

**Tilt-to-length coupling in LISA Pathfinder: A data analysis**

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We present a study of the tilt-to-length coupling noise during the LISA Pathfinder mission and how it depended on the system's alignment. Tilt-to-length coupling noise is the unwanted coupling of angular and lateral spacecraft or test mass motion into the primary interferometric displacement readout. It was one of the major noise sources in the LISA Pathfinder mission and is likewise expected to be a primary noise source in LISA. We demonstrate here that a recently derived and published analytical model describes the dependency of the LISA Pathfinder tilt-to-length coupling noise on the alignment of the two freely falling test masses. This was verified with the data taken before and after the realignments performed in March (engineering days) and June 2016, and during a two-day experiment in February 2017 (long cross-talk experiment). The latter was performed with the explicit goal of testing the tilt-to-length coupling noise dependency on the test mass alignment. Using the analytical model, we show that all realignments performed during the mission were only partially successful and explain the reasons why. In addition to the analytical model, we computed another physical tilt-to-length coupling model via a minimizing routine making use of the long cross-talk experiment data. A similar approach could prove useful for the LISA mission.

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## I. INTRODUCTION

In December 2015, LISA Pathfinder (LPF) [1–3] was launched as technology demonstrator mission for the Laser Interferometer Space Antenna (LISA) [4–6], the first space-based gravitational-wave detector. LPF not only successfully proved the technology planned to be implemented in LISA but also exceeded its requirements, already reaching the LISA performance requirements in the entire frequency band [2,3].

A residual noise originated from the lateral and angular jitter of the spacecraft (S/C) (and subsequently the optical bench) with respect to its two hosted test masses (TMs) in free fall. The jitter affected the path of the beam being reflected at the TMs (red beam in Fig. 1) and induced alterations of the measured length signal. This coupling noise is called tilt to length (TTL) coupling [7,8]. It limited the mission performance between 20 and 200 mHz before

its subtraction in postprocessing [9]. TTL coupling will also be a major noise source in LISA [10,11].

For the suppression of the TTL coupling in LPF, realignments of the two TMs were conducted three times during the mission (in March and twice in June 2016) [9,13]. These realignments significantly reduced the overall TTL coupling. However, the observed TTL noise was not fully understood then, and the existent model described the data insufficiently. Consequently, the realignments did not fully mitigate the noise, making a further subtraction strategy necessary.

In [14], a new analytical model for the TTL coupling in LPF was presented. Within this work, we show that this model, for the first time, successfully explains the dependency of the TTL noise in LPF on the TM alignments. With this model, we were able to reproduce the TTL noise changes due to the TM realignments for TTL suppression, e.g., during the engineering days (ED) in March 2016. Furthermore, we derived how the TMs should have been aligned during the mission for the TTL noise mitigation and compare these newly computed angles with the angles that were commanded instead.

We start with a brief summary of the functionalities of LPF relevant for our analysis in Sec. II and a characterization of the TTL coupling noise in LPF in Sec. III. In Sec. IV, we then introduce the two TTL models, which are the core of our analysis: the fit model that was used for TTL subtraction during the mission and the recently published analytical TTL model. Both models are applied to mission data of experiments, that we explain in Sec. V. The results

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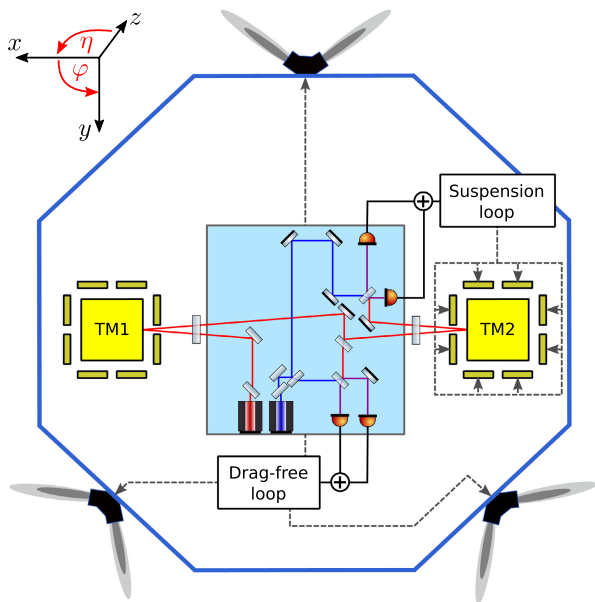


FIG. 1. Simplified sketch of the LPF setup. The yellow squares represent the two TMs which are surrounded by the electrodes from the electrode housing. The light-blue square in the center is the optical bench. The optical setup is reduced to the components relevant for the TM distance changes and control loop measurements. The same holds for the shown beam paths. The red beam represents the measurement beam, i.e., the beam affected by the motion of the S/C or the TMs. The blue beam is not affected by this motion and holds as a reference. Further, the principle of the nominal control mechanisms is shown. The drag-free loop utilized the measurement of the S/C relative to TM1 to define S/C accelerations via the thrusters. The suspension loop is fed in by the readout of the S/C-TM2 alignment used to control the TM2 alignment via electrostatic forces. Figure reproduced from [12].

for the data of the long cross-talk experiment (LXE), that was designed to test TTL coupling, are presented in Sec. VI, and for the data around the TM realignments carried out for TTL suppression in Sec. VII. Finally, we summarize our findings in Sec. VIII.

## II. THE LISA PATHFINDER INSTRUMENT

LPF hosted two TMs in free fall, which were each placed inside an electrode housing. In the following, we briefly introduce the four interferometers in LPF and explain how their measurements were used to control the stability of the optical setup.

### A. The interferometers

LPF had a total of four interferometers, measuring the heterodyne interference signal of two local Gaussian beams. Out of these interferometers, two were maintaining the reliability of the readouts of the other two: the reference and the frequency interferometer. The signal of the *frequency interferometer* was used to stabilize the laser frequency, thus minimizing the noise due to frequency

fluctuations. The *reference interferometer* provided a reference phase signal, which was subtracted from the readouts of the other interferometers.

The *x1-interferometer* measured the interference signal of the local reference beam and a beam that was reflected at the first TM. From this, the longitudinal displacement (i.e., along the  $x$ -axis in Fig. 1) and angular alignment of the S/C with respect to the first TM were obtained. Further, the *x12-interferometer* detected the interference signal of the local reference beam and a beam that was reflected at both TMs. The angular alignment changes of the second TM, as well as the distance changes between both TMs, were obtained from this signal. In the two latter interferometers, the angular alignments were measured utilizing differential wavefront sensing (DWS) [15,16]. In general, the measurements of the  $x1$ - and  $x12$ -interferometers were used to control the stability of the whole system (Sec. II B) and contained the main science signal: the distance variations between the two TMs.

More detailed information about the interferometers in LPF is given in [17–19].

### B. The control mechanisms

The stability of the whole system was maintained by the drag-free attitude control system (DFACS) [12,20]. Its control loops used the readouts of the  $x1$ - and the  $x12$ -interferometers as well as the displacement readout by the gravitational reference sensor (GRS) [21–23] as input. The latter determined the relative positions of the TMs with respect to their housings via electrostatic measurements. Electrodes inside the electrode housings of the TMs were used partly for these measurements and partly to apply forces for alignment correction.

In nominal operation, the DFACS ensured that the S/C followed the first TM (*drag-free control loop*), which was not controlled along the sensitive  $x$ -axis. Then, the second TM followed the S/C (*suspension control loop*) to sustain the alignment of the full optical system. For the S/C and TM alignment corrections, either actuations via the S/C thrusters or the electrodes inside the housings were applied, see Fig. 1. To prevent the electrostatic forces and torques from perturbing the science signal, they were applied at frequencies below the LPF measurement band. Additionally, they were subtracted in post-processing.

To preserve the angular stability of the system, its angular alignment was continuously tracked (mostly via the differential wavefront sensing (DWS) measurements of the  $x1$ - and  $x12$ -interferometer) and kept at predefined nominal offsets by the DFACS. These nominal alignments were redefined three times during the LPF mission for TTL suppression, see Sec. V.

## III. TTL COUPLING IN LISA PATHFINDER

The main science signal in LPF was the residual acceleration between the two TMs along the  $x$ -axis.

Angular and lateral jitter of both the S/C and TMs coupled into that readout and added TTL noise. The TMs were very quiet since they were nominally in free fall and the forces acting on them were kept small. Hence, most of the jitter leading to the TTL coupling noise in LPF originated from the S/C itself. However, for an easier modeling of this coupling, we can equally interpret the S/C jitter as a simultaneous jitter of both TMs with respect to the optical bench in Fig. 1 around the S/C's center of rotation.

We consider two types of jitter: *angular* and *lateral* jitter. The angular jitter of the S/C changed the orientation of the beam that was reflected at the first TM. Consequently, the beam's path length and detection point at the photodiodes changed. Both yielded TTL coupling noise on the final signal [7,8]. Lateral jitter of the S/C added TTL noise if the TM surfaces were tilted with respect to the optical bench. In this case, the TM surfaces shifted into and out of the beam path due to the lateral jitter [7].

In general, angular realignments of the TMs affect the beam's orientation after reflection and the degree of lateral jitter coupling. Therefore, TTL coupling noise can be reduced by optimal rotations of the TMs. Such a realignment also was part of the TTL suppression strategy of the LPF mission. In total, the TMs were realigned three times. This is discussed in Secs. V and VII. We present a corresponding analytical model in the following section.

#### IV. TTL COUPLING MODELS

Modeling TTL coupling is necessary for the successful suppression of this noise. First, simple TTL models are used for the subtraction of the coupling noise in the measurement band. In addition, more complex models that describe the dependency of the coupling on the setup parameters can be used for a suppression via design or realignment.

In this work, we investigate the TTL coupling in LPF with two models: a fit model that was used during the LPF mission for TTL subtraction (Sec. IVA) and the analytical model derived in [14], which additionally describes how the TTL coupling depends on the TM alignments (Sec. IV B). We show in Sec. VIE that a third model can be derived from the mission data. This model describes the dependency of the TTL coupling on the alignment like the analytical model but was computed using only the fit results of different alignment configurations.

##### A. The linear fit model

The TM realignments performed at the beginning of the LPF mission did not fully mitigate the TTL coupling, see Sec. VA. Therefore, a linear TTL model was fitted and then subtracted from the data. In detail, the dependency of the measured acceleration  $\Delta g$  on the mean TM accelerations in the orthogonal degrees of freedom ( $\ddot{\varphi}$ ,  $\ddot{\eta}$ ,  $\ddot{y}$ ,  $\ddot{z}$ ) and on the displacement of the TMs via stiffnesses ( $\bar{y}$ ,  $\bar{z}$ ) was fitted

(see Fig. 1 for the coordinate system definition). These relative accelerations and displacements describe, in a good approximation, the inverse S/C jitter. Additionally, the coupling of S/C jitter along the sensitive axis between both TMs ( $\ddot{o}_1$ ) was considered in the fit. These movements did not alter the distance between both TMs but nonetheless coupled into the signal due to imperfections in the symmetry of the setup. These contributors added up to the following linear fit model [2,3]:

$$\begin{aligned} \Delta g_{\text{xtalk}}^{\text{fit}} = & C_{\varphi}^{\text{fit}} \ddot{\varphi} + C_{\eta}^{\text{fit}} \ddot{\eta} + C_y^{\text{fit}} \ddot{y} + C_z^{\text{fit}} \ddot{z} \\ & + C_{y,s}^{\text{fit}} \bar{y} + C_{z,s}^{\text{fit}} \bar{z} + C_{o_1}^{\text{fit}} \ddot{o}_1. \end{aligned} \quad (1)$$

We make use of this fit model in our TTL data analysis presented in this paper. Analogously to the data analysis and the TTL coupling subtraction during the LPF mission, we performed our computations in MATLAB using the LPF Data Analysis package (LTPDA) toolbox [24]. For the fit of the model Eq. (1) to the  $\Delta g$  measurements, we applied a LTPDA function, which performs a least-square fit in the frequency domain. We chose to consider all frequencies between 2 mHz and 70 mHz. At the upper frequency bound, noise originating from the thrusters coupled into the readout [25], which affected the cross-coupling results. The lower frequency limit was set to 2 mHz to cover the differential frequencies in the LXE (Sec. VI). Further, the fit procedure used the 4-term Blackman-Harris window (BH92). The algorithm stopped when the previous and the current relative residuals differed by less than  $10^{-10}$  (tolerance criterion).

