|----------|------------------|----------------|---|--------------|--------------------------|----------------|---------------|-------------|------------|
|                                |                  |                      | SATURD           | X              |              | SUNDAY       |            |              | MONDAY       |            |              | TUESDAY                |          |                  | VEDAESI        | ~   | -            | A COOL II                | ł              | ľ             |             |            |
| ABU ANZ 1 INTERSE              | CTION            | -                    | ₹ı               | (              |              | Hdy          |            |              | ΗdΛ          |            |              | ΗdΛ                    |          |                  | HHA            | ŧ   |              | HdA                      |                | 1             | VPUAY       | Τ          |
| FROM NORTH                     | 1ST HR           | 138                  |                  | z Ş            | 782          |              |            |              | H            | <u>ه</u>   | 4            | -                      | æ        | -                | Н              | 2   | -            | -                        | R              | -             | -           | œ          |
|                                | 2ND HR           | 8                    |                  | 8              | 33           |              | <u>5</u> 8 | 87<br>192    |              | 107        | 9 9<br>9 9   |                        | £ 8      | 755              |                | 23  | 797          |                          | 126            | 89<br>198     |             | 6          |
| FROM EAST                      | 1ST HR<br>2ND HR |                      | 1183<br>1084     | 814<br>RdB     |              | 1206         | 86         |              | 1273         | 82<br>82   |              | 1118                   | 86       |                  | 1227           | 8   | 22           | 1298                     | 1010           | 2             | 559         | R          |
| FROM WEST                      | 18T HR           | 334                  | 1032             |                | 968<br>306   | 8            | 840        | 385          | 1078         | 822        | 408          | 1141                   | 88       | 176              | 1963           | 852   |              | 1106                     | 824            |               | 570         | 421        |
| DENCENE TOUCO                  | 2ND HR           | 333                  | 950              |                | 407          | 206          |            |              | 926<br>926   |            | 9 SS         | 802<br>802             |          | 5 Q              | £2 <b>6</b> 8  |   | 362<br>438   | 1209<br>1107             |                | <u>ដ</u> ្ឋ ខ | 495<br>50   |            |
| FERCENT INUCKS                 | T                |                      | 17 10 2%         | T              |              | *            |            |              | 1% to 2%     |            |              | 1% to 2%               |          |                  | 7              |   |              | 2%                       | +-             |               | ž           | T          |
| ABU ANZ 2 INTERSEC<br>NODE 200 | CTION            |                      |                  |                |              |              |            |              |              |            |              |                        |          |                  |                |   |              |                          |                |               |             |            |
| FROM SOUTH                     | 1ST HR<br>2ND HR | 324<br>313           | ₽ <del>4</del>   | <del>4</del> 6 | 322<br>280   | 84           | 42         | 367          | 8            | 88         | 69 E         | 82                     | 64       | 372              | 33             | 8   | 393          | 42                       | 84             | 161           | 8           | 26         |
| FROM EAST                      | 1ST HR           | 116<br>116           | 1624             | 28             | ₿.           | 1763         | 81         | £            | 1 <u>8</u>   | <b>9</b>   | 116          | 1733                   | 21<br>21 | <b>8</b> 8       | 30<br>1786     |   | 88           | <del>1</del> 851<br>1851 | <del>9</del> 4 | 8             | 10          | 27         |
| FROM WEST                      | 18T HR           | 8                    | ŝ                | 3 5 9          | 8            | 1414         | 11         | 8            | 1619         | នាន        | 37           | 1680<br>1523           | 28<br>67 | 6년 두             | 1575<br>1534   | ম ৰ   | 5 <u>5</u> % | 1561<br>1507             | 23             | 85            | 943         | 9          |
| PERCENT TRUCKB                 | HHAN             | F                    | 1411             | 2              | Ş            | 1423         | 8          | 31           | 1511         | 8          | 9            | 1380                   | 7        | 35               | 1449           | 22  | 8            | 1541                     | 3 89           | 16<br>16      | 819         | 3 5        |
|                                | T                |                      | 27721            |                |              | 12 10 27     |            |              | 17.10 2%     | Ť          |              | *                      | ╋        |                  | % to 2%        |   |              | 2%                       |                |               | 1%          |            |
| AMBASSADOR INTER<br>NODE 300   | SECTION          |                      |                  |                |              |              |            |              |              |            |              |                        |          |                  |                |   |              |                          |                |               |             |            |
| FROM NORTH                     | 1ST HR<br>2ND HR |                      |                  | <u>8</u> 2     |              |              | 191<br>194 |              |              | 12         |              |                        | 8        |                  |                | 153   |              |                          | 210            |               |             | 2          |
| FROM SOUTH                     | IST HR           | 256<br>235           | 88               | 1011<br>1215   | 275          | <b>4</b> %   | 1092       | <b>583</b>   | 88           | <u>8</u>   | 252          | 8                      | 1073     | 245              | 29             | 10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>1 | 284          | 33                       | 152            | 142           | ₽           | 卷ۇ         |
| FROM EAST                      | IST HR           | 942<br>942           | 1463             | 8              | 282          | 1556         | 8          | 885          | 1620         | ន្តីន      | 102          | 1531                   | 714/     | 212              | 25<br>1226     | 8<br>8<br>5<br>5<br>5<br>5<br>5<br>5  | 572<br>88    | 23<br>1572               | 828            | 123           | 4           | 88 x       |
| FROM WEST                      | IST HR           | \$                   | 466              | s E            | 21           | 20 <u>5</u>  | 182        | 88           | 1549         | 8 ž        | 88           | <b>1</b><br>100<br>100 | æ≊       | <b>687</b><br>29 | 1414           | z‡  | 280          | 1336                     | 22             | 586           | 887         | 28         |
| PERCENT TRINCKS                | AND HR           | 77                   | 1613<br>14 to 24 | 2              | 8            | 1452         | 2          | 35           | 1599         | 8          | 31           | 1480                   | 134      | R                | 1420           | 8   | : 8          | 1666                     | 8              | ۲ <u>۲</u>    | 874<br>874  | e 19       |
| AFEWAY INTERSECT               | NOL              |                      |                  |                |              |              |            |              | 47 01 V      | 1          |              | 2%                     | +        |                  | *              | +-  |              | 2%                       |                |               | *           |            |
| YODE 400                       | 1                |                      |                  |                |              |              |            |              |              |            |              |                        |          |                  |                |   |              |                          |                |               |             | -          |
| ROM NORTH                      | ST HR            | 1214<br>1183         |                  | 934<br>876     | 1211<br>1083 |              | 932<br>802 | 1345<br>1345 |              | 845<br>845 | 1284<br>1145 |                        | 1070     | 1268             |                | 12  | 1503         |                          | 074            | 476           |             | 433        |
| ROM EAST                       | ND HR.           |                      | 1573<br>1565     | 948<br>839     |              | 1687<br>1493 | 945<br>847 |              | 1785<br>1603 | £95<br>295 |              | 1632<br>1870           | 916      |                  | 1863           | <u>8</u> 88   | R            | 1732                     | 88             | <b>B</b>      | 759         | 419<br>479 |
| ROM WEST 1                     | ST HR<br>ND HR   | <u>5</u><br>29<br>29 | 1330<br>1373     |                | 1023         | 1292         |            | 1045         | 1311         |            | <b>260</b>   | 1289                   | 2        | 1194             | 8 <u>8</u>     | 9   | <u>8</u>     | 1352                     | 22             | 487           | 5835<br>583 | 220        |
| PERCENT IRUCKS                 |                  |                      | 3K               | t              |              | *            |            | 9            | 1311         |            | 5            | 1323                   | +        | 1128             | 1263           | +   | 1140         | 1458                     |                | 491           | 567         | 1          |
|                                |                  |                      |                  | 1              |              |              |            |              | 47 M V       | 1          |              | 47.014                 | 1        | 7                | <u>k to 2%</u> | 1   |              | ž                        | -              |               | 3%          | T          |
|                                |                  | z                    |                  |                |              | +»           |            |              | 4            |            |              |                        | -        | 4                |                |   | <b>.</b>     |                          |                |               |             |            |
|                                | Ŀ                | <u>ئ</u> ے           |                  | ↓ I            |              | NODE<br>100E |            |              |              |            |              |                        |          | Soc.             |                |   | - Jope       | Ļ                        | 1              |               |             |            |
|                                | ľ                | <u>,</u>             |                  |                |              | ]            |            |              | •            |            |              |                        |          |                  |                | Ī   | 2            |                          | <b>▲</b>       |               |             |            |

TABLE 3.4 Tabular Summary of Vehicle Counts Validation Network (Safeway Street)

# CHAPTER IV

# STATISTICAL ANALYSIS

### Introduction

The data analysis of the applicability and adaptability of a microscopic urban simulation model is presented in this chapter. Engineers and scientists rely on statistical analysis techniques as a tool to aid researchers in conducting scientific experiments. However, the major aspect of statistical inquiries, is to incorporate specific procedures for reasoning mathematically from numerical observations of variables in the form of raw data, into what is known as statistical conclusions; which comprise the object of a specific study.

This research utilized Traf-Netsim (version 5.0), a highly accepted network simulation model among the profession, to test the general hypothesis of whether or not Traf-Netsim can simulate the traffic behavior on selected roads in the city of Amman, Jordan. The verification and validation of the simulation model was accomplished through actual field observations on two selected sites. The two sites are The Test Network and The Validation Network, both of which were presented in the Methodology chapter.

The Test Network was used for the following:

1. To collect the Mean Start-Up Lost Time and Mean Queue Discharge Headway along with their distributions to be used in the calibrated Netsim model.

- 2. To measure Travel Time at predetermined locations along the arterial.
- Compute Delay Time. This is route delay time not intersection delay time, and it is defined as the difference between Travel Time and Ideal Travel time. Where;
  - Travel Time is the actual time traveling on a specific links under the existing traffic and roadway conditions.
  - Ideal Travel Time is the time traveling on a specific link under free flow conditions. This is computed by dividing the link length by the posted speed limit.
- 4. To determine if the simulated travel times and delay times derived from Traf-Netsim are different when using the default or calibrated parameters. Also to determine if the simulated values are different from the measured values obtained during the floating car study.

The Validation Network was used for the following:

- 1. To measure Travel Time at predetermined locations along the arterial.
- 2. To compute Delay Time.
- 3. Model Validation: To evaluate if the simulated travel time and delay time using the calibrated Netsim model differ from the measured values obtained from the floating car study while traveling along the validation network.

This research will use the Statistical Analysis Software version 7.0 (abbreviated SAS), a known and respected statistical package among scientists and engineers, to test and analyze data collected in the field against data produced by the Traf-Netsim model while simulating the traffic environment in Amman, Jordan. Specific statistical test

procedures in SAS will be employed to evaluate and test the different hypotheses underlined in this research. The reminder of this chapter is devoted to hypotheses testing, evaluating and data presentation.

### **Test Network**

The first site, referred to as the Test Network, is a segment of Mecca Street and is approximately 2.5 Kilometers long (or 1.562 miles). The Test Network as the name implies was used to test the following:

In order to calibrate the Traf-Netsim model, several traffic parameters were collected under existing traffic conditions to reflect the behavior of the local environment and thus, the behavior of a Jordanian driver to a specific stimulus. The traffic parameters used to calibrate the Traf-Netsim model are:

- a- The mean Start-Up Lost Time for the first vehicle when the traffic signal indication changes from red to green.
- b- The mean Queue Discharge Headway of vehicles standing in queue when the traffic signal indication change from red to green.

These traffic parameters along with their respective distributions replaced the default parameters impeded in Traf-Netsim model to produce what this research refers to as the calibrated Traf-Netsim model.

### **Defining the Hypotheses**

To test if the measured Start-Up Lost Time and Queue Discharge Headway are statistically significant from the default values embedded in TRAF-NETSIM the

following Hypotheses were constructed.

Start-Up Lost Time:

- The Null Hypothesis states that there is no statistical significance between the observed (calibrated) Start-up Lost Time of 1.8 seconds and the default value of 2.0 seconds.
- The Alternative Hypothesis states that there is a statistical significance between the calibrated Start-up Lost Time of 1.8 seconds and the default value of 2.0 seconds.

To perform statistical tests for the above Hypotheses the Univariate Procedure in SAS was invoked. Table 4-1 shows the output of the statistical test performed by SAS. The complete statistical output produced by the Univariate Procedure in SAS software is presented in Appendix A.

### Interpretation of the Statistical Results:

For the Start-Up Lost Time study, a total of 163 observations were collected in the field under normal driving conditions. The field study indicates that the Average Start-Up Lost Time observed in Amman is approximately 1.8 seconds, with a Standard Deviation 0.69.

In order to test the above stated Hypotheses, several steps were performed:

- 1. To test both the Null and Alternative hypotheses, one should decide whether to use a parametric or non-parametric test.
- 2. At what significant level (or alpha level) should the rejection region be set?

|             | Table        | 4-1      |        |      |
|-------------|--------------|----------|--------|------|
| Statistical | analysis for | Start-Up | Lost ' | Time |

|  | THE UNI                 | VARIATE     | PROCEDURE         |           |  |  |  |
|--|-------------------------|-------------|-------------------|-----------|--|--|--|
| Mariahlan Jasmina (Q   |                         | ·           |                   | ·         |  |  |  |
| Variable: lostume (St  | art-Up Los              | st Time Ioi | the first venicle | in Queue) |  |  |  |
|  |                         | Momer       | nts               |           |  |  |  |
| N  | 163                     | Sur         | n Weights         | 163       |  |  |  |
| Mean   | 1.8245                  | Sw          | n Observations    | 297.4     |  |  |  |
| Std Deviation  | 0.6920                  | ) Va        | ariance           | 0.4788    |  |  |  |
| Skewness   | 1.2768                  | Ku Ku       | irtosis           | 1.2493    |  |  |  |
| Uncorrected SS   | 620.19                  | 9 Co        | orrected SS       | 77.579    |  |  |  |
| Coeff Variation  | 37.928                  | 3 Sto       | d Error Mean      | 0.0542    |  |  |  |
|  | Tests 1                 | for Locatio | n : Mu0=0         |           |  |  |  |
| Test   | S                       | tatistic    | P `               | Value     |  |  |  |
| Student's t  | <u>t 3</u>              | 3.66151     | Pr> t             | <.0001    |  |  |  |
| Sign   | <u>M</u>                | 81.5        | Pr >   M          | <.0001    |  |  |  |
| Signed Ran   | <u>k</u>                | 6683        | Pr >   S          | <.0001    |  |  |  |
| Tests for Normality  |                         |             |                   |           |  |  |  |
| Test   | Test Statistic P ValueP |             |                   |           |  |  |  |
| Shapiro-Wilk   | <u>W</u> 0.             | .8761       | Pr < W            | <0.0001   |  |  |  |
| Kolmogorov-Smirnov   | D 0.                    | .16037      | Pr > D            | <0.0001   |  |  |  |
| Cramer-Von Mises   | W-Sq 1.                 | 19401       | Pr > W-Sq         | <0.005    |  |  |  |
| Anderson-Darling   | <u>A-Sq 6</u>           | .6296       | Pr > A-Sq         | <0.005    |  |  |  |
| $H_{o}: u_{\text{losttime}} = 2.0$ $H_{a}: u_{\text{losttime}} \neq 2.0$ |                         |             |                   |           |  |  |  |

.

The second question involves the rejection or failing to reject the specified null hypothesis given a predetermined alpha level. Traditionally, engineers have used significant levels of 0.01, 0.05, and 0.1. These three levels can be thought of as "extremely significant," "significant," and "moderately significant," respectively. However, the Traffic Engineering Handbook <sup>(14)</sup> suggests that traffic engineers should consider results significant at the 0.05 level for most traffic engineering studies and should consider results significant at the 0.01 level when performing safety-related studies. This research will use an alpha level equal to 0.05 in all the statistical tests presented. An alpha level of 0.05 gives a confidence coefficient equal to 0.95 (1 – alpha) or 95% confidence level. In other words, we are 95% sure that a sample collected from a population will yield a confidence interval that includes the true population mean.

The first question addresses the issue of Normality. If the data is normally distributed, then a parametric test is considered. Otherwise an equivalent non-parametric test should be employed. Looking at Table 4-1, under the heading "Tests for Normality" a Shapiro-Wilk test gives a p-value of 0.0001. This is a very small value and is close to zero indicating the data for the Start-Up Lost Time are not a sample from a normal distribution. This suggests that a non-parametric test should be used. However, since the sample size of 163 is fairly large, the parametric test should be reasonably accurate. Therefore both parametric and non-parametric tests will be performed.

For a non-parametric test:

The Signed Rank test, gives a p-value of  $Pr \ge |S| < 0.001$ 

For a parametric test:

The Student's t test, gives a p-value of Pr > |t| < 0.001

Since the attained probability or the p-value is less than the reference probability or the alpha value (0.001 < 0.05), for both parametric and non-parametric tests, the null hypothesis is rejected.

Based on the above, this research concludes that the average Start-Up Lost Time of 1.8 seconds collected in Amman is significantly different from the Start-Up Lost Time of 2.0 seconds used by Netsim as a default value.

### Queue Discharge Headway:

- The Null Hypothesis states that there is no statistical significance between the calibrated Queue Discharge Headway of 1.5 seconds and the default value of 1.8 seconds
- The Alternative Hypothesis states that there is a statistical significance between the calibrated Queue Discharge Headway of 1.5 seconds and the default value of 1.8 seconds.

To perform statistical tests for the above Hypotheses the Univariate Procedure in SAS was invoked. Table 4-2 shows the output of the statistical test performed by SAS. The complete statistical output produced by the Univariate Procedure from the SAS software is presented in Appendix A.

#### Interpretation of the Statistical Results:

For the Queue Discharge Headway study, a total of 780 observations were collected in the field under normal driving conditions. The study indicates that the Average Queue Discharge Headway observed in Amman is approximately 1.5 seconds.

| Table 4-2  |
|--|
| Statistical analysis for Queue Discharge Headway |

|   | THE UI     | NIVARIA      | TE PROCEDURE     | ]       |  |  |  |
|---|------------|--------------|------------------|---------|--|--|--|
| Variab                                      | ole: hea   | dway (Qu     | eue Discharge He | adway)  |  |  |  |
|   |            | Mor          | nents            |         |  |  |  |
| N   | 7          | /80          | Sum Weights      | 780     |  |  |  |
| Mean  | 1.50       | )64          | Sum Observation  | s 1175. |  |  |  |
| Std Deviation                               | 0.5        | 483          | Variance         | 0.3006  |  |  |  |
| Skewness                                    | 1.7        | 176          | Kurtosis         | 4.0901  |  |  |  |
| Uncorrected SS                              | 200        | 04.3         | Corrected SS     | 234.17  |  |  |  |
| Coeff Variation                             | 36.3       | 396          | Std Error Mean   | 0.0196  |  |  |  |
|   | Tes        | ts for Loca  | ation : Mu0=0    |         |  |  |  |
| Test  |            | - Statistic- | P                | Value   |  |  |  |
| Student's t                                 | <u>t</u> 7 | 76.73606     | Pr> t            | <.0001  |  |  |  |
| Sign  | M          | 390          | Pr >  M          | <.0001  |  |  |  |
| Signed Rank                                 | S          | 152295       | Pr>ISI           | <.0001  |  |  |  |
| Tests for Normality                         |            |              |                  |         |  |  |  |
| Test Statistic P ValueP                     |            |              |                  |         |  |  |  |
| Shapiro-Wilk                                | W          | 0.8589       | Pr < W           | <0.0001 |  |  |  |
| Kolmogorov-Smirn                            | ov D       | 0.12771      | <u>Pr &gt; D</u> | <0.0100 |  |  |  |
| Cramer-Von Mises                            | W-Sq       | 4.97415      | Pr > W-Sq        | <0.005  |  |  |  |
| Anderson-Darling                            | A-Sq       | 29.3306      | Pr > A-Sq        | <0.005  |  |  |  |
| $H_o: u_{headway} = 1.8$                    |            |              |                  | 1       |  |  |  |
| $\mathbf{H}_a: u_{\text{headway}} \neq 1.8$ | )<br>      |              |                  |         |  |  |  |

To test the above null and alternative hypotheses the following is presented:

Looking at Table 4-2, under the heading "Tests for Normality" a Shapiro-wilk test gives a p-value of 0.0001. This is a very small value and is close to zero indicating the data for the Queue Discharge Headway are not a sample from a normal distribution. This suggests that a non-parametric test should be used. However, since the sample size of 780 is very large, the parametric test should be reasonably accurate. Therefore both parametric and non-parametric tests will be performed.

For a non-parametric test:

The Signed Rank test, gives a p-value of Pr >= |S| < 0.001

For a parametric test:

The Student's t test, gives a p-value of Pr > |t| < 0.001

Since the attained probability or the p-value is less than the reference probability or the alpha value (0.001 < 0.05), for both parametric and non-parametric tests, the null hypothesis is rejected.

Based on the above, this study concludes that the average Queue Discharge Headway of 1.5 seconds collected in Amman is significantly different from the mean Queue Discharge Headway of 1.8 seconds observed in Washington D.C. and is used by The Traf-Netsim model as a default value.

Up to this point this research has only shown that the observed values for Start-Up Lost Time and Queue Discharge Headway of 1.8 and 1.5 seconds respectively are statistically significant from the default values impeded into Traf-Netsim model. This doesn't imply that model's ability to simulate the actual traffic conditions on the street network will improve. To found out how the model will perform the following is presented.

- 1- To determine if the Traf-Netsim model using the impeded default parameters can simulate Travel Time and Delay Time along the test network "Mecca Street" within an acceptable range. This was accomplished by comparing the simulated values produced by the default model against the measured values obtained during the flouting-car study.
- 2- To determine if the Traf-Netsim model using the calibrated parameters can simulates Travel Time and Delay time along the test network "Mecca Street" within an acceptable level of accuracy. This was also accomplished by comparing the simulated values produced by the calibrated model against the observed values collected in the field.

#### **Defining the Hypotheses for Travel Time and Delay Time**

To test if the mean Travel Time and Delay Time between the simulated model, the simulated calibrated model, and the observed values obtained from the floating car study are statistically significant from one to another the following hypotheses were constructed:

## Travel Time along the Arterial:

• The Null Hypothesis states that the mean Travel Times for the three groups are the same.

The three groups are:

1. Simulated model with default parameters.

- 2. Simulated model with calibrated parameters.
- 3. Observed values form the field.

In terms of a mathematical expression the Null Hypothesis is:

# $H_o: u_{default} = u_{calibrated} = u_{observed}$

• The Alternative Hypothesis states that at least the mean Travel Time of one group is statistically significant from another group.

In terms of a mathematical expression the Alternative Hypothesis is:

# H<sub>a</sub>: At least one mean is different

### Delay Time along the Arterial:

Similar null and alternative hypotheses for the mean Delay Time were also constructed.

 $H_o: u_{default} = u_{calibrated} = u_{observed}$ 

# H<sub>a</sub>: At least one mean is different

It should be brought to the readers attention that the above hypotheses are comparing three groups to one another, and that the Alternative Hypotheses for both the Travel Time and Delay time does not specify which means are different from one another. It only tells us that some differences exist. In order to find out which means are different, an appropriate multiple comparison procedure will be employed.

To test and evaluate if the three groups presented in the above hypotheses are statistically significant from one to another a statistical procedure referred to Analysis of Variance "or ANOVA" will be used and is presented below:

#### Analysis of Variance:

The analysis of variance in a single-factor study is mainly to determine whether or not the factor level means are equal. Expressed mathematically, is  $\mu_1 = \mu_2 = \mu_3$ . If the answer is true, then we fail to reject the Null hypothesis and conclude that the three means are the same. On the other hand, if the answer is false, we would reject the Null hypothesis and conclude that at least one mean is different.

Obviously, the more that these groups would differ from each other in terms of the dependent variable, the more variability we would expect among their means. This variability is measured in terms of how the group means vary about the mean of all groups put together. This mean is referred to as the grand mean and is abbreviated as Y<sub>GRAND</sub>. In fact, analysis of variance calculates the groups' variance about the grand mean. This variance is called the between-groups variance. Therefore, it would be expected that the more differences there are among the groups, the larger would be the value of the between-groups variance. In addition, analysis of variance looks at how much variability among individual scores would be expected. Mainly, what is the probability of this variance occurring under the terms of the null hypothesis due to sampling error? In analysis of variance, this value is based on the amount of variability that was observed within each of the groups. This is appropriately referred to as the within-groups variance. The point to remember thus far in analysis of variance is that if there are no differences among the groups, then the between-groups variance and the within-group should be approximately equal. Therefore, the larger the value of the between-groups variance to within-groups variance, the greater is the probability that at
least one of the group means is different. The test statistic used by ANOVA for choosing between the above hypotheses is:

# $\mathbf{F} = \text{Variance between groups} / \text{Variance within groups}$

If the null hypothesis is true and there is no sampling error at all, one would expect the value of F to be exactly 1. But in the true world of data collection sampling error is present. Therefore, under the assumptions of the null hypothesis, the sampling distribution of F tells us the probability that one can expect the between-groups variance to be so many times larger than the within-groups variance. And if this probability is less than the preset probability level, say 0.05, then the null hypothesis is rejected in favor of the alternative hypothesis. Thus, the researcher concludes that there is adequate evidence to suggest that at least one of the population means is significantly different from the rest.

Assumptions of a one-way Analysis of Variance:

Before performing any statistical tests with a one-way analysis of variance the following assumptions should be evaluated.

- 1- Observations are independent random samples.
- 2- Observations are sampled from a normal distribution.
- 3- Groups have equal variances.

First, the assumption of independent observations is met, since in this research the measurement for one item in the data set did not affect the measurement for another item. That is, the value of Travel Time for one simulation is unrelated to the value of Travel Time for another simulation. This was easily accomplished by using a different random number seed for each run which generates a different pattern of driver types and vehicle paths moving through the analysis network.

Second, the assumption of normality is difficult to meet, since there were only 7 observations in each group. To truly test this assumption, a normality test should be performed for each group. And since the data in each group is small, this research didn't have enough data to perform an appropriate normality test. However, even if the assumption of normality is not met, it is not too critical since we are basing the analysis of variance test on group means, and hence the Central Limit Theorem should still be applicable <sup>(20)</sup>. Also the F test for the equality of the population means is slightly effected by the lack of normality and is considered to be a robust test against departures from normality <sup>(29)</sup>.

Third, the last assumption required by analysis of variance is that the populations have a common variance. The data in this research appeared in some situations to have unequal values for standard deviation, and thus the variance. Concerning this assumption, the F test used by analysis of variance procedure is slightly affected by unequal variance, if all factor level sample sizes are close or equal <sup>(20)</sup>. In order to minimize the effects of unequal variances on inferences with the F distribution and related tests this research will use equal sample sizes for all factor levels. To accomplish the equal sample size in each factor level for both the Test and Validation Networks, equal number of simulation runs were performed in both the default and calibrated Netsim models to match the observed values obtained from the floating car method.

In summary, Since the data set in each factor level is fairly small several assumptions required by analysis of variance procedure where not satisfied. Therefore, to

guard against violations of the normality and unequal variance assumptions, both ANOVA, which is a parametric test, and Kruskal-Wallis test which is a non-parametric analogue to the one way analysis of variance will be employed.

Before presenting the data and statistical findings several factors related to the variability in the simulation output follows:

### **Simulation of Traf-Netsim**

Traf-Netsim is a discrete event simulation model that simulates the traffic flow on urban street networks by representing the movement of individual driver-vehicle combinations. The simulation output produced by Traf-Netsim contains some variability from one simulation run to the next. This variability is more apparent in Traf-Netsim due to the fact that the model represents the behavior of traffic flow microscopicity. That is, each vehicle is handled as a distinct entity. Of course, the presence of high variability in simulation output can lead to questions concerning the model's reliability. However, the amount of variability in a given situation depends on several factors such as:

- 1. The number of simulation runs
- 2. The length of each simulation
- 3. The length of worm-up time (initialization time)

In order to achieve meaningful simulation results and to reduce the risk of drawing incorrect conclusions, the above issues concerning the variability of the output will be addressed in the following.

Traf-Netsim model uses two random number seeds the "base seed" and the "common seed" to generate the traffic movement and all the time-dependent stochastic

decisions for a given simulation run. Therefore, to reduce the variance between simulation runs, this research will use multiple independent replications. This means that the simulation model will be executed several times for a given set of identical input data, except that the base random number seed will be changed. This type of variance reduction technique is known as the Common Random Numbers (CRN) reduction procedure, in simulation experiments <sup>(18,28)</sup>.

In summary a series of runs with different values for the base seed will be used in this study to show the variance in the selected traffic performance measures of effectiveness (i.e. Travel Time and Delay Time) which are due to variations in individual vehicle traffic patterns. This type of variance reduction technique has been shown to significantly reduce the simulation output variability even though the simulation time for each run was only 900 seconds <sup>(28)</sup>. The only requirement to apply this variance reduction procedure is the matching of the set of the random number seeds in simulation experiments.

Table 4-3 shows the set of random numbers for the "base seed", entry 11 on card type 2, used for all simulation runs trough out this study. The random numbers where picked from a table of random number digits and are presented below <sup>(29)</sup>:

The set of random numbers used had to meet the criteria set by Traf-Netsim simulation model. Which basically states that the random number seed must be an odd number of up to eight digits is size and that the last digit in every number is not 5. If a seed number didn't meet the above criteria, Traf-Netsim will print a fatal error message and will terminate the simulation run.

| REPLICATION<br>NUMBER | BASE RANDOM<br>NUMBER |
|-----------------------|-----------------------|
| 1                     | 132841                |
| 2                     | 21224003              |
| 3                     | 9905247               |
| 4                     | 199509                |
| 5                     | 6057                  |
| 6                     | 91240283              |
| 7                     | 974581                |
| 8                     | 352493                |
| 9                     | 10750527              |
| 10                    | 3624727               |

Table 4-3 Random Numbers

The second factor affecting the output variability is the simulation length. In simulation studies there are two methods available for performing simulation experiments. The first method is to make a single run and execute the simulation for a long duration. Then use the data generated in this single, continuous, long run to estimate Travel Time and Delay Time. The second method for conducting simulation experiments is to make several independent simulation runs. Independent replications are achieved by starting each run with a different random number seed. The second method was used by this research since it produced several samples in each group as opposed to one in the case of a single long run. Also, by applying the Common Random Number technique discussed earlier the variability in the simulation output should be reduced. In addition simulating with independent replications is very simple to implement in Traf-Netsim through the use of the base random number seed. The third issue of concern is how long should the initialization period be to assure a steady state condition. That is, to estimate the transient phase (or initialization period) to reduce the effects of early unstable observation on the output results. To ensure that equilibrium is reached (Input = Output), the user must specify a large initialization period that is longer than the time needed to reach equilibrium. It is recommended that the initialization period should be equal to the travel time at free flow speed along the longest path in the network <sup>(16)</sup>. This research used an upper bond for initialization of 10 minutes (600 seconds) and 30 minutes (1800 seconds) for both the validation and test networks respectively. These values are extremely high. However, if Traf-Netsim attains equilibrium before the specified time, then the remaining time available for initialization will be discarded and the program will immediately enter the simulation phase and will start accumulating statistics. It should be mentioned that in all the simulation runs through out this study, equilibrium was attained at around 5 to 7 minutes into the initialization period.

In summary, this research observed and recorded traffic conditions on each of the test and validation networks. The floating car method was performed concurrently during the collection of traffic volumes required to execute the simulation model. The data was recorded for two continuous hours on seven consecutive days. For each day, two simulations were performed in order to reflect the changes in traffic conditions that occurred during the first and second hours of data collection respectively.

For each hour, eight to ten independent replications were made for traffic operations under the default model using the set of random number seeds presented in Table 4-3 above. Each simulation run was executed for 3600 seconds and the simulated

Travel times and Delay times were compared with those observed in the field during the same hour (i.e. first hour or second hour of observation). It should be mentioned that statistics were collected on specific sections along the test network (Mecca Street), at the end of each simulation run. This was repeated for all seven days during which data was collected. The same procedure was also followed for traffic operations under the modified or calibrated Netsim model. That is, all the data remained constant except the calibrated parameters were changed in Traf-Netsim.

As mentioned earlier both the Analysis of Variance and the Kruskal-Wallis tests were invoked by SAS to test the null and alternative hypotheses at the 0.05 confidence interval.

Recall that for both the Travel Time and Delay Time, the Null Hypothesis states that the means for the three different groups are the same. And that the Alternative Hypothesis states that at least the mean of one group is statistically significant from another group.

#### **Statistical Interpretation**

The following section will present the statistical summaries of the above null and alternative hypotheses for travel time and delay time on the test network. But, before interpolating the statistical results it should be brought to the readers attention that the naming of the links were modified for added clarity and simplicity when looking at the tables. For example, road segment A1 represents in Netsim the aggregate links from node 100 to node 114, A2 represents the aggregate links from node 114 to node 122 and so on and so forth. This is best demonstrated by looking at figure 4-1.





### Travel Time on Test Network "First Hour":

Looking at the statistical analysis of Travel Time on the Test Network for the first hour (Table 4-4) the following comments and interpretations are presented:

First, the column labeled ANOVA Pr > F gives the p-values for comparing the three groups. The numbers in this column are all below the reference probability of 0.05 set by this study. This is true for all the road segments through out the week, with the exception of Thursday in which link A3 had a p-value of .0529 slightly larger than 0.05. In conclusion, since the p-values are less than 0.05, the stated null hypothesis is rejected in favor of the alternative hypothesis. Therefore this study concludes, based on the statistical analysis presented during the first hour of observation, that the mean Travel Time is significantly different among the three study groups (observed, default, and calibrated).

This is very true, especially when comparing the default travel time versus observed travel time. It appears that the observed values of travel time are always shorter than the simulated default values. This finding supports the overall statement made by this research that the driver behavior in Jordan is different from those observed in Washington D.C. In addition, the observed traffic parameters in Amman - Jordan, such as queue discharge headway and start-up lost time for vehicles of 1.5 seconds and 1.8 seconds respectively also enhances this finding. This could suggest that the Jordanian driver is more aggressive than the American driver since the observed values of queue discharge headway of 1.5 seconds and start up lost time of 1.8 seconds are lower than the default parameters of 1.8 and 2.0 embedded in Traf-Netsim.

Table 4-4 Statistical Analysis of Travel Time on Test Network "First Hour" First hour of observation (12:30 - 13:30)

| -             |         |        |                    |                            |  |   |                            | _         | _                 |                    |                            |  |   |  |
|---------------|---------|--------|--------------------|----------------------------|--|---|----------------------------|-----------|-------------------|--------------------|----------------------------|--|---|--|
|               | Kruskal | Wallis | Pr >               | 0.0011                     | 0.0004<br>0.0004<br>0.0012<br>0.0011   | 0.0008<br>0.0011<br>0.0012<br>0.0012  | 0.0008                     |           | Kruskal<br>Walie  | Pr > chi-souare    | 0.0054<br>0.0008<br>0.0016 | 0.0034<br>0.0007<br>0.0008<br>0.001                                      | 0.0011<br>0.0012<br>0.0008<br>0.0011        | 0.0012<br>0.0012<br>0.0526                         |
| leo 4         | lian i  | ANOVA  | Pr > F             | 1000.5<br>1000.5<br>1000.5 | 000<br>000<br>000<br>000<br>000<br>000 | <ul><li>0001</li><li>0001</li><li>0001</li><li>0002</li><li>0002</li><li>0002</li></ul> | <.0001<br><.0001<br>0.0015 | h cell    | ANOVA             | Pr > F             | 0.0007<br>4.0001<br>4.0001 | 0.0039<br>. 0001<br>. 0009<br>0.0009                                     | 0.0042<br>0.001<br>0.001<br>0.001<br>0.001  | <ul><li>0001</li><li>0001</li><li>000371</li></ul> |
| in eac        | 100111  |        | Stand.             | 0.010                      | 0000<br>1000<br>1000                   | 0.2   | 0.2                        | in eac    |                   | Stand.<br>Dev.     | 1.1.0                      | 0.1<br>0.2<br>7.5  | 0.1<br>0.2<br>0.1<br>1.8                    | 0.2<br>0.2<br>1.2                                  |
| et e          |         | ratec  | ¥                  | 444                        | < 0 < <                                | ~ ~ ~ ~   | 404                        | ation 1   | ta ta             | ¥                  | 444                        | ***  | ~ ~ ~ ~                                     | ~ ~ ~  |
| 7 Ohsan       |         | Cali   | Mean               | 36.9<br>37.0<br>53.0       | 20.9<br>21.7<br>33.8<br>48.4           | 19.9<br>21.8<br>32.2<br>65.9  | 43.9<br>30.7<br>30.0       | : 7 Obser | C.                | Mean               | 36.5<br>36.8<br>52.5       | 20.8<br>21.6<br>33.8<br>49.6   | 19.8<br>21.8<br>32.1<br>63.8                | 44.0<br>30.6<br>29.8                               |
| 1997          |         |        | Stand.<br>Dev.     | 033                        | 0.1<br>0.2<br>1.7                      | 0.1<br>0.1<br>1.2   | 0.3                        | 3. 1997   |                   | Stand.<br>Dev.     | 0.3<br>0.2<br>1.0          | 0.1<br>0.1<br>2.2  | 2.0.0.1                                     | 0.3  |
| lav 1         |         | Bult   | ¥                  | 0 0 0                      |  | 60 60 60 60   | 0000                       | Aav 1     | ŧ                 | ¥                  | 000                        |  |   | 8 8 4  |
| Sunday A      |         | å      | Mean               | 39.7<br>45.5<br>56.9       | 24.5<br>26.3<br>68.2<br>58.2           | 23.4<br>26.7<br>39.6<br>69.4  | 62.2<br>37.5<br>32.1       | Tuesday   | Det               | Mean               | 39.5<br>45.4<br>54.9       | 24.5<br>26.3<br>41.1<br>59.7   | 23.3<br>26.6<br>39.6<br>71.6                | 52.6<br>37.5<br>31.3                               |
|               |         |        | Stand.<br>Dev.     | 1.3<br>1.1<br>1.8          | 1.3<br>1.9<br>2.9                      | 0.3<br>0.3<br>2.7   | 2.3                        |           |                   | Stand.<br>Dev.     | 3.4<br>2.1<br>0.8          | 3.1<br>1.1<br>1.5  | 2.64  | 3.1<br>1.8<br>1.4                                  |
|               |         | ष्ट्र  | ¥                  | <b>&lt;</b> < <            | ~ ~ ~ ~                                | ***   | < < <                      |           | bey               | ¥                  | < < <                      | 8<br>4 4 4 4   | <b>&lt;</b> <<<                             | ~ ~ ~  |
|               |         | Obse   | Mean               | 36.6<br>37.4<br>51.8       | 21.8<br>20.4<br>33.9<br>48.2           | 20.1<br>21.8<br>32.2<br>63.7  | 42.6<br>28.2<br>30.2       |           | Obsei             | Mean               | 34.6<br>35.6<br>52.0       | 22.1<br>20.2<br>33.2<br>50.3   | 19.9<br>21.3<br>32.8<br>63.4                | 43.5<br>30.0<br>31.4                               |
|               |         | Road   | Segment            | 83 F 4                     | 22222                                  | ខ្លួនខ្លួ   | 883                        |           | Road              | Segment            | 83 F3 F3                   | 22222  | ខ្លួនខ្លួ                                   | 883  |
|               | Kruskel | Wallis | Pr ><br>chi-square | 0.0007<br>0.001<br>0.0169  | 0.0008<br>0.0006<br>0.0008<br>0.0008   | 0.001<br>0.0059<br>0.006<br>0.006   | 0.0008<br>0.0012<br>0.0235 |           | Kruskal<br>Wallis | Pr ><br>chi-square | 0.0008<br>0.0011<br>0.0344 | 0.0009<br>0.007<br>0.0008<br>0.0008                                      | 0.0214<br>0.0012<br>0.0004<br>0.0201        | 0.0011<br>0.0007<br>0.0235                         |
| ch cell       |         | ANOVA  | ц~л                | <.0001<br><.0001<br>0.0148 | 0001<br>0001<br>0001<br>0001<br>0001   | <ul><li>0001</li><li>0003</li><li>0002</li><li>0001</li><li>0001</li></ul>              | <.0001<br><.0001<br>0.0086 | h cel     | ANOVA             | Pr > F             | <.0001<br><.0001<br>0.0129 | <ul> <li>0001</li> <li>0.0198</li> <li>0.0039</li> <li>0.0039</li> </ul> | 0.0065<br>< 0001<br>< 0001<br>0.0062        | <.0001<br><.0001<br>0.0208                         |
| ns in ea      |         |        | Clev.              | 0.2<br>0.2<br>2.4          | 6.2<br>3<br>3<br>3<br>2<br>3           | 0.1<br>0.2<br>1.8   | 0.2<br>0.3<br>1.5          | s in eac  |                   | Stand.<br>Dev.     | 0.2                        | 072<br>072<br>66   | 0.1   | 0.4  |
| <b>INatio</b> |         | ğ      | ¥                  | < < <sup>8</sup>           | < < < U                                | ~~~~  | <b>4 4 4</b>               | /ation    | ated              | ¥                  | A A A                      | < 8 < <  | < <u<< td=""><td>∢υ<sup>Β</sup>γ</td></u<<> | ∢υ <sup>Β</sup> γ                                  |
| 7 Obse        | 1       | Callb  | Mean               | 37.2<br>36.9<br>53.6       | 20.9<br>21.7<br>33.8<br>52.2           | 19.8<br>21.8<br>32.4<br>65.9  | 43.9<br>30.6<br>29.6       | . 7 Obser | Calibr            | Mean               | 37.1<br>37.0<br>55.7       | 21.0<br>21.7<br>33.9<br>53.2   | 19.8<br>21.9<br>32.3<br>67.1                | 44.1<br>30.7<br>30.7                               |
| 0, 199        |         |        | Dev                | 0.3<br>0.2<br>1.9          | 0.2<br>0.3<br>1.4                      | 0.1<br>0.2<br>3.0   | 0.3<br>0.3<br>2.4          | . 1997    |                   | Stand.<br>Dev.     | 0.3                        | 22222  | 0.2   | 0.4<br>0.4<br>1.1                                  |
| May 1         | 1       | ۳.     | ¥                  | 60 60 60                   | 00000                                  | 00000   | 000                        | lav 12    | aut               | ¥                  | 000                        | 8 <sup>4</sup> 8 8   | 00000                                       | 000  |
| Saturday      | i       | 90     | upaw               | 40.1<br>45.5<br>57.4       | 24.6<br>26.3<br>41.3<br>59.7           | 23.4<br>26.7<br>39.8<br>72.3  | 52.4<br>37.4<br>32.4       | Monday A  | Def               | Mean               | 39.9<br>45.5<br>57.3       | 24.8<br>28.3<br>41.1<br>61.4   | 23.3<br>26.7<br>39.7<br>70.0                | 52.9<br>37.9<br>32.7                               |
|               |         |        | Dev                | 23<br>45                   | 1.7<br>2.1<br>0.8                      | 1.0<br>3.8<br>5.7<br>1.1  | 3.0<br>1.8<br>0.4          |           |                   | Stand.<br>Dev.     | 1.9<br>2.7<br>2.8          | 2.<br>5.0<br>4.<br>4.<br>7.  | 32<br>2.1<br>2.9                            | 2.0<br>2.9<br>2.9                                  |
|               |         |        | ¥                  | <b>« « «</b>               | <b>«</b> « « « «                       | <b>«</b> « « «  | <b>444</b>                 |           | pevie             | ¥                  | <b>« « «</b>               | <b>«</b> « « «   | <b>4 4 4</b><br><b>0</b>                    | <b>«</b> « «                                       |
|               | ð       |        | Lipaw              | 35.4<br>35.9<br>52.1       | 20.2<br>21.1<br>33.0<br>40.9           | 19.2<br>21.1<br>31.2<br>64.7  | 43.1<br>30.2<br>29.9       |           | Obsi              | Mean               | 38.1<br>36.0<br>53.9       | 19.9<br>22.8<br>32.2<br>55.6   | 20.7<br>21.7<br>29.6<br>68.0                | 44.7<br>29.2<br>29.4                               |
|               | 2       | DBOX   | wiawingac.         | A2 A3                      | 2882                                   | 6889  | 883                        |           | Road              | Segment            | A3 23                      | 22,22,22   | 2882  | 883  |

Note: Tukey's Studentized Range Test (TK) = Means with the same letter are not significant at the 0.05 level

Table 4-4 (continued) Statistical Analysis of Travel Time on Test Network "First Hour" First hour olobservation (12:30 - 13:30 )

| Γ              | 1_                |         | ġ          |   |   |  |   | 1         | _                 |                 |   |  | <u></u>  |                            |
|----------------|-------------------|---------|------------|---|---|--|---|-----------|-------------------|-----------------|---|--|--|----------------------------|
|                | Kruska            | Wallis  | Pr >       | 0.0006  | 0.0009<br>0.0008<br>0.0008  | 0.0008<br>0.0012<br>0.0012<br>0.0005                 | 0.0011<br>0.0012<br>0.0007  |           |                   |                 |   |  |  |                            |
|                | 1102 112          | ANOVA   | Ч          | <ul><li>.0001</li><li>0.0036</li><li>0.0529</li></ul> | 6001<br>6001<br>6001<br>6001<br>6001<br>6001                                      | 000<br>000<br>000<br>000<br>000<br>000<br>000<br>000 | <ul><li>&lt; 0001</li><li>&lt; 0001</li><li>&lt; 0001</li><li>&lt; 0001</li></ul> |           |                   |                 |   |  |  |                            |
| e e e e        |                   |         | Dev.       | 0.2<br>0.2<br>0.2                                     | 0.1<br>0.1<br>7.3   | 0.2<br>0.3<br>1.6                                    | 0.4   |           |                   |                 |   |  |  |                            |
| - Hort         |                   |         | ¥          | A 8 8   | <0<<  | ~ ~ ~ ~  | <b>444</b>  | 1         |                   |                 |   |  |  |                            |
| 7 - 7 Ohee     |                   | Call    | Mean       | 37.8<br>37.1<br>53.5                                  | 21.0<br>21.7<br>33.8<br>47.3  | 19.8<br>21.9<br>32.3<br>64.5                         | 44.4<br>30.9<br>30.3  |           |                   |                 |   |  |  |                            |
| 15 199         |                   | 1       | Dev.       | 0.3   | 0.2   | 202  | 0.3   | 1         |                   |                 |   |  |  |                            |
| Mav            |                   | JINE    | ¥          | ممم   | 0000  | 0000   | നനന   | 1         |                   |                 |   |  |  |                            |
| Thursday       |                   |         | lipaw      | 40.4<br>45.7<br>58.0                                  | 24.7<br>26.5<br>41.3<br>59.3  | 23.4<br>26.8<br>39.9<br>69.8                         | 52.8<br>37.8<br>32.8  |           |                   |                 |   |  |  |                            |
|                |                   | 200     | Dev.       | 2.3<br>12.0<br>6.6                                    | 22 22 22 22 22 22 22 22 22 22 22 22 22  | 1.9<br>3.3<br>1.9                                    | 2.1<br>2.6<br>1.8   |           |                   |                 |   |  |  |                            |
|                | 1                 | han     | ¥          | 4 4 <del>8</del>                                      | <b>« « « «</b>  | < < < <  | <b>« « «</b>  | 1         |                   |                 |   |  |  |                            |
|                | d                 |         | 1004       | 36.3<br>31.2<br>55.4                                  | 20.4<br>20.0<br>33.0<br>45.7  | 19.2<br>21.6<br>32.7<br>62.1                         | 43.4<br>30.5<br>28.7  |           |                   |                 |   |  |  |                            |
|                | Perd              | Secment | u buiño    | 225   | 22222   | ខខខខ   | 883   |           |                   |                 |   |  |  |                            |
|                | Kruskal<br>Wallie |         | chi-squate | 0.0008  | 0.0007<br>0.0008<br>0.0019<br>0.0019  | 0.0004<br>0.0007<br>0.0011<br>0.0011                 | 0.0012<br>0.0012<br>0.0012  |           | Kruskal<br>Waliia | Pr > chi-square | 0.0004<br>0.0011<br>0.0009                                    | 0.0007<br>0.0001<br>0.0008<br>0.0012         | 0.0035<br>0.0004<br>0.0012<br>0.0011   | 0.0009<br>0.0001<br>0.0039 |
| each cell      | ANOVA             | ц ^ ц   |            | 2000<br>1000<br>1000<br>1000                          | <ul><li>&lt;.0001</li><li>&lt;.0001</li><li>&lt;.0001</li><li>&lt;.0015</li></ul> | 0.0032<br>< 0001<br>< 0001                           | <ul><li>0001</li><li>0001</li><li>0002</li></ul>                                  | jej       | ANOVA             | Pr > F          | <ul><li>0001</li><li>0001</li><li>0001</li><li>0001</li></ul> | * 000<br>* 000<br>* 000<br>* 000<br>* 000    | <ul><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li><li>0001</li>&lt;</ul> | <.0001<br><.0001<br>0.0017 |
| ations in      |                   | Stand   | Dev.       | 0.1   | 0.00  | 0.1  | 0.2<br>0.3<br>0.7   | in each   |                   | Stand.<br>Dev.  | 0.2   | 3222   | 0.1<br>0.2<br>0.3  | 0.2                        |
| iviesd         | nated             |         | ¥          | ~ ~ ~   | <b>~ ~ ~ ~</b>  | <b>« « « «</b>                                       | <b>&lt; &lt; &lt;</b>   | tions     | ated              | ¥               | ०४४   | <0<<   | <0<<   | < 0 <                      |
| 97:79          | Callb             | Mean    |            | 36.8<br>37.0<br>53.3                                  | 20.9<br>21.7<br>33.8<br>50.5  | 19.7<br>21.8<br>32.2<br>66.3                         | 44.1<br>30.7<br>30.4  | 7 Observa | Calibr            | Mean            | 33.5<br>36.1<br>42.1  | 21.0<br>21.0<br>33.2<br>43.2                 | 19.9<br>21.7<br>32.0<br>49.0   | 42.9<br>29.6<br>24.4       |
| <u>v 14. 1</u> |                   | Stand   | Dev        | 0.2<br>0.2<br>1.6                                     | 0.1   | 0.1<br>2.2<br>2.2                                    | 0.2<br>0.3<br>0.9   | 1997 :    |                   | Stand.<br>Dev.  | 0.2<br>2.2<br>2.2   | 0.2<br>0.3<br>1.8                            | 0.1<br>2.0<br>2.0  | 0.4<br>1.3<br>1.3          |
| dev Mc         | fault             |         | ¥          | 000   | 0000  | 00000  | 000   | v 16      | ault              | ¥               | 000   |  | 0000   | 888                        |
| Wednesd        | ڴ                 | Mean    |            | 39.7<br>45.6<br>56.0                                  | 24.5<br>26.3<br>41.2<br>60.4  | 23.3<br>26.6<br>39.7<br>71.9                         | 52.7<br>37.7<br>32.7  | Friday Ma | Ğ                 | Mean            | 36.9<br>44.6<br>47.4  | 24.5<br>25.7<br>40.7<br>51.5                 | 23.3<br>26.5<br>39.4<br>55.9   | 51.4<br>36.5<br>27.0       |
| ſ              | _                 | Stand.  | Dev        | 1.6<br>0.8<br>0.8                                     | 1.4<br>2.4<br>1.4<br>1.4  | 5 0 3 5<br>5 5 3 5                                   | 2.8<br>1.5<br>1,4   |           |                   | Stand.<br>Dev.  | 3.7   | 3.1<br>2.0<br>2.3                            | 1.8<br>3.9<br>2.8  | 3.5<br>2.3<br>2.3          |
| 1              | 8                 |         | ¥          | < < <   | ~ ~ ~ ~   | ~~~  | <b>«</b> « «  |           | terved            | ¥               | < < <   | ~ ~ ~ ~                                      | <b>&lt;</b> < < <  | < < <                      |
|                | Serv              | -       |            |   |   |  |   |           | Qbs               | E S             |   |  | ~~~ ~ 10   |                            |
|                | Observ            | Mean    |            | 35.9<br>37.6<br>52.7                                  | 20.3<br>20.8<br>34.1<br>54.2  | 20.1<br>20.9<br>31.9<br>65.4                         | 43.2  |           |                   | Σ               | 8.9.8   | 81<br>30<br>18<br>18<br>18<br>18<br>18<br>18 | 30.20  | 29.9<br>23.0<br>23.0       |

Note: Tukeys Studentized Range Test (TK) = Means with the same letter are not significant at the 0.05 level

Second, the column labeled Kruskal Wallis Pr > chi-square, which is a nonparametric analog to ANOVA, gives the p-value for comparing the three groups. The numbers in this column are all well below 0.05 with the exception of Tuesday in which link D3 had a p-value of .0526, slightly greater than 0.05. Therefore similar conclusion can be drawn based on the non-parametric test.

Third, to determine which mean is different from the other, the Tukey's Studentized Range Test was used. Since there are three groups, Tukey's test will perform all pair wise comparisons. Observed vs. default, observed vs. calibrated, and default vs. calibrated.

The first comparison (observed vs. default): Looking at the columns labeled TK, abbreviation for tukey, one can see that the majority of the observed travel times and the default travel times through out the week have different letters beside their means. This is true along all road segments through out the week, with the exception of road segments B2 and C4 on Monday, B1 and D3 on Tuesday, and A3 on Thursday. In other words, from the possible 98 comparisons (14 segments \* 7 day) only 5 had similar means. Therefore, given the above one can conclude that there is a statistical significance at the 0.05 level between most of the observed travel times and the simulated travel times derived from the default model.

The second comparison (observed vs. calibrated): From table 4-4 it appears that the majority of road segments have similar letters beside their means. The observed travel times and the calibrated travel times are similar with the exception of road segments B4 on Saturday, B2 and D2 on Sunday, B2, C3 and D2 on Monday, B2 on Thursday, and A1, B2, C2 and D2 on Friday. Therefore, from the 98 possible comparisons 11

comparisons had different means. In summary, the tukey's test indicates that 87 (98-11) comparisons of travel times have no significant differences between the observed and calibrated travel times at the 0.05 significant level. This is a positive indication of how well the calibrated model performs in the test network. However, since a total of 4 road segments were significantly different on Friday (weak-end and low volume) it appears that the calibrated model doesn't predict as well under low traffic volumes.

The third comparison (default vs. calibrated): Looking at table 4-4 it can be seen that there are only 7 out of 98 comparisons which indicates that the means are similar. Therefore it can be said that there is a significant difference at the 0.05 level between the simulated travel times from both the default and calibrated Netsim model.

### Delay Time on Test Network "First Hour":

Looking at the statistical analysis of Delay Time on the Test Network during the first hour of observation (Table 4-5) the following comments and interpretations are drawn:

First, the column titled ANOVA Pr> F gives the p-values for comparing the three group means for route delay time. The majority of numbers in this column are above the reference probability of 0.05 set by this research for comparison purposes. From the 98 comparisons (14 \* 7), 37 comparisons have a p-value less than 0.05. This means that 37 comparisons suggests that the average groups are statistically significant while the reminder 61 comparisons suggests that there is no difference among the groups. The two days that showed the most differences among the groups are Sunday and Friday with 9 road segments and 8 road segments respectively.

| Table 4-5 | Statistical Analysis of Delay Time on Test Network "First Hour" | First hour of observation (12:30 - 13:30) |
|-----------|---|---|
|-----------|---|---|

.

| <u> </u>  | -       | _        |           |            | _      |        |              | -        |            |        |        | -      |   | _      | -      | -          |        |       | -      |             |        |       |               |          |              |         | -          |             |                |        | _       | • • •   | _          |                | _        |        | _      | _          | _      | _      |        |            |        | _ |
|-----------|---------|----------|-----------|------------|--------|--------|--------------|----------|------------|--------|--------|--------|---|--------|--------|------------|--------|-------|--------|-------------|--------|-------|---------------|----------|--------------|---------|------------|-------------|----------------|--------|---------|---------|------------|----------------|----------|--------|--------|------------|--------|--------|--------|------------|--------|---|
|           | Kruskal | Wallis   | Å         | chi-square |        | 710000 | 1600.0       | C01-0-0  | 0.0343     | 0.0138 | 0.1651 | 0.004  |   | 0.0081 | 0 0056 | 0.0014     | 0.0178 |       | 0.584  | 0.0079      | 0.865  |       |               | Krieksi  | Multin       |         | chi-souara | A RANKA TIA | 0.0264         | 0.0099 | 0./ 846 | 0.0504  | 0.0918     | 0.0375         | 0.0046   |        | 0.1633 | 0.1685     | 0.0314 | 0.0038 | 0.4606 |            | 0.0292 | - |
| 1         | li cell | ANOVA    | р, ч      |            | 1000   | 0000   | 0.0375       | 0.000    | 0.56       | 0 0096 | 0 7275 | 0.0049 |   | 0.0479 | 0.0035 | < 0001×    | 0.0123 |       | 0.398  | 0.0055      | 0.8195 |       |               | 11 7 61  | ANOWA        |         |            |             | 0.0986         | 0.0682 | 0.0900  | 0.6043  | 0.1866     | 0.3143         | 0.0247   |        | 8006.0 | 917.0      | 0.4342 | 1010.0 | AFLO O | 0.1573     | 0.0153 | : |
|           | 111 920 |          | Stand.    | Dev        | 60     | 20     | 4 U<br>2 7   | <u>;</u> | 6.0        | 0      | 03     | 9.0    |   | 0      | 0.2    | 0.3        | 1.8    |       | 0.2    | 0.2         | 4      |       | 1             |          |              | Stand   |            |             | 0.0            |        | -       | 0.1     | 0.2        | 5              | 7.5      | 3      | 5 6    |            |        | 0      | ĉ      | 03         | 12     |   |
| etion -   | lina    | brated   |           | ¥          | 4      | <      |              | i<br>C   | <          | а      | 4      | <      |   | A B    | •      | ۷          | ω      | -     | <      | A,B         | 4      | <br>1 |               |          | <b>Pater</b> |         | ¥          |             | ۷.             | ٩ «    | (       | ۲       | <          | <              | ۲        |        | • •    | ۲.         | < 0    |        | 4      |            | 8      | 1 |
| · 7 Ohean |         | Call     | Mean      |            | 107    |        | 804          | 2        | 3.7        | 2.3    | 2.9    | 34.3   |   | 3.6    | 2.4    | 2.9        | 50.0   |       | 7.2    | 3.9         | 22.0   |       | - 7 Obeau     | IASNA TT | Calib        | Mean    |            |             | 12.3           | 2.7    |         | 3.5     | 2.2        | 2.9            | 35.4     | 30     | 00     | 2 0        | R 7    | P. 77  | 22     | 3.7        | 21.8   |   |
| 1997      |         |          | Stand     | ð          | 60     | 10     |              | 2        | 0.1        | 0      | 0.2    | 1.7    |   | 0.1    | 0.1    | 0.1        | 1.2    |       | 0.3    | 0.4         | -<br>0 |       | 1007          |          |              | Stand   | ð          |             |                |        | 2       | 01      | 5          | 5              | 2.2      |        |        |            | 30     | 4      | 0.3    | 6.0        | 0.9    |   |
| Aav 1     |         | aut      |           | ¥          | œ      | •      |              | }        | <          | ۵      | <      | æ      |   | ß      | B      | æ          | 60     |       | <      | m           | ۲      | <br>1 | May 1         |          | autt         |         | ¥          | •           | < <            | <      | :       | <       | <          | <              | æ        | <      | < <    |            | c a    | 2      | <      | <          | 8      |   |
| Sundav A  |         | å        | Mean      |            | 10.0   | 3.3    | 42.0         |          | 3.3        | 2.5    | 3.2    | 40.9   |   | 3.4    | 2.8    | 3.8        | 49.8   |       | 7.2    | 4.5         | 22.2   |       | Tuesday       |          | Def          | Mean    |            | 0           | 0 C<br>0 C     | 7 U U  | 1       | 3.3     | 2.5        | 3.2            | 42.3     |        |        | 0 0<br>V 0 | 0.5    | 2      | 7.5    | 4.5        | 21.5   |   |
|           |         |          | Stand.    | Š          | 1.3    | 11     | 1.8          |          | 1.7        | 1.3    | 6.1    | 2.9    |   | 0.8    | 0.2    | 0.3        | 3.7    | 1     | 2.3    | 1.5         | 0.4    |       |               |          |              | Stand   | Dev.       | ,           | 7 <del>-</del> |        |         | 31      | 2.5        | -              | 1.5      | 44     |        | C          | 1      | ;      | 3.1    | 1.8        | 4.4    |   |
|           |         | <b>B</b> |           | ¥          | ۷      | <      | <            |          | <          | ۲      | <      | <      |   | <      | A B    | <          | <      |       | <      | <           | ۲      | 1     |               |          | Per          | F       | ¥          |             | ( <            | <      |         | <       | <          | < !            | A, B     | 4      | <      | ( 4        | (      | <br>:  | <      | ۲          | <      |   |
|           |         | Obse     | Mean      |            | 12.7   | 3.5    | 39.8         |          | 3.9        | 1.2    | 3.3    | 34.9   |   | 4.0    | 2.6    | 3.3        | 48.1   |       | 6.3    | 2.7         | 22.3   |       |               |          | Obsei        | Mean    |            | 40.4        | 5              | 40.0   |         | 4.2     | -          | 2.6            | 36.4     | 3.8    | , c    | - 0        | 45.8   |        | 7.2    | 3.5        | 23.4   |   |
|           |         | Road     | Segment   |            | A1     | R      | EA           |          | 6          | 82     | 8      | 8      |   | 5      | 8      | ខ          | 2      | 2     | 5      | 8           | 8      |       |               |          | Road         | Segment | ,          | 44          | 4              | 2      |         | 6       | 3          | 27             | 8        | 5      | 58     | 58         | 3 2    |        | б      | 8          | ឌ      |   |
|           | Kruskal | Wallis   | <u>ب</u>  | chi-square | 0.0165 | 0.0305 | 0.2998       |          | 0.0074     | 0.0846 | 0.0432 | 0.001  | : | 0.1149 | 0.0311 | 0.0308     | 0.0342 | 0.050 | SOC7 D | 0.0568      | 0.7227 |       |               | Kruskel  | Wallis       | Å.      | chi-square | 0.0014      | 0.0439         | 0.301  |         | 0.020   | 0.4151     | 9/90.0         | 0.0526   | 0.154  | 0.102  | 0 0035     | 0.2247 |        | 0.1464 | 0.0074     | 0.5327 |   |
| ch cell   |         | ANOVA    |           |            | 0.0052 | 0.3151 | 0.3656       |          | 0.0389     | 0.477  | 0.5352 | <.0001 |   | 0.3/14 | 0.7199 | 0.6656     | 0.0334 | 00000 | 0.000  | 0.3578      | 0.5279 |       | 1 cell        |          | ANOVA        | Pr > F  |            | 0000        | 0.2957         | 0.2862 | 0000    | 0.0428  | 1970.0     | 07.0           | 0.0946   | 0.3978 | 0.8368 | 0.0068     | 0.6673 |        | 0.2795 | 0.0038     | 0.3796 |   |
| 19 IN 98  |         |          | Stand.    | Š          | 0.3    | 0.2    | 2.3          |          | 0          | 5      | 6      | 6.2    | ; | 5      | 0.2    | 0.7        | 1.7    | ç     | N 0    | 0.0         | 0      |       | in eacl       |          |              | Stand.  | Dev        | 03          | 0.2            | 5      | 6       |         |            | - 9            | 0        | 0.1    | 01     | 0.2        | 1.7    |        | 0.3    | 0.3        | 1.6    |   |
| rvation   |         | ated     | Ì         |            | ۲      | ۲      | <            | 1        | 10         | <      | <      | 6      | • | ۲.     | <      | ۲.         | A,B    | <     |        | <           | ۲      |       | rations       |          | led          |         | ¥          | ٩           | •              | <      |         | 0 4     | < <        | < <            | ×        | <      | <      | 8          | ۲      |        | ۲      | AB<br>AB   | < ا    |   |
| . 7 Obse  | ;       | Callb    | Mean      |            | 13.1   | 2.5    | 41,4         | 1        | 3.7        | 2.3    | 2.8    | 38.1   | 6 | 5      | 4 6    | 2 E        | 49.9   | 7.4   | - 6    | 5.0         | 0.12   |       | 7 Obsen       |          | Callbr       | Mean    |            | 12.9        | 2.6            | 43.5   | r .     |         |            | 20.4           |          | 3.5    | 2.5    | 3.1        | 51.1   |        | 7.4    | 40         | 22.7   |   |
| 0. 199    |         |          | Stand.    | Ň          | 0.3    | 0.2    | 1.9          |          | 5 6        | 7.0    | 0.0    | 1.5    | 2 | 5      | 5      | 5          | 202    | 60    | 2      | 5           | Z.4    |       | 1997          |          | 1            | Stand.  | Ъ.         | 0.2         | 0.1            | 0.9    | 5       | 5 6     |            | 4 F            | N.       | 0.1    | 0.2    | 0.2        | 1.5    |        | 4      | 0.3        | 5      |   |
| May .     |         |          | È         | 4          | æ      | <      | <            |          | <          | < ·    | < (    | 8      | • | ~      | <      | < 1        | 10     | •     | ( <    | <           | <      |       | <b>Jay 12</b> |          | tin l        |         | ¥          | a           | ۲              | <      | 4       | <u></u> | ( <        | ( <            | ¢        | <      | ۲      | 8          | ۲      | _      | <      | <b>B</b> · | <      |   |
| Saturday  | (       | <u></u>  | URAM      |            | 10.4   | 3.3    | 42.8         |          | 4 u<br>5 c |        | 2.5    | 42.3   |   |        |        | 4 {<br>2 { | 1.20   | 7.3   |        | 4<br>0<br>0 | 0.77   |       | Monday A      |          | ð            | Mean    |            | 10.1        | 3.3            | 42.4   | **      |         | ) (<br>  ( | 444            | ļ        | 3.3    | 2.8    | 3.8        | 50.4   |        | 7.7    | 5.0        | 9.77   |   |
|           | _       | 1        |           | 5          | 2.3    | 5      | 4.5          | 1        | -          | -      | N C    | 2.8    | • |        | 0 M    |            | 0<br>4 | 30    |        | - c         | ţ      |       |               |          |              | Stand.  | <u>S</u>   | 1.9         | 2.7            | 2.8    | , ,     |         | 5 6        | ) <del>-</del> | <u>r</u> | 3.2    | 2.0    | 2.8        | 5.4    |        | 50     | 6, C       | RZ     |   |
|           |         |          | ž         |            | A, B   | ٩      | <            | 4        | (          | <      | •      | •      | < | < <    | ( <    | •          | ۲      | 4     | <      | < <         | ¢      |       |               |          |              | _       | ¥          | ۲           | <              | <      | •       | <       | <          | ( 4            | c        | ۲      | ۲      | <          | ۲      |        | < ۲    | < •        | -      |   |
|           | č       |          | Wc9       |            | 11.5   | 20     | <del>8</del> | ;        |            | - c    |        | R:07   | • | - c    | - c    | + C        | 41.0   | 68    |        | è è         |        |       |               | 1        | ő            | Mean    |            | 12.3        | 2.0            | 41.9   | 00      | ie      | • •        | 41.7           | -        | 4.6    | 2.5    | 0.7        | 50.4   |        | 8.4    | 2.6        | 21.4   |   |
|           | 2       | Section  | Tip: 1600 |            | ¥1     | 2      | 2            | ð        | ā 6        | 2 2    | 8 8    | 8      | 5 | 3 8    | 38     | 32         | 3      | δ     | 12     | 3 2         | 3      |       |               |          | Koad         | Segment |            | A1          | ¥              | ę      | ł       | i &     | 8          | 3 2            | 5        | δ      | 8      | ខ          | 2      | 1      | 58     | 38         | 3      |   |

Note: Tukey's Studentized Range Test (TK) = Means with the same letter are not significant at the 0.05 level

|            | <del></del>       |                        |                         | -                |        |            | _          |        |            | _               |        | _          |        | 71 | -             |         |        |                            |          |                            |                                      |                            |  |
|------------|-------------------|------------------------|-------------------------|------------------|--------|------------|------------|--------|------------|-----------------|--------|------------|--------|----|---------------|---------|--------|----------------------------|----------|----------------------------|--------------------------------------|----------------------------|--|
|            | Kruskal           | Pr >                   | 0.0042                  | 0.0078           | 0.0058 | 0.0185     | 0.0312     | 0 3801 | 0.1017     | 0.0997<br>0.002 | 0 796K | 0.0314     | 0.0192 |    |               |         |        |                            |          |                            |                                      |                            |  |
| ch cell    | ANOWA             | д ~ 1 <u>д</u>         | 0.0021                  | 0.2034<br>0.3072 | 0.0631 | 0.0343     | 0.3288     | 0 7068 | 0.7311     | 0.6593          | 0.6252 | 0.4458     | 0.0196 |    |               |         |        |                            |          |                            |                                      |                            |  |
| in ea      |                   | Stand.                 | 0.4                     | 10.2             | 0.1    | 5          | 1.0        | 00     | 0.2        | 1.6             | 40     | 0.3        | 1.2    |    |               |         |        |                            |          |                            |                                      |                            |  |
| Ivatios    | reter             | 4                      | <                       | <b>~</b> ~       | ۲      | A B        | 4 4        | 4      | <          | < 10            | •      | 4          | AB     |    |               |         |        |                            |          |                            |                                      |                            |  |
| 7 Obse     | C                 | Mean                   | 13.6                    | 2.8<br>40.4      | 3.8    | 2.4        | 33.2       | 3.5    | 2.5        | 3.1<br>48.5     | 7.5    | 40         | 22.2   |    |               |         |        |                            |          |                            |                                      |                            |  |
| 5, 1997    |                   | tand.                  | 0.2                     | 1.4              | 0.1    | 0.5        | 12         | 0.1    | 0.2        | 2.3             | 0.3    | 0.1        | ÷      |    |               |         |        |                            |          |                            |                                      |                            |  |
| May 15     | ž                 | ř                      | 60                      | ≪ ∢              | ۲      | ω.         | < 60       | <      | < •        | < 00            | <      | ۲          | 60     |    |               |         |        |                            |          |                            |                                      |                            |  |
| [hursday   | Def               | Mean                   | 10.6                    | 43.2             | 3.5    | 2.7        | 42.0       | 3.4    | 2.9        | 50.1            | 7.7    | 4.9        | 22.9   |    |               |         |        |                            |          |                            |                                      |                            |  |
|            |                   | Stand.                 | 23                      | 6.6              | 1.7    | 55         | 517        | 1,4    | 53         | 3.7             | 2.1    | 2.6        | 1.6    |    |               |         |        |                            |          |                            |                                      |                            |  |
|            | pev               | ¥                      | A,B                     | < <              | ۲      | < <        | (∢         | ۷      | ٨.         | < ∢             | ۲      | <          | ۲      |    |               |         |        |                            |          |                            |                                      |                            |  |
|            | Obse              | Mean                   | 12:4                    | 43.4             | 2.5    | 0 0<br>0 7 | 31.8       | 3.2    | 2.4        | 44.5            | 7.1    | 4.0        | 20.7   |    |               |         |        |                            |          |                            |                                      |                            |  |
|            | Road              | Segment                | A1<br>55                | ¥ 8              | 8      | 88         | 3 2        | δ      | 88         | 32              | δ      | 8          | 8      |    |               |         |        |                            |          |                            |                                      |                            |  |
|            | Kruekel<br>Waltis | Pr >                   | 0.0048                  | 0.382            | 0.0035 | 0.1272     | 0.0084     | 0.008  | 0.0309     | 0.0465          | 0.6024 | 0.0466     | 0.2727 |    |               | Kruekal | Pr >   | 0.0253<br>0.0504<br>0.0085 | 0.0049   | 0.0005<br>0.0671<br>0.0024 | 0.067<br>0.0048<br>0.00667<br>0.0025 | 0.6182<br>0.0004<br>0.2344 |  |
| ach cell   | ANOVA             | д<br>т                 | < 0001                  | 0.6871           | 0.0285 | 0.4999     | 0.0297     | 0.7287 | 0.3092     | 0.028           | 0.7462 | 0.0979     | 0.2918 |    | ell           | ANOVA   | Pr - F | 0.0506<br>0.2561<br>0.0031 | 0.021    | <.0001<br>0.5286<br>0.0027 | 0.089<br>0.0028<br>0.3808<br>0.0035  | 0.1217<br>0.0006<br>0.2448 |  |
| tions in e |                   | Stand.<br>Dev.         | 0.5                     | 0.7              | 6.1    | 55         | 1.7        | 0.1    | 0.0        | 4               | 0.2    | 6.0        | 0.7    |    | 1 each o      |         | Stand. | 0.2                        | 0.1      | 3202                       | 0.2                                  | 0.2                        |  |
| bserva     | rated             | ΤK                     | < <                     | < <              | ø.     | < <        | <          | ۲      | < <        | A,B             | ۲      | <          | <      | 1  | hons li       | atad    | ¥      | 00 < <del>0</del>          | B        | <b>n</b> < <               | × ¤ × ¤                              | < 8 <                      |  |
| 97 : 76    | Cellb             | Mean                   | 12.6                    | 41.2             | 3.7    | 5 B        | 36.4       | 3.5    | 9 9<br>9 0 | 50.3            | 7.4    | 3.9        | 22.4   |    | 7 Observi     | Caliby  | Mean   | 9.3<br>1.8<br>30.0         | 3.7      | 2.2<br>29.1                | 3.6<br>2.8<br>33.0                   | 6.2<br>2.8<br>16.3         |  |
| N 14.1     |                   | Stand.<br>Dev.         | 0.1                     | 1.6              | 0.1    | 0.2        | 1.5        | 0.2    | 5 5        | 2.2             | 0.3    | 0.3        | 6.0    | 1  | 1997          |         | Stand. | 0.1<br>0.2<br>2.2          | 0.2      | 1.8                        | 0.1                                  | 0.4<br>0.3<br>1.3          |  |
| day Ma     | sfault            | ¥                      | 62 ⊲                    | •                | A,B    | ₹ <        | 8          | < ۲    | < <        | 80              | ٩.     | <          | <      |    | <u>ay 16.</u> | fault   | Ě      | 8 × 8                      | A,B      | 0 < 0                      | < 00 < 00                            | < 00 <                     |  |
| ednes      | ۵                 | Mean                   | 10.0<br>3.4             | 41.1             | 3.3    | 3.2        | 43.0       | 3.3    | 3.8        | 52.3            | 7.6    | 4.8        | 22.8   |    | Friday M      | å       | Mean   | 7.2<br>2.4<br>32.5         | 3.3      | 27.0<br>34.2               | 3.4<br>2.7<br>3.6<br>36.2            | 6.3<br>3.6<br>17.1         |  |
| 5          |                   | _                      |                         |                  |        | 10         | 4          | 5      | 202        | 4.3             | 2.8    | 0          | 4.     |    | T             |         | Stand. | 3.7<br>2.7<br>4.1          | 3.1      | 53                         | 1.8<br>1.4<br>2.7                    | 3.5<br>2.4<br>2.2          |  |
| 5          |                   | Stand.<br>Dev          | 1.8<br>4.5              | 0.8              | ÷ 6    | vi roj     | -          |        |            |                 |        |            |        | 11 |               | pey     | - Y    |                            |          |                            |                                      |                            |  |
| N.         | served            | TK Dev.                | A 1.6<br>A 4.5          | A 0.8            | × •    | vi ei<br>  | A,B        | <      | < <        | ۲               | < ۲    | • >        | <      |    |               | ē       | F      | <b>«</b> « «               | ۷.       | ~ ~ ~                      | ~~~~                                 | <b>&lt; &lt; &lt;</b>      |  |
| 4          | Observed          | Mean Stand.<br>TK Dev. | 12.0 A 1.6<br>3.6 A 4.5 | 40.7 A 0.8       | 2.4 A  | 3.6 A 3.   | 40.2 A,B 1 | 4.0    | 3.0 A      | 47.7 A          | 6.9 A  | 9.6<br>V V | A 9.12 |    |               | Obser   | Mean   | 6.4 A<br>1.0 A<br>26.5 A   | 0.9<br>A | 30.0<br>30.0<br>30.0       | 4.6<br>0.9 A<br>29.9 A<br>29.9 A     | 4.2 A<br>0.2 A<br>15.7 A   |  |

Table 4-5 (continued) Statistical Analysis of Delay Time on Test Network "First Hour" First hour olobservation (12:30 - 13:30 )

Second, the column labeled Kruskal Wallis Pr > chi-square, which is a nonparametric analog to ANOVA, gives the p-value for comparing the three groups. The numbers in this column gives a different prospective. Here 61 comparisons have a pvalue less than 0.05 while the reminder 37 have a p-value greater than 0.05. Looking closely at the delay times presented in the table, it can be seen that the values are different. It appears that a 10% to 18% change between default and calibrated means (i.e. Saturday, Monday, and Wednesday on link B4) showed no statistical significance according to ANOVA. On the other hand, the Kruskal Wallis test on the same values showed statistical significance. To conclude that the means are significantly different based on the Kruskal-Wallis test can increase the probability of committing a type I error. This means rejecting the Null Hypothesis when it is true. Based on the above, for the data presented on delay time this research does not enough evidence to conclude that the means are significantly different.