The lateral accelerations and displacements ( $\ddot{y}$ ,  $\ddot{z}$ ,  $\bar{y}$ ,  $\bar{z}$ ) considered in the fit were measured electrostatically by the GRS within the TMs housings [22]. These readouts were processed via the DFACS [20]. Therefore, we also used the DFACS data for the angular (DWS) readouts and the  $o_1$  and  $\Delta g$  measurements in our data analysis. Note that the DWS readouts were also available as optical metrology system [26,27] data. However, there were small shifts between the time sets that would have to be corrected.

Due to cross-sensing in general and the similar pattern of the lateral accelerations ( $\ddot{y}$ ,  $\ddot{z}$ ) and displacements ( $\bar{y}$ ,  $\bar{z}$ ) in particular, the jitter readouts were partially correlated. The coefficient errors provided by the fit algorithm are caused by these correlations and the measurement noise.

##### B. The linear analytical model

In LPF, TTL coupling originated from the lateral and angular jitter of its two hosted TMs or the hosting S/C itself, which can be interpreted as a simultaneous jitter of the TMs relative to the S/C. This jitter coupling can be described via the lever arm and the piston effect. Additionally, the windows between the optical bench and the vacuum housing of the TMs added a small amount



of TTL coupling. All these coupling effects can be computed analytically, as shown in [7,8].

A full analytical TTL coupling model was derived for the LPF setup in [14] considering these effects and further wavefront and detector geometry-dependent coupling terms. The parameters used to describe the LPF optical setup relied on the measurement of the LPF in-flight model [28]. The result was then verified against the numerical computations by the C++ library IfoCAD [15,29,30]. We transformed the model to the form of the fit model [Eq. (1)]—with the exception of the displacements terms  $\bar{y}$  and  $\bar{z}$ , and the longitudinal term  $\ddot{o}_1$ , which were not modeled analytically—to make both models comparable. This yielded

$$\Delta g_{\text{xacc}}^{\text{ana}} = C_{\varphi}^{\text{ana}} \ddot{\varphi} + C_{\eta}^{\text{ana}} \ddot{\eta} + C_y^{\text{ana}} \ddot{y} + C_z^{\text{ana}} \ddot{z} \quad (2)$$

with

$$C_{\varphi}^{\text{ana}} = C_{\varphi,0} + 0.210_{-0.016}^{+0.017} \frac{\text{m}}{\text{rad}^2} \varphi_1 + 0.182_{-0.020}^{+0.018} \frac{\text{m}}{\text{rad}^2} \varphi_2 \quad (3a)$$

$$C_{\eta}^{\text{ana}} = C_{\eta,0} + 0.209_{-0.015}^{+0.017} \frac{\text{m}}{\text{rad}^2} \eta_1 + 0.177_{-0.019}^{+0.018} \frac{\text{m}}{\text{rad}^2} \eta_2 - 0.005_{-0}^{+0} \frac{\text{m}}{\text{rad}^2} \varphi_1 + 0.005_{-0}^{+0} \frac{\text{m}}{\text{rad}^2} \varphi_2 \quad (3b)$$

$$C_y^{\text{ana}} = C_{y,0} + 1.000_{-0}^{+0} \frac{1}{\text{rad}} (-\varphi_1 + \varphi_2) \quad (3c)$$

$$C_z^{\text{ana}} = C_{z,0} + 1.000_{-0}^{+0} \frac{1}{\text{rad}} (\eta_1 - \eta_2). \quad (3d)$$

The model shown here provides the dependency of the coefficients on the TM alignments. These alignments are not the TM tilts relative to the optical bench ( $\hat{\varphi}_i, \hat{\eta}_i$ , but are defined relative to a nominal offset ( $\varphi_i = \hat{\varphi}_i - \varphi_{0i}$ ,  $\eta_i = \hat{\eta}_i - \eta_{0i}$ ). As nominal offsets, we understand here the unknown mean alignment of the TMs relative to the optical bench at the beginning of the investigated timespan.

The errors shown in Eq. (3) for the coefficient estimates were derived by implementing measurement uncertainties of the beam parameters [31] and the location of the S/C's center of mass [32] into the analytical model. Furthermore, we considered a drift of the S/C's center of mass due to nonbalanced fuel consumption. These errors were derived along with the coefficients in [14]. Note that the errors given for the lateral coupling coefficients are not precisely zero but seven orders of magnitude smaller than the coefficients themselves.

The constant offsets  $C_{j,0}$ ,  $j \in \{\varphi, \eta, y, z\}$ , of the coefficients depend on various setup parameters, which are not all precisely known. Additionally, the unknown nominal

rotations of the TMs add into these coefficients. In the following analysis, we therefore substitute these constants by their fitted correspondences. These are either the fitted coefficients during a noise run prior to realignments or the mean of the coefficients computed for different timespans with nonaltered TTL coupling within an experiment, e.g., the LXE.

Note that the effect of tiny instabilities in the system (e.g., temperature-related) and noise variations on the fit almost canceled out for longer noise runs, but altered the results for shorter segments. The corresponding variations of the fitted coefficients were neither covered by their error bars nor modeled analytically. For a better comparison of the fitted coefficients with the analytical computation, we additionally computed the variations of the fit results during a noise run. These could be seen as uncertainties of the offsets  $C_{j,0}$ ,  $j \in \{\varphi, \eta, y, z\}$ , in the analytical model due to the unmodeled instabilities. We split ten days of a noise run in mid-February 2017 into two-hour segments and investigated the variance of the fitted coefficients (Fig. 2). This yielded the deviations (root-mean-squares) of the coefficient estimates presented in Table I. In the following, we will plot the analytical coefficients always with twice these root-mean-squares, which cover all fitted coupling coefficients but the outliers. Since we cannot certainly say whether these deviations are uncorrelated to analytically computed errors, we add both linearly (worst-case estimate). Note that, while the variance of the coefficients can differ over the mission time, these estimates are considered to be useful for the analysis of experiments with small temporal distance and no lasting changes in the setup, e.g., the LXE analyzed in Sec. VI. However, mind also that these variations could even be bigger during the LXE due to the experiments being performed.

When comparing the presented analytical model to the TTL models available during the LPF mission, we find some significant differences. First, the model Eq. (2) only depends on the angular TM alignments, i.e., any lateral displacements of the TMs would not affect the coupling. This finding depends on the center of rotation we take in our evaluation into account: since the S/C jitter is dominant, we apply the rotations in our analysis around its center of mass. In the early models used during the mission, the relevance of the location of the center of rotation was underestimated. For simplicity, the jitter of the TMs was analyzed individually with the center of rotation lying in the TM's center of mass. In this case, lateral TM displacements would have shifted the center of rotation relative to the beam axis. Since such offsets significantly affect the TTL coupling [7], the old models included lateral TM alignment terms not present in the new model presented here. Also, the longitudinal location of the center of rotation was neglected before. This contributed

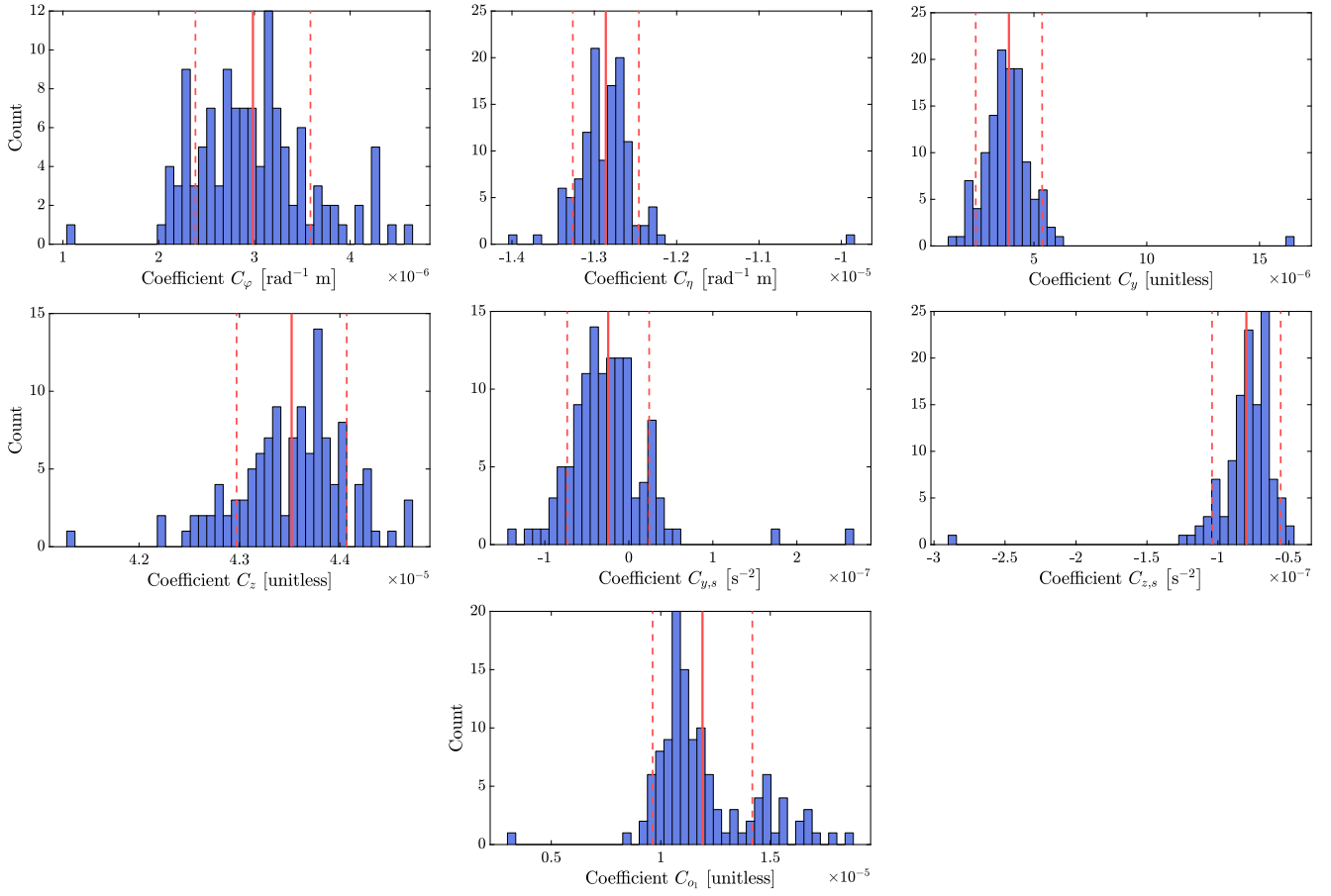


FIG. 2. Histogram of the coupling coefficients fitted for 120 2-hour timespans during the noise run which started on 13th Feb. 2017. The coefficients are not constant but spread about a mean. The dashed red lines are offset from the mean by the root-mean-square. With twice this deviation, we would cover all coefficient estimates but the outliers.

non-negligibly to  $C_\phi^{\text{ana}}$  and  $C_\eta^{\text{ana}}$ . Furthermore, nongeometric coupling effects have been shown to contribute significantly to the overall coupling [8,14].

TABLE I. Fitted coefficients and their variations during the noise measurement starting on the 13th Feb. 2017, 8 AM UTC. The coefficients were computed for 120 2-hour segments of this noise run. Their distribution is shown in Fig. 2. Twice the root-mean-squares of the coefficient deviations cover most of these fit results except for the extreme outliers.

Coefficient name	[unit]	Mean value	Absolute deviations	Root-mean-square
$C_\phi$	$[\mu\text{m rad}^{-1}]$	2.98	$\pm 1.76$	0.60
$C_\eta$	$[\mu\text{m rad}^{-1}]$	-12.86	$\pm 2.05$	0.40
$C_\gamma$	$[10^{-6}]$	3.89	$\pm 7.55$	1.47
$C_z$	$[10^{-6}]$	43.52	$\pm 1.70$	0.55
$C_{y,s}$	$[10^{-6} \text{ s}^{-2}]$	-0.02	$\pm 0.20$	0.05
$C_{z,s}$	$[10^{-6} \text{ s}^{-2}]$	-0.08	$\pm 0.12$	0.02
$C_{o1}$	$[10^{-6}]$	11.90	$\pm 7.76$	2.28

## V. THE TTL COUPLING EXPERIMENTS DURING THE MISSION

As we explained in Sec. III and will further show in Secs. VI and VII, the TTL coupling during the LPF mission depended on the alignment of the TMs. By realigning either of the TMs, we modified the coupling of the different TTL mechanisms acting together in the case of the LPF setup [7,8]. Therefore, suitable TM tilts can suppress the full TTL coupling if the single effects counteracted each other. During the mission, the TMs were realigned three times for a TTL noise suppression: on the 16th March, 19th June and 26th June 2016.

Furthermore, we performed an experiment during the LPF mission extension phase with the aim of studying the dependency of the TTL coupling on the TM positions, the LXE.

In the following, we introduce these two TTL coupling investigations.

### A. Redefinition of the TM set-points

The TM alignment set-points were redefined three times during the LPF mission (Table II). The new set-points were

TABLE II. Adaptations of the TM set-points in their angular degrees of freedom (DoF) for TTL suppression relative to the TM alignment before the 16th March 2016. Times are given in UTC and correspond to the year 2016. The angles were partially corrected compared to [13].

DoF	[unit]	16.03. 14:28	19.06. 8:20	25.06. 8:00
$\varphi_1$	[ $\mu\text{rad}$ ]	-59.25	-57.32	-61.2
$\varphi_2$	[ $\mu\text{rad}$ ]	-21.35	-33.01	-9.7
$\eta_1$	[ $\mu\text{rad}$ ]	-3.5	-2.14	-4.9
$\eta_2$	[ $\mu\text{rad}$ ]	3.5	10.3	-3.3

derived from simplified geometrical TTL models. The analytical model [Eq. (2)] used for the analyses in this work was not yet available by then.

The first realignment, in March 2016, reduced the TTL coupling by a factor of two. The residual TTL noise was then subtracted as shown in [9,33]. Yet, the question remained whether better alignment could be achieved suppressing the noise prior to subtraction even further. Therefore, the TM realignment was repeated in June 2016 after continuing theoretical investigations of the TTL noise. The first attempt on 19th June was less successful than expected and even increased the noise level. This was caused by a sign error and corrected for by a second realignment performed on 25th June. These alignment settings were then left untouched until the mission ended. A comparison of the different levels of TTL noise in the  $\Delta g$  observable is plotted in Fig. 3. When we compare the “bump” before (dark green) and after (yellow) the two TM realignments in June, we see that the noise was only

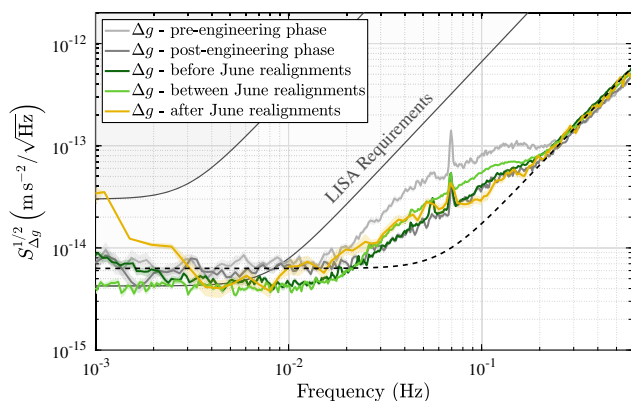


FIG. 3. Changes of the  $\Delta g$  observable due to realignments of the TMs. Dark green:  $\Delta g$  before the realignments in June (three day noise run ending on the 18th June 2016). Light green:  $\Delta g$  in between the realignments in June (noise run from the 20th to 24th June 2016). Yellow:  $\Delta g$  after the realignments in June (one hour data with low noises at the 26th June 2016). These noise runs are defined in further detail in Sec. VII B 1. The gray curves show the  $\Delta g$  observable before and after the realignment during the ED for comparison. Black dashed curve: LPF performance model for the time of the ED.

reduced above 70 mHz. Below these frequencies, the new alignments yielded an increased noise. The shape of the bump depends on the dominant TTL noise contributors, which we further discuss for these cases in Sec. VII B.

Since neither of the realignments resulted in a full TTL noise suppression, it was at all times of the mission necessary to subtract the residual TTL noise from the data.

We show in Sec. VII that the noise level changes caused by the three realignments can be reconstructed and explained by the analytical model Eq. (2). Also, we present TM alignments which presumingly would have made a full TTL suppression via realignment possible.

## B. Description of the cross-talk experiments

For a detailed study of the TTL coupling in LPF and the insufficiency of the former analytical models, two cross-talk experiments were performed during the mission extension phase of LPF (starting in Dec. 2016). First, a short experiment was executed on the 20th Jan. 2017, followed by the LXE about two weeks later [13].

The short cross-talk experiment (SXE) consisted of a series of sinusoidal injections applied to the TMs about their nominal alignment, causing a sinusoidal S/C motion due to the attitude control loops. At first, parallel lateral displacements of the TMs along  $y$  were commanded, inducing a sinusoidal lateral translations of the S/C. After a short break, antiparallel lateral displacements of the TMs in the same plane were injected. These were compensated by a sinusoidal rotation of the S/C. Finally, a sinusoidal injection with one frequency was applied to the first TM, while at the same time a sinusoidal injection with another frequency was applied to the second TM. This corresponded to a more complex superposition of translations and rotations of the S/C. This series of injections was then repeated along  $z$ , resulting in the total of six different injection types summarized in Table III.

The LXE was performed between the 4th Feb. 2017, 21:00 UTC, and 6th Feb. 2017, 23:00 UTC, in order to provide data for an exhaustive test and correction of the physical TTL coupling model containing the TMs alignment information. The data obtained from the LXE allowed

TABLE III. Sequence of performed injections during the SXE. Table reprinted from the authors’ publication [13].

Injection type	Amplitude [ $\mu\text{m}$ ]	Frequency [mHz]	Duration [min]	Ramp duration [min]	Wait time [min]
$y_1 = y_2$	0.5	17	30	8	5
$y_1 = -y_2$	0.5	12	30	8	5
$y_1, y_2$	0.3	10, 17	50	8	10
$z_1 = z_2$	0.5	5	50	8	5
$z_1 = -z_2$	0.5	8	30	8	5
$z_1, z_2$	0.3	5, 8	50	5	...

TABLE IV. Timeline of the LXE that was performed between the 4th and 6th of February 2017. Times are given in UTC. The shown set-points were commanded relative to the initial TM positions. Table reprinted from the authors' publication [13].

#	Start time (month.day hour:minutes)	End time	Set-point (Relative to initial)
1	02.04 22:02	02.05 00:08	$y_1: -30 \mu\text{m}$
2	02.05 00:36	02.05 03:34	$z_2: 10 \mu\text{m}$
3	02.05 04:00	02.05 07:00	$z_1: 21.6 \mu\text{m}$
4	02.05 07:27	02.05 09:34	$y_2: -22 \mu\text{m}$
5	02.05 10:00	02.05 13:00	$\eta_1: 12.1 \mu\text{rad}$
6	02.05 13:25	02.05 15:25	$\varphi_2: 20 \mu\text{rad}$
7	02.05 16:00	02.05 18:11	$\varphi_1: 30 \mu\text{rad}$
8	02.05 18:35	02.05 21:34	$\eta_2: -20.3 \mu\text{rad}$
9	02.05 22:05	02.06 03:27	$y_1: -10 \mu\text{m}, z_1: 5 \mu\text{m}$
10	02.06 04:32	02.06 09:35	$y_1: -20 \mu\text{m}, y_2: -10 \mu\text{m}, z_1: 15 \mu\text{m}, z_2: 5 \mu\text{m}$
11	02.06 10:03	02.06 15:34	$y_1: -25 \mu\text{m}, y_2: -15 \mu\text{m}, z_1: 20 \mu\text{m}, z_2: 15 \mu\text{m}, \varphi_1: 10 \mu\text{rad}, \eta_1: 5 \mu\text{rad}$
12	02.06 16:00	02.06 21:35	$y_1: -35 \mu\text{m}, y_2: -25 \mu\text{m}, z_1: 25 \mu\text{m}, z_2: 25 \mu\text{m}, \varphi_1: 20 \mu\text{rad}, \eta_1: 10 \mu\text{rad}, \varphi_2: 10 \mu\text{rad}, \eta_2: -5 \mu\text{rad}$

testing the analytical model Eq. (3). The experiment consisted of twelve SXE-type subexperiments with different set-points. This means that first, one or both TMs were shifted or rotated with respect to their nominal alignment. An overview of the chosen set-points is given in Table IV. Note, that also lateral set-points were chosen since these were assumed to change the TTL noise according to the old coupling models (see Sec. IV B). Depending on the set-point, SXE-type injection were applied: If the TM position or orientation was changed only in the  $xy$ -plane ( $y_1, y_2, \varphi_1, \varphi_2$  alignments), only the  $y$ -injections were applied. Analogously, only  $z$ -injections were commanded if the respective set-point included only changes in the  $xz$ -plane ( $z_1, z_2, \eta_1, \eta_2$  alignments). For TMs set-points in both planes, the full set of SXE injections was chosen. In the last step, after the injections, the TMs were brought back to their nominal position.