However, from a practical point of view, it should be mentioned that the simulated delay values derived from the calibrated model seems closer to the observed values in comparison with the simulated values produced by the default model. <u>Travel Time on Test Network "Second Hour":</u>

Referring to the summary of statistical analysis of Travel Time on the Test Network during the second hour (Table 4-6) the following comments and interpretations are presented:

First, the column labeled ANOVA Pr > F gives the p-value for comparing the groups. The numbers in this column are all below the alpha value of 0.05 with the exception of road segment D3 on Mondays, and Thursdays in which the level of

| 11  |                 |                                   |   |  |   |                                  |  |  |   |  | _   |  |  |  |        |   | -   | · · ·                                 |  |                              |   | -  |            |  |  |  | -  |  | _  |   | _  | -  |
|---|-----------------|-----------------------------------|---|--|---|----------------------------------|--|--|---|--|---|--|--|--|--------|---|---|---------------------------------------|--|------------------------------|---|--|------------|--|--|--|--|--|--|---|--|--|
|   | Kruskal         | Wallie                            | Pr >  | 0 0012                                     | 0.0012                                      | 0.00                             | 0.001                                      | 0.0008                                     | 0.0008                                      | 0.0012   | 0.0002                                      | 0.0007                                       |  | 0.007  | 0.0113 |   |   | Kruskal                               | Walls                                    | chi-square                   | 0.0005  | 0.0008                                       | 0.0121     | 0.0015   | 0.0007   | 6000.0                                       | 0.0764                                       | 0.0016                                       | 0.001  | 0.0014                                    | 0.0012   | 0.0011                                       |
|   | h Cel           | ANOVA                             | н, F  | ¢ 000 ×                                    | <.0001<br>00000                             | 9000-0                           | <.0001                                     | 1000.×                                     | < 0001                                      | <.0001   | × 000                                       | 1000, A                                      | 6 000 s                                    | <000.*   | 600.0  |   | ch cell   | ANOUA                                 | EVONA<br>2 / 2                           |                              | < 0001  | <:0001                                       | 0.003/     | 0.0001   | 00<br>00<br>00<br>00<br>00<br>00<br>00<br>00<br>00<br>00<br>00<br>00<br>00 | 0.0042                                       | 0.0046                                       | 1000.2                                       | <.0001   | 0.0014                                    | <.0001   | <.0001<br>0.0218                             |
|   | s in eac        | -                                 | Stand.  | 0.2  | 0.2   | 2                                | 6.0  | 5 6  | 6.4   | 0.1  | 000   | 5 1 2  | 4  | 0.3  | 1.4    |   | is in eac   |                                       | Stand                                    |                              | 0.2   | 5.6  | <b>C</b> 7 | 0.1  |  | 5.5  | 60   | 0 7  | 4.0  | 2.7                                       | 0.3  | 0.3  |
|   | 19110U          | orated                            | Ĕ   | ×  | < <   | c                                | ۷.   | < <  | ۲   | ۲  | 0.  | < <  | . 4  | <  | ۲      |   | /atior  | - teter                               |  | ¥                            | U   | <  | ۲.         | ۲  | <del>ک</del> م   | <  | •  | <  | ۲  | ۲   | ۲  | < 8  |
|   | Ueson /         | Cali                              | Mean  | 40.1                                       | 37.1  | 0.00                             | 210  | 33.7                                       | 51.4  | 19.8   | 21.9  | 32.5<br>71.6                                 | 44.6                                       | 31.4   | 31.8   |   | : 7 Obser   | -<br>LieO                             | Mean                                     |                              | 37.7  | 37.1   | 2.00       | 21.1   | 21.9<br>34.0   | 56.3   | 19.9   | 22.3   | 33.1   | 69.4                                      | 44.6   | 31.4<br>32.8                                 |
|   | 1441            |                                   | Stand.<br>Dev.                                      | 1.5  | 0.6<br>3.5                                  | 2                                | 0.5  | 0.0  | 1.9   | 0.1  | 0 0   | 5 6<br>7 7                                   | 0.2  | 0.3  | 4      |   | 3, 1997   |                                       | Stand                                    | à                            | 0.2   | 0,0  | 2          | 5  | 7 7  | 12   | 0.2  | 0.2  | 0.2  | 8.8                                       | 0.4  | 0.3  |
|   | A A             | Bult                              | ¥   |  | co a  | )                                | 0.0  | 0 00                                       | 8   | Ð  | œ 0   | 0 00   | ۵  | æ  | ۵      |   | Aav 1   | ŧ                                     |  | ¥                            | 8   | ۵ ۵  | 0          | •  | 0 00   | æ  | ß  | 60   | æ  | 8   | æ  | 8 8  |
|   | AND             | ð                                 | Mean  | 37.1                                       | 45.8<br>61 2                                |                                  | 24.6<br>28.5                               | 41.2                                       | 61.8  | 23.3   | 26.9<br>70 0                                | 79.4   | 52.9                                       | 38.3   | 34.7   |   | <b>Tuesday h</b>                                  | Defe                                  | Mean                                     |                              | 40.2  | 46.0<br>81 5                                 | 2          | 24.7   | 41.3   | 62.8   | 23.6   | 27.2   | 40.7   | 80.2                                      | 53.0   | 38.4<br>34.8                                 |
|   |                 |                                   | Stand.<br>Dev.                                      | 0.2  | <u>.</u> 6                                  |                                  | 9.5  | 17   | 10  | 11   |   | 5 6<br>7 8                                   | 2.4  | 2.1  | 3.0    |   | Ī   | _                                     | Stand.                                   | <u>Sev</u>                   | 0.7   | 9 0  | 3          | 2.8  | 2.5  | 3.5  | 3.2  | 2.2  | 2.5  | 1.5                                       | 2.6  | 23   |
|   |                 | BS                                | R   | ۷  | < <   |                                  | < <  | <  | <   | ٨.   | < 4   | <  | <  | < ۲  | <      |   |   | bey                                   | Γ  | ¥                            | < ۲   | < 4  | :          | < <  | <  | ۲  | A,B  | <  | < ۲  | ۸   | ٨.   | < <  |
|   |                 | Obse                              | Mean  | 37.1                                       | 37.1<br>56.7                                |                                  | 20.3                                       | 32.7                                       | 49.0  | 19.5   | 4 C C                                       | 70.8   | 44.0                                       | 29.8   | 30.9   |   |   | Obser                                 | Mean                                     |                              | 37.0  | 36.4<br>55.0                                 |            | 20.0   | 32.9   | 55.5   | 21.2   | 23.7   | 32.2   | 69.1                                      | 43.3   | 30.5<br>32.2                                 |
|   |                 | Road                              | Segment   | A1   | 8 8   | 2                                | 5 2  | 8  | 2   | 58   | 38  | 33   | δ  | 81   | 3      |   |   | Road                                  | Segment                                  | •                            | ¥.  | 2 2  |            | <u>ب</u>   | 8  | 2  | δ  | 8  | 83   | 8   | 58   | 88   |
|   | Ē               | <u>.</u>                          | vare v  | 8  | <u>چ</u>                                    | ę                                | 58   | 8  | -   | 88   | 2 4   | 6  | 2  | 2 9  | 2      | T | ŀ   | ē. e                                  |  | are                          | ŝ   | 24   |            |  | - 4  | 8  |  |  |  | 4   | _ •  | <b>ი</b> ო                                   |
|   | 1 💇 '           |                                   | ~ 31  | - O (                                      | <u> </u>                                    |                                  |  | ō  | -   |  |   |  |  |  | ñ.     |   | - 13  |                                       | ~  | 5                            | - 5 2   | ະຫຼ  | •          |  | _  |  | _  |  |  |   | òS   | 201  |
|   | ž               | Š                                 | 방   | 0.0  | 0.0   |                                  |  | 8  | 00.0  | 88   | 88  | 800  | 8.0  | 0.0  | 5      |   |   | Val<br>Val                            | <u>م</u>                                 | Ch-B                         | 0.0   | 50   |            | 88   | 800  | 0.0  | 0.00   | 0.00   |  | 0.0                                       | 0.2  | 38   |
| ach call  | Ę               | ANOVA W                           | Pr > F  | 0.0086 0.0                                 | 0.0003                                      | 1000                             | 1000                                       | < 0001                                     | <.0001 0.00                                 | <ul> <li>.0001</li> <li>.0001</li> <li>.0004</li> <li></li></ul> | × 0001                                      | 0.008  | <.0001 0.00                                | c.0001   | 0.003  |   | h celi  | ANOVA Wal                             | ъ.<br>ъ.<br>ъ.                           | Chi-9                        | <ul> <li>- 0001</li> <li>- 0001</li></ul> | 0.0161 0.01                                  |            | <ul> <li>0.00</li> <li>0.00</li> <li>0.00</li> <li>0.00</li> </ul>                     | <.0001   | <.0001 0.000                                 | <.0001 0.000                                 | <.0001 0.001                                 | 0.000  |   | <ul> <li>× 0001</li> <li>× 0001</li> <li>× 0001</li> <li>× 0001</li> </ul>           | 0.4201 0.38                                  |
| ns in each cell                                     | Ţ               | ANOVA W                           | Dev. Pr > F F Chi-s                                 | 0.2 0.0086 0.0                             | 1.3 0.0003 0.0                              | 0.1<br>0.0                       | 0.2 < 0.00                                 | 0.2 < 0001 0.0                             | 4./ <.0001 0.00                             | 0.1 <.0001 0.00  | 0.3 < 0001 0.00                             | 1.9 0.008 0.00                               | 0.2 <.0001 0.00                            | 0.2 <.0001 0.00  |        |   | s in each cell                                    | ANOVA Wal                             | Stand Pr > F Pr                          | Dev. Chi-a                   | 0.4 < 0001 0.0  | 1.3 0.0161 0.01                              |            | 0.1 <.0001 0.00  | 0.2 <.0001 0.000   | 1.6 <.0001 0.000                             | 0.1 <.0001 0.000                             | 0.1 <.0001 0.001                             | 0.2 <.0001 0.000   | 0.00                                      | 0.3 <.0001 0.0   | 1.1 0.4201 0.38                              |
| rvations in each call                               | Ţ               | ated ANOVA We                     | TK Dev Pr>F Chi-                                    | A 0.2 0.0086 0.0                           | A 1.3 0.0003 0.0                            | A 0.1                            | A 0.2 <0001 0.00                           | A 0.2 <.0001 0.0                           | A 4.7 <.0001 0.00                           | A 0.1 <0001 0.00   | C 0.3 <0001 0.00                            | A 1.9 0.0008 0.00                            | A 0.2 <.0001 0.00                          | A 0.2 <.0001 0.00  |        |   | rations in each cell                              | ated ANOVA Wal                        | Stand Pr > F Pr                          | TK Dev. Chi-a                | A 0.4 < 0001 0.0  | A 1.3 0.0161 0.01                            |            | A 0.1 <.0001 0.00<br>A 0.2 < 0001 0.00   | C 0.2 < 0001 0.000   | A 1.6 <.0001 0.000                           | C 0.1 <.0001 0.000                           | A 0.1 <.0001 0.001                           | A 0.2 <.0001 0.000   | A 1.6 <.0001 0.000                        | A 0.3 < 0001 0.0   | A 1.1 0.4201 0.38                            |
| 7: 7 Observations in each call                      | Ϋ́Υ.            | Calibrated ANOVA We               | Mean Stand Pr > F F F                               | 37.5 A 0.2 0.0086 0.0                      | 55.2 A 1.3 0.0003 0.0                       |                                  | 21.8 A 0.2 <0001 0.00                      | 33.9 A 0.2 < 0001 0.0                      | 0.00 × 0.001 0.00                           | 19.9 A 0.1 < 0001 0.00   | 32.8 C 0.3 <0001 0.00                       | 66.4 A 1.9 0.0008 0.00                       | 44.2 A 0.2 < 0001 0.00                     | 31.1 A 0.2 <0001 0.00  |        |   | : 7 Observations in each cell                     | Celibrated ANOVA Val                  | Mean Stand Pr > F Pr                     | TK Dev chia                  | 37.5 A 0.4 < 0001 0.0   | 56.1 A 1.3 0.0161 0.01                       |            | 21.1 A 0.1 <0001 0.00<br>21.8 A 0.2 <0001 0.00   | 33.8 C 0.2 < 0001 0.000  | 56.6 A 1.6 <.0001 0.000                      | 19.9 C 0.1 <.0001 0.000                      | 22.3 A 0.1 <.0001 0.001                      | 33.0 A 0.2 < 0001 0.000<br>699 A 16 2001 2000                            | 09:3 A 1.6 <.0001 0.000                   | 44.3 A 0.3 < 0001 0.0  | 32.3 A 1.1 0.4201 0.38                       |
| 10. 1997:7 Observations in each call                | Ϋ́Υ.            | Calibrated ANOVA We               | stand. Mean Stand. Pr > F F<br>Dev. TK Dev. chi-    | 0.4 37.5 A 0.2 0.0086 0.0                  | 2.6 55.2 A 1.3 0.0003 0.0                   |                                  | 0.2 21.8 A 0.2 <0001 0.00                  | 0.2 33.9 A 0.2 < 0001 0.0                  | 1.0 00.0 A 4.7 < 0001 0.00                  | 0.2 19.9 A 0.1 < 0001 0.00<br>0.1 222 A 0.1 20001 0.00   | 0.2 32.8 C 0.3 <0001 0.00                   | 5.1 66.4 A 1.9 0.0008 0.00                   | 0.2 44.2 A 0.2 <0001 0.00                  | 0.2 31.1 A 0.2 <0001 0.00  |        |   | . 1997 : 7 Observations in each cell              | Calibrated ANOVA Val                  | Stand Mean Stand Pr > F Pr               | Dev. IK Dev. chia            | 0.3 37.5 A 0.4 < 0.001 0.0  | 5.0 56.1 A 1.3 0.0161 0.01                   |            | 0.1 21.1 A 0.1 <0001 0.00<br>0.1 21.8 A 0.2 <0001 0.00                                 | 0.1 33.8 C 0.2 < 0001 0.000  | 1.6 56.6 A 1.6 <.0001 0.000                  | 0.1 19.9 C 0.1 <.0001 0.000                  | 0.1 22.3 A 0.1 <.0001 0.001                  | U.Z 33.0 A 0.2 <0001 0.000<br>17 609 A 16 20001 2000                     | 1.7 08.8 A 1.8 <.0001 0.000               | 0.2 44.3 A 0.3 < 0.01 0.0<br>03 314 A 0.2 < 0001 0.0                                 | 2.2 32.3 A 1.1 0.4201 0.30                   |
| May 10, 1897 ; 7 Observations in each call          | K2              | Bult Calibrated ANOVA We          | tk Dev. Mean Stand Pr > F F                         | B 0.4 37.5 A 0.2 0.0086 0.0                | B 2.6 55.2 A 1.3 0.0003 0.0                 |                                  | B 0.2 21.8 A 0.2 <0001 0.00                | B 0.2 33.9 A 0.2 <0001 0.0                 | a 1.9 33.2 A 4.7 <0001 0.00                 | B 0.2 19.9 A 0.1 <0.001 0.00<br>B 0.1 222 A 0.1 2.0001 0.00  | B 0.2 32.8 C 0.3 <0001 0.00                 | B 5.1 66.4 A 1.9 0.0008 0.00                 | B 0.2 44.2 A 0.2 < 0001 0.00               | B 0.2 31.1 A 0.2 <0001 0.00  |        |   | lav 12. 1997 : 7 Observations in each cell        | ault Celibrated ANOVA Val             | Stand Mean Stand Pr > F Pr               | TK Dev. TK Dev. chia         | B 0.3 37.5 A 0.4 <0001 0.0  | B 5.0 56.1 A 1.3 0.0161 0.01                 |            | B 0.1 21.1 A 0.1 <0001 0.00<br>B 0.1 21.8 A 0.2 <0001 0.00                             | B 0.1 33.8 C 0.2 < 0001 0.000  | B 1.6 56.6 A 1.6 <0001 0.000                 | B 0.1 19.9 C 0.1 < 0001 0.000                | B 0.1 22.3 A 0.1 <0001 0.001                 | B U.Z 33.U A 0.2 <0001 0.000<br>B 17 699 A 16 2005 0.000                 | 0.000 V. 0.000 V. 0.000 V. 0.000 V. 0.000 | B 0.2 44.3 A 0.3 <0001 0.0<br>B 0.3 314 A 0.2 <0001 0.0                              | A 22 323 A 11 0.4201 0.30                    |
| Saturday May 10, 1997 : 7 Observations in each ceil | Pda #           |                                   | wean Stand. Mean Stand. Pr>F F                      | 40.2 B 0.4 37.5 A 0.2 00086 0.0            | 60.9 B 2.6 55.2 A 1.3 0.0003 0.0            | 246 B 01 210 A 01 2000           | 26.5 B 0.2 21.8 A 0.2 <0001 0.0            | 41.3 B 0.2 33.9 A 0.2 <0001 0.0            | 0.00 1.0 20.2 A 4.7 < 0001 0.00             | 23.5 B 0.2 19.9 A 0.1 <0001 0.00<br>27.1 B 0.1 222 A 0.1 <0001 0.00  | 40.5 B 0.2 32.8 C 0.3 <0001 0.00            | 74.8 B 5.1 66.4 A 1.9 0.0008 0.00            | 527 B 0.2 44.2 A 0.2 <0001 0.00            | 35.2 B 1.8 31.1 A 0.2 <0001 0.00   |        |   | Monday May 12. 1997 : 7 Observations in each cell | Default Cellbrated ANOVA Wal          | Mean Stand Mean Stand Pr > F Pr          | TK Dev. TK Dev Chia          | 40.2 B 0.3 37.5 A 0.4 < 0001 0.0<br>461 B 1.0 37.5 A 0.4 < 0001 0.0   | 60.8 B 5.0 56.1 A 1.3 0.0161 0.01            |            | 24.0 B 0.1 21.1 A 0.1 <0001 0.00<br>26.4 B 0.1 21.8 A 0.2 <0001 0.00                   | 41.3 B 0.1 33.8 C 0.2 < 0001 0.000   | 62.0 B 1.6 56.6 A 1.6 <0001 0.000            | 23.6 B 0.1 19.9 C 0.1 <.0001 0.000           | 27.1 B 0.1 22.3 A 0.1 <0001 0.001            | 745 B 17 600 A 16 2001 0.000   |   | 52.9 B 0.2 44.3 A 0.3 <0001 0.0<br>38.2 B 0.3 31.4 A 0.2 7.0001 0.0                  | 33.6 A 22 32.3 A 1.1 0.4201 0.30             |
| Saturday May 10, 1897 : 7 Observations in each call | Ka<br>Ka        | Calibrated ANOVA We               | orana. wean stand. Pr>F F<br>Dev TK Dev TK Dev Chis | 31 402 B 0.4 375 A 0.2 0.0086 0.0          | 3.3 60.9 B 2.6 55.2 A 1.3 0.0003 0.0        | 20 246 B 01 210 A 01 2004        | 3.0 26.5 B 0.2 21.8 A 0.2 <0001 0.0        | 22 413 B 0.2 33.9 A 0.2 <0001 0.0          | 1.3 04.3 0 1.3 03.2 A 4.7 <0001 0.00        | 1.3 23.5 B 0.2 19.9 A 0.1 < 0001 0.00<br>2.1 27.1 B 0.1 222 A 0.1 - 0001 0.00  | 1.1 40.5 B 0.2 32.8 C 0.3 <0001 0.00        | 3.7 74.8 B 5.1 66.4 A 1.9 0.0008 0.00        | 3.5 52.7 B 0.2 44.2 A 0.2 <0001 0.00       | 25 35 35 1 0.2 31.1 A 0.2 <0001 0.00   |        |   | Monday May 12, 1997 ; 7 Observations in each cell | Default Celibrated ANOVA Wal          | Stend Mean Stand Mean Stand Pr > F Pr    | Dev. TK Dev. TK Dev. chia    | 2.0 40.2 B 0.3 37.5 A 0.4 <.0001 0.0<br>08 481 B 10 37.5 A 0.4 <.0001 0.0   | 1.8 60.8 B 5.0 56.1 A 1.3 0.0161 0.01        |            | 2.3 2.4.0 B 0.1 21.1 A 0.1 <0001 0.00<br>2.3 26.4 B 0.1 21.8 A 0.2 <0001 0.00          | 2.0 41.3 B 0.1 33.8 C 0.2 <0001 0.00                                       | 1./ 62.0 B 1.6 56.6 A 1.6 <0001 0.000        | 1.2 23.6 B 0.1 19.9 C 0.1 <0001 0.000        | 2.8 27.1 B 0.1 22.3 A 0.1 <0001 0.001        | 34 40.0 B 0.2 33.0 A 0.2 <0001 0.000<br>1.2 745 B 17 600 A 18 2001 0.000 |   | 2.6 52.9 B 0.2 44.3 A 0.3 <0001 0.0<br>2.2 38.2 B 0.3 31.4 A 0.7 7 0004 0.00         | 22 33.8 Å 22 32.3 Å 11 0.4201 0.30           |
| Saturday May 10, 1997 : 7 Observations in each ceil |                 | Pryod Default Calibrated ANOVA We | TK Dev. TK Dev. TK Dev. Chis                        | A 31 40.2 B 0.4 37.5 A 0.2 0.0086 0.0      | A 3.3 60.9 B 2.6 55.2 A 1.3 0.0003 0.0      | A 20 246 B 01 210 A 01 7000 02   | A 3.0 26.5 B 0.2 21.8 A 0.2 <0001 0.00     | A 22 41.3 B 0.2 33.9 A 0.2 <0001 0.0       | A 1.9 0.00 1.9 03.2 A 4.7 <.0001 0.00       | A 113 23.5 B 0.2 19.9 A 0.1 <0001 0.00<br>A 21 271 B 0.1 222 A 0.1 0.00  | A 1.1 40.5 B 0.2 32.8 C 0.3 <0001 0.00      | A 3.7 74.8 B 5.1 66.4 A 1.9 0.0008 0.00      | A 35 527 B 02 442 A 02 <0001 0.00          | A 1.4 00.2 B 0.2 31.1 A 0.2 <0001 0.00<br>A 25 35 35 1 1 1 1 2 2 5 5 5 5 5 5 5 5 5 5 5 5 5 |        |   | Monday May 12, 1997; 7 Observations in each cell  | arrus Celibrated ANOVA Val            | Stend Mean Stand Mean Stand Pr > F       | TK Dev. TK Dev. TK Dev Cohia | A 2.0 40.2 B 0.3 37.5 A 0.4 <0001 0.01<br>A 0.8 461 B 1.0 37.5 A 0.4 <0001 0.01   | A 1.8 60.8 B 5.0 56.1 A 1.3 0.0161 0.01      |            | A 2.3 28.4 B 0.1 21.1 A 0.1 50001 0.00<br>A 2.3 28.4 B 0.1 21.8 A 0.2 50001 0.00       | A 2.0 41.3 B 0.1 33.8 C 0.2 <0001 0.000                                    | A 1.7 62.0 B 1.6 56.6 A 1.6 <0001 0.000      | A 1.2 23.6 B 0.1 19.9 C 0.1 <0001 0.000      | A 2.8 2/1 B 0.1 22.3 A 0.1 <0001 0.001       | A 1.2 745 A 17 600 A 16 7001 0.000                                       |   | A 2.6 52.9 B 0.2 44.3 A 0.3 <0001 0.0<br>A 2.2 38.2 B 0.3 31.4 A 0.2 7001 0.00       | A 22 338 A 22 32.3 A 1.1 0.4201 0.30         |
| Saturday May 10, 1997 : 7 Observations In each call | Cheaned Cheaned | VOSERVED ANOVA WE                 | mean Stand Mean Stand Pr>F F                        | 37.0 A 3.1 40.2 B 0.4 37.5 A 0.2 00086 0.0 | 54.4 A 3.3 60.9 B 2.6 55.2 A 1.3 0.0003 0.0 | 19.8 A 20 246 B 01 210 A 01 2001 | 20.9 A 3.0 26.5 B 0.2 21.8 A 0.2 <0001 0.0 | 32.2 A 2.2 41.3 B 0.2 33.9 A 0.2 <0001 0.0 | 2000 V 1:2 04:3 0 1:3 05:2 V 4.7 <0001 0.00 | 203 A 113 235 B 0.2 19.9 A 0.1 <0001 0.00<br>220 A 21 271 B 0.1 222 A 0.1 -0001 0.00   | 31.8 A 1.1 40.5 B 0.2 32.8 C 0.3 <0001 0.00 | 68.9 A 3.7 74.8 B 5.1 66.4 A 1.9 0.0008 0.00 | 42.3 A 3.5 527 B 0.2 44.2 A 0.2 <0001 0.00 | 318 A 25 35 20 1 1 4 0.00 0.00 0.00 0.00 0.00 0.00 0.                                      |        |   | Monday May 12, 1997 : 7 Observations in each cell | Observed Default Celibrated ANOVA Val | Mean Stand Mean Stand Mean Stand Pr F Pr | TK Dev. TK Dev. TK Dev. CHI3 | 367 A 2.0 40.2 B 0.3 37.5 A 0.4 <0001 0.01<br>37.5 A 0.8 461 B 1.0 37.5 A 0.4 <0001 0.01  | 56.1 A 1.8 50.8 B 5.0 58.1 A 1.3 0.0161 0.01 |            | 21.0 A 1.0 24.0 B 0.1 21.1 A 0.1 <0001 0.00<br>22.4 A 2.3 26.4 B 0.1 21.8 A 0.2 cmm mm | 31.7 A 2.0 41.3 B 0.1 33.8 C 0.2 <0001 0.00                                | 33.2 A 1.7 52.0 B 1.6 58.6 A 1.6 <0001 0.000 | 21.0 A 1.2 23.6 B 0.1 19.9 C 0.1 <0001 0.000 | 21.7 A 2.8 27.1 B 0.1 22.3 A 0.1 <0001 0.001 | 881 A 1.2 745 A 1.7 600 A 1.6 2001 0.000                                 |   | 42.8 A 2.6 52.9 B 0.2 44.3 A 0.3 <0001 0.0<br>30.7 A 2.2 38.2 B 0.3 31.4 A 0.7 7 000 | 32.7 A 2.2 33.6 A 2.2 32.3 A 1.1 0.4201 0.30 |

Table 4-6 Statistical analysis of Travel Time on Test Network "Second Hour" Second hour observation (13:30 - 14:30)

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Note: Tukey's Studentized Range Test (TK) = Means with the same letter are not significant at the 0.05 level

Table 4.6 (continued) Statistical analysis of Travel Time on Test Network "Second Hour" Second hour observation ( 13:30 - 14:30 )

|           | 1                |              | -          | ,        |                 |             |        | -          | -      |               |        | -          | -                          |        |            |             |        |   | 1   |         | -        |         |            |            |              | <u></u> | -    |              | 1             |              |              |              |      |                      |       |
|-----------|------------------|--------------|------------|----------|-----------------|-------------|--------|------------|--------|---------------|--------|------------|----------------------------|--------|------------|-------------|--------|---|---|---------|----------|---------|------------|------------|--------------|---------|------|--------------|---------------|--------------|--------------|--------------|------|----------------------|-------|
|           | Kruekal          | Wallis       | Chi-eonare |          |                 | 0.0012      | 0000   | 00000      |        | 0.0013        |        | 100.0      | 0 0004                     | 0.0024 |            |             | 0.1954 |   |   |         |          |         |            |            |              |         |      |              |               |              |              |              |      |                      |       |
| ch call   |                  | ANOVA        | -<br>-     | 1000     |                 | 000         |        |            |        | , 000<br>1000 | 1000   |            | × 000                      | 0.0055 | 1000       | 1000        | 0.3497 |   |   |         |          |         |            |            |              |         |      |              |               |              |              |              |      |                      |       |
| ns in ea  |                  |              | Dev.       | 6        | 200             | ; [         | 5      | 100        | : 2    | 4             | 5      | 5 6        | 5                          | 2.3    | 50         | 0.0         | 15     |   | 1   |         |          |         |            |            |              |         |      |              |               |              |              |              |      |                      |       |
| ervatio   |                  | brated       | ¥          |          | <               | <           | <      | <          | . 4    | <             | <      | <          | ٩                          | ۲      | C          | ~           | <      |   | 1   |         |          |         |            |            |              |         |      |              |               |              |              |              |      |                      |       |
| 7:7 Obs   |                  | Call         | lipaw      | 37.6     | 37.3            | 57.1        | 24.4   | 219        | 33.9   | 58.0          | 19.0   | 22.2       | 32.9                       | 70.7   | 44 G       | 31.4        | 32.4   |   |   |         |          |         |            |            |              |         |      |              |               |              |              |              |      |                      |       |
| 15, 199   |                  | Chand        | Dev.       | 0,2      | 8.8             | <b>6</b> .6 | 00     | 0          | 00     | 3.2           | 60     | 50         | 0.3                        | 9.2    | 0.3        | 0.3         | 4.4    |   |   |         |          |         |            |            |              |         |      |              |               |              |              |              |      |                      |       |
| y May     |                  | laut         | Я          | 8        | æ               | 8           | đ      | р          | 8      | æ             | a      | 60         | 8                          | 8      | 8          | 0           | ۲      | _ | 1   |         |          |         |            |            |              |         |      |              |               |              |              |              |      |                      |       |
| Thursda   | 1                | Mean         |            | 40.5     | 52.1            | 73.1        | 24.8   | 26.6       | 41.3   | 66.3          | 23.6   | 27.0       | 40.3                       | 79.8   | 52.8       | 38.1        | 33.9   |   |   |         |          |         |            |            |              |         |      |              |               |              |              |              |      |                      |       |
|           |                  | Stand        | Dev.       | 1.9      | 1.4             | 0.8         | 2.5    | 2.0        | 3.8    | 3.2           | 1.7    | 1.5        | 2.4                        | 2.2    | 2.9        | 3.0         | 2.5    |   |   |         |          |         |            |            |              |         |      |              |               |              |              |              |      |                      |       |
|           |                  |              | ¥          | •        | ۲               | ۲           | <      | <          | <      | ۲             | ٨      | ۲          | ۷.                         | <      | ۲          | ۲           | ۲      |   | 1   |         |          |         |            |            |              |         |      |              |               |              |              |              |      |                      |       |
|           | ð                | Mean         |            | 36.9     | 34.4            | 56.3        | 22.1   | 20.8       | 32.9   | 56.6          | 20.2   | 21.7       | 31.4                       | 63.5   | 42.2       | 30.8        | 33.2   |   |   |         |          |         |            |            |              |         |      |              |               |              |              |              |      |                      |       |
|           | 1                | Segment      | •          | Ł        | Ş               | EA.         | 8      | <b>B</b> 2 | 8      | 2             | 5      | 8          | ខ                          | 3      | Б          | 8           | 8      |   |   |         |          |         |            |            |              |         |      |              |               |              |              |              |      |                      |       |
|           | Kruskel<br>Watte | - 1 <u>-</u> | chi-square | 0.0064   | 0.0012          | 0.0004      | 0.0012 | 0.0061     | 0.0008 | 0.0047        | 0.0217 | 0.0012     | 0.0012                     | 1810.0 | 0.0012     | 0.0001      | 0.0018 |   |   | Kruskal | Wallis   | â       | cni-square | 0.0003     | 0.0004       | 900     |      | 0.0006       | 0.0008        | 0.0059       | 0.0008       | 0.0011       |      | 0.0012               | 10.0  |
| each cell | ANOVA            | Pr>F         |            | 0.0002   | ×<br>600<br>600 | × 0001      | <.0001 | <:0001     | ×.0001 | 0.0034        | 0.0047 | < 0001     | 1000.v                     | 70+0.0 | <:0001     | ×.000       | 0.002  |   | lloo  |         | ANOVA    | Pr > F  |            | <.0001     | 000          | 1000    |      | × 000        | <.000<br>2000 | 0.0003       | <.0001       | 500          |      | 6001<br>6001<br>6001 | 70000 |
| ations in |                  | Stand.       | Å          | 0.2      | 0.2             | 1.8         | 0.1    | 0          | 0.0    | <b>4</b><br>8 | 0.2    | 0.2        | 2 a<br>4 c                 | 7.0    | 5          | 0.2         | 1.7    |   | - Hoe C   |         |          | Stand   |            | 0.1        | 11           | 5       |      | 60           | N<br>0        | 0.1          | 0.1          | 5 G<br>7 G   |      | 0.0.4                | 2     |
| bservi    | reted            |              | ¥          | ۲        | <               | υ           | <      | •          | <      | <             | ۲      | < ۲        | < <                        | ¢      | 4          | 0           | •      |   | those is a large state of the second state of |         | ated     | È       | 1          | υ          | υ <b>⊲</b>   | 4       | ( () | < •          | <             | ۲            | ۲.           | 4 ح          |      | < U ∢                |       |
| 997.7C    | Callb            | Mean         |            | 37.2     | 37.5            | 56.4        | 21.0   | 21.7       | 33.8   | 54.9          | 19.9   | 22.2       | 1.55                       |        | 44.7       | 31.5        | 33.3   |   | 7 Oheany  |         | Calibi   | Mean    |            | 34.1       | 36.2<br>45.1 | 20.0    | 212  | 33.4         | 1.40          | 19.7         | 21.2         | 55.1<br>55.1 |      | 30.0                 |       |
| y 14, 1   |                  | Stand        | ð          | 0.3      | 2 0             | 1.8         | 0.2    | 0.0        | 5      |               | 0.     | 0.2        | 20                         | 4      | 0.4        | 9.0         | 1.3    |   | 1997  |         |          | Stand.  |            | 0.2        | 1.7          | 00      | 00   | 0.5          | 5             | 0.2          | 200          | 15           |      | 0.1                  |       |
| dev Ms    | fault            |              | ¥          | 6        | 0 0             | n           | •      | -          | 20 0   | 8             | 8      | 60 (       | 0 0                        | 3      | ωı         | <b>10</b> ( | 20     |   | 8   |         | aut      | ř       |            | <b>æ</b> 1 | 20 00        | α       | 6    | 60 0         | 0             | Ð            | 60 0         | 0 00         |      | 000                  |       |
| Wednes    | مٌ               | Mean         |            | <b>6</b> |                 | 0.00        | 24.6   | 6.92<br>82 | 0.14   | 879           | 23.6   | 27.2       | 2<br>2<br>2<br>2<br>2<br>2 |        | 53.4       | 8           | 30.05  |   | Fridav Ma   |         | 8        | Mean    |            | 37.4       | 52.1<br>52.1 | 245     | 26.0 | 40.9<br>40.9 | 7             | 23.1         | 25.9         | 63.8<br>63.8 |      | 36.8<br>29.0         |       |
|           |                  | Stand        | ð          | 24       |                 | 2           | 5.4    | 9 0        |        | 3.5           | 3.2    | 10 T       | 2.4                        |        | 1.<br>2. 5 |             | 0.     |   |   |         |          | Stand   |            | 30         | 9 4          | 3.7     | 2.0  | 23           | 5             | 0.5          | 80 T<br>Ci e | 3.7          |      | 1 7 8                |       |
|           | served           | c            | ¥          | < •      | ( <             | τ.          | < •    | < <        | <      | ¢             | < •    | < <        | A B                        | ł      | < <        | <           | <      |   |   |         |          | Ě       |            | ۲.         | < <          | <       | ۷    | < <          | c             | < ۲          | < <          | (∢           | <    | < < <                | ╢     |
|           | 90<br>O          | Mear         |            | 36.2     | 2.70            | 1.20        | 20.6   | 200        | 1070   |               | 21.0   | 0 6<br>5 6 | 22.8                       |        | 45.3       | 2 2         | 0.0    |   |   |         | 600<br>0 | Mean    |            | 2.15       | 42.5         | 19.5    | 22.9 | 32.5<br>35.5 | 2             | 19.1<br>20.0 | 202          | 53.0         | V 1V | 28 8<br>28 9         |       |
|           | Road             | Segment      |            | ¥.       | 28              | 2           | 2 2    | 8 8        | 3 5    | 8             | 58     | 38         | 32                         | i      | 58         | 3 8         | 3      |   |   |         | Koad     | Segment |            | <b>F</b> { | 28           | 2       | 8    | 88           | 5             | ចន           | 38           | 88           | 2    | 588                  |       |

Note: Tukey's Studentized Range Test (TK) = Means with the same letter are not significant at the 0.05 level

significance (p-value) are 0.4201 and 0.3497 respectively. Therefore, since most of the pvalues are less than the level set for rejection of the null hypothesis. This translates that based on the data presented there is a large evidence for rejecting the null hypothesis in favor of the alternative hypothesis. In conclusion, there is evidence that the Travel Times will be different among the three study groups (observed, default, and calibrated). This finding is similar to the Travel Time study during the first hour of data collection.

Second, the values under the Kruskal Wallis Pr > chi-square, gives the p-values for comparing the three mean groups for Travel Time. The values are all below the 0.05 significance level with the exception of road segment D3 on Mondays and Thursdays in which the p-values where .3823 and .1954 respectively. For this comparison it seems that both the parametric and non-parametric tests produces the same statistical conclusion. That is, since the p-values are less than the reference probability, the null hypothesis is rejected and one concludes' that the averages for the groups are significantly different.

Third, since the above conclusion only states that at least two means are different. The next step would be to use the Tukey's Studentized Range test, a multiple comparison procedure, to further investigate differences between groups. The outcome of this test is presented in the table under the heading TK. Tukey's test will perform all pair-wise comparisons among the groups. That is, it will compare observed vs. default, observed vs. calibrated, and default vs. calibrated.

In comparing the observed travel times vs. the travel times produced by the default model, it is clearly seen that most of the observed travel time means have the letter A and most of the default travel times have the letter B next to them. This implies

that the majority of the simulated travel times produced by the default model are statistically significant from those observed in the field at the 0.05 confidence level. This conclusion is true for most of the road segments through out the week with the exception of road segments D3 on Monday and Thursday, and C1 on Tuesday. In other words, from the possible 98 comparisons only 3 had similar means.

The second comparison (observed vs. calibrated) the following remarks are drawn: Looking at the travel times under observed and calibrated columns it is clear that the majority of the means have similar letters next to them. This means that the observed travel times and the simulated travel times from the calibrated model are not significantly different at the 0.05 level. This is true for all the road segments with the exception of C3 on Saturday, C2 on Sunday, B3 and C1 on Monday, A1 and B2 on Tuesday, A3 and D2 on Wednesday, D1 on Thursday, and A1, A2, B2, and D2 on Friday. Therefore, from the 98 possible comparisons only 13 road segments showed statistically significant differences among their mean travel times.

In summary, the default model for the second hour correctly predicted only 3 travel times where the calibrated model for the same hour correctly predicted 85 travel times out of a possible 98. This indicates that the calibrated Netsim model is able to correctly predict travel times in mush more instances than the default Netsim model.

The third and final comparison is comparing the default travel times and the calibrated travel times. Looking at both columns it is obvious that most of the values have different letters. This is a good indication that based on the second hour of data collection, the simulated travel times produced by both default and calibrated models are

statistically significant at the 0.05 level. This fact was observed in all the road links with the exception of road segment D3 on Monday, Tuesday, and Thursday.

### Delay Time on Test Network "Second Hour":

In reference to Table 4-7, titled summary of statistical analysis of Delay Time on the Test Network during the second hour of observation, the following is presented:

First, the column under the heading ANOVA Pr > F gives the p-values for comparing delay time for the three group. It appears that some of the numbers are below 0.05 and some are above the 0.05 level set by this research. From the 98 possible values only 36 had a p-value less than 0.05. This says that only 36 road segments through out the week had mean delay times significantly different, and that the reminder 62 road segments showed no statistical differences. The two days that showed the most differences among the groups are Sunday and Friday each with 7 road segments having p-values less than 0.05. It showed be mentioned that similar conclusion was drawn for delay time during the first hour of observation.

Second, the column labeled Kruskal Wallis Pr > chi-square, a non-parametric statistical procedure, gives the p-values for comparing the three groups. According to this test 55 out of the possible 98 had a p-value less than 0.05. Therefore, according to the results of a non-parametric test more than half of the links had group means that are statistically different.

To summarize the findings on delay time based on both parametric and nonparametric tests, it appears that about 63% (62 road segments) and 44% (43 road segments) of the road segments had a p-value > 0.05 for both ANOVA and Kruskal-Wallis tests respectively. These percentages are pretty high, therefore this study

| Calibrated<br>Mem         Kood         Observed<br>Description         Road<br>Frand<br>Frand         Constrate<br>Mem         Road<br>Frand         Constrate<br>Mem         Road<br>Frand         Constrate<br>Mem         Constrate<br>Frand         Constrate<br>Frand | Saturday May 10, 199 | Saturday May 10, 199 | Saturday May 10, 199 | saturday May 10, 1997 | May 10, 1997 | <b>7.199</b> | 1              | 7 Obser        | vations    | s in eact.    | l cell           | Kruskal          |         |             |        | 8           | unday M     | av 11.     | 1897       | Z Observ    | ations     | in each  | celt             | 2                |
|--|----------------------|----------------------|----------------------|-----------------------|--------------|--------------|----------------|----------------|------------|---------------|------------------|------------------|---------|-------------|--------|-------------|-------------|------------|------------|-------------|------------|----------|------------------|------------------|
| Main         Main         Stand         Main         Stand         Main         Stand         Main         Stand         Main         Stand         Main   |                      | obsed                | IVed                 |                       | Def          | aut          |                | Calibra        | ted        | 1             | ANOVA            | Wallis           | Road    | Obsen       | ved    |             | Defe        | ţ          |            | Calib       | rated      |          | ANOVA            | Wallis           |
| 7        | -                    | vean                 | ¥                    | Dev.                  | Mean         | ¥            | Stend.<br>Dev. | Mean           | ¥          | Stand.<br>Dev | ۲. ۲<br>۲        | Pr >             | Segment | Mean        | ž      | tand        | Mean        | 2          | tand.      | Mean        |            | stand.   | Pr > F           | br >             |
| 4         7         32         33         43         41         A8         01         01472         00013         A2         31         441         A         96         A         19         66         B         13         31         41         A         96         51         A         105         227         A         105         227         A         105         227         A         101         236         A         101         237         A         101         237         A         101         237         A         101         237         A         101         236         A         101         237         A         101         236         A         131         131         131         131         131         131         131         131         131         131         131         131         131         131  | 5                    | 2                    | ۲.                   | 3.1                   | 10.8         |              | 0.3            | 13.4           | <          | 0.2           | 0.0109           | 0.0081           | A1      | 13.3        | •      | 1.5         | 10.4        | < 0        | 0.2        | 13.5        | 4 4        |          | < 0001           | Chi-square       |
| 7        | N 4                  | 4 4                  | < <                  | 3.3                   | 3.8<br>45.9  | < 0          | 2.6            | 2.9<br>43.1    | < 8 ×      | 0 F<br>7 4    | 0.1572<br>0.0438 | 0.0313<br>0.0283 | 8 8     | 3.1<br>44.7 | A,B    | 1.0         | 3.6<br>46.3 | <b>م</b> م | 0.5<br>3.5 | 2.7         | <          | 0.1      | 0.0483           | 0.0149           |
| 8         A         30         27         A         012         235         A         011         011         0  | -                    | ą                    | <                    | 2.1                   | 3.5          | AB           | 01             | 37             | ď          |               | 0.0217           | 9000             | ā       |             | •      | 4           |             | -          |            |             | : 1        | 2        |                  | F 77 10          |
| 1       1       3       5       1       3       5       1       3       5       1       3       5       1       3       5       1       3       5       1       3       5       1       3       5       1       3       5       1       3       5       1       3       5       1       3       5       1       3       5       1       3       5       1       3       5       1       3       5       1       3       5       5       4       1       3       5       5       4       5       5       4       1       3       5       5       4       1       3       5       5       4       1       3       5       5       4       1       3       5       5       4       1       3       5       5       4       1       3       5       5       4       1       3       5       5       4       1       3       3       5       5       4       1       3       3       5       5       4       1       3       3       5       5       4       1       1       3       3  |                      | افع                  | ٨.                   | 3.0                   | 2.7          | <            | 0.2            | 2.4            |            | 5             | 0.6292           | 0.0933           | 5 25    | 5 0<br>7 7  | <      | 2 2         | 2.7         | n<br>A     | 0.1        | 22          | 8 <        | 5 6      | 0.0437<br>0.1633 | 0.0304           |
| 2       A       13       35       A       02       36       A       01       02165       00235       C2       22       A       021       35       A       01       35       A       021       023       00173       022       00173       022       00173       022       00173       021       021       00174       A       A       A       A       A <td>- 4</td> <td>~ ~</td> <td>&lt; &lt;</td> <td>1.9</td> <td>3.3<br/>47.6</td> <td>&lt; 0</td> <td>1.4</td> <td>3.0<br/>41.1</td> <td>&lt; &lt;</td> <td>0.2<br/>4.7</td> <td>0.0692<br/>0.0012</td> <td>0.0926<br/>0.0012</td> <td>83</td> <td>2.1<br/>35.1</td> <td>&lt; &lt;</td> <td>1.7</td> <td>3.2<br/>445</td> <td>&lt; ۵</td> <td>0.2</td> <td>2.8</td> <td>&lt;</td> <td>5.5</td> <td>0.14</td> <td>0.075</td>   | - 4                  | ~ ~                  | < <                  | 1.9                   | 3.3<br>47.6  | < 0          | 1.4            | 3.0<br>41.1    | < <        | 0.2<br>4.7    | 0.0692<br>0.0012 | 0.0926<br>0.0012 | 83      | 2.1<br>35.1 | < <    | 1.7         | 3.2<br>445  | < ۵        | 0.2        | 2.8         | <          | 5.5      | 0.14             | 0.075            |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$  | •                    | c                    | •                    |                       | •            |              |                |                |            |               |                  |                  | i       |             | :      |             |             | )          | 2          | 0.50        | τ.         | 4<br>0   | 1000.0           | 9.00.0           |
| 0.0         11         46         B         0.2         3.0         A         0.0         0.0007         Cd         53.2         A         0.4         4.1         B         0.2         2.5         A         0.5         7.7         A         2.4         7.7         A         0.3         7.8         A         0.3         7.7         A         2.4         7.7         A         0.3         7.8         A         0.4         5.5         A         0.4         5.5         A         0.5         7.8         A         0.4         7.4         2.4         7.7         A         0.3         7.8         A         1.4         2.4         7.7         A         0.3         7.8         A         1.4         2.4         7.7         A         0.3         7.8         A         1.4         2.4         7.7         2.4         7.7         2.4         A         1.4         2.4         A         1.4         2.4   | 4 (4                 | N 60                 | < <                  | 213                   | 0 0<br>0 0   | < <          | 0.1            | 3.8<br>2.8     | < <        | 5.6           | 0.2195           | 0.0252           | ខខ      | 9.0<br>0.0  | < <    | <u>+</u> ;; | 9.4<br>9.4  | < 0        | 5.5        | 35          | < •        | 5.6      | 0.9426           | 0.5715           |
| 92         A         61         561         A         51         504         A         20         00697         Cd         532         A         35         568         B         34         556         A           10         7.5         7         0.0         7.7         A         2.4         7.7         A         0.3         7.8         A           19         2.52         7.3         A         0.3         0.2863         0.7895         0.0173         D2         33         A         2.4         7.7         A         0.3         7.8         A           10         7.55         7.3         0.0         0.2863         0.7895         0.0013         D2         233         A         1.3         2.4         7.7         A         0.3         7.8         A           Mondav Mav 12.1697 : 7 Observation         D278         0.0103         D2         2.33         A         1.3         2.4         7.7         A         0.3         7.8         A           Mondav Mav 12.1697 : 7 Observation         D278         Mav         Mav         Mav         Mav         Mav         Mav         Mav         Mav         Mav <td< td=""><td></td><td>9.0</td><td>A</td><td>Ę</td><td>4.6</td><td>0</td><td>62</td><td>3.6</td><td>. ◄</td><td>0.3</td><td>0.0008</td><td>0.0039</td><td>38</td><td>9 P</td><td>&lt; ◄</td><td>7 7<br/>7 7</td><td>4 0<br/>1</td><td>ρœ</td><td>7 0</td><td>0 0<br/>N 0</td><td>٩ ٩</td><td>0.0</td><td>- 1000<br/>1000</td><td>0.0009</td></td<>  |                      | 9.0                  | A                    | Ę                     | 4.6          | 0            | 62             | 3.6            | . ◄        | 0.3           | 0.0008           | 0.0039           | 38      | 9 P         | < ◄    | 7 7<br>7 7  | 4 0<br>1    | ρœ         | 7 0        | 0 0<br>N 0  | ٩ ٩        | 0.0      | - 1000<br>1000   | 0.0009           |
| 50         A         35         76         01         75         A         03         0.2883         0.7685         D1         77         A         24         77         A         03         78         A           31         A         14         52         A         02         00012         00012         00012         00012         00013         D3         A   | v                    | 9.2                  | <                    | 61                    | <b>5</b> 5.1 | ۲            | 5.1            | 50.4           | <          | 2.0           | 0.0699           | 0.0677           | 2       | 53.2        | ۲      | 3.5         | 59.8        |            | 3.4        | 55.6        | A B        | 5.1      | 0.0218           | 0.0158           |
| Nonderview         Defervit         23         A         21         53         A         14         23         A         02         0.0013         023         0.0103         023         0.0103         023         0.0103         023         0.0103         023         0.0103         023         0.01036         023         024         023         024         023         023         023         023         023         023         023         023         023         023         023         023         023         023         023         023         023         023 <th023< th="">         023</th023<>  | -                    | 0.0                  |                      | 3.5                   | 7.6          | ٩.           | 5.0            | 7.5            | ٨.         | 0.3           | 0.2983           | 0.7695           | â       | 7.7         | ۲      | 2.4         | 7.7         | ۲          | 0.3        | 7.8         | ۲          | 0.4      | 0.9768           | 0.637            |
|  |                      | 9 B B                | < <                  | 2.5                   | 5.2<br>25.3  | < <          | <br>7 8 1      | 4.2<br>23.8    | < <        | 0.2           | 0.0912           | 0.0173           | 88      | 3.3<br>23 D | < <    | 1.0         | 5.3         | <b>a</b> < | 0.3        | 4.6<br>6.6  | A B        | 0.3      | 0.0186           | 0.0118           |
| Mondav Mav 12, 1997 : 7 Observations in sech cell         Transition         Tweeder Wav 13, 1997 : 7 Observation           Observations         Mondav Wav 12, 1997 : 7 Observation         Tweeder Mav 13, 1997 : 7 Observation           Observation         Default         Cell particle         ANOVA         Walken         Road         Observation         Default         Colspan="5">Constrained           Mean         TK         Dev         TK         Dev         Wean         TK         Dev         TK   | - 1                  |                      |                      |                       |              | -            |                |                |            |               |                  |                  |         |             | :      |             | )<br>ř      |            |            | 0.07        | <          | <u>†</u> | 0.2904           | 0.2244           |
| Observed<br>Mem         Default         Cellpreted         ANOVA         Walls         Road         Observed         Default         Cellpreted  |                      |                      |                      | 2                     | fondav M     | av 12.       | 1997 :         | 7 Observ       | ations     | n each c      | a la             |                  |         |             |        | F           |             |            |            |             |            |          |                  |                  |
| Mean         Kind         Mean         Kind         Mean         TK         Depart Mean         TK   |                      | 2                    | 1                    |                       | 2            |              |                |                |            |               |                  | Kruskal          |         |             |        | -           | II THAFAA   | 77 AB      |            | VIASOD /    | 100112     |          | Cell             | Kruskal          |
| TK         Dev         Dev   |                      | Mean                 | S                    | tand                  | Mean         | S S          | tand           | Mean           | S          | tand          | Pr > F           |                  | Seoment | Mean        |        | - Part      | Mean Wear   | ۳<br>۲     | -          | Callb       |            |          | ANOVA            | Vallis           |
| 12.6       A       0.3       13.4       A       0.4       0.0064       A1       131       A       0.6       13.4       A       0.4       0.0064       A1       131       A       16       316       B       0.3       13.4       A       0.4       0.0064       A1       131       A       16       316       B       0.3       13.6       A         33       A       1.5       356       A       0.1       38       A       0.1       38       A       0.1       38       B       0.4       20       36       A       0.1       38       A       0.1       36       B       0.1       38       A       0.1       0.03       0.0355       0.0355       0.1       0.1       38       A       0.1       38       A       0.1       0.2       0.4       A       1.5       0.1       0.2       0.1       0.2  |                      |                      | ¥                    | <u>N</u>              |              | ¥            | à              |                | ¥          | <u>ev</u>     |                  | chi-souare.      | 0       |             | ,<br>X | à           |             | 2          | 2 A        |             | ž          | i vi     | 121              | chi-square       |
| 35       AB       08       39       B       10       28       A       011       00411       0018       A2       24       A       15       36       B       04       28       A       01       38       A       15       36       B       04       28       A       01       38       A       16       36       B       04       28       440       A       13       0.4532       0.0824       0.1034       B1       22       A       36       466       A       35       440       A         33       A       23       35       A       01       23       0824       01034       B1       22       47       A       13       440       A       13       0455       A       01       38       A       01       28       A       01       28       38       A       0  | •                    | 12.8                 | ۲                    | 2.0                   | 10.5         | 8            | 0.3            | 13.4           | •          | 0.4           | 0.0006           | 0.0064           | ų       | 13.1        | <      | 8.0         | 10.5        | α          | 60         | 13.6        | •          |          | 1000             | 0.0014           |
| 33       A       13       0.4532       0.0532       0.0518       A3       430       A       35       440       A       13       0.4532       0.0518       A3       430       A       35       440       A       13       0.4532       0.0518       A3       430       A       35       440       A       13       0.4532       0.0518       B3       14       A       35       A       01       38       A       01       27       28       31       27  |                      | 3.5                  | 80                   | 8.0                   | 3.9          | 6            | 1.0            | 2.8            | ٨.         | 0.1           | 0.0411           | 0.018            | 8       | 2.4         | <      | 1.6         | 3.8         | ) 60       | 4          | 2.8         | 8 ¥        | 0.0      | 6600             | 0.0114           |
| 33       A       13       34       A       01       38       A       12       42       A       01       38       A       12       42       A       01       38       A       41       A       15       37       A       A       12       42       A       12       42       A       10       0003       0003       CC       52       A       12       42       A       12       <  | •                    |                      | A, H                 | 8. F                  | 45.8         | 4            | <br>2:0        | 44.0           | <          |               | 0.4532           | 0.8218           | A3      | 43.0        | ۲      | 3.9         | 46.6        | <          | 3.5        | 44.0        | ×          | 2.3      | 0.1439           | 0.1719           |
| 1.2       7       2.7       2.7       2.7       2.7       8.7       1.4       7       8.7       1.4       7       8.7       1.4       7       8.7       1.4       7       8.7       1.4       7       8.7       1.4       7       8.7       1.4       7       9.7       2.7       8.9       1.7       4.7       8       1.7       4.7       8       1.7       4.7       8       1.2       3.0  |                      | 9.6                  | < <                  | 5.0                   | 9.0<br>9.0   | <            |                | 8.0            | < •        |               | 0.6324           | 0.1094           | 201     | 2.2         | ۲      | 2.9         | 3.5         | <          | 0.1        | 3.8         | ۲          | 0.1      | 0.1621           | 0.0049           |
| 11.3       1.7       44.7       18       1.6       4.25       A.8       1.6       0.0035       0.0007       184       4.16       A       23       4.02       3.0       4.2       3.0       4.2       3.0       4.2       3.0       4.2       4.16       0.0       3.7       4       4.16       A       23       4.5       A       1.2       3.0       4.2       A       4.2       3.0       4.2       3.0       4.2       3.0       4.2       4.12       3.0       4.2       4.2       3.0       4.2       3.0       4.2   |                      | 12                   | ( <                  | 50                    | 9.0          | < a          | 50             | 4 G            | < 0        |               | 0.01             | 0.2551           | 83      | 4.          | < <    | 1.0         | 2.7         | <b>•</b>   | 0.2        | 2.5         | 8          | 0.1      | 0.0138           | 0.099            |
| 50     A     1.2     36     B     0.1     3.7     B     0.1     3.7     B     0.1     3.7     B     0.1     3.7     B     0.1     2.8     A     0.2     3.3     A     0.2     2.8     A     0.2     3.8     A     0.2     2.8     A     0.2     3.8     A     B     8.8     5.3.4     A     B     4.8     A     B     5.3.4     A     B     4.8     A     B     3.3     A     B     3.3.4  | -                    | 41.3                 | <                    | 1.7                   | 44.7         | 0.00         | 1.6            | 42.5           | A B        | 1.6           | 0.0035           | 0.0097           | 8 2     | 41.6        | < <    | 3.5         | 45.5        | < <        | 1.2        | 3.0<br>42.2 | <b>ح</b> ح | 5.5      | 0.485<br>0.1509  | 0.1516<br>0.0276 |
| 25       A       28       3.3       A       0.1       28       A       0.1       28       A       0.1       28       A       0.2       28       A         0.4       A       53       54       A       0.3       38       A       0.2       28       A         0.4       A       53       54       A       1.7       539       A       1.9       0.0495       0.0178       C3       3.3       A       25       4.7       A       0.2       28       A         0.4       A       5.3       54       A       1.7       0.0495       0.0178       C3       3.3       A       25       4.7       A       0.2       28       A         0.4       A       5.3       54       A       1.9       0.0495       0.0178       C4       51       A       0.2       2.8       A         1.4       A       5.3       54       A       1.9       0.0495       0.0178       C4       51       A       0.2       2.8       A       B       8.3.4       A       B       3.3.4       B       3.3.4       B       3.3.4       A       B       3.3   |                      | 5.0                  | •                    | 1.2                   | 3.6          | 8            | 0.1            | 3.7            | 8          | 50            | 0.0026           | 0.0009           | 5       | 5.2         | •      | 3.2         | 3.6         | -          | 0.2        | 3.7         | ٩          | 0,0      | 0 22R7           | 0.7830           |
| 0.4     A     5.3     5.4     4.0     0.3     3.8     A     0.2     0.0069     0.0056     C.3     3.3     A     2.5     4.7     A     0.2     3.8     A       0.4     A     5.3     5.4     A     1.7     53.9     A     1.9     0.0495     0.0178     C.4     51.4     A     50     60.6     B     8.8     53.4     A       15     A     0.3     6.6     A     2.5     7.8     A     0.2     0.34     A       15     A     0.3     6.6     A     2.6     7.8     A     0.3     7.9     A       12     A     0.3     0.3407     0.0348     D2     4.0     A     2.6     7.9     A     0.3     7.9     A       12     A     2.3     A     2.1     2.4.5     A     1.1     0.03418     D2     4.0     A     2.3     7.9     A     0.3     7.9     A       14     A     2.2     2.37     A     2.1     2.4.5     A     1.1     0.03453     0.3453     0.3     2.4.3     A     2.3     2.4.9     A     1.2     2.4.6     A   | ••••                 | 00                   | • •                  | 5.8                   | 3.3          | • •          | 5.5            | 2.8            | <b>A</b> - | 01            | 0.7066           | 0.0932           | 8       | 4.4         | ۲      | 2.2         | 3.3         | <          | 0.2        | 2.8         | <          | 0.2      | 0.0833           | 0.03             |
| 45       A       0.3       6.6       A       2.5       7.8       A       0.2       0.293       0.4662       D1       7.0       A       2.6       7.9       A       0.3       7.8       A         42       A       2.3       5.3       A       0.3       4.5       A       0.3       0.3101       0.0318       D2       4.0       A       2.6       7.9       A       0.3       7.8       A         48       A       2.1       2.4.2       A       1.1       0.6061       0.3763       D3       24.3       A       2.3       24.9       A       1.3       24.8       A  |                      | 9.4<br>9.7           | < <                  | 1 0<br>0              | 54.9<br>54.9 | • •          | 1.7            | 3.8<br>53.9    | < <        | 1.9           | 0.0485           | 0.0058           | 88      | 3.3<br>51.4 | < «    | 2.5         | 4.7<br>60.6 | < 0        | 0.2        | 3.8<br>53.4 | < d        | 0.3      | 0.2121           | 0.0294           |
| 42 A 23 53 A 21 24 A 03 03 45 A 03 04003 04003 D   |                      | 45                   | 4                    |                       | 99           | 4            | 35             | a 7            | <          |               |                  | 0 1050           | 2       |             |        |             |             |            |            |             | <u>.</u>   |          |                  | 70000            |
| 248 A 22 23.7 A 2.1 24.2 A 1.1 0.6061 0.3763 03 24.3 A 2.3 24.9 A 1.2 24.8 A   |                      | 4                    | <                    | 53                    | 500          | <            | 20             | - <del>4</del> | <          | 0.3           | 0.3101           | 0.0318           | 58      | 40          | < <    | 2.0         | 7.9         | <          | 0.0        | 7.9<br>8 k  | < <        | 0.0      | 0.4623           | 0.8515           |
|  |                      | 24.8                 | ۲                    | 2.2                   | 23.7         | •            | 2.1            | 24.2           | <          | ÷             | 0.6061           | 0.3763           | 58      | 24.3        | < <    | 53          | 24.9        | < <        | 20         | 4.0<br>24.8 | • •        | 1.2      | 0.7158           | 0.0259           |

Table 4.7 Statistical analysis of Delay Time on Test Network "Second Hour" Second hour observation ( 13:30 - 14:30 )

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Note: Tukey's Studentized Range Test (TK) = Means with the same letter are not significant at the 0.05 level

|            | 1                 |                        | a)         | _           |          |            |             |            |        |            |            |          |              |            |        | 'n | -         | _       |        | -        |                            |        |            |        |                                     | ·                         |
|------------|-------------------|------------------------|------------|-------------|----------|------------|-------------|------------|--------|------------|------------|----------|--------------|------------|--------|----|-----------|---------|--------|----------|----------------------------|--------|------------|--------|-------------------------------------|---------------------------|
|            | Kruskal           | - id                   | chi-squar  | 0.0001      | 0.0012   | 0.2623     | 0.0697      | 0.0047     |        | 0.93       | 0.0034     | 0.0245   | 29000        | 0.0698     | 0.6289 |    |           |         |        |          |                            |        |            |        |                                     |                           |
| ch cell    |                   | 4<br>1<br>1<br>1       | 10000      | 0.008       | 0.0004   | 0.758      | 0.174       | 0.0019     |        | 0.6464     | 0.0566     | 0.0598   | 0.0787       | 0.6529     | 0.4749 |    |           |         |        |          |                            |        |            |        |                                     |                           |
| ae ni su   |                   | Stand.                 | 3 2        | 50          | <u>-</u> | 0.2        | 0 0         | 0 0<br>7 4 |        |            | 5          | 2.3      | , u          | 0.0        | 1.5    |    |           |         |        |          |                            |        |            |        |                                     |                           |
| vatior     | - Posto           |                        | <u> </u>   | 8           | ₹        | <          | < <         | <b>.</b> . |        | ٨ ۵        | 8          | ۲        | •            | . ◄        | ۲      |    |           |         |        |          |                            |        |            |        |                                     |                           |
| : 7 Obser  | -<br>Hile<br>C    | Mean                   | 13.4       | 2.9         | 40.0     | 3.9        | 5 Q         | 43.8       | 0      | 3.6        | 3.6        | 54.8     | 7.8          | 4.6        | 24.4   |    |           |         |        |          |                            |        |            |        |                                     |                           |
| 15, 1997   |                   | Stand.                 |            | 8.8         | 0        | 0.2        |             | 3.3        | ,<br>, | 200        | 0.3        | 9.2      | 0.3          | 0.3        | 1.4    |    |           |         |        |          |                            |        |            |        |                                     |                           |
| Mav        | ŧ                 |                        | ≤ α        | 000         | D        | ٩.         | <           | ( 00       |        | < <        | 8          | <        | <            | ۲          | ۲      |    |           |         |        |          |                            |        |            |        |                                     |                           |
| Thursday   | Def               | Mean                   | 10.8       | 9.6         | 7.00     | 3.6<br>0.0 | 10 e<br>N e | 49.0       | 90     | 3.2<br>3.7 | 4.4        | 60.2     | 7.7          | 5.1        | 24.1   |    |           |         |        |          |                            |        |            |        |                                     |                           |
|            |                   | Stand                  | 19         | 4 0         | 2        | 5.5        | 2.6         | 3.2        | 4      | 5          | 2.4        | 20       | 2.9          | 3.0        | 2.5    |    |           |         |        |          |                            |        |            |        |                                     |                           |
|            | bey               | F                      |            | < <         | τ.       | < •        | < 4         | <          | •      | <          | <          | <        | ۲            | ۲          | ۷      |    |           |         |        |          |                            |        |            |        |                                     |                           |
|            | Obser             | Mean                   | 13.0       | 0.4<br>4 0  | ,<br>F   | 4 4        | 23          | 42.7       | 4 1    | 54         | 2.5        | 51.8     | 5.9          | 4.2        | 25.3   |    |           |         |        |          |                            |        |            |        |                                     |                           |
|            | Road              | Segment                | ¥          | 88          | 2        | <u>ت</u>   | 88          | 84         | 5      | 58         | 8          | 3        | δ            | 8          | 8      |    |           |         |        |          |                            |        |            |        |                                     |                           |
|            | Kruskal<br>Wallis | Pr >                   | 0.0088     | 0.0258      |          | 0.2602     | 0.053       | 0.116      | 0 5008 | 0.0937     | 0.0223     | 0.4289   | 0.0585       | 0.0001     | 0.0413 |    |           | Kruskat | Wallis | Pr >     | 0.0067<br>0.0042<br>0.0011 | 0.0514 | 0.0125     | 8000.0 | 0.0719<br>0.0852<br>0.0682<br>0.061 | 0.843<br>0.0032<br>0.1754 |
| cel        | AVC               | ц.                     | 087        | 153<br>01   |          | 961        | 767         | 745        | 974    | 346        | 613        | 5        | 939          | <u>6</u>   | 184    |    |           |         | A N    | <u> </u> | 643<br>01 23               | 174    | 882        | 3      | 88                                  | 63<br>63                  |
| 1 each     | Å.                | <u>م</u>               | 0.0        | <u>.</u> 5  |          | 0.5        | 0.0         | 0.0        | 0.2    | 0          | 56         | <u>.</u> | 0.0          | Ş          | 00     |    | je,       |         | Ă      | ፚ        | 000                        | 0.18   | 000        | 5      | 0 0 0 0<br>7 4 9 0                  | 0 0 0<br>4 0 4            |
| ations i   |                   | Stand.                 | 0.3        | 0.2         |          | 55         | 0.2         | 4.8        | 0.2    | 0.2        | 0.0        | 0.0      | 0.2          | 0.2        | 1.7    |    | in each   |         |        | Stand.   | 0.1<br>0.2<br>1.1          | 0.1    | 0.7        | N C    | 2225                                | 0.4<br>0.3<br>1.8         |
| <b>D30</b> | rated             | Ĕ                      | <          | < 0         |          | < <        | <           | ۲          | ۷      | ×          | <          | ۲.       | ۲            | U .        | A,B    |    | ations    |         | Bled   | Ĭ        | 8 4 4<br>9 8 8             | ۲      | 8 < <      | <      | < < < <sup>8</sup>                  | < 8. <                    |
| 02 266     | Callb             | Mean                   | 12.9       | 2.7         | 4        | 3.8        | 2.9         | 40.8       | 3.6    | 2.8        | 3.8        | 4.10     | 8.7          | 4.7        | 25.2   |    | 7 Observa |         | Callbi | Mean     | 9.9<br>1.9<br>32.9         | 3.7    | 2.4<br>2.4 | 0.07   | 3.4<br>2.3<br>39.2                  | 6.5<br>3.2<br>18.2        |
| 8Y 14.1    |                   | Stand.<br>Dev.         | 0.3        | 0.2         |          | 0.2        | 0.2         | 3.1        | 0.2    | 0.2        | 0.0        | 7.6<br>6 | 4            | 0.2        | 1.2    |    | 1997 :    |         |        | Stand.   | 0.3<br>0.3<br>1.7          | 0.1    | 0 0 0      | 3      | 002                                 | 0.3                       |
| M Ver      | fault             | ¥                      | 60         | < 0         |          | < <        | ۲           | ×          | A      | ¥          | < <        | ¢        | <            | <b>m</b> 1 | 20     |    | N 16.     |         |        | ¥        | 8 8 8<br>8                 | ۲      | a<br>A ⊂ a | ٥      | < < < 0                             | < 0 <                     |
| 100        | å                 | Mean                   | 10.4       | 3.4<br>45.1 | ų        | 2.7        | 3.3         | 45.6       | 3.6    | 3.3        | 6.7<br>6.7 | 0.70     | 8.3          | 5.7        | 0.97   |    | Eridey Me |         |        | Mean     | 7.7<br>2.6<br>37.2         | 3.4    | 30 E       | 2      | 3.1<br>3.0<br>44.2                  | 6.6<br>3.9<br>19.1        |
| Š          | •                 |                        |            |             |          | 4 6        | 2.9         | 3.2        | 3.2    | 2.8        |            | N<br>S   | 1.5          | 7 7        | ~      |    |           |         |        | Stand.   | 3 7 8<br>3 7 8             | 3.7    | 230        | 5      | 2.6<br>7.8<br>4 4                   | 41.1.2                    |
| Wex        |                   | Stand.<br>Dev          | 2.4        | 27          |          |            |             | _          |        |            | -          | _        | -            |            |        |    |           |         |        | ¥        | < < <                      | <      |            | r      |                                     |                           |
| Wex        | erved             | TK Dev.                | A 24       | × ×         |          | < <        | ۲           | ۲          | ۲      | < •        | < <        | c        | < ۲          | < •        | ≺      | 11 | - 1       |         | _      |          |                            |        |            |        | < < < <                             | < < <                     |
| Wex        | Observed          | Mean Stand.<br>TK Dev. | 12.3 A 2.4 | 40.7 A 1.1  |          | 4 V V      | 2.4 A       | 44.2 A     | 4.9 A  | 23 A       | 58.7 A     | 4.00     | 8 0 0<br>0 0 | 3.6 A      | 40.4 A |    |           | ð       |        | Mean     | 7.3<br>0.1<br>30.6         | 1.6    | 2.0        | 2      | 3.2 A<br>1.0 A<br>35.4 A            | 51<br>23<br>181<br>8      |

Table 4-7 (continued) Statistical analysis of Delay Time on Test Network "Second Hour" Second hour observation (13:30 - 14:30)

concludes that for the second hour of observation, there was not enough evidence to reject the Null hypothesis and concludes that the averages of delay time among the three groups are not significantly different at the 0.05 level. However, from a practical point of view, and looking back at delay values it appears that the simulated delay values from the calibrated model are closer to the delay values observed in the field in comparison with the simulated delay values generated by the default model.