## VI. LONG CROSS TALK EXPERIMENT

In this section, we use the data of the LXE introduced in the previous section for the analysis of the performance of both introduced TTL models. We first analyze the performance of both models on subtracting the induced TTL noise (Sec. VI A), and directly compare the corresponding TTL coefficients (Sec. VI B). The residual differences between both models are discussed in Sec. VI C based on the noise contributors in the single subexperiments of the LXE. In Sec. VI D, we extend the former linear TTL models to quadratic models. Finally, we present in Sec. VI E a simple method how the realignment information could be derived without an analytical model. We show that this method provides comparable results for the LXE data as the analytical model.

### A. Performance of the TTL models

To assess the performance of the fit and the analytical TTL model, we applied both to the data of the LXE and investigated the residual after subtraction from the observable  $\Delta g$  (see Ref. [3] for the preparation of  $\Delta g$ ). Since the fit model Eq. (1) also considers stiffness terms and the residual acceleration of the S/C along the optical axis ( $\ddot{o}_1$ -term), these needed to be added to the analytical model for the comparison of both models. We fitted these coefficients ( $C_{y,s}, C_{z,s}, C_{o_1}$ ) to the difference of the  $\Delta g$  measurement and the analytical model Eq. (2). The offsets  $C_{i,0}$  of the analytical coupling coefficients [Eq. (3)] were replaced by the mean of the fitted coefficients in subexperiments in which they should not (or only negligibly) change according to the analytical model (i.e., the experiments 1-5 and 8-10 in the case of  $C_{\varphi,0}$  and  $C_{y,0}$  and experiments 1-4, 6-7 and 9-10 in the case of  $C_{\eta,0}$  and  $C_{z,0}$ ). While these coefficients changed during the mission due to stresses and relaxations of the optical system [34], they can be assumed constant in short timespans, e.g., for the time of the LXE.

Let us first investigate the performance of the fit model shown in Fig. 4. Note here that the coupling coefficients of Eq. (1) were fitted for each subexperiment individually, resulting in one set of coefficients per subexperiment. The subtraction of these fits from the  $\Delta g$  observable removed different levels of noise in the different experiments. The subtraction worked better at frequencies belonging to the injections along  $y$  than for the  $z$ -injections, compare, e.g. the blue residual in subexperiment no. 1 ( $y$ -injections at 10, 12 and 17 mHz) with the blue residual in subexperiment no. 2 ( $z$ -injections at 5 and 8 mHz). We further discuss this in Sec. VI C. Also, the linear fit model does not well subtract the TTL noise at sums and multiples of or the



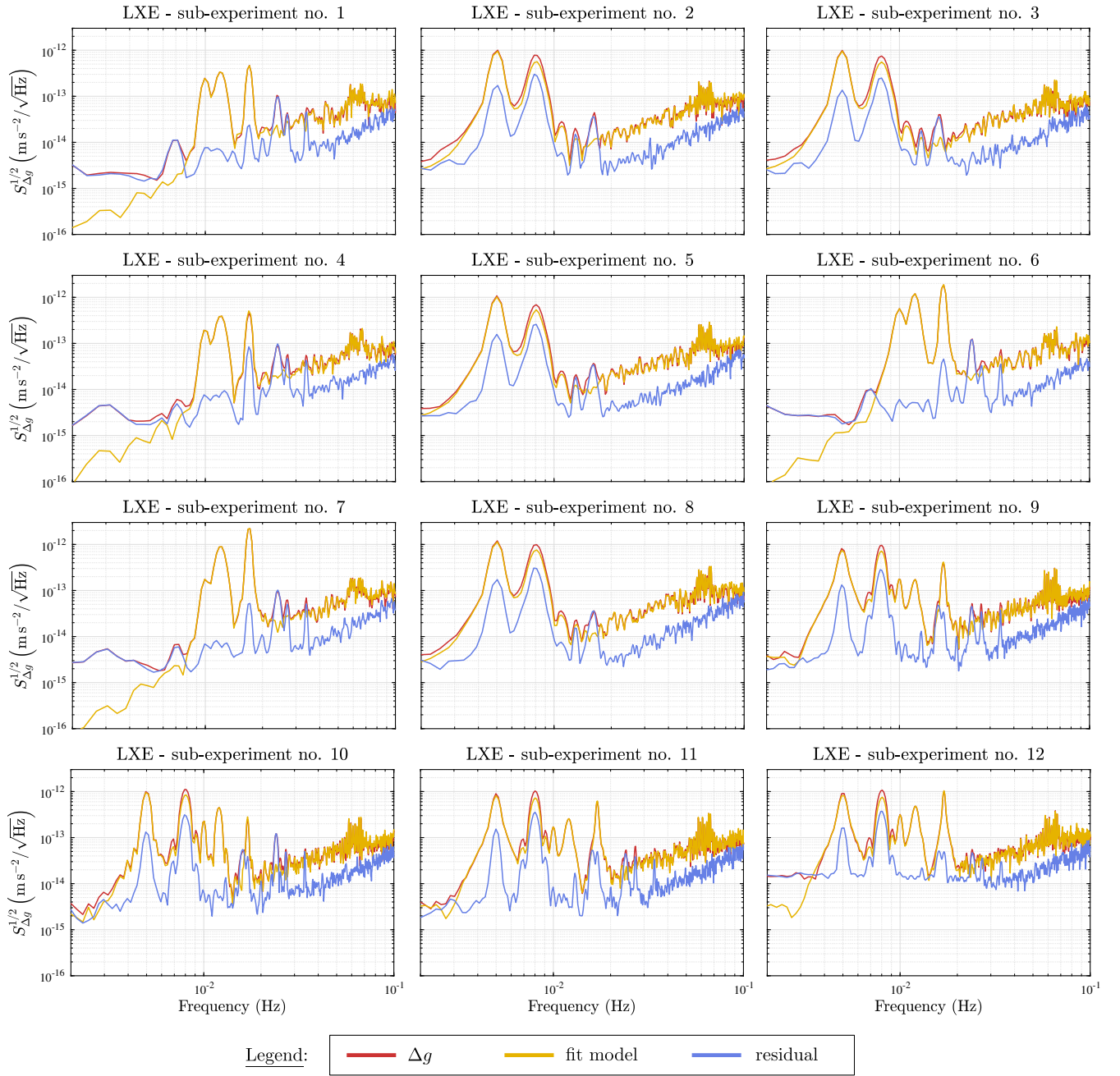


FIG. 4. Performance of the fit model for the twelve subexperiments of the LXE. The red curve shows the ASD of the observable  $\Delta g$ . The yellow curve shows the respective density of the linear model fitted to the data. The blue curve shows the residual remaining after the subtraction of the fit from  $\Delta g$ . The noise peaks at the injection frequencies of the  $y$ -injections (10, 12 and 17 mHz) are well subtracted, and the noise at the injection frequencies of the  $z$ -injections (5 and 10 mHz) is significantly reduced. The noise above 20 mHz is suppressed except for the multiples of the injections frequencies not covered by the linear fit model.

differential injection frequencies. Most prominent are here the residual peaks at 7, 24, 27 and 34 mHz for  $y$ -injections and at 13 and 16 mHz for  $z$ -injections. Since the noise at these frequencies originated from higher-order effects, it is naturally not covered by linear models. However, we show in Sec. VI D that this noise is subtracted by second-order models. In general, the TTL coupling induced noise

at frequencies above 20 mHz (the “bump” [3,9]), where it was dominating during the mission, was well reduced in all subexperiments.

Also, the analytical model subtracted the noise at the injection frequencies well, see Fig. 5. However, the residual at the injection frequencies is, in most cases, larger than the remaining noise after the subtracted fit model, compare e.g.

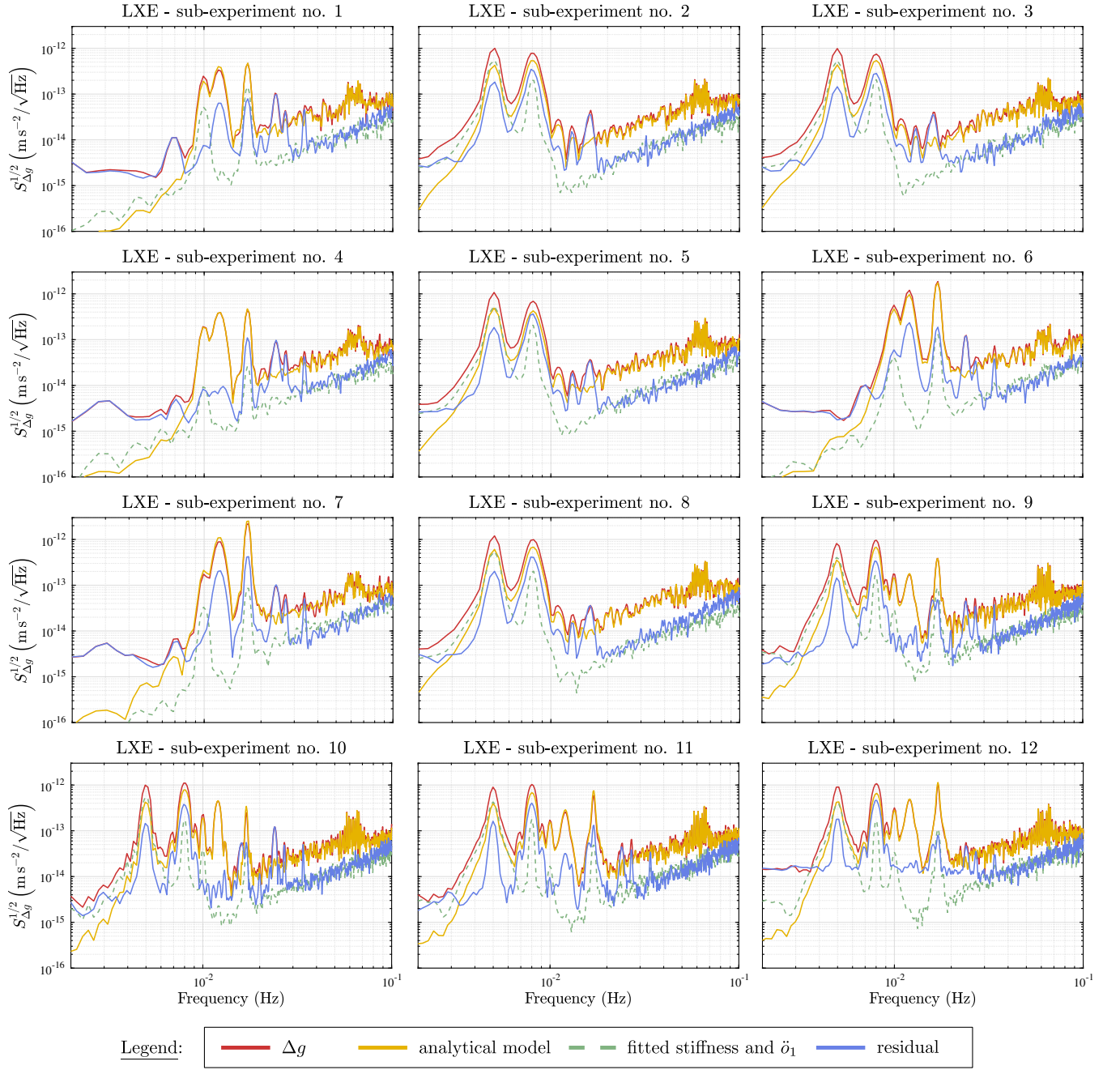


FIG. 5. Performance of the analytical model for the twelve subexperiments of the LXE. The red curve shows the ASD of the observable  $\Delta g$ . The yellow curve shows the ASD of the linear analytical model [Eq. (2)]. The dashed green line pictures the ASD of the stiffness terms and the cross-coupling of residual S/C motion along the optical axis fitted to the difference between  $\Delta g$  and the analytical model. The blue curve shows the residual remaining after the subtraction of the analytical model and the fitted terms from the measurement. The subtraction analytical model significantly reduces the noise at the full frequency range dominated by the TTL coupling, with the exception of the multiples of the injections frequencies, which are not covered by this linear model.

the residuals in subexperiment 6 in Figs. 4 and 5. Still, the analytical model significantly reduced the TTL noise in all subexperiments. Like the fit model, the analytical model performs slightly worse at the frequencies of the  $z$ -injections and naturally does not cover coupling at sums and multiples of or the differential injection frequencies.