The same conclusion was drawn with respect to delay time during the first hour of data collection.

### Summary of Findings on the Test Network

This research observed and recorded traffic volumes, signal timings, traffic composition and other related factors on the Test Network (Mecca Street) for a period of two hours on seven consecutive days in Amman-Jordan. The study performed a total of 98 traffic simulation runs using the Traf-Netsim model with both the default and calibrated parameters. The main objective of this phase was to determine if Traf-Netsim model can or can't accurately predict Travel Times and Delay Times along the arterial street. This was accomplished by the following:

First, the Traf-Netsim model was executed 49 times using the default parameters embedded in to the model (default model)

Second, the model was modified using the observed values for mean free flow speed, start-up lost time and queue discharge headway along with their respective distributions (calibrated model). Third, the simulated Travel Times and route Delay Times derived from both the default and calibrated models were compared with the observed values in the field.

To compare the three group means several statistical hypotheses were setup. The null hypothesis for Travel Time states that the population means for all groups are the same and the alternative hypothesis says that at least two means are different. Similar hypotheses were used for Delay Time along the route.

The summary of statistical analysis of Travel Time and Delay Time were presented for the Test Network (Mecca Street) in Tables 4-4, 4-5, 4-6 and 4-7. For Travel Time the null hypothesis was rejected in favor of the alternative hypothesis. Further investigation revealed that the simulated Travel Times from the calibrated model produced values similar to the observed values. On the other hand, for Delay Time there was not enough evidence to reject the null hypothesis. However, differences between the simulated Delay Times from the calibrated model and observed values were less in comparison with the differences between the simulated delay values from the default model and those observed in the field.

### Validation Network

The second site, referred to as the Validation Network, is a stretch of Al Shareef Nasser bin Jameel Street (or Safeway Street), which is approximately 1.5 kilometers long (or 0.94 miles). The second site was used to answer the following question:

• Can the Traf-Netsim model using the calibrated parameters adequately simulate both Time and Delay time along a second arterial street? This was also accomplished by comparing the simulated values produced by the calibrated model with observed values collected in the field for the validation Network.

### **Defining the Hypotheses**

To test if the simulated Travel Times and Delay Times derived from the calibrated model are statistically significant from the observed values obtained from the floating car study, the following hypotheses were constructed:

### Travel Time along the Arterial:

• The Null Hypothesis states that the Travel Time means are the same.

The two groups are:

- 1. Simulated model with calibrated parameters.
- 2. Observed values form the field.

In terms of a mathematical expression the Null Hypotheses is:

# $H_o: u_{calibrated} = u_{observed}$

• The Alternative Hypotheses states that the Travel Time means are significantly different.

In terms of a mathematical expression the Alternative Hypotheses is:

## $H_a: u_{calibrated} \neq u_{observed}$

### Delay Time along the Arterial:

Similar null and alternative hypotheses for the mean Delay Time were also constructed.

## $H_o: u_{calibrated} = u_{observed}$

## $H_a: u_{calibrated} \neq u_{observed}$

To test and evaluate if the two group means for both travel time and delay time presented in the above hypotheses are statistically significant a Two-Sample t-test will be used and is presented below:

#### Two sample t-test:

The t-test is a parametric procedure that compares two samples. However, before performing the Two-Sample t-tests the following assumptions should be checked.

- 1- Observations are independent random samples.
- 2- Observations for each group are a sample from a population with a normal distribution.
- 3- The two groups have equal variances.

The first assumption of independent observations is met, since in this research every Travel Time or Delay Time whether simulated or measured in the field is unrelated to every other measurement. For the simulated measurements this was accomplished by using a different random number seed for each simulation run which generates internally a different pattern of driver types and vehicle paths along the network.

The second assumption of normality is hard to meet since there are only 8 to 10 observations in each group. Conclusively, this assumption was not met.

The third and final assumption is concerned whether the variances for the two groups are equal. This assumption is tested using the PROC TTEST procedure in SAS. The output produced by SAS contains two values for the t-test one based on equal variances the other on unequal variances. For this research some of the means had equal variances and others had unequal variances. The probability value in the table reflects the appropriate t-test.

In summary, since the data in each group was small, the assumption of normality could not be checked. Thus, both the Two-Sample t-test and the Wilcoxon Rank Sum Test for comparing two independent groups were used. The Wilcoxon Rank Sum Test is a non-parametric analogue to the two-sample t-test and is sometimes referred to as the Mann-Whitney U test. The only assumption required for this non-parametric test is that the observations are independent and this assumption was met.

### **Statistical Interpretation**

The following section will present the summaries of the statistical tests and will evaluate the null and alternative hypotheses for travel time and delay time on the validation network. Prior to presenting the statistical results, it should be mentioned that the naming of the links in the validation network were also modified for added clarity and simplicity when viewing the statistical analysis. Figure 4-2 shows the aggregated links and nodes for the validation network.

### Travel Time on Validation Network "First Hour":

Looking at the statistical analysis of Travel Time on the Validation Network for the first hour (Table 4-8) the following comments and interpretations are made:

First, the column labeled T-Test Pr > |t| gives the p-values for comparing the two groups. In looking at the values it seems that most of the p-values are well above the rejection criteria of 0.05 set by this research. This is true for all the road segments through out the week, with the exception of road segment D1 on Friday, B1 on Saturday,



Figure 4-2 Validation Network

Table 4.8 Statistical analysis of Travel Time on Validation Network "First Hour" First hour of observation (12:30 - 13:30 )

|          | Seterday June  | 27, 199        | 8. 8 Observation | ns in eac     | h cell           |                  |                 | Sunday June 2  | 8, 1998        | 8 Observations              | s in each     | n celt           |                  |
|----------|----------------|----------------|------------------|---------------|------------------|------------------|-----------------|----------------|----------------|-----------------------------|---------------|------------------|------------------|
| pend     | Chean          |                | Callbrated       |               | T Tank           | Allocated a      |                 |                |                |                             |               |                  |                  |
| Segment  | Mean<br>(sec.) | Stand.<br>Dev. | Mean<br>(sec.)   | Stand<br>Dev. | Pr> t            | Pr > [2]         | Segment         | Mean<br>(sec.) | Stand.<br>Dev. | Valinateu<br>Mean<br>(sec.) | Stand.<br>Dev | Pr-1681          | Pr > Z {         |
| ۲        | 18.2           | 3.9            | 17.1             | 0.2           | 0.4572           | 0.958            | ۷               | 16.4           | 4              | 16.8                        | 0.2           | 0.8038           | -                |
| 66 FE    | 25.0<br>41.1   | 0.9<br>3.6     | 26.0<br>39.2     | 0.2           | 0.0195<br>0.1905 | 0.1025<br>0.1556 | <b>8</b> 8      | 21.6<br>42.7   | 3.9            | 25.5<br>40.0                | 0.2<br>1.6    | 0.0014<br>0.1041 | 0.0133<br>0.1559 |
| υ        | 26.8           | 2.0            | 28.2             | 2.1           | 0.206            | 0.2268           | U               | 27.2           | 4.1            | 28.1                        | 2.7           | 0.6056           | 0.4733           |
| ٥        | 35.4           | 1.9            | 37.8             | 2.6           | 0.0584           | 0.0659           | ۵               | 43.5           | 3.2            | 43.4                        | 4.9           | 0.9915           | 0.7965           |
| E1<br>E2 | 22.5<br>30.6   | 1.9<br>2.7     | 23.8<br>30.8     | 1.5<br>0.4    | 0.1265<br>0.81   | 0.1563<br>0.4945 | E3              | 21.6<br>31.8   | 1.9<br>3.2     | 24.0<br>31.0                | 0.9           | 0.0071<br>0.5164 | 0.018<br>0.958   |
| Ľ.       | 19.8           | 3.6            | 21.5             | 0.8           | 0.2121           | 0.3717           | u.              | 19.6           | 5.4            | 21.5                        | 0.7           | 0.3481           | 0.1036           |
|          | Monday June    | <u>9. 1988</u> | : 8 Observation  | s in each     | ) cell           |                  |                 | Tuesday June   | 30, 199        | 9: 8 Observation            | IS IN BRC     | h cell           |                  |
| Road     | Observed       |                | Calibrated       |               | T-Test           | Wikoxon          | Road            | Observed       |                | Calibrated                  |               | T-Test           | Wilcoxon         |
| Segment  | Mean<br>(sec.) | Stand.<br>Dev. | Mean<br>(sec.)   | Stand<br>Dev  | Pr> t            | Pr >   Z         | Segment         | Mean<br>(sec.) | Stand.<br>Dev  | Mean<br>(sec)               | Stand.<br>Dev | Pr> t            | Pr > 121         |
| ۲        | 18.9           | 4.0            | 17.1             | 0.2           | 0.243            | 0.5789           | ۷               | 18.2           | 4.8            | 16.8                        | 0.2           | 0.4654           | -                |
| 88       | 25.6<br>37.8   | 1.5<br>5.6     | 26.6<br>39.3     | 0.2           | 0.1266<br>0.4562 | 0.1028<br>0.8766 | <del>2</del> 28 | 24.8<br>38.9   | 2.0            | 26.0<br>39.7                | 0.1<br>2.0    | 0.1416<br>0.7185 | 0.1824<br>0.958  |
| υ        | 28.9           | 3.2            | 29.0             | 1.5           | 0.1062           | 0.1275           | U               | 33.1           | 3.0            | 33.4                        | 3.0           | 0.8082           | 0.9581           |
| ٥        | 39.9           | 2.0            | 42.1             | 3.5           | 0.1376           | 0.1278           | ۵               | 38.1           | 4.6            | 42.1                        | 4.5           | 0.1021           | 0.0831           |
| £ 5      | 24.5<br>33.3   | 1.9<br>3.6     | 26.1<br>31.8     | 1.9<br>0.7    | 0.1252<br>0.2804 | 0.1275<br>0.5635 | 5<br>2<br>2     | 21.4<br>32.8   | 1.4<br>3.8     | 24.6<br>31.1                | 0.9           | <.0001<br>0.229  | 0.0009<br>0.4932 |
| u.       | 20.6           | 4.0            | 23.3             | 1.0           | 0.0955           | 0.0659           | u.              | 23.2           | 3.7            | 21.9                        | 0.6           | 0.3653           | 0.5629           |

|          |                  |                |                  | -              |                  | ODSEL ABIOL      | - 76:21 ) 1  | 13:30)         |                |                |                | :                |                 |
|----------|------------------|----------------|------------------|----------------|------------------|------------------|--|----------------|----------------|----------------|----------------|------------------|-----------------|
|          | Wednesday Jr     | ilv 1. 18      | 98; 8 Observatio | ns in ee       | ch celt          |                  |  | Thursday July  | 2.1998         | 8 Observations | in each        | celt             |                 |
| Road     | Observed         |                | Calibrated       |                | T-Test           | Wilcoxon         | Road   | Observed       | -              | Calibrated     |                | T.Test           | Witcown         |
| Segment  | Mean<br>(sec.)   | Stand.<br>Dev. | Mean<br>(sec.)   | Stand.<br>Dev. | Pr > [1]         | Pr >   Z         | Segment  | Mean<br>(sec.) | Stand.<br>Dev. | Mean<br>(sec.) | Stand.<br>Dev. | Pr >   t         | Pr >   Z        |
| 4        | 15.9             | 1.2            | 16.8             | 0.4            | 0.084            | 0.0653           | ۲  | 20.0           | 4.6            | 17.2           | 0.3            | 0.1361           | 0.2698          |
| B1<br>B2 | 25.3<br>39.2     | 1.7<br>2.4     | 25.9<br>37.6     | 0.2            | 0.3236<br>0.2152 | 0.2265<br>0.0831 | 18<br>16<br>16<br>16<br>16<br>16<br>16<br>16<br>16<br>16<br>16<br>16<br>16<br>16 | 25.7<br>37.3   | 2.1            | 26.8<br>39.0   | 0.2<br>1.9     | 0.1598<br>0.1419 | 0.0813          |
| υ        | 24.8             | 1.5            | 26.2             | 4.1            | 0.0765           | 0.0831           | υ  | 33.3           | 3.1            | 36.1           | 5.6            | 0.2359           | 0.3181          |
| ۵        | 33.7             | 2.7            | 34.9             | 1.4            | 0.2856           | 0.2271           | ٥  | 43.0           | 6.6            | 47.0           | 4.6            | 0.1747           | 0.1563          |
| £3       | 18.7<br>31.2     | 1.5<br>3.6     | 22.2<br>30.6     | 0.4            | 0.0002<br>0.6221 | 0.0009<br>0.9581 | E2   | 23.8<br>33.6   | 3.1            | 25.5<br>32.0   | 1.3            | 0.1832<br>0.1376 | 0.1563<br>0.317 |
| Ľ        | 20.0             | 2.2            | 21.4             | 0.5            | 0.1262           | 0.3717           | u  | 21.7           | 4.0            | 23.8           | 0.8            | 0.1838           | 0.0404          |
|          | Friday July 3. 1 | 996: 10        | Observations in  | h each ce      |                  |                  |  |                |                |                |                |                  |                 |
| Road     | Observed         |                | Calibrated       |                | T-Test           | Wilcoxon         |  |                |                |                |                |                  |                 |
| Segment  | Mean<br>(seo.)   | Stand.<br>Dev. | Mean<br>(sec.)   | Stand.<br>Dev  | Pr >   [         | Pr >   Z         |  |                |                |                |                |                  |                 |
| ٩        | 14.0             | 4.0            | 15.8             | 0.5            | 0.1971           | 0.0885           |  |                |                |                |                |                  |                 |
| 81<br>82 | 20.9<br>28.4     | 3.9            | 23.1<br>30.6     | 0.3            | 0.0083           | 0.0072<br>0.3845 |  |                |                |                |                |                  |                 |
| υ        | 16.7             | 2.0            | 19.2             | 0.3            | 0.0037           | 0.0013           |  |                |                |                |                |                  |                 |
| ۵        | 21.3             | 2.3            | 23.3             | 0.7            | 0.0274           | 0.0311           |  |                |                |                |                |                  |                 |
| E G      | 16.0<br>26.5     | 20             | 19.6<br>27.5     | 0.2            | 0.0002<br>0.5198 | 0.0027<br>0.578  |  |                |                |                |                |                  |                 |
| Ŀ        | 14.1             | 24             | 16.6             | 0.3            | 0.0077           | 0.0028           |  |                |                |                |                |                  |                 |

Table 4.8 (continued) Statistical analysis of Travel Time on Validation Network "First Hour" First hour of observation (12:30 - 13:30)

Sunday, and Friday, E1 on Sunday, Tuesday, Wednesday, and Friday. Thus from the possible 56 comparisons only 8 had a p-value less than 0.05. With Friday and Sunday having 3 and 2 road segments respectively.

Second, in looking at the column labeled Wilcoxon Pr > |Z| which gives the pvalues for the non-parametric procedure. In this column the majority of the p-values are also greater than 0.05 with the exception of Sunday links B1 and E1, Tuesday link E1, Wednesday link E1, Thursday link F, and Friday links B1, C, D, and E1. Of the possible 56 comparisons only 9 had a p-value less than 0.05, again with Friday and Sunday having 4 and 2 links respectively.

In conclusion, since the majority of the p-values are greater than the reference probability of 0.05, this means failure to reject the null hypothesis. And since we are comparing independent groups, this research will conclude that the mean travel time for the two groups are not significantly different. In other words, it appears that the calibrated Netsim model can accurately predict the Travel Times in Amman-Jordan.

### Delay Time on Validation Network "First Hour":

Looking at the statistical analysis of Delay Time on the Validation Network during the first hour (Table 4-9) the following conclusions are drawn:

First, the column under the heading T-Test Pr > |t| gives the p-values for comparing delay time for the two groups. The numbers in most cases are larger than the reference probability value of 0.05. Looking at the six weekdays (Saturday, Sunday, Monday, Tuesday, Wednesday, and Thursday) it appears that only 5 out of possible 48 (8\*6) links had a p-value greater than 0.05. However it seems that on the weekend (Friday) there were 5 road segments with a p-value greater than 0.05.

 Table 4.9
 Statistical analysis of Delay Time on Validation Network "First Hour"

 First hour of observation (17:30 - 13:30)

|  | Saterday. June | 27.199         | 6: 8 Observation | na hi eac      | h cell          |                  |              | Sunday June 2  | 8, 1998        | B Observation:   | s in eact      | h celt           |                  |
|--|----------------|----------------|------------------|----------------|-----------------|------------------|--------------|----------------|----------------|------------------|----------------|------------------|------------------|
| Roed   | Observed       |                | Calibrated       |                | T-Test          | Wilcoxon         | Road         | Observed       |                | Calibrated       |                | T-Test           | Wilcowoo         |
| Segment  | Mean<br>(990.) | Stand.<br>Dev. | Mean<br>(sec.)   | Stand.<br>Dev. | Pr> 1           | Pr >   Z         | Segment      | Mean<br>(sec.) | Stand.<br>Dev  | Mean<br>(sec.)   | Stand.<br>Dev. | Pr>11            | Pr >   Z         |
| <  | 9.8            | 3.9            | 8.6              | 0.2            | 0.4188          | 0.958            | <            | 0.0            | 4              | 8.3              | 0.2            | 0.8558           | -                |
| 28   | 12.2<br>21.6   | 0.8<br>3.6     | 13.0<br>19.4     | 0.2            | 0.0442          | 0.1031<br>0.1556 | <b>15</b> 28 | 8.8<br>23.1    | 3.9            | 12.5<br>20.2     | 0.2            | 0.0018<br>0.0781 | 0.0133<br>0.1559 |
| υ  | 14.2           | 2.0            | 15.4             | 2.1            | 0.2552          | 0 2268           | U            | 14.5           | 4,1            | 15.3             | 2.7            | 0.6747           | 0.5835           |
| ۵  | 22.8           | 1.9            | 26.0             | 2.6            | 0.0772          | 0.0659           | ٥            | 30.9           | 3.2            | 30.7             | 4.9            | 0.9396           | 0.7929           |
| 5<br>5<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1 | 8.8<br>12.0    | 1.9<br>2.7     | 10.0<br>12.0     | 1.1            | 0.1756<br>0.997 | 0.1893<br>0.5629 | ភ្ល          | 7.9<br>13.2    | 1.9<br>3.3     | 10.1<br>12.2     | 0.9<br>0.4     | 0.0107<br>0.421  | 0.0353           |
| ĸ  | 11.0           | 3.6            | 12.6             | 8.0            | 0.2416          | 0.5629           | u.           | 10.7           | 5.4            | 12.6             | 0.7            | 0.3704           | 0.1036           |
|  | Monday June 2  | 39. 1996       | . 8 Observetion: | s in each      | Cell            |                  |              | Tuesday June   | 30.199         | 1: 8 Observation | 19 in eac      | h celi           |                  |
| Road   | Observed       |                | Callbrated       |                | T-Test          | Wilcown          | Road         | Observed       |                | Calibrated       |                | T-Test           | Wikown           |
| Segment  | Mean<br>(sec.) | Stand.<br>Dev. | Mean<br>(sec.)   | Stand.<br>Dev  | Pr >  t         | Pr> Z            | Segment      | Mean<br>(sec.) | Stand.<br>Dev. | Mean<br>(sec.)   | Stand.<br>Dev. | Pr> 1            | Pr > [Z]         |
| <  | 10.5           | 4.0            | 8.8              | 0.2            | 0.2203          | 0.4299           | <            | 9.6            | 4.8            | 8.3              | 0.2            | 0.4336           | ~                |
| 8 B  | 12.8<br>18.2   | 1.5<br>5.6     | 13.6<br>19.5     | 0.2            | 0.2006          | 0.1876<br>0.958  | £ 8          | 12.0<br>19.3   | 2.0            | 13.0<br>19.9     | 0.1            | 0.2003<br>0.8099 | 0.3703           |
| υ  | 14.2           | 3.2            | 16.2             | 1.5            | 0.129           | 0.1275           | v            | 20.4           | 3.0            | 20.6             | 3.0            | 980              | 0.9581           |
| ٥  | 27.3           | 2.0            | 28.4             | 3.5            | 0.1717          | 0.1278           | ۵            | 25.5           | 4.6            | 29.3             | 4.4            | 0.1159           | 0.1036           |
| ធា   | 10.8<br>14.7   | 1.9<br>3.6     | 12.2<br>13.0     | 1.9            | 0.1614<br>0.22  | 0.2701<br>0.4309 | 60           | 7.7<br>14.2    | 1.4<br>3.8     | 10.7<br>12.3     | 0.9            | 0.0002<br>0.1984 | 0.0009<br>0.4939 |
| ÷  | 11.7           | 4.0            | 14.4             | 1.0            | 0.1052          | 0.0659           | L            | 14.4           | 3.7            | 13.0             | 8.0            | 0.3297           | 0.4306           |

|              |                  |               |                  | ι.             | Inst hour of     | observation      | n (12:30 - | 13:30)         |               |                |                |                  |                  |
|--------------|------------------|---------------|------------------|----------------|------------------|------------------|------------|----------------|---------------|----------------|----------------|------------------|------------------|
|              | uk. vebsedev.    | k 1 19        | BB- B Observatio | ns in en       | ch cell          |                  |            | Thursday, luty | 2 1008        | 8 Chaenterione | in each        | llor             |                  |
|              |                  |               |                  |                |                  |                  |            |                |               |                |                |                  |                  |
| Road         | Observed         |               | Calibrated       |                | T-Test           | Wikowon          | Road       | Observer       |               | Calibrated     |                | T-Test           | Wilcoxon         |
| Segment      | Mean<br>(sec.)   | Stand.<br>Dev | Mean<br>(sec.)   | Stand.<br>Dev. | Pr >   t         | Hz   < Jd        | Segment    | Mean<br>(sec.) | Stand.<br>Dev | Mean<br>(sec.) | Stand.<br>Dev. | Pr > [1]         | Pr >  Z          |
| ۲            | 7.5              | 1.2           | 8.3              | 0.4            | 0.1179           | 0.188            | ¥          | 11.6           | 4.6           | 8.7            | 0.3            | 0.1245           | 0.2698           |
| 8<br>8       | 12.4<br>19.7     | 1.7           | 12.8<br>17.8     | 0.2<br>2.6     | 0.4416<br>0.1563 | 0.4942<br>0.0406 | B<br>8     | 12.8<br>17.8   | 2.1           | 13.8<br>19.2   | 0.2            | 0.2174<br>0.2101 | 0.1023<br>0.1278 |
| υ            | 12.1             | 1.5           | 13.4             | 1.4            | 0.1093           | 0.1033           | U          | 20.6           | 3.1           | 23.2           | 5.6            | 0.2639           | 0.3181           |
| ٥            | 21.1             | 2.7           | 22.2             | 1.4            | 0.3435           | 0.2694           | ۵          | 30.4           | 9.9           | 34.3           | 4.6            | 0.1919           | 0.1893           |
| E 6          | 5.0<br>12.8      | 1.5<br>3.6    | 8.3<br>11.7      | 0.4            | 0.0003           | 0.0009           | E 2        | 10.1<br>15.0   | 3.1<br>2.7    | 11.7<br>13.2   | 1.3            | 0.2266<br>0.0975 | 0.1889<br>0.2694 |
| Ľ            | 11.2             | 2.2           | 12.4             | 0.5            | 0.1532           | 0.713            | u.         | 12.8           | 4.0           | 14.9           | 0.8            | 0.2012           | 0.04             |
|              | Fridey July 3. 1 | 996: 10       | Observations in  | Leach G        |                  |                  |            |                |               |                |                |                  |                  |
| Road         | Observed         |               | Cetibrated       | ·              | T-Test           | Wilcoxon         |            |                |               |                |                |                  |                  |
| Segment      | Mean<br>(sec.)   | Stand.<br>Dev | Mean<br>(sec.)   | Stand.<br>Dev  | Pr >  t          | Pr> Z            |            |                |               |                |                |                  |                  |
| <            | 5.6              | 4.0           | 7.3              | 0.5            | 0.2212           | 0.1036           |            |                |               |                |                |                  |                  |
| <u>19</u> 99 | 8.8<br>8.8       | 2.1<br>3.9    | 10.1<br>10.8     | 0.3            | 0.012<br>0.1502  | 0.0088<br>0.4267 |            |                |               |                |                |                  |                  |
| υ            | 4.0              | 2.0           | 6.3              | 0.3            | 0.0055           | 0.0028           |            |                |               |                |                |                  |                  |
| ٥            | 8.7              | 2.3           | 10.5             | 0.7            | 0.0395           | 0.0311           |            |                |               |                |                |                  |                  |
| 5<br>2<br>2  | 2.4              | 2.0<br>4.8    | 5.8<br>8.7       | 0.2            | 0.0003           | 0.0028           |            |                |               |                |                |                  |                  |
| Ŀ            | 6.3              | 2.4           | 7.7              | 0.3            | 0.0098           | 0.0028           |            |                |               |                |                |                  |                  |

 Table 4-9 (continued)

 Statistical analysis of Delay Time on Validation Network "First Hour"

 First hour of observation (12:30 - 13:30)

Second, the column labeled Wilcoxon Pr > |Z|, a non-parametric test, also gives the p-values for comparing the two group means. According to the data presented, there are 6 road segments with a p-value greater than 0.05 during the six week days (Saturday through Thursday). And on Friday the weekend there are 5 road segments with a p-value greater than 0.05.

In summary, based on the results presented by both parametric and nonparametric procedures the p-values for most links are much greater than 0.05. This means that this study would fail to reject the null hypothesis and conclude that the average Delay Times simulated from the calibrated Netsim model and those observed in the field are not significantly different based on the data presented during the first hour of observation. This is a positive indication of how well the calibrated Traf-Netsim simulation model performs in Amman-Jordan. However, on Friday's there is a statistical significance between the calibrated Netsim model and the observed values in the field. Travel Time on Validation Network "Second Hour":

In reference to the summary of statistical analysis of Travel Time on the Validation Network for the second hour (Table 4-10) the following is presented:

First, the column under the heading T-Test Pr > |t| gives the p-values for comparing the means derived from the calibrated model and those observed in the validation network. The majority of the values are greater than the 5% significance level. From the possible 48 links (8 segments \* 6 weekdays) only 6 showed differences that are significant at the 5% level. However, on Friday the weekend, 5 out of 8 links showed significant differences between the calibrated and observed Travel Times.

Table 4-10 Statistical analysis of Travel Time on Validation Network "Second Hour" Second hour of observation (13:30 - 14:30)

|             | Saterday June  | 27.199         | 8: 8 Observation | ns in eac      | th cell          |                 |              | Sunday June 2  | 8. 1999        | . 8 Observations | s in eac      | h cel            |                  |
|-------------|----------------|----------------|------------------|----------------|------------------|-----------------|--------------|----------------|----------------|------------------|---------------|------------------|------------------|
| Road        | Observed       |                | Calibrated       |                | T-Test           | Włcoxon         | Road         | Observed       | -              | Calibrated       |               | T-Test           | Wilcoron         |
| Segment     | Mean<br>(sec.) | Stand.<br>Dev. | Mean<br>(sec.)   | Stand.<br>Dev  | Pr> t            | Pr> Z           | Segment      | Mean<br>(sec.) | Stand.<br>Dev. | Mean<br>(sec.)   | Stand.<br>Dev | Pr >  t          | Pr > [Z]         |
| ۲           | 18.0           | 3.4            | 17.4             | 1.7            | 0.654            | 0.8744          | <            | 20.1           | 4.4            | 17.1             | 0.3           | 0.0797           | 0.4302           |
| 88          | 23.4<br>38.6   | 3.3            | 25.4<br>39.8     | 0.1            | 0.121<br>0.409   | 0.013<br>0.6365 | 66<br>66     | 23.5<br>36.3   | 2.4            | 25.6<br>37.4     | 0.2           | 0.0226<br>0.5138 | 0.0649           |
| U           | 23.5           | 3.7            | 26.6             | 1.4            | 0.0553           | 0.0659          | v            | 22.4           | 4.8            | 24.6             | 1.0           | 0.2287           | 0.3717           |
| ۵           | 34.6           | 3.0            | 36.8             | 3.2            | 0.1614           | 0.1559          | ۵            | 32.4           | 3.5            | 34.9             | 2.6           | 0.1276           | 0.2271           |
| 9<br>6<br>6 | 20.0<br>29.4   | 2.5            | 23.0<br>31.8     | 0.7<br>4.5     | 0.0107<br>0.3105 | 0.0136          | E G          | 20.9<br>31.2   | 2.4<br>3.4     | 22.3<br>30.3     | 0.6<br>0.6    | 0.154<br>0.4986  | 0.3184<br>0.9581 |
| μ           | 19.9           | 5.4            | 22.0             | 4.4            | 0.4145           | 0.0657          | Ľ            | 19.4           | 1.8            | 20.0             | 0.6           | 0.3683           | 0.2268           |
|             | Monday June ;  | 29.1996        | : 8 Observation: | s in each      | Cel              |                 |              | Tuesday June   | 30, 199        | 3: 8 Observation | te in eac     | th cell          |                  |
| Road        | Observed       |                | Calibrated       |                | T-Test           | Wilcoxon        | Road         | Observed       |                | Calibrated       |               | T-Test           | Witcom           |
| Segment     | Mean<br>(sec.) | Stand.<br>Dev  | Mean<br>(sec.)   | Stand.<br>Dev. | Pr> 1            | Pr> 2           | Segment      | Mean<br>(sec.) | Stand.<br>Dev. | Mean<br>(sec.)   | Stand.<br>Dev | Pr > [t]         | Pr > [Z]         |
| ٩           | 20.7           | 3.9            | 17.1             | 0.3            | 0.0324           | 0.1028          | ۲            | 19.6           | 3.7            | 17.7             | 0.3           | 0.1762           | 0.1141           |
| £ 8         | 26.6<br>40.3   | 4.3            | 25.6<br>38.8     | 1.4            | 0.5525<br>0.2655 | 1<br>0.5632     | <b>1</b> 8 8 | 22.4<br>37.6   | 3.2<br>3.2     | 26.7<br>38.8     | 0.2           | 0.0065<br>0.3339 | 0.0134<br>0.372  |
| υ           | 26.3           | 4.1            | 27.4             | 4.             | 0.494            | 0.7128          | υ            | 27.1           | 3.8            | 28.3             | 1.7           | 0.4221           | 0.4948           |
| ٥           | 42.0           | 2.0            | 38.9             | 3.1            | 0.0317           | 0.0681          | ٥            | 41.0           | 3.8            | 41.1             | 4.2           | 0.9547           | ~                |
| ደ ቧ         | 21.2<br>32.4   | 3.9            | 23.2<br>31.3     | 0.8            | 0.0325<br>0.4348 | 0.0659          | ធនា          | 24.1<br>30.1   | 2.8            | 25.2<br>31.8     | 1.4<br>0.8    | 0.1112<br>0.0823 | 0.1893<br>0.2268 |
| Ŀ           | 20.2           | 2.2            | 21.5             | 0.6            | 0.1269           | 0.0404          | ù.           | 19.7           | 3.6            | 21.7             | 0.5           | 0.1398           | 0.1036           |
|          |                  |                |                   | ŝ              | cond hour c      | of observativ    | on ( 13:30 | - 14:30 )      |                |                |              |                  |  |
|----------|------------------|----------------|-------------------|----------------|------------------|------------------|------------|----------------|----------------|----------------|--------------|------------------|--|
|          | Wednesday Ju     | IV 1. 19       | 95. 8 Observation | ons in ea      | ch cell          |                  |            | Thursday July  | 2, 1998        | 8 Observations | s in each    | 8                |  |
| Road     | Observed         |                | Calibrated        |                | T-Test           | Wilcoxon         | Road       | Observed       |                | Calibrated     |              | T-Test           | Wilcowon   |
| Segment  | Mean<br>(sec.)   | Stand.<br>Dev. | Mean<br>(9ec.)    | Stand.<br>Dev. | Pr> 1            | Pr > JZ          | Segment    | Mean<br>(sec.) | Stand.<br>Dev. | Mean<br>(sec.) | Stand<br>Dev | Pr > [1]         | Pr >  Z  |
| ۲        | 16.8             | 3.0            | 17.2              | 0.3            | 0.5916           | 0.4302           | ۲          | 15.7           | 3.9            | 17.0           | 0.1          | 0.3575           | 0.1015   |
| 87<br>82 | 23.8<br>37.7     | 2.5<br>3.3     | 25.7<br>39.8      | 0.3<br>1.5     | 0.0682<br>0.1695 | 0.1889<br>0.3184 | 88         | 26.9<br>36.6   | 1.7            | 26.1<br>39.4   | 0.2          | 0.1669<br>0.1191 | 0.4289<br>0.2271   |
| υ        | 28.9             | 2.3            | 30.6              | 3.2            | 0.2508           | 0.3181           | v          | 27.3           | 2.1            | 29.8           | 3.3          | 0.0881           | 0.1033   |
| ٥        | 38.9             | 4.0            | 41.5              | 4.6            | 0.254            | 0.372            | ٥          | 36.6           | 3.4            | 38.8           | 3.1          | 0.2488           | 0.7927   |
| 12 II    | 21.2<br>30.1     | 4.0            | 23.6<br>30.8      | 0.6<br>0.7     | 0.1347<br>0.5214 | 0.0829<br>0.7923 | E2         | 21.4<br>28.7   | 4.4<br>3.5     | 23.3<br>30.7   | 0.6<br>0.6   | 0.2442<br>0.1413 | 0.8767<br>0.1033   |
| Ŀ        | 20.4             | 3.4            | 21.3              | 0.6            | 0.4787           | 0.4306           | LL.        | 20.8           | 1.9            | 21.7           | 0.6          | 0.2059           | 0.5277   |
|          | Friday July 3. 1 | 998: 9 (       | Observations in   | each ce        |                  |                  |            |                |                |                |              |                  |  |
| Road     | Observed         | _              | Calibrated        |                | T-Test           | Wilcoxon         |            |                |                |                |              |                  | - 11 -   |
| Segment  | Mean<br>(sec)    | Stand.<br>Dev  | Mean<br>(sec.)    | Stand.<br>Dev. | Pr >  t          | Pr >  Z          |            |                |                |                |              |                  |  |
| <        | 14.9             | 2.7            | 15.7              | 0.4            | 0.3925           | 0.9296           |            |                |                |                |              |                  |  |
| 83<br>87 | 19.9<br>28.0     | 1.3<br>5.3     | 23.3<br>31.0      | 0.2<br>0.6     | < 0001<br>0.1282 | 0.0004<br>0.2327 | <u></u>    |                |                |                |              |                  |  |
| υ        | 15.9             | 2.8            | 19.1              | 0.3            | 9600.0           | 0.0061           |            |                |                |                |              |                  |  |
| ۵        | 21.6             | 1.9            | 23.7              | 0.8            | 0.0101           | 0.0092           |            |                |                |                |              |                  |  |
| E G      | 16.5<br>29.3     | 1.6<br>3.9     | 19.9<br>27.6      | 0.1<br>0.3     | 0.0003           | 0.0004<br>0.1327 |            |                |                |                |              |                  |  |
| Ľ        | 13.2             | 2.7            | 15.8              | 0.7            | 0.0162           | 0.0061           |            |                |                |                |              |                  | <u>, 1997</u> , 19977, 1997, 19977, 1997, 1997, 1997, 1997, 1997, 1997, 1997, 19977, |

Table 4-10 (continued) Statistical analysis of Travel Time on Validation Network "Second Hour" Second hour of observation (13:30 - 14:30)

Second, Looking at the column labeled Wilcoxon Pr > |Z| which gives the p-values for the non-parametric procedure. In this column the majority of the p-values are also greater than 0.05 with the exception of links B1 and E1 on Saturday, F on Monday, B1 on Tuesday, and B1, C, D, E1, and F on Friday.

In closure, since the majority of the p-values during the weekday (i.e. Saturday, Sunday, Monday, Tuesday, Wednesday, and Thursday) are greater than the reference probability of 0.05. This means that I would fail to reject the null hypothesis and conclude that it appears that the simulated Travel Times from the calibrated Traf-Netsim model are not significantly different from the observed Travel Times in the field. This supports the finding of Travel Times during the first hour and further supports the idea that the calibrated Netsim model is transposable and can accurately predict the traffic performance in Amman-Jordan. However, Looking at Friday, which is the weak end in Jordan, It appears that the calibrated model doesn't predict the traffic performance in Jordan. The values derived from the model are larger than those observed in the field. This could mean that drivers are more aggressive on Fridays and don't follow the speed limit signs. An important fact to state is that on Friday's the traffic volumes are down by 50% in comparison with the weekday traffic volumes during the same hour.

#### Delay Time on Validation Network "Second Hour":

Looking at the statistical inquiry of Delay Time on the Validation Network during the second hours of data collection (Table 4-11) the following remarks and interpretations are presented:

First, the column under the heading T-Test Pr > |t| gives the p-values for comparing delay times during the second hour for the two groups. The numbers in most

Table 4-11 Statistical analysis of Delay Time on Validation Network "Second Hour" Second hour of observation (13:30 - 14:30 )

|                  | Saterday June    | 27, 199           | 8. 8 Observation   | ts in eac     | h cell             |                      |                 | Sunday June 2    | 8.1998         | 8 Observation:              | s in each      | , celi             |                      |
|------------------|------------------|-------------------|--------------------|---------------|--------------------|----------------------|-----------------|------------------|----------------|-----------------------------|----------------|--------------------|----------------------|
| Road<br>Segment  | Observed<br>Mean | Stand.            | Calibrated<br>Mean | Stand         | T-Test<br>Pr > [t] | Witcoxon<br>Pr > [Z] | Road<br>Segment | Observed<br>Mean | Stand          | Calibrated<br>Mean<br>(sec) | Stand          | T.Test<br>Pr > [1] | Wilcoxon<br>Pr >   Z |
| 4                | 9.6              | 3.4               | 8.9                | 1.7           | 0.6022             | 0.8744               | ۲               | 11.7             | 4.4            | 8.6                         | 0.3            | 0.0913             | 0.3713               |
| <b>15</b> 66     | 10.6<br>19.1     | 6. 6<br>6. 8<br>8 | 12.4<br>20.0       | 0.1           | 0.1474<br>0.5241   | 0.013                | <b>16</b> 68    | 10.7<br>18.8     | 4.2            | 12.8<br>17.6                | 0.2            | 0.0311<br>0.6099   | 0.1008<br>0.9581     |
| v                | 10.8             | 3.7               | 13.8               | 1.4           | 0.065              | 0.0829               | υ               | 9.7              | 4.8            | 11.8                        | 1.0            | 0.2619             | 0.3717               |
| ٥                | 22.0             | 3.0               | 24.1               | 3.2           | 0.1902             | 0.1889               | ۵               | 19.8             | 3.4            | 22.1                        | 2.6            | 0.1515             | 0.2701               |
| 2 Q              | 6.3<br>10.8      | 4.5               | 9.2<br>12.9        | 0.8<br>4.5    | 0.0145<br>0.3608   | 0.0239<br>0.7927     | 56              | 7.3<br>12.6      | 3.4            | 8.4<br>11.5                 | 0.6            | 0.214<br>0.3882    | 0.4306<br>0.7132     |
| ٤.               | 11.1             | 5.4               | 13.1               | 4.4           | 0.4367             | 0.0659               | ц.              | 10.6             | 1.8            | 11.1                        | 0.6            | 0.447              | 0.2271               |
|                  | Monday June 2    | <b>1998</b>       | : 8 Observation    | s in each     | ) cell             |                      |                 | Tuesday June     | 30.199         | 3: 8 Observation            | 15 In eac      | h ceil             |                      |
| Road             | Observed         |                   | Callbrated         |               | T-Test             | Wilcoxon             | Road            | Observed         |                | Calibrated                  |                | T-Test             | Wilcoxon             |
| Segment          | Mean<br>(sec.)   | Stand.<br>Dev     | Mean<br>(Sec.)     | Stand.<br>Dev | Pr>+!!             | Pr > [Z]             | Segment         | Mean<br>(sec.)   | Stand.<br>Dev. | Mean<br>(sec.)              | Stand.<br>Dev. | Pr>[1]             | Pr >   Z             |
| ۷                | 12.3             | 3.9               | 8.6                | 0.3           | 0.0291             | 0.1028               | ۲               | 11.2             | 3.7            | 9.2                         | 0.3            | 0.158              | 0.1028               |
| <b>8</b> 3<br>87 | 13.8<br>20.8     | 4.3               | 12.7<br>18.8       | 0.2           | 0.4994<br>0.1942   | 1<br>0.3181          | 66              | 9.5<br>18.0      | 2.5<br>3.2     | 12.7<br>19.0                | 0.2            | 0.0083<br>0.4399   | 0.0134<br>0.4945     |
| U                | 13.6             | 4.0               | 14.6               | 1.4           | 0.5542             | 0.7963               | υ               | 14.4             | 3.8            | 15.5                        | 1.7            | 0.4802             | 0.5283               |
| ٥                | 29.4             | 2.0               | 26.1               | 3.1           | 0.027              | 0.0661               | G               | 28.4             | 3.8            | 28.4                        | 0.2            | 0.982              | 0.7929               |
| ធន               | 7.5<br>13.8      | 3.9               | 9.3<br>12.4        | 0.6           | 0.0491<br>0.343    | 0.1036               | E3              | 10.4             | 1.2<br>2.6     | 11.3<br>13.0                | 1,4<br>0.8     | 0.1884<br>0.1435   | 0.2701<br>0.3177     |
| Ŀ.               | 11.3             | 2.2               | 12.6               | 0.7           | 0.159              | 0.0406               | Ŀ               | 10.9             | 3.6            | 12.B                        | 0.6            | 0.1797             | 0.1036               |

|              |                  |                |                  | -              |                  |                  |          |                |               |                |               |                  |                  |
|--------------|------------------|----------------|------------------|----------------|------------------|------------------|----------|----------------|---------------|----------------|---------------|------------------|------------------|
|              | Wednesday Ju     | N 1. 195       | 38: 8 Observatio | ee in ee       | ch cell          |                  |          | Thursday July  | 2, 1998;      | 8 Observations | s in each     | celi             |                  |
| Road         | Observed         |                | Calibrated       |                | T-Test           | Wilcoxon         | Roed     | Observed       |               | Calibrated     |               | T-Test           | Wilcoxon         |
| Segment      | Mean<br>(sec.)   | Stand.<br>Dev. | Mean<br>(sec.)   | Stand.<br>Dev  | Pr> 1            | Pr >  Z          | Segment  | Meen<br>(sec.) | Stand.<br>Dev | Mean<br>(sec.) | Stand.<br>Dev | Pr > [1]         | Pr >   Z         |
| ۲            | 8.2              | 3.0            | 8.7              | 0.3            | 0.6546           | 0.4302           | ۷        | 7.3            | 3.9           | 8.5            | 0.1           | 0.392            | 0.1015           |
| <u> 8</u> 8  | 10.9<br>18.2     | 33<br>33       | 12.7<br>19.8     | 0.3            | 0.0765<br>0.2426 | 0.2268<br>0.4309 | 83<br>83 | 14.1<br>17.1   | 1.7           | 13.1<br>19.6   | 0.2<br>1.4    | 0.1308<br>0.1558 | 0.2698           |
| υ            | 16.3             | 2.3            | 17.8             | 3.2            | 0.2896           | 0.4306           | U        | 14.6           | 2.1           | 17.0           | 3.3           | 0.1079           | 0.1033           |
| ۵            | 26.3             | 4.0            | 28.7             | 4.5            | 0.2869           | 0.372            | ۵        | 24.2           | 3.4           | 26.0           | э.<br>1       | 0.2948           | 0.7926           |
| ۲ <u>۳</u>   | 7.5<br>11.5      | 40<br>26       | 9.7<br>12.0      | 0.6            | 0.1588<br>0.6579 | 0.1031<br>0.8745 | ۵<br>۳   | 7.7<br>10.1    | 3.5           | 9.5<br>11.9    | 0.6<br>0.6    | 0.3066<br>0.2016 | 0.8748<br>0.1033 |
| Ŀ            | 11.5             | 3.4            | 12.3             | 0.6            | 0.5362           | 0.4306           | LL.      | 11.9           | 1.9           | 12.8           | 0.7           | 0.2565           | 0.6363           |
|              | Friday July 3, 1 | 9995:9 (       | Observations In  | eech ce        |                  |                  |          |                |               |                |               |                  |                  |
| Road         | Observed         |                | Calibrated       |                | T-Test           | Wilcoxon         |          |                |               |                |               |                  |                  |
| Segment      | Mean<br>(sec.)   | Stend.         | Mean<br>(sec.)   | Stand.<br>Dev. | Pr> 1            | Pr >  Z          |          |                |               |                |               |                  |                  |
| ۷            | 6.5              | 2.7            | 7.2              | 0.4            | 0.4508           | 0.8598           |          |                |               |                |               |                  |                  |
| <b>16</b> 88 | 7.1<br>8.4       | 1.3<br>5.3     | 10.3             | 0.2            | <.0001<br>0.1605 | 0.0004<br>0.4283 | <u></u>  |                |               |                |               |                  |                  |
| υ            | 3.2              | 2.8            | 6.3              | 0.3            | 0.0122           | 0.0061           |          |                |               |                |               |                  |                  |
| ۵            | 0.6              | 1.9            | 10.9             | 0.8            | 0.0166           | 0.0216           |          |                |               |                |               |                  |                  |
| 5 E          | 2.8<br>10.7      | 1.6<br>3.9     | 6.0<br>8.8       | 0.1<br>0.3     | 0.0004<br>0.1841 | 0.0004<br>0.0766 |          |                |               |                |               |                  |                  |
| u.           | 4.3              | 2.7            | 7.0              | 0.7            | 0.0193           | 0.0061           |          |                |               |                |               |                  |                  |

Table 4-11 (continued) Statistical analysis of Deley Time on Valkation Network "Second Hour" Second hour of observation (13:30 - 14:30)

cases are larger than the reference probability value of 0.05. This is true of all the weekdays with the exception of road segment E1 on Saturday, B1 on Sunday, D and E1 on Monday, and B1 on Tuesday. Therefore from the total 48 road segments during the weekday only 5 showed statistical differences at the 5% significant level. On Friday, the following 5 road segments showed statistical differences at the 5% level. The five segments are B1, C, D, E1, and F.

Second, the column under the heading Wilcoxon Pr > |Z| gives the associated p values based on a non-parametric test. The majority of the p-values during the weekdays are larger than the 5% significant level. This is true for all road segments in the validation network with the exception of road segment B1 on Saturday, Sunday, and Tuesday. Therefore only 3 out of possible 48 links showed statistical differences at the 5% significant level. On Friday, the values say a different story. As can be seen from the table, there are 5 road segments having a p-value less than 0.05. This indicates that for Friday the results are significantly different. The five road segments are B1, C, D, E1, and F, which are the same according to the two-sample t-test.

In summary, the statistical tests for Delay Time during the second hour produces large p-values on the majority of the road segments during the weekdays. This means that this research would fail to reject the null hypothesis and concludes that the average Delay Times simulated from the calibrated Traf-Netsim model are not significantly different from those observed in the field during the validation study. This is a good indication of how well the calibrated model performed in the validation network.

Nonetheless, since the p-values for Friday are less than the reference probability of 0.05, this implies that there is a statistical difference between the calibrated and

observed delay times, thus the null hypothesis is rejected.

#### Summary of Findings on the Validation Network

This research recorded and observed traffic volumes on the Validation Network (Safeway Street) for a period of two hours on seven consecutive days in Amman-Jordan. This phase of the study performed a total of 57 simulation runs using the calibrated Traf-Netsim model with the following parameters reflecting the Jordanian driving environment.

- The mean Start-up Lost Time was modified from 2.0 seconds to 1.8 seconds.
- The distribution of Start-up Lost Time was modified as shown below

| Driver<br>Characteristic<br>K | 1   | 2   | 3   | 4   | 5   | 6  | 7  | 8  | 9  | 10 |
|-------------------------------|-----|-----|-----|-----|-----|----|----|----|----|----|
| Default                       | 218 | 140 | 125 | 118 | 102 | 86 | 78 | 63 | 47 | 23 |
| Calibrated                    | 211 | 169 | 141 | 121 | 101 | 83 | 64 | 48 | 37 | 25 |

- The mean Queue Discharge headway was modifies from 1.8 seconds to 1.5 seconds.
- The distribution of Queue Discharge Headway was modified as shown below:

| Driver<br>Characteristic<br>K | 1   | 2   | 3   | 4   | 5   | 6   | 7  | 8  | 9  | 10 |
|-------------------------------|-----|-----|-----|-----|-----|-----|----|----|----|----|
| Default                       | 170 | 120 | 120 | 110 | 100 | 100 | 90 | 70 | 70 | 50 |
| Calibrated                    | 180 | 134 | 118 | 105 | 95  | 88  | 81 | 75 | 67 | 57 |

The mean Free Flow Speed was modified from 30 mph (48 Km/h) to 38 mph (60 Km/h) the posted speed limit.

The main objective of this phase is to test if the calibrated Traf-Netsim model is transportable. That is, to test if the model can simulate traffic conditions at a second site

without changes to any of the calibrated parameters measured in the Test Network. The only change would be the input data directly related to the characteristics of the validation network. This was accomplished by the following:

First, the validation network had to be coded into Netsim in the form of nodes and links as specified by Traf-Netsim format.

Second, the calibrated model was executed several times and the simulated Travel Times and Delay Times were compared with the observed values derived from the floating car method.

To compare the two group means the following hypotheses were used. The null hypothesis for Travel Time states that the population means are the same. And the alternative hypothesis states that the population means are different. For Delay Time similar hypotheses where setup. The summary of statistical analysis of Travel Time and Delay Time for the Validation Network was presented in Tables 4-8, 4-9, 4-10, and 4-11.

The statistical tests for Travel Time indicated that there are no differences between the calibrated values and the observed values for all weekdays. Thus, the null hypothesis could not be rejected and this study concluded that the calibrated Netsim model could accurately predict Travel Times during the weekdays. An exception was found for Friday, which is a public holiday, thus the null hypothesis was rejected in favor of the alternative hypothesis and this research concluded that the calibrated model couldn't accurately predict the Travel Times under low traffic volumes.

The statistical tests for Delay Time also indicated that there are no differences between the calibrated and the observed values for all the weekdays. As before, the calibrated model failed to predict, within a given accuracy, the observed Delay Times on

Friday's. Although from a practical point of view it appears that the calibrated values were higher than the observed values. This would mean that under low traffic conditions drivers do act quicker than under heavy traffic conditions.

#### CHAPTER V

#### DISCUSSION AND RECOMMENDATIONS

#### Discussion

As urban traffic congestion continues to increase in many metropolitan cities around the globe, traffic engineers are constantly applying the latest technology to help manage traffic problems. The traffic engineer's responsibility goes beyond optimization of movement on a limited network to a complete and comprehensive evaluation of different transportation strategies on a systemwide basis. TRAF-NETSIM, which is a microscopic computer simulation program developed in the United States of America, is one of the most accepted and respected traffic network simulation models among the profession. In addition it is probably one of the most extensively tested and validated traffic simulation model in America. However, to use TRAF-NETSIM in other regions around the world, the model's ability to simulate the traffic performance within an acceptable tolerance should be properly tested and validated.

Amman, the capital of Jordan is a major commercial, economic, and cultural center of almost two million inhabitants. The city of Amman, like many other cities in the region, has its share of traffic congestion on its main streets. However, the traffic department in Amman – Jordan does not employ this computer software technology to assist municipal engineers and policy makers in making decisions, as to which design schemes should be implemented on the road network. The main objective of this research is to test whether or

not TRAF-NETSIM can accurately simulate the driving conditions in Amman - Jordan. This was accomplished through actual field observations of traffic flow on two selected high-volume urban arterial roads in Amman. To capture all of the traffic activities along the arterial road, several high-tech video cameras, positioned in strategic locations on top of high buildings were used to record traffic counts. This procedure required more equipment than manual traffic counts, but it had the advantage of requiring fewer personnel in the field, thus minimizing possible error in data collection. Nonetheless, additional time was required to summarize traffic data from the videos.

Based on the data collected and gathered through out this study and the statistical analysis on the various measures of performance, the following conclusions were reached:

- The TRAF-NETSIM model can be used to simulate the traffic conditions in Amman-Jordan provided that the following values of various traffic parameters are used.
  - A mean Start-Up Lost Time of 1.8 seconds should be specified instead of the default value of 2.0 seconds in the model.
  - The distribution of Start-up Lost Time should be modified as shown below:

| Driver<br>Characteristic | 1   | 2   | 3   | 4   | 5   | 6  | 7  | 8  | 9  | 10 |
|--------------------------|-----|-----|-----|-----|-----|----|----|----|----|----|
| K<br>Default             | 218 | 140 | 125 | 118 | 102 | 86 | 78 | 63 | 47 | 23 |
| Calibrated               | 211 | 169 | 141 | 121 | 101 | 83 | 64 | 48 | 37 | 25 |

- A mean Queue Discharge Headway of 1.5 seconds should be specified instead of the default value of 1.8 seconds embedded in the model.
- The distribution of Queue Discharge Headway should be modified as shown below:

| Driver<br>Characteristic<br>K | 1   | 2   | 3   | 4   | 5   | 6   | 7  | 8  | 9  | 10 |
|-------------------------------|-----|-----|-----|-----|-----|-----|----|----|----|----|
| Default                       | 170 | 120 | 120 | 110 | 100 | 100 | 90 | 70 | 70 | 50 |
| Calibrated                    | 180 | 134 | 118 | 105 | 95  | 88  | 81 | 75 | 67 | 57 |

- The Calibrated TRAF-NETSIM was able to predict Travel Time within a 5% confidence level for Saturday, Sunday, Monday, Tuesday, Wednesday, and Thursday on both the Test and Validation networks. As can be seen from Tables 5-1 and 5-2, the majority of the road segments showed no significant differences between the simulated travel times from the calibrated model and the observed travel times in the field.
- The Calibrated TRAF-NETSIM was able to predict Delay Time within a 5% confidence level for Saturday, Sunday, Monday, Tuesday, Wednesday, and Thursday on both the Test and Validation networks Tables 5-3, and 5-4. The majority of the links showed no statistical significance between the simulated delay times and those observed in the field.
- The Calibrated TRAF-NETSIM model was not able to simulate the observed Travel Time and Delay Time during a Friday. It should be mentioned that Jordan has a six-day workweek with Fridays off and that Friday traffic is similar to Sunday traffic encountered in the United States.
- The simulated Travel Time's using the default values were significantly different from the observed Travel Times. Table 5-5 shows a summary of travel times between the observed and simulated values on the test network.
- The simulated Delay Time's using the default values were significantly different from the observed delay time. Table 5-6 shows delay times between the simulated values and those observed in the field.

| OBSERVED                           | S          | ¥.                  | TURDAY                                   |                      | ONDS                 | Aγ                    |       | MONDAY  |            |             | TUESDAY         |        |               | VEDNES | DAY |               | THURSD       |            |               | VACIA        |            |   |
|------------------------------------|------------|---------------------|--|----------------------|----------------------|-----------------------|-------|---------|------------|-------------|-----------------|--------|---------------|--------|-----|---------------|--------------|------------|---------------|--------------|------------|---|
| CALIBRATED                         | 0          | S8                  | AL Y I                                   | NOB                  | SCAL                 | 2 × ×                 | OBS   | CAL     | Z          | SHO         | CAI V           | - 1    | å             | 2      |     | 900           | 1            | ,          | 40            |              |            |   |
|                                    |            |                     |  |                      |                      |                       |       |         |            |             |                 |        | 2007          |        |     | 200           | AN I         |            | 25            | S            |            |   |
| 41<br>14<br>14                     | <br>       | 4 G 4               | 2.2<br>1.2                               | 8                    | 6 36.5               | <b>z</b> :            | 38.1  | 37.1    | z          | 34.6        | 36.5            | z      | 35.9          | 36.8   | z   | 36.3          | 37.8         | z          | 30.3          | 33.5         | ≻          | _ |
| A2 1st                             | 0 80<br>   |                     |  | 2                    |                      | za                    | 298   | 37.5    | z          | 37.0        | 37.7            | > :    | 36.2          | 37.2   | Ż   | 36.9          | 37.6         | z          | 31.2          | 34.1         | 7          | _ |
| ž                                  | 5 ₹        | 9.4                 | 7.2<br>N                                 |                      | 37.1                 | z                     | 37.5  | 37.5    | <b>z</b> z | 0.00<br>19  | 8. <del>-</del> | 2 2    | 57.6          | 37.0   | z   | 31.2          | 37.1         | <b>z</b> : | 34.9          | 36.4         | Z          |   |
| A3 1st                             | H-         | 2.1 5               | 3.6 N                                    | 1 51.                | 8 53.0               | Ż                     | 53.9  | 222     | : 2        | 52.0        | 525             | : 2    | 2.02          |        | 2 2 |               | 2.5          | 2 7        | 5             | 36.2         | ≻ :        | _ |
| 22                                 | 14 5       | 44 5                | 52 N                                     | 8                    | 7 55.8               | Z                     | 56.1  | 56.1    | Z          | 55.0        | 58.2            | N      | 52.7          | 56.4   | • > | 38            | 57.1         | zz         | 5 C F         | 45.1         | <b>z</b> 2 |   |
| 81 (st                             | н.<br>     |                     | N 0.0                                    |                      | 8<br>200             | 2                     | 9 9 9 | 6 70    | 2          | 1           | 4               |        |               |        |     |               |              |            |               | 172          |            |   |
| i k                                | ; ≠<br>: ± |                     |  |                      |                      | 2 2                   |       |         | 2 3        |             | R a             | 2 :    | 20.3          | 20.9   | z   | 20.4          | 21.0         | z          | 18.8          | 21.0         | z          | l |
| B2<br>1#1                          | Hr 5       | 11                  | - 1- 1- 1- 1- 1- 1- 1- 1- 1- 1- 1- 1- 1- |                      | a 21.7               | 2 >                   | 228   | 24.7    | z >        |             | 246             | z      | 20.6          | 210    | z:  | 22.1          | 21.1         | z          | 19.5          | <b>5</b> 0.9 | z          |   |
| 240                                | H H        | 3.9                 | 1.8<br>N                                 | 7                    | 1 216                | Z                     | 224   | 810     | - 2        | 3.04        | 017             | 2 >    |               | 112    | z : | 20.0          | 21.7         | > :        | 18.9          | 21.0         | ≻          |   |
| B3<br>1#1                          | ю<br>Ŧ     | 3.0                 | 3.8                                      |                      | 9 33.8               | Ż                     | 32.2  | 33.9    | 2 2        | 0.07<br>M 0 | 8.12            | - 2    | 0.07          | 1.17   | z : | 807           | 21.8         | z          | 22.8          | 21.2         | ≻ :        | _ |
| ž                                  | H 3        | 2.2 3               | 3.9 N                                    | 32                   | 7 33.7               | z                     | 317   | 33.6    | : >        | 30.6        | 22              | : z    | , e           |        | 2 2 | <b>93.0</b>   | 97.92<br>0   | z 2        | 32.5          | 33.2         | <b>z</b> : | _ |
| B4 1st                             | ¥          | 9.9                 | 2.2 N                                    | 1 48.                | 2 48.4               | z                     | 55.6  | 53.2    | z          | 50.3        | 49.6            | : z    | 273           | 20.5   | : 2 | 44.7<br>44.7  | 8.00<br>87.8 | 2 2        | 0.76          | 4.00         | z a        | - |
| 2m                                 | HL S       | 2.0 5.              | 5.2 N                                    | 49.1                 | 0 51.4               | z                     | 55.2  | 56.6    | Z          | 55.5        | 50.3            | 2      | 58.1          | 54.9   | z   | 26.6          | 280          | 2 2        | , .<br>, .    | 1.0          | 2 2        | ~ |
| C1<br>11                           | Hr         | 1.2                 | 9.8<br>N                                 | 20.                  | 1 19.9               | Z                     | 20.7  | 19.8    | 2          | 10 0        | 404             | 2      | 90 4          | 101    | -   | 0.01          |              | :          |               |              |            |   |
| 2nd                                | H.         | 13 1                | 9.9 N                                    | 19.                  | 5 19.8               | z                     | 210   | 19.9    | : >        |             | 0 Q             | : 2    |               | 100    | 2 2 | 7.81          | 9.61         | 2 7        | 20.7          | 19.9         | z          | _ |
| 8<br>1                             | 5<br>H     | 1.1 2               | 1.6 N                                    | 217                  | 8 21.8               | z                     | 21.7  | 21.9    | z          | 21.3        | 21.8            | : 2    | 50.0          | 21 B   | 2 2 | 7.07          | 14.8<br>0 16 | z          | 19.1          | 19.7         | z          | _ |
| She                                | ±          | 2.0 2               | 2.2 N                                    | 31                   | 4 21.9               | ۶                     | 21.7  | 22.3    | z          | 23.7        | 22.3            | z      | 21.5          | 22.2   | : 2 | 2.12          |              | 2 2        |               |              | - 2        |   |
| ₽<br>03                            | 5<br>      | 1.2 3               | 2.4 N                                    | 32.                  | 2 32.2               | z                     | 29.6  | 32.3    | >          | 32.8        | 32.1            | z      | 31.8          | 32.2   | : z | 32.7          |              | : 2        | 7 O 7         | 7.12         | 2 2        | _ |
| R<br>S                             | e<br>t     | 1.8                 | 2.8                                      | 3                    | 3 32.5               | z                     | 31.1  | 33.0    | z          | 32.2        | 33.1            | z      | 33.3          | 33.1   | z   | 31.4          | 32.9         | : z        | 500           | 315          | 2 2        | _ |
| ي <u>م</u><br>2                    |            |                     | 8.0<br>8.0                               | 3                    | 7 65.9               | <b>z</b> :            | 68.0  | 67.1    | 2          | 63.4        | 63.8            | z      | 65.4          | 66.3   | Ż   | 62.1          | 64.5         | z          | 47.5          | 49.0         | : z        |   |
|                                    |            | 2                   | 1 1 1                                    |                      |                      |                       | 8     | 667     | z          | 59.1        | 59.4            | z      | 75.8          | 13.4   | z   | 69.5          | 7.07         | z          | 53.0          | 56.1         | z          |   |
| 10<br>14                           | Hr 43      | 1.1 4               | 3.9 N                                    | 42.6                 | 8 43.9               | z                     | 44.7  | 44.1    | z          | 43.5        | 44.0            | z      | 43.2          | 44.1   | z   | <b>7</b> .64  | 777          | z          | 4 04          | 4 C M        | 3          |   |
| 2                                  | *          | ₹<br>               | 2 :<br>2 :<br>2                          | 4                    | 0 44.6               | z                     | 42.9  | 44.3    | z          | 43.3        | 44.6            | z      | 45.3          | 44.7   | z   | 42.2          | 44.6         | : >        | 414           | 43 d         | : Z        |   |
| D2 1#                              | ส 3<br>    |                     | 8.0<br>8.1                               | 8                    | 2.28                 | ~                     | 28.2  | 30.7    | ~          | 30.0        | 30.6            | z      | 30.3          | 30.7   | z   | 30.5          | 30.9         | z          | 28.7          | 29.6         | : >        | _ |
| 5 5                                | 58<br>     | n 6                 | 22                                       | 162 C                |                      | z:                    | 200   | 31.4    | z          | 30.5        | 31.4            | z      | 30.2          | 31.5   | 7   | 30.8          | 31.4         | z          | 28.8          | 30.0         | · >-       |   |
|                                    | <br>       | 9 00<br>9 00        | 2 Z                                      | 38                   | 9.00<br>9.18         | 2 2                   | 202   |         | ż 2        | 31.4        | <b>39.8</b>     | z 2    | 29.9          | 30.4   | z   | 28.7          | 30.3         | z          | 23.6          | 24.4         | z          | _ |
| SUMMARY                            |            | 2 YES 2             | 6 NO                                     | 3                    | YES 25 A             | 0                     | 5 YE  | S 23 NO |            | 2 YES       | 326 NO          | <br>z  | 21.3<br>2 YEB | 26 NO  | z   | 33.2<br>2 YES | 32.4         | z          | 26.0<br>a vec | 26.2         | z          |   |
| Y = YES = Ν<br><u>Y = NO = M</u> E | IEANS ARI  | E SIGNIF<br>NOT SIC | ICANTLY I                                | DIFFEREN<br>LY DIFFE | VT AT THE<br>RENT AT | 5% LEVEL<br>THE 5% LE | Ē     |         | - °        | st Hr = 12  | 30 - 13:30      | ł      |               |        |     | -             |              |            |               | 2010         | Τ          |   |
|                                    |            |                     |  |                      |                      |                       |       |         | 1          |             |                 |        |               |        |     |               |              |            |               |              |            | _ |
|                                    |            | <u> </u>            | +<br>8                                   |                      | 02                   | ╀                     |       | 6       |            |             |                 | 4      |               | 8      |     | +             | 3            | +          | 5             | T            |            |   |
| 1                                  |            | _                   |  |                      |                      |                       |       |         |            |             |                 | _      |               |        |     | _             |              |            | _             |              |            | _ |
|                                    |            |                     |  |                      |                      |                       |       |         |            | 1           |                 | ]      |               |        |     | ר<br>ן        |              |            | 7             |              |            | _ |
|                                    | õ          |                     |  |                      |                      |                       |       |         |            | 200         |                 |        |               |        |     |               |              |            | 8             | ~            |            |   |
| 1                                  | Г          | L                   |  | ſ                    |                      |                       |       | ا<br>۲  |            | ,           |                 | [      |               |        | ſ   |               |              |            | ]             | L            |            | _ |
|                                    |            | '                   |  | _                    |                      |                       |       | _       |            |             |                 | _      |               |        |     |               |              |            |               |              |            | _ |
|                                    |            | ∎                   |  | ╞                    |                      | - A2 -                |       |         | T C        |             | - <b>18</b>     | 1<br>1 |               | 82     | Ì   | ă۵<br>        | 0            | ₽<br>↓     | Ť             |              |            | _ |
|                                    |            |                     |  |                      |                      |                       |       |         |            |             |                 |        |               | ļ      |     |               |              | -          | -             |              |            | - |

TABLE 5-1 Summary of Travel Time on Test Network (Observed vs. Catibrated)

|          |          | N                |   | 2 2     | z     | ,          | - ;     |          | z    | z    | ,             | - >  |      | ~          |      | Γ,       | - ;    | - :      | 2 2           |          | <u> </u> | Ţ       | T                    |   |          |   |   |          |   |  | - |
|----------|----------|------------------|---|---------|-------|------------|---------|----------|------|------|---------------|------|------|------------|------|----------|--------|----------|---------------|----------|----------|---------|----------------------|---|----------|---|---|----------|---|--|---|
|          |          |                  | _                                       |         |       |            |         |          |      |      |               |      |      |            |      |          |        |          |               |          |          | 5       | 2                    |   |          |   |   |          |   |  |   |
| 10101    |          | CAL              |   |         | 76    |            |         | 52       | 9    | 310  | ç             |      | 2    | 23.3       | 23.7 | 407      |        |          | 6.12<br>8 7 C |          | 10.0     |         | 0                    |   | Т        |   |   |          |   |  |   |
|          |          | OBS              | 1                                       |         | 2.4   | 20.0       |         | 2        | 4-8Z | 28.0 | 48.7          | 15.0 | 271  | 21.3       | 21.6 | 44.0     | 2.4    |          | 20.3          |          |          | 22      |                      |   |          |   |   | 400<br>1 | 2 |  | - |
|          |          | N<br>V           | 2                                       | : 2     |       | z          | : 2     | z :      | z :  | z    | 2             | 2 2  |      | z          | z    | 2        | : z    | 2 2      | : z           |          | 2 3      |         |                      |   |          | 1 |   |          |   | ĮŢ                                     |   |
| VU301    |          | AL.              | c 71                                    |         |       | 8.8        | -       |          |      | 8 4  | 1             | ģ    |      | 7.0        | 88   | 20<br>19 |        |          | 10            |          | 0 N      | UN NO   |                      |   |          |   |   |          |   | ن ــــــــــــــــــــــــــــــــــــ |   |
|          |          | 85 (             | 5                                       |         |       | 1          |         |          |      |      |               |      |      | •          | 8    |          |        |          | 2             | с<br>г   | .α<br>   | N VES   |                      |   | T        |   |   | 306      |   |  |   |
| $\ $     | -        | 0<br>Z           | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | -<br>-  | 1     | 25         |         |          | 58   | 8    | 33            |      | 1    | 4          | 8    | 3        | 5      |          | 28            | 2        | 1.5      |         |                      |   |          |   |   |          |   |  |   |
| SDAV     |          |                  | 2                                       | : z     |       | Z          | 2       | : 1      | 2 2  |      | Z             | : z  |      | Z          | Z    | 7        | z      | : z      | Z             | 2        | 2        |         |                      |   | Ē        |   |   |          |   |  |   |
| WEDN     |          | 8                | 16.8                                    | 17.2    |       | 25.9       | 7.57    | 2.5      | 20.6 | 220  | 26.2          | 30.6 |      | 9.10<br>1  | 5    | 22.2     | 23.6   | 30.6     | 30.8          | 24 A     | 5        | S 15 NC |                      |   |          |   |   |          |   |  |   |
|          |          | SBO              | 15.9                                    | 16.6    |       | 25.3       | 23.8    |          | 1.12 |      | 24.8          | 28.9 |      | 33.7       | 38.9 | 18.7     | 21.2   | 31.2     | 3             | 20.0     | 20.4     | 1 YE    |                      |   |          |   |   |          |   | - 82                                   |   |
|          |          | z                | z                                       | N       |       | z          | >       | z        | : 2  | ł    | z             | N    |      | <b>z</b> : |      | >        | z      | z        | z             |          | z        |         |                      |   | Ť        |   |   |          |   |  |   |
| ESDAY    |          | N.               | 16.8                                    | 17.7    |       | <b>0.0</b> | 25.7    | 19.7     | 8.8  |      | 3.4           | 8.3  |      |            |      | 4.6      | 5.2    | 4.4      | 1.8           | 1.9      | 1.7      | 4 NO    | - 13:30              |   |          |   |   |          |   |  |   |
| P        |          | 3                |   | . 9.6   |       | 8          | 4       | 8        | 1.0  |      | 5             | -    |      | 5          | 2    | 4        | 5      | 8        | 5             | 2        | 7 2      | 2 YES   | r= 12:30<br>F= 13:30 |   |          |   |   |          |   | _                                      |   |
| ┡        |          |                  | ÷                                       | Ĭ       |       | 3          | 2       | 8        | 6    | -    | 8             | 27   |      | 3 -        | 1    | 3        | 2      | 3        | 8             | 8        | 19       |         | 1st Hr<br>2nd H      |   | ы<br>Ш   |   |   |          |   |  |   |
| <u>ک</u> | ,        |                  | Z                                       | Z       |       | z          | z       | z        | : Z  |      | Z             | Z    | :    | 2 3        | 1    | Z        | z      | z        | Z             | Z        | N        | _       |                      |   | 1        |   |   |          |   |  |   |
| MOND     | đ        |                  | 17.1                                    | 11      |       | 26.6       | 25.6    | 39.3     | 38.6 |      | 29.0          | 27.4 | 5    | 1.14       |      | 26.1     | 23.2   | 31.8     | 31.3          | 23.3     | 21.5     | S 16 N  |                      |   |          |   |   |          |   |  |   |
|          | ą        | 8                | 18.9                                    | 20.7    |       | 9.CZ       | 26.6    | 37.8     | 40.3 |      | 26.9          | 28.3 |      | 8.9C       |      | 24.5     | 21.2   | 33.3     | 32.4          | 20.6     | 202      | 0 YE    | B                    |   |          |   |   |          |   | <b>6</b> 0                             |   |
| Π        | 4        |                  | z                                       | z       | ;     | -          | z       | z        | z    |      | z             | z    |      | . 2        |      | 7        | z      | z        | z             | z        | z        | 1       | EVEL<br>S% LEV       |   | t        |   |   | 80       |   | _                                      |   |
| NDAY     | ,<br>,   |                  | 6.8                                     | 7.1     |       |            | 5.6     | 0.0      | 7.4  |      | 8.1           | 46   |      | 10         |      | 0,4      | 23     | 0        | 13            | 5        | 2        | 4 NO    | HE 5% (<br>VI THE (  |   |          |   |   |          |   |  |   |
| ß        | g        |                  | 4                                       |         | •     |            | د،<br>ت | 4        | 3    |      | ~             | 4    | 4    | ie<br>19   |      | 6        | N<br>8 | é)<br>BO | 2             | ю́<br>в  | 4        | YES 1   | VT AT T              |   | <br>L    |   |   |          |   |  |   |
|          | 2<br>    |                  | \$                                      | ิส<br>- | š<br> | 5          | 8       | 42       | 8    |      | 2.            | 8    |      | 8          |      | 2        | R      | 2        | 7             | <b>6</b> | 6        | _       | r feren<br>L diffe   |   | Ī        |   |   |          | i |  |   |
| λYC      | - X      |                  | Z                                       | z       | 3     | 2 3        | z       | z        | z    |      | 2             | z    | 2    | z          |      | 2 :      | -      | Z        | Z             | z        | z        |         | VTLY DI              |   |          |   |   |          |   | ×                                      |   |
| SATURI   | <b>N</b> |                  | 17.1                                    | 114     | 26.0  |            | 20.4    | 39.2     | 39.8 | :    | 28.2          | 26.6 | 17 e | 36.8       |      | 23.8     | 73.0   | 30.8     | 31.8          | 21.5     | 22.0     | S 15 NC | SIGNE                | - | <u>*</u> |   | ך | o        |   |  |   |
|          | ORS      |                  | 18.2                                    | 18.0    | 26.0  |            | 23.4    | 41.1     | 386  |      | 2 <b>6</b> .8 | 23.5 | 35.4 | 34.6       |      | 22.5     | 2      | 9.9      | 29.4          | 19.8     | 19.9     | 1 YE    | RE NOT               |   |          |   | - | ₽        |   |  |   |
| si<br>S  |          | $\left  \right $ | Ŧ                                       | 7       | ŧ     | 5 3        |         | Ŧ        | Ħ    |      | Ì             | H +  | ÷    | H          |      | ž        | Ì      | Ŧ        | ╞             | Ť        | H        |         | EANSA                |   |          |   |   |          |   |  |   |
| ERVED    | IBRATED  |                  | A 1.                                    | ŝ       | 1     | : i        | 5       | 32       | ž    |      |               | Ā    |      | 200        |      | te<br>te | Ĕ.     | # ;<br>; | Ř             | 1        | E.       | MARY    | Ves = A<br>NO = M    |   |          |   | I |          | 1 |  |   |
| В<br>В   | 5        |                  | <u> </u>                                |         |       | _          |         | <u>ت</u> |      |      | _             |      |      |            |      | ш        |        | ц        |               | -        |          | Ŋ,      | = N                  |   |          |   |   |          |   |  | ł |

TABLE 5-2 Summary of Travel Time on Validation Network (Ob

|      | λ        |       |        | • >   | · 2         | z   | Z         | N     | ;      | - 2        | 2 >         | - >          | 2        | : z | z             | Z    | 1      | : Z      | :>           | · Z    | : z        | : z        | z            | Z    | 2      | : z   | >          | z                 | z          | z        |                          | Ī |    |   |        |     | - <del></del> |
|------|----------|-------|--------|-------|-------------|-----|-----------|-------|--------|------------|-------------|--------------|----------|-----|---------------|------|--------|----------|--------------|--------|------------|------------|--------------|------|--------|-------|------------|-------------------|------------|----------|--------------------------|---|----|---|--------|-----|---------------|
|      | FRIDA    | č     | 10     | 000   | , <b>4</b>  | 1.9 | 30.0      | 32.9  | ;      |            | - 14<br>0 4 | 9 <b>4</b>   |          | 24  | 28.1          | 25.6 |        | 4        |              | : =    | 2.8        | 23         | 33.0         | 38.2 | 6.9    | 6.5   | 2.8        | 3.2               | 16.3       | 18.2     |                          |   | Ţ  |   |        | 300 | L             |
|      |          |       | 84     | 5     | 1           | 0   | 26.5      | 30.6  |        | 8 9<br>7 7 |             | 2.6          | <b>•</b> | 20  | 30.0          | 21.6 |        |          |              | 2      | 6          | 50         | 29.9         | 35.4 | 4.2    | 5     | 0.2        | 23                | 15.7       | 18.1     |                          |   | 5  | _ | ]      | ••• | Γ             |
|      | SDAY     | ~     | Z      | z     | z           | z   | z         | z     | 2      | 2 2        | : >         | ·z           | z        | ż   | z             | z    | 2      | : z      | z            | z      | z          | z          | 7            | z    | z      | Ż     | z          | z                 | z          | z        |                          |   | *  | - | ר<br>ר |     | L<br>F        |
|      | THURS    | Ω.    |        | 13.4  | 2.8         | 2.9 | 40.4      | 45.0  |        |            | 46          | 2.6          | 2.8      | 2.9 | 33.2          | 43.8 | 5.6    | 3.6      | 2.5          | 2.8    | 3.5        | 3.6        | 48.5         | 54.8 | 7.5    | 78    | 4.0        | 4.6               | 222        | ES 28 N  |                          |   | 5  |   |        |     |               |
| (nou |          |       | 12.4   | 13.0  | -2.8        | 0.4 | 43.4      | 44.8  | 3 6    | 34         | 60          | 9.1          | 24       | 2.3 | 31.8          | 42.1 | 3.2    | 4        | 2.4          | 2.4    | 3.9        | 2.5        | 44.5         | 51.8 | 2.5    | 5.9   | 4          | 4.2               | 20.7       | <u> </u> |                          |   |    |   | ]      |     |               |
|      | ESDAY    | 4 1 X | ¥      | z     | z           | z   | z         | Я     | >      | ·z         | : 2         | z            | z        | z   | Ż             | z    | Z      | z        | z            | z      | z          | z          | 2            | z    | z      | z     | z          | ≻ :               | <b>z</b> 2 | 2        |                          |   | 3  |   |        |     |               |
|      | WEDN     | CAL   | 12.6   | 12.9  | 2.7         | 2.7 | 41.2      | 44.3  | 17     | 3.8        | 2.3         | 2.3          | 2.8      | 2.9 | 36.4          | 40.0 | 3.5    | 3.6      | 2.4          | 2.8    | 3.0        | 3.8        | 6.95<br>1    | 51.4 | 7.4    | 7.9   | 3.9        | 4.7               | 22.4       | ES 25 NK |                          |   |    |   |        |     |               |
|      |          | N OBS | 12.0   | 12.3  | 3.6         | 31  | 40.7      | 407   | 2.4    | 2.8        | 1.6         | 1.5          | 3.6      | 2.4 | 40.5          | 7    | 4.0    | 4.9      | 1.7          | 2.3    | 3.0        | 4          | 47.7         | 28   | 6.9    | 0.0   | 3.8        | 3.6               | 8.12       | 3 1      |                          |   |    |   |        |     | L             |
|      | AY       | 4 / X | z      | z     | z           | z   | Z         |       | z      | z          | z           | ۲            | z        | z   | z             |      | z      | z        | Ż            | z      | z          | z          | ≻ :          |      | z      | z     | Z          | z ;               | ⊢ z        |          | 9 6                      |   | 04 | _ | ]      |     |               |
|      | TUESD    | G     | 12.3   | 13.6  | 2.5         | 2.8 | 40.4      | 44.0  | 3.5    | 3.8        | 2.2         | 2.5          | 2.8      | 3.0 | 1.55          |      | 3.5    | 3.7      | 2.3          | 2.8    | 2.9        | 3.8        | 47.9         | 23.4 | 7.2    | 2.9   | 3.7        | 4 8<br>9 7<br>9 8 | 872        | ES 24 NC | 230-133                  |   | •  |   | ]      | 0   | L             |
|      |          | 088   | 10.7   | 13.1  | 1.6         | 5.4 | 40.0<br>9 | 43.0  | 4.2    | 2.2        | 7           | 1.4          | 5.6      | 0.4 | 1.86          |      | 3.8    | 5.2      | 2.1          | 4      | 3.8        | 3.3        | 45.8         | 610  | 7.2    | 2.0   | 3.5        | 4                 | 6 P.C      | 4 11     | 1st Hr = 1<br>2nd Hr = 1 |   |    | _ | 1      | 20  | F             |
|      | >        | Y 7 N | z      | z     | z           | z:  | z         | z     | ۲      | z          | z           | z            | z        | 7   | 2 2           |      | Z      | ٢        | z            | z      | ۲          | z          | z            | 2    | 2      | z     | z          | z 2               | e z        |          | ſ                        |   | 5  |   |        |     |               |
|      | MONDA    | CAL   | 12.9   | 13.4  | 2.8         | 2.8 | 43.5      | 1410  | 3.7    | 3.8        | 2.4         | 2.4          | 2.8      | 2.9 | 30.1<br>4 7 F |      | 3.5    | 3.7      | 2.5          | 2.8    | <b>.</b> . | 3.8        | 51.1         | 2.00 | 7.4    | 7.8   |            | 4.6               | 242        | S 24 NC  |                          |   | Ī  |   |        |     | Γ             |
|      |          | OBS   | 12.3   | 12.8  | 50          | 5   | 8.14      |       | 2.0    | 3.9        | 3.6         | 3.3          | 1.7      | 77  | <b>11.7</b>   |      | 4.6    | 5.0      | 2.5          | 2.5    | 0.7        | 5.2        | 8            |      | 8.4    | 4.5   | 9 (<br>N   |                   | 24.8       | 4 YE     | VEL                      |   |    |   |        |     |               |
|      | •        | X V N | z      | z     | z           | z : | 2 2       |       | z      | ۲          | ۲           | z            | z        | z   | <b>z</b> 2    |      | z      | z        | z            | z      | <b>z</b> : | z          | ≻ 2          |      | z      | z     | z          | 2 2               | : z        |          | % LEVEL<br>1E 5% LE      |   | +  |   |        |     |               |
|      | SUNUS    | G     | 12.7   | 13.5  | 5.0         |     | 8.09      | 10.01 | 3.7    | 3.7        | 2.3         | 2.2          | 5.0      | 2.8 |               |      | 3.6    | 3.5      | 2.4          | 5.2    | 2.9        | <u>6.6</u> |              |      | 7.2    | 7.8   | 8 9<br>9 9 | 33.4              | 23.8       | S 25 NO  | AT THE 5<br>NI AL TH     |   | 2  |   |        |     |               |
|      |          | SBO   | 12.7   | 13.3  | 22          | 5   | 2.97      |       | 3.9    | 2.4        | 1.2         | 50           | 9.9      | 5.1 |               |      | 4.0    | 3.5      | 2.6          | 5.5    |            | 4.6        | 1997<br>1977 |      | 6.3    | 1.2   | 2.5        | 20.5              | 23.0       | 3 YE     | DIFFERE                  |   | 6  |   |        |     | L             |
|      | I        | N / X | z      | z     | <b>z</b> :  | 2 2 | 2 2       | ſ     | 7      | 7          | z           | z            | Z        | z ; | ≻ z           |      | z      | z        | 2            | z      | 2 :        | z:         | ZZ           |      | Z      | Z 2   | 2 2        | 2 2               | : z        |          | UTLY DIFF                |   | ł  |   |        |     |               |
|      | SAI UR   | CAL   | 1.1    | 13.4  | in d<br>N d |     |           |       | 3.7    | 3.7        | 2.3         | 20           | 5.8<br>7 | 30  | 1.14          |      | 3.6    | 36       | 5            | 8.7    |            | 50         | 102          |      | 2      | 0. e  |            | 21.8              | 23.8       | S 25 NO  | SNIFICAN<br>SIGNED       |   | 8  |   |        |     |               |
|      |          | OBS   | 1.5    | 13.2  |             |     | 1.1       |       | 2.3    | 6          | <b>9</b>    | <del>,</del> | <b>9</b> | 2   | 8.64          |      | 3.1    | 42       | <b>6</b> , 6 |        |            | 2.5        | 0.78         |      | 8.8    | 0 F   | - 0 V      | 22.0              | 23.9       | 3 YE     | S ARE SI(<br>ARE NO)     |   | *  | - |        | ŝ   | L             |
| -    | TED VS.  | 2     | 1at Hr | H Puz | H H         |     |           |       | 1st Hr | 2nd H      | 1st Hr      | 2 dH         | Ĩ        | Ť : | H H           |      | 1st Hr | The Part | 1            | ZINGHE | IS H       | HDUZ       | 2nd Hr       |      | 1st Hr | TH DI |            |                   | 2nd Hr     | 2        | = MEAN                   |   |    |   |        |     | Γ             |
| 1000 | CALIBRA' |       | ł      |       | A2          | 54  | 2         |       | 81     | ;          | 83          | ŝ            | 8        | 2   | <b>P</b>      |      | 5      | 8        | 3            | 8      | 3          | 2          | 3            |      | 5      | 2     | 20         | 03                |            | SUMMA    | V = YES                  |   |    |   |        |     |               |

TABLE 5-3 Summary of Delay Time on Test Network ( Obse

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|-------------|-------|----------|-------------|-------------|--------|--------|---------|--------|------|--------|--------|--------|--------|------|--------|-------|------------------|--------|----------|---------------|---------|---------|----------------------------|---|------------|---|---|----|---|--------|--|
|             |       | X / N    |             | Z           | z      | >      | ~       | z      | z    | :      | ~ >    |        | >      | γ    |        | >     | 7                | z      | z        | 7             | >       | ·       |                            |   |            |   |   |    |   |        |  |
| CONDAU      |       | CAL      |             | 7.3         | 7.2    | 10.1   | 10.3    | 10.8   | 11.1 |        | 5 C    |        | 10.6   | 10.9 |        | 6.8   | 6.0              | 8.7    | 8.8      | 1.7           | 7.0     | S B NO  |                            |   | Ŧ          |   |   |    |   |        |  |
|             |       | OBS      | 1           | 9.9<br>9.0  | 6.5    | 8.1    | 7.1     | 8.8    | 8.4  | 4      | 3.2    |        | 8.7    | 9.0  |        | 4.7   | 2.8              | 6.7    | 10.7     | 6.3           | 4.3     | 10YE    |                            |   |            |   |   | Ę  | Ş |        |  |
|             |       | X / N    |             | z :         | z      | z      | z       | z      | z    | 2      | z      |        | z      | z    | ;      | z     | z                | 2 :    | z        | z             | z       |         |                            |   |            |   |   |    |   |        |  |
| THURSO      |       | CAL      | •           | 200         | 6.9    | 13.8   | 13.1    | 19.2   | 19.8 |        | 17.0   |        | 34.3   | 28.0 |        |       | 9.5              | 13.2   | R.L      | 14.9          | 12.8    | 16 NO   |                            |   | -          |   |   | 8  | 3 |        |  |
|             |       | OBS      | •           | P. c<br>E P | 3      | 12.8   | 14.1    | 17.8   | 121  | 20 G   | 14.6   |        | 30.4   | 24.2 |        | 5     | 2                | 0.0    | N.       | 12.8          | 11.8    | 0 YES   |                            |   |            |   |   | C. | , |        |  |
| SDAY 1      |       | N / Y    | 2           | 2 2         | 2      | z      | z       | z      | z    | 2      | : z    | ;      | z      | z    | >      | - :   | z 2              | 2 2    | =        | z             | z       |         | -                          |   | Ш<br>Ш     |   |   |    |   |        |  |
| WEDNE       |       | GA       | 6<br>8      | 5 G         | 1.4    | 12.9   | 12.7    | 17.8   | 19.8 | 13.4   | 17.8   | ł      | 2.22   | 797  | • •    |       |                  | ; ;    | ~        | 12.4          | 12.3    | 5 15 NO |                            |   |            |   |   |    |   |        |  |
|             |       | OBS      | 7.6         |             |        | 12.4   | 10.8    | 19.7   | 18.2 | 12.1   | 16.3   |        | 1.12   | 50.3 | 2      | , u   |                  | 1      | 2.11     | 11.2          | 11:5    | 1 YE    |                            |   |            |   |   |    |   | - 82 - |  |
| \\<br>\\    |       | <u> </u> | Z           | : z         | :      | z      | > :     | z :    | z    | Z      | z      | a      | z      |      | >      | • 2   | 2 2              | : z    |          | 2 2           | z       |         |                            | - | Ť          |   |   |    |   |        |  |
| TUESD/      |       | CAL      | 8.3         | 8.2         |        | 13.0   | 12.7    | 19.9   | 18.0 | 20.6   | 15.5   | 6 00   | 787    | 10.1 | 10.7   | : :   | - <del>-</del> - | 13.0   |          | 13.0          | 871     | S 14 NO | 30 - 13 30<br>30 - 14 30   |   |            |   |   |    |   |        |  |
|             | 000   | OBS      | <b>9</b> .6 | 11.2        |        | 0.21   | 0.5     |        | 20   | 20.4   | 14.4   | 36.6   | 284    |      | 1.7    | 104   | 14.2             | 11.5   |          | 14.4          | R'DL    | ZYE     | 1et Hr = 12<br>2nd Hr = 13 |   | E2         |   |   |    |   |        |  |
| <b>&gt;</b> |       |          | z           | Z           | 2      | 2 3    | z :     | Z 2    |      | z      | z      | 2      | : z    |      | z      | z     | z                | z      |          | 2 2           | z       |         |                            |   |            |   |   |    |   |        |  |
| MONDA       | NV.   | Z,       | 8.6         | 8.6         | 9 2 5  |        | 1.1     | 19.0   | 2.2  | 16.2   | 14.6   | 29.4   | 28.1   |      | 12.2   | 9.3   | 13.0             | 12.4   |          | 4.41<br>A.C.  | 10.0    | 201     |                            |   |            |   |   |    | ļ |        |  |
|             | ä     | 800      | 10.5        | 12.3        | 4 C B  |        | 2       | 20.8   | 2    | 14.2   | 13.6   | 27.3   | 29.4   |      | 10.8   | 7.5   | 14.7             | 13.8   | 1        | ) :<br>;<br>; | 2       | 2       | H                          |   |            |   |   |    |   |        |  |
|             | N ~ > |          | z           | Z           | >      |        | 2 2     | : z    |      | z      | z      | z      | z      |      | 7      | z     | z                | Z      | ;        | 2 2           | -       | I EVEI  | 5% LEV                     | - |            | · | ר | 20 |   |        |  |
| SUNDA       | CAL   |          | 8.3         | 9.6         | 12.6   | a ct   | 0.00    | 17.6   |      | 16.3   | 11.8   | 30.7   | 22.1   |      | 10.1   | 8.4   | 12.2             | 11.5   |          | 11.1          | S 14 NO | THE 54  | IT AT THE                  |   |            |   |   |    |   |        |  |
|             | OBS   | 2        | 8.0         | 11.7        | 8.8    | ţ0     | 23.1    | 16.8   |      | 14.6   | 1.8    | 30.9   | 19.8   |      | 7.9    | 7.3   | 13.2             | 12.6   |          | 10.6          | 3 YE    | FRENT A | DIFFEREN                   | 1 | <b>.</b>   |   |   |    |   |        |  |
| AV<br>V     | N / Х |          | z           | z           | z      | z      | : Z     | z      |      | 2 :    | z      | z      | Z      |      | z      | 7     | z                | z      | a        | : z           |         |         | ANTLY                      |   |            |   |   |    |   | <      |  |
| SATUR       | CAL   |          | <b>8.6</b>  | 8.8         | 13.0   | 12.4   | 19.4    | 20.0   |      | 16.4   | 13.8   | 26.0   | 24.1   |      | 10.0   | 9.2   | 12.0             | 12.9   | a ( †    | 13.1          | S 15 NO | NIFICAN | SIGNIFK                    | 1 | <b>L</b> . |   | J | 8  |   |        |  |
|             | OBS   |          | 8.6         | 9.6         | 12.2   | 10.5   | 21.6    | 19,1   |      | 14.2   | 10.0   | 22.8   | 22.0   |      | 8.8    | 6.3   | 12.0             | 10.8   |          | Ŧ             | 1 1     | ARE SIG | ARE NOT                    |   | -          |   | 1 | ¥  |   |        |  |
| ED VS.      |       |          | 1et Hr      | 2nd Hr      | 1st Hr | 2nd Hr | 1 at Hr | 2nd Hr |      | 1st Hr | JH DUX | 1at Hr | 2nd Hr |      | fat Hr | 2nd H | tet Hr           | 2nd Hr | 1        | 2nd Hr        | 2       | = MEANS | - MEANS                    |   |            |   |   |    |   |        |  |
| CALIBRA     |       |          | ۲           |             | 6      |        | 82      |        |      | v      |        | ٥      |        |      | Ē      | 1     | EZ               |        | <u>u</u> |               | SUMMA   | Y = YES | N=NO                       |   |            |   |   |    |   |        |  |

|             |          |              |              |             |               |              |               |                       |                |        | 01 Liavei     |                                    | DATINE 120    | IX (CDSB       | Ved vs. L    | efeur  |              |              |               |                      |               |  |
|-------------|----------|--------------|--------------|-------------|---------------|--------------|---------------|-----------------------|----------------|--------|---------------|------------------------------------|---------------|----------------|--------------|--|--------------|--------------|---------------|----------------------|---------------|--|
| OBSERVED V  | <u>ອ</u> | S            | ATURDA       |             |               | SUNDAY       |               |                       | MONDAY         |        |               | TUESDAY                            |               |                | VEDNES       | ΝA   |              | THURSD/      | ٨             |                      | FRIDAY        |  |
|             |          | OBS          | DEF          | N / X       | OBS           | DEF          | X / N         | OBS                   | DEF            | X / N  | OBS           | DEF                                | Y / N         | OBS            | DEF          | χ / N  | SBO          | DEF          | N / Y         | SHO                  |               | N / /  |
| A1 1st      |          | 36.4         | 40.1         | ~           | 36.6          | 39.7         | ~             | 36.1                  | 39.9           | >      | 34.6          | 20 K                               | >             | 98.0           | 20.7         | ,  |              |              |               |                      |               |  |
| 2nd         | ĩ        | 37.0         | 40.2         | 7           | 37.1          | 37.1         | · >-          | 36.7                  | 40.2<br>2      | • >    | 37.0          | 40.2<br>2<br>2<br>2<br>2<br>2<br>2 | - >           | 98.9<br>38.7   | 38.7         | - >  | 26.3<br>2    | 4.04<br>4.04 | ≻ >           | 30.3                 | 36.9          | ≻ :  |
| A2 1#       |          | 36.9         | 45.6         | 7           | 37.4          | 46.5         | 7             | 36.0                  | 46.5           | 7      | 35.6          | 45.4                               | · >-          | 37.6           | 46.6         | - >  | 31.2         | 46.7         | - >           | 21.0                 | 9.75          | ≻ >  |
| 24q         | <br>Ì    | 38.4         | 48.0<br>1.0  | > :         | 37.1          | 45.8         | 7             | 37.5                  | 48.1           | >      | 36.4          | 48.0                               | ۲             | 37.0           | 45.6         | ~  | 34.4         | 52.1         | • >           | 2                    | 448           | • >  |
| 8<br>8<br>9 | ± 1      | 52.1<br>54.4 | 67.4<br>80 a | > >         | <b>61.8</b>   | 56.9<br>54.9 | > >           | 83.8                  | 67.3           | ≻ ;    | 62.0          | 64.9                               | ~             | 52.7           | 66.0         | 7  | 66.4         | 68.0         | z             | 38.6                 | 47.4          | - >-   |
| 114         |          |              | 0.05         | ł           | 20.1          | 716          |               | 8                     | 80.0           | -      | 0.00          | 61.5                               | +<br>>        | 52.7           | 60.0         | 7  | 56.3         | 73.1         | >             | 42.5                 | 52.1          | >  |
| B1 1st      |          | 20.2         | 24.6         | 7           | 21.8          | 24.5         | ۲             | 19.9                  | 24.6           | 7      | 22.1          | 24.6                               | z             | 20.3           | 24.6         | >  | 20.4         | 7.40         | >             | 0                    |               | ,  |
| 2nd         | Ī        | 19.8         | 24.8         | ≻           | 20.3          | 24.6         | ۲             | 21.8                  | 24.6           | ۲      | 20.0          | 24.7                               | : >           | 20.6           | 24.6         | • >  | 21           | 24.8         | - >           | 0.0<br>7<br>8        | 0.42<br>0.42  | ~ >  |
| B2 1st      | ± :      | 21.1         | 26.3         | ≻ :         | 20.4          | 26.3         | 7             | 22.8                  | 26.3           | z      | 20.2          | 26.3                               | ~             | 20.8           | 26.3         | • >  | 20.0         | 26.6         | - >           | 18.9                 | 26.7          | - >  |
| R3 2md      |          | 20.9         | 28.5         | ≻>          | 21.1          | 26.5         | >>            | 22.4                  | 26.4           | ≻ ;    | 20.6          | 26.5                               | ~ :           | 20.6           | 26.5         | ~  | 20.8         | 26.6         | ~             | 22.9                 | 26.0          | • <b>&gt;</b>                                |
| 2002        |          |              | 0 I 4        | - >         | 8.90<br>1 C C | 4 F          | ->            | 32.2                  |                | > >    | 33.2          |                                    | > :           | <b>34.1</b>    | 41.2         | > :  | 33.0         | 41.3         | ≻             | 32.6                 | 40.7          | ۲  |
| B4 teri     |          | 10.9         | 69.7         | - >         | 48.2          | 58.2         | - >           | 55.6                  |                | - >    | R: 75         | 41.3<br>Kg 7                       | ≻ >           | 32.8<br>84 2   | 41.3         | > >  | 32.9         | 41.3         | >:            | 32.5                 | 40.9          | 7  |
| 2nd         |          | 55.6         | 64.9         | >           | 49.0          | 61.8         | >             | 55.2                  | 62.0           | • >    | 56.5          | 62.8                               | - >           | 58.1           | <b>6</b> 2.9 | - z  | 56.6         | 66.3<br>66.3 | <b>&gt;</b> > | <b>44</b> .0<br>35.5 | 61.5<br>49.1  | <b>~                                    </b> |
| C1 1#1      |          | 19.2         | 23.4         | ~           | 20.1          | 23.4         | ~             | 20.7                  | 23.3           | ~      | 19.9          | 23.3                               | <b>`</b>      | 20.1           | 23.3         | >  | 10.0         | 22.6         | ,             |                      |               | . ,  |
| 2md         |          | 20.3         | 23.5         | ~           | 19.5          | 23.3         | ~             | 21.0                  | 23.6           | 7      | 21.2          | 23.6                               | z             | 21.0           | 3.8          | - >  | 1 00         | 1.02         | - >           | 1.07                 | 2. S          | ► >  |
| C2 1#1      | +        | 21.1         | 26.7         | 7           | 21.8          | 26.7         | 7             | 21.7                  | 26.7           | 7      | 21.3          | 26.6                               | . >           | 20.9           | 26.6         | - <b>&gt;</b> -                              | 21.6         | 28.8         | - >           | 20.1                 | 28.5          | - >  |
| 2nd         | <br>     | 200          | 27.1         | ≻ :         | 21.4          | 26.9         | ≻             | 21.7                  | 27.1           | 7      | 23.7          | 27.2                               | 7             | 21.5           | 27.2         | ~  | 21.7         | 27.0         | • >           | 20.2                 | 25.9          | - >  |
| 3           | <br>+ +  | 21.2         | 38.8         | > >         | 32.2          | 39.6         | > ;           | 29.6                  | 39.7           | ≻ :    | 32.8          | 39.6                               | >             | 31.9           | 39.7         | >  | 32.7         | 39.9         | ~             | 30.7                 | 39.4          | • >  |
|             |          | 0.1          | 13 U         | - >         | 27.2          | 0.04         | <br>≻ >       | 31.1                  | 40.0<br>0.0    | ≻ ;    | 32.2          | 40.4<br>7.9                        | <b>&gt;</b> : | 33.3           | 40.5         | ~  | 31.4         | 40.3         | >             | 30.8                 | 38.8          | ۲  |
| 2nd         | He -     | 89           | 74.B         | - >         | 20.B          | 78.4         | - 7           | 68.1                  | 74.5           | z >    | 63.4          | 9. L2                              | > >           | 05.4<br>75 8   | 71.9         | > 2  | 62.1<br>80 E | <b>69.</b> 8 | > >           | 47.5                 | 6.69          | > :  |
| į           |          | ļ            |              | ;           |               |              | ;             |                       |                |        |               |                                    |               |                |              |  |              | 08           |               | 1.66                 | 818           |  |
| 2nd         | <br>     | 1.23         | 52.7<br>52.7 | ► ≻         | 87.8<br>7 1 1 | 62.2<br>52 0 | <b>&gt;</b> > | 1<br>1<br>1<br>1<br>1 | 62.9<br>52.0   | > >    | 83.6<br>8.5   | 62.6<br>52.6                       | > >           | <b>4</b> 3.2   | <b>52.7</b>  | > ;  | 43.4         | 62.8         | >             | 40.5                 | 61.4          | ~  |
| D2 (#)      |          | 0.2          | 37.4         | ~ >         | 29.2          | 37.6         | - >-          | 28.2                  | 37.9           | - >    | 30.0          | 37.6                               | - <b>-</b>    | 80.3           | 87.4<br>87.4 | <b>~                                    </b> | 42.2<br>80 8 | 52.8<br>37 8 | ≻ >           | 41.4                 | 51.7          | ≻ >  |
| 2nd         |          | 31.4         | 38.2         | <b>&gt;</b> | 29.8          | 36.3         | ۲             | 30.7                  | 38.2           | 7      | 30.5          | 36.4                               | • ≻           | 30.2           | 36.7         | - >-   | 9.8<br>8.00  | 36.1         | - >           | 28.8                 | 0.00<br>2.9 E | - >  |
| 141         | <br>     | 8.82<br>1    | 32.4<br>32.4 | <b>≻</b> >  | 30.2          | 32.1         | ≻ >           | 29.4                  | 32.7           | ≻ :    | 31.4          | 31.3                               | Z             | 29.9           | 32.7         | *  | 28.7         | 32.8         | ~             | 23.6                 | 27.0          | • >  |
| SUMMARY     |          | 28 YES       | ONO 1        | -           | 28 YE         | S ONO        | -             | 32./<br>25 YE         | 33.6<br>S 3 NO | z      | 32.2<br>25 YE | 34.8<br>S 3 NO                     | >             | 31.3<br>28 VES | 35.8<br>2 NO | >  | 33.2         | 33.9         | z             | 26.0                 | 29.0          | 7  |
| Y = YES = M | ANS AR   | RE SIGN      | FICANTL      | Y DIFFE     | RENT AT       | THE 5%       | LEVEL         |                       |                | 1      | et Hr = 12:   | 30 13:30                           | -             | 50 IEI         | 2            |  | 21 07        | DN 7 C       |               | 28 75                | S ONO         |  |
| N = NO = ME | ANS AR   | E NOT S      | IGNIFICA     | NTLYD       | IFFEREN       | I AT THE     | 5% LEV        | L.                    |                |        | nd Hr = 13.   | 30-14:30                           |               |                |              |  |              |              |               |                      |               |  |
|             |          | Ŧ            | - B3         |             | 8             |              | ł             |                       | 2              |        |               | 1                                  |               |                | 8            |  | 3            | ç            | 1             | 2                    |               |  |
|             |          |              | -            |             | 5             | -            |               |                       | כ              | _      |               |                                    | t.            | ,              | 3            |  |              | 5            |               | 5                    | <b>T</b> -    | -  |
| 1           |          | -            | ]            |             |               |              |               |                       |                |        |               |                                    | 7             |                |              |  | <br>         |              |               |                      |               |  |
|             | 10<br>1  | ~            |              |             |               |              |               |                       |                |        | 200           |                                    |               |                |              |  |              |              |               | 8                    | 。             |  |
|             |          | 1            |              |             |               |              |               |                       |                |        |               |                                    |               |                |              |  |              |              |               |                      | ł             |  |
| I           | ┎╌╽      |              | A1           |             |               |              |               |                       |                |        | <b></b> .     |                                    |               |                |              |  |              |              |               | Γ                    |               |  |
|             | -        | :            | E            |             | _             |              | 2             |                       | Ĺ              | 2<br>2 |               | 8                                  | ⊥<br>↑        |                | 82           |  |              | Ī            |               | <b>†</b>             |               |  |
|             |          |              |              |             |               |              |               |                       |                |        |               |                                    |               |                |              |  |              |              |               |                      |               |  |

TABLE 5-5 Summary of Travel Time on Test Network (O

| OBS DEF Y / N OBS DEF Y / N OB                            | -          |
|---|------------|
| 12.3 10.1 Y 10.7 9.8 N 12.                                |            |
| 12.8 10.5 Y 13.1 10.5 Y 12.<br>20 33 N 18 32 V 20         |            |
| 3.5 3.9 N 2.4 3.8 Y 3.1                                   |            |
| 1.8 42.4 N 40.0 40.0 N 40.                                | 4          |
| 4.1 45.9 N 43.0 46.6 N 40.                                | •          |
| 2.0 3.4 N 4.2 3.3 N 2.4                                   |            |
| 3.9 3.5 N 2.2 3.5 N 2.6                                   |            |
| 3.6 2.6 N ] 1.1 2.5 N ] 1.4                               |            |
| 3.3 2.6 N 1.4 2.7 Y 1.                                    | ••••       |
| ·/ 9.4 N 2.6 3.2 N 3.4                                    |            |
| 1.7 44.1 N 36.4 473 N 2.4                                 |            |
| 1.3 44.7 Y 41.6 45.5 N 44.                                | 4          |
| 6 3.3 N 3.8 3.3 N 4.0                                     | 4          |
| 50 3.6 Y 5.2 3.6 N 4.9                                    |            |
| .6 2.8 N 2.1 2.8 N 1.7                                    | 2          |
| 5 3.3 N 4.4 3.3 N 2.3                                     | N          |
| 7 3.8 Y 3.9 3.8 N 3.0                                     | Ó          |
| 2 4.6 N 3.3 4.7 N 4.4                                     | 2          |
| 4. 548 N 546 01.8 Y 47.                                   | 8 8        |
| 7.7 N 7.2 7.5 N 4.0                                       | 4.8        |
| 6.6 N 7.0 7.9 N 9.0                                       | 4.5        |
| .6 5.0 Y 3.6 4.6 N 3.8                                    | <b>N</b> . |
| 4.2 5.3 N 4.0 5.4 N 3.6                                   | •          |
| 1.4 ZZ.0 N Z3.4 Z1.5 Y Z1.<br>4.8 Z3.7 N Z4.3 24.9 N 23.4 | <b>4</b> 0 |
| 7 YES 21 NO 6 YES 22 NO 6                                 | ş 1        |
| 1at Hr = 12.30 - 13.30<br>2nd Hr = 13.30 - 14.30          | J          |
|   |            |
| -   |            |
|   |            |
| 200   |            |
|   |            |
|   |            |
|   | - 11       |

TABLE 5-6 Summary of Delay Time on Test Network (Ot

#### **Recommendations for Future Research**

This research study illustrated the high degree of conformity and reliability of the TRAF-NETSIM model's ability to simulate actual traffic conditions in Amman-Jordan provided that some of the model's default values are modified to reflect the local driving conditions. However, due to the limited resources available for this research the following recommendations are appropriate:

- The model should be tested and validated on additional street networks in Amman, such as an urban grid network.
- The model should be tested with the presence of high pedestrian activities.
- The TRAF-NETSIM model should be tested and calibrated on low to moderate traffic volumes in Amman-Jordan.
- The model's credibility in simulating other measures of performance such as Stopped Delay Time and Phase Failure should be investigated.
- The simulated MOE's produced by the model should be compared with other network simulation models such as Transyt-7F.

#### **Possible Applications**

The TRAF-NETSIM model is a very useful tool for Traffic Engineers. The applications of the simulation model covers most of the traffic situations encountered in most urban areas. The following is a brief list of possible applications.

- Signal timing plan evaluation
- Left-turn and right -turn pocket length evaluation
- Near-side bus stop versus far-side bus stop

- Effects of lane closure due to construction
- Effects of introducing a new overpass or underpass
- Evaluating the effects of enforcing different parking regulations
- HOV lane evaluations

#### **Traf-Netsim Model Limitations**

Despite the modifications and new enhancements made to NETSIM over the past several years, there are some specific scenarios in which the model is not applicable. However, the model can be "tricked" into representing some of the desired operations.

- TRAF-NETSIM does not simulate four-way stop sign.
- The model does not simulate the behavior of traffic travelling around a traffic circle.
- Railroad Crossing simulation can not be modeled.
- Two-way left-turn lanes are not explicitly simulated in the model.
- Currently, the model uses the Uniform Headway distribution logic to generate all vehicles into the network. However, in the interest of providing more valid output especially under low traffic volume conditions, the model should allow the engineer to specify the type of distribution to be used to generate vehicle arrivals.

#### Contributions

TRAF-NETSIM model is designed as a tool to aid engineers in testing a variety of complex traffic related problems. It was originally developed to simulate traffic performance in the United States. Yet, this study demonstrated that TRAF-NETSIM is capable of simulating the traffic performance in Amman, provided that some of the model's default

parameters be modified to reflect the local driving behavior. This will substantially help traffic engineers in Jordan to test different traffic control and traffic management strategies, on a network wide basis, which under normal circumstances can not be analyzed due to the highly variable nature of traffic operations. In addition, this study was able to ascertain the identity of some of the driver's characteristics at signalized intersections like Queue Discharge Headway's and Start-Up Lost Times. This, of course, would be beneficial information for local traffic engineers to use when timing traffic signals or estimating intersection capacity, especially since there are a lack of technical reports addressing driver's characteristics at signalized intersections in Amman Jordan.

#### Disclaimer

This study was able to determine that the calibrated TRAF-NETSIM model can accurately simulate travel time and delay time in Amman-Jordan. Further studies should be performed to test the applicability of other measures of effectiveness, fuel consumption, and vehicle emission values produced by the simulation model. REFERENCES

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Appendices

Appendix A

SAS output Start-Up Lost Time and Queue Discharge Headway

#### BAR CHART Vehicle Departure Headways at a Signalized Intersection From End of 3 rd Vehicle in Queue

Frequency

|         |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |         | **** | **** * | **** **** **** * | fffffffffffffffffffffffffffffffffffff |
|---------|------|------|------|------|------|------|------|---------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|---------|------|--------|------------------|---------------------------------------|
|         |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |         |      | ***    | ***              | ffff.<br>2                            |
|         |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      | **** | **** | **** | **** | **** | ****    | **** | ****   | ****             | fffff<br>2_1                          |
|         |      |      |      |      |      |      |      |         |      |      |      |      |      | **** | **** | **** | **** | **** | **** | **** | **** | **** | **** | **** | * * * * | **** | ****   | ****             | fffff<br>1_8                          |
|         |      |      |      |      |      |      |      | * * * * | **** | **** | **** | **** | **** | **** | **** | **** | **** | **** | **** | **** | **** | **** | **** | **** | ****    | **** | ****   | ****             | fffff.<br>1.5                         |
| * * * * | **** | **** | **** | **** | **** | **** | **** | ****    | **** | **** | **** | **** | **** | **** | **** | **** | **** | **** | **** | **** | **** | **** | **** | **** | ****    | **** | ****   | ****             | [                                     |
|         |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      | **** | **** | **** | **** | **** | **** | ****    | **** | ****   | ****             | fffff<br>0.9                          |
|         | ~ (  |      |      |      | . (  |      |      |         | • 4  |      |      |      |      |      |      |      | . (  |      |      |      | . (  |      |      |      |         |      |        | ****             | Šfffffffffffff<br>0.3 0.6             |
|         | 210  |      |      |      | 180  | •    |      |         | 150  |      |      |      | 120  |      |      |      | 06   |      |      |      | 60   |      |      |      | 30      |      |        |                  |                                       |

#### Queue Discharge Headways Normality Test

### The UNIVARIATE Procedure Variable: headway (Queue Discharge Headways)

#### Moments

| N               | 780        | Sum Weights      | 780        |
|-----------------|------------|------------------|------------|
| Mean            | 1.5064359  | Sum Observations | 1175.02    |
| Std Deviation   | 0.54827503 | Variance         | 0.30060551 |
| Skewness        | 1.71755977 | Kurtosis         | 4.09012076 |
| Uncorrected SS  | 2004.264   | Corrected SS     | 234.171692 |
| Coeff Variation | 36.3955102 | Std Error Mean   | 0.0196314  |
|                 |            |                  |            |

# Basic Statistical Measures

|             | 0.54828       | 0.30061  | 3.90000  | 0.62000             |
|-------------|---------------|----------|----------|---------------------|
| Variability | Std Deviation | Variance | Range    | Interquartile Range |
| ation       | 1.506436      | 1.350000 | 1.130000 |                     |
| Loca        | Mean          | Median   | Mode     |                     |

## Tests for Location: Mu0=0

| 1e        | <.0001<.0001<.0001<.0001           |
|-----------|------------------------------------|
| p Valu    | Pr >  t <br>Pr >=  M <br>Pr >=  S  |
| tatistic- | 76.73606<br>390<br>152295          |
| ι<br>Ι    | v ∑ t                              |
| Test      | Student's t<br>Sign<br>Signed Rank |

### Tests for Normality

| Test               | Sta  | tistic   |    |   | p Val | ue      |
|--------------------|------|----------|----|---|-------|---------|
| Shapiro-Wilk       | Μ    | 0.858921 | Pr | v | м     | <0.0001 |
| Kolmogorov-Smirnov | ۵    | 0.12771  | Ρr | Λ | D     | <0.0100 |
| Cramer-von Mises   | W-Sq | 4.974149 | Ρr | ٨ | W-Sq  | <0.0050 |
| Anderson-Darling   | A-Sq | 29.33061 | Ρr | Λ | A-Sq  | <0.0050 |
|                    |      |          |    |   |       |         |

### Quantiles (Definition 5)

| Estimate |  |
|----------|--|
| Quantile |  |

|         |            |          |          | Headways) |
|---------|------------|----------|----------|-----------|
| 4.250   | 2.665      | est      | rocedure | Discharge |
| X       |            | ality Te | ARIATE I | (Queue    |
| 100% Ma | 958<br>958 | Norn     | The UNIV | headway   |
|         |            |          |          | Variable: |

# Quantiles (Definition 5)

| Estimate | 2.125<br>1.760<br>1.350<br>1.140<br>1.035<br>0.940<br>0.660<br>0.350          |
|----------|---|
| Quantile | 90%<br>75% Q3<br>50% Median<br>25% Q1<br>10%<br>5%<br>5%<br>01<br>8<br>0% Min |

,

### Extreme Observations

| est  | Obs   | 776<br>777<br>778<br>778<br>779<br>780 |
|------|-------|--|
| High | Value | 3.77<br>3.84<br>4.00<br>4.06<br>4.25   |
| st   | Obs   | 01945                                  |
| Lowe | Value | 0.35<br>0.35<br>0.37<br>0.52<br>0.56   |

# The UNIVARIATE Procedure Variable: dh ( Difference between Observed and Default Headways)

#### Moments

| N               | 780        | Sum Weights      | 780        |
|-----------------|------------|------------------|------------|
| Mean            | -0.2935641 | Sum Observations | -228.98    |
| Std Deviation   | 0.54827503 | Variance         | 0.30060551 |
| Skewness        | 1.71755977 | Kurtosis         | 4.09012076 |
| Uncorrected SS  | 301.392    | Corrected SS     | 234.171692 |
| Coeff Variation | -186.76501 | Std Error Mean   | 0.0196314  |
|                 |            |                  |            |

# Basic Statistical Measures

|             | 0.54828<br>0.30061<br>3.90000<br>0.62000                  |  |
|-------------|---|--|
| Variability | Std Deviation<br>Variance<br>Range<br>Interguartile Range |  |
| ation       | -0.29356<br>-0.45000<br>-0.67000                          |  |
| Loca        | Mean<br>Median<br>Mode                                    |  |

# Tests for Location: Mu0=0

| ne        | <.0001<.0001<.0001                 |
|-----------|------------------------------------|
| p Valı    | Pr >  t <br>Pr >=  M <br>Pr >=  S  |
| tatistic- | -14.9538<br>-217.5<br>-95480.5     |
| S<br>I    | sи                                 |
| Test      | Student's t<br>Sign<br>Signed Rank |

### Quantiles (Definition 5)

| Estimate | 2.450<br>1.740  | 0.865<br>0.325 | -0.040<br>-0.450     | -0.660<br>-0.765 | -0.860<br>-1.140 | -1.450 |
|----------|-----------------|----------------|----------------------|------------------|------------------|--------|
| Quantile | 100% Max<br>99% | 958<br>908     | 75% Q3<br>50% Median | 25% Q1<br>10%    | 58<br>18         | O% Min |

### The UNIVARIATE Procedure ( Difference between Observed and Default Headways) dh Variable:

### Extreme Observations

| st     | obs   | 776<br>777<br>778<br>778<br>779<br>780               |
|--------|-------|--|
| Highes | Value | 1.97<br>2.04<br>2.20<br>2.26<br>2.45<br>Headway data |
| t      | obs   | 2<br>1<br>4<br>5<br>mmary of                         |
| Lowes  | Value | -1.45<br>-1.45<br>-1.43<br>-1.28<br>-1.28            |

### The MEANS Procedure

# Difference between Observed and Default Headways Analysis Variable : dh

| ue Pr >  t | 95 <.000   |
|------------|------------|
| e t Val    | 5 -14.     |
| Variance   | 0.3006055  |
| Range      | 3.900000   |
| Std Dev    | 0.5482750  |
| Mean       | -0.2935641 |
| Z          | 780        |

value of T-statistic for 95% CI with 780 DF

#### Obs tvalue

1.96301

---

#### BAR CHART

# Sart-Up Lost Time for First Vehicle at a Signalized Intersection

Frequency

|      | * * * *<br>* * * *<br>* * * *<br>* * * * | * * * *<br>* * * *<br>* * * *<br>* * * *<br>* * * * | * * * * * *<br>* * * * * *<br>* * * * * *<br>* * * * *<br>* * * * * | * | * |
|------|--|---|---|---|---|
| **** | * * * * *                                | ****  | ****  | ****                                    | ****                                    |
| **** | ****                                     | ****  | ****  | ****                                    | ****                                    |
|      | ****                                     | ****  | ****  | ****                                    | ****                                    |
|      | ****                                     | ****  | ****  | ****                                    | ****                                    |
|      | ****                                     | ****  | ****  | ****                                    | ****                                    |
|      | ****                                     | ****  | * * * * *   | ****                                    | ****                                    |
|      |  | ****  | ****  | ****                                    | ****                                    |
|      |  |   | ****  | ****                                    | ****                                    |
|      |  |   |   | ****                                    | ****                                    |
|      |  |   |   | ****                                    | ****                                    |
|      |  |   |   | ****                                    | ****                                    |
|      |  |   |   | ****                                    | ****                                    |
|      |  |   |   | ****                                    | ****                                    |
|      |  |   |   | ****                                    | ****                                    |
|      |  |   |   | ****                                    | ****                                    |
|      |  |   |   | ****                                    | ****                                    |
|      |  |   |   | ****                                    | ****                                    |
|      |  |   |   | ****                                    | ****                                    |
|      |  |   |   |   | * * * * *                               |
|      |  |   |   |   | ****                                    |
|      |  |   |   |   | * * * * *                               |
|      |  |   |   |   | * * * * *                               |
|      |  |   |   |   | ****                                    |
|      |  |   |   |   |   |
|      |  |   |   |   | ****                                    |

Start Up Lost Time for the first Vehcile in Queue

#### Normality Test

# The UNIVARIATE Procedure (Start Up Lost Time for the first Vehcile in Queue) Variable: losttime

#### Moments

| N                      | 163        | Sum Weights      | 163        |
|------------------------|------------|------------------|------------|
| Mean                   | 1.82453988 | Sum Observations | 297.4      |
| Std Deviation          | 0.69201192 | Variance         | 0.4788805  |
| Skewness               | 1.27689477 | Kurtosis         | 1.24934208 |
| Uncorrected SS         | 620.1968   | Corrected SS     | 77.5786405 |
| <b>Coeff Variation</b> | 37.9280238 | Std Error Mean   | 0.05420256 |

# Basic Statistical Measures

|             | 0.69201       | 0.47888  | 3.41000  | 0.88000             |
|-------------|---------------|----------|----------|---------------------|
| Variability | Std Deviation | Variance | Range    | Interquartile Range |
| ation       | 1.824540      | 1.600000 | 1.240000 |                     |
| Loci        | Mean          | Median   | Mode     |                     |

NOTE: The mode displayed is the smallest of 5 modes with a count of 4.

## Tests for Location: Mu0=0

| Ρ  |           |
|--|-----------|
| Pr >  t <br>Pr >  t <br>Pr >=  M           |           |
| tatistic-<br>33.66151<br>81.5<br>6683      | ) > > > > |
| א אד ו<br>מער ו                            | ג         |
| Test<br>Student's t<br>Sign<br>Signed Bank |           |

### Tests for Normality

| Test   | Sta         | tistic                          | d                          | Valu | 1e                            |
|--|-------------|---------------------------------|----------------------------|------|-------------------------------|
| Shapiro-Wilk<br>Kolmogorov-Smirnov<br>Cramer-von Mises | W D<br>W-Sq | 0.876143<br>0.160368<br>1.19402 | Pr < W<br>Pr > D<br>Pr > W | -Sq  | <0.0001<br><0.0100<br><0.0050 |
| Anderson-Darling                                       | A-Sq        | 6.629633                        | Pr > A                     | -Sq  | <0.0050                       |
|  |             |                                 |                            |      |                               |

#### Normality Test

# The UNIVARIATE Procedure (Start Up Lost Time for the first Vehcile in Queue) Variable: losttime

### Quantiles (Definition 5)

| Estimate | 4.31     | 4.15 | 3.16 | 2.88 | 2.18   | 1.60       | 1.30   | 1.18 | 1.10 | 0.97 | 0.90   |
|----------|----------|------|------|------|--------|------------|--------|------|------|------|--------|
| Quantile | 100% Max | 866  | 958  | 806  | 75% Q3 | 50% Median | 25% Q1 | 10%  | 58   | 18   | 0% Min |

### Extreme Observations

| Lowe  | est | High  | est |
|-------|-----|-------|-----|
| Value | SdO | Value | obs |
| 0.90  | 1   | 3.66  | 159 |
| 0.97  | 2   | 3.67  | 160 |
| 1.00  | m   | 3.79  | 161 |
| 1.04  | 4   | 4.15  | 162 |
| 1.06  | 9   | 4.31  | 163 |

### ( Difference between Observed and Default Start-Up Lost Times) The UNIVARIATE Procedure dlt Variable:

#### Moments

| Z                      | 163        | Sum Weights      | 163        |
|------------------------|------------|------------------|------------|
| Mean                   | -0.1754601 | Sum Observations | -28.6      |
| Std Deviation          | 0.69201192 | Variance         | 0.4788805  |
| Skewness               | 1.27689477 | Kurtosis         | 1.24934208 |
| Uncorrected SS         | 82.5968    | Corrected SS     | 77.5786405 |
| <b>Coeff Variation</b> | -394.3984  | Std Error Mean   | 0.05420256 |

Interquartile Range

NOTE: The mode displayed is the smallest of 5 modes with a count of 4.

0.69201 0.47888 3.41000 0.88000 Std Deviation Variance Range -0.17546 -0.40000 -0.76000 Median Mean Mode

Variability

Location

Basic Statistical Measures
# Tests for Location: Mu0=0

| Test        | -Statistic- | p Valu   | 1e1    |
|-------------|-------------|----------|--------|
| Student's t | t -3.23712  | Pr >  t  | 0.0015 |
| Sign        | M -35.5     | Pr >=  M | <.0001 |
| Signed Rank | S -2365.5   | Pr >=  S | <.0001 |

# Quantiles (Definition 5)

| Estimate | 2.31<br>2.15<br>2.15<br>0.88<br>0.18<br>0.18<br>-0.40<br>-0.70<br>-0.82<br>-1.03              |
|----------|---|
| Quantile | 100% Max<br>99%<br>95%<br>90%<br>75% Q3<br>50% Median<br>25% Q1<br>10%<br>5%<br>13%<br>0% Min |

.

# The UNIVARIATE Procedure ( Difference between Observed and Default Start-Up Lost Times) Variable: dlt

### Extreme Observations

| est    | obs   | 159<br>160<br>161<br>162<br>162<br>163<br>data       |
|--------|-------|--|
| -Highe | an    | 66<br>67<br>79<br>15<br>31<br>Time                   |
|        | Valı  | 1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.               |
| 1      | bs    | 1<br>2<br>3<br>6<br>8<br>Start-Up                    |
| st     | 0     | of   |
| Lowe   | Value | -1.10<br>-1.03<br>-1.00<br>-0.96<br>-0.96<br>Summary |

The MEANS Procedure

Analysis Variable : dlt Difference between Observed and Default Start-Up Lost Times

| Mean         Std Dev         Range         Val           Mean         0.6920119         3.4100000         0.47 | riance t Value Pr >  t | 788805 -3.24 0.001 |
|--|------------------------|--------------------|
| Mean Std Dev Std Dev 0.1754601 0.6920119   | Range Var              | 3.4100000 0.47     |
| Mean<br>Mean<br>9 -0.1754601   | Std Dev                | 0.6920119          |
| 2 I ITA  | Mean                   | 9 -0.1754601       |

value of T-statistic for 95% CI with 162 DF

Obs tvalue

1 1.97472

156

H

### Appendix B

Analysis of Variance

### **Analysis of Variance**

To compare the mean of the three Travel Times and Delay Times obtained from the three different study types Default, Calibrated, and Observed. Independent random samples of both Travel Times and Delay Times were selected from each of the three study types (Populations). Most likely the three sample means would be different. However, this doesn't necessarily imply a difference among the population means for the three study types used in this research. To decide whether the differences among the sample means are large enough to suggest that the corresponding population means are significantly different, the Analysis of Variance procedure was utilized.

### The Logic Underlying Analysis of Variance:

A first point to remember in looking back at the Null and Alternative hypotheses for travel time and delay time is that the hypotheses to be tested are considered as an overall statement. In other words, analysis of variance will tell us only if there are significant variations among the means in the total hypothesis statement. ANOVA will not tell us about the comparison of individual means. That is, ANOVA will not tell us if the mean travel time produced by the default model is significantly different from the mean travel time produced by the calibrated model, and so on and so forth. If the analysis of variance indicates that the means among the three study types differ, then an appropriate multiple comparison procedure such as Tukey's method will be used to determine which means are and are not significantly different form one another.

Before preceding any further, some of the terminology used by analysis of variance will be introduced now.

### Factor:

A factor in analysis of variance is an independent variable being analyzed. In this research, I am measuring Travel Time and Delay Time under three different types of study. Therefore, the factor under investigation is the variable study type as defined by this research.

### Factor Level:

A factor level is a specific entity of the factor under study. In the study of the effect of different study type on Travel Time, study type is the factor under study and the three study types, observed, calibrated, and default are levels of that factor. Hence, you conclude that the study type factor has three levels in this study.

### Single Factor Study:

A single-factor study as opposed to a multi-factor study is an investigation in which the effect of only one factor is of concern. Since this research is concerned with what are the effects of different study types on travel time and delay time, this research is conducting a single-factor analysis of variance study. An example of a multi-factor study could be the effects on study types and traffic volumes on travel time and delay time. Here, the two factors, study type and traffic volume would be investigated simultaneously to gain further insight on their effects on the variable or variables being observed. Table B-1 shows the symbolic notation used by a single factor analysis of variance, for Travel Time in the Test Network:

| FACTOR LEVEL | 1                               | 2               | 3                               |                    |
|--------------|---------------------------------|-----------------|---------------------------------|--------------------|
| STUDY TYPE   | DEFAULT                         | CALIBRATED      | OBSERVED                        |                    |
| OBSERVATIONS | Y <sub>11</sub> Y <sub>17</sub> | $Y_{21}Y_{27}$  | Y <sub>31</sub> Y <sub>37</sub> |                    |
| SAMPLE SIZE  | nl                              | n2              | N3                              | N <sub>TOTAL</sub> |
| TOTAL        | Y <sub>T1</sub>                 | Y <sub>T2</sub> | Y <sub>T3</sub>                 | Y <sub>total</sub> |
| VARIANCE     | S1 <sup>2</sup>                 | S2 <sup>2</sup> | S3 <sup>2</sup>                 |                    |
| MEAN         | Y1                              | Y2              | Y3                              | Y <sub>GRAND</sub> |

Table B-1 Notation used by ANOVA

Where:

- $Y_{11}$ : Travel Time for the first simulation run obtained from the default model.
- $Y_{17}$ : Travel Time for the seventh simulation run obtained from the default model.
- n<sub>1</sub>: Number of simulation runs for default model.
- Y<sub>T1</sub>: Total Travel Time from default model.
- Y1: Mean Travel Time from default model.
- N<sub>TOTAL</sub>: Total number of observations across all groups.
- S1<sup>2</sup>: Variance of Travel Time from default model.
- $Y_{GRAND}$ : The average of all sample observations;  $Y_{GRAND} = (Y_{TOTAL} / N_{TOTAL})$  etc.