In summary, both TTL models, Eqs. (1) and (2), allow subtracting the TTL noise sufficiently well. While the fit model subtracts the injected noise better, the presented analytical model explains additionally the dependency of the TTL coupling on the TM alignments in all subexperiments.

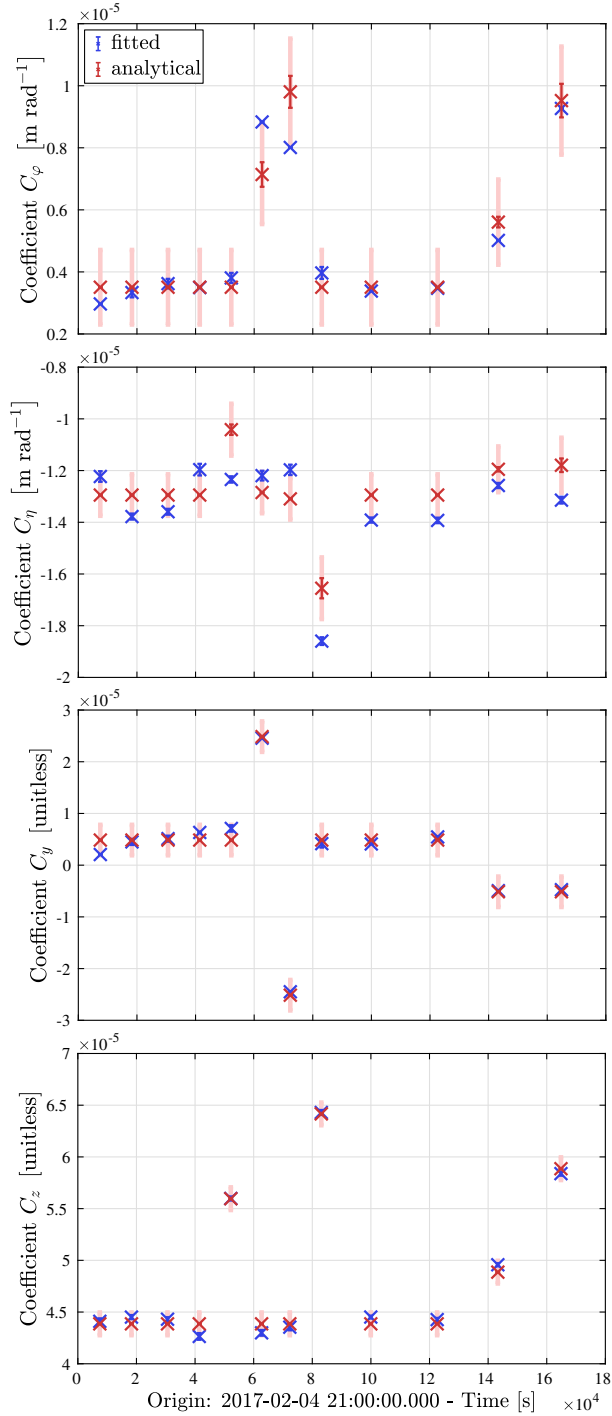


FIG. 6. Comparison of the fitted (blue) and analytically derived (red) coupling coefficients for the 12 subexperiments of the LXE. They are representatively plotted in the mid of the timespan of the experiments each. The fit was conducted in the frequency range from 2 to 70 mHz. The error bars of the fit are plotted. The error bars of the analytical coefficients correspond to their uncertainties given in Eq. (3). Moreover, we show the respective additional double root-mean-square of the fit deviations within a noise run to cover unmodeled instabilities (see Sec. IV B) in light red. Times are given in UTC. Most coefficients match when considering the error bars and expected variations of the fit results. Only in the case of the  $C_\eta$  coefficient we find few mismatches.

## B. Comparison of the TTL models

The four TTL coefficients  $C_\varphi$ ,  $C_\eta$ ,  $C_\gamma$ , and  $C_z$  are contained by the fit and the analytical model. Hence, we can directly compare these coefficients with each other. In the last section, we have seen that the coefficients provided by the fit approach yield a slightly better suppression of the TTL noise. However, they do not provide information about the physical origin of the TTL noise or how to suppress it. On the other hand, the analytical coefficients directly correspond to the TM alignments. An agreement of both sets of coefficients within their error bars and expected variations would be a mutual confirmation of both TTL coupling models.

The comparison of both sets of coefficients is illustrated in Fig. 6. In this figure, we see that the lateral coefficients  $C_\gamma$  and  $C_z$  match to a high degree in all twelve subexperiments. In the case of the angular coupling coefficients, we see a deviation in some experiments.

For the  $C_\varphi$  coefficient, the values of the 6th and 7th subexperiment do not match well. At these times, the TMs were realigned in  $\varphi$ . Compared to the fitted result, the analytical  $C_\varphi$  coefficient yields a slightly smaller value in the case of the rotation of TM2 and a larger value in the case of the rotation of TM1. The differences are small and are mostly covered by the variations of the fitted coefficients seen during the noise run mid-February. In the analytical model they could result from incorrect assumptions concerning the setup parameters or their uncertainties. For example, a longitudinal displacement of the center of rotation by 1.4 cm could explain these differences. This shift would be twice as big as the uncertainty assumed for this parameter.

The differences of the  $C_\eta$  coefficient are, for the most part, of another origin. From the analytical model [Eq. (3)], we would have expected the coefficient to be (almost) constant in all experiments without pitch rotations of the TMs (compare Table IV). However, out of these eight experiments, we find four larger fit-coefficients in the cases where only  $y$ -injections were applied (the 1st, 4th, 6th, and 7th subexperiment). The four other experiments (the 2nd, 3rd, 9th, and 10th subexperiment) include  $z$ -injections, and the corresponding fit-coefficients distribute about a lower level. Additionally, we find the fit-coefficients of the other four experiments with  $z$ -injections but also TM set-point in pitch (the 5th, 8th, 11th, and 12th subexperiment) below their analytical correspondence. No such characteristic of the fit-coefficients was discovered for the  $C_\varphi$  coefficients. Thus, we suspect the  $z$ -injections themselves altered the level of the  $C_\eta$  coefficients and investigate this in the following paragraphs. This means that the coupling coefficient for the stimulated motion at the injection frequencies is different than the coupling in the bump (increased noise at frequencies above 20 mHz), where the S/C jitters freely.

### 1. Adaptations of the fit settings

For comparison, we repeated the fit restricting the considered frequency span to the bump frequencies, i.e.,

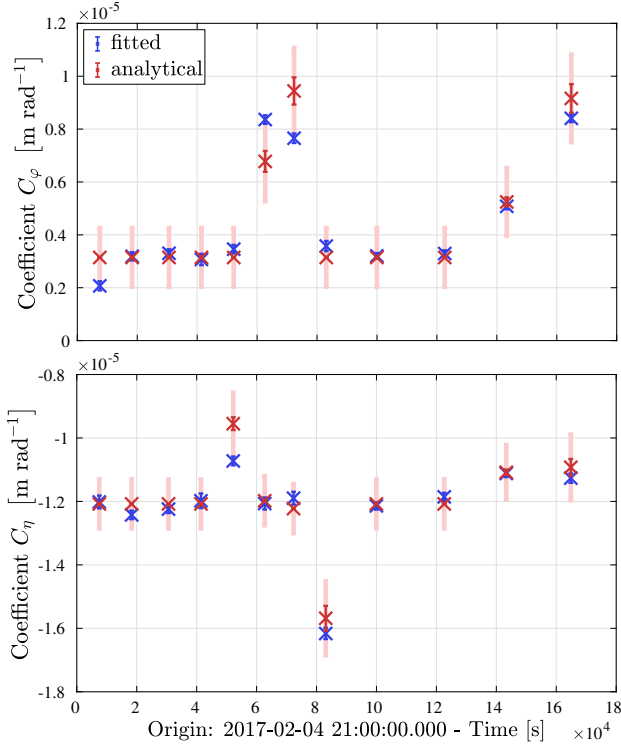


FIG. 7. Same as Fig. 6 but with the fit using a frequency range restricted to the bump only (i.e., 20 to 70 mHz). The results of this fit is shown in blue. The distribution of the analytical coefficients is again plotted in red. Their offset was adjusted to the new mean of the fitted coefficients in experiments in which they are not expected to (significantly) change. Compared to Fig. 6, the fitted  $C_\eta$  coefficients do not split into two levels. Therefore, the fitted and analytical coefficients match better.

20 mHz to 70 mHz (the original upper bound). This changed the lateral coefficients only negligibly. The changes of the angular coupling coefficients are shown in Fig. 7. In this figure, the fitted  $C_\eta$  coefficients do not distribute about two levels and almost match the analytical predictions, which confirms our assumption that the  $z$ -injections affect the fit result. The absolute difference of the  $C_\eta$  coefficients, fitted for frequency regimes with and without the injection frequencies, is almost  $2 \mu\text{m}/\text{rad}$  in experiments with  $z$ -injections.

We further compared these results with the numbers we find when fitting the coefficients for the injection frequencies only. We chose to fit the oscillations in the time domain (least-squares routine) by finding a model

$$f(t) = C_s \sin(\Omega_{\text{inj}} t) + C_c \cos(\Omega_{\text{inj}} t) + \sum_{i=0}^4 c_i t^i, \quad (4)$$

with the time  $t$  and the injection frequency  $\Omega_{\text{inj}}$ , for the measurements of  $\Delta g$  and the exceeded coupling parameter  $\vec{j}$ ,  $j \in \{\varphi, \eta, y, z\}$ . The coupling coefficients correspond to

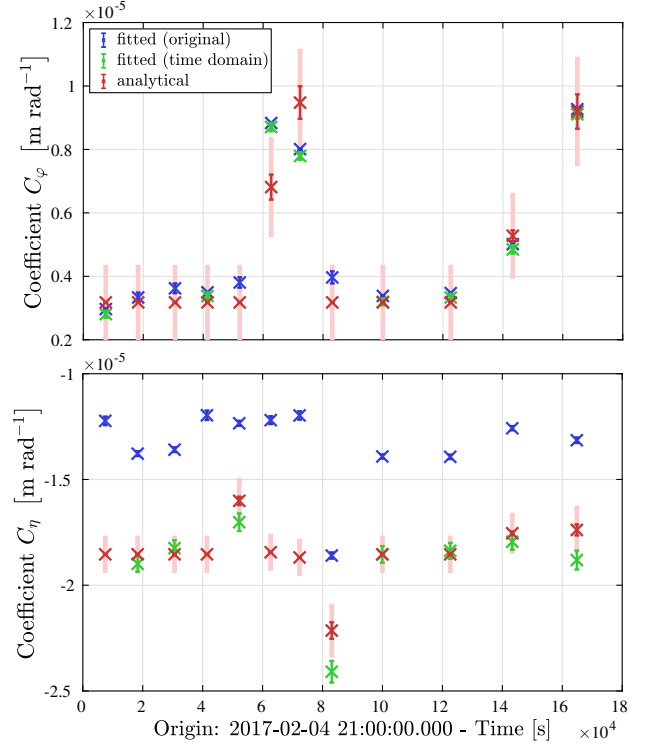


FIG. 8. Comparison of the fitted (injections only, green) and analytically derived (red) coupling coefficients for the 12 sub-experiments of the LXE. The time domain fit for the injection frequencies is further described in Sec. VI B 1. Compared to Fig. 7, the resulting  $C_\eta$  coefficients distribute about a significantly lower level, while the  $C_\varphi$  coefficients did not significantly change. The distribution of the analytical coefficients is plotted in red. Their offset was adjusted to the mean of the fitted coefficients (green) in experiments in which they are not expected to (significantly) change. The blue coefficients correspond to the original fit result shown in Fig. 6.

the quotient of the two fitted  $C_s$ 's. The results are plotted in Fig. 8 together with the fit results in the original frequency domain and the analytical computations. We find that the  $C_\eta$  coupling coefficients for the injection and bump frequencies differ even by approximately  $6 \mu\text{m}/\text{rad}$ . This is in the same order of magnitude as the fitted coefficients themselves.

We do not see a comparable splitting into different levels in the case of the  $C_\varphi$  coefficients (compare  $C_\varphi$ -graphs in Figs. 6 and 7). Thus, the split of the  $C_\eta$  coefficients into two levels must be related to a characteristic difference between the jitter coupling in the  $xy$ - and the  $xz$ -plane. We discuss these in detail in the following subsection.

## 2. Origin of the different $C_\eta$ coupling levels

First, it was shown in [14] that the lateral coupling coefficients almost only depend on the differential angular alignment of the two TMs in LPF. Thus, we cannot only compute the coupling coefficients from the TM alignment



angles but also derive the differential TM angles from the coupling coefficient fits. This is discussed in further detail in [34]. Using the mean levels of the fitted coefficients in Fig. 6 and their relation to the TM alignments in Eqs. (3c) and (3d), we find an approximate differential pitch angle  $\Delta\eta = \eta_2 - \eta_1 \approx -45 \mu\text{rad}$ , which is nine times as big as the differential yaw angle  $\Delta\varphi = \varphi_2 - \varphi_1 \approx 5 \mu\text{rad}$ . Therefore, any TTL coupling differences for the injection and bump frequency span that depend on the TM alignments were different for yaw and pitch jitter. A level change of the  $C_\varphi$  coefficient of a ninth of the magnitude of the observed  $C_\eta$  coefficient changes is smaller than the alternations due to the fit itself. Hence, we would not see it in Fig. 6, which could explain the absence of levels in the  $C_\varphi$  case.

The equations presented in this paper show the TTL coupling effect for a S/C rotation about its center of rotation. This is representative for the TTL noise measured during noise runs. However, in the case of the applied injections during the LXE, the S/C rotated about a pivot defined by the control loops. This pivot was the geometrical center of the optical bench. Both centers of rotation differ by less than a millimeter in  $x$ - and  $y$ -direction. However, in  $z$ -direction, the S/C center of mass lies several centimetres below the optical bench. If computing the differences of the angular coupling coefficients ([13], supplemental material), we find the TM alignment dependent terms of  $C_\varphi$  and  $C_\eta$  to change only in the third relevant digit. Using the numbers of the differential TM alignment angles presented above, we deduce that the different centers of rotation can explain at most 10% of the coupling coefficient differences.

S/C jitter in  $\eta$  about the lowered center of rotation at the bump frequencies would also make the S/C jitter along the  $x$ -axis. Thus, we further investigated whether a correlation between the  $\eta$ - and  $\varphi$ -jitter caused the  $C_\eta$  coefficient changes. Therefore, we repeated the fit using the frequency range of the bump without the  $C_{\varphi_1}$  coefficients. This attempt yielded only minimal coefficient changes.

To preserve the stability of the LPF satellite, its control scheme [20] not only commanded the S/C response to TM displacements but also rotated the TMs with respect to the S/C. This control loop was implemented at low frequencies. Thus, it was too slow to play a role in the analysis of TTL coupling at the frequencies of the bump. However, for the injections, we can expect TM rotations of approximately 10% of the measured S/C jitter but of inverse sign. The DWS measurements were the sum of both rotations. These TM rotations would alter the angular coupling coefficients for the injections compared to the bump. The exact change depends on the absolute alignment angles of the TMs, which are unknown. We estimated that the mechanism could only explain the  $C_\eta$  coefficient levels if the TMs were nominally rotated by more than  $100 \mu\text{rad}$  in pitch but not in yaw. These large angles are very unlikely. Therefore, TM rotations were not the only reason for the  $C_\eta$  coefficient levels but could explain parts of it.

As we will show in Sec. VIC, the stiffness terms of the fit model [Eq. (1)] contribute significantly at the injection frequencies but are almost negligible at the bump frequencies. Thus, they potentially altered the fit results of the coefficient in the same plane if injections were applied. However, the relevance of the stiffness terms in our analysis remains unknown since we cannot study them on their own: If injections were applied, the terms  $\bar{y}, \bar{z}$  oscillate at the same frequency as their second derivatives  $\ddot{y}, \ddot{z}$ .

Figure 4 showed that the linear fit model did not cover the noise peaks at the sums of the injections frequencies, which result from higher-order TTL coupling. Since these peaks are within the fit regime, the question arises whether they alter the fit results. We discuss higher-order coupling in Sec. VID. There, we show that extensions of the fit model to higher-order coefficients do not significantly alter the linear coupling coefficients. Thus, the coefficient changes were not related to the higher-order effects.

In summary, we have learned that different coupling coefficients explain the  $C_\eta$  jitter at the injection and the bump frequencies. Also, we found a few mechanisms that yield a deviation of the  $C_\eta$  coupling coefficient fit for these frequencies. Neither of these mechanisms could explain the coefficient changes we found alone. Therefore, we assume that a combination of several effects sums up to the observed deviations.

All together, we could show the fitted and analytical TTL coupling coefficients match to a high degree in the absence of injections, i.e., during noise runs. We make use of this result in Sec. VII.

### C. Noise contributors

We have shown in the Sec. VIB 1 that we find different  $C_\eta$  coefficients if fitting either only the bump or only the injections. When applying the fit to the full frequency regime (2–70 mHz), the resulting coupling coefficient is a compromise between both single coupling coefficients. The impact of either of the coefficients on the combined result was the higher, the higher the noise in the respective frequency regime. Here, we investigate the noise levels of the single TTL coupling contributors. These are illustrated in Fig. 9. We find that the jitter in  $\ddot{\eta}$  was one of the main noise contributors at the bump frequencies. Thus, it significantly contributes to the  $C_\eta$  fit in the combined frequency regime. Consequently, when using the resulting compromise fit coefficient for the noise subtraction, we expect considerable residuals at the  $z$ -injection frequencies (compare Fig. 4).

In general, Fig. 9 shows that the TTL coupling jitter terms add with very different levels to the full noise. We found that the stiffness coupling was large at the injection frequencies (if injections were applied in the corresponding plane) but negligible at the bump frequencies. The accelerations along  $y$  and  $\varphi$  were small if no realignments in  $\varphi_1$  or  $\varphi_2$  were applied (6th, 7th, 11th, and 12th subexperiment). In these cases, the acceleration

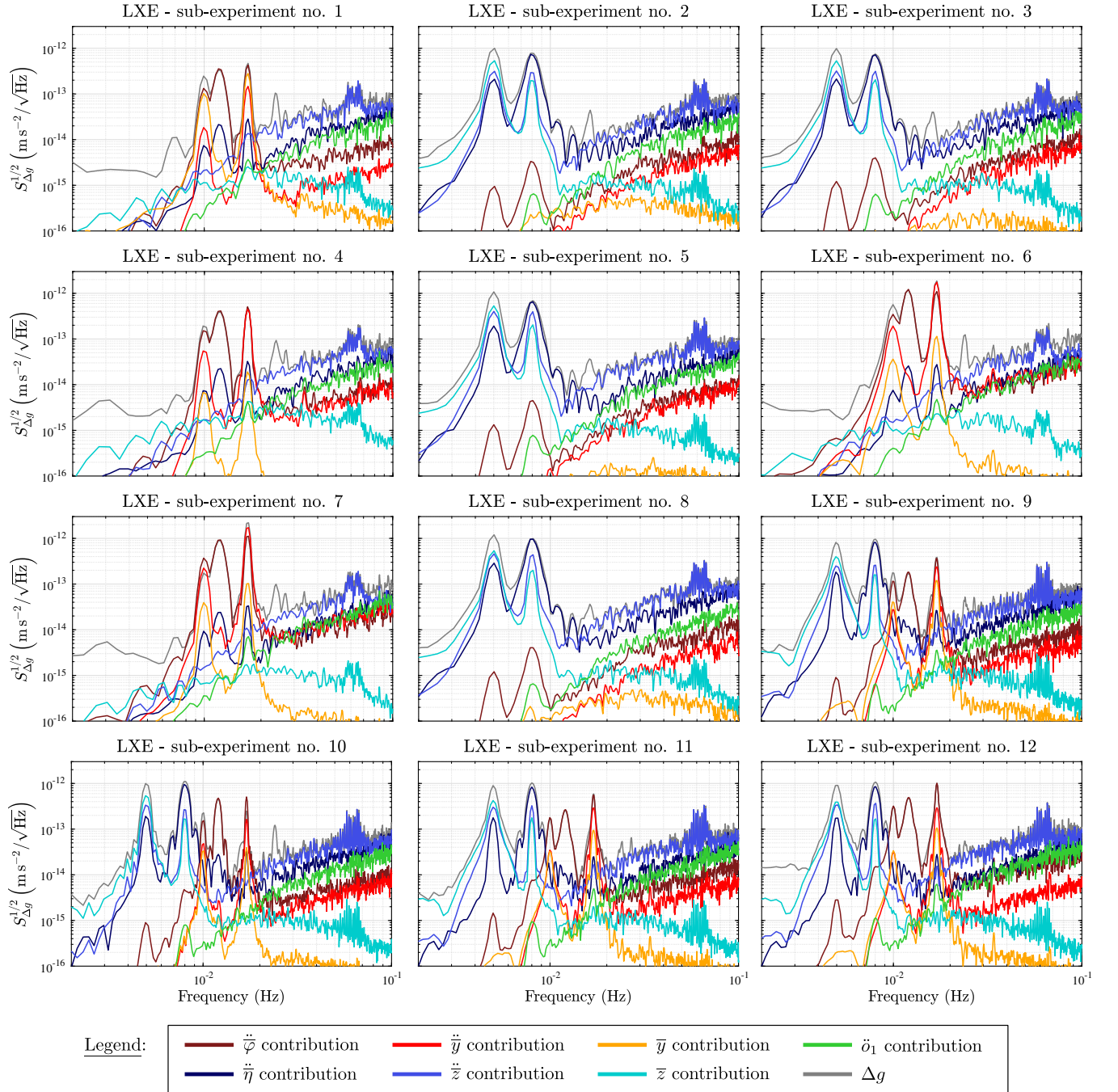


FIG. 9. The ASDs of the noise contributors during the subexperiments of the LXE. The observable  $\Delta g$  is given in gray. The colored curves show the measurements in the respective DoF scaled by their fitted coupling coefficients. In all experiments, the acceleration noise in the  $xz$ -plane is dominant at TTL noise bump. The most dominant is the  $\ddot{z}$  noise contribution, which almost only explains the bulge between 55 and 70 mHz.

along  $z$  and  $\eta$  were the largest TTL noise contributors to the TTL noise bump. Particularly, the  $z$ -jitter explains almost completely the bulge between 55 and 70 mHz.