### Appendix C

TRAF-NETSIM Simulation output

Test Network Default Model

INTELLIGENT VEHICLE HIGHWAY SYSTEM RESEARCH DIVISION U. S. DEPARTMENT OF TRANSPORTATION FEDERAL HIGHWAY ADMINISTRATION

DEVELOPED FOR

**RELEASE DATE MAR 1995** TRAF SIMULATION MODEL **VERSION 5.00** 

MICRO-COMPUTER PROTECTED-MODE VERSION (REQUIRES 80386 AND 80387 OR ABOVE)

RRR RRR

RRR

RRR

RRR RRR RRR RRR

INPUT FILE NAME: MWED1.TRF

: 08/05/99 RUN DATE

EFFFFFFFFFF EFFFFFFFFF FFFFFFFFFFFF

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AAA AAA

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RRR RRR

RRR RRR

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RRRRRRRRRR

RRRRRRRRR

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AAAAAAAA AAAAAA

FFFFFF FFFFFF

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| 88                                      | 0      | 0      | 0      | 0     | 0     | ן<br>ו  | 2       | m     | 4     | S   | 11      | 11     | 11     | 11      | 11      | 11      | 11      | 11      | 11      | 11      | 11    | 11      | 11      | 11      | 11      | 11      | 11      | 11      | 11      | 11      | 11     | 11    |
|---|--------|--------|--------|-------|-------|---------|---------|-------|-------|-----|---------|--------|--------|---------|---------|---------|---------|---------|---------|---------|-------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------|-------|
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|   |        |        |        |       |       |         | 1328    |       |       |     |         |        |        |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |        |       |
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| LIST                                    |        |        | TES    |       |       | 16      |         |       |       |     | 100     | 100    | 101 1( | 102     | 104 10  | 103     | 101     | 106     | 108     | H       | 112   | 114     |         | 120     | 122     | i.      |         |         | 202     | 202     | 206    | 200   |
| D FILE<br>4-                            |        | 1997   | O MINU |       |       | 05      |         |       |       |     |         |        | 103    | 8       | 101     | 8       | 8       | 8       |         |         | 8     |         |         | 8       |         |         |         |         |         | 8       |        | 1     |
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| + | RT :   |        |        |       |       | GHEZAWI |         |       |       |     |         |        | 50     | 50      | 28      | 28      | 00      | 00      |         | 00      | 00    |         | 00      | 00      |         | 00      | 31      | 70      | 43      | 37      |        | 00    |
|   | VETWO  |        |        |       |       | SAID    |         |       |       |     | 102     | 103    | 100 1  | 102 1   | 100 1   | 103 1   | 101 1   | 106 1   | 106     | 108 1   | 112 1 | 112     | 14 1    | 120 1   | 120     | 122 1   | 126 1   | 204     | 204     | 202 1   | 202    | 206 1 |
| -+                                      | TEST N |        |        |       |       | SAMI S  | •       | :3600 |       |     | :8102 ] | 8103 1 | 102 1  | : 100 1 | : 103 1 | : 100 1 | : 100 ] | : 108 ] | :8106 ] | : 106 ] | 114   | :8112 ] | : 112 ] | : 122 ] | :8120 ] | : 120 1 | : 125 1 | : 126 2 | : 200 2 | : 204 2 | 8202 2 | 202   |
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| 1<br>OSE(                               |        |        |        |       |       |         |         |       |       |     |         |        |        |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         | 1      | 74    |

| +212  | 8     |       | 216              |       |       | 218   |       |       | 226   |       |       | 228   | +302  |       |       |       | +306  |         | +308   |       |       | +307  | +305      |         | +303    |       |       | +227  |         |       | +311  |       |       | 315   |       |       |
|-------|-------|-------|------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|---------|--------|-------|-------|-------|-----------|---------|---------|-------|-------|-------|---------|-------|-------|-------|-------|-------|-------|-------|
|       | 8210  | 212   |                  | 8214  | 216   |       | 8220  | 222   |       | 8224  | 226   |       |       | 302   | 8302  | 304   | 300   | 227 305 |        | 308   | 8300  | 300   |           | 310 227 |         | 8301  | 301   | 300   | 306 310 | 303   |       | 8309  | 311   |       | 8313  | 315   |
| 0     | 0     | 0     | 0                | 0     | 0     | 0     | 0     | 0     | 0     | 0     | 0     | 0     | 0     | 0     | 0     | 0     | 0     | 0       | ε<br>Γ | -4    | -4    | +4    | <b>14</b> | +4 T81  | ,<br>+3 | 0     | 0     | 0     | 0       | 0     | +3    | 0     | 0     | 0     | 0     | 0     |
| 1     | 1     | 1     | <del>, , ,</del> | 1     | 1     | 1     | 1     | 1     | 1     | 1     | 1     | 1     | 1     | m     | ń     | m     | m     | ო       | 1      | ო     | ო     | m     |           | m       |         | ო     | ო     | m     | ო       | ო     | 1     | 1     | 1     | 7     | -1    | 1     |
| 88    | 100   |       | 100              | 100   |       | 100   | 100   |       | 100   | 100   |       | 100   | 77    | 47    | 100   |       | 100   | 41      | 60     | 48    | 200   |       | 190       | 243     | 58      | 100   |       | 100   | 37      | 25    | 40    | 78    |       | 78    | 100   |       |
| 208   | 210   | 210   | 212              | 214   | 214   | 216   | 220   | 220   | 222   | 224   | 224   | 226   | 310   | 310   | 302   | 302   | 304   | 300     | 306    | 306   | 308   | 308   | 307       | 300     | 305     | 303   | 303   | 301   | 300     | 305   | 227   | 309   | 309   | 311   | 313   | 313   |
| : 206 | : 212 | :8210 | : 210            | : 216 | :8214 | : 214 | : 222 | :8220 | : 220 | : 226 | :8224 | : 224 | : 228 | : 300 | : 310 | :8302 | : 302 | : 304   | : 304  | : 300 | : 306 | :8300 | : 308     | : 308   | : 307   | : 305 | :8301 | : 303 | : 301   | : 300 | : 301 | : 311 | :8309 | : 309 | : 315 | :8313 |
| 34    | 35    | 36    | 37               | 38    | 39    | 40    | 41    | 42    | 43    | 44    | 45    | 46    | 47    | 48    | 49    | 50    | 51    | 52      | 53     | 54    | 55    | 56    | 57        | 58      | 59      | 60    | 61    | 62    | 63      | 64    | 65    | 99    | 67    | 68    | 69    | 70    |

|   | 11    | 11    | 11    | 11  |        | 11    | 11  | 11    | 11    | 11    | 11    | 11     | 11    | 11     | 11     | 11    | 11              | 11      | 11    | 11     | 11     | 11      | 11    | 11   | 11     | 11    | 11   | 11     | 11    | 11    | 11    | 11    | 11    | 11         | 11         | 11      | 11   |
|---|-------|-------|-------|-----|--------|-------|-----|-------|-------|-------|-------|--------|-------|--------|--------|-------|-----------------|---------|-------|--------|--------|---------|-------|------|--------|-------|------|--------|-------|-------|-------|-------|-------|------------|------------|---------|------|
|   |       |       |       |     |        |       |     |       |       |       |       |        |       |        |        |       |                 |         |       |        |        |         |       |      |        |       |      |        |       | 21    |       |       |       |            |            |         |      |
|   |       |       |       |     |        |       |     |       |       |       |       |        |       |        |        |       |                 |         |       |        |        |         |       |      |        |       |      |        |       |       |       |       |       |            |            |         |      |
|   | 218   |       |       | 323 |        |       | 327 |       |       | 331   |       |        | 335   |        |        | 337   | +201            |         |       |        | +207   |         | +209  |      |        | 219   |      |        | 100   |       | 106   |       | 112   |            |            | 120     | +126 |
| · |       | 8317  | 218   |     | 8321   | 323   |     | 8325  | 327   |       | 8329  | 331    |       | 8333   | 335    |       |                 | 201     | 8201  | 275    | 200    | 208 204 |       | 8215 | 217    |       | 8223 | 225    |       | 108   | 110   | 114   | 116   | 118        | 122        | 125     | 200  |
|   |       |       |       |     |        |       |     |       |       |       |       |        |       |        |        |       |                 |         |       |        |        | 8       |       |      |        |       |      |        |       |       |       |       |       |            |            |         |      |
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|   | Г     | Ч     | Ч     | Ч   | Ч      | Ч     | Ч   | Ч     | 1     | 1     | 1     | Ч      | -     | -1     | -1     | Ч     | <del>ا</del> مع | ო       | m     | 2      | ო      | л<br>1  | 1     | 1    | 1      | г     | ٦    |        | 1     | 4     | ო     | ო     | m     | m          | m          | m       | ო    |
|   |       |       |       |     |        |       |     |       |       |       |       |        |       |        |        |       |                 |         |       |        |        | 30      |       |      |        |       |      |        |       |       |       |       |       |            |            |         |      |
|   | 100   | 100   |       | 100 | 100    |       | 100 | 100   |       | 100   | 100   |        | 100   | 100    |        | 100   | 108             | 54      | 50    |        | 50     | 35      | 49    | 100  |        | 100   | 100  |        | 100   | 160   | 98    | 70    | 70    | 112        | 200        | 254     | 40   |
|   | 315   | 317   | 317   | 218 | 321    | 321   | 323 | 325   | 325   | 327   | 329   | 329    | 331   | 333    | 333    | 335   | 205             | 205     | 201   | 203    | 275    | 200     | 207   | 215  | 215    | 217   | 223  | 223    | 225   | 104   | 108   | 110   | 114   | 116        | 118        | 122     | 125  |
|   | 313   | 218   | 3317  | 317 | 323    | 3321  | 321 | 327   | 3325  | 325   | 331   | 3329   | 329   | 335    | 3333   | 333   | 337             | 200     | 205   | 3201   | 203    | 275     | 275   | 217  | 3215   | 215   | 225  | 3223   | 223   | 100   | 104   | 108   | 110   | 114        | 116        | 118     | 122  |
|   | <br>1 | <br>2 | <br>ო | 4   | ۍ<br>د | <br>9 | 7 : | <br>8 | <br>б | <br>0 | <br>1 | 5<br>5 | <br>ო | 4<br>7 | ۍ<br>۳ | <br>9 | :               | ••<br>∞ | <br>6 | ₩<br>0 | <br>,  | <br>7   | <br>ო | 4 :  | с<br>С | <br>و |      | ₩<br>∞ | <br>ი | <br>0 | <br>- | <br>5 | <br>ო | 4 :        | 5          | ۰۰<br>و | : -  |
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|            |         |     |     |       |     |      |     |     |       |     |     |     |     |     |     |      |     |        |     |         |     |     |     |     |     |        | 15   |      |      |      |      |      |      |      |      |
|------------|---------|-----|-----|-------|-----|------|-----|-----|-------|-----|-----|-----|-----|-----|-----|------|-----|--------|-----|---------|-----|-----|-----|-----|-----|--------|------|------|------|------|------|------|------|------|------|
|            |         |     |     |       |     | 0    |     |     |       |     |     |     |     |     |     | 10   |     |        |     |         |     |     |     |     |     | 103    | 85   | 100  | 100  | 100  | 100  | 100  | 100  | 100  | 100  |
|            | 210     | 214 |     | 220   | 224 | +31( |     |     | 309   | 313 | 317 | 321 | 325 | 329 | 333 | +205 |     |        |     |         |     | 215 |     |     | 223 | 101    | 308  | 302  | 303  | 202  | 203  | 102  | 103  | 215  | 120  |
| 208<br>212 | 216     | 218 | 222 | 226   | 228 | 300  | 306 | 311 | 315   | 218 | 323 | 327 | 331 | 335 | 337 | 200  | 207 | 209    | 211 | 213     | 217 | 219 | 221 | 225 | 100 | 103    | 8300 | 8302 | 8301 | 8202 | 8201 | 8102 | 8103 | 8215 | 8120 |
| 205        |         |     |     |       |     |      | 305 |     |       |     |     |     |     |     |     |      | 204 |        |     |         |     |     |     |     |     | 102    |      |      |      |      |      |      |      |      |      |
| TTT1       |         |     |     |       |     |      | TT8 |     |       |     |     |     |     |     |     |      | TT8 |        |     |         |     |     |     |     |     | 7T81   |      |      |      |      |      |      |      |      |      |
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|            |         |     |     |       |     |      |     |     |       |     |     |     |     |     |     |      |     |        |     |         |     |     |     |     |     |        |      | 00   |      | 48   |      | 23   |      | 44   |      |
| יי ידא     | (*)     | (7) | (7) | (7)   | (°) | (*)  | (T) | (7) | (7)   | (T) | (°) | ന   | m   | m   | m   | m    | ന   | m      | m   | m       | m   | m   | m   | ო   | m   | 4      |      |      |      | 1    |      |      |      |      |      |
| 150        |         |     |     |       |     |      |     |     |       |     |     |     |     |     |     |      | 70  |        |     |         |     |     |     |     |     |        | 825  |      | 314  | 531  | 814  | 022  | 398  | 600  | 858  |
| 160<br>68  | 216     | 319 | 155 | 124   | 230 | 187  | 45  | 28  | 240   | 187 | 133 | 134 | 126 | 125 | 96  | 173  | 06  | 40     | 131 | 66      | 200 | 135 | 65  | 200 | 177 | 132    | 512  |      | 217  |      | 208  | Ч    | 202  |      | 458  |
| 200<br>208 | 212     | 216 | 218 | 222   | 226 | 228  | 300 | 227 | 311   | 315 | 218 | 323 | 327 | 331 | 335 | 337  | 200 | 207    | 209 | 211     | 213 | 217 | 219 | 221 | 225 | 100    | 300  | 307  | 300  | 304  | 300  | 228  | 300  | 301  | 200  |
| 125<br>200 | 208     | 212 | 216 | 218   | 222 | 226  | 228 | 300 | 227   | 311 | 315 | 218 | 323 | 327 | 331 | 335  | 337 | 200    | 207 | 209     | 211 | 213 | 217 | 219 | 221 | 225    | 308  | 308  | 304  | 302  | 228  | 226  | 301  | 303  | 337  |
|            |         | ••  |     | <br>m | ••• |      | ••  |     | <br>~ | ••  |     | ••• |     | ••  | ••• |      | ••• |        | ••  |         |     | ••  | ••  | ••  | ••  | •••    | ••   |      | ••   |      |      | ••   | ••   | ••   | ••   |
| 10501      | 11(     | 111 | 112 | 11    | 114 | 115  | 11( | 117 | 118   | 119 | 12( | 12] | 122 | 123 | 124 | 125  | 126 | 127    | 128 | 129     | 130 | 131 | 132 | 133 | 134 | 135    | 136  | 137  | 136  | 135  | 14C  | 141  | 142  | 143  | 144  |

| 290  |     | 83  |      | 100 | 100 |     | 476  |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     | 10  |     |     | 100 | 100 | 100 |     |     |     |     |     |     |
|------|-----|-----|------|-----|-----|-----|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
|      |     |     |      |     |     |     |      | 888 | 33  | 43  |     |     |     | 1   |     | 100 |     |     | 2   |     | 100 |     |     | -   |     |     | 100 |     |     |     | 10  |     | 100 | 27  |     | 100 |
| 1316 | 515 | 754 | 715  |     |     | 405 | 1029 | 25  | 929 | 725 | 100 | 100 | 100 | 66  | 100 |     | 100 | 100 | 98  | 100 |     | 100 | 100 | 66  | 90  | 100 |     |     |     |     | 90  | 100 |     | 73  | 100 |     |
|      | 239 |     | 1261 |     |     | 624 |      | 600 | 259 | 971 |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| 337  | 200 | 206 | 2001 | 126 | 204 | 200 | 275  | 100 | 100 | 100 | 102 | 103 | 101 | 108 | 106 | 108 | 104 | 110 | 114 | 112 | 114 | 116 | 118 | 122 | 125 | 120 | 122 | 207 | 310 | 208 | 212 | 210 | 212 | 216 | 214 | 216 |
| 335  | 206 | 202 | 125  | 125 | 126 | 275 | 203  | 102 | 103 | 225 | 100 | 100 | 100 | 104 | 108 | 106 | 100 | 108 | 110 | 114 | 112 | 114 | 116 | 118 | 122 | 122 | 120 | 275 | 228 | 206 | 208 | 212 | 210 | 212 | 216 | 214 |
| ••   | ••  | ••  | ••   | ••  | ••  | ••  | ••   | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  |
| 145  | 146 | 147 | 148  | 149 | 150 | 151 | 152  | 153 | 154 | 155 | 156 | 157 | 158 | 159 | 160 | 161 | 162 | 163 | 164 | 165 | 166 | 167 | 168 | 169 | 170 | 171 | 172 | 173 | 174 | 175 | 176 | 177 | 178 | 179 | 180 | 181 |

| 210<br>214<br>333<br>329     | 224<br>309<br>223<br>223<br>223<br>223<br>317<br>313<br>321<br>321                   | 9 N T |
|------------------------------|--|-------|
| 8210<br>8214<br>8333<br>8333 | 8224<br>8309<br>8309<br>8112<br>8223<br>8223<br>8213<br>8313<br>8317<br>8321<br>8321 | απτα  |

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|     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     | 100 | 100 | 100 | 100 |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
|     | e   |     | 100 | 1   |     | 100 | Ч   |     |     |     |     |     |     | 1   |     |     |     |     | 9   |     | 100 |     |     | ი   |     | 100 |     |     |     |     |     |     |     |     |     |     |
| 100 | 97  | 100 |     | 66  | 100 |     | 66  | 100 | 100 | 100 | 100 | 100 | 100 | 66  | 100 | 100 | 100 | 100 | 94  | 100 |     | 100 | 100 | 91  | 100 |     | 100 | 100 | 100 | 100 | 100 | 100 |     |     |     |     |
| 218 | 222 | 220 | 222 | 226 | 224 | 226 | 311 | 201 | 204 | 205 | 208 | 207 | 317 | 323 | 202 | 209 | 211 | 213 | 217 | 215 | 217 | 219 | 221 | 225 | 223 | 225 | 305 | 310 | 306 | 303 | 302 | 308 | 306 | 305 | 227 | 205 |
| 216 | 218 | 222 | 220 | 222 | 226 | 224 | 227 | 205 | 200 | 200 | 200 | 200 | 218 | 218 | 204 | 207 | 209 | 211 | 213 | 217 | 215 | 217 | 219 | 221 | 225 | 223 | 300 | 300 | 300 | 305 | 310 | 306 | 304 | 307 | 301 | 337 |
| ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  |
| 182 | 183 | 184 | 185 | 186 | 187 | 188 | 189 | 190 | 191 | 192 | 193 | 194 | 195 | 196 | 197 | 198 | 199 | 200 | 201 | 202 | 203 | 204 | 205 | 206 | 207 | 208 | 209 | 210 | 211 | 212 | 213 | 214 | 215 | 216 | 217 | 218 |
|     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     | 179 | 9   |

|     | 2   | 100 |     |     | 100 | 0   | 100 |     | 100 | 0   |     | 100 | 2   |     | 100 | m   |     | 100 |     |     |     |     |     |     |     |     |     |     |     | 216 |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 100 | 98  |     | 100 | 100 |     | 98  |     | 100 |     | 98  | 100 |     | 98  | 100 |     | 97  | 100 |     | 200 |     |     | 300 | 300 | 300 | 300 | 227 | 222 | 311 | 218 | 315 | 218 | 212 | 323 | 327 | 331 | 208 |
|     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     | 126 | 125 | 122 | 301 | 307 | 304 | 228 | 309 | 224 | 313 | 220 | 317 | 321 | 214 | 325 | 329 | 333 | 210 |
| 309 | 315 | 311 | 227 | 313 | 315 | 218 | 218 | 321 | 323 | 327 | 325 | 327 | 331 | 329 | 331 | 335 | 333 | 335 |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| 311 | 311 | 309 | 300 | 315 | 313 | 315 | 317 | 323 | 321 | 323 | 327 | 325 | 327 | 331 | 329 | 331 | 335 | 333 | 204 | 126 | 125 | 227 | 305 | 306 | 310 | 311 | 226 | 315 | 222 | 218 | 323 | 216 | 327 | 331 | 335 | 212 |
| ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••• | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  |
| 219 | 220 | 221 | 222 | 223 | 224 | 225 | 226 | 227 | 228 | 229 | 230 | 231 | 232 | 233 | 234 | 235 | 236 | 237 | 238 | 239 | 240 | 241 | 242 | 243 | 244 | 245 | 246 | 247 | 248 | 249 | 250 | 251 | 252 | 253 | 254 | 255 |

|     |     |     | 217  |     | 225  |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
|-----|-----|-----|------|-----|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 207 | 209 | 211 | 8215 | 219 | 8223 | 226 | 302 | 308 | 303 | 203 | 217 |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
|     |     |     |      |     |      |     |     |     |     |     |     | Ч   | 7   |     | Ч   | 51  |     | Ч   | 51  | 1   | -   | 51  | ٦   | ч   | 1   | 51  | Ч   |     | Ч   | Ч   | -   | 01  | 1   | 1   | 01  |
| 209 | 211 | 213 | 215  | 221 | 223  | 228 | 304 | 307 | 301 | 275 | 219 | 102 | 101 | 103 | 104 | 225 | 106 | 221 | 114 | 112 | 116 | 217 | 215 | 118 | 213 | 122 | 126 | 125 | 219 | 211 | 120 | 207 | 206 | 202 | 205 |
| ••  | ••  | ••  | ••   | ••  | ••   | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  |
| 293 | 294 | 295 | 296  | 297 | 298  | 299 | 300 | 301 | 302 | 303 | 304 | 305 | 306 | 307 | 308 | 309 | 310 | 311 | 312 | 313 | 314 | 315 | 316 | 317 | 318 | 319 | 320 | 321 | 322 | 323 | 324 | 325 | 326 | 327 | 328 |

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| 36<br>36<br>36<br>36<br>36<br>36<br>43                      | 80 0 43<br>10 0 43<br>45     | 44444<br>40000           | 4 4 4 4<br>7 0 0                      | 4 4 7<br>4 2<br>7 | 4 4 4 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 | 4 4 4 4<br>4 9 0 0 4   | 4 4 4 4 4<br>9 9 9 4 4 4<br>9 9 9 9 7 7<br>7 9 9 7<br>7 9 7 7 9 7 7 9 7 7 9 7 7 7 7 |
|---|------------------------------|--------------------------|---------------------------------------|-------------------|---|--|---|
| 7 28  | 1,38                         |                          |                                       |                   |   |  |   |
| 5.  | 118<br>2469                  |                          |                                       |                   |   |  |   |
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|   |                              | 222                      | 222<br>222<br>222<br>222              | 222<br>222<br>112 |   |  | 100 400   |
|   | 200<br>300                   |                          |                                       |                   |   |  |   |
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| 2 10  | 8 30<br>8 30                 |                          |                                       |                   | 18<br>40<br>40<br>40                    | 1<br>1<br>1<br>1<br>1<br>8<br>1<br>1<br>8<br>1<br>9<br>1<br>9<br>1<br>9<br>1<br>9<br>1<br>9<br>1 | 16<br>15<br>15<br>15  |
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| 225   | 337<br>301                   |                          |                                       |                   |   | 116.65   | 12:12<br>996<br>940<br>30<br>40   |
| 100   | 200<br>300<br>211            | 221<br>221<br>112        | 222<br>222<br>112                     | 222<br>222<br>222 | 113<br>213<br>24<br>24<br>24            | 1 4 0 0 0<br>1 4 0 0 0   | 30<br>19<br>19<br>19<br>19<br>19<br>19<br>19<br>19<br>19  |
| 01  | 275<br>28<br>3               | - 10 4 - 10              | 1641                                  | 1 C1 CN 4         | 0 0 0 0 0<br>0 0 0 0 0                  | 0000   | оооооо<br>  |
| 00 1 00 1 00 00 00 00 00 00 00 00 00 00                     |                              |                          |                                       | 000               |   |  |   |
|   | 0 0 A F                      | 5 6 F F F                | ง ลั ลั คั<br>                        |                   |   |  | ٥   |
| 366<br>367<br>368<br>368<br>368<br>368<br>370<br>371<br>372 | 373<br>374<br>375<br>375     | 377<br>378<br>379<br>379 | 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 | 384<br>385<br>385 | 300 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9  | 396<br>397<br>398<br>399<br>401<br>401  |

| 47    | 47                      | 64  | 4 7   | - <del>1</del>         | - F<br>- F | 47                     | 47                    | 47                    | 47                      | 50           | 50           | 50         | 50           | 50          | 50          | 50          | 50    | 170   | 195   | 195   | 195   | 195   | 195   | 195   | 195   | 195   | 195   | 195   | 195   | 195   | 195   | 195   | 195   | 195   | 195   |
|-------|-------------------------|---|---|------------------------|------------|------------------------|-----------------------|-----------------------|-------------------------|--------------|--------------|------------|--------------|-------------|-------------|-------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
|       | J 40U 30 10010100000000 | J 600 30 10010100000000000000000000000000 | ) 400 30 1001010000000<br>) 400 30 10010100010000 | 0 400 30 1001010000000 |            | 0 600 30 1001010000000 | 0 400 0 0010100000000 | 0 400 0 0011100010000 | 0 400 30 10010100010000 | 8120 120 126 | 8214 214 156 | 8329 329 4 | 8309 309 106 | 8325 325 15 | 8313 313 15 | 8317 317 15 |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 400   | 400                     |   |   | 400                    | 400        | 600                    | 400                   | 400                   | 400                     |              |              |            |              |             |             |             |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 10.1  |                         | 0 6                                       |   |                        |            | -                      | 1                     | 10                    | 1                       | 5 38         | ) 24         | 3 371      | 1 43         | L 15        | 5 15        | 2 15        | ) 15  |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| •     | 5                       | וש  | - 1 -   |                        |            |                        |                       | Ű                     | [-                      | 215          | 210          | 333        | 224          | 321         | 106         | 112         | 220   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
|       |                         |   |   |                        |            |                        |                       |                       |                         | 8215         | 8210         | 8333       | 8224         | 8321        | 8106        | 8112        | 8220  |       | 374   | 380   | 337   | 392   | 378   | 393   | 282   | 345   | 161   | 06    | 120   | 163   | 177   | 127   | 387   | 280   | 345   |
| 640   | 040                     | 000                                       | 010   | 740                    | 740        | 760                    | 740                   | 640                   | 740                     | 1            | 1            | -          |              | 1           | . 1         | -           | -1    |       |       |       | _     |       |       |       |       | -     | _     |       | _     |       | _     |       |       |       |       |
| 30    | 202                     | $   \frac{1}{2} $                         | 000   | 90<br>90<br>90         | 20         | 25                     | 20                    | 10                    | 17                      | 81578        | 2 680        | 3 644      | 2 837        | 31505       | 21513       | 31186       | 3 315 |       | 356   | 428   | 1280  | 1884  | 2038  | 1905  | 2342  | 2167  | 2530  | 2554  | 262C  | 2577  | 2575  | 127   | 127   | 01    | 265   |
| 20    | n -                     | <b>7</b> - 7                              | - ~   | i m                    | 4          | m                      | Ч                     | 2                     | 4                       | 30           | 30           | 30         | 20           | 20          | 10          | 10          | 22    |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| : 200 |                         |   | . 300   | : 300                  | : 300      | : 100                  | : 100                 | : 100                 | : 100                   | :8300        | :8302        | :8301      | :8202        | :8201       | :8102       | :8103       | :8223 | 0<br> | : 108 | : 110 | : 204 | : 216 | : 218 | : 323 | : 311 | : 315 | : 228 | : 310 | : 307 | : 305 | : 301 | : 102 | : 101 | : 103 | : 104 |
| 403   | 404                     | 402                                       | 407   | 408                    | 409        | 410                    | 411                   | 412                   | 413                     | 414          | 415          | 416        | 417          | 418         | 419         | 420         | 421   | 422   | 423   | 424   | 425   | 426   | 427   | 428   | 429   | 430   | 431   | 432   | 433   | 434   | 435   | 436   | 437   | 438   | 439   |

| 287       | 380       | 140       | 344       | 444       | 262       | 382       | 379       | 279       | 379       | 382       | 482       | 378       | 382       | 378       | 378       | 381       | 278       | 363       | 381       | 380       | 304       | 212       | 434       | 420       | 480       | 480       | 380       | 383       | 385       | 387       | 285       | 487       | 389       | 489       | 392       | 492     |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|
| 127       | 1281      | 2569      | 255       | 255       | 358       | 428       | 498       | 498       | 610       | 675       | 675       | 810       | 810       | 1104      | 1064      | 1010      | 1064      | 1214      | 1110      | 1241      | 1282      | 1281      | 1277      | 1276      | 1273      | 1270      | 1350      | 1385      | 1566      | 1558      | 1566      | 1558      | 1654      | 1654      | 1779      | 1779    |
| 440 : 100 | 441 : 200 | 442 : 300 | 443 : 225 | 444 : 223 | 445 : 106 | 446 : 221 | 447 : 114 | 448 : 112 | 449 : 116 | 450 : 217 | 451 : 215 | 452 : 118 | 453 : 213 | 454 : 125 | 455 : 122 | 456 : 211 | 457 : 120 | 458 : 126 | 459 : 209 | 460 : 207 | 461 : 206 | 462 : 202 | 463 : 205 | 464 : 275 | 465 : 201 | 466 : 203 | 467 : 208 | 468 : 337 | 469 : 212 | 470 : 335 | 471 : 210 | 472 : 333 | 473 : 331 | 474 : 329 | 475 : 327 | 476:325 |

| 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95  | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|-----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|
| Ч  |    |    | Ч  | ٦  |    | Ţ  | Ļ  | Ē  |    |    | Ч  |    |    | -  | ÷-+ | ÷- | Ļ, |    | -  | -  | Ч  | ÷. | ÷- | -  | -  | ÷. | ÷, | ÷, | -  |    | ÷. | ÷. | ÷. | Ē. | ÷. | H  |

### START OF CASE

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### U. S. DEPARTMENT OF TRANSPORTATION FEDERAL HIGHWAY ADMINISTRATION INTELLIGENT VEHICLE HIGHWAY SYSTEM RESEARCH DIVISION

### DEVELOPED FOR

## TRAF SIMULATION MODEL

| 292      | 493      | 493     | 345      | 245      | 445     | 262      | 162      | 345            | 06       | 01       | 112      | 6        | 270      | 382     | 155      |          |          |          |          |          |          |          |          |  |
|----------|----------|---------|----------|----------|---------|----------|----------|----------------|----------|----------|----------|----------|----------|---------|----------|----------|----------|----------|----------|----------|----------|----------|----------|--|
| 14 1884  | 21 1905  | 17 2038 | 22 2157  | 20 2157  | 13 2167 | 26 2371  | 24 2371  | <b>09 2390</b> | 04 2556  | 02 2545  | 06 2610  | 38 2776  | 03 2588  | 19 610  | 27 2545  | 04 108 1 | 21 225 2 | 16 218 1 | 18 323 2 | 22 226 1 | 28 310 1 | 04 306 1 | 11 315 2 |  |
| 477 : 21 | 478 : 32 | 479 : 3 | 480 : 22 | 481 : 22 | 482 : 3 | 483 : 22 | 484 : 22 | 485 : 3(       | 486 : 3( | 487 : 3( | 488 : 3( | 489 : 3( | 490 : 3( | 491 : 2 | 492 : 22 | 493 : 1( | 494 : 2; | 495 : 2] | 496 : 2: | 497 : 22 | 498 : 2; | 499 : 3( | 500 : 3  |  |

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| TEST NETWORT : MECCA STREET<br>WEDNESDAY MAY 14, 1997<br>DEFAULT , EVERY 60 MINUTES<br>12:30 13:30 | DATE = 05/ 16/ 97<br>USER = SAMI SAID GHEZAWI<br>AGENCY =<br>RUN CONTROL DATA | VALUE RUN PARAMETERS AND OPTIONS | <pre>1 RUN IDENTIFICATION NUMBER<br/>0 NEXT CASE CODE = (0,1) IF ANOTHER CASE (DOES NOT, DOES) FOLLOW<br/>1 RUN TYPE CODE = (1, 2, 3) TO RUN (SIMULATION, ASSIGNMENT, BOTH)<br/>(-1,-2,-3) TO CHECK (SIMULATION, ASSIGNMENT, BOTH) ONLY</pre> | NETSIM ENVIRONMENTAL OPTIONS | 0 FUEL/EMISSION RATE TABLES ARE NOT PRINTED<br>0 SIMULATION: PERFORMED<br>0 SIMULATION: PERFORMED | RATE TABLES: EMBEDDED TRAJECTORY FILE: | 1 INPUT UNITS CODE = (0,1) IF INPUT IS IN (ENGLISH, METRIC) UNITS<br>0 OUTPUT UNITS CODE = (0,1,2,3) IF OUTPUT IS IN (SAME AS INPUT, ENGLISH, | ITS<br>1230 CLOCK TIME AT START OF SIMULATION (HHMM)<br>0 SIGNAL TRANSITION CODE = (0,1,2,3) IF (NO, IMMEDIATE, 2-CYCLE, 3-CYCLE) | EQUESTED<br>7581 RANDOM NUMBER SEED<br>132841 RANDOM NUMBER SEED TO GENERATE TRAFFIC STREAM FOR NETSIM OR LEVEL I |
|--|---|----------------------------------|---|------------------------------|---|--|---|---|---|
| 00000  | 001   |                                  | 000   | 0                            |   | CALCULATED                             | NOT WRITTEN<br>0  | METRIC, BOTH) UNITS<br>0<br>0   | TRANSITION WAS REQUE<br>0<br>strutton   |

| TPUTS<br>C STOR<br>C STOR   | F) REQUESTED FOR                                   | (IS NOT, IS)          | DS ASSUMED.                                      |                  | PERCENT<br>DI FFERENCE        |
|---|--|-----------------------|--|------------------|-------------------------------|
| 1<br>5<br>3ER OF TIME INTERVALS<br>SUCCESSIVE STANDARD OU7<br>2IN AT INTEPVALS OF (                                 | CODE = (0, 1) (IF NOT, II)                         | 1) IF GRAPHICS OUTPUT | E FOLLOWING REASON -<br>FAULT VALUE OF 60 SECONI | STATISTICS       | CURRENT CONTENT<br>(VEHICLES) |
| ) OF TIME PERIOD NO.<br>IME INTERVAL, SECONI<br>ALIZATION TIME, NUME<br>E INTERVALS BETWEEN<br>TATE OUTPUT WILL BEC | NT-SPECIFIC OUTPUT (                               | CS OUTPUT CODE = (0,  | BY THE MODEL FOR THE<br>URATION OMITTED. DEE     | INITIALIZATION 5 | PRIOR CONTENT<br>(VEHICLES)   |
| DURATION (SEC<br>LENGTH OF A T<br>MAXIMUM INITL<br>NUMBER OF TIM<br>TIME INTERMED                                   | NETSIM MOVEME                                      | NETSIM GRAPHI         | VALUE ASSERTED<br>TIME INTERVAL D                |                  | SUBNETWORK<br>TYPE            |
| 3600<br>30<br>30<br>30<br>30  | CS. FOR MICROSCOPIC MODELS<br>1<br>TSIM SUBNETWORK | OUESTED 0             | *  |                  | TIME INTERVAL<br>NUMBER       |
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ALL EXISTING SUBNETWORKS REACHED EQUILIBRIUM

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| SECONDS                       |           |           |       |       |         |       |                |         |           |  |
|-------------------------------|-----------|-----------|-------|-------|---------|-------|----------------|---------|-----------|--|
| AVEDACE VALUES                | VE        | HICLE MIN | UTES  | RATIO | MINUTES | / KM  | <br> <br> <br> | SECONDS | / VEHICLE |  |
| STOP STOPS VOLUME SF          | LE MOVE   | DELAY     | TOTAL | MOVE/ | TOTAL   | DELAY | TOTAL          | DELAY   | QUEUE     |  |
| LINK KM TF<br>TIME (%) VPH KM | KIPS TIME | TIME      | TIME  | TOTAL | TIME    | TIME  | TIME           | TIME    | TIME      |  |
|                               |           |           |       |       |         |       |                |         |           |  |
| (8102, 102) 1<br>1510         | 1519      |           |       |       |         |       |                |         |           |  |
| (8103, 103)                   | 188       |           |       |       |         |       |                |         |           |  |

CUMULATIVE NETSIM STATISTICS AT TIME 13:30: 0

ELAPSED TIME IS 1: 0: 0 ( 3600 SECONDS),

TIME PERIOD 1 ELAPSED TIME IS 3600

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| 17.6           | 0.0           | 25.1   |               |                                       | 0.0    |      | 0.5    |      |        |    | 7.2    |      | 0.0    |      |        |    | 19.2   |      | 0.0   |      |        |     | 10.8   |      | 0.0    |      | 1.8    |      | 0.4    |      | 0.0    |      |
|----------------|---------------|--------|---------------|---------------------------------------|--------|------|--------|------|--------|----|--------|------|--------|------|--------|----|--------|------|-------|------|--------|-----|--------|------|--------|------|--------|------|--------|------|--------|------|
| 23.5           | 3.3           | 30.5   | ע<br>ר        | 0.0                                   | 0.8    |      | 2.9    |      |        |    | 9.9    |      | 2.4    |      |        |    | 20.8   |      | 1.8   |      |        |     | 12.9   |      | 0.7    |      | 3.8    |      | 1.8    |      | 3.3    |      |
| 34.7           | 14.5          | 40.0   | 131           | T • C T                               | 8.1    |      | 10.3   |      |        |    | 17.3   |      | 9.8    |      |        |    | 28.3   |      | 9.2   |      |        |     | 20.4   |      | 10.5   |      | 0.6    |      | 5.0    |      | 13.5   |      |
| 2.62           | 0.37          | 3.97   | 0 47          | · · · · · · · · · · · · · · · · · · · | 0.13   |      | 0.50   |      |        |    | 1.65   |      | 0.41   |      |        |    | 3.47   |      | 0.31  |      |        |     | 2.16   |      | 0.09   |      | 0.90   |      | 0.70   |      | 0.40   |      |
| 3.86           | 1.61          | 5.21   | 171           |                                       | 1.37   |      | 1.74   |      |        |    | 2.89   |      | 1.65   |      |        |    | 4.71   |      | 1.55  |      |        |     | 3.40   |      | 1.33   |      | 2.14   |      | 1.94   |      | 1.65   |      |
| 0.32           | 0.77          | 0.24   | 0 73          |                                       | 0.91   |      | 0.72   |      |        |    | 0.43   |      | 0.75   |      |        |    | 0.26   |      | 0.80  |      |        |     | 0.37   |      | 0.93   |      | 0.58   |      | 0.64   |      | 0.75   |      |
| 880.8          | 224.1         | 785.4  | 282.9         | <b>1</b> 01                           | 44.2   |      | 2.6    |      |        |    | 4.3    |      | 6.5    |      |        |    | 7.1    |      | 1.8   |      |        |     | 43.2   |      | 30.1   |      | 25.9   |      | 61.9   |      | 204.9  |      |
| 597.1          | 51.3          | 598.1  | 6 - 22        | 1                                     | 4.2    |      | 0.7    |      |        | ,  | 2.5    |      | 1.6    |      |        |    | 5.2    |      | 0.4   |      |        |     | 27.4   |      | 2.1    |      | 10.9   |      | 22.3   |      | 50.3   |      |
| 283.6          | 172.8         | 187.3  | 205.7         |                                       | 40.0   |      | 1.8    |      |        |    | 1.9    |      | 4.9    |      |        |    | 1.9    |      | 1.5   |      |        |     | 15.8   |      | 28.0   |      | 15.0   |      | 39.6   |      | 154.6  |      |
| 1522 $15.5$    | 930<br>37.2   | 1177   | 1293          | 35.1                                  | 327    | 43.7 | 15     | 34.5 | 15     |    | 15     | 20.8 | 40     | 36.3 | 15     |    | 15     | 12.7 | 12    | 38.7 | 126    |     | 127    | 17.6 | 172    | 45.0 | 172    | 28.0 | 742    | 30.9 | 606    | 36.4 |
| 228.24<br>1522 | 139.08<br>930 | 150.68 | 1177          | 1293                                  | 32.22  | 327  | 1.48   | 15   |        |    | 1.50   | 15   | 3.94   | 40   |        |    | 1.50   | 15   | 1.18  | 12   |        |     | 12.70  | 127  | 22.54  | 172  | 12.06  | 172  | 31.89  | 742  | 124.40 | 606  |
| 100)<br>59     | 102)<br>0     | 100)   | 75<br>103)    | 0                                     | 101)   | 0    | 106)   | 0    | 106)   |    | 108)   | 73   | 112)   | 0    | 112)   |    | 114)   | 100  | 120)  | 0    | 120)   |     | 122)   | 100  | 126)   | 0    | 204)   | 22   | 204)   | 4    | 202)   | 0    |
| (102,<br>16.9  | ( 100,        | ( 103, | 24.5<br>(100. | 0.0                                   | ( 100, | 0.0  | ( 108, | 0.0  | (8106, | CT | ( 106, | 7.2  | ( 114, | 0.0  | (8112, | 15 | ( 112, | 18.9 | (122, | 0.0  | (8120, | 126 | ( 120, | 10.6 | ( 125, | 0.0  | ( 126, | 1.8  | ( 200, | 0.2  | ( 204, | 0.0  |

|                       | 0.0          | 49.6   |      | 4.8          |              | 0.0     |            |    | 3.8   | •    | 0.0    | •    |        |     | 3.2   |      | 0.0    | •    |        |    | 3.5   | •         | 0.0   | )<br>•<br>• |        |    | 5.3   | )<br>• | 2.4    |      | 0.0    |      |
|-----------------------|--------------|--------|------|--------------|--------------|---------|------------|----|-------|------|--------|------|--------|-----|-------|------|--------|------|--------|----|-------|-----------|-------|-------------|--------|----|-------|--------|--------|------|--------|------|
|                       | 0.2          | 54.8   |      | 6.7          | 1            | 2.5     |            |    | 6.2   |      | 2.7    |      |        |     | 5.4   |      | 2.5    | •    |        |    | 6.1   | <br> <br> | 2.3   | •           |        |    | 7.1   |        | 5.1    |      | 1.1    |      |
|                       | 7.6          | 60.4   |      | 13.3         | (            | 9.8     |            |    | 13.7  |      | 10.0   | 1    |        |     | 12.9  |      | 6.6    |      |        |    | 13.6  |           | 9.6   |             |        |    | 14.6  |        | 10.8   |      | 4.6    |      |
|                       | 0.03         | 12.18  |      | 1.27         |              | 0.42    |            |    | 1.04  |      | 0.45   |      |        |     | 0.90  |      | 0.43   |      |        |    | 1.02  |           | 0.39  |             |        |    | 1.19  |        | 1.09   |      | 0.38   |      |
|                       | 1.27         | 13.43  |      | 2.51         | (<br>(<br>,  | 1.00    |            |    | 2.28  |      | 1.69   |      |        |     | 2.14  |      | 1.67   |      |        |    | 2.27  |           | 1.63  |             |        |    | 2.43  |        | 2.34   |      | 1.62   |      |
|                       | 0.98         | 0.09   |      | 0.50         |              | c/ • N  |            |    | 0.55  |      | 0.73   |      |        |     | 0.58  |      | 0.74   |      |        |    | 0.55  |           | 0.76  |             |        |    | 0.51  |        | 0.53   |      | 0.77   |      |
|                       | 106.2        | 764.1  |      | 15.7         | -<br>-       | 71.12   |            |    | 5.5   |      | 54.3   |      |        |     | 33.2  |      | 5.3    |      |        |    | 3.4   |           | 1.8   |             |        |    | 10.4  |        | 26.3   |      | 65.0   |      |
|                       | 2.1          | 693.3  |      | 7.9          | с<br>Ц       | с.<br>С |            |    | 2.5   |      | 14.4   |      |        |     | 14.0  |      | 1.4    |      |        |    | 1.5   |           | 0.4   |             |        |    | 5.1   |        | 12.3   |      | 15.3   |      |
|                       | 104.1        | 70.7   |      | 7.8          | 1<br>0<br>0  | 0.C1    |            |    | 3.0   |      | 39.9   |      |        |     | 19.3  |      | 3.9    |      |        |    | 1.9   |           | 1.3   |             |        |    | 5.3   |        | 14.0   |      | 49.8   |      |
| 837                   | 838<br>47.3  | 759    | 4.5  | 71           | دی. ۲<br>۲۵۵ | 36.1    | 24         |    | 24    | 26.3 | 326    | 35.5 | 156    |     | 155   | 28.0 | 32     | 35.9 | 15     |    | 15    | 26.5      | 11    | 36.8        | 43     |    | 43    | 24.7   | 146    | 25.7 | 853    | 36.9 |
|                       | 83.78<br>838 | 56.91  | 759  | 6.25<br>71   | 12 70        | 129     | )<br>]<br> |    | 2.40  | 24   | 32.09  | 326  |        |     | 15.50 | 155  | 3.15   | 32   |        |    | 1.50  | 15        | 1.08  | 11          |        |    | 4.30  | 43     | 11.26  | 146  | 40.04  | 853  |
| 202)                  | 206)<br>0    | 200)   | 86   | 208)         | 43           | 017     | 210)       |    | 212)  | 100  | 214)   | 0    | 214)   |     | 216)  | 100  | 220)   | 0    | 220)   |    | 222)  | 100       | 224)  | 0           | 224)   |    | 226)  | 100    | 310)   | 26   | 310)   | 0    |
| (8202 <b>,</b><br>837 | (202,<br>0.0 | ( 206, | 48.8 | (206,<br>, 7 | 4.1          | 0.0     | (8210,     | 24 | (210, | 3.7  | ( 216, | 0.0  | (8214, | 156 | (214, | 3.1  | ( 222, | 0.0  | (8220, | 15 | (220, | 3.5       | (226, | 0.0         | (8224, | 43 | (224, | 5.2    | ( 228, | 2.3  | ( 300, | 0.0  |

| 0.0    | •    |        |     | 0.3    |      | 8.5    | •    | 2.0    |      | 0.0    |      | 0.0    |      |
|--------|------|--------|-----|--------|------|--------|------|--------|------|--------|------|--------|------|
|        |      |        |     |        |      | С      |      |        |      |        |      |        |      |
| 3.0    |      |        |     | 0.8    |      | 42.9   |      | 4.0    |      | 1.3    |      | 4.1    |      |
| 10.4   |      |        |     | 8.3    |      | 46.0   |      | 8.5    |      | 4.8    |      | 19.0   |      |
| 0.50   |      |        |     | 0.14   |      | 17.39  |      | 1.11   |      | 0.44   |      | 0.34   |      |
| 1.74   |      |        |     | 1.38   |      | 18.63  |      | 2.35   |      | 1.68   |      | 1.59   |      |
| 0.71   |      |        |     | 0.90   |      | 0.07   |      | 0.53   |      | 0.74   |      | 0.78   |      |
| 173.7  |      |        |     | 94.1   |      | 407.1  |      | 21.6   |      | 73.2   |      | 335.2  |      |
| 49.7   |      |        |     | 9.6    |      | 379.9  |      | 10.2   |      | 19.2   |      | 72.5   |      |
| 124.0  |      |        |     | 84.5   |      | 27.2   |      | 11.4   |      | 54.0   |      | 262.6  |      |
| 966    | 34.5 | 681    |     | 680    | 43.4 | 531    | 3.2  | 153    | 25.5 | 908    | 35.6 | 1057   | 37.8 |
| 99.77  | 998  |        |     | 67.98  | 680  | 21.85  | 531  | 9.19   | 153  | 43.45  | 908  | 211.35 | 1057 |
| 302)   | 0    | 302)   |     | 304)   | ო    | 300)   | 81   | 306)   | 26   | 306)   | 0    | 308)   | 0    |
| ( 310, | 0.0  | (8302, | 681 | ( 302, | 0.3  | ( 304, | 37.9 | ( 304, | 2.0  | ( 300, | 0.0  | ( 306, | 0.0  |

AVERAGE QUEUE AND STOP TIME ARE COMPUTED AS TOTAL QUEUE TIME OR TOTAL STOP TIME DIVIDED BY TOTAL NUMBER OF VEHICLES DISCHARGED FROM LINK PLUS NUMBER OF VEHICLES CURRENTLY ON THE LINK.

|                   |       | VEHI | CLE MINU | JTES  | RATIO | MINUTES | / KM  |       | SECONDS / | / VEHICLE |  |
|-------------------|-------|------|----------|-------|-------|---------|-------|-------|-----------|-----------|--|
| AVERAGE VALUES    | ł     |      |          |       |       |         |       |       |           |           |  |
| VEH               | ICLE  | MOVE | DELAY    | TOTAL | MOVE/ | TOTAL   | DELAY | TOTAL | DELAY     | OUEUE     |  |
| STOP STOPS VOLUME | SPEED |      |          |       |       |         |       |       |           | 2         |  |
| LINK KM           | TRIPS | TIME | TIME     | TIME  | TOTAL | TIME    | TIME  | TIME  | TIME      | TIME      |  |
| TIME (%) VPH      | KMPH  |      |          |       |       |         |       |       |           |           |  |
|                   |       |      |          |       |       |         |       |       |           |           |  |
|                   |       |      |          |       |       |         |       |       |           |           |  |

TIME PERIOD 1 ELAPSED TIME IS 3600

CUMULATIVE NETSIM STATISTICS AT TIME 13:30: 0

ELAPSED TIME IS 1: 0: 0 ( 3600 SECONDS),

SECONDS

ч

| (8300, | 308) |        | 1581 |       |       |        |      |       |       |      |      |      |
|--------|------|--------|------|-------|-------|--------|------|-------|-------|------|------|------|
| 1581   |      |        |      |       |       |        |      |       |       |      |      |      |
| (308,  | 307) | 45.00  | 237  | 55.9  | 4.4   | 60.3   | 0.93 | 1.34  | 0.10  | 15.3 | 1.1  | 0.0  |
| 0.0    | 0    | 237    | 44.8 |       |       |        |      |       |       |      |      |      |
| (308,  | 300) | 322.36 | 1327 | 400.6 | 867.3 | 1267.9 | 0.32 | 3.93  | 2.69  | 57.3 | 39.2 | 31.9 |
| 31.3   | 79   | 1327   | 15.3 |       |       |        |      |       |       |      |      |      |
| ( 307, | 305) | 13.73  | 237  | 17.1  | 8.9   | 25.9   | 0.66 | 1.89  | 0.65  | 6.6  | 2.2  | 0.7  |
| 0.7    | 16   | 237    | 31.8 |       |       |        |      |       |       |      |      |      |
| ( 305, | 303) | 73.48  | 735  | 91.3  | 38.4  | 129.8  | 0.70 | 1.77  | 0.52  | 10.6 | 3.1  | 0.0  |
| 0.0    | 0    | 735    | 34.0 |       |       |        |      |       |       |      |      |      |
| (8301, | 303) |        | 644  |       |       |        |      |       |       |      |      |      |
| 644    |      |        |      |       |       |        |      |       |       |      |      |      |
| ( 303, | 301) | 64.38  | 644  | 80.0  | 29.6  | 109.6  | 0.73 | 1.70  | 0.46  | 10.2 | 2.8  | 1.9  |
| 1.8    | 10   | 644    | 35.2 |       |       |        |      |       |       |      |      |      |
| ( 301, | 300) | 22.13  | 600  | 27.5  | 409.4 | 436.9  | 0.06 | 19.74 | 18.50 | 43.7 | 40.9 | 37.4 |
| 36.8   | 72   | 600    | 3.0  |       |       |        |      |       |       |      |      |      |
| ( 300, | 305) | 12.45  | 498  | 15.5  | 8.1   | 23.6   | 0.65 | 1.90  | 0.65  | 2.8  | 1.0  | 0.0  |
| 0.0    | 0    | 498    | 31.6 |       |       |        |      |       |       |      |      |      |
| ( 301, | 227) | 1.88   | 47   | 2.3   | 3.4   | 5.8    | 0.40 | 3.07  | 1.83  | 7.4  | 4.4  | 2.8  |
| 2.8    | 25   | 47     | 19.5 |       |       |        |      |       |       |      |      |      |
| ( 311, | 309) | 0.61   | 8    | 0.8   | 0.2   | 0.9    | 0.80 | 1.55  | 0.31  | 7.1  | 1.4  | 0.0  |
| 0.0    | 0    | 8      | 38.7 |       |       | ,      |      |       |       |      |      |      |
| (8309, | 309) |        | 106  |       |       |        |      |       |       |      |      |      |
| 106    |      |        |      |       |       |        |      |       |       |      |      |      |
| (309,  | 311) | 8.27   | 106  | 10.3  | 14.9  | 25.2   | 0.41 | 3.04  | 1.80  | 14.3 | 8.4  | 6.5  |
| 6.5 1  | 00   | 106    | 19.7 |       |       |        |      |       |       |      |      |      |
| (315,  | 313) | 2.56   | 26   | 3.2   | 1.0   | 4.2    | 0.76 | 1.63  | 0.39  | 9.7  | 2.3  | 0.0  |
| 0.0    | 0    | 26     | 36.7 |       |       |        |      |       |       |      |      |      |
| (8313, | 313) |        | 15   |       |       |        |      |       |       |      |      |      |
| 15     |      |        |      |       |       |        |      |       |       |      |      |      |
| ( 313, | 315) | 1.50   | 15   | 1.9   | 1.6   | 3.4    | 0.54 | 2.29  | 1.05  | 13.7 | 6.3  | 4.3  |
| 4.3 1  | 00   | 15     | 26.2 |       |       |        |      |       |       |      |      |      |
| (218,  | 317) | 2.76   | 28   | 3.4   | 1.1   | 4.6    | 0.75 | 1.65  | 0.41  | 9.8  | 2.4  | 0.0  |
| 0.0    | 0    | 28     | 36.4 |       |       |        |      |       |       |      |      |      |
| (8317, | 317) |        | 15   |       |       |        |      |       |       |      |      |      |
| 15     |      |        |      |       |       |        |      |       |       |      |      |      |

,

| 7.4      | 0.0                           | 5.9               | 0.0                    | 7.9           | 0.0                     | 3.3               | 0.0                           | 7.0           | 5.6           | 0.0           | 0.0                            | 31.7           |
|----------|-------------------------------|-------------------|------------------------|---------------|-------------------------|-------------------|-------------------------------|---------------|---------------|---------------|--------------------------------|----------------|
| 9.5      | 2.0                           | 7.5               | 2.6                    | 9.6           | 2.2                     | 5.0               | 2.4                           | 11.2          | 8.8           | 0.6           | 0.8                            | 38.2           |
| 17.0     | е.<br>б                       | 14.9              | o.o                    | 17.1          | 9.6                     | 12.5              | 9.7                           | 18.6          | 16.8          | 4.6           | 4.5                            | 42.0           |
| 1.59     | 0.34                          | 1.25              | 0.43                   | 1.60          | 0.38                    | 0.84              | 0.41                          | 1.86          | 1.35          | 0.19          | 0.25                           | 12.75          |
| 2.83     | 1.58                          | 2.49              | 1.68                   | 2.85          | 1.62                    | 2.08              | 1.65                          | 3.10          | 2.59          | 1.43          | 1.49                           | 13.99          |
| 0.44     | 0.79                          | 0.50              | 0.74                   | 0.44          | 0.77                    | 0.60              | 0.75                          | 0.40          | 0.48          | 0.87          | 0.83                           | 0.09           |
| 4.3      | 0.9                           | 3.7               | 3.5                    | 4.3           | 4.6                     | 0.8               | 5.0                           | 114.8         | 76.2          | 119.5         | 136.0                          | 916.4          |
| 2.4      | 0.2                           | 1.9               | 0.0                    | 2.4           | 1.1                     | 0.3               | 1.2                           | 68.8          | 39.7          | 15.8          | 22.9                           | 835.0          |
| 1.9      | 0.7                           | 1.9               | 2.6                    | 1.9           | 3.5                     | 0.5               | 3.8                           | 46.0          | 36.5          | 103.7         | 113.1                          | 81.4           |
| 15<br>21 | 21.2<br>38.0<br>15            | 15<br>24 1        | 21<br>21<br>35.8<br>15 | 15<br>21.1    | 29<br>37.0              | 28.8              | 31<br>36.4<br>371             | 370<br>19.3   | 272<br>23.1   | 1547<br>41.9  | 1821<br>40.1<br>1317           | 1310<br>4.3    |
| 1.50     | L5<br>0.59<br>6               | 1.50              | 21.07                  | 1.50<br>15    | 2.85                    | 0.40<br>4         | 3.05<br>31                    | 36.99<br>370  | 29.35<br>272  | 83.46<br>1547 | 91.03<br>1821                  | 65.48<br>1310  |
| 218)     | 321)<br>0<br>321)<br>321)     | 323)<br>100       | 325)<br>0<br>325)      | 327)<br>100   | 329)<br>0<br>329)       | 331)<br>100       | 333)<br>0<br>333)             | 335)<br>100   | 205)<br>38    | 205)<br>0     | 201)<br>0<br>203)              | 275)<br>56     |
| ( 317,   | ,3<br>( 323,<br>0.0<br>(8321, | 1)<br>(321,<br>59 | (327,<br>0.0<br>(8325, | ( 325,<br>7.7 | ( 331,<br>0.0<br>(8329, | ;<br>(329,<br>3.0 | (335,<br>0.0<br>(8333,<br>371 | ( 333,<br>6.5 | ( 337,<br>5.3 | (200,<br>0.0  | (205,<br>0.0<br>(8201,<br>1317 | ( 203,<br>29.9 |

| 48.6      |      | 12.9      |      | 0.0       |      |           |    | 6.7       |      | 0.0      |      |           |     | 4.6      | 1    | 0.3         | )<br>•<br>• |
|-----------|------|-----------|------|-----------|------|-----------|----|-----------|------|----------|------|-----------|-----|----------|------|-------------|-------------|
| 53.6      |      | 18.4      |      | 2.5       |      |           |    | 8.8       |      | 2.3      |      |           |     | 8.8      |      | 3.4         |             |
| 56.2      |      | 22.1      |      | 9.8       |      |           |    | 16.3      |      | 9.7      |      |           |     | 16.2     |      | 15.0        |             |
| 25.49     |      | 6.27      |      | 0.42      |      |           |    | 1.47      |      | 0.40     |      |           |     | 1.47     |      | 0.37        |             |
| 26.74     |      | 7.51      |      | 1.66      |      |           |    | 2.71      |      | 1.64     |      |           |     | 2.71     |      | 1.61        |             |
| 0.05      |      | 0.17      |      | 0.75      |      |           |    | 0.46      |      | 0.76     |      |           |     | 0.46     |      | 0.77        |             |
| 833.2     |      | 154.0     |      | 15.2      |      |           |    | 10.3      |      | 18.2     |      |           |     | 85.3     |      | 443.0       |             |
| 794.4     |      | 128.5     |      | 3.9       |      |           |    | 5.6       |      | 4.4      |      |           |     | 46.1     |      | 101.6       |             |
| 38.7      |      | 25.5      |      | 11.4      |      |           |    | 4.7       |      | 13.8     |      |           |     | 39.1     |      | 341.5       |             |
| 889       | 2.2  | 418       | 8.0  | 93        | 36.1 | 38        |    | 38        | 22.1 | 113      | 36.6 | 315       |     | 315      | 22.2 | 1776        | 37.2        |
| 31.16     | 889  | 20.51     | 418  | 9.16      | 63   |           |    | 3.80      | 38   | 11.12    | 113  |           |     | 31.49    | 315  | 274.77      | 1776        |
| 275, 200) | 54   | 275, 207) | , 66 | 217, 215) | 0    | 215, 215) |    | :15, 217) | 100  | 25, 223) | 0    | (23, 223) |     | 23, 225) | 100  | .00, 104)   | 4           |
| ~         | 48.C | ~         | 11.7 | ~         | 0.0  | (82       | 38 | ~         | 6.6  | ~        | 0.0  | (82       | 315 | 2        | 4.4  | 、<br>(<br>1 | 0.2         |

\* AVERAGE QUEUE AND STOP TIME ARE COMPUTED AS TOTAL QUEUE TIME OR TOTAL STOP TIME DIVIDED BY TOTAL NUMBER OF VEHICLES DISCHARGED FROM LINK PLUS NUMBER OF VEHICLES CURRENTLY ON THE LINK.

TIME PERIOD 1 ELAPSED TIME IS 3600 CUMULATIVE NETSIM STATISTICS AT TIME 13:30: 0 ELAPSED TIME IS 1: 0: 0 ( 3600 SECONDS), SECONDS -

| | | ----- SECONDS / VEHICLE QUEUE DELAY TOTAL DELAY MINUTES / KM TOTAL RATIO MOVE/ TOTAL VEHICLE MINUTES DELAY MOVE SPEED VEHICLE -- AVERAGE VALUES --STOPS VOLUME STOP ı

| TIME           | ,<br>,<br>,<br>,<br>,           | 0.3            |          | 7.0         | 0.0    | •    | 0.0    |      | 0.0    | •    | 0.0    | •     | 0.6    |      | 38.5   |      | 0.0    | )<br>-<br>) | 0.0    | )<br>, | 0.1    | <br>•<br>• | 0.1    | <br> -<br> | 0.0    | )    | 0.0    | )<br>-<br>) | 1.8    | )<br>  | 33.3  |      |
|----------------|---------------------------------|----------------|----------|-------------|--------|------|--------|------|--------|------|--------|-------|--------|------|--------|------|--------|-------------|--------|--------|--------|------------|--------|------------|--------|------|--------|-------------|--------|--------|-------|------|
| TIME           | 1<br>1<br>1<br>1<br>1<br>1<br>1 | 4.4            | с с<br>С | 1.1         | 0.4    |      | 0.6    |      | 1.0    | •    | 1.7    | ,<br> | 2.4    | •    | 46.1   | 1    | 1.1    | <br>•<br>!  | 2.4    | •      | 3.6    |            | 1.3    | k<br>1     | 0.8    | •    | 1.4    | •<br>•<br>  | 4.1    | I<br>• | 37.9  |      |
| TIME           |                                 | 11.8           | ר<br>ז   |             | 5.6    |      | 8.9    |      | 16.0   |      | 20.6   | •     | 5.3    | )    | 58.0   | •    | 6.2    | <br>•       | 18.5   |        | 27.4   |            | 12.8   |            | 10.0   |      | 18.6   | 5<br>5      | 18.1   |        | 41.2  |      |
| TIME           |                                 | 0.75           | 0 53     | ••••        | 0.09   |      | 0.08   |      | 0.09   |      | 0.11   |       | 0.99   |      | 4.80   |      | 0.27   |             | 0.19   |        | 0.19   |            | 0.13   |            | 0.10   |      | 0.10   |             | 0.37   |        | 13.99 |      |
| TIME           |                                 | 2.00           | 77.1     | •           | 1.33   |      | 1.33   |      | 1.33   |      | 1.35   |       | 2.23   |      | 6.04   |      | 1.51   |             | 1.43   |        | 1.43   |            | 1.38   |            | 1.35   |      | 1.35   |             | 1.61   |        | 15.23 |      |
| TOTAL          |                                 | 0.62           | 070      | -           | 0.93   |      | 0.94   |      | 0.93   |      | 0.92   |       | 0.56   |      | 0.21   |      | 0.82   |             | 0.87   |        | 0.87   |            | 0.90   |            | 0.92   |      | 0.92   |             | 0.77   |        | 0.08  |      |
|                |                                 | 347.7          | 220.6    |             | 165.7  |      | 259.3  |      | 462.8  |      | 597.3  |       | 165.4  |      | 1601.2 |      | 122.1  |             | 389.8  |        | 532.5  |            | 209.8  |            | 163.5  |      | 297.4  |             | 298.2  |        | 587.6 |      |
| TIME           |                                 | 131.2          | 65.9     | )<br>-<br>- | 10.8   |      | 16.3   |      | 30.4   |      | 47.9   |       | 73.2   |      | 1271.9 |      | 21.8   |             | 50.6   |        | 70.1   |            | 20.5   |            | 12.7   |      | 23.2   |             | 67.9   |        | 539.7 |      |
| TIME           |                                 | 216.5          | 154.6    | )           | 154.9  |      | 243.0  |      | 432.4  |      | 549.3  |       | 92.2   |      | 329.3  |      | 100.3  |             | 339.2  |        | 462.4  |            | 189.3  |            | 150.8  |      | 274.3  |             | 230.3  |        | 47.9  |      |
| TRIPS<br>KMPH  |                                 | 1775<br>30 1   | 1775     | 33.8        | 1778   | 45.1 | 1748   | 45.2 | 1740   | 45.1 | 1741   | 44.4  | 1859   | 26.9 | 1656   | 9.9  | 1187   | 39.7        | 1263   | 42.0   | 1166   | 41.9       | 982    | 43.6       | 978    | 44.5 | 959    | 44.5        | 066    | 37.3   | 855   | 3.9  |
| KM<br>VPH      |                                 | 174.21<br>1775 | 124.44   | 1775        | 124.65 | 1778 | 195.53 | 1748 | 347.91 | 1740 | 442.04 | 1741  | 74.23  | 1859 | 264.99 | 1656 | 80.68  | 1187        | 272.94 | 1263   | 372.10 | 1166       | 152.35 | 982        | 121.32 | 978  | 220.69 | 959         | 185.28 | 066    | 38.57 | 855  |
| IK<br>(8)<br>- |                                 | 108)<br>0      | 110)     | 0           | 114)   | 0    | 116)   | 0    | 118)   | 0    | 122)   | 0     | 125)   | 4    | 200)   | 80   | 208)   | 0           | 212)   | 0      | 216)   | 0          | 218)   | 0          | 222)   | 0    | 226)   | 0           | 228)   | 10     | 300)  | 70   |
| LIN<br>TIME    | 1<br>1<br>1                     | ( 104,<br>0.0  | ( 108,   | 0.0         | ( 110, | 0.0  | ( 114, | 0.0  | ( 116, | 0.0  | ( 118, | 0.0   | ( 122, | 0.4  | ( 125, | 37.9 | ( 200, | 0.0         | ( 208, | 0.0    | (212,  | 0.1        | (216,  | 0.0        | (218,  | 0.0  | (222,  | 0.0         | (226,  | 1.6    | (228, | 32.7 |

| 0.0<br>0.0<br>0.0<br>0.0 | 1.9<br>1.5<br>0.7<br>2.1 | 16.8<br>11.6<br>5.5<br>16.7<br>15.3 | 0.16<br>0.19<br>0.18<br>0.15<br>0.20 | 1.40<br>1.43<br>1.42<br>1.39<br>1.44 | 0.88<br>0.87<br>0.87<br>0.89<br>0.86 | 405.5<br>279.7<br>128.6<br>390.5<br>363.8 | 46.7<br>37.2<br>16.3<br>41.3<br>50.8 | 358.8<br>242.5<br>112.3<br>349.1<br>312.9 | 1444 $42.7$ $1445$ $11445$ $41.9$ $1232$ $42.2$ $42.2$ $42.2$ $1405$ $1422$ $43.2$ $41.5$ | 73<br>11<br>93<br>37<br>37<br>37<br>37<br>37<br>32                    | 288.<br>1444<br>1445<br>1445<br>1392<br>1392<br>1392<br>1392<br>1392<br>1405<br>1405  | 213) 288.<br>0 1444<br>217) 195.<br>0 1445<br>219) 90.<br>0 1392<br>0 1392<br>0 1405<br>0 1405<br>0 1405<br>0 1422   |
|--------------------------|--------------------------|-------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|---|--------------------------------------|---|---|---|---|--|
| 1.8<br>1.0<br>1.9        |                          | 11.6<br>8.3<br>16.8                 | 0.23<br>0.16<br>0.16                 | 1.47<br>1.40<br>1.40                 | 0.85<br>0.89<br>0.88                 | 283.8<br>202.9<br>405.5                   |                                      | 43.7<br>23.2<br>46.7                      | 240.1 43.7<br>179.7 23.2<br>358.8 46.7  | 1474 240.1 43.7<br>40.8<br>1460 179.7 23.2<br>42.8<br>1444 358.8 46.7 | 193.19     1474     240.1     43.7       1474     40.8     144.63     1460     179.7     23.2       1460     42.8     1444     358.8     46.7 | 209)     193.19     1474     240.1     43.7       0     1474     40.8     211     144.63     1460     179.7     23.2       0     1460     42.8     46.7     213     288.73     1444     358.8     46.7 |
| 50.4<br>1.3              |                          | 57.1<br>4.3                         | 9.34<br>0.53                         | 10.58<br>1.78                        | 0.12<br>0.70                         | 1176.7<br>75.1                            |                                      | 1038.5<br>22.6                            | 138.2 1038.5<br>52.5 22.6   | 1237 138.2 1038.5<br>5.7<br>1059 52.5 22.6<br>33.8                    | 111.23 1237 138.2 1038.5<br>1237 5.7<br>42.28 1059 52.5 22.6<br>1059 33.8   | 200) 111.23 1237 138.2 1038.5<br>82 1237 5.7<br>207) 42.28 1059 52.5 22.6<br>0 1059 33.8   |
| 2.3                      |                          | 15.2                                | 0.22                                 | 1.46                                 | 0.85                                 | 376.2                                     | თ                                    | 55.                                       | 320.4 55.   | 43.0<br>1489 320.4 55.0<br>41 1                                       | 1139 43.0<br>257.79 1489 320.4 55.9<br>1489 41 1  | 337) 257.79 1489 320.4 55.4<br>1 1489 41 1   |
| 6.0                      |                          | 8.0                                 | 0.15                                 | 1.40                                 | 0.89                                 | 155.3                                     | 0                                    | 17.                                       | 138.3 17.   | 43.8<br>1159 138.3 17.  | 1186 43.8<br>111.28 1159 138.3 17.<br>1150 42.0   | U 1186 43.8<br>335) 111.28 1159 138.3 17.<br>0 1160 42.0   |
| 1.0                      |                          | 10.3                                | 0.13                                 | 1.37                                 | 0.91                                 | 203.1                                     | თ                                    | 18.                                       | 184.2 18.   | 43.4<br>1186 184.2 18.  | $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |
| 1.1                      |                          | 10.4                                | 0.14                                 | 1.38                                 | 0.90                                 | 207.5                                     | 0                                    | 21.                                       | 186.5 21.   | 44.0 1192 186.5 21.   | $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | 0 1183 44.0<br>327) 150.05 1192 186.5 21.  |
| 1.0                      |                          | 11.0                                | 0.12                                 | 1.36                                 | 0.91                                 | 216.4                                     | 2                                    | 19.                                       | 197.2 19.   | 43.3<br>1183 197.2 19.  | 1197 43.3<br>158.66 1183 197.2 19.  | 0 1197 43.3<br>323) 158.66 1183 197.2 19.  |
|                          |                          | 11.0                                | 0.14                                 | 1.38                                 | 0.90                                 | 220.3                                     | 9                                    | 22.                                       | 197.7 22.   | 42.7<br>1197 197.7 22.  | 1208 42.7<br>159.07 1197 197.7 22.  | 0 1208 42.7<br>218) 159.07 1197 197.7 22.  |
|                          | 1 ~-                     | 15.8                                | 0.16                                 | 1.41                                 | 0.88                                 | 317.8                                     | ი                                    | 36.                                       | 281.0 36.   | 42.5<br>1208 281.0 36.  | 1109 42.5<br>226.07 1208 281.0 36.  | 0 1109 42.5<br>315) 226.07 1208 281.0 36.  |
| 2.4                      |                          | 20.3                                | 0.17                                 | 1.41                                 | 0.88                                 | 375.3                                     | 2                                    | 44.                                       | 330.6 44.   | 33.9<br>1109 330.6 44.  | 1049 33.9<br>266.03 1109 330.6 44.  | 0 1049 33.9<br>311) 266.03 1109 330.6 44.  |
| 0.9                      |                          | 3.0                                 | 0.53                                 | 1.77                                 | 0.70                                 | 52.1                                      | ഹ                                    | 15.                                       | 36.6 15.  | 1049 36.6 15.   | 29.42 1049 36.6 15.   | 227) 29.42 1049 36.6 15.   |

| 20 00 1023 12.0<br>SUBNETWORK= 9437.64 8990 195.48 183.34 378.81 0.52 2.41 1.17 2.53 1.22 0.84<br>.82 132.7 24.9 | VEHICLE - HOURS ER  |
|--|---|
| 0°7 C70T 00 C°C  | SUBNETWORK= 9437.64 8990 195.48 183.34 378.81 0.52 2.41 1.17 2.53 1.22 0.84<br>.82 132.7 24.9 |

TRIP

CUMULATIVE NETSIM STATISTICS AT TIME 13:30: 0

ELAPSED TIME IS 1: 0: 0 ( 3600 SECONDS),

TIME PERIOD 1 ELAPSED TIME IS 3600

SECONDS

-

|                                       |                             |  |            | DI   | SCHARGE BY | LANE      |           |             |     |           |           |
|---------------------------------------|-----------------------------|--|------------|------|------------|-----------|-----------|-------------|-----|-----------|-----------|
| T ANF 6                               | T. Z                        | LANE                                       |            | LANE | 5 2        | LANE      | m         | LANE        | 4   | LANE      | 5         |
| LANE O<br>LINK<br>VEH VPH             | Ϋ́Ϋ́Ϋ́Ϋ́Ϋ́Ϋ́Ϋ́Ϋ́Ϋ́Ϋ́Ϋ́Ϋ́Ϋ́Υ | VEH<br>VEH<br>EH VF                        | HdA<br>HdA | VEH  | ЧРН        | VEH       | HdV       | VEH         | NPH | VEH       | ЧРН       |
| 1                                     |                             | <br> <br>                                  | <br> <br>  |      | <br> <br>  | <br> <br> | <br> <br> | 1<br>1<br>1 |     | <br> <br> | <br> <br> |
| 1                                     |                             |  |            |      |            |           |           |             |     |           |           |
| (102, 100)                            |                             | 254  | 254        | 384  | 384        | 0         | 0         | 0           | 0   | 0         | 0         |
| 0 0<br>(100,102)                      | 884                         | $\begin{array}{c} 884\\ 118\\ \end{array}$ | 118        | 341  | 341        | 471       | 471       | 0           | 0   | 0         | 0         |
| 0 0<br>(103,100)                      |                             | 23<br>0                                    | 23         | 464  | 464        | 416       | 416       | 274         | 274 | 0         | 0         |
| ( 100, 103)                           | -                           | 397<br>0                                   | 397        | 473  | 473        | 423       | 423       | 0           | 0   | 0         | 0         |
| ( 100, 101)                           | ⊃ (                         | 101<br>101                                 | 101        | 226  | 226        | 0         | 0         | 0           | 0   | 0         | 0         |
| 0 0<br>(108,106)                      |                             | 15<br>15                                   | 15         | 0    | 0          | 0         | 0         | 0           | 0   | 0         | 0         |
| 0 0<br>(106,108)                      |                             | 15 0                                       | 15         | 0    | 0          | 0         | 0         | 0           | 0   | 0         | 0         |
|                                       |                             | 40 0                                       | 40         | 0    | 0          | 0         | 0         | 0           | 0   | 0         | 0         |
|                                       |                             | 15 0                                       | 15         | 0    | 0          | 0         | 0         | 0           | 0   | 0         | 0         |
| ( 122, 120)                           |                             | 12 0                                       | 12         | 0    | 0          | 0         | 0         | 0           | 0   | 0         | 0         |
| ( 120, 122)                           |                             | 127  | 127        | 0    | 0          | 0         | 0         | 0           | 0   | 0         | 0         |
| (125,126)                             |                             | 172  | 172        | 0    | 0          | 0         | 0         | 0           | 0   | 0         | 0         |
| ( 126, 204)                           | 5 C                         | 172  | 172        | 0    | 0          | 0         | 0         | 0           | 0   | 0         | 0         |
| 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 0                           | 0<br>88<br>0                               | 88         | 192  | 192        | 462       | 462       | 0           | 0   | 0         | 0         |
|                                       |                             |  |            |      |            |           |           |             |     |           |           |
| 0         | 0                | 0         | 0              | 0         | 0         | 0         | 0            | 0                | 0         | 0         | 0          | 0              | 0              | 0         | 0                | 0          | 0              |
|-----------|------------------|-----------|----------------|-----------|-----------|-----------|--------------|------------------|-----------|-----------|------------|----------------|----------------|-----------|------------------|------------|----------------|
| 0         | 0                | 0         | 0              | 0         | 0         | 0         | 0            | 0                | 0         | 0         | 0          | 0              | 0              | 0         | 0                | 0          | 0              |
| 0         | 0                | 176       | 0              | 0         | 0         | 0         | 0            | 0                | 0         | 0         | 0          | 0              | 0              | 0         | 0                | 0          | 0              |
| 0         | 0                | 176       | 0              | 0         | 0         | 0         | 0            | 0                | 0         | 0         | 0          | 0              | 0              | 0         | 0                | 0          | 0              |
| 336       | 423              | 205       | 0              | 0         | 0         | 0         | 0            | 0                | 0         | 0         | 0          | 0              | 466            | 385       | 294              | 242        | 0              |
| 336       | 423              | 205       | 0              | 0         | 0         | 0         | 0            | 0                | 0         | 0         | 0          | 0              | 466            | 385       | 294              | 242        | 0              |
| 309       | 386              | 216       | 0              | 0         | 0         | 0         | 0            | 0                | 0         | 0         | 0          | 0              | 273            | 343       | 347              | 180        | 0              |
| 309       | 386              | 216       | 0              | 0         | 0         | 0         | 0            | 0                | 0         | 0         | 0          | 0              | 273            | 343       | 347              | 180        | 0              |
| 264       | 29               | 162       | 71             | 129       | 24        | 326       | 155          | 32               | 15        | 11        | 43         | 146            | 114            | 270       | 39               | 109        | 153            |
| 264       | 0<br>5<br>0<br>0 | 0 162     | , 71<br>0      | 129       | 0 54 0    | 326       | 0 155<br>0 0 | 32 0             | 15        | 11        | 43         | 0 146<br>0 146 |                | 270       | 2<br>2<br>3<br>0 | 0 109 0    | 0 153<br>0 0 0 |
| 204, 202) | 202, 206)        | 206, 200) | 206, 208)<br>0 | 212, 210) | 210, 212) | 216, 214) | 214, 216)    | 222, 220)        | 220, 222) | 226, 224) | 224, 226)  | 228, 310)<br>0 | 300, 310)<br>0 | 310, 302) | 302, 304)        | 304, 300)  | 304, 306)<br>0 |
| $\sim c$  |                  | , – c     | , – с          | , – с     |           | ,~~ <     | , – с        | , <del>-</del> c |           |           | , <u> </u> |                | , ~ 0          | , – c     | , – c            | <u>م</u> ر | 0 - 0          |

| 0                 | 0                 | 0                | 0                 | 0                 | 0                 | 0          | 0         | 0         | 0           | 0                | 0           | 0         | 0    | 0         | 0         | 0           | 0                |
|-------------------|-------------------|------------------|-------------------|-------------------|-------------------|------------|-----------|-----------|-------------|------------------|-------------|-----------|------|-----------|-----------|-------------|------------------|
| 0                 | 0                 | 0                | 0                 | 0                 | 0                 | 0          | 0         | 0         | 0           | 0                | 0           | 0         | 0    | 0         | 0         | 0           | 0                |
| 0                 | 0                 | 0                | 0                 | 0                 | 0                 | 0          | 0         | 0         | 0           | 0                | 0           | 0         | 0    | 0         | 0         | 0           | 0                |
| 0                 | 0                 | 0                | 0                 | 0                 | 0                 | 0          | 0         | 0         | 0           | 0                | 0           | 0         | 0    | 0         | 0         | 0           | 0                |
| 409               | 355               | 0                | 415               | 0                 | 205               | 319        | 277       | 209       | 0           | 0                | 0           | 0         | 0    | 0         | 0         | 0           | O                |
| 409               | 355               | 0                | 415               | 0                 | 205               | 319        | 277       | 209       | 0           | 0                | 0           | O         | 0    | 0         | 0         | 0           | 0                |
| 301               | 353               | 0                | 446               | 0                 | 186               | 305        | 210       | 180       | 0           | 0                | 0           | 0         | 0    | 0         | 0         | 0           | 0                |
| 301               | 353               | 0                | 446               | 0                 | 186               | 305        | 210       | 180       | 0           | 0                | 0           | 0         | 0    | 0         | 0         | 0           | 0                |
| 1 98              | 349               | 237              | 466               | 237               | 344               | 20         | 113       | 109       | 47          | 8                | 106         | 26        | 15   | 28        | 15        | 9           | 15               |
| 198<br>0          | 349               | 237              | 466<br>0          | 237               | 344               | 20         | 113       | 109       | 47          | ີຜິ              | 106<br>106  | 26<br>2   | 12 O | 58 °      | 15 0      | ک د         | 15<br>0          |
| C                 |                   |                  |                   |                   |                   |            |           |           | > (         |                  | 5 (         | > 0       | э с  |           |           |             | 0 0              |
| (300, 306)<br>0 0 | (306, 308)<br>0 0 | (308,307)<br>0 0 | (308, 300)<br>0 0 | (307, 305)<br>0 0 | (305, 303)<br>0 0 | (303, 301) | (301,300) | (300,305) | ( 301, 227) | 0 0<br>(311,309) | ( 309, 311) | (315,313) |      | (218,317) | (317,218) | ( 323, 321) | (321,323)<br>000 |

| 0          | 0                | 0                | 0                | 0         | 0         | 0         | 0         | 0         | 0         | 0                        | 0         | 0         | 0          | 0         | 0         | 0    | 0                |
|------------|------------------|------------------|------------------|-----------|-----------|-----------|-----------|-----------|-----------|--------------------------|-----------|-----------|------------|-----------|-----------|------|------------------|
| 0          | 0                | 0                | 0                | 0         | 0         | 0         | 0         | 0         | 0         | 0                        | 0         | 0         | 0          | 0         | 0         | 0    | 0                |
| 0          | 0                | 0                | 0                | 0         | 0         | 0         | 0         | 0         | 0         | 0                        | 0         | 0         | 0          | 0         | 0         | 50   | 0                |
| 0          | 0                | 0                | 0                | 0         | 0         | 0         | 0         | 0         | 0         | 0                        | 0         | 0         | 0          | 0         | 0         | 50   | 0                |
| 0          | 0                | 0                | 0                | 0         | 0         | 0         | 666       | 665       | 625       | 244                      | 0         | 0         | 0          | 0         | 0         | 563  | 210              |
| 0          | 0                | 0                | 0                | 0         | 0         | 0         | 666       | 665       | 625       | 244                      | 0         | 0         | 0          | 0         | 0         | 563  | 210              |
| 0          | 0                | 0                | 0                | 0         | 0         | 0         | 715       | 705       | 450       | 192                      | 0         | 0         | 0          | 0         | 0         | 1163 | 668              |
| 0          | 0                | 0                | 0                | 0         | 0         | 0         | 715       | 705       | 450       | 192                      | 0         | 0         | 0          | 0         | 0         | 1163 | 668              |
| 21         | 15               | 29               | Ą                | 31        | 370       | 272       | 166       | 451       | 235       | 88                       | 418       | 93        | 38         | 113       | 315       | 0    | 897              |
| 21         | 15               | 29               | <b>4</b>         | 31,0      | 370       | 272       | 166       | 451       | 235<br>0  | 88<br>86                 | 418       | 63<br>63  | 38 0<br>38 | 113       | 315       | 00   | 0<br>0           |
|            | 0 0              |                  |                  |           |           |           | ) c       |           |           | о<br>С                   |           |           |            |           |           |      | 0                |
| (327, 325) | 0 0<br>(325,327) | (331,329)<br>0 0 | (329,331)<br>000 | (335,333) | (333,335) | (337,205) | (200,205) | (205,201) | (203,275) | (275, 200)<br>(275, 200) | (275,207) | (217,215) | (215,217)  | (225,223) | (223,225) |      | (104,108)<br>0 0 |

| 0         | 0             | 0                  | 0                | 0                  | 0                | 0                 | 0         | 0           | 0          | 0          | 0         | 0         | 0                | 0                 | 0           | 0                | 0                |
|-----------|---------------|--------------------|------------------|--------------------|------------------|-------------------|-----------|-------------|------------|------------|-----------|-----------|------------------|-------------------|-------------|------------------|------------------|
| 0         | 0             | 0                  | 0                | 0                  | 0                | 0                 | 0         | 0           | 0          | 0          | 0         | 0         | 0                | 0                 | 0           | 0                | 0                |
| 0         | 0             | 0                  | 0                | 0                  | 0                | 509               | 0         | 0           | 0          | 0          | 0         | 0         | 0                | 0                 | 0           | 0                | 0                |
| 0         | 0             | 0                  | 0                | 0                  | 0                | 509               | 0         | 0           | 0          | 0          | 0         | 0         | 0                | 0                 | 0           | 0                | 0                |
| 210       | 212           | 232                | 289              | 339                | 1199             | 182               | 534       | 463         | 348        | 322        | 322       | 302       | 415              | 350               | 206         | 297              | 317              |
| 210       | 212           | 232                | 289              | 339                | 1199             | 182               | 534       | 463         | 348        | 322        | 322       | 302       | 415              | 350               | 206         | 297              | 317              |
| 665       | 690           | 725                | 740              | 746                | 575              | 323               | 514       | 462         | 345        | 349        | 332       | 339       | 494              | 309               | 378         | 353              | 368              |
| 665       | 069           | 725                | 740              | 746                | 575              | 323               | 514       | 462         | 345        | 349        | 332       | 339       | 494              | 309               | 378         | 353              | 368              |
| 006       | 876           | 791                | 711              | 656                | 85               | 115               | 139       | 338         | 473        | 311        | 324       | 318       | 81               | 196               | 465         | 459              | 523              |
| 006       | 0<br>876<br>0 | 791                | 711              | 656<br>0           | 85<br>0          | 115               | 139       | 338         | 473        | 311        | 324       | 318       | 810              | 196               | 465         | 459              | 523<br>0         |
| c         |               |                    |                  |                    |                  | с.<br>2           | 1 0       |             |            |            |           |           |                  |                   |             |                  | > 0              |
| (108,110) |               | ( 114, 116)<br>0 0 | (116,118)<br>0 0 | ( 118, 122)<br>0 0 | (122,125)<br>0 0 | (125, 200)<br>0 0 | (200,208) | ( 208, 212) | (212, 216) | (216, 218) | (218,222) | (222,226) | (226,228)<br>0 0 | (228, 300)<br>0 0 | ( 300, 227) | (227,311)<br>0 0 | (311,315)<br>0 0 |

| 0                | 0                 | 0                | 0                | 0                      | 0                      | 0          | 0           | 0           | 0           | 0          | 0          | 0         | 0         | 0         | 0                       |
|------------------|-------------------|------------------|------------------|------------------------|------------------------|------------|-------------|-------------|-------------|------------|------------|-----------|-----------|-----------|-------------------------|
| 0                | 0                 | 0                | 0                | 0                      | 0                      | 0          | 0           | 0           | 0           | 0          | 0          | 0         | 0         | 0         | 0                       |
| 0                | 0                 | 0                | 0                | 0                      | 0                      | 0          | 0           | 0           | 0           | 0          | 0          | 0         | 0         | 0         | 558                     |
| 0                | 0                 | 0                | 0                | 0                      | 0                      | 0          | 0           | 0           | 0           | 0          | 0          | 0         | 0         | 0         | 558                     |
| 332              | 340               | 342              | 331              | 333                    | 650                    | 307        | 409         | 398         | 394         | 374        | 386        | 384       | 389       | 476       | 438                     |
| 332              | 340               | 342              | 331              | 333                    | 650                    | 307        | 409         | 398         | 394         | 374        | 386        | 384       | 389       | 476       | 438                     |
| 372              | 382               | 382              | 383              | 397                    | 670                    | 330        | 396         | 470         | 480         | 517        | 506        | 517       | 519       | 645       | 256                     |
| 372              | 382               | 382              | 383              | 397                    | 670                    | 330        | 396         | 470         | 480         | 517        | 506        | 517       | 519       | 645       | 256                     |
| 493              | 461               | 468              | 472              | 429                    | 169                    | 254        | 254         | 606         | 586         | 553        | 553        | 491       | 497       | 301       | 373                     |
| 493<br>0         | 461<br>0          | 468<br>0         | 472<br>0         | 429                    | 169                    | 254<br>276 | 254<br>254  | 606<br>0    | 586         | 553        | 553<br>0   | 491       | 497       | 301       | 0<br>373<br>0           |
| C                |                   |                  | ) C              |                        |                        | 246        |             |             |             |            |            |           |           |           | 0 0                     |
| (315,218)<br>0 0 | (218, 323)<br>0 0 | (323,327)<br>0 0 | (327,331)<br>000 | (331,335)<br>(331,335) | (335,337)<br>(335,337) | (337,200)  | ( 200, 207) | ( 207, 209) | ( 209, 211) | (211, 213) | (213, 217) | (217,219) | (219,221) | (221,225) | 0 0<br>(225,100)<br>0 0 |

## NETSIM PERSON MEASURES OF EFFECTIVENESS

| TRAVEL TIME           | LINK        | PERSON | PERSON | регат      |
|-----------------------|-------------|--------|--------|------------|
| PERSON-MIN            |             | KM     | TRIPS  | PERSON-MIN |
|                       | (102, 100)  | 296.4  | 1976.4 | 775.4      |
| 1140.7<br>201 3       | (100, 102)  | 180.8  | 1208.9 | 66.7       |
| C.1C2                 | (103, 100)  | 195.7  | 1528.9 | 776.9      |
| 2.0201<br>267 E       | (100, 103)  | 215.0  | 1679.7 | 100.3      |
| 001.00<br>L           | (100, 101)  | 41.8   | 424.6  | 5.4        |
|                       | (108, 106)  | 1.9    | 19.5   | 1.0        |
| ני נ <u>י</u><br>די א | (106, 108)  | 1.9    | 19.5   | 3.2        |
| о<br>о<br>о           | ( 114, 112) | 5.1    | 52.0   | 2.1        |
| n                     | ( 112, 114) | 1.9    | 19.5   | 6.8        |
| · · ·                 | (122, 120)  | 1.5    | 15.6   | 0.5        |
| ۰. م<br>م             | (120,122)   | 16.5   | 165.1  | 35.6       |
| 39.1                  | (125, 126)  | 29.3   | 223.6  | 2.7        |

|        | 126,<br>200, | 204)<br>204) | 15.7<br>41.4<br>161 6 | 223.6<br>963.5 | 14.1<br>29.0 |
|--------|--------------|--------------|-----------------------|----------------|--------------|
|        | 202,         | 206)         | 108.9                 | 1088.8         | 2.8          |
| ~ ~    | 206,<br>206, | 200)<br>208) | 73.9<br>8.1           | 986.2<br>92.2  | 00.9<br>10.3 |
| $\sim$ | 212,         | 210)         | 16.5                  | 167.7          | 6.9          |
| ~      | 210,         | 212)         | 3.1                   | 31.2           | 3.2          |
|        | 216,         | 214)         | 41.7                  | 423.2          | 18.7         |
|        | 214,         | 216)         | 20.1                  | 201.5          | 18.2         |
|        | 222,         | 220)         | 4.1                   | 41.6           | 1.8          |
|        | 220,         | 222)         | 1.9                   | 19.5           | 2.0          |
|        | 226,         | 224)         | 1.4                   | 14.3           | 0.5          |
|        | 224,         | 226)         | 5.6                   | 55.9           | 6.6          |
|        | 228,         | 310)         | 14.6                  | 189.6          | 16.0         |
| -      | 300,         | 310)         | 52.0                  | 1108.3         | 19.8         |
| $\sim$ | 310,         | 302)         | 129.6                 | 1296.6         | 64.6         |
| $\sim$ | 302,         | 304)         | 88.3                  | 883.3          | 12.5         |
|        |              |              |                       |                |              |

| 520 Q          | ( 304, | 300) | 28.4            | 689.9                 | 493.6     |
|----------------|--------|------|-----------------|-----------------------|-----------|
| 6.020          | ( 304, | 306) | 11.9            | 198.6                 | 13.3      |
| 20.1<br>95.0   | ( 300, | 306) | 56.4            | 1179.2                | 24.9      |
|                |        |      |                 |                       |           |
| 1              |        |      | NETSIM PERSON N | 4EASURES OF EFFECTIVE | NESS      |
| TRAVEL TIME    | LII    | NK   | PERSON          | PERSON                | DELAY     |
| PERSON-MIN     |        |      | KM              | TRIPS                 | ERSON-MIN |
| 10E 0          | ( 306, | 308) | 274.5           | 1372.6                | 94.2      |
|                | ( 308, | 307) | 58.5            | 308.0                 | 5.7       |
| 10.47 A        | ( 308, | 300) | 418.9           | 1724.4                | 1127.0    |
| 10#/.0<br>22 7 | ( 307, | 305) | 17.8            | 308.0                 | 11.5      |
| 160 6          | ( 305, | 303) | 95.5            | 954.8                 | 49.9      |
| 140.0          | ( 303, | 301) | 83.6            | 836.4                 | 38.5      |
| 146.1<br>567 5 | ( 301, | 300) | 28.7            | 779.3                 | 531.7     |
|                | ( 300, | 305) | 16.2            | 646.8                 | 10.6      |
|                | ( 301, | 227) | 2.4             | 61.0                  | 4.5       |
| 1.2            | ( 311, | 309) | 0.8             | 10.4                  | 0.2       |

|     | 7 7 7            | (309, 311)  | 10.  | 8 | 137.8  | 19.4   |
|-----|------------------|-------------|------|---|--------|--------|
|     |                  | (315, 313)  | 3.   | Э | 33.8   | 1.3    |
|     | r                | (313, 315)  | 1.   | 6 | 19.5   | 2.0    |
|     | с с<br>т         | (218, 317)  | З.   | 6 | 36.4   | 1.5    |
|     | с и<br>          | (317, 218)  | 1.   | 6 | 19.5   | 3.1    |
|     |                  | (323, 321)  | 0.   | 8 | 7.8    | 0.3    |
|     | 2.T              | (321, 323)  | 1.   | 6 | 19.5   | 2.4    |
|     |                  | (327,325)   | 2.   | 7 | 27.2   | 1.2    |
|     | י<br>י<br>ני     | (325, 327)  | 1.   | 6 | 19.5   | 3.1    |
|     |                  | (331, 329)  | з.   | 7 | 37.7   | 1.4    |
|     |                  | (329, 331)  | 0.   | 5 | 5.2    | 0.4    |
|     | ין די<br>די ע    | ( 335, 333) | 4.   | 0 | 40.2   | 1.6    |
|     |                  | (333, 335)  | 48.  | 1 | 481.0  | 89.4   |
|     | 7.0ET            | (337, 205)  | 38.  | 2 | 353.6  | 51.6   |
|     | 15.0             | (200,205)   | 108. | 4 | 2009.6 | 20.5   |
|     | 2.001<br>7 AFL   | (205, 201)  | 118. | 3 | 2365.8 | 29.8   |
|     | 1,0.,/<br>1190 2 | (203,275)   | 85.  | 0 | 1701.4 | 1084.5 |
|     | 1081.7           | ( 275, 200) | 40.  | 2 | 1154.2 | 1031.4 |
| 210 |                  |             |      |   |        |        |

|                           | (275, 207)  | 26.7     | 543.1                | 167.0        |
|---------------------------|-------------|----------|----------------------|--------------|
| 10001                     | (217,215)   | 11.9     | 120.8                | 5.0          |
| 1.0                       | (215,217)   | 4.9      | 49.4                 | 7.3          |
| 23.7                      | (225,223)   | 14.5     | 146.8                | 5.7          |
|                           |             |          |                      |              |
| 1                         |             | NETSIM I | PERSON MEASURES OF E | FFECTIVENESS |
| TATE TOTAGE               | LINK        | PERSON   | PERSON               | DELAY        |
| IKAVEL IIME<br>PERSON-MIN |             | KM       | TRIPS                | PERSON-MIN   |
|                           | (223,225)   | 40.9     | 409.3                | 60.0         |
| 110.0<br>575 A            | (100, 104)  | 356.9    | 2306.6               | 131.9        |
| 515.4<br>AF1 6            | (104, 108)  | 226.3    | 2305.3               | 170.4        |
| 0.104<br>202 5            | ( 108, 110) | 161.6    | 2305.4               | 85.6         |
| 200.J                     | (110, 114)  | 161.9    | 2309.3               | 14.1         |
| C.U.2                     | ( 114, 116) | 254.0    | 2270.3               | 21.2         |
|                           | (116, 118)  | 451.9    | 2259.9               | 39.5         |
| 1.100                     | (118, 122)  | 574.1    | 2261.1               | 62.3         |
|                           |             |          |                      |              |

|                 | ( 122, | 125) | 96.4  | 2414.5 | 95.1   |
|-----------------|--------|------|-------|--------|--------|
| 2.14.Y          | ( 125, | 200) | 344.1 | 2150.6 | 1651.7 |
| 2019.4<br>160 F | (200,  | 208) | 104.8 | 1541.2 | 28.3   |
| L 20. J         | ( 208, | 212) | 354.4 | 1639.9 | 65.7   |
| 200.I<br>601 3  | (212,  | 216) | 483.1 | 1513.7 | 91.0   |
|                 | (216,  | 218) | 197.8 | 1275.1 | 26.6   |
| 4.712<br>c ctc  | (218,  | 222) | 157.5 | 1269.9 | 16.5   |
| د 212.<br>200   | ( 222, | 226) | 286.6 | 1245.3 | 30.1   |
| 2.00C<br>C Foc  | ( 226, | 228) | 240.6 | 1285.6 | 88.2   |
| 2.100           | ( 228, | 300) | 50.1  | 1110.3 | 700.8  |
| 0.601           | ( 300, | 227) | 38.2  | 1363.1 | 20.2   |
|                 | ( 227, | 311) | 345.7 | 1441.0 | 58.1   |
| 401.7<br>413 D  | ( 311, | 315) | 293.8 | 1569.7 | 47.9   |
| 586.2           | ( 315, | 218) | 206.7 | 1555.4 | 29.3   |
| 200.2           | (218,  | 323) | 206.2 | 1537.2 | 25.0   |
| 2.102           | ( 323, | 327) | 195.0 | 1548.9 | 27.3   |
| 0.002           | ( 327, | 331) | 192.6 | 1541.2 | 24.5   |
| 201.9           | ( 331, | 335) | 144.6 | 1506.1 | 22.1   |

| 180.0                               | ( 335,     | 337)          | 335.0                | 1935.2                 | 72.6                   |
|-------------------------------------|------------|---------------|----------------------|------------------------|------------------------|
| 1520.2                              | ( 337,     | 200)          | 144.5                | 1607.6                 | 1349.6                 |
| 2.020T                              | ( 200,     | 207)          | 55.0                 | 1376.5                 | 29.4                   |
| 360 0                               | ( 207,     | 209)          | 251.1                | 1915.7                 | 56.8                   |
| 200.0<br>263 0                      | ( 209,     | 211)          | 188.0                | 1897.5                 | 30.2                   |
|                                     | (211,      | 213)          | 375.2                | 1876.7                 | 60.7                   |
| 26.1.0<br>26.2 E                    | ( 213,     | 217)          | 253.6                | 1878.0                 | 48.4                   |
| 163.1<br>167.1                      | (217,      | 219)          | 117.5                | 1809.2                 | 21.2                   |
| 10.1 E                              | (219,      | 221)          | 365.1                | 1826.1                 | 53.7                   |
|                                     | ( 221,     | 225)          | 327.3                | 1848.2                 | 66.0                   |
| 4/2.0<br>1309.0                     | ( 225,     | 100)          | 278.7                | 2111.9                 | 962.6                  |
|                                     |            |               |                      |                        |                        |
| 1 *** NOTE ***<br>OF TIME PERIOD 1. | TNEY JANTT | OD I SPECIFIC | NETSIM STATISTICS AR | KE THE SAME AS CUMULAT | TIVE OUTPUT AT THE END |
|                                     |            |               |                      |                        |                        |
| 1                                   |            |               | NETSIM MOVEMENT S    | PECIFIC STATISTICS -   | TABLE I                |
|                                     |            |               |                      |                        |                        |

0 LINK STOPS (PCT) 213

SPEED (KMPH)

VEHICLE-TRIPS

VEHICLE-KM

| LEFT | THRU                       | LE<br>RIGHT   | ΕT | THRU    | RIGHT       | LEFT | THRU         | RIGHT | LEFT   | THRU | RIGH' |
|------|----------------------------|---------------|----|---------|-------------|------|--------------|-------|--------|------|-------|
|      | (8102, 102)<br>(8103, 103) |               |    |         |             | 00   | 1519<br>1188 | 00    |        |      |       |
|      | (102, 100)                 | 92.           | 08 | 3.60    | 132.57      | 614  | 24           | 884   | 10.1   | 10.3 | 25.4  |
| 85.8 | ( 100, 102)                | 41.2          | 00 | 139.08  | 0.00        | 0    | 930          | 0     | 0.0    | 37.2 | 0.0   |
| 0.0  | 0.0                        | 0.0           | 0  | 11.7 CE | r<br>c      |      |              | ç     |        | . L. |       |
| 77.0 | 1 76.6                     | , 30.4        | 00 | C0.211  | 6.34        | 517  | 880          | 23    | 10.9   | C.11 | . O S |
|      | (100, 103)                 | .00           | 00 | 165.53  | 0.00        | 0    | 1293         | 0     | 0.0    | 35.1 | 0.0   |
|      | ( 100, 101)                | ) (           | 00 | 32.22   | 00.00       | 0    | 327          | 0     | 0.0    | 43.7 | 0.0   |
| 0.0  | 0.0<br>(108, 106)          | 0.0           | 00 | 1.48    | 0.00        | 0    | 15           | 0     | 0.0    | 34.5 | .0    |
| 0.0  | 0.0                        | 0.0           |    |         |             |      |              |       |        |      |       |
|      | (8106, 106)                |               | 0  |         | 1.<br>C T   | 00   | 15           | 0 4   | c      | c    | Ċ     |
| 0.0  | 0.0<br>1 0.0               | 73.3 U.       | 00 | 00.0    | 00.1        | 5    | 5            | CT    | 0.0    | 0.0  | 20.2  |
|      | (114, 112)                 | ) 0.          | 00 | 3.94    | 0.00        | 0    | 40           | 0     | 0.0    | 36.3 | 0.0   |
| 0.0  | 0.0                        | 0.0           |    |         |             |      |              |       |        |      |       |
|      | (8112, 112)                |               | 6  |         | 0<br>1<br>1 | 0    | 15           | 0     |        |      |       |
|      | (112, 114)                 | ) 0.<br>100 0 | 00 | 0.00    | 1.50        | 0    | 0            | 15    | 0.0    | 0.0  | 12.   |
| •    | ( 122, 120)                | ) 0.          | 00 | 1.18    | 0.00        | 0    | 12           | 0     | 0.0    | 38.7 | 0.0   |
| 0.0  | 0.0                        | 0.0           |    |         |             |      |              |       |        |      |       |
|      | (8120, 120)                | -             |    |         |             | 0    | 126          | 0     |        |      |       |
|      | (120, 122)                 | .0.           | 00 | 0.00    | 12.70       | 0    | 0            | 127   | 0.0    | 0.0  | 17.0  |
| 0.0  | 0.0                        | 100.0         |    |         |             |      |              |       |        |      |       |
|      | (125, 126)                 | .0.           | 00 | 22.54   | 0.00        | 0    | 172          | 0     | 0.0    | 45.0 | 0.0   |
| 0.0  | 0.0                        | 0.0           |    |         |             |      |              |       |        |      |       |
| ,    | (126, 204)                 | 0.            | 00 | 12.06   | 0.00        | 0    | 172          | 0     | 0.0    | 28.0 | 0.0   |
| 0.0  | 22.1                       | 0.0           |    |         |             | c    |              | c     | (<br>( |      | Ċ     |
|      | ( 200, 204,<br>A 2         |               | 00 | 20.1C   | 00          | Ð    | 7 17 1       | Ð     | 0.0    | 30.9 | 0.0   |
|      | 4.7                        | 0.0           |    |         |             |      |              |       |        |      |       |
|      |                            |               |    |         |             |      |              |       |        |      |       |

| 0.0          | 0.0             | 0.0    | 0.0          |       | 0.0         |        | 26.3      | 0.0    |     |        | 28.0  |       | 0.0    |     |        | 26.5  |       | 0.0    |     |        | 24.7  |       | 0.0    |      | 0.0    |     | 0.0    |     |        |
|--------------|-----------------|--------|--------------|-------|-------------|--------|-----------|--------|-----|--------|-------|-------|--------|-----|--------|-------|-------|--------|-----|--------|-------|-------|--------|------|--------|-----|--------|-----|--------|
| 36.4         | 47.3            | 4.5    | 23.9         | 1 20  | T • 0 C     |        | 0.0       | 35.5   |     |        | 0.0   |       | 35.9   |     |        | 0.0   |       | 36.8   |     |        | 0.0   |       | 25.7   |      | 36.9   |     | 34.5   |     |        |
| 0.0          | 0.0             | 4.5    | 0.0          |       |             |        | 0.0       | 0.0    |     |        | 0.0   |       | 0.0    |     |        | 0.0   |       | 0.0    |     |        | 0.0   |       | 0.0    |      | 0.0    |     | 0.0    |     |        |
| 0            | 00              | 0      | 0            | C     | þ           | 0      | 24        | 0      |     | 0      | 155   |       | 0      |     | 0      | 15    |       | 0      |     | 0      | 43    |       | 0      |      | 0      |     | 0      |     | 0      |
| 606          | 837<br>838      | 516    | 71           | 129   | 1<br>1<br>1 | 24     | 0         | 326    |     | 156    | 0     |       | 32     |     | 15     | 0     |       | 11     |     | 43     | 0     |       | 146    |      | 853    |     | 998    |     | 681    |
| 0            | 00              | 243    | 0            | C     | >           | 0 0    | 0         | 0      |     | 0      | 0     |       | 0      |     | 0      | 0     |       | 0      |     | 0      | 0     |       | 0      |      | 0      |     | 0      |     | 0      |
| 0.00         | 0.00            | 0.00   | 0.00         | 00 0  | •           |        | 2.40      | 0.00   |     |        | 15.50 |       | 0.00   |     |        | 1.50  |       | 0.00   |     |        | 4.30  |       | 0.00   |      | 0.00   |     | 0.00   |     |        |
| 124.40       | 83.78           | 38.69  | 6.25         | 12.70 | -           |        | 0.00      | 32.09  |     |        | 0.00  |       | 3.15   |     |        | 0.00  |       | 1.08   |     |        | 0.00  |       | 11.26  |      | 40.04  |     | 99.77  |     |        |
| 0.00         | 0.00            | 18.22  | 0.00         | 0.00  | •           |        | 0.00      | 0.00   |     |        | 0.00  |       | 0.00   |     |        | 0.00  |       | 0.00   |     |        | 0.00  |       | 0.00   |      | 0.00   |     | 0.00   |     |        |
| 0.0          |                 | ><br>> | ⊃            | 0.0   | 0.0         |        | 0.00      |        | 0.0 |        |       | 00.00 |        | 0.0 |        |       | 00.00 |        | 0.0 |        |       | 00.00 |        | 0.0  |        | 0.0 |        | 0.0 |        |
| 202)         | 202)<br>206)    | ,200)  | ,<br>208)    | 1010  |             | 210)   | 1<br>(212 | 214)   |     | 214)   | 216)  |       | 220)   |     | 220)   | 222)  | -     | 224)   |     | 224)   | 226)  | 1     | 310)   |      | 310)   |     | 302)   |     | 302)   |
| (204,<br>0.0 | (8202,<br>(202, | (206,  | 85.<br>(206, | 43.7  | 0.0         | (8210, | 0.0       | ( 216, | 0.0 | (8214, | (214, | 0.0   | ( 222, | 0.0 | (8220, | (220, | 0.0   | ( 226, | 0.0 | (8224, | (224, | 0.0   | ( 228, | 26.0 | ( 300, | 0.0 | ( 310, | 0.0 | (8302, |
| 0.0          |                 |        | 88.I         | 0.0   | 0.0         |        | 0.0       |        | 0.0 |        |       | 0.0   |        | 0.0 |        |       | 0.0   |        | 0.0 |        |       | 0.0   |        | 0.0  |        | 0.0 |        | 0.0 |        |

|      | ( 302, | 304) |     | 0.00 | 67.98        | 0.00        | 0      | 680        | 0          | 0.0     | 43.4     | 0.0       |
|------|--------|------|-----|------|--------------|-------------|--------|------------|------------|---------|----------|-----------|
| 0.0  | 3.2    |      | 0.0 |      |              |             |        |            |            |         |          |           |
|      | ( 304, | 300) |     | 8.48 | 13.37        | 0.00        | 206    | 325        | 0          | 2.9     | 3.4      | 0.0       |
| 79.6 | 83.    | 4    | 0.0 |      |              |             |        |            |            |         |          |           |
|      | ( 304, | 306) |     | 0.00 | 9.19         | 0.00        | 0      | 153        | 0          | 0.0     | 25.5     | 0.0       |
| 0.0  | 26.1   |      | 0.0 |      |              |             |        |            |            |         |          |           |
|      | ( 300, | 306) |     | 0.00 | 43.45        | 0.00        | 0      | 908        | 0          | 0.0     | 35.6     | 0.0       |
| 0.0  | 0.0    |      | 0.0 |      |              |             |        |            |            |         |          |           |
|      | ( 306, | 308) |     | 0.00 | 211.35       | 0.00        | 0      | 1057       | 0          | 0.0     | 37.8     | 0.0       |
| 0.0  | 0.0    |      | 0.0 |      |              |             |        |            |            |         |          |           |
| 0    |        |      |     |      | EACH VEHICLE | WHICH CROSS | ES THE | STOPLINE I | S CONSIDER | ED AS 1 | VEH-TRIP | FOR THESE |
| STAT | ISTICS |      |     |      |              |             |        |            |            |         |          |           |

NETSIM MOVEMENT SPECIFIC STATISTICS - TABLE I (CONT.)

| ( H           | RIGHT        |             | 0.0        | 0.0              |      |
|---------------|--------------|-------------|------------|------------------|------|
| EED (KMP      | THRU         |             | 44.8       | 15.0             |      |
| SP            | LEFT         |             | 0.0        | 15.8             |      |
| IPS           | RIGHT        | 0           | 0          | 0                |      |
| HICLE-TR      | THRU         | 1581        | 237        | 846              |      |
| VE            | LEFT         | 0           | 0          | 481              |      |
|               | RIGHT        |             | 0.00       | 0.00             |      |
| EHICLE-KM     | THRU         |             | 45.00      | 205.52           |      |
| Λ             | LEFT<br>LGHT |             | 0.00       | u.u<br>116.85    | 0.0  |
| LINK<br>(PCT) | THRU R       | (8300, 308) | (308, 307) | 0.0<br>(308,300) | 80.3 |
| 0<br>STOPS    | LEFT         |             | c<br>c     |                  | 77.1 |

| 0.0               | 0.0     | 0.0                | 0.0               | 0.0                        | 0.0              | 0.0                | ۲<br>م             |                     |             | 26.2               |                     |        | c 1 c              | 1<br>•<br>•<br>2 | 0.0               |         | 24.1               | 0.0     |                  |         |
|-------------------|---------|--------------------|-------------------|----------------------------|------------------|--------------------|--------------------|---------------------|-------------|--------------------|---------------------|--------|--------------------|------------------|-------------------|---------|--------------------|---------|------------------|---------|
| 31.8              | 34.0    | 35.2               | 3.1               | 31.6                       | 19.5             | 38.7               |                    | о. г<br>о и         |             | 0.0                | 36.4                | -      |                    | •                | 38.0              |         | 0.0                | 35.8    |                  |         |
| 0.0               | 0.0     | 0.0                | 3.0               | 0.0                        | 0.0              | 0.0                |                    |                     |             | 0.0                | 0.0                 | •      |                    | )<br>-<br>)      | 0.0               |         | 0.0                | 0.0     |                  |         |
| 0                 | 0       | 00                 | 0                 | 0                          | 0                | 0                  | 0                  |                     | )           | 0<br>15            | 0                   | )      | 0                  | )<br>            | 0                 | 0       | 15                 | 0       | ¢                | 0       |
| 237               | 735     | 644<br>644         | 374               | 498                        | 47               | 8                  | 106<br>0           | ۍ<br>د              | )<br>1      | 15<br>0            | 28                  | e<br>T | 15<br>0            |                  | 9                 | 15      | 0                  | 21      | L<br>T           | ٩T      |
| 0                 | 0       | 00                 | 226               | 0                          | 0                | 0                  | 00                 | · c                 | •           | 00                 | 0                   | ı      | 00                 |                  | 0                 | 0       | 0                  | 0       | ¢                | D       |
| 0.00              | 0.00    | 0.00               | 0.00              | 0.00                       | 0.00             | 0.00               | 8.27               | 00.00               | 6<br>9<br>1 | 1.50               | 0.00                |        | 1.50               |                  | 0.00              |         | 1.50               | 0.00    |                  |         |
| 13.73             | 73.48   | 64.38              | 13.79             | 12.45                      | 1.88             | 0.61               | 0.00               | 2.56                | 1           | 0.00               | 2.76                |        | 0.00               |                  | ec.U              |         | 0.00               | 2.07    |                  |         |
| 0.00              | 0.00    | 0.00               | 8.34              | 0.00                       | 0.00             | 0.00               | 0.00               | 0.00                |             | 0.00               | 0.00                |        | 0.00               |                  | 0.00              |         | 0.00               | 0.00    |                  |         |
| 7, 305)<br>.0 0.0 | 5, 303) | 1, 303)<br>3, 301) | .4 0.0<br>1, 300) | 6.5 U.U<br>0,305)<br>0 0 0 | 1, 227)<br>5 0.0 | 1, 309)<br>0 0 0.0 | 9, 309)<br>9, 311) | .0 100.0<br>5, 313) | .0 0.0      | 3, 313)<br>3, 315) | .0 100.0<br>8, 317) | 0.0    | 7, 317)<br>7, 218) | .0 100.0         | 3, 321)<br>.0 0.0 | 1, 321) | 1, 323)<br>0 100 0 | 7, 325) | .0 0.0<br>5 335) | 1070 10 |
| 0.0 16            | ( 30    | (830               | 0.0 10<br>(30     | 0,0<br>0,0<br>0,0<br>0,0   | 0.0 25           | 0.0 0.0            | (830)              | 0.0 0.0<br>(31:     | 0.0         | (831)<br>(31.      | 0.0 0<br>(21)       | 0.0    | (831)              | 0.0              | 0.0               | (832    | 0 0 ( 32.          | ( 32    | 0.0 0.0          | 1072    |

|     | ( 325, 3<br>0.0 | (27)<br>100_0 | 0.00  | 0.00   | 1.50  | 0   | 0        | Ĥ | 10  | 0.0     | 0.0 0.0      |
|-----|-----------------|---------------|-------|--------|-------|-----|----------|---|-----|---------|--------------|
| •   | ( 331, 3        | 129)          | 0.00  | 2.85   | 0.00  | 0   | 7        | 6 | 0 6 | 9 0 0.0 | 9 0 0.0 37.0 |
| 0.0 | 0.0             | 0.0           |       |        |       |     | •        |   |     | ·       | ·            |
|     | (8329, 3        | (62)          |       |        |       | 00  | Φ' C     |   | 0 < | 0       | 0<br>•       |
| 0.0 | c 1670 1        | 100.0         |       |        | 0.40  | 5   | 5        |   | 4   | 4 0.0   | 4 0.0 0.0    |
|     | ( 335, 3        | (33)          | 0.00  | 3.05   | 0.00  | 0   | 31       |   | 0   | 0 0.0   | 0 0.0 36.4   |
| 0.0 | 0.0             | 0.0           |       |        |       |     |          |   |     |         |              |
|     | (8333, 3        | 333)<br>257)  |       |        |       | 0 0 | 371<br>î |   | 0   | 0       | 0            |
| c   | (333, 3         | 100 0         | 0.00  | 0.00   | 36.99 | 0   | 0        |   | 370 | 370 0.0 | 370 0.0 0.0  |
|     | ( 337, 2        | 105)          | 0.00  | 29.35  | 0.00  | 0   | 272      |   | 0   | 0 0.0   | 0 0.0 23.1   |
| 0.0 | 38.2            | 0.0           |       |        |       |     |          |   |     |         |              |
| 0   | ( 200, 2        | :05)<br>      | 0.00  | 83.46  | 0.00  | 0   | 1547     |   | 0   | 0.0     | 0 0.0 41.9   |
| 0.0 | 0.0             | 0.0           |       |        |       | (   |          |   | ¢   |         |              |
| 0   | ( 202, 2<br>0 0 | (10)<br>0 0   | 0.00  | 91.03  | 0.00  | 0   | 1821     |   | 0   | 0 0.0   | 0 0.0 40.1   |
|     | (8201, 2        | 03)           |       |        |       | 0   | 1317     |   | 0   | 0       | 0            |
|     | ( 203, 2        | (15)          | 0.00  | 65.48  | 0.00  | 0   | 1310     |   | 0   | 0.0     | 0 0.0 4.3    |
| •   | 56.6            | 0.0           |       |        |       |     |          |   |     |         |              |
|     | (275,2          | (00)          | 19.80 | 11.36  | 0.00  | 565 | 324      |   | 0   | 0 2.4   | 0 2.4 2.1    |
| 0.0 | 64.2            | 0.0           | ~     |        |       |     |          |   |     |         |              |
|     | (275,2          | (20)          | 0.00  | 20.51  | 0.00  | 0   | 418      |   | 0   | 0.0     | 0 0.0 8.0    |
| 0   | 66.3            | 0.0           |       |        |       |     |          |   |     |         |              |
|     | (217,2          | :15)          | 0.00  | 9.16   | 0.00  | 0   | 93       |   | 0   | 0.0     | 0 0.0 36.1   |
| 0   | 0.0             | 0.0           |       |        |       |     |          |   |     |         |              |
|     | (8215, 2        | 15)           |       |        |       | 0   | 38       |   | 0   | 0       | 0            |
|     | (215, 2         | 17)           | 0.00  | 0.00   | 3.80  | 0   | 0        |   | 38  | 38 0.0  | 38 0.0 0.0   |
| 0.0 | 0.0             | 100.0         |       |        |       |     |          |   |     |         |              |
|     | (225,2          | :23)          | 0.00  | 11.12  | 0.00  | 0   | 113      |   | 0   | 0.0 0.0 | 0 0.0 36.6   |
| 0.0 | 0.0             | 0.0           |       |        |       |     |          |   |     |         |              |
|     | (8223, 2        | :23)          |       |        |       | 0   | 315      |   | 0   | 0       | 0            |
|     | (223,2          | (25)          | 0.00  | 0.00   | 31.49 | 0   | 0        |   | 315 | 315 0.0 | 315 0.0 0.0  |
| 0.  | 0.0             | 100.0         |       |        |       | (   |          |   | ć   |         |              |
| C   | 1 1 1 1 1 1 1   | .04)          | 0.00  | 11.417 | 00    |     | 9//T     |   | D   | 0.0     | 0 0.0 37.2   |
| >   |                 | ›<br>•<br>>   |       |        |       |     |          |   |     |         |              |

EACH VEHICLE WHICH CROSSES THE STOPLINE IS CONSIDERED AS 1 VEH-TRIP FOR THESE 23.2 30.1 0.0 15 1760 0 1.47 0.00 172.74 0.0 (104,108) 0.1 ( 0.0 0.1 0 STATISTICS

NETSIM MOVEMENT SPECIFIC STATISTICS - TABLE I (CONT.)

Ξ

|               | RIGHT       |      | 0.0       |       | 33.8      |     | 0.0       |     | 0.0       |     | 42.1      |       | 0.0       |       | 0.0       |      | 0.0       |     | 38.3      |       | 38.9      |       |
|---------------|-------------|------|-----------|-------|-----------|-----|-----------|-----|-----------|-----|-----------|-------|-----------|-------|-----------|------|-----------|-----|-----------|-------|-----------|-------|
| ED (KMPH)     | THRU I      |      | 33.8      |       | 45.5      |     | 45.2      |     | 45.1      |     | 44.4      |       | 26.9      |       | 11.2      |      | 39.7      |     | 42.5      |       | 43.2      |       |
| SPE           | LEFT        |      | 0.0       |       | 0.0       |     | 0.0       |     | 0.0       |     | 0.0       |       | 0.0       |       | 9.3       |      | 0.0       |     | 0.0       |       | 0.0       |       |
| PS            | RIGHT       |      | 0         |       | 40        |     | 0         |     | 0         |     | 11        |       | 0         |       | 0         |      | 0         |     | 128       |       | 327       |       |
| HICLE-TRI     | THRU        |      | 1775      |       | 1738      |     | 1748      |     | 1740      |     | 1730      |       | 1859      |       | 620       |      | 1187      |     | 1135      |       | 839       |       |
| VEF           | LEFT        |      | 0         |       | 0         |     | 0         |     | 0         |     | 0         |       | 0         |       | 1036      |      | 0         |     | 0         |       | 0         |       |
|               | RIGHT       |      | 0.00      |       | 2.80      |     | 0.00      |     | 0.00      |     | 2.79      |       | 0.00      |       | 0.00      |      | 0.00      |     | 27.66     |       | 104.35    |       |
| EHICLE-KM     | THRU        |      | 124.44    |       | 121.84    |     | 195.53    |     | 347.91    |     | 439.25    |       | 74.23     |       | 99.21     |      | 80.68     |     | 245.28    |       | 267.75    |       |
| ΓΛ            | LEFT<br>CHT | 1110 | 0.00      | 0.    | 0.00      | 0.  | 0.00      | 0.  | 0.00      | 0.  | 0.00      | 0.    | 0.00      | 0.    | 165.78    | 0.0  | 0.00      | 0.  | 0.00      | 0.    | 0.00      | е.    |
| LINK<br>(PCT) | тнап вт     |      | 108, 110) | 0.0 0 | 110, 114) | 0.0 | 114, 116) | 0.0 | 116, 118) | 0.0 | 118, 122) | 0.2 0 | 122, 125) | 4.0 0 | 125, 200) | 70.6 | 200, 208) | 0.0 | 208, 212) | 0.2 0 | 212, 216) | 0.4 0 |
| 0<br>STOPS    | 1.6.67      |      | )         | 0.0   | <u> </u>  | 0.0 | ~         | 0.0 | )         | 0.0 | )         | 0.0   | <u> </u>  | 0.0   | )         | 86.7 | <b>`</b>  | 0.0 | )         | 0.0   | <u> </u>  | 0.0   |

0. 0 219

| 0.0 43.6 0.0 | 0.0 44.9 34.9 | 0.0 44.6 41.2 | 0.0 37.3 0.0 | 3.9 4.0 0.0          | 0.0 33.9 0.0 | 0.0 42.5 41.4 | 0.0 42.9 35.2 | 0.0 43.6 35.1 | 0.0 44.0 38.1 |              | 0.0 43.6 0.0 | 0.0 44.1 35.2 | 0.0 43.2 36.0 |           |        | 5.4 5.8 0.0 | 0.0 33.8 0.0   |     | 0.0 40.8 0.0  | 0.0 42.8 0.0 |
|--------------|---------------|---------------|--------------|----------------------|--------------|---------------|---------------|---------------|---------------|--------------|--------------|---------------|---------------|-----------|--------|-------------|----------------|-----|---------------|--------------|
| 0            | 32            | 11            | 0            | 0                    | 0            | 8             | 26            | 28            | 9             | ۲C           | 17           | 30            | 32            | c         | 5      | 0           | 0              |     | 0             | 0            |
| 982          | 946           | 948           | 066          | 682                  | 1049         | 1101          | 1182          | 1169          | 1177          |              | T/T†         | 1156          | 1127          |           | T407   | 819         | 1059           |     | 1474          | 1460         |
| 0            | 0             | 0             | 0            | 173                  | 0            | 0             | 0             | 0             | 0             | c            | 0            | 0             | 0             | c         | 5      | 418         | 0              |     | 0             | 0            |
| 0.00         | 3.97          | 2.53          | 0.00         | 0.00                 | 0.00         | 1.92          | 4.87          | 3.72          | 0.80          | <b>V</b> 7 C | 7 · 04       | 3.75          | 3.07          |           | 0.00   | 0.00        | 0.00           |     | 0.00          | 0.00         |
| 152.35       | 117.36        | 218.16        | 185.28       | 30.77                | 29.42        | 264.11        | 221.21        | 155.35        | 157.85        | 14 741       | 14/.4T       | 144.46        | 108.21        | 0 L L J C | 61.102 | 73.64       | 42.28          |     | 193.19        | 144.63       |
| 0.00         | 0.00          | 0.00          | 0.00         | 7.80                 | 0.00         | 00.00         | 0.00          | 0.00          | 0.00          |              | 0.00         | 0.00          | 0.00          |           | 0.00   | 37.59       | 0.00           |     | 0.00          | 0.00         |
| 0<br>0       |               |               | 0.0          | 0.0                  |              |               |               |               | 0.0           | 0.0          | 0.0          | c             | 0.0           | 0.0       | 0.0    | (           |                | 0.0 | 0.0           | •            |
| 218)         | 222)          | 226)          | 228)         | 300)                 | 227)         | 311)          | 315)          | 218)          | 323)          | 1200         | 1170         | 331)          | 335)          | 1200      | 1.00   | 200)        | 207)           |     | 209)          | 211)         |
| (216,        | 0.0<br>(218,  | 0.0<br>(222,  | 0.0          | 10.5<br>(228,<br>7,3 | ( 300,       | ( 227,        | 0.0<br>(311,  | ( 315,        | 0.0<br>(218,  | 0.1          | 0.0          | ( 327,        | 0.2<br>(331,  | 0.0       | 1.2    | ( 337,      | 81. /<br>(200, | 0.0 | ( 207,<br>0.0 | (209,        |
| (<br>(       |               |               | 0.0          | 0.0                  |              |               |               |               | 0.0           | 0.0          | 0.0          | c             | 0.0           | 0.0       | 0.0    |             | <b>۲.</b> ۵    | 0.0 | 0.0           | )<br>•<br>•  |

|      | (211,  | 213) | 0.00   | 288.73 | 0.00  | 0   | 1444 | 0   | 0.0  | 42.7        | 0.0        |
|------|--------|------|--------|--------|-------|-----|------|-----|------|-------------|------------|
| 0.0  | 0.3    | .0   | 0      |        |       |     |      |     |      |             |            |
|      | (213,  | 217) | 0.00   | 182.56 | 12.56 | 0   | 1352 | 93  | 0.0  | 42.4        | 35.1       |
| 0.0  | 0.1    | .0   | 0      |        |       |     |      |     |      |             |            |
|      | ( 217, | 219) | 0.00   | 90.37  | 0.00  | 0   | 1392 | 0   | 0.0  | 42.2        | 0.0        |
| 0.0  | 0.0    | 0.   | 0      |        |       |     |      |     |      |             | •          |
|      | (219,  | 221) | 0.00   | 280.93 | 0.00  | 0   | 1405 | 0   | 0.0  | 43.2        | 0.0        |
| 0.0  | 0.1    | .0   | 0      |        |       |     |      |     |      | <br>•       | )<br>)     |
|      | ( 221, | 225) | 0.00   | 231.81 | 20.01 | 0   | 1309 | 113 | 0.0  | 42.0        | 37.2       |
| 0.0  | 0.5    | 1.   | 8      |        |       |     |      |     |      | )<br>,<br>, | <br> -<br> |
|      | ( 225, | 100) | 121.68 | 89.09  | 3.70  | 922 | 675  | 28  | 11.7 | 14.5        | 17.1       |
| 73.8 | 63.4   | 0 46 | 4      |        |       |     |      |     |      |             |            |
|      |        |      |        |        |       |     |      |     |      |             |            |

| - TABLE II                          | TOTAL TIME             |
|-------------------------------------|------------------------|
| NETSIM MOVEMENT SPECIFIC STATISTICS | DELAY TIME             |
|                                     | MOVING TIME            |
|                                     | LINK<br>MOUTE / TOTANI |

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|          | (         |        | RIGHT |      |
|----------|-----------|--------|-------|------|
|          | VEH-MINS  |        | THRU  |      |
|          |           |        | LEFT  |      |
|          |           |        | RIGHT |      |
|          | VEH-MINS) |        | THRU  |      |
|          | )         |        | LEFT  |      |
|          |           |        | RIGHT |      |
|          | VEH-MINS) |        | THRU  |      |
|          | <u> </u>  |        | LEFT  | -    |
| AL       |           |        |       | RIGH |
| MOVE/TOT |           | (SNI   |       | THRU |
| RATIO    |           | (VEH-N |       | LEFT |

(8102, 102)

|       | (8103, 103) |        |        |        |        |        |        |        |        |        |
|-------|-------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
|       | (102, 100)  | 114.43 | 4.47   | 164.75 | 432.41 | 16.41  | 148.30 | 546.83 | 20.88  | 313.05 |
| 0.21  | 0.21        | 0.53   |        |        |        |        |        |        |        |        |
|       | (100, 102)  | 0.00   | 173.32 | 0.00   | 0.00   | 50.80  | 0.00   | 0.00   | 224.12 | 0.00   |
| 0.00  | 0.77        | 0.00   |        |        |        |        |        |        |        |        |
|       | (103, 100)  | 43.59  | 140.00 | 3.66   | 148.78 | 447.13 | 2.21   | 192.37 | 587.13 | 5.87   |
| 0.23  | 0.24        | 0.62   |        |        |        |        |        |        |        |        |
|       | (100, 103)  | 0.00   | 205.70 | 0.00   | 0.00   | 77.23  | 0.00   | 0.00   | 282.93 | 0.00   |
| 00.00 | 0.73        | 0.00   |        |        |        |        |        |        |        |        |
|       | (100, 101)  | 0.00   | 40.63  | 0.00   | 0.00   | 3.57   | 0.00   | 0.00   | 44.20  | 0.00   |
| 0.00  | 0.92        | 0.00   |        |        |        |        |        |        |        |        |
|       | (108, 106)  | 0.00   | 1.86   | 0.00   | 0.00   | 0.70   | 0.00   | 0.00   | 2.57   | 0.00   |
| 0.00  | 0.73        | 0.00   |        |        |        |        |        |        |        |        |
|       | (8106, 106) |        |        |        |        |        |        |        |        |        |
|       | (106, 108)  | 00.00  | 0.00   | 1.86   | 0.00   | 0.00   | 2.47   | 0.00   | 0.00   | 4.33   |
| 0.00  | 0.00        | 0.43   |        |        |        |        |        |        |        |        |
|       | (114, 112)  | 0.00   | 4.97   | 0.00   | 0.00   | 1.55   | 0.00   | 0.00   | 6.52   | 0.00   |
| 0.00  | 0.76        | 0.00   |        |        |        |        |        |        |        | •      |
|       | (8112, 112) |        |        |        |        |        |        |        |        |        |
|       | (112, 114)  | 0.00   | 0.00   | 1.86   | 0.00   | 0.00   | 5.20   | 0.00   | 0.00   | 7.07   |
| 0.00  | 0.00        | 0.26   |        |        |        |        |        |        |        |        |
|       | (122, 120)  | 00.00  | 1.49   | 0.00   | 0.00   | 0.34   | 0.00   | 0.00   | 1.83   | 0.00   |
| 0.00  | 0.81        | 0.00   |        |        |        |        |        |        |        |        |
|       | (8120, 120) |        |        |        |        |        |        |        |        |        |
|       | (120, 122)  | 0.00   | 0.00   | 15.78  | 0.00   | 0.00   | 27.40  | 0.00   | 0.00   | 43.18  |
| 0.00  | 0.00        | 0.37   |        |        |        |        |        |        |        |        |
|       | (125, 126)  | 0.00   | 28.02  | 0.00   | 0.00   | 2.05   | 0.00   | 0.00   | 30.07  | 0.00   |
| 0.00  | 0.93        | 0.00   |        |        |        |        |        |        |        |        |
|       | (126, 204)  | 00.00  | 14.98  | 0.00   | 0.00   | 10.87  | 0.00   | 0.00   | 25.85  | 0.00   |
| 0.00  | 0.58        | 0.00   |        |        |        |        |        |        |        |        |
|       | (200, 204)  | 0.00   | 39.63  | 0.00   | 0.00   | 22.30  | 0.00   | 0.00   | 61.93  | 0.00   |
| 0.00  | 0.64        | 0.00   |        |        |        |        |        |        |        |        |
|       | (204, 202)  | 0.00   | 154.60 | 0.00   | 0.00   | 50.33  | 0.00   | 0.00   | 204.93 | 0.00   |
| 0.00  | 0.75        | 0.00   |        |        |        |        |        |        |        |        |
|       | (8202, 202) |        |        |        |        |        |        |        |        |        |
|       | (202, 206)  | 0.00   | 104.12 | 0.00   | 0.00   | 2.12   | 0.00   | 0.00   | 106.23 | 0.00   |
| 0.00  | 0.98        | 0.00   |        |        |        |        |        |        |        |        |

|        | (206, 200)  | 22.64 | 48.08  | 0.00  | 222.49 | 470.85 | 0.00  | 245.13 | 518.93 | 0.00  |
|--------|-------------|-------|--------|-------|--------|--------|-------|--------|--------|-------|
| ת      | 0.09        | 0.00  |        |       |        |        |       |        |        |       |
|        | (206, 208)  | 0.00  | 7.77   | 0.00  | 00.00  | 7.93   | 0.00  | 0.00   | 15.70  | 0.00  |
| 0      | 0.50        | 0.00  |        |       |        |        |       |        |        |       |
|        | (212, 210)  | 0.00  | 16.03  | 0.00  | 0.00   | 5.06   | 0.00  | 0.00   | 21.08  | 0.00  |
| 0      | 0.76        | 0.00  |        |       |        |        |       |        |        |       |
|        | (8210, 210) |       |        |       |        |        |       |        |        |       |
|        | (210, 212)  | 0.00  | 0.00   | 2.98  | 0.00   | 0.00   | 2.48  | 0.00   | 0.00   | 5.47  |
| 0      | 0.00        | 0.55  |        |       |        |        |       |        |        |       |
|        | (216, 214)  | 0.00  | 40.50  | 0.00  | 0.00   | 13.78  | 0.00  | 0.00   | 54.28  | 0.00  |
| 0      | 0.75        | 0.00  |        |       |        |        |       |        |        |       |
|        | (8214, 214) |       |        |       |        |        |       |        |        |       |
|        | (214, 216)  | 0.00  | 0.00   | 19.26 | 0.00   | 0.00   | 13.98 | 0.00   | 0.00   | 33.23 |
| 0      | 0.00        | 0.58  |        |       |        |        |       |        |        |       |
|        | (222, 220)  | 0.00  | 3.98   | 0.00  | 0.00   | 1.29   | 0.00  | 0.00   | 5.27   | 0.00  |
| 0      | 0.75        | 0.00  |        |       |        |        |       |        |        |       |
|        | (8220, 220) |       |        |       |        |        |       |        |        |       |
|        | (220, 222)  | 0.00  | 0.00   | 1.86  | 0.00   | 0.00   | 1.54  | 0.00   | 0.00   | 3.40  |
| 0      | 0.00        | 0.55  |        |       |        |        |       |        |        |       |
|        | (226, 224)  | 00.00 | 1.37   | 0.00  | 0.00   | 0.40   | 0.00  | 0.00   | 1.77   | 0.00  |
| 0      | 0.77        | 0.00  |        |       |        |        |       |        |        |       |
|        | (8224, 224) |       |        |       |        |        |       |        |        |       |
|        | (224, 226)  | 0.00  | 0.00   | 5.34  | 0.00   | 0.00   | 5.11  | 0.00   | 0.00   | 10.45 |
| 0      | 0.00        | 0.51  |        |       |        |        |       |        |        |       |
|        | (228, 310)  | 0.00  | 13.99  | 0.00  | 0.00   | 12.31  | 0.00  | 0.00   | 26.30  | 0.00  |
| 0      | 0.53        | 0.00  |        |       |        |        |       |        |        |       |
|        | (300, 310)  | 0.00  | 49.76  | 0.00  | 0.00   | 15.27  | 0.00  | 0.00   | 65.03  | 0.00  |
| ~      | 0.77        | 0.00  |        |       |        |        |       |        |        |       |
|        | (310, 302)  | 0.00  | 123.99 | 0.00  | 0.00   | 49.74  | 0.00  | 0.00   | 173.73 | 0.00  |
| 0      | 0.71        | 0.00  |        |       |        |        |       |        |        |       |
|        | (8302, 302) |       |        |       |        |        |       |        |        |       |
|        | (302, 304)  | 0.00  | 84.48  | 0.00  | 0.00   | 9.60   | 0.00  | 0.00   | 94.08  | 0.00  |
| $\sim$ | 0.90        | 0.00  |        |       |        |        |       |        |        |       |
|        | (304, 300)  | 10.53 | 16.62  | 0.00  | 162.10 | 217.81 | 0.00  | 172.63 | 234.43 | 0.00  |
| s      | 0.07        | 0.00  |        |       |        |        |       |        |        |       |
|        | (304, 306)  | 0.00  | 11.42  | 0.00  | 0.00   | 10.22  | 0.00  | 0.00   | 21.63  | 0.00  |
| 0      | 0.53        | 0.00  |        |       |        |        |       |        |        |       |

|   | (300, 306)                         |       | 0.00  | 54.00      | 0.00  | 0.00      | 19.17      | 0.00       | 0.00       | 73.17      | 0.00  |
|---|------------------------------------|-------|-------|------------|-------|-----------|------------|------------|------------|------------|-------|
| 0.00  | (306, 308)<br>0.78                 | 0.00  | 0.00  | 262.65     | 0.00  | 0.00      | 72.53      | 0.00       | 0.00       | 335.18     | 0.00  |
| Ч   |                                    |       |       |            |       | NETSIM MO | VEMENT SPI | ECIFIC STA | ATISTICS - | TABLE II   |       |
| ()<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1 | LINK<br>MOUT / MOMAT               |       |       | MOVING TIN | Æ     |           | DELAY TIM  | G          |            | TOTAL TIME |       |
| KAT1C   | MOVE/TUTAL                         | _     |       | (VEH-MINS) | -     |           | (VEH-MINS  | ~          |            | (NEH-MINS) |       |
| (VEH-<br>LEFT   | MINS)<br>THRU                      | RIGHT | LEFT  | THRU       | RIGHT | LEFT      | THRU       | RIGHT      | LEFT       | THRU       | RIGHT |
|   | (8300, 308)<br>(308, 307)          |       | 0.00  | 55.93      | 0.00  | 0.00      | 4.40       | 0.00       | 0.00       | 60.33      | 0.00  |
| 00.00   | 0.93<br>(308,300)                  |       | 15.21 | 255.40     | 0.00  | 299.09    | 568.20     | 0.00       | 444.30     | 823.60     | 0.00  |
| 0.00  | ( 307, 305)                        | 0.00  | 0.00  | 17.06      | 0.00  | 0.00      | 8.88       | 0.00       | 0.00       | 25.93      | 00.00 |
| 0.00  | 0.66<br>(305,303)                  | 0.00  | 00.00 | 91.32      | 0.00  | 0.00      | 38.43      | 0.00       | 0.00       | 129.75     | 0.00  |
| 0.00  | 0.70<br>(8301, 303)<br>( 303, 301) | 0.00  | 0.00  | 80.01      | 0.00  | 0.00      | 29.62      | 0.00       | 0.00       | 109,63     | 00.00 |
| 0.00  | 0.73<br>(301, 300)                 | 0.00  | 0.36  | 17.14      | 0.00  | 158.82    | 250.58     | 0.00       | 169.18     | 267.72     | 0.00  |
| 0.06  | 0.06<br>(300,305)                  | 0.00  | 00.00 | 15.47      | 0.00  | 0.00      | 8.15       | 0.00       | 0.00       | 23.62      | 0.00  |
| 0.00  | 0.65<br>(301,227)                  | 0.00  | 0.00  | 2.33       | 0.00  | 0.00      | 3.43       | 0.00       | 0.00       | 5.77       | 0.00  |
| 0.00  | 0.40<br>(311, 309)                 | 0.00  | 0.00  | 0.78       | 0.00  | 0.00      | 0.17       | 0.00       | 0.00       | 0.95       | 0.00  |
| 0.00  | 0.82<br>(8309, 309)                | 0.00  |       |            |       |           |            |            |            |            |       |