We show in Sec. VII that the large  $\ddot{\eta}$ - and  $\ddot{z}$ -jitter noise at high frequencies resulted partially from their insufficient suppression by TM realignments. Their reduction was worse compared to the jitter in the other plane. Further, we discuss

in [34] that additional TTL coupling changes resulted from drifts of the coefficients (largest for the  $C_z$ -coefficient).

#### D. Second-order models

We have seen in Figs. 4 and 5 that neither of the linear models subtract the noise peaks at sums and

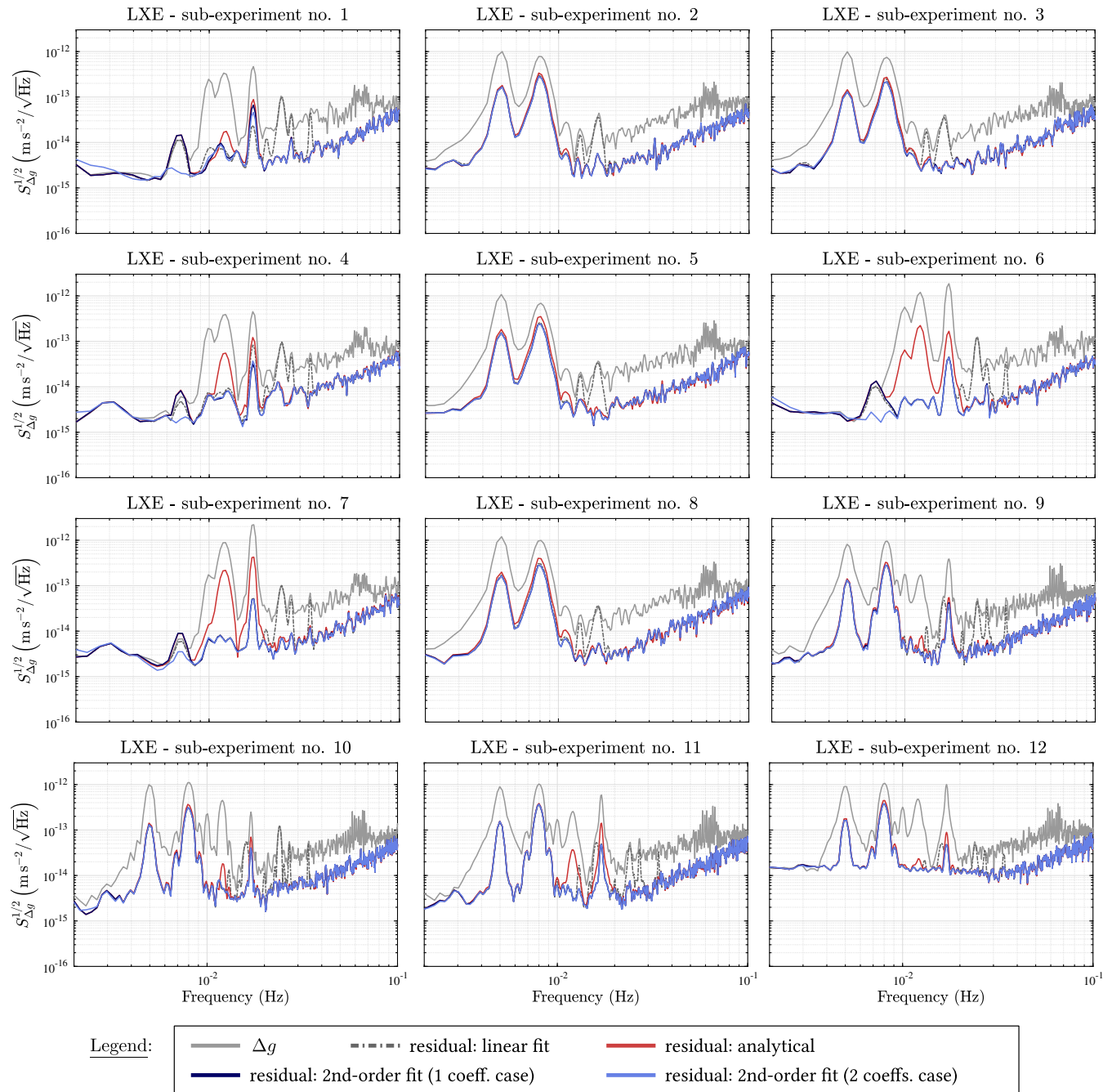


FIG. 10. Residuals after subtracting the second-order models for the twelve subexperiments of the LXE. The continuous gray curve shows the ASD of the observable  $\Delta g$ . The colored curves show the ASD of the residuals after subtracting the second-order models from  $\Delta g$ . Red: second-order analytical model plus the fitted stiffness and  $\sigma_1$  terms. Dark blue: fit model with one additional angular second-order coefficient in each plane. Blue: fit model with two additional angular second-order coefficients in each plane. For comparison, we show the ASD of the residual after subtracting the linear fit model (dashed gray). All three models subtract the peaks at the multiples of the injections frequencies that were not subtracted by the linear models. However, the extensions change very little at the injection better (see 7 mHz peaks).

multiples of, or the differential injection frequencies. These would, for sinusoidal injections, be covered by a higher-order noise model according to trigonometric addition theorems.

When extending the accelerations in  $\varphi$ ,  $\eta$ ,  $y$  and  $z$  to the second-order noise contributions within the fit model, this model would contain ten additional coupling coefficients. The resulting large fit model would be computationally



expensive and largely affected by correlations between the fit quantities.

However, the evaluation of the analytical TTL coupling model [14] has shown that most second-order noise contributors are negligibly small. Based on this analysis, we can reduce the second-order model to

$$\Delta g_{\text{xtalk},2\text{nd}} = \Delta g_{\text{xtalk}} + C_{\varphi 2}[2(\bar{\varphi} \ddot{\varphi} + \dot{\varphi}^2)] + C_{\eta 2}[2(\bar{\eta} \ddot{\eta} + \dot{\eta}^2)]. \quad (5)$$

The two additional second-order coupling coefficients do not depend on the TM alignments. Therefore, they are invariant to the realignments at the beginning of the mission and the TM set-points during the LXE. Moreover, the analytical model derivation shows that these coefficients originate mainly from geometric TTL coupling [7] and are very stable. Therefore, the analytical derivation of these coefficients is assumed to hold for the entire mission duration.

The analytical model yields:

$$C_{\varphi 2}^{\text{ana}} = 0.196_{-0.002}^{+0.001} \frac{\text{m}}{\text{rad}^2}, \quad (6a)$$

$$C_{\eta 2}^{\text{ana}} = 0.193_{-0.002}^{+0.001} \frac{\text{m}}{\text{rad}^2}. \quad (6b)$$

The extended analytical model additionally subtracts the noise peaks at the sums of, but not the differential injection frequencies (e.g., 17 mHz–10 mHz = 7 mHz), see the red residual in Fig. 10.

Next, we fit the TTL coupling using the model Eq. (5) with  $\Delta g_{\text{xtalk}}$  being replaced by Eq. (1). Like in the case of the analytical model, this second-order fit model subtracts the peaks at the sums of the injection frequencies nicely but not at the differential frequencies, see dark blue curve in Fig. 10. Also, the fit yielded second-order TTL coefficients comparable to the analytical results [Eq. (6)]:

$$C_{\varphi 2}^{\text{fit}} = 0.194 \frac{\text{m}}{\text{rad}^2}, \quad (7a)$$

$$C_{\eta 2}^{\text{fit}} = 0.193 \frac{\text{m}}{\text{rad}^2}, \quad (7b)$$

These numbers correspond to the mean of the second-order coefficients in the eight subexperiments with injections in the respective plane. For both coefficients, the root-mean-square of their deviations from this mean is small, i.e., 0.005 m/rad<sup>2</sup>. We neglected the other four fitted coefficients since the higher-order coupling was too small in these cases yielding large error bars.

It is evident that neither the second-order analytical nor the fit model subtract the peaks at the differential frequencies (e.g., visible at 7 mHz in the first subexperiment). We found that these could be covered by a set of two additional

second-order coefficients. Therefore, we fit a coefficient for the two second-order terms in both planes, each, i.e.,

$$\Delta g_{\text{xtalk},2\text{nd}^*}^{\text{fit}} = \Delta g_{\text{xtalk}}^{\text{fit}} + 2C_{\varphi 2A}^{\text{fit}} \bar{\varphi} \ddot{\varphi} + 2C_{\varphi 2B}^{\text{fit}} \dot{\varphi}^2 + 2C_{\eta 2A}^{\text{fit}} \bar{\eta} \ddot{\eta} + 2C_{\eta 2B}^{\text{fit}} \dot{\eta}^2. \quad (8)$$

Subtracting this model from the  $\Delta g$  measurements subtracted additionally the differential peaks, see blue curve in Fig. 10. While, in general, more fit terms could provide a more accurate fit, we see no physical explanation for the extension of the second-order model Eq. (5) to the model Eq. (8).

### E. Extraction of a TTL model from the fit results

So far, we have discussed two TTL coupling models: First, we have introduced the fit model, which successfully subtracts the TTL coupling in noise runs as well as during the LXE but does not provide a physical explanation of the cross-coupling. Second, there is the analytical model, which is the first model explaining how the TTL coupling depends on the system parameters, but its derivation is based on a lengthy analysis. Here, we show that we can build a model that, like the analytical model, describes how the TM alignments change the TTL coupling coefficients and is based only on the LXE data.

We find this system by searching for coefficients that describe the dependency of the fitted coupling coefficients on the set-points best. Mathematically speaking, we compute the coefficients  $k_j^\alpha$  that minimize the systems of equations

$$0 = -C_{ji}^{\text{fit}} + \sum_{\alpha} k_j^\alpha \cdot \alpha_i, \quad i = 1, \dots, 12, \quad (9)$$

where

- (i)  $C_{ji}^{\text{fit}}$ ,  $i = 1, \dots, 12$ , are the coupling coefficients fitted in the bump frequency range for each of the twelve subexperiments of the LXE and for each S/C degree of freedom  $j \in \{\varphi, \eta, y, z\}$ ,
- (ii)  $\alpha \in \{\varphi_1, \varphi_2, \eta_1, \eta_2, y_1, y_2, z_1, z_2, 1\}$  are the TM set-points chosen in each experiment, see Table IV, plus an additional entry accounting for coupling coefficient offsets  $C_{j,0}$ .

Note that we intentionally do not discard any of the  $k_j^\alpha$ 's that are assumed to be negligible based on the analytical modeling. Showing that the minimizing routine also yields small results for these coefficients is a further confirmation of our model Eq. (2).

We ran the LTPDA minimizer ‘‘IscoV’’ (least-squares algorithm) on Eq. (9) for each coefficient yielding



TABLE V. Rounded absolute errors of the coefficients in Eq. (10) found by the minimizing routine.