|       | (309, 311)  | 0    | .00 | 0.00   | 10.28 | 0.00 | 0.00  | 14.90 | 0.00 | 0.00   | 25.18  |
|-------|-------------|------|-----|--------|-------|------|-------|-------|------|--------|--------|
| 0.00  | 0.00        | 0.41 |     |        |       |      |       |       |      |        |        |
|       | (315, 313)  | 0    | .00 | 3.23   | 0.00  | 0.00 | 0.95  | 0.00  | 0.00 | 4.18   | 0.00   |
| 0.00  | 0.77        | 0.00 |     |        |       |      |       |       |      |        |        |
|       | (8313, 313) |      |     |        |       |      |       |       |      |        |        |
|       | (313, 315)  | 0    | .00 | 0.00   | 1.86  | 0.00 | 0.00  | 1.57  | 0.00 | 0.00   | 3.43   |
| 0.00  | 0.00        | 0.54 |     |        |       |      |       |       |      |        |        |
|       | (218, 317)  | 0    | .00 | 3.48   | 0.00  | 0.00 | 1.07  | 0.00  | 0.00 | 4.55   | 0.00   |
| 0.00  | 0.76        | 0.00 |     |        |       |      |       |       |      |        |        |
|       | (8317, 317) |      |     |        |       |      |       |       |      |        |        |
|       | (317, 218)  | 0    | .00 | 0.00   | 1.86  | 0.00 | 0.00  | 2.39  | 0.00 | 0.00   | 4.25   |
| 0.00  | 0.00        | 0.44 |     |        |       |      |       |       |      |        |        |
|       | (323, 321)  | 0    | .00 | 0.75   | 0.00  | 0.00 | 0.19  | 0.00  | 0.00 | 0.93   | 0.00   |
| 0.00  | 0.80        | 0.00 |     |        |       |      |       |       |      |        |        |
|       | (8321, 321) |      |     |        |       |      |       |       |      |        |        |
|       | (321, 323)  | 0    | .00 | 0.00   | 1.86  | 0.00 | 0.00  | 1.87  | 0.00 | 0.00   | 3.73   |
| 00.00 | 0.00        | 0.50 |     |        |       |      |       |       |      |        |        |
|       | (327, 325)  | 0    | .00 | 2.61   | 0.00  | 0.00 | 0.86  | 0.00  | 0.00 | 3.47   | 0.00   |
| 0.00  | 0.75        | 0.00 |     |        |       |      |       |       |      |        |        |
|       | (8325, 325) |      |     |        |       |      |       |       |      |        |        |
|       | (325, 327)  | 0    | .00 | 0.00   | 1.86  | 0.00 | 0.00  | 2.40  | 0.00 | 0.00   | 4.27   |
| 0.00  | 0.00        | 0.44 |     |        |       |      |       |       |      |        |        |
|       | (331, 329)  | 0    | .00 | 3.60   | 0.00  | 0.00 | 1.03  | 0.00  | 0.00 | 4.63   | 0.00   |
| 0.00  | 0.78        | 0.00 |     |        |       |      |       |       |      |        |        |
|       | (8329, 329) |      |     |        |       |      |       |       |      |        |        |
|       | (329, 331)  | 0    | .00 | 0.00   | 0.50  | 0.00 | 0.00  | 0.34  | 0.00 | 0.00   | 0.83   |
| 0.00  | 0.00        | 0.60 |     |        |       |      |       |       |      |        |        |
|       | (335, 333)  | 0    | .00 | 3.85   | 0.00  | 0.00 | 1.18  | 0.00  | 0.00 | 5.03   | 0.00   |
| 0.00  | 0.77        | 0.00 |     |        |       |      |       |       |      |        |        |
|       | (8333, 333) |      |     |        |       |      |       |       |      |        |        |
|       | (333, 335)  | 0    | .00 | 0.00   | 45.97 | 0.00 | 0.00  | 68.78 | 0.00 | 0.00   | 114.75 |
| 0.00  | 0.00        | 0.40 |     |        |       |      |       |       |      |        |        |
|       | (337, 205)  | 0    | .00 | 36.47  | 0.00  | 0.00 | 39.68 | 0.00  | 0.00 | 76.15  | 0.00   |
| 0.00  | 0.48        | 0.00 |     |        |       |      |       |       |      |        |        |
|       | (200, 205)  | 0    | .00 | 103.72 | 0.00  | 0.00 | 15.78 | 0.00  | 0.00 | 119.50 | 0.00   |
| 0.00  | 0.87        | 0.00 |     |        |       |      |       |       |      |        |        |

|       | TOTAL TIME  | -          | ы         | DELAY TIM   |           | ME    | MOVING TI             |               | LINK<br>MOVE/TOTAL        | RATIO |
|-------|-------------|------------|-----------|-------------|-----------|-------|-----------------------|---------------|---------------------------|-------|
|       | TABLE II    | ATISTICS - | ECIFIC ST | VEMENT SP   | NETSIM MO |       |                       |               |                           | 1     |
|       |             |            |           |             |           |       |                       | 0.00          | 0.94                      | 0.00  |
| 0.00  | 259.30      | 0.00       | 0.00      | 16.30       | 0.00      | 0.00  | 243.00                | 0.00          | (114, 116)                | •     |
| 4.98  | 160.75      | 0.00       | 1.50      | 9.33        | 0.00      | 3.48  | 151.42                | 0.00          | (110, 114)<br>0.94        | 0.00  |
| 0.00  | 220.57      | 0.00       | 0.00      | 65.93       | 0.00      | 0.00  | 154.64                | 0.00          | ( 108, 110)<br>0.70       | 0.00  |
| 3.80  | 343.88      | 0.00       | 1.97      | 129.22      | 0.00      | 1.83  | 214.67                | 0.00          | ( 104, 108)<br>0.62       | 0.00  |
| 0.00  | 443.02      | 0.00       | 0.00      | 89.83       | 0.00      | 0.00  | 353.18                | 0.00          | (100,104)<br>0.80         | 0.00  |
| 85.28 | 0.00        | 0.00       | 40.13     | 00          | 0.00      | 39.14 | 0.00                  | 0.46          | (c77' C77 )               | 0.00  |
|       |             |            |           |             |           |       |                       |               | (8223, 223)               |       |
|       | C 2 • C 7   | ••••       |           | · · · ·     | •         | •     |                       | 0.00          | 0.77                      | 0.00  |
|       | CC 01       |            |           | , 10<br>,   |           |       | VU V L                | 0.46          | 0.00                      | 0.00  |
| 10.30 | 0.00        | 0.00       | 5.58      | 0.00        | 0.00      | 4.72  | 0.00                  | 0.00          | (8215, 215)<br>(215, 217) |       |
|       |             |            |           |             |           |       |                       | 0.00          | 0.76                      | 0.00  |
| 0.00  | 15.23       | 0.00       | 0.00      | 3.68        | 0.00      | 0.00  | 11.55                 | 0.00<br>0.00  | 0.17<br>(217,215)         | 0.00  |
| 0.00  | 154.02      | 0.00       | 0.00      | 128.52      | 0.00      | 0.00  | 25.49                 | 0.00          | (275, 207)                |       |
| 0.00  | 332.00      | 501.15     | 0.00      | 317.89      | 476.54    | 0.00  | 14.11                 | 24.61<br>0.00 | (275,200)<br>0.04         | 0.05  |
|       |             |            |           |             |           |       |                       | 0.00          | 0.09                      | 0.00  |
| 0.00  | 916.38      | 0.00       | 0.00      | 835.00      | 0.00      | 0.00  | 81.38                 | 0.00          | (8201, 203)<br>(203, 275) |       |
|       | · · · · · · |            |           | 1<br>1<br>1 |           | •     | ]<br>-<br>-<br>-<br>- | 0.00          | 0.83                      | 0.00  |
| 0     | 136 03      | 00 0       | 0.00      | 22.91       | 00.00     | 0.00  | 113.12                | 0.00          | (205, 201)                |       |

| UEH- | MTNS)               |                | (VEH-MINS | ()     |            | (VEH-MINS | ~       |         | (VEH-MINS | (      |
|------|---------------------|----------------|-----------|--------|------------|-----------|---------|---------|-----------|--------|
|      | (ONTE               | LEFT           | THRU      | RIGHT  | 1. F. F. T | тнвп      | втент   | ተደግ     | UDUT      | ылла   |
| LEFT | THRU                | RIGHT          |           |        |            |           |         |         |           | 10014  |
|      | (116, 118)          | 00.00          | 432.36    | 00.00  | 0.00       | 30.44     | 0.00    | 0.00    | 462.80    | 0.0    |
| 0.00 | 0.93                | 0.00           | 545 87    | 7 47   |            | 5V LV     | 0<br>51 |         | 500 20    | c<br>c |
| 0.00 | 0.92                | 0.87           |           |        |            | )<br>     | +0.0    | 00.0    | 00.000    | 0.40   |
|      | (122, 125)          | 0.00           | 92.25     | 0.00   | 0.00       | 73.19     | 0.00    | 0.00    | 165.43    | 0.00   |
| 0.00 | 0.56                | 0.00           |           |        |            |           |         |         |           |        |
| 0.19 | ( 125, 200)<br>0.23 | 206.02<br>0.00 | 123.30    | 0.00   | 865.93     | 405.94    | 0.00    | 1071.95 | 529.23    | 0.00   |
|      | (200, 208)          | 0.00           | 100.27    | 0.00   | 0.00       | 21.82     | 0.00    | 0.00    | 122.08    | 0.00   |
| 0.00 | 0.82                | 0.00           |           |        |            |           |         |         |           |        |
|      | (208, 212)          | 0.00           | 304.82    | 34.38  | 0.00       | 41.62     | 8.97    | 0.00    | 346.43    | 43.35  |
| 0.00 | 0.88                | 0.79           |           |        |            |           |         |         |           |        |
|      | (212, 216)          | 0.00           | 332.74    | 129.69 | 0.00       | 38.98     | 31.13   | 0.00    | 371.72    | 160.82 |
| 0.00 | 0.90                | 0.81           |           |        |            |           |         |         |           |        |
|      | (216, 218)          | 00.00          | 189.33    | 0.00   | 0.00       | 20.47     | 0.00    | 0.00    | 209.80    | 0.00   |
| 0.00 | 0.90                | 0.00           |           |        |            |           |         |         |           |        |
|      | (218, 222)          | 00.00          | 145.84    | 4.93   | 0.00       | 10.84     | 1.88    | 0.00    | 156.68    | 6.82   |
| 0.00 | 0.93                | 0.72           |           |        |            |           |         |         |           |        |
|      | (222, 226)          | 0.00           | 271.11    | 3.15   | 0.00       | 22.62     | 0.54    | 0.00    | 293.73    | 3.68   |
| 0.00 | 0.92                | 0.85           |           |        |            |           |         |         |           |        |
|      | (226, 228)          | 00.00          | 230.25    | 0.00   | 0.00       | 67.93     | 0.00    | 0.00    | 298.18    | 0.00   |
| 0.00 | 0.77                | 0.00           |           |        |            |           |         |         |           |        |
|      | (228, 300)          | 9.70           | 38.23     | 0.00   | 110.60     | 429.05    | 0.00    | 120.30  | 467.28    | 0.00   |
| 0.08 | 0.08                | 0.00           |           |        |            |           |         |         |           |        |
|      | (300, 227)          | 0.00           | 36.56     | 0.00   | 0.00       | 15.54     | 0.00    | 0.00    | 52.10     | 0.00   |
| 0.00 | 0.70                | 0.00           |           |        |            |           |         |         |           |        |
|      | (227, 311)          | 0.00           | 328.21    | 2.38   | 0.00       | 44.32     | 0.40    | 0.00    | 372.53    | 2.78   |
| 0.00 | 0.88                | 0.86           |           |        |            |           |         |         |           |        |
|      | (311, 315)          | 0.00           | 274.90    | 6.05   | 0.00       | 34.65     | 2.24    | 0.00    | 309.55    | 8.28   |
| 0.00 | 0.89                | 0.73           |           |        |            |           |         |         |           |        |
|      | (315, 218)          | 0.00           | 193.06    | 4.62   | 0.00       | 20.82     | 1.74    | 0.00    | 213.88    | 6.37   |
| 0.00 | 0.90                | 0.73           |           |        |            |           |         |         |           |        |

| 33.03 4.48   96.68 6.38 | <b>96.68</b> 6.38                       |            |        | 50.22 5.12          | 76.22 0.00 | 57.72 0.00    | 75 13 0 00     |                  | 33.77 0.00 | 32.95 0.00 |                   | 10.0<br>0.01                            | 58.23 21.47 | 0 0 00 0 00       | 10.0<br>0.00 | <b>30.47 0.0</b> C | 00 00 20 20 10 | 07.7C / F.TC                          | 58.78 12.93 |               | ABLE III      |
|-------------------------|---|------------|--------|---------------------|------------|---------------|----------------|------------------|------------|------------|-------------------|---|-------------|-------------------|--------------|--------------------|----------------|---------------------------------------|-------------|---------------|---------------|
| 0.00 20                 |   | 0.00 15    |        | 0.00 15             | 0.00 37    | 418.98 75     | 0.00           | -<br>)<br>)<br>) | 0.00 28    | 0.00 20    |                   | 0.00 40                                 | 0.00 25     |                   |              | 0.00 35            |                | · · · · · · · · · · · · · · · · · · · | 625.50 36   |               | ATISTICS - TF |
| 1.20                    |   | 1.72       | •      | 1.30                | 0.00       | 0.00          | 0.00           |                  | 0.00       | 0.00       |                   |   | 5.86        |                   |              | 0.00               | 10 7           | T F • 1                               | 8.34        |               | ECIFIC STF    |
| 19 84                   | ר<br>•<br>•<br>•                        | 17.15      |        | c/.cI               | 55.86      | 666.20        | 22.58          |                  | 43.68      | 23.22      | 16 67             |   | 31.36       | 16 27             | 1 7 . 0 1    | 41.35              | 65 57          |                                       | 258.07      |               | VEMENT SP     |
|                         | >>·>                                    | 0.00       |        | 0.00                | 0.00       | 372.27        | 0.00           |                  | 0.00       | 0.00       |                   |   | 0.00        |                   | •••          | 0.00               | 00.0           | •••                                   | 474.28      |               | NETSIM MO     |
| сс<br>с                 | 3.24                                    | 4.66       | c<br>c | 3.82                | 0.00       | 0.00          | 0.00           |                  | 00         | 0.00       |                   | ••••                                    | 15.61       | 00 0              | •••          | 0.00               | 24,87          |                                       | 4.59        |               |               |
| 183 10                  | 1 · · · · · · · · · · · · · · · · · · · | 179.53     |        | 134.4/              | 320.36     | 91.52         | 52.55          |                  | 24U.U8     | 179.73     | 358 A1            | + > > > > > > > > > > > > > > > > > > > | 226.87      | 112.31            |              | 349.12             | 288.08         | •                                     | 110.71      |               |               |
|                         | 0.00                                    | 00.0       | 0.73   | 0.75                | 0.00       | 0.00<br>46.71 | 0.00<br>0.00   | 0.00             | 0.00       | 0.00       | 0.00              | 0.00                                    | 0.00        | 0.73              | 0.00         | 0.00               | 0.00           | 0.77                                  | 151.22      | 00.0          |               |
|                         | ( 323, 327)<br>0 90                     | (327, 331) | 0.91   | ( 331, 333)<br>0.90 | (335, 337) | 337, 200)     | 0.12 200, 207) | 0.70             | 0.85       | 209, 211)  | 0.89<br>211, 213) | 0.88                                    | 213, 217)   | 0.88<br>217, 219) | 0.87         | 219, 221)          | 221, 225)      | 0.87                                  | 225, 100)   | 0000          |               |
|                         | ) 00 0                                  | )          | 0.00   | 0.00                |            | )<br>)<br>)   | 0.11<br>(      | 0.00             | 0.00       |            | 0.00              | 0.00                                    | )           | 0.00              | 0.00         |                    | ~<br>^^^       | 0.00                                  |             | <b>1</b><br>7 | -1            |

TINK TIME\*\*

QUEUE TIME\*\*

DELAY TIME

TOTAL TIME

|      |         |      |      | <u>.</u> | SECS/VEH) |       | (SEC | CS/VEH) |                | (VE         | (SNIM-H    |             |
|------|---------|------|------|----------|-----------|-------|------|---------|----------------|-------------|------------|-------------|
| (VEH | (SNIM-H |      |      |          |           |       |      |         |                |             |            |             |
|      |         |      | н    | LEFT     | THRU      | RIGHT | LEFT | THRU    | RIGHT          | LEFT        | THRU       | втент       |
| LEFT | THR THR | U R  | IGHT |          |           |       |      |         | <br> <br> <br> | 4<br>1<br>1 |            |             |
|      | (8102,  | 102) |      |          |           |       |      |         |                |             |            |             |
|      | (8103,  | 103) |      |          |           |       |      |         |                |             |            |             |
|      | ( 102,  | 100) | ц,   | 53.4     | 52.2      | 21.2  | 42.3 | 41.0    | 10.1           | 370.3       | 14.2       | 64.8        |
| 362. | 8 14    | 0.   | 55.4 |          |           |       |      |         |                | )           | 1          |             |
|      | ( 100,  | 102) |      | 0.0      | 14.5      | 0.0   | 0.0  | 3.3     | 0.0            | 0.0         | 0.2        | 0.0         |
| 0.0  | 0.0     |      | 0.0  |          |           |       |      |         |                | )           | <br>•<br>• | •           |
|      | ( 103,  | 100) | 7    | 12.1     | 40.0      | 15.3  | 32.6 | 30.5    | 5.8            | 127.2       | 371.9      | 0.9         |
| 124. | 6 362   | .4   | 0.9  |          |           |       |      |         |                |             |            | •           |
|      | ( 100,  | 103) |      | 0.0      | 13.1      | 0.0   | 0.0  | 3.6     | 0.0            | 0.0         | 0.4        | 0.0         |
| 0.0  | 0.0     |      | 0.0  |          |           |       |      |         |                |             | •          | •           |
|      | ( 100,  | 101) |      | 0.0      | 8.1       | 0.0   | 0.0  | 0.7     | 0.0            | 0.0         | 0.1        | 0.0         |
| 0.0  | 0.0     | -    | 0.0  |          |           |       |      |         |                | 1           | )<br>•     |             |
|      | ( 108,  | 106) |      | 0.0      | 10.3      | 0.0   | 0.0  | 2.8     | 0.0            | 0.0         | 0.1        | 0.0         |
| 0.0  | 0.0     | -    | 0.0  |          |           |       |      |         |                |             | •          | ,<br>,      |
|      | (8106,  | 106) |      |          |           |       |      |         |                |             |            |             |
|      | ( 106,  | 108) |      | 0.0      | 0.0       | 17.3  | 0.0  | 0.0     | 9.9            | 0.0         | 0.0        | 1.8         |
| 0.0  | 0.0     |      | 1.8  |          |           |       |      |         |                |             | 1          | )<br>-<br>  |
|      | ( 114,  | 112) |      | 0.0      | 9.8       | 0.0   | 0.0  | 2.3     | 0.0            | 0.0         | 0.0        | 0.0         |
| 0.0  | 0.0     | 1    | 0.0  |          |           |       |      |         |                |             |            | •           |
|      | (8112,  | 112) |      |          |           |       |      |         |                |             |            |             |
|      | ( 112,  | 114) |      | 0.0      | 0.0       | 28.3  | 0.0  | 0.0     | 20.8           | 0.0         | 0.0        | 4.8         |
| 0.0  | 0.0     | 7    | 4.7  |          |           |       |      |         |                |             |            | •           |
|      | ( 122,  | 120) |      | 0.0      | 9.2       | 0.0   | 0.0  | 1.7     | 0.0            | 0.0         | 0.0        | 0.0         |
| 0.0  | 0.0     | -    | 0.0  |          |           |       |      |         |                |             |            |             |
|      | (8120,  | 120) |      |          |           |       |      |         |                |             |            |             |
|      | ( 120,  | 122) |      | 0.0      | 0.0       | 20.4  | 0.0  | 0.0     | 12.9           | 0.0         | 0.0        | 23.0        |
| 0.0  | 0.0     | 2    | 2.5  |          |           |       |      |         |                |             |            | )<br>,<br>, |
|      | ( 125,  | 126) |      | 0.0      | 10.5      | 0.0   | 0.0  | 0.7     | 0.0            | 0.0         | 0.0        | 0.0         |
| 0.0  | 0.0     | -    | 0.0  |          |           |       |      |         |                |             |            |             |
|      | ( 126,  | 204) |      | 0.0      | 0.0       | 0.0   | 0.0  | 3.8     | 0.0            | 0.0         | 5.3        | 0.0         |
| 0.0  | 5.2     | -    | 0.0  |          |           |       |      |         |                |             |            |             |
|      | ( 200,  | 204) |      | 0.0      | 5.0       | 0.0   | 0.0  | 1.8     | 0.0            | 0.0         | 4.8        | 0.0         |
| 0.0  | 2.7     | -    | 0.0  |          |           |       |      |         |                |             |            |             |

|      | ( 204, | 202) |     | 0.0  | 13.5 | 0.0  | 0.0  | 3.3  | 0.0 | 0.0   | 0.1   | 0.0 |
|------|--------|------|-----|------|------|------|------|------|-----|-------|-------|-----|
| 0.0  | 0.0    |      | 0.0 |      |      |      |      |      |     |       |       |     |
|      | (8202, | 202) |     |      |      |      |      |      |     |       |       |     |
|      | (202,  | 206) |     | 0.0  | 7.6  | 0.0  | 0.0  | 0.2  | 0.0 | 0.0   | 0.0   | 0.0 |
| 0.0  | 0.0    |      | 0.0 |      |      |      |      |      |     |       |       |     |
|      | (206,  | 200) |     | 60.5 | 60.3 | 0.0  | 54.9 | 54.8 | 0.0 | 204.4 | 437.7 | 0.0 |
| 201. | 7 430  | .6   | 0.0 | ~    |      |      |      |      |     |       |       |     |
|      | ( 206, | 208) |     | 0.0  | 13.3 | 0.0  | 0.0  | 6.7  | 0.0 | 0.0   | 5.7   | 0.0 |
| 0.0  | 5.6    |      | 0.0 |      |      |      |      |      |     |       |       |     |
|      | ( 212, | 210) |     | 0.0  | 9.8  | 0.0  | 0.0  | 2.4  | 0.0 | 0.0   | 0.0   | 0.0 |
| 0.0  | 0.0    |      | 0.0 |      |      |      |      |      |     |       |       |     |
|      | (8210, | 210) |     |      |      |      |      |      |     |       |       |     |
|      | ( 210, | 212) |     | 0.0  | 0.0  | 13.7 | 0.0  | 0.0  | 6.2 | 0.0   | 0.0   | 1.5 |
| 0.0  | 0.0    |      | 1.5 |      |      |      |      |      |     |       |       |     |
|      | ( 216, | 214) |     | 0.0  | 10.0 | 0.0  | 0.0  | 2.5  | 0.0 | 0.0   | 0.0   | 0.0 |
| 0.0  | 0.0    |      | 0.0 |      |      |      |      |      |     |       |       |     |
|      | (8214, | 214) |     |      |      |      |      |      |     |       |       |     |
|      | (214,  | 216) |     | 0.0  | 0.0  | 12.9 | 0.0  | 0.0  | 5.4 | 0.0   | 0.0   | 8.4 |
| 0.0  | 0.0    |      | 8.1 |      |      |      |      |      |     |       |       |     |
|      | ( 222, | 220) |     | 0.0  | 9.9  | 0.0  | 0.0  | 2.4  | 0.0 | 0.0   | 0.0   | 0.0 |
| 0.0  | 0.0    | _    | 0.0 |      |      |      |      |      |     |       |       |     |
|      | (8220, | 220) |     |      |      |      |      |      |     |       |       |     |
|      | ( 220, | 222) |     | 0.0  | 0.0  | 13.6 | 0.0  | 0.0  | 6.1 | 0.0   | 0.0   | 0.9 |
| 0.0  | 0.0    | _    | 0.9 |      |      |      |      |      |     |       |       |     |
|      | ( 226, | 224) |     | 0.0  | 9.6  | 0.0  | 0.0  | 2.2  | 0.0 | 0.0   | 0.0   | 0.0 |
| 0.0  | 0.0    | _    | 0.0 |      |      |      |      |      |     |       |       |     |
|      | (8224, | 224) |     |      |      |      |      |      |     |       |       |     |
|      | ( 224, | 226) |     | 0.0  | 0.0  | 14.6 | 0.0  | 0.0  | 7.1 | 0.0   | 0.0   | 3.8 |
| 0.0  | 0.0    |      | 3.7 |      |      |      |      |      |     |       |       |     |
|      | ( 228, | 310) |     | 0.0  | 10.8 | 0.0  | 0.0  | 5.1  | 0.0 | 0.0   | 5.8   | 0.0 |
| 0.0  | 5.6    |      | 0.0 |      |      |      |      |      |     |       |       |     |
|      | ( 300, | 310) |     | 0.0  | 4.6  | 0.0  | 0.0  | 1.1  | 0.0 | 0.0   | 0.4   | 0.0 |
| 0.0  | 0.0    | _    | 0.0 |      |      |      |      |      |     |       |       |     |
|      | ( 310, | 302) |     | 0.0  | 10.4 | 0.0  | 0.0  | 3.0  | 0.0 | 0.0   | 0.1   | 0.0 |
| 0.0  | 0.0    | _    | 0.0 |      |      |      |      |      |     |       |       |     |
|      | (8302, | 302) |     |      |      |      |      |      |     |       |       |     |

| 0.0                  | 0.0                        | 0.0                    | 0.0 | 0.0     |              |                     |            | тсна       | THOTY       |             | 0.0       |                      |             | 0.0       |             | •           | c                         | 0.0      | 0.0        |             | 0.0         |         |
|----------------------|----------------------------|------------------------|-----|---------|--------------|---------------------|------------|------------|-------------|-------------|-----------|----------------------|-------------|-----------|-------------|-------------|---------------------------|----------|------------|-------------|-------------|---------|
| 3.9                  | 199.8                      | 5.3                    | 0.4 | 0.1     | BLE III      | E TIME**            | (SNIM-H    | тиви       |             |             | 0.0       | 471 9                | · · · · ·   | 2.8       |             | •           |                           | 70.7     | 230.3      |             | 0.3         |         |
| 0.0                  | 146.5                      | 0.0                    | 0.0 | 0.0     | STICS - TA   | QUEU                | (VE        | 1.12.12    |             |             | 0.0       | 247.3                |             | 0.0       | 0.0         | •           | c                         | 0.0      | 144.5      |             | 0.0         |         |
| 0.0                  | 0.0                        | 0.0                    | 0.0 | 0.0     | LEIC STATI   |                     |            | втснт      |             |             | 0.0       | 0.0                  | •           | 0.0       | 0.0         | )<br>,<br>) | c<br>c                    | 0.0      | 0.0        |             | 0.0         |         |
| 0.8                  | 40.2                       | 4.0                    | 1.3 | 4.1     | JENT SPEC    | AY TIME             | S/VEH)     | тнвп       |             |             | 1.1       | 40.3                 | )<br>-<br>- | 2.2       | 3.1         | <br>•       | o<br>c                    | 0.2      | 40.2       |             | 1.0         |         |
| 0.0                  | 47.2                       | 0.0                    | 0.0 | 0.0     | NETSIM MOVEN | DELP                | (SEC       | 1,         | 1           |             | 0.0       | 37.3                 | )<br>•<br>• | 0.0       | 0.0         | 1           | c                         |          | 42.2       |             | 0.0         |         |
| 0.0                  | 0.0                        | 0.0                    | 0.0 | 0.0     |              |                     |            | RIGHT      |             |             | 0.0       | 0.0                  | )<br>-<br>- | 0.0       | 0.0         |             |                           |          | 0.0        |             | 0.0         |         |
| 8.3                  | 43.3                       | 8.5                    | 4.8 | 19.0    |              | TOTAL TIME          | (SECS/VEH) | THRU       | 1           |             | 15.3      | 58.4                 |             | 6.6       | 10.6        |             | c 01                      | 7.01     | 42.9       |             | 2.8         |         |
| 0.0                  | 50.3<br>0.0                | 0.0                    | 0.0 | 0.0 0.0 |              | -                   |            | LEFT       | IGHT        |             | 0.0       | u.u<br>55.4          | 0.0         | 0.0       | 0.0         | 0.0         |                           | 0.0      | 44.9       | 0.0         | 0.0         | 0.0     |
| (302,304)<br>0.0 3.8 | ( 304, 300)<br>144.0 196.4 | ( 304, 306)<br>0.0 5.1 |     | 0.0 0.0 | 1            | LINK<br>STOD TIMF** |            | ( AEN-HAN) | LEFT THRU R | (8300, 308) | (308,307) | 0.0 0.0<br>(308,300) | 242.4 462.1 | (307,305) | ( 305, 303) | 0.0 0.0     | (8301, 303)<br>/ 303 301/ | 0.0 19.3 | (301, 300) | 142.3 226.8 | ( 300, 305) | 0.0 0.0 |

|     | ( 301, 227)            | 0.0    | 7.4 | 0.0  | 0.0 | 4.4 | 0.0  | 0.0 | 2.2 | 0.0  |
|-----|------------------------|--------|-----|------|-----|-----|------|-----|-----|------|
| 0.0 |                        | (<br>( |     | •    |     | •   |      |     |     |      |
| 0.0 | ( 311, 309)<br>0.0 0.0 | 0.0    | 1.1 | 0.0  | 0.0 | 1.3 | 0.0  | 0.0 | 0.0 | 0.0  |
| •   | (8309, 309)            |        |     |      |     |     |      |     |     |      |
|     | (309, 311)             | 0.0    | 0.0 | 14.3 | 0.0 | 0.0 | 8.4  | 0.0 | 0.0 | 11.6 |
| 0.0 | 0.0 11.5               |        |     |      |     |     |      |     |     |      |
|     | (315, 313)             | 0.0    | 9.7 | 0.0  | 0.0 | 2.2 | 0.0  | 0.0 | 0.0 | 0.0  |
| 0.0 | 0.0 0.0                |        |     |      |     |     |      |     |     |      |
|     | (8313, 313)            |        |     |      |     |     |      |     |     |      |
|     | (313, 315)             | 0.0    | 0.0 | 13.7 | 0.0 | 0.0 | 6.3  | 0.0 | 0.0 | 1.1  |
| 0.0 | 0.0 1.1                |        |     |      |     |     |      |     |     |      |
|     | (218, 317)             | 0.0    | 9.8 | 0.0  | 0.0 | 2.3 | 0.0  | 0.0 | 0.0 | 0.0  |
| 0.0 | 0.0 0.0                |        |     |      |     |     |      |     |     |      |
|     | (8317, 317)            |        |     |      |     |     |      |     |     |      |
|     | (317, 218)             | 0.0    | 0.0 | 17.0 | 0.0 | 0.0 | 9.5  | 0.0 | 0.0 | 1.9  |
| 0.0 | 0.0 1.8                |        |     |      |     |     |      |     |     |      |
|     | (323, 321)             | 0.0    | 9.3 | 0.0  | 0.0 | 1.9 | 0.0  | 0.0 | 0.0 | 0.0  |
| 0.0 | 0.0 0.0                |        |     |      |     |     |      |     |     |      |
|     | (8321, 321)            |        |     |      |     |     |      |     |     |      |
|     | (321, 323)             | 0.0    | 0.0 | 14.9 | 0.0 | 0.0 | 7.5  | 0.0 | 0.0 | 1.5  |
| 0.0 | 0.0 1.5                |        |     |      |     |     |      |     |     |      |
|     | (327, 325)             | 0.0    | 9.9 | 0.0  | 0.0 | 2.5 | 0.0  | 0.0 | 0.0 | 0.0  |
| 0.0 | 0.0 0.0                |        |     |      |     |     |      |     |     |      |
|     | (8325, 325)            |        |     |      |     |     |      |     |     |      |
|     | (325, 327)             | 0.0    | 0.0 | 17.1 | 0.0 | 0.0 | 9.6  | 0.0 | 0.0 | 2.0  |
| 0.0 | 0.0 1.9                |        |     |      |     |     |      |     |     |      |
|     | (331, 329)             | 0.0    | 9.6 | 0.0  | 0.0 | 2.1 | 0.0  | 0.0 | 0.0 | 0.0  |
| 0.0 | 0.0 0.0                |        |     |      |     |     |      |     |     |      |
|     | (8329, 329)            |        |     |      |     |     |      |     |     |      |
|     | (329, 331)             | 0.0    | 0.0 | 12.5 | 0.0 | 0.0 | 5.0  | 0.0 | 0.0 | 0.2  |
| 0.0 | 0.0 0.2                |        |     |      |     |     |      |     |     |      |
|     | (335, 333)             | 0.0    | 9.7 | 0.0  | 0.0 | 2.3 | 0.0  | 0.0 | 0.0 | 0.0  |
| 0.0 | 0.0 0.0                |        |     |      |     |     |      |     |     |      |
|     | (8333, 333)            |        |     |      |     |     |      |     |     |      |
|     | (333, 335)             | 0.0    | 0.0 | 18.6 | 0.0 | 0.0 | 11.2 | 0.0 | 0.0 | 43.7 |
| 0.0 | 0.0 40.8               |        |     |      |     |     |      |     |     |      |

| ( 337 | , 205) |      | 0.0  | 16.8 | 0.0  | 0.0  | 8.8  | 0.0 | 0.0   | 25.6  | 0.0  |
|-------|--------|------|------|------|------|------|------|-----|-------|-------|------|
| 24.   | 4      | 0.0  |      |      |      |      |      |     |       |       |      |
| (200  | , 205) |      | 0.0  | 4.6  | 0.0  | 0.0  | 0.6  | 0.0 | 0.0   | 0.5   | 0.0  |
| 0.    | 0      | 0.0  |      |      |      |      |      |     |       |       |      |
| (205  | , 201) |      | 0.0  | 4.5  | 0.0  | 0.0  | 0.8  | 0.0 | 0.0   | 0.3   | 0.0  |
| 0.    | 0      | 0.0  |      |      |      |      |      |     |       |       |      |
| (8201 | , 203) |      |      |      |      |      |      |     |       |       |      |
| (203  | , 275) |      | 0.0  | 42.0 | 0.0  | 0.0  | 38.2 | 0.0 | 0.0   | 702.3 | 0.0  |
| 663.  | 6      | 0.0  |      |      |      |      |      |     |       |       |      |
| ( 275 | , 200) |      | 53.2 | 61.5 | 0.0  | 50.6 | 58.9 | 0.0 | 436.5 | 294.8 | 0.0  |
| 2 29  | 1.7    | 0.0  | ~    |      |      |      |      |     |       |       |      |
| ( 275 | , 207) |      | 0.0  | 22.1 | 0.0  | 0.0  | 18.4 | 0.0 | 0.0   | 91.0  | 0.0  |
| 82.   | 6      | 0.0  |      |      |      |      |      |     |       |       |      |
| ( 217 | , 215) |      | 0.0  | 9.8  | 0.0  | 0.0  | 2.4  | 0.0 | 0.0   | 0.0   | 0.0  |
| .0    | 0      | 0.0  |      |      |      |      |      |     |       |       |      |
| (8215 | , 215) |      |      |      |      |      |      |     |       |       |      |
| (215  | , 217) |      | 0.0  | 0.0  | 16.3 | 0.0  | 0.0  | 8.8 | 0.0   | 0.0   | 4.3  |
| .0    | 0      | 4.2  |      |      |      |      |      |     |       |       |      |
| (225  | , 223) |      | 0.0  | 9.7  | 0.0  | 0.0  | 2.2  | 0.0 | 0.0   | 0.0   | 0.0  |
| 0.    | 0      | 0.0  |      |      |      |      |      |     |       |       |      |
| (8223 | , 223) |      |      |      |      |      |      |     |       |       |      |
| ( 223 | , 225) |      | 0.0  | 0.0  | 16.2 | 0.0  | 0.0  | 8.8 | 0.0   | 0.0   | 24.0 |
| 0     | 0      | 23.1 |      |      |      |      |      |     |       |       |      |
| ( 100 | , 104) |      | 0.0  | 15.0 | 0.0  | 0.0  | 3.0  | 0.0 | 0.0   | 8.6   | 0.0  |
| 4.    | 5      | 0.0  |      |      |      |      |      |     |       |       |      |
| ( 104 | , 108) |      | 0.0  | 11.7 | 15.2 | 0.0  | 4.4  | 7.9 | 0.0   | 8.8   | 0.3  |
| 0.    | 6      | 0.1  |      |      |      |      |      |     |       |       |      |
| (108  | , 110) |      | 0.0  | 7.5  | 0.0  | 0.0  | 2.2  | 0.0 | 0.0   | 6.7   | 0.0  |
| 0     | 0      | 0.0  |      |      |      |      |      |     |       |       |      |
| ( 110 | , 114) |      | 0.0  | 5.5  | 7.5  | 0.0  | 0.3  | 2.2 | 0.0   | 0.0   | 0.0  |
|       | 0      | 0.0  |      |      |      |      |      |     |       |       |      |
| ( 114 | , 116) |      | 0.0  | 8.9  | 0.0  | 0.0  | 0.6  | 0.0 | 0.0   | 0.1   | 0.0  |
| 0.    | 0      | 0.0  |      |      |      |      |      |     |       |       |      |
|       |        |      |      |      |      |      |      |     |       |       |      |

NETSIM MOVEMENT SPECIFIC STATISTICS - TABLE III

|        | LINK        |       | Ľ    | CTAL TIME  |       | DEL  | AY TIME |       | QUEU  | IE TIME** |       |
|--------|-------------|-------|------|------------|-------|------|---------|-------|-------|-----------|-------|
| 30105  |             |       | )    | (SECS/VEH) |       | (SE  | CS/VEH) |       | (VF   | (SUTM-H)  |       |
| (VEH-I | (SNIM       |       |      |            |       |      |         |       |       |           |       |
|        |             |       | LEFT | THRU       | RIGHT | LEFT | THRU    | RIGHT | LEFT  | THRU      | RIGHT |
| LEFT   | THRU        | RIGHT | _    |            |       |      |         |       |       |           |       |
|        | (116, 118)  | _     | 0.0  | 16.0       | 0.0   | 0.0  | 1.0     | 0.0   | 0.0   | 0.0       | 0.0   |
| 0.0    | 0.0         | 0.0   |      |            |       |      |         |       |       |           |       |
|        | (118, 122)  | ~     | 0.0  | 20.6       | 21.7  | 0.0  | 1.6     | 2.8   | 0.0   | 0.3       | 0.0   |
| 0.0    | 0.1         | 0.0   |      |            |       |      |         |       |       |           |       |
|        | (122, 125)  | _     | 0.0  | 5.3        | 0.0   | 0.0  | 2.4     | 0.0   | 0.0   | 19.3      | 0.0   |
| 0.0    | 11.7        | 0.0   |      |            |       |      |         |       |       |           |       |
|        | (125, 200)  | -     | 62.1 | 51.2       | 0.0   | 50.2 | 39.3    | 0.0   | 730.4 | 358.8     | 0.0   |
| 720.5  | 349.5       | 0.    | 0    |            |       |      |         |       |       |           |       |
|        | (200, 208)  |       | 0.0  | 6.2        | 0.0   | 0.0  | 1.1     | 0.0   | 0.0   | 0.4       | 0.0   |
| 0.0    | 0.0         | 0.0   |      |            |       |      |         |       |       |           | •     |
|        | (208, 212)  | ~     | 0.0  | 18.3       | 20.3  | 0.0  | 2.2     | 4.2   | 0.0   | 0.2       | 0.4   |
| 0.0    | 0.1         | 0.3   |      |            |       |      |         |       |       |           |       |
|        | (212, 216)  |       | 0.0  | 26.6       | 29.5  | 0.0  | 2.8     | 5.7   | 0.0   | 0.8       | 1.3   |
| 0.0    | 0.2         | 0.8   |      |            |       |      |         |       |       |           |       |
|        | (216, 218)  | _     | 0.0  | 12.8       | 0.0   | 0.0  | 1.3     | 0.0   | 0.0   | 1.7       | 0.0   |
| 0.0    | 0.0         | 0.0   |      |            |       |      |         |       |       |           |       |
|        | (218, 222)  | _     | 0.0  | 9.9        | 12.8  | 0.0  | 0.7     | 3.5   | 0.0   | 0.0       | 0.0   |
| 0.0    | 0.0         | 0.0   |      |            |       |      |         |       |       |           |       |
|        | (222, 226)  | _     | 0.0  | 18.6       | 20.1  | 0.0  | 1.4     | 2.9   | 0.0   | 0.2       | 0.0   |
| 0.0    | 0.0         | 0.0   |      |            |       |      |         |       |       |           |       |
|        | (226, 228)  | _     | 0.0  | 18.1       | 0.0   | 0.0  | 4.1     | 0.0   | 0.0   | 29.6      | 0.0   |
| 0.0    | 26.5        | 0.0   |      |            |       |      |         |       |       |           |       |
|        | (228, 300)  | _     | 41.7 | 41.1       | 0.0   | 38.4 | 37.7    | 0.0   | 96.2  | 381.2     | 0.0   |
| 94.7   | 374.2       | 0.0   | _    |            |       |      |         |       |       |           |       |
|        | ( 300, 227) | _     | 0.0  | 3.0        | 0.0   | 0.0  | 0.9     | 0.0   | 0.0   | 0.4       | 0.0   |
| 0.0    | 0.0         | 0.0   |      |            |       |      |         |       |       |           |       |
|        | (227, 311)  | -     | 0.0  | 20.3       | 20.9  | 0.0  | 2.4     | 3.0   | 0.0   | 0.0       | 0.0   |
| 0.0    | 0.0         | 0.0   |      |            |       |      |         |       |       |           |       |

| 0.3         | 0.1                    | 0.0      | 0.0                    | 0.1      | 0.0 | 0.0                 | 0.0               | 0.0      | 0.0                                   | 0.0             | 0.0                    | 0.2      | 0.0             | 0.0      | 0.2      | 6.0               |
|-------------|------------------------|----------|------------------------|----------|-----|---------------------|-------------------|----------|---------------------------------------|-----------------|------------------------|----------|-----------------|----------|----------|-------------------|
| 1.3         | 0.2                    | 0.2      | 0.2                    | 0.4      | 0.1 | 7.7                 | 571.9             | 0.5      | 0.4                                   | 0.0             | 0.7                    | 0.5      | 0.4             | 0.1      | 1.4      | 201.4             |
| 0.0         | 0.0                    | 0.0      | 0.0                    | 0.0      | 0.0 | 0.0                 | 330.5             | 0.0      | 0.0                                   | 0.0             | 0.0                    | 0.0      | 0.0             | 0.0      | 0.0      | 373.3             |
| 5.2         | 3.7                    | 2.7      | 3.4                    | 3.4      | 2.4 | 0.0                 | 0.0               | 0.0      | 0.0                                   | 0.0             | 0.0                    | 3.8      | 0.0             | 0.0      | 3.9      | 17.9              |
| 1.8         | 1.1                    | 1.0      | 1.0                    | 0.9      | 0.8 | 2.3                 | 48.8              | 1.3      | 1.8                                   | 1.0             | 1.9                    | 1.4      | 0.7             | 1.8      | 2.0      | 22.9              |
| 0.0         | 0.0                    | 0.0      | 0.0                    | 0.0      | 0.0 | 0.0                 | 53.4              | 0.0      | 0.0                                   | 0.0             | 0.0                    | 0.0      | 0.0             | 0.0      | 0.0      | 30.9              |
| 19.1        | 13.6                   | 12.7     | 12.8                   | 12.8     | 9.6 | 0.0                 | 0.0               | 0.0      | 0.0                                   | 0.0             | 0.0                    | 13.8     | 0.0             | 0.0      | 17.1     | 27.7              |
| 15.7        | 11.0                   | 11.0     | 10.4                   | 10.2     | 8.0 | 15.2                | 55.5              | 4.3      | 11.6                                  | 8.3             | 16.8                   | 11.5     | 5.5             | 16.7     | 15.2     | 32.8              |
| 0.0         | 0.0                    | 0.0      | 0.0                    | 0.0      | 0.0 | 0.0                 | 60.1              | 0.0      | 0.0                                   | 0.0             | 0.0                    | 0.0      | 0.0             | 0.0      | 0.0      | 40.7              |
| ()          |                        |          |                        |          |     |                     |                   |          |                                       |                 | 0.0<br>0.0             |          |                 |          |          |                   |
| 311, 315    | 0.2<br>315, 218<br>0 0 | 218, 323 | и.т<br>323, 327<br>0 0 | 327, 331 |     | 335, 337<br>35, 337 | 337, 200<br>560 5 | 200, 207 | 207, 209                              | 0.0<br>209, 211 | 0.0<br>211, 213<br>0 5 | 213, 217 | 217, 219<br>0 0 | 219, 221 | 221, 225 | 225, 100<br>189.8 |
| )<br>,<br>, | , o<br>0.0             |          |                        |          |     |                     | 326.7             | ) ) ) )  | , , , , , , , , , , , , , , , , , , , | 0.0             | )<br>0.0               |          |                 |          |          | 357.8             |

\*\* TIME FOR VEHICLES CURRENTLY ON THE LINK ARE INCLUDED IN THESE VALUES.

3500). 429 VEHICLES (MAXIMUM ALLOWED IS THE HIGHEST NUMBER OF VEHICLES ON THE NETWORK WAS THIS MAXIMUM OCCURED AT 3321 SECONDS.

0\*\*\*\*\* THERE WERE 1 WARNING MESSAGES IN DATA FOR CASE 1.

1

MESSAGE DESCRIPTION

Specified oncoming link (P1,P2) may not have been specified correctly. Its traffic opposes traffic on link (P3,P2) but no receiving link (P2,P3) was input. Check Record Type 11. 500 ł

TOTAL CPU TIME FOR SIMULATION = 192.40 SECONDS TOTAL CPU TIME FOR THIS RUN = 192.46 SECONDS 0LAST CASE PROCESSED
Appendix D

TRAF-NETSIM Simulation output

Validation Network Calibrated Model

INPUT FILE NAME: SMOC1.TRF RUN DATE : 08/15/99

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FFFFFFFFFFF FFFFFFFFFFF FFFFFFFFFFFF FFFFFF FFFFFF FFF FFF ЕFF ЕFF FF FFF ЕFF AAA AAA AAA AAA AAA AAA AAA AAAAAAAAAAA AAAAAAAAAAA AAAAAAAAAAA AAAAAAAA AAAAAAA AAA AAA AAA AAA AAA AAA AAA RRR RRR RRRRRRRRRR RRRRRRRR RRR RRRRRRRRRR RRR RRRRRRRRR RRR RRRRRRRR RRR RRR RRR RRR RRR RRR RRR RRR RRR TTTTTTTTTT TTTTTTTTTT TTTTTTTTTT TTT TTTTTTTTT TTT TTTTTT TTT TTT

MICRO-COMPUTER PROTECTED-MODE VERSION (REQUIRES 80386 AND 80387 OR ABOVE)

VERSION 5.00 RELEASE DATE MAR 1995 TRAF SIMULATION MODEL

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DEVELOPED FOR

INTELLIGENT VEHICLE HIGHWAY SYSTEM RESEARCH DIVISION U. S. DEPARTMENT OF TRANSPORTATION FEDERAL HIGHWAY ADMINISTRATION

START OF CASE

CARD FILE LIST

| 1      |         |               |    | CAR          | ID FILE LIST |       |    |        |      |     |
|--------|---------|---------------|----|--------------|--------------|-------|----|--------|------|-----|
| OSEQ.# | +       | 1             | -2 | -+3+         | 445          | +     | 9  | +      | +    | 8 - |
| 1      | :Validé | ation Network | :  | afeway Stree | t            |       |    |        |      | 0   |
| 2      |         |               | ž  | JNDAY, JUNE  | 29 , 1998    |       |    |        |      | 0   |
| č      |         |               | Ĥ  | 3:00 14:00   |              |       |    |        |      | 0   |
| 4      |         |               |    |              |              |       |    |        |      | 0   |
| 2      | :Sami   | Said Ghezawi  |    |              | 11 03 98     |       |    |        | 10   |     |
| 9      | 0<br>   | 1             | 0. |              | 1 0          | 31300 |    | 132841 | 7581 | 2   |
| 7      | :3600   |               |    |              |              |       |    |        |      | m   |
| 8      |         |               |    |              |              |       |    |        |      | 4   |
| 6      | ••      |               |    |              | 1            |       |    |        |      | £   |
| 10     | :8101   | 101           | 2  | 02           | 100          |       | 18 | 15     |      | 11  |
| 11     | :8104   | 104           | m  | 02           | 100          |       | 18 | 15     |      | 11  |
| 12     | :8202   | 202           | 2  | 02           | 200          |       | 18 | 15     |      | 11  |
| 13     | : 8222  | 222           | 2  | 02           | 220          |       | 18 | 15     |      | 11  |
| 14     | :8242   | 242           | 2  | 02           | 240          |       | 18 | 15     |      | 11  |
| 15     | :8302   | 302           | 2  | 02           | 300          |       | 18 | 15     |      | 11  |
| 16     | :8301   | 301           |    | 02           | 300          |       | 18 | 15     |      | 11  |

|       | +401  |       | 104   |       |         |       |       | 400     |       |       |       | 300     | 220     |       |       |       | 240              |       | 300   |       | 310   |       | 200   | 8401  |       | 202     | 222   | 242   | 302     |         | 301     | 311   | 201     | 101   |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|---------|-------|-------|---------|-------|-------|-------|---------|---------|-------|-------|-------|------------------|-------|-------|-------|-------|-------|-------|-------|-------|---------|-------|-------|---------|---------|---------|-------|---------|-------|-------|-------|-------|-------|-------|-------|
| 310   | 400   | 400   | 200   | 8101  | 101 200 | 8104  | 8302  | 310 301 | 8403  | 300   | 8401  | 403 402 | 100 201 | 8202  | 8201  | 8222  |                  | 8242  |       | 8301  |       | 8311  |       |       | 8402  | 201 220 | 240   | 300   | 301 400 | 401 403 | 302 310 | 200   | 202 100 | 104   |       |       |       |       |       |       |
| -32   | 02    | 02    | 02411 | 02    | +42 81  | -42   | 02    | 1 0281  | -32   | +32   | 02    | 024     | 02481   | 02    | +22   | 02    | 02               | 02    | 02    | 02    | 02    | +32   | -32   | 02    | 02    | +12     | 02    | -32   | 1-72    | -32 8   | +32 8   | +72   | +52     | 1-12  |       |       |       |       |       |       |
| -1    | ო     | с     | e     | 2     | m       | ო     | m     | 40 2    | т     | m     | ო     | 4       | m       | 2     | 2     | 2     | <del>, - 1</del> | 2     |       | Ч     | Ч     |       |       | -     | 1     | 31      | m     | e     | 40 3 1  | 31      | 31      | m     | 31      | 35 3  |       |       |       |       |       |       |
|       |       |       |       |       |         |       |       |         |       |       |       |         |         |       |       |       |                  |       |       |       |       |       |       |       |       | 30      |       |       | 50      | 100     | 100     |       | 40      |       | 100   | 100   | 100   | 100   | 100   | 100   |
|       |       |       | 400   | 400   | 400     | 400   | 400   | 400     | 400   | 400   | 400   | 400     | 400     | 400   | 100   | 100   | 100              | 100   | 100   | 100   | 100   | 100   | 100   | 285   | 50    | 140     | 122   | 92    | 326     | 211     | 210     | 228   | 310     | 147   |       |       |       |       |       |       |
| 311   | 403   | 401   | 100   | 101   | 100     | 104   | 302   | 300     | 403   | 400   | 401   | 400     | 200     | 202   | 201   | 222   | 220              | 242   | 240   | 301   | 300   | 311   | 310   | 401   | 402   | 200     | 220   | 240   | 300     | 400     | 300     | 310   | 200     | 100   | 401   | 101   | 104   | 202   | 222   | 242   |
| :8311 | :8403 | :8401 | : 101 | : 100 | : 104   | : 100 | : 300 | : 302   | : 400 | : 403 | : 400 | : 401   | : 202   | : 200 | : 200 | : 220 | : 222            | : 240 | : 242 | : 300 | : 301 | : 310 | : 311 | : 403 | : 400 | : 100   | : 200 | : 220 | : 240   | : 300   | : 400   | : 300 | : 310   | : 200 | :8401 | :8101 | :8104 | :8202 | :8222 | :8242 |
| 17    | 18    | 19    | 20    | 21    | 22      | 23    | 24    | 25      | 26    | 27    | 28    | 29      | 30      | 31    | 32    | 33    | 34               | 35    | 36    | 37    | 38    | 39    | 40    | 41    | 42    | 43      | 44    | 45    | 46      | 47      | 48      | 49    | 50      | 51    | 52    | 53    | 54    | 55    | 56    | 57    |

|      |      |      | ß    |     |       |     |     |      |      |     |     |      |      |      |     |      |      |      |     |     |     |     | 100 |     |     |     |     |     |     |     |     |     |     |     |     |     |     |      |     |      |
|------|------|------|------|-----|-------|-----|-----|------|------|-----|-----|------|------|------|-----|------|------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|-----|------|
|      |      |      |      | 99  |       | 056 | 100 | 55   | 204  | 10  | 38  | 40   | 53   |      | 112 | 952  | 52   | 19   | 100 | 100 | 100 |     | +   |     |     |     |     |     |     |     |     |     |     |     |     |     |     | 400  |     |      |
| 100  | 100  | 100  | 95   | 10  | 1311  | 321 |     | 1620 | 1549 | 90  | 32  | 1871 | 1619 | 1078 |     | 1273 | 1657 | 1661 |     |     |     | 100 |     | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 200 | 220 | 403  | 300 | 100  |
|      |      |      |      | 24  | 10451 | 283 |     | 6821 | 48]  |     | 367 | 1721 | 351  | 5231 | 826 | -    | -    | -    |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     | 222 | 242 | 3401 | 311 | 3101 |
| 302  | 301  | 311  | 403  | 400 | 400   | 300 | 300 | 300  | 300  | 310 | 200 | 200  | 200  | 100  | 100 | 100  | 220  | 240  | 220 | 240 | 310 | 400 | 401 | 104 | 202 | 242 | 301 | 401 | 403 | 101 | 201 | 222 | 302 | 311 | 402 |     |     | w    |     | w    |
| 3302 | 3301 | 3311 | 3403 | 401 | 300   | 302 | 301 | 400  | 240  | 300 | 202 | 310  | 100  | 104  | 101 | 200  | 200  | 220  | 222 | 242 | 311 | 403 | 403 | 100 | 200 | 240 | 300 | 400 | 400 | 100 | 200 | 220 | 300 | 310 | 400 | 220 | 240 | 401  | 310 | 101  |
|      |      |      |      | ••  | ••    | ••  | ••  | ••   | ••   | ••  | ••  | ••   | ••   | ••   | ••  | ••   | ••   | ••   | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••   | ••  | ••   |
| 58   | 59   | 60   | 61   | 62  | 63    | 64  | 65  | 66   | 67   | 68  | 69  | 70   | 71   | 72   | 73  | 74   | 75   | 76   | LL  | 78  | 79  | 80  | 81  | 82  | 83  | 84  | 85  | 86  | 87  | 88  | 89  | 90  | 91  | 92  | 93  | 94  | 95  | 96   | 97  | 98   |

£

|     |      |     |      |      |     |     |      |     |      |     |     |       |     |     |     |     |     |     |     |     |     |       |     |     |       |       |         |       | 01    | 01    |     |     |     |     |     |     |     |     |     |     |
|-----|------|-----|------|------|-----|-----|------|-----|------|-----|-----|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-------|-----|-----|-------|-------|---------|-------|-------|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
|     |      |     |      |      |     |     |      |     |      |     |     |       |     |     |     |     |     |     |     |     |     |       |     |     |       |       |         |       | 10    | 10    |     |     |     |     |     |     |     |     |     |     |
|     |      |     |      |      |     |     |      |     |      |     |     |       |     |     |     |     |     |     |     |     |     |       |     |     |       |       |         |       |       |       |     |     |     |     |     |     |     |     |     |     |
|     |      |     |      |      |     |     |      |     |      |     |     |       |     |     |     |     |     |     |     |     |     |       |     |     |       |       |         |       |       |       |     |     |     |     |     |     | 111 | 211 | 221 | 221 |
|     |      |     |      |      |     |     |      |     |      |     |     |       |     |     |     |     |     |     |     |     |     |       |     |     |       |       | 300     |       | 45    | 45    |     |     |     |     |     |     |     |     |     |     |
|     |      |     |      |      |     |     |      |     |      |     |     |       |     |     |     |     |     |     |     |     |     |       |     |     |       |       | 240     |       | 25    | 25    | 21  | 22  | 11  | 211 | 221 | 121 | 221 | 221 | 221 | 111 |
|     |      |     |      |      |     |     |      |     |      |     |     |       |     |     |     |     |     |     |     |     |     |       |     |     | 1 100 | 0 200 | 2 300   | 400   |       |       |     |     |     |     |     |     |     |     |     |     |
|     |      |     |      |      |     |     |      |     |      |     |     |       |     |     |     |     |     |     |     |     |     |       |     |     | 0 104 | 0 100 | 0 302   | 0 300 | 25    | 25    | 11  | 21  | 22  | 222 | 111 | 222 | 221 | 211 | 111 | 221 |
| 0   | 0    |     | 0    | 0    | 0   | 0   | 0    |     | 0    |     |     |       |     |     |     |     |     |     |     |     |     |       |     |     | 0 10  | 2 20  | õe<br>o | 3 40  | 50    | 5     |     |     |     |     |     |     |     |     |     |     |
| 10  | 20   |     | 22   | 24   | 30  | 30  | 40   |     | 31   |     |     |       |     |     |     |     |     |     |     |     |     |       |     |     | 20    | 20    | 40      | 40    | 5     | 4     |     |     |     |     |     |     |     |     |     |     |
| 104 | 3202 | 200 | 3222 | 3242 | 301 | 302 | 3403 | 400 | 3311 |     |     |       |     |     |     |     |     |     |     |     |     |       |     |     | 100   | 200   | 300     | 400   | 30 25 | 30 25 | 2 2 | 1 1 | 2 2 | 211 | 221 | 121 | 221 | 221 | 221 | 221 |
| ω   | ω    |     | ω    | ω    | ω   | ω   | ω    |     | ω    | .0  | .0  | ~     |     | _   | _   | _   | _   | _   |     | 1   |     |       | _   |     | 101   | 310   | 301     | 10T   | 75 .  | 75    | 2   | ო   | Ч   | 2   | е   | 1   | Ч   | 0   | ო   | 4   |
| 104 | 202  | 201 | 222  | 242  | 301 | 302 | 403  | 402 | 311  | 220 | 240 | 401 ( | 310 | 101 | 104 | 202 | 201 | 222 | 242 | 301 | 302 | 311 . | 402 | 403 | 100   | 200   | 300     | 400   | . 001 | 200   | 100 | 100 | 100 | 200 | 200 | 200 | 300 | 300 | 300 | 300 |
| ••• | ••   | ••  | ••   | ••   | ••  | ••  | ••   | ••  | ••   | ••  | ••  | ••    | ••  | ••  | ••• | ••  | ••  | ••• | ••  | ••  | ••  | ••    | ••  | ••  |       |       | ••      | ••    | ••    | ••    | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  |
| 66  | 100  | 101 | 102  | 103  | 104 | 105 | 106  | 107 | 108  | 109 | 110 | 111   | 112 | 113 | 114 | 115 | 116 | 117 | 118 | 119 | 120 | 121   | 122 | 123 | 124   | 125   | 126     | 127   | 128   | 129   | 130 | 131 | 132 | 133 | 134 | 135 | 136 | 137 | 138 | 139 |

T77

| Ч   | -   | 2   |     |     |     |     |     |     |     |     |     |     |     |     |               |     |     |     |     |     |     |     |     |     |     |     |     |        |     |     |     |     |     |     |     |      |      |      |      |      |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|---------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|--------|-----|-----|-----|-----|-----|-----|-----|------|------|------|------|------|
| -   | 2   | 2   | Ч   | 1   |     | ٦   |     |     |     | Ч   | 1   |     |     |     | <del> 1</del> | 1   | Ч   | Ъ   | Ч   | Ч   | ч   | 7   | 0   | ٢   | 7   | 0   | ٢   | പ      | ß   | പ   | പ   | പ   | പ   | ъ   | പ   |      |      |      |      |      |
|     |     |     | 10  | 10  | 10  | 10  | 10  | 10  | 50  | 50  | 10  | 50  | 10  | 10  | 10            | 10  | 10  | 10  | 50  | 10  | 10  | 10  | ~   |     |     |     |     |        |     |     |     |     |     |     |     |      |      |      |      |      |
|     |     |     | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0             | 0   | 0   | 0   | 0   | 0   | 0   | 0   |     |     |     |     |     |        |     |     |     |     |     |     |     |      |      |      |      |      |
| 2   | ٦   | 2   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 0             | 0   | 0   | 0   | 0   | 0   | 0   | 0   |     |     |     |     |     |        |     |     |     |     |     |     |     |      |      |      |      |      |
|     |     |     | 50  | 50  | 50  | 50  | 50  | 50  | 50  | 50  | 50  | 50  | 50  | 50  | 50            | 50  | 50  | 50  | 50  | 50  | 50  | 50  | 0   | 0   | 0   | 0   | 0   | 0      | 0   | 0   | 0   | 0   | 0   | 0   | 0   | 2    | 2    | 1    |      |      |
|     |     | 7   | 6   | 6   | 6   | 13  | 13  | 12  | 7   | L   | 13  | 2   | 12  | 13  | 12            | m   | 6   | 13  | 5   | 6   | :13 | 6   | 203 | 73  | 73( | 203 | 73  | ъ<br>Э | 53  | 53  | 53  | 53  | 53  | 53  | 53  | 80   | 35   | 11   | L 1  | 12   |
| 22  | 22  | 11  | 2   | Ч   | m   |     | m   | 2   | Ч   | m   | 4   | 4   | ~   | 4   | N             | ~   | ო   | ო   | ო   | 2   | (m  |     |     | 25  | 20  |     | 25  | 20     | 10  | 80  | 30  | 15  | 40  | 50  | 45  | 126  | 188  | 137  |      | Ļ.   |
| Ч   | 2   | ო   | 2   | 2   | 2   | 2   | 2   | 2   | 2   | 2   | 2   | 2   | 2   | 2   | 2             | 2   | 2   | 2   | 2   | 2   | 2   | 2   |     |     |     |     | ~   |        |     | • • | ~   |     |     | ~ 1 | ~   | 101  | 103  | 302  | 301  | 311  |
|     |     |     | 2   | m   |     | 2   | 2   | m   | Ч   | Ч   |     | ~-1 | 2   | 2   | ന             | ო   | 4   |     | Ч   | 2   | 2   | ო   | 2   | (7) |     | ~   | (1) |        | Ч   | ~   | (1) | v   | -   | ~   | ,   | 7.   | 7.   |      |      | (.)  |
| 400 | 400 | 400 | 100 | 100 | 100 | 200 | 200 | 200 | 200 | 200 | 300 | 300 | 300 | 300 | 300           | 300 | 300 | 400 | 400 | 400 | 400 | 400 | 100 | 100 | 100 | 200 | 200 | 200    | 300 | 300 | 300 | 300 | 400 | 400 | 400 | 8401 | 8403 | 8302 | 8301 | 8311 |
| ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••            | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••     | ••  | ••  | ••  | ••  | ••  | ••  | ••  | ••   | ••   | ••   | ••   | ••   |
| 140 | 141 | 142 | 143 | 144 | 145 | 146 | 147 | 148 | 149 | 150 | 151 | 152 | 153 | 154 | 155           | 156 | 157 | 158 | 159 | 160 | 161 | 162 | 163 | 164 | 165 | 166 | 167 | 168    | 169 | 170 | 171 | 172 | 173 | 174 | 175 | 176  | 177  | 178  | 179  | 180  |

| -10        | 0   | Ч    | 0   | 0   | 0   | ٦   | 0   | Ч   | 0   | ٦   |     |
|------------|-----|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 1111       | 1 1 | 1111 | 1 1 | 1 1 | 1 1 | 11  | 1 1 | 1 1 | 1 1 | 1 1 | 1 1 |
| 10         |     | 10   | 10  | 10  |     |     | 10  | 10  | 10  | 10  | 10  |
| 90 go      | 30  | 30   | 30  | 30  | 30  | 30  | 30  | 30  | 30  | 30  | 30  |
| 300<br>300 | 300 | 300  | 300 | 300 | 300 | 300 | 300 | 300 | 300 | 300 | 300 |
| 300<br>300 | 300 | 300  | 300 | 300 | 300 | 300 | 300 | 300 | 300 | 300 | 300 |

| .0 | 0 | ŝ | 6 | 6 | 6 | G | s | ဖ | s | 6 | ە | ە | ە | ى | و | و | و | 9 | ە | و | و | ە | ~ | ~ | 2 | ~ | 5 | 7 | 2 | 5 | 5 | 5 | - | 7 | 2 | 0 | 0 | 0 | 0 | 0 |
|----|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 4  | 4 | 4 | 4 | 4 | 4 | ব | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | Ą | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | S | ഹ | വ | ഹ | S |

| 50  | 50  | 50   | 50  | 50  | 51   | 51     | 51  | 51  | 51   | 149 | 149    | 1/0 | 195  | 195 | 195  | 195  | 195  | 195  | 195         | 195  | 195  | 195  | 195  | 195<br>195 | 195  | 76T  | 195  | 195  | 195  | 195  | 195  | 210 | 88                                      |
|-----|-----|------|-----|-----|------|--------|-----|-----|------|-----|--------|-----|------|-----|------|------|------|------|-------------|------|------|------|------|------------|------|------|------|------|------|------|------|-----|---|
|     |     |      |     |     |      |        |     |     |      |     |        |     |      |     |      |      |      |      |             |      |      |      |      |            |      |      |      |      |      |      |      |     | <br>+<br> <br>                          |
|     |     |      |     |     |      |        |     |     |      |     |        |     |      |     |      |      |      |      |             |      |      |      |      |            |      |      |      |      |      |      |      | I   |   |
|     |     |      |     |     |      |        |     |     |      |     |        |     |      |     |      |      |      |      |             |      |      |      |      |            |      |      |      |      |      |      |      |     | <br>+<br> <br> <br>                     |
|     |     |      |     |     |      |        |     |     |      |     |        |     |      |     |      |      |      |      |             |      |      |      |      |            |      |      |      |      |      |      |      | 1   | 9                                       |
|     |     |      |     |     |      |        |     |     |      |     |        |     |      |     |      |      |      |      |             |      |      |      |      |            |      |      |      |      |      |      |      |     | +++++++++++++++++++++++++++++++++++++++ |
|     |     |      |     |     |      |        |     |     |      |     | _      |     |      |     |      |      |      |      |             |      |      |      |      |            |      |      |      |      |      |      |      |     |   |
|     |     |      |     |     |      |        |     |     |      | 3   | 5<br>G |     |      |     |      |      |      |      |             |      |      |      |      |            |      |      |      |      |      |      |      |     | +                                       |
|     |     |      |     |     |      |        |     |     |      | 37  | 67     |     |      |     |      |      |      |      |             |      |      |      |      |            |      |      |      |      |      |      |      |     |   |
|     |     |      |     |     |      |        |     |     |      | 48  | 75     |     |      |     |      |      |      |      |             |      |      |      |      |            |      |      |      |      |      |      |      |     | 6                                       |
|     |     |      |     |     |      |        |     |     |      | 64  | 81     |     |      |     |      |      |      |      |             |      |      |      |      |            |      |      |      |      |      |      |      |     | <br> <br> <br> <br>                     |
|     |     |      |     |     |      |        |     |     |      | 83  | 88     |     |      |     |      |      |      |      |             |      |      |      |      |            |      |      |      |      |      |      |      |     |   |
|     |     |      |     |     |      |        |     |     |      | 101 | 95     |     |      |     |      |      |      |      |             |      |      |      |      |            |      |      |      |      |      |      |      |     | +                                       |
|     |     |      |     |     |      |        |     |     |      | 121 | 105    |     |      |     |      |      |      |      |             |      |      |      |      |            |      |      |      |      |      |      |      |     |   |
|     |     |      |     |     |      |        |     |     |      | 141 | 118    |     | 502  | 285 | 302  | 384  | 284  | 334  | 347         | 297  | 351  | .301 | .353 | 403        | 1398 | 148  | 1348 | 1543 | 1343 | 1343 | 1293 |     | 2                                       |
|     | -   | 2    |     |     | 422  | 8<br>1 | 9-  | 45  | 197  | 169 | 134    |     |      | Ч   | -    | Π    | -1   | Г    |             | -    | -    | -    |      | •          |      | ••   | ••   |      | •••  | •••  | •••  |     | i<br>+<br>!                             |
| 437 | 938 | 601  | 4   | 144 | 400- | 300    | 300 | 200 | 200- | 211 | 180    |     | 1019 | 819 | 1019 | 1159 | 1159 | 1159 | 1267        | 1267 | 1358 | 1358 | 1484 | 1484       | 1699 | 1699 | 1699 | 1910 | 2110 | 1910 | 1910 |     | - <del>-</del>                          |
| 202 | 101 | 1041 | 222 | 242 | 300  | 400    | 240 | 310 | 100  | 0   | -      |     |      |     | -    | •    |      |      | <b>F</b> -1 | • •  | • •  | • •  | •••  | • •        | • •  |      |      |      |      |      |      |     |   |
| 202 | 101 | 104  | 222 | 242 | 300  | 400    | 200 | 500 | 100  | 2   | 2      | 0   | 101  | 104 | 100  | 201  | 202  | 200  | 220         | 222  | 240  | 242  | 310  | 311        | 301  | 302  | 300  | 401  | 403  | 400  | 402  |     |   |
| 8   | ω.  | 8    | 8   | 8   | .2   | ~      | :2  | 2   | :2   | ••  | ••     | ••  | ••   | ••  | ••   | ••   | ••   |      |             | ••   | ••   | ••   | ••   | •••        | •••  |      |      |      |      | ••   |      |     | <br>+                                   |
| 181 | 182 | 183  | 184 | 185 | 186  | 187    | 188 | 189 | 190  | 191 | 192    | 193 | 194  | 195 | 196  | 197  | 198  | 199  | 200         | 201  | 202  | 203  | 204  | 205        | 206  | 207  | 206  | 205  | 210  | 211  | 212  | 213 | OSEQ.                                   |