Term	$C_\varphi$	$C_\eta$	$C_y$	$C_z$
$\varphi_1$	0.02 m/rad <sup>2</sup>	0.00 m/rad <sup>2</sup>	0.01/rad	0.01/rad
$\varphi_2$	0.02 m/rad <sup>2</sup>	0.00 m/rad <sup>2</sup>	0.02/rad	0.02/rad
$\eta_1$	0.04 m/rad <sup>2</sup>	0.01 m/rad <sup>2</sup>	0.02/rad	0.03/rad
$\eta_2$	0.02 m/rad <sup>2</sup>	0.00 m/rad <sup>2</sup>	0.02/rad	0.02/rad
$y_1$	0.01 m/rad	0.00 m/rad	0.01	0.01
$y_2$	0.02 m/rad	0.00 m/rad	0.01	0.02
$z_1$	0.02 m/rad	0.00 m/rad	0.01	0.02
$z_2$	0.03 m/rad	0.01 m/rad	0.02	0.03
1	0.21e-6 m/rad	0.04e-6 m/rad	0.14e-6	0.19e-6

$$C_\varphi^{\min} = \frac{0.15}{\text{rad}^2} \varphi_1 + \frac{0.25}{\text{rad}^2} \varphi_2 + \frac{0.02}{\text{rad}^2} \eta_1 - \frac{0.01}{\text{rad}^2} \eta_2 + \frac{0.03}{\text{rad}} y_1 + \frac{0.02}{\text{rad}} z_1 + \frac{0.01}{\text{rad}} z_2 + \frac{3.21\text{e-}6\text{m}}{\text{rad}}, \quad (10a)$$

$$C_\eta^{\min} = \frac{0.01}{\text{rad}^2} \varphi_1 + \frac{0.01}{\text{rad}^2} \varphi_2 + \frac{0.13}{\text{rad}^2} \eta_1 + \frac{0.19}{\text{rad}^2} \eta_2 - \frac{0.01}{\text{rad}} y_1 - \frac{0.01}{\text{rad}} y_2 - \frac{0.01}{\text{rad}} z_2 - \frac{12.26\text{e-}6\text{m}}{\text{rad}}, \quad (10b)$$

$$C_y^{\min} = -\frac{0.97}{\text{rad}} \varphi_1 + \frac{1.06}{\text{rad}} \varphi_2 + \frac{0.15}{\text{rad}} \eta_1 + \frac{0.01}{\text{rad}} \eta_2 - \frac{0.06}{\text{m}} y_1 + \frac{0.01}{\text{m}} y_2 - \frac{0.13}{\text{m}} z_2 + 5.97\text{e-}6, \quad (10c)$$

$$C_z^{\min} = -\frac{0.02}{\text{rad}} \varphi_1 - \frac{0.06}{\text{rad}} \varphi_2 + \frac{0.97}{\text{rad}} \eta_1 - \frac{1.01}{\text{rad}} \eta_2 + \frac{0.03}{\text{m}} y_2 - \frac{0.04}{\text{m}} z_1 + \frac{0.07}{\text{m}} z_2 + 43.53\text{e-}6. \quad (10d)$$

The absolute errors of the terms in Eq. (9) are given in Table V. We see in Fig. 11 that the coefficients obtained via the minimizing routine agree with the fitted coefficients within their error bars.

The coefficients found via the minimizer [Eq. (10)] show similarities to the corresponding analytically derived coefficients [Eq. (3)]. This is particularly true for the lateral coefficients  $C_y$  and  $C_z$ , which mainly depend on the differential angular TM alignment in the same plane. All factors that scale with other alignment parameters are comparatively small. Also, the angular coefficients  $C_\varphi$  and  $C_\eta$  show the most significant dependency on the same-plane angular TM alignments. Here, the factors scaling this dependency differ for the analytical and the minimizer result by about 25% but show the same characteristic behavior.

We conclude that by varying set-points in a laser interferometric setup, a model showing the dependency of the TTL coupling on the alignment parameters can potentially be found computationally. This is particularly

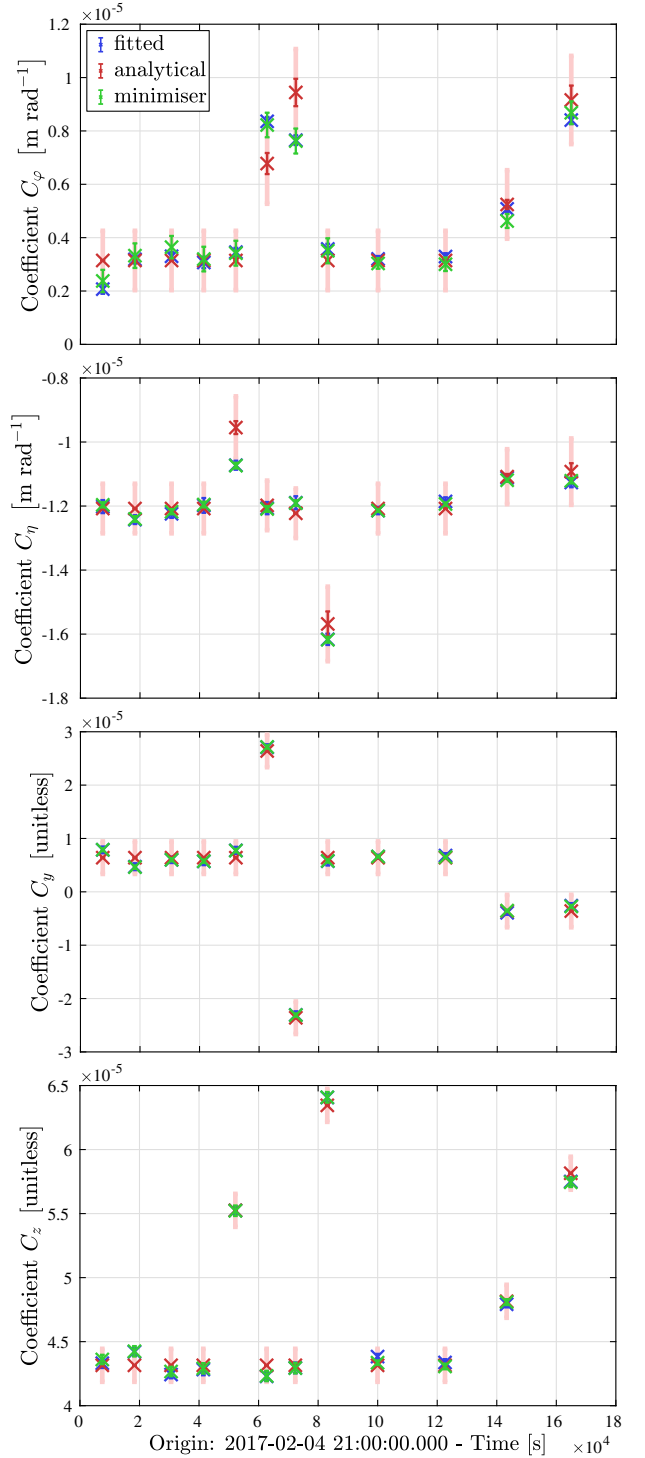


FIG. 11. Comparison of the coefficients derived via the minimizing routine with the fitted (fit range 20 to 70 mHz) and analytically derived coupling coefficients. The minimizer and fit coefficients match well. The coefficient changes due to TM realignments show the same characteristic behavior as analytically predicted with the deviations discussed in Sec. VI B. The time is given in UTC.

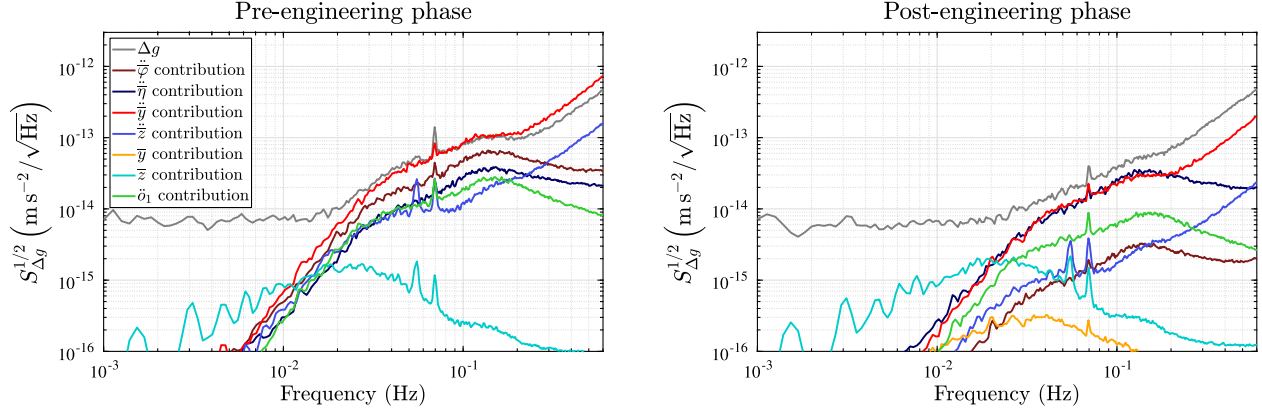


FIG. 12. Noise contributors in the pre- and postengineering phase of the ED. The noise contributions due to accelerations in  $\varphi$ ,  $y$ ,  $z$  and  $o_1$  were reduced due to the realignments. The largest noise contributors after the realignments were the accelerations in  $\eta$  and  $y$ .

interesting in the case of LISA, where the setup is too complex to evaluate a detailed TTL model analytically.

## VII. TEST MASS REALIGNMENTS

After analyzing the LXE in the previous section, we investigate here the three TM realignments introduced in Sec. VA. We show here how the realignments changed the TTL coupling. Also, we show that the observed TTL noise changes can be explained with our new analytical model.

### A. Engineering days

At the beginning of the mission phase, TTL was the largest noise contributor between 20 and 200 mHz. In order to optimize the TM orientations for TTL suppression, injections at different set-points were applied to the TMs during the ED, which took place from the 14th to the 17th of March 2016 [13,35]. Based on these experiments, the TMs were rotated by the angles shown in Table II, which reduced the TTL coupling by a factor of two but did not fully mitigate it [9].

We start here with investigating how the TTL coupling contributors changed due to this first realignment. Therefore, we compare the contributing jitter noise before (*preengineering phase*) and after (*postengineering phase*) the realignments. This is shown in Fig. 12. We see significant differences. Due to the new alignment, the coupling of the accelerations along  $z$  (blue curve) was well suppressed. The same applied to the coupling of the accelerations along  $\varphi$  (brown) and  $o_1$  (green). The main noise contributors after the realignment were the accelerations along  $y$  (red), which was also dominant before and decreased approximately by a factor of three, and  $\eta$  (dark-blue), which was almost not affected by the realignments.

For the preengineering phase, we observe that the  $\ddot{y}$  noise contributor appears to be larger than the measured  $\Delta g$  above 20 mHz (left plot of Fig. 12). However, this noise is not part of the  $\Delta g$  measurement. The GRS measurement of the lateral accelerations at frequencies above 0.2 Hz are

dominated by displacement readout noise [22]. This measurement noise adds up to the true accelerations in  $y$  and  $z$  and is scaled by the corresponding coupling coefficient. Due to the large coupling of the  $y$ -accelerations in the preengineering