## TRAF SIMULATION MODEL

### DEVELOPED FOR

## FEDERAL HIGHWAY ADMINISTRATION INTELLIGENT VEHICLE HIGHWAY SYSTEM RESEARCH DIVISION U. S. DEPARTMENT OF TRANSPORTATION

\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*

---START OF CASE

| ******     | ******** | ***************************************  |
|------------|----------|--|
| ********** | *******  |  |
| 00000      | Val.     | dation Network : Safeway Street<br>MONDAY, JUNE 29 , 1998<br>13:00 14:00   |
| 0 0 1      |          | DATE = 11/ 03/ 98<br>USER = Sami Said Ghezawi<br>AGENCY =<br>RUN CONTROL DATA  |
|            | VALUE    | RUN PARAMETERS AND OPTIONS   |
| 000        | 10<br>1  | RUN IDENTIFICATION NUMBER<br>NEXT CASE CODE = (0,1) IF ANOTHER CASE (DOES NOT, DOES) FOLLOW<br>RUN TYPE CODE = (1, 2, 3) TO RUN (SIMULATION, ASSIGNMENT, BOTH)<br>(-1,-2,-3) TO CHECK (SIMULATION, ASSIGNMENT, BOTH) |
| ONLY       |          |  |
| 0          |          | NETSIM ENVIRONMENTAL OPTIONS   |

FUEL/EMISSION RATE TABLES ARE NOT PRINTED

| 0                            | SIMULATION:                        | PERFORMED   | ENVIRO   | NMENTAL                |
|------------------------------|------------------------------------|---|--|------------------------|
| MEASURES: CALCULATED         | DATE TADIES.                       | MBFDDFD   | ΨRΔ.ΤΓ.  | TORV FILE.             |
| NOT WRITTEN                  | CALA IABLAN                        | 1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1 | DEDANT   |                        |
| 1.0                          | INPUT UNITS (                      | CODE = (0, 1) IF INPUT  | IS IN (ENGLISH, METRIC)                        | UNITS                  |
| ENGLISH, METRIC, BOTH) UNITS |                                    | 0 IT /0/7/7/0/ _ HOV  |  | 110                    |
| 1300                         | CLOCK TIME AT                      | START OF SIMULATION   | (ММНН)   |                        |
| 0 0                          | SIGNAL TRANSI                      | $\GammaION CODE = (0, 1, 2, 3)$   | IF (NO, IMMEDIATE, 2-CY                        | CLE, 3-                |
| CYCLE) TRANSITION WAS REQUES | TED                                |   |  |                        |
| 0 132841 132841              | RANDOM NUMBER<br>RANDOM NUMBER     | SEED TO GENERATE TRA  | FFIC STREAM FOR NETSIM O                       | R LEVEL I              |
| SIMULATION                   |                                    |   |  |                        |
| 3600                         | DURATION (SEC                      | OF TIME PERIOD NO.  | 1  |                        |
| 0 60*                        | LENGTH OF A T                      | IME INTERVAL, SECONDS   |  |                        |
| 0 10                         | MAXIMUM INITI                      | ALIZATION TIME, NUMBE   | R OF TIME INTERVALS                            |                        |
| 0 0                          | NUMBER OF TIM                      | INTERVALS BETWEEN S   | UCCESSIVE STANDARD OUTPU                       | ITS                    |
| 0 0                          | TIME INTERMED                      | LATE OUTPUT WILL BEGI   | N AT INTERVALS OF 0 S                          | ECS. FOR               |
| 0 SECS. FOR MICROSCOPIC MODE | LS                                 |   |  |                        |
| 0 1 при спривенного 1        | NETSIM MOVEMEI                     | NT-SPECIFIC OUTPUT CO   | DE = (0, 1) (IF NOT, IF)                       | REQUESTED              |
| FOR NEISIM SUBNEIWORN        | NETSIM GRAPHI                      | CS OUTPUT CODE = (0,1   | .) IF GRAPHICS OUTPUT (IS                      | NOT, IS)               |
| REQUESTED                    |                                    |   |  |                        |
| *                            | VALUE ASSERTED<br>TIME INTERVAL DI | 3Y THE MODEL FOR THE<br>JRATION OMITTED. DEFA   | FOLLOWING REASON -<br>NULT VALUE OF 60 SECONDS | ASSUMED.               |
|                              |                                    | INITIALIZATION ST   | ATISTICS                                       |                        |
| TIME INTERVAL<br>NUMBER      | SUBNETWORK<br>TYPE                 | PRIOR CONTENT<br>(VEHICLES)   | CURRENT CONTENT<br>(VEHICLES)                  | PERCENT<br>DI FFERENCE |
| 1                            | NETSIM                             | 0   | 128  | 10000                  |
| 2                            | NETSIM                             | 128   | 217  | 69                     |
| ¢                            | NETSIM                             | 217   | 281  | 29                     |
| 4                            | NETSIM                             | 281   | 308  | 6                      |
| 5                            | NETSIM                             | 308   | 288  | 9                      |
| EQUILIBRIUM ATTAINED         |                                    |   |  |                        |
|                              | A                                  | LL EXISTING SUBNETWOR   | KKS REACHED EQUILIBRIUM                        |                        |

CUMULATIVE NETSIM STATISTICS AT TIME 14: 0: 0

TIME PERIOD 1 ELAPSED TIME IS ELAPSED TIME IS 1: 0: 0 ( 3600 SECONDS),

3600 SECONDS

---

|   |                         |                                |                              |                       |                                 |                         | 0.                      | · 2                      |
|---|-------------------------|--------------------------------|------------------------------|-----------------------|---------------------------------|-------------------------|-------------------------|--------------------------|
| QUE(  |                         |                                |                              |                       |                                 | 20                      | 0                       | 18                       |
| ECONDS /<br>DELAY<br>TIME                     |                         |                                |                              |                       |                                 | 26.3                    | 6.7                     | 24.6                     |
| TOTAL<br>TIME                                 |                         |                                |                              |                       |                                 | 50.6                    | 30.5                    | 48.9                     |
| / KM<br>DELAY<br>TIME                         |                         |                                |                              |                       |                                 | 1.10                    | 0.29                    | 1.03                     |
| MINUTES<br>TOTAL<br>TIME                      |                         |                                |                              |                       |                                 | 2.11                    | 1.30                    | 2.04                     |
| RATIO<br>MOVE/<br>TOTAL<br>                   |                         |                                |                              |                       |                                 | 0.48                    | 0.78                    | 0.50                     |
| JTES<br>TOTAL<br>TIME                         |                         |                                |                              |                       |                                 | 794.8                   | 794.6                   | 1314.5                   |
| ICLE MINU<br>DELAY<br>TIME                    |                         |                                |                              |                       |                                 | 413.4                   | 175.7                   | 661.7                    |
| VEHI<br>ALUES<br>MOVE<br>TIME                 |                         |                                |                              |                       |                                 | 381.5                   | 618.9                   | 652.8                    |
| AGE VI<br>LE<br>SPEED<br>SPEED<br>RIPS<br>MPH | 940<br>1607             | 437<br>4                       | 144<br>1374                  | 177                   | 142<br>1886                     | 1272<br>942             | 28.4<br>1563            | 1612<br>29.4             |
|   |                         |                                |                              |                       |                                 | 376.70                  | 942<br>611.16<br>1563 4 | - 1000<br>644.64<br>1612 |
|   | 101)<br>104)            | 202)<br>222)                   | 242)<br>302)                 | 301)                  | 311)<br>403)                    | 401)<br>100)            | 78<br>101)<br>0         | 100)<br>66               |
| VEHICLE<br>STOP ST<br>LINF<br>TIME (          | (8101,<br>940<br>(8104, | 437<br>(8202,<br>437<br>(8222, | ,<br>(8242,<br>144<br>(8302, | 1374<br>(8301,<br>177 | (8311,<br>142<br>(8403,<br>1886 | (8401,<br>1272<br>(101, | 19.6<br>(100,           | ( 104,<br>18.0           |

| 0.0    | 0.0            | •    | 18.7   |      | 0.0    |      | 26.7   |      | 0.0    |      | 23.8   |      | 30.8   |      | 0.1    |      | 0.1    |      | 0.3    |      | 30.8  |      | 0.2   |      | 11.1  |      | 0.1    |      | 7.5    |      | 0.3    |      | 23.0   |      | 2.8   |      | 0.4   |      |
|--------|----------------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|-------|------|-------|------|-------|------|--------|------|--------|------|--------|------|--------|------|-------|------|-------|------|
| 7.3    | 6.6            |      | 30.0   |      | 5.7    |      | 34.7   |      | 6.7    |      | 32.3   |      | 35.8   |      | 4.9    |      | 2.0    |      | 4.1    |      | 32.7  |      | 4.1   |      | 14.1  |      | 4.0    |      | 11.9   |      | 4.3    |      | 27.1   |      | 7.1   |      | 3.2   |      |
| 31.6   | 30.7           |      | 54.3   |      | 30.0   |      | 59.0   |      | 31.0   |      | 56.6   |      | 60.1   |      | 29.0   |      | 7.8    |      | 10.1   |      | 38.8  |      | 10.1  |      | 20.1  |      | 9.6    |      | 18.0   |      | 10.3   |      | 33.2   |      | 24.4  |      | 6.2   |      |
| 0.31   | 0.28           |      | 1.25   |      | 0.24   |      | 1.45   |      | 0.28   |      | 1.34   |      | 1.49   |      | 0.21   |      | 0.35   |      | 0.70   |      | 5.45  |      | 0.70  |      | 2.34  |      | 0.71   |      | 1.99   |      | 0.73   |      | 4.53   |      | 0.41  |      | 1.06  |      |
| 1.32   | 1.29           |      | 2.26   |      | 1.25   |      | 2.46   |      | 1.29   |      | 2.36   |      | 2.51   |      | 1.22   |      | 1.37   |      | 1.71   |      | 6.46  |      | 1.71  |      | 3.36  |      | 1.73   |      | 3.00   |      | 1.74   |      | 5.54   |      | 1.43  |      | 2.08  |      |
| 0.77   | 0.79           |      | 0.45   |      | 0.81   |      | 0.41   |      | 0.78   |      | 0.43   |      | 0.40   |      | 0.83   |      | 0.74   |      | 0.59   |      | 0.16  |      | 0.59  |      | 0.30  |      | 0.59   |      | 0.34   |      | 0.58   |      | 0.18   |      | 0.71  |      | 0.49  |      |
| 770.0  | 492.5          |      | 1250.3 |      | 698.4  |      | 1745.2 |      | 526.9  |      | 1199.0 |      | 438.0  |      | 108.0  |      | 13.8   |      | 7.9    |      | 2.6   |      | 3.0   |      | 48.3  |      | 18.8   |      | 53.1   |      | 38.1   |      | 78.1   |      | 38.2  |      | 14.9  |      |
| 178.5  | 105.5          |      | 691.1  |      | 133.1  |      | 1026.8 |      | 114.3  |      | 683.9  |      | 261.0  |      | 18.3   |      | 3.6    |      | 3.2    |      | 2.2   |      | 1.2   |      | 33.7  |      | 7.8    |      | 35.2   |      | 16.0   |      | 63.8   |      | 11.1  |      | 7.6   |      |
| 591.6  | 387.0          |      | 559.2  |      | 565.3  |      | 718.4  |      | 412.6  |      | 515.1  |      | 177.0  |      | 89.6   |      | 10.2   |      | 4.7    |      | 0.4   |      | 1.8   |      | 14.6  |      | 11.0   |      | 17.9   |      | 22.1   |      | 14.3   |      | 27.1  |      | 7.2   |      |
| 1463   | 45.5<br>964    | 46.6 | 1381   | 26.5 | 1396   | 48.0 | 1774   | 24.4 | 1019   | 46.4 | 1272   | 25.5 | 437    | 23.9 | 223    | 49.2 | 106    | 43.9 | 47     | 35.1 | 4     | 9.3  | 18    | 35.1 | 144   | 17.9 | 117    | 34.8 | 177    | 20.0 | 222    | 34.4 | 141    | 10.8 | 94    | 42.1 | 143   | 28.9 |
| 584.19 | 1463<br>382.18 | 964  | 552.26 | 1381 | 558.26 | 1396 | 709.42 | 1774 | 407.50 | 1019 | 508.67 | 1272 | 174.76 | 437  | 88.52  | 223  | 10.06  | 106  | 4.63   | 47   | 0.40  | 4    | 1.77  | 18   | 14.40 | 144  | 10.89  | 117  | 17.70  | 177  | 21.85  | 222  | 14.10  | 141  | 26.79 | 94   | 7.15  | 143  |
| 104)   | 0<br>302)      | 0    | 300)   | 79   | 403)   | 0    | 400)   | 71   | 401)   | 0    | 400)   | 62   | 200)   | 87   | 202)   | 0    | 201)   | 0    | 222)   | 0    | 220)  | 100  | 242)  | 0    | 240)  | 100  | 301)   | 0    | 300)   | 59   | 311)   | 0    | 310)   | 100  | 401)  | 21   | 402)  | 0    |
| ( 100, | 0.0<br>(300,   | 0.0  | ( 302, | 17.1 | (400,  | 0.0  | (403,  | 26.2 | (400,  | 0.0  | (401,  | 23.2 | ( 202, | 30.2 | ( 200, | 0.0  | ( 200, | 0.0  | ( 220, | 0.0  | (222, | 30.8 | (240, | 0.0  | (242, | 11.0 | ( 300, | 0.0  | ( 301, | 7.3  | ( 310, | 0.0  | ( 311, | 22.5 | (403, | 2.8  | (400, | 0.0  |

| ( 100,   | 200)  | 251.13  | 1795 | 254.3  | 279.4    | 533.7  | 0.48 | 2.13 | 1.11 | 17.8  | 9.3      | 4.5   |
|----------|-------|---------|------|--------|----------|--------|------|------|------|-------|----------|-------|
| 4.2      | 36    | 1795    | 28.2 |        |          |        |      |      |      |       |          |       |
| ( 200,   | 220)  | 201.90  | 1658 | 204.4  | 192.2    | 396.6  | 0.52 | 1.96 | 0.95 | 14.4  | 7.0      | 0.2   |
| 0.1      | 0     | 1658    | 30.5 |        |          |        |      |      |      |       |          |       |
| ( 220,   | 240)  | 148.29  | 1611 | 150.2  | 172.9    | 323.0  | 0.46 | 2.18 | 1.17 | 12.0  | 6.4      | 0.4   |
| 0.0      | 0     | 1611    | 27.5 |        |          |        |      |      |      |       |          |       |
| (240,    | 300)  | 557.80  | 1711 | 564.8  | 542.4    | 1107.2 | 0.51 | 1.98 | 0.97 | 38.8  | 19.0     | 11.9  |
| 11.3     | 49    | 1711    | 30.2 |        |          |        |      |      |      |       |          |       |
| ( 300,   | 400)  | 483.23  | 2345 | 489.3  | 1122.7   | 1612.0 | 0.30 | 3.34 | 2.32 | 41.2  | 28.7     | 20.9  |
| 20.2     | 51    | 2345    | 18.0 |        |          |        |      |      |      |       |          |       |
| (400,    | 300)  | 546.26  | 2619 | 553.1  | 1899.2   | 2452.4 | 0.23 | 4.49 | 3.48 | 56.2  | 43.5     | 30.0  |
| 28.1     | 74    | 2619    | 13.4 |        |          |        |      |      |      |       |          |       |
| ( 300,   | 310)  | 510.80  | 2244 | 517.2  | 396.4    | 913.7  | 0.57 | 1.79 | 0.78 | 24.4  | 10.6     | 1.    |
| 0.5      | 4     | 2244    | 33.5 |        |          |        |      |      |      |       |          |       |
| ( 310,   | 200)  | 676.69  | 2183 | 685.2  | 555.7    | 1240.9 | 0.55 | 1.83 | 0.82 | 34.1  | 15.3     | 8.4   |
| 7.8      | 41    | 2183    | 32.7 |        |          |        |      |      |      |       |          |       |
| ( 200,   | 100)  | 347.45  | 2365 | 351.8  | 541.4    | 893.2  | 0.39 | 2.57 | 1.56 | 22.7  | 13.7     | 6.1   |
| 5.6      | 43    | 2365    | 23.3 |        |          |        |      |      |      |       |          |       |
| OSUBNETV | VORK= | 9451.55 | 8005 | 159.51 | 172.52   | 332.03 | 0.48 | 2.11 | 1.10 | 2.49  | 1.29     | 0.74  |
| 0.70 15  | 56.1  |         | 28.5 |        |          |        |      |      |      |       |          |       |
|          |       |         |      | VEH    | ICLE - H | OURS   |      |      |      | TUNIM | ES / VEH | ICLE- |
| TRIP     | 1     | PER     |      |        |          |        |      |      |      |       |          |       |
|          |       |         |      |        |          |        |      |      |      |       |          |       |
| TRLF     |       |         |      |        |          |        |      |      |      |       |          |       |
|          |       |         |      |        |          |        |      |      |      |       |          |       |

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CUMULATIVE NETSIM STATISTICS AT TIME 14: 0: 0

TIME PERIOD 1 ELAPSED TIME IS ELAPSED TIME IS 1: 0: 0 ( 3600 SECONDS), 3600 SECONDS

|     |             | VEH-N   | * SNIM                 | AVERAGE   | CONGES  | NOIL    | 1<br> <br> <br> |         | <b>Ο U E U E</b> | LEN   | С<br>Т |
|-----|-------------|---------|------------------------|-----------|---------|---------|-----------------|---------|------------------|-------|--------|
| Н   | (VEHICLE)   | 1<br>1  |                        | NUMBER    |         |         |                 |         |                  |       |        |
|     |             | QUEUE   | STOP                   | OCCUPANCY | STORAGE | PHASE   |                 | AVERAGE | QUEUE BY LAN     | 1E ** |        |
| MAX | IMUM QUEUE  | BY LANE | OF                     | LANE      |         |         |                 |         |                  |       |        |
|     | LINK        | TIME    | TIME                   | (VEHICLE) | (8)     | FAILURE |                 | 3 3     | 4 5              | 9     | ٢      |
| Ч   | 2 3 4       | 5 6     | 7 C                    | HANGES    |         |         |                 |         |                  |       |        |
|     | t<br>1<br>1 |         | \$<br>1<br>1<br>1<br>1 |           |         |         | ı               | 1       | 1                | 1     | I      |

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| 0     | 0              | 0            | 0            |             | 0    | ٣   | 5            | 0    | C           | >                  | 0        | ¢   | >     | C      | >       | 0          |        | 0    | C      | >      | 0           |   | 0     | Ċ | >     | C | 2      | С           | )           | 0      |   |
|-------|----------------|--------------|--------------|-------------|------|-----|--------------|------|-------------|--------------------|----------|-----|-------|--------|---------|------------|--------|------|--------|--------|-------------|---|-------|---|-------|---|--------|-------------|-------------|--------|---|
| 0     | 0              | 0            | 0            |             | 0    | c   | >            | 0    | c           | >                  | 0        | c   | 5     | C      | >       | 0          |        | 0    | c      | 2      | 0           | , | 0     | c | 0     | c | 5      | С           | >           | 0      |   |
| 0     | 0              | 0            | 0            |             | 0    | c   | >            | 0    | c           | >                  | 0        | Ċ   | S     | c      | >       | 0          |        | 0    | c      | >      | 0           |   | 0     | ¢ | D     | c | >      | c           | >           | 0      |   |
| 0     | 0              | 0            | 0            |             | 0    | c   | >            | 0    | c           | þ                  | 0        | ų   | ٥     | c      | >       | 0          |        | 0    | c      | 5      | 0           |   | 0     | c | c     | c | Þ      | C           | <b>&gt;</b> | 0      |   |
| e     | 0              | ъ            | 0            |             | 0    | c   | >            | 0    | ۲           | -                  | 0        | ,   | -     | ç      | ٩       | 0          |        | 0    | c      | 5      | 0           |   | 0     | Ċ | D     | c | >      | C           | >           | 0      |   |
| e     | 0              | m            | 0            |             | 0    | ~   | r            | 0    | Ľ           | r                  | 0        | •   | 1     | ç      | 4       | 0          |        | 0    | ¢      | 5      | 0           |   | 0     | Ċ | 0     | Ċ | ∍      | c           | þ           | 0      |   |
| 0     | 0              | 7            | 0            |             | 0    | ç   | ۷            | 0    | ~           | ť                  | 0        | •   | 2     | c      | >       | 0          |        | 0    | c      | Þ      | 0           | - | 0     | ( | 0     | Ċ | D      | c           | >           | 0      |   |
| 1     | 0              | 18           | 0            |             | 0    | ~   | Ţ            | 0    | c           | 5                  | 0        |     | თ     | -      | 4       | 0          |        | 0    | c      | D      | 0           |   | 0     |   | 0     | ¢ | Ð      | C           | 5           | 0      |   |
| 7.6   | 11.4           | 12.3         | 7.4          | 9<br>9<br>9 | 4.9  |     | 0.01         | 6.8  | L<br>(      | C.01               | 5.1      |     | 8.5   | ,<br>, | 4 · J   | 1.8        |        | 1.3  | (      | 0.8    | 0.5         |   | 0.3   |   | 9.4   | ( |        | 2           | 0.0         | 6.3    |   |
| 13.6  | 892<br>13.6    | 436<br>22.1  | 1258<br>13.2 | 275         | 8.7  | 367 | 21.U<br>641  | 12.1 | 546<br>22 7 | 29.0<br>875        | 9.1      | 479 | 20.3  | 1522   | 426     | 2.1        | 76     | 0.4  | ς<br>ε | 0.3    | 0.1         | 0 | 0.1   | ς | 1.4   | 0 | 0.5    | ,<br>,<br>0 | 1.4<br>D    | 0.9    | 0 |
| 310.9 | 0.0            | 0<br>490.7   | 0            | 0           | 0.0  | 000 | 396.I<br>7   | 0.0  | 001         | د.88/<br>۱         | 0.0      | 0   | 502.6 | 000    | 223.2   | 0.0        | 0      | 0.0  | 0      | 0.0    | 2.0         | 0 | 0.0   | 0 | 26.3  | 0 | 0.0    | ,<br>0 6    | 0.12        | 0.0    | 0 |
| 318.3 | 0 0 0 1.0      | 0 0<br>502.9 | 0<br>0<br>0  | 0.0         | 0.4  | 000 | 433.U<br>0 0 | 1.0  | 0 0         | 803.9<br>0 0       | 0.4      | 0   | 514.6 | 0      | 227.1   | 0.2        | 0<br>0 | 0.2  | 0      | 0.2    | 0<br>2.0    | 0 | 0.1   | 0 | 26.7  | 0 | 0.1    | 0000        | 0.22        | 1.3    | 0 |
| (001  | 1 0<br>101)    | 0 0<br>100)  | 11 0         | 0 0         | 302) | 0 0 | 300)<br>0 0  | 403) | 0 0         | 400)<br>21 N       | 401)     | 0   | 400)  | 4 23   | 200)    | 202)       | 0      | 201) | 0      | 222)   | 0 0<br>220) | 0 | 242)  | 0 | 240)  | 0 | 301)   | 0           | 300)        | 311)   | 0 |
| 101,  | 10 1           | 104,         | 100          | ,<br>001    | 300, | 0   | 302,<br>13   | 400, | 0           | 403 <b>,</b><br>18 | 400,     | 0   | 401,  | 5      | 202,    | 200.       | 0      | 200, | 0      | ( 220, | 0           | 0 | (240, | 0 | (242, | 0 | ( 300, | 0           | ( 301,      | ( 310. | 0 |
| -     | ΄ <sub>Μ</sub> | 0            | 10,          | <b>^</b> 0  | -    | 0   | 18 (         | -    | 0           | ים ~<br>ר          | , )<br>+ | 0   | -     | с<br>Г | ~<br>`` | <u>ر</u> د | 0      | _    | 0      |        | ວີ          |   | -     | 0 | -     | m | -      | 0           | ſ           | ۰ آ    | 0 |

| 0      | Ċ | 0     |   | 0     |   | 0      |      | 0      |     | 0      |    |       |                  | 8      |      | <u>б</u> |        | 0      |     | 0      |      | ~~1    |     |         |      |
|--------|---|-------|---|-------|---|--------|------|--------|-----|--------|----|-------|------------------|--------|------|----------|--------|--------|-----|--------|------|--------|-----|---------|------|
| 0      | ¢ | 0     |   | 0     |   | 0      |      | 0      |     | 0      |    | 0     |                  | 0      |      | 0        |        | 0      |     | 0      |      | 0      |     |         |      |
| 0      | c | 0     |   | 0     |   | 0      |      | 0      |     | 0      |    | 0     |                  | 0      |      | 0        |        | 0      |     | 0      |      | 0      |     |         |      |
| 0      | ( | 0     |   | 0     |   | 0      |      | 0      |     | 0      |    | 0     |                  | 0      |      | 0        |        | 0      |     | 0      |      | 0      |     |         |      |
| 0      | ¢ | 0     |   | 0     |   | -1     |      | 0      |     | 0      |    | 2     |                  | 4      |      | ٢        |        | 0      |     | Ч      |      | -      |     |         |      |
| 0      | ¢ | 0     |   | 0     |   | ч      |      | 0      |     | 0      |    | 2     |                  | 0      |      | ო        |        | 0      |     |        |      | -1     |     |         |      |
|        | ¢ | 0     |   | 0     |   | 0      |      | 0      |     | 0      |    | 2     |                  | Ч      |      | m        |        | 0      |     | 7      |      | Ч      |     |         |      |
|        |   |       |   |       |   |        |      |        |     |        |    |       |                  |        |      |          |        |        |     |        |      |        |     |         |      |
| 0      | ¢ | 0     |   | 0     |   | 0      |      | 0      |     | 0      |    | 2     |                  | 0      |      | 14       |        | 0      |     | 4      |      | 0      |     | 53      |      |
| 2.3    |   | 2.9   |   | 4.2   |   | 3.9    |      | 2.6    |     | 3.9    |    | 2.1   |                  | 4.9    |      | 7.8      |        | 5.3    |     | 4.7    |      | :1.6   |     | 1.0     |      |
|        |   |       |   |       |   | 1      |      | -1     |     | Ч      |    | 1     |                  | 2      |      | m        |        | Г      |     | Г      |      | ~      |     | -       |      |
| 1.8    | 0 | 1.2   | 0 | 0.3   | 0 | 9.3    | 462  | 6.9    | 250 | 5.7    | 79 | 19.3  | 419              | 27.3   | 1931 | 41.2     | 1771   | 15.6   | 889 | 21.2   | 759  | 15.3   | 066 | 343.3   |      |
| 53.2   | 0 | 4.5   | 0 | 0.0   | 0 | 125.1  | ო    | 2.3    | 0   | 0.0    | 0  | 328.7 | 9                | 7.067  | 17   | 1238.6   | 17     | 20.7   | 0   | 285.6  | ٢    | 220.8  | 6 1 | 5832.1  |      |
| 54.5   | 0 | 4.5   | 0 | 0.9   | 0 | 135.8  | 0    | 5.9    | 0   | 11.2   | 0  | 344.4 | 0 4              | 817.0  | 0    | 323.6    | 0      | 58.3   | 0   | 306.7  | 0    | 243.1  | 0   | 5162.2  |      |
| 310)   | 0 | 401)  | 0 | 402)  | 0 | 200)   | 0 01 | 220)   | 0   | 240)   | 0  | 300)  | 14 0             | 400)   | 21 0 | 300) 1   | 34 0   | 310)   | 0   | 200)   | 7 0  | 100)   | 06  | VORK= 6 |      |
| ( 311, | 0 | (403, | 0 | (400, | 0 | ( 100, | 8    | ( 200, | 0   | ( 220, | 0  | (240, | 6 14             | ( 300, | 5 11 | (400,    | 1 26   | ( 300, | Ч   | ( 310, | 1 13 | ( 200, | 2   | SUBNET  | 5425 |
|        | 4 |       | 2 |       | 0 |        | 9    |        | 0   |        | 0  |       | <del>, - 1</del> |        |      |          | $\sim$ |        | ഹ   |        | Ч    |        | ω   | 0       | Ч    |

\* THESE VALUES INCLUDE THE TIME FOR VEHICLES CURRENTLY ON THE LINK. \*\* AVERAGE QUEUE CALCULATED BASED ON TIME SINCE BEGINNING OF SIMULATION

# CUMULATIVE NETSIM STATISTICS AT TIME 14: 0: 0

TIME PERIOD 1 ELAPSED TIME IS 1: 0: 0 (3600 SECONDS), ELAPSED TIME IS 3600 SECONDS

DISCHARGE BY LANE

|                  |               |                   |          | 1         |     |             |     |           |             |           |           |
|------------------|---------------|-------------------|----------|-----------|-----|-------------|-----|-----------|-------------|-----------|-----------|
| I.ANF. 6         | LANE          | ANE<br>7          | 1        | LANE      | 7   | LANE        | £   | LANE      | 4           | LANE      | ß         |
| LINK<br>VEH VPH  | VEH           | H<br>UPH          | VРН<br>I | VEH       | ИРН | VEH         | VPH | VEH       | Чрн         | VEH       | ЧРН       |
|                  |               | ł                 | ¦ .      | <br> <br> | 1   | 1<br>1<br>1 | 1   | <br> <br> | 1<br>1<br>1 | <br> <br> | <br> <br> |
| ( 101, 100)<br>, | 11            | ň                 | 113      | 390       | 390 | 439         | 439 | 0         | 0           | 0         | 0         |
| ( 100, 101)      | 0 87          | 5,0               | 872      | 691       | 691 | 0           | 0   | 0         | 0           | 0         | Q         |
| ( 104, 100)      | 0<br>86       | ے<br>م            | 863      | 388       | 388 | 361         | 361 | 0         | 0           | 0         | 0         |
| ( 100, 104)      | 0<br>46       |                   | 468      | 514       | 514 | 481         | 481 | 0         | 0           | 0         | 0         |
| ( 300, 302)      | 0<br>31<br>0  | ာရှိ              | 319      | 323       | 323 | 322         | 322 | 0         | 0           | 0         | 0         |
| u u<br>(302,300) |               | 22                | 102      | 212       | 212 | 0           | 0   | 0         | 0           | 0         | 0         |
| 0 0<br>(400,403) | 106/ 10<br>48 | )<br>9 ()<br>9 () | 483      | 497       | 497 | 416         | 416 | 0         | 0           | 0         | 0         |
| 0 0<br>(403,400) | 0<br>54       | ວຼິ               | 543      | 592       | 592 | 639         | 639 | 0         | 0           | 0         | 0         |
| 0 0<br>(400,401) | 0<br>26       | ي<br>وي ر         | 265      | 345       | 345 | 409         | 409 | 0         | 0           | 0         | 0         |
| 0 0<br>(401,400) | 0<br>82       | ີວູ               | 820      | 72        | 72  | 70          | 70  | 310       | 310         | 0         | 0         |
| 0 0<br>(202,200) | т<br>с с      | کي د              | 32       | 202       | 202 | 203         | 203 | 0         | 0           | 0         | 0         |
| 0 0<br>(200,202) | 0 10          | ں<br>ھ د          | 108      | 115       | 115 | 0           | 0   | 0         | 0           | 0         | U         |
| ><br>>           | 2             | >                 |          |           |     |             |     |           |             |           |           |

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| 0          | 0                | 0           | 0          | 0          | 0           | 0           | 0         | 0          | 0         | 0           | 0            | 0           | 0            | 0                 | 0                    | 0                | 0                | 0           | 0  |
|------------|------------------|-------------|------------|------------|-------------|-------------|-----------|------------|-----------|-------------|--------------|-------------|--------------|-------------------|----------------------|------------------|------------------|-------------|--|
| 0          | 0                | 0           | 0          | 0          | 0           | 0           | 0         | 0          | 0         | 0           | 0            | 0           | 0            | 0                 | 0                    | 0                | 0                | 0           | 0  |
| 0          | 0                | 0           | 0          | 0          | 0           | 0           | 0         | 0          | 0         | 0           | 0            | 0           | 0            | 0                 | 0                    | 0                | 0                | 0           | 0  |
| 0          | 0                | 0           | 0          | 0          | 0           | 0           | 0         | 0          | 0         | 0           | 0            | 0           | 0            | 0                 | 0                    | 0                | 0                | 0           | 0  |
| 0          | 0                | 0           | 0          | 0          | 0           | 0           | 0         | 0          | 0         | 0           | 391          | 459         | 471          | 452               | 580                  | 546              | 630              | 419         | 559  |
| 0          | 0                | 0           | 0          | 0          | 0           | 0           | 0         | 0          | 0         | 0           | 391          | 459         | 471          | 452               | 580                  | 546              | 630              | 419         | 559  |
| 64         | 0                | 0           | ε          | 0          | 0           | 0           | 0         | 0          | 0         | 0           | 550          | 523         | 549          | 490               | 296                  | 564              | 683              | 819         | 457  |
| 64         | 0                | 0           | £          | 0          | 0           | 0           | 0         | 0          | 0         | 0           | 550          | 523         | 549          | 490               | 296                  | 564              | 683              | 819         | 457  |
| 42         | 47               | 4           | 15         | 144        | 117         | 177         | 222       | 141        | 94        | 143         | 719          | 676         | 591          | 527               | т<br>641             | 1036             | 931              | 786         | 337  |
| 42         | 0 0 0 47 0       | 0<br>4<br>0 | 0 12 0     | 0 0<br>144 | 0 0 0       | 0 0<br>177  | 222       |            | 0 64 0    | 0 0<br>143  | 0 0 0<br>719 | 676<br>676  | 0 0 0<br>591 | 0 0<br>527        | 41 4<br>641          | 7 617<br>1036    | 9 469<br>931     | 786<br>186  | $\begin{array}{cccc} 1 & 181 \\ 337 \\ 2 & 1012 \end{array}$ |
|            |                  |             |            |            |             |             |           |            |           |             | Ċ            | 0           |              |                   |                      | 61               | 46               |             | 101<br>101   |
| (200, 201) | 0 0<br>(220,222) | ( 222, 220) | (240, 242) | (242, 240) | ( 300, 301) | ( 301, 300) | (310,311) | (311, 310) | (403,401) | ( 400, 402) | ( 100, 200)  | ( 200, 220) | (220,240)    | 0 0<br>(240, 300) | 198 198<br>(300,400) | 0 0<br>(400,300) | 0 0<br>(300,310) | ( 310, 200) | 0 0<br>(200,100)<br>0 0                                      |

| EFFECTIVENESS |
|---------------|
| OF            |
| MEASURES      |
| PERSON        |
| NETSIM        |

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| амты талкам               | LIN    | K    | PERSON | PERSON | DELAY      |
|---------------------------|--------|------|--------|--------|------------|
| FRAVEL LIME<br>PERSON-MIN |        |      | KM     | TRIPS  | PERSON-MIN |
|                           | ( 101, | 100) | 489.0  | 1222.8 | 536.6      |
| 1031.8                    | ( 100, | 101) | 793.6  | 2029.5 | 228.2      |
| 1031.7                    | (104,  | 100) | 836.3  | 2091.4 | 858.5      |
| 1/00.4                    | ( 100, | 104) | 758.7  | 1899.9 | 231.8      |
|                           | ( 300, | 302) | 496.0  | 1251.0 | 136.9      |
| 039.I                     | ( 302, | 300) | 717.6  | 1794.5 | 0.898      |
| 1 6 2 4 . /               | (400,  | 403) | 724.6  | 1812.0 | 172.8      |
| 906.5                     | (403,  | 400) | 920.8  | 2302.7 | 1332.8     |
| C.C022                    | (400,  | 401) | 529.2  | 1323.4 | 148.4      |
|                           | (401,  | 400) | 660.4  | 1651.3 | 887.9      |
| 0.0CL                     | ( 202, | 200) | 227.2  | 568.1  | 339.4      |
|                           | ( 200, | 202) | 115.0  | 289.6  | 23.8       |
| 140.2                     | ( 200, | 201) | 13.1   | 137.6  | 4.6        |
| 0./I                      | ( 220, | 222) | 6.0    | 61.0   | 4.2        |
| 3.4                       | (222,  | 220) | 0.5    | 5.2    | 2.8        |

| ημη το πιστηκου τους συμα στης ΟΠΙΦΕΙΑΝΟ ΜΕΙΟΝΟ | THIS IN INTERNATION OF THE STAR STAR STARTED AND THE START STARTED AND THE START STARTED AND ST |            |
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| c<br>-  | ג<br>ר  |            |
|   | FERIOD  |            |
|   | TME.  | г.         |
| -   | NOTE ***  | IME PERIOD |
| -   | *   | F          |
|   | *   | END O      |

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|     | *** NOTE *** | TIME  | PERIOD | 1 SPECIFIC | C NETSIM | STATISTICS | ARE | THE S | AME A | S CUMUL | ATIVE | OUTPUT | AT | E |
|-----|--------------|-------|--------|------------|----------|------------|-----|-------|-------|---------|-------|--------|----|---|
| END | OF TIME PERI | OD 1. |        |            |          |            |     |       |       |         |       |        |    |   |

|        | (240,  | 242) | 2.3   | 23.2   | 1.6    |
|--------|--------|------|-------|--------|--------|
| 3.9    | (242,  | 240) | 18.7  | 187.2  | 43.8   |
| 62.8   | ( 300, | 301) | 14.2  | 152.0  | 10.1   |
| 24.4   | ( 301, | 300) | 23.0  | 230.1  | 45.7   |
| 69.0   | ( 310, | 311) | 28.4  | 288.2  | 20.7   |
| 49.5   | ( 311, | 310) | 18.3  | 183.3  | 82.9   |
| c.101  | (403,  | 401) | 34.7  | 121.8  | 14.4   |
| 49.5   | (400,  | 402) | 9.3   | 185.8  | 9.9    |
| 19.3   | (100,  | 200) | 325.9 | 2329.5 | 362.6  |
| 692.6  | (200,  | 220) | 262.0 | 2151.8 | 249.4  |
| 514.8  | ( 220, | 240) | 192.5 | 2090.8 | 224.4  |
| 419.2  | (240,  | 300) | 724.1 | 2221.0 | 704.1  |
| 1437.2 | ( 300, | 400) | 627.5 | 3045.0 | 1457.8 |
| 2093.2 | (400,  | 300) | 709.0 | 3399.3 | 2465.1 |
| 3183.0 | ( 300, | 310) | 663.3 | 2913.8 | 514.8  |
| 1180.4 | ( 310, | 200) | 878.8 | 2835.0 | 721.7  |
| 1611.6 | ( 200, | 100) | 451.3 | 3071.9 | 703.2  |

NETSIM MOVEMENT SPECIFIC STATISTICS - TABLE I

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| 0     | LINK        | Λ             | EHICLE-KM |        | VEF  | HICLE-TR] | IPS   | SPE          | ЕD (КМРН | ~     |
|-------|-------------|---------------|-----------|--------|------|-----------|-------|--------------|----------|-------|
| STOPS | (PCT)       |               |           |        |      |           |       |              |          |       |
| LEFT  | THRU        | LEFT<br>RIGHT | THRU      | RIGHT  | LEFT | THRU      | RIGHT | LEFT         | THRU     | RIGHT |
|       | 9<br>       | 1             |           |        |      |           |       |              |          |       |
|       | (8101, 101) |               |           |        | 0    | 940       | 0     |              |          |       |
|       | (8104, 104) |               |           |        | 0    | 1607      | 0     |              |          |       |
|       | (8202, 202) |               |           |        | 0    | 437       | 0     |              |          |       |
|       | (8222, 222) |               |           |        | 0    | 4         | 0     |              |          |       |
|       | (8242, 242) |               |           |        | 0    | 144       | 0     |              |          |       |
|       | (8302, 302) |               |           |        | 0    | 1374      | 0     |              |          |       |
|       | (8301, 301) |               |           |        | 0    | 177       | 0     |              |          |       |
|       | (8311, 311) |               |           |        | 0    | 142       | 0     |              |          |       |
|       | (8403, 403) |               |           |        | 0    | 1886      | 0     |              |          |       |
|       | (8401, 401) |               |           |        | 0    | 1272      | 0     |              |          |       |
|       | (101, 100)  | 331.52        | 0.00      | 45.19  | 829  | 0         | 113   | 27.1         | 0.0      | 43.8  |
| 77.9  | 0.0         | 78.8          |           |        |      |           |       |              |          |       |
|       | (100, 101)  | 0.00          | 611.16    | 0.00   | 0    | 1563      | 0     | 0.0          | 46.1     | 0.0   |
| 0.0   | 0.0         | 0.0           |           |        |      |           |       |              |          |       |
|       | (104, 100)  | ) 218.74      | 425.89    | 0.00   | 547  | 1065      | 0     | 20.3         | 38.3     | 0.0   |
| 97.1  | 51.5        | 0.0           |           |        |      |           |       |              | 1        |       |
| 0     | (100, 104)  | 0.00          | 584.19    | 0.00   | 0    | 1463      | 0     | 0.0          | 45.5     | 0.0   |
| 0.0   | 0.0         | 0.0           |           |        | c    |           | c     | с<br>с       | U U      |       |
| 0     | ( 300, 302) |               | 382.18    | 00     | 5    | 904       | Þ     | 0.0          | 40.0     | 0.0   |
| •     | ( 302, 300) | 113.97        | 11.60     | 426.69 | 285  | 29        | 1067  | 17.0         | 18.3     | 31.6  |
| 88.4  | 82.8        | 76.8          |           |        |      |           |       |              |          |       |
|       | (400,403)   | 0.00 (        | 558.26    | 0.00   | 0    | 1396      | 0     | 0.0          | 48.0     | 0.0   |
| 0.0   | 0.0         | 0.0           |           |        |      |           |       |              |          |       |
|       | (403,400)   | 00.00         | 709.42    | 0.00   | 0    | 1774      | 0     | 0.0          | 24.4     | 0.0   |
| 0.0   | 71.2        | 0.0           |           |        |      |           |       |              |          |       |
|       | (400, 401)  | ) 0.00        | 407.50    | 0.00   | 0    | 1019      | 0     | 0.0          | 46.4     | 0.0   |
| 0.0   | 0.0         | 0.0           |           |        |      |           |       | (<br>1.<br>* |          |       |
|       | (401,400    | ) 123.57      | 57.19     | 327.92 | 309  | 143       | 820   | 15.8         | 21.5     | 34.5  |
| 88.0  | 76.2        | 51.0          |           |        |      |           |       |              |          |       |

|        | ( 202, 2        | (00)       | 149.96    | 12.00       | 12.80      | 375         | 30          | 32  | 23.3        | 22.9        | 36.6        |
|--------|-----------------|------------|-----------|-------------|------------|-------------|-------------|-----|-------------|-------------|-------------|
| 88.3   | 90.0<br>200, 20 | 02)<br>12) | ء<br>0.00 | 88.52       | 0.00       | 0           | 223         | 0   | 0.0         | 49.2        | 0.0         |
| 0.0    | 0.0             | 0.0        |           | •           |            |             |             | •   | ,<br>,      |             | )<br>•<br>• |
| ¢      | ( 200, 2        | 01)        | 0.00      | 10.06       | 0.00       | 0           | 106         | 0   | 0.0         | 43.9        | 0.0         |
| 0.0    | 0.0<br>(220, 2; | 22)<br>22) | 0.00      | 4.63        | 0.00       | 0           | 47          | 0   | 0.0         | 35.1        | 0.0         |
| 0.0    | 0.0             | 0.0        |           |             |            |             |             |     |             | <br>•<br>•  | •           |
|        | ( 222, 2        | 20)        | 0.00      | 0.00        | 0.40       | 0           | 0           | 4   | 0.0         | 0.0         | 9.3         |
| 0.0    | 0.0             | 100.0      |           |             |            |             |             |     |             |             |             |
| c      | (240, 2         | 42)        | 0.00      | 1.77        | 0.00       | 0           | 18          | 0   | 0.0         | 35.1        | 0.0         |
| 0.0    | (242, 2         | 40)        | 0.00      | 0.00        | 14.40      | 0           | 0           | 144 | 0.0         | 0.0         | 17.9        |
| 0.0    | 0.0             | 100.0      |           |             |            |             |             |     |             |             |             |
| c      | ( 300, 3        | 01)        | 0.00      | 10.89       | 0.00       | 0           | 117         | 0   | 0.0         | 34.8        | 0.0         |
| 0.0    | 0.0<br>(301, 3  | 00) 0.0    | 00.00     | 0.00        | 17.70      | 0           | 0           | 177 | 0.0         | 0.0         | 20.0        |
| 0.0    | 0.0             | 59.9       | •         | )<br>)<br>) |            |             |             |     | 9<br>9<br>1 | •           | 1<br>1<br>1 |
|        | ( 310, 3        | 11)        | 0.00      | 21.85       | 0.00       | 0           | 222         | 0   | 0.0         | 34.4        | 0.0         |
| 0.0    | 0.0             | 0.0        |           | •           |            |             |             |     |             | •           |             |
| Ċ      | (311,3          | 10)        | 0.00      | 0.00        | 14.10      | 0           | 0           | 141 | 0.0         | 0.0         | 10.8        |
| 0.0    | ( 403, 4        | 01)        | 0.00      | 26.79       | 0.00       | 0           | 94          | 0   | 0.0         | 42.1        | 0.0         |
| 0.0    | 21.3            | 0.0        |           |             |            |             |             |     |             |             |             |
|        | (400,4          | 02)        | 0.00      | 7.15        | 0.00       | 0           | 143         | 0   | 0.0         | 28.9        | 0.0         |
| 0.0    | 0.0             | 0.0        |           |             | 1          |             |             |     |             |             |             |
|        | (100, 2         | (00)       | 5.88      | 238.54      | 6.72       | 42          | 1705        | 48  | 9.5         | 29.7        | 28.7        |
| 78.6   | 35.1            | 41.        | 7         |             | (<br>[     | c           | ,<br>,<br>, | ŗ   | 0           |             |             |
| c      | ( 200, 2<br>0 8 | 20)<br>0 0 | 0.00      | 196.18      | 21.6       | Ð           | 1191        | 4 / | 0.0         | 30.1        | 20.9        |
|        | ( 220, 2        | 40)        | 0.00      | 146.63      | 1.66       | 0           | 1593        | 18  | 0.0         | 27.5        | 28.3        |
| 0.0    | 0.0             | 0.0        |           |             |            |             |             |     |             |             |             |
|        | (240, 3         | (00)       | 13.37     | 479.89      | 64.55      | 41          | 1472        | 198 | 14.8        | 30.3        | 37.8        |
| 85.4   | 51.7            | 29.        | 8         |             |            |             |             |     |             |             |             |
|        | ( 300, 4        | (00        | 238.42    | 244.81      | 0.00       | 1157        | 1188        | 0   | 14.3        | 24.1        | 0.0         |
| 71.2   | 36.0            |            | 0         |             |            | C<br>T<br>T |             |     | 0           | 7<br>[<br>7 |             |
|        | (400,3          | 00)<br>707 | 101.UZ    | 67.616      | 10.01      | 711         | 7 / JA      | 4 Q | α.α         | T · / T     | 18.D        |
| 0.0°.4 | 01.0            | 10)        | 0.00      | 460.04      | 50.76      | С           | 2021        | 223 | 0.0         | 34.1        | 29.4        |
| 0.0    | 4.0             | 12.1       | )<br>     |             | )<br> <br> | )           | <br> <br>   | 1   | 1           |             | 1           |

|                   | (310, 200)   | 56.11                  | 608.50    | 12.09  | 181       | 1963      | 39         | 16.9      | 35.8      | 33.2   |
|-------------------|--|------------------------|-----------|--------|-----------|-----------|------------|-----------|-----------|--------|
| 0.0               | 3/.1<br>(200,100)<br>39.1  | 41.0<br>49.7           | 198.77    | 148.68 | 0         | 1353      | 1012       | 0.0       | 22.6      | 24.4   |
| 1                 |  |                        |           |        | NETSIM MO | VEMENT SP | ECIFIC STA | TISTICS - | TABLE II  |        |
|                   |  |                        | MOVING TI | ME     |           | DELAY TIM | ГIJ        | ·         | TOTAL TIM | (J     |
| KATIC             | MOVE/TUTAL   |                        | (VEH-MINS | ~      |           | (VEH-MINS | (          |           | (VEH-MINS |        |
| ( VЕН-<br>т б б т | LIGHT<br>(SNTW   | LEFT<br>DTCHT          | THRU      | RIGHT  | LEFT      | THRU      | RIGHT      | LEFT      | THRU      | RIGHT  |
|                   | (8101, 101)<br>(8104, 104)<br>(8202, 202)<br>(8222, 222)<br>(8302, 242)<br>(8302, 302) |                        |           |        |           |           |            |           |           |        |
|                   | (101, 101)<br>(111, 111, 111)<br>(111, 111, 111, 111, 111, 111, 111, 111               | 335.69                 | 0.00      | 45.76  | 397.17    | 0.00      | 16.21      | 732.87    | 0.00      | 61.97  |
| 0.46              | 0.00 ( 100, 101)   | 0.74 0.00              | 632.92    | 0.00   | 0.00      | 161.66    | 0.00       | 0.00      | 794.58    | 0.00   |
| 0.00              | 0.80<br>(104,100)  | 0.00<br>221.50         | 431.26    | 0.00   | 425.38    | 236.34    | 0.00       | 646.88    | 667.60    | 0.00   |
| 0.34              | 0.65<br>(100,104)  | 0.00                   | 592.42    | 0.00   | 0.00      | 177.61    | 0.00       | 0.00      | 770.03    | 0.00   |
|                   | ( 300, 302)  | 0.00                   | 390.36    | 0.00   | 0.00      | 102.14    | 0.00       | 0.00      | 492.50    | 0.00   |
|                   | ( 302, 300)  | 0.00<br>115.41<br>0.53 | 11.74     | 432.07 | 285.68    | 26.27     | 379.15     | 401.08    | 38.02     | 811.22 |
| 0.00              | (400,403)<br>0.81  | 0.00                   | 565.29    | 0.00   | 0.00      | 133.11    | 0.00       | 0.00      | 698.40    | 0.00   |

|            |              |        |             |                  |             |             |                    | 0.64            | 0.51                | 0.25 |
|------------|--------------|--------|-------------|------------------|-------------|-------------|--------------------|-----------------|---------------------|------|
| 102.55     | 950.58       | 54.08  | 37.16       | 464.46           | 40.54       | 65.39       | 486.12             | 13.54           | (240, 300)          |      |
| 30.0       | 31.7.0       | >      | r<br>       | ~~ + + +         | >           | ><br>•<br>• | >r<br>• >r<br>• >r | 0.48            | 0.46                | 0.00 |
| (<br> <br> |              |        | 40 F        | C                |             | 1 60        | 07 07 1            | 0.45            | 0.52                | 0.00 |
| 12.78      | 383.87       | 0.00   | 6.98        | 184.98           | 0.00        | 5.80        | 198.89             | 0.00            | (200, 220)          |      |
| 14.U3      | 482.02       | 00.10  | 62.1        | 10.142           | 01.10       | 00.0        | 24T.J4             | 0.48            | 0.50<br>0.50        | 0.16 |
|            |              |        | c<br>r      |                  | 0 F<br>F C  |             |                    | 0.00<br>E 0E    | 0.49                | 0.00 |
| 0.00       | 14.85        | 0.00   | 0.00        | 7.61             | 0.00        | 00.00       | 7.24               | 0.00            | (400,402)           |      |
| >><br>>    | 20.00        | >      | ><br>•<br>• | \                | >           | ><br>•<br>• | )<br>-<br>-        | 0.00            | 0.71                | 0.00 |
|            | <i>τι</i> αε |        |             | 11 00            |             |             | 27 13              | 0.18<br>D DD    | U.UU<br>1 403 401)  | 0.00 |
| 78.07      | 0.00         | 0.00   | 63.79       | 0.00             | 0.00        | 14.27       | 0.00               | 0.00            | (311, 310)          |      |
| 0.00       | 38.10        | 0.00   | 0.00        | 50.CI            | 0.00        | 00          | 1 1                | 0.00            | ( 210, 211)<br>0.59 | 0.00 |
|            |              |        |             |                  |             |             |                    | 0.34            | 0.00                | 0.00 |
| 53.08      | 0.00         | 0.00   | 35.16       | 0.00             | 0.00        | 17.92       | 0.00               | 0.00            | ( 301, 300)         | )    |
| 0.00       | 18.80        | 0.00   | 0.00        | 6.96             | 0.00        | 0.00        | 11.84              | 0.00            | ( 300, 301)         |      |
| 00.05      |              |        |             | •••              | •           |             | •                  | 0.30            | 0.00                | 0.00 |
|            |              |        |             |                  |             |             |                    | 0.00            | 0.60                | 0.00 |
| 0.00       | 3.03         | 0.00   | 0.00        | 1.21             | 0.00        | 0.00        | 1.82               | 0.00            | (240, 242)          |      |
| 86.2       | 00           | 0.00   | 01.2        | 00.0             |             | 0.40        |                    | 0.16            | 0.00                | 0.00 |
|            |              |        |             |                  |             |             |                    | 0.00            | 0.60                | 0.00 |
| 0.00       | 7.92         | 0.00   | 0.00        | 3.16             | 0.00        | 00.00       | 4.76               | 0.00            | (220, 222)          | •    |
| 0.00       | 13.75        | 0.00   | 0.00        | 3.02             | 0.00        | 0.00        | 10.73              | 00.00           | (200,201)<br>078    | 00 0 |
|            |              |        |             |                  |             |             |                    | 0.00            | 0.84                | 0.00 |
| 0.00       | 107.97       | 00.00  | 0.00        | 17.67            | 0.00        | 0.00        | 90.30              | 0.00            | ( 200, 202)         |      |
| cv.uz      | 06.16        |        | 66.1        | CC • C T         | 01.002      | 06.24       | 01.21              | 1.01.02<br>0.62 | 0.39                | 0.39 |
|            | 0<br>1<br>7  |        |             | 1 C C F          | 05 666      | 20 61       | 1 C L              | 0.58<br>151 85  | 0.36                | 0.27 |
| 569.75     | 159.72       | 469.55 | 237.70      | 101.81           | 344.42      | 332.05      | 57.91              | 125.13          | (401,400)           |      |
|            |              | •••    | •           | ><br>•<br>•<br>• | )<br>•<br>• | •           |                    | 0.00            | 0.78                | 0.00 |
| 00.00      | 526.93       | 0.00   | 00.00       | 114.30           | 00.0        | 0.00        | 412.63             | 0.00            | ( 400, 401)         | •    |
| 0.00       | 1745.15      | 0.00   | 0.00        | 1026.79          | 0.00        | 0.00        | /T8.30             | 0.00            | (403,400)<br>0.41   | 0.00 |
|            | 1745 15      |        |             | 1026 79          | 00 0        | 00 0        | 718 36             | 00 0            | 1 403 4001          |      |

| 0.00    | 2.30             | 3.63         | 1.83      | 5.37      |            |                  |           | тсита      |               |        |        |        |        |        |        |        |                 | 8.6   | •     | 0.0    |     | 0.0    |       | 0.0    | 0      | 0.0            |       |
|---------|------------------|--------------|-----------|-----------|------------|------------------|-----------|------------|---------------|--------|--------|--------|--------|--------|--------|--------|-----------------|-------|-------|--------|-----|--------|-------|--------|--------|----------------|-------|
| 47      | 43 3.            | 03 10        | 23 2      | 82 36     | E III      | TIME**           | (SNIM     | TIDUT      | 0\111 T       |        |        |        |        |        |        |        |                 | 0.0   |       | 1.0    |     | 41.1   |       | 0.8    |        | 0.4            |       |
| 3 609.  | ; 1317.          | ) 810.       | 5 1020.   | ) 527.    | - TABL     | QUEUE            | (VEH-     | ц<br>ц     | •             |        |        |        |        |        |        |        |                 | 3.6   |       | 0.0    |     | l.8 1  |       | 0.0    | (      | 0.0            |       |
| 1002.53 | 1102.65          | 0.00         | 198.85    | 0.0       | ATISTICS   |                  |           | Т.Т<br>Т.Т | ;             |        |        |        |        |        |        |        |                 | 305   |       | U      |     | 361    |       | 0      | ·      |                |       |
| 0.00    | 22.09            | 52.15        | 9.59      | 214.82    | SCIFIC ST  |                  |           | ртснт      | ***>          |        |        |        |        |        |        |        |                 | 8.6   |       | 0.0    |     | 0.0    |       | 0.0    | (<br>( | 0.0            |       |
| 355.73  | 934.87           | 343.46       | 404.07    | 326.54    | EMENT SPI  | LAY TIME         | ECS/VEH)  | пянт       | •             |        |        |        |        |        |        |        |                 | 0.0   |       | 6.2    |     | 13.3   |       | 7.3    | ļ      | 6.4            |       |
| 755.42  | 938.48           | 0.00         | 142.04    | 0.00      | NETSIM MOV | DE               | (S        | 1. F. F. T | +<br>1<br>1   |        |        |        |        |        |        |        |                 | 28.7  |       | 0.0    |     | 46.7   |       | 0.0    | 0      | 0.0            |       |
| 0.00    | 10.21            | 51.48        | 12.24     | 150.55    |            | ы                | ~         | втснт      | • • • • • • • |        |        |        |        |        |        |        |                 | 32.9  |       | 0.0    |     | 0.0    |       | 0.0    | (<br>( | 0.0            |       |
| 253.73  | 382.57           | 466.58       | 616.16    | 201.28    |            | TOTAL TIM        | (SECS/VEH | тнъп       | 2             |        |        |        |        |        |        |        |                 | 0.0   |       | 30.5   |     | 37.6   |       | 31.6   | г<br>с | 30.1           |       |
| 247.11  | 1.00<br>164.17   | 0.50<br>0.50 | 56.81     | 0.00      |            | -                |           | 1. F. F. F | IGHT          |        |        |        |        |        |        |        |                 | 53.0  | 8.3   | 0.0    | 0.0 | 71.0   | 0.0   | 0.0    | 0.0    | 0.0<br>0       | · · · |
| 400)    | 300) (<br>300) ( | 310)         | 200)<br>0 | 100)<br>8 |            | Х                |           |            | U R.          | 101)   | 202)   | 222)   | 242)   | 302)   | 301)   | 311)   | 403)            | 100)  | 0.    | 101)   | -   | 100)   | .4    | 104)   |        | 302)           | -     |
| ( 300,  | 0.4<br>(400,     | ( 300, 0.5   | (310,     | (200, 0.3 |            | LIN<br>TMF**     |           | (SNTM      | THR           | (8101, | (8202, | (8222, | (8242, | (8302, | (8301, | (8311, | (8403,<br>(8401 | (101) | . 0   | ( 100, | 0.0 | ( 104, | 134   | ( 100, | 0.0    | ( 300 <b>,</b> | > · > |
| L<br>C  | 0.15             | 0.00         | 6C U      | 0.00      | r-1        | a<br>C<br>t<br>S |           | - L L -    | LEFT          |        |        |        |        |        |        |        |                 |       | 302.5 |        | 0.0 |        | 356.2 | (<br>( | 0.0    | c              | >.>   |

| 160.8         | 0.0  | 0.0           | 0.0  | 109.9       | ר<br>ע        |             | 0.0  | 0.0  | 0.0              | 2.0         |             | 0.0   | 26.7 | 0.0         |     | 22.0        | 0.0  | 54.5        |           | 0.0         | 0.0    | 3.9         |      | 1.4  |     |
|---------------|------|---------------|------|-------------|---------------|-------------|------|------|------------------|-------------|-------------|-------|------|-------------|-----|-------------|------|-------------|-----------|-------------|--------|-------------|------|------|-----|
| 21.3          | 1.0  | 803.9         | 0.4  | 91.5        | ע<br>דע       |             | 0.2  | 0.2  | 0.2              | 0.0         |             | 0.1   | 0.0  | 0.1         |     | 0.0         | 1.3  | 0.0         |           | 4.5         | 0.9    | 104.3       |      | 4.5  |     |
| 250.9         | 0.0  | 0.0           | 0.0  | 313.1       | 5 VUC         | 0.102       | 0.0  | 0.0  | 0.0              | 0.0         | (           | 0.0   | 0.0  | 0.0         |     | 0.0         | 0.0  | 0.0         | (         | 0.0         | 0.0    | 27.6        |      | 0.0  |     |
| 21.3          | 0.0  | 0.0           | 0.0  | 17.4        | 1<br>0        | 0<br>• • •  | 0.0  | 0.0  | 0.0              | 32.7        | (<br>(      | 0.0   | 14.1 | 0.0         |     | 11.9        | 0.0  | 27.1        | 0         | 0.0         | 0.0    | 0.6         |      | 8.9  |     |
| 54.4          | 5.7  | 34.7          | 6.7  | 42.7        | 7 85          |             | 4.8  | 1.7  | 4.0              | 0.0         |             | 4.0   | 0.0  | 3.6         |     | 0.0         | 4.2  | 0.0         |           | 1.1         | 3.2    | 8.5         |      | 6.9  |     |
| 60.1          | 0.0  | 0.0           | 0.0  | 66.9        | V LE          | <b>F</b>    | 0.0  | 0.0  | 0.0              | 0.0         | (<br>(      | 0.0   | 0.0  | 0.0         |     | 0.0         | 0.0  | 0.0         | с<br>с    | 0.0         | 0.0    | 44.4        |      | 0.0  |     |
| 45.6          | 0.0  | 0.0           | 0.0  | 41.7        | 5 95          | ר<br>י<br>י | 0.0  | 0.0  | 0.0              | 38.8        | с<br>с      | 0.0   | 20.1 | 0.0         | •   | 18.0        | 0.0  | 33.2        | с<br>с    | 0.0         | 0.0    | 17.5        |      | 16.3 |     |
| 78.7          | 30.0 | 59.0          | 31.0 | 67.0        | 63 0          | ••••        | 29.0 | 7.8  | 10.1             | 0.0         | -<br>-<br>- | T.0.T | 0.0  | 9.6         |     | 0.0         | 10.3 | 0.0         |           | 24.4        | 6.2    | 17.0        |      | 14.3 |     |
| 84.4<br>127 8 | 0.0  | 0.0           | 0.0  | 0.0<br>91.2 | 102.0<br>61 7 | 6.2         | 0.0  | 0.0  | 0.0              | 0.0         | 2.0         | 0.0   | 0.0  | 26.3<br>0.0 | 0.0 | 0.0<br>21.6 | 0.0  | 0.0         | i3.2<br>^ | 0.0         | 0.0    | 0.U<br>52.9 | 3.6  | 0.0  | 1.1 |
| 300)<br>5     | 403) | 400)          | 401) | 400)        | .6            | .1          | 202) | 201) | 222)             | 220)        |             | (787  | 240) | 301)        |     | 300)        | 311) | 310)        | u,<br>,   | 40T)        | 402)   | 200)        | 0    | 220) |     |
| 302,          | 400, | 403,<br>788 5 | 400, | 0.0<br>401, | 90<br>202     | 10.1        | 200, | 200, | 220,             | 0.0<br>222, | 0.0         | 240,  | 242, | 0.0<br>300, | 0.0 | 301,<br>0.0 | 310, | 0.U<br>311, | 0.0       | 403,<br>4.5 | 400,   | 100,        | 94.( | 200, | 1.1 |
| )<br>9 7 4 7  |      |               |      | )<br>)<br>) | 310.0         | 200.9       |      |      | )<br>)<br>)<br>) | 0.0         | 0.0         | 0.0   | )    | )<br>0.0    | 0.0 | 0.0         |      | )<br>)<br>) | 0.0       | 0.0         | )<br>i | ),<br>U.U   | 27.5 |      | 0.0 |

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|             |      |      |      |      |      |      |      | `     |       |      |
|-------------|------|------|------|------|------|------|------|-------|-------|------|
| ( 220, 2    | 40)  | 0.0  | 12.0 | 11.7 | 0.0  | 6.4  | 6.1  | 0.0   | 11.1  | 0.1  |
| 0.0 0.0     | 0.   | 0    |      |      |      |      |      |       |       |      |
| (240, 3     | (00) | 79.1 | 38.7 | 31.1 | 59.3 | 18.9 | 11.3 | 36.4  | 300.0 | 8.1  |
| 35.9 285.8  | 9    | 6.   |      |      |      |      |      |       |       |      |
| ( 300, 4    | (00  | 52.0 | 30.8 | 0.0  | 39.2 | 18.0 | 0.0  | 608.3 | 208.7 | 0.0  |
| 595.2 195.6 |      | 0.0  |      |      |      |      |      |       |       |      |
| (400, 3     | (00) | 85.7 | 43.9 | 40.4 | 72.9 | 31.2 | 27.6 | 753.9 | 557.7 | 12.0 |
| 729.2 498.4 | 1    | 1.0  |      |      |      |      |      |       |       |      |
| ( 300, 3    | 10)  | 0.0  | 24.0 | 27.9 | 0.0  | 10.2 | 14.0 | 0.0   | 45.8  | 12.4 |
| 0.0 13.9    | 9    | 8    |      |      |      |      |      |       |       |      |
| ( 310, 2    | (00) | 65.9 | 31.2 | 33.6 | 47.1 | 12.4 | 14.8 | 121.3 | 181.1 | 4.3  |
| 119.0 162.9 |      | 3.8  |      |      |      |      |      |       |       |      |
| ( 200, 1    | (00  | 0.0  | 23.4 | 21.7 | 0.0  | 14.5 | 12.7 | 0.0   | 196.2 | 46.9 |
| 0.0 186.1   | 34.  | ٢    |      |      |      |      |      |       |       |      |

\*\* TIME FOR VEHICLES CURRENTLY ON THE LINK ARE INCLUDED IN THESE VALUES.

399 VEHICLES (MAXIMUM ALLOWED IS 3500). THE HIGHEST NUMBER OF VEHICLES ON THE NETWORK WAS THIS MAXIMUM OCCURED AT 3209 SECONDS.

TOTAL CPU TIME FOR SIMULATION = 215.47 SECONDS TOTAL CPU TIME FOR THIS RUN = 215.47 SECONDS 0LAST CASE PROCESSED

### VITA

Sami Said Ghezawi, a Jordanian-American citizen, was born in Jordan on April 16. 1960. He attended public school in Knoxville, Tennessee and graduated from Holston High School in June 1978. He then attended the University of Tennessee at Knoxville and received a Bachelor of Science in Civil Engineering on March 18, 1983. During his military service in the Jordanian Armed Forces, he was an instructor in algebra from 1984 to 1986. Upon his return to the United States, he entered the Master's Program at the University of Tennessee, Knoxville and obtained his Master of Science Degree in Civil Engineering (Transportation) on June 1, 1988. His thesis work involved observing both deceleration rates for vehicles and driver reactions while approaching a Traffic Signal on Chapman Hwy., entitled "An Evaluation of a Traffic Signal with a White Bar Strobe Light". He employed his education in the engineering sciences at the Greater City of Amman Municipality as a City Traffic Engineer from 1988 to 1991. As a Traffic Engineer he designed and evaluated traffic signal plans, traffic signs and roadway markings, and was involved in several transportation management studies. In the spring of 1992 he reentered the Graduate School at the University of Tennessee, Knoxville to acquire his Doctorate in Transportation. He held a position as a graduate teacher associate at the University in the Civil and Environmental Engineering Department while completing his courses. The Doctor of Philosophy Degree with a major in Civil Engineering was earned and received in December 1999. Sami Said Ghezawi plans to follow a career in higher education in Amman, Jordan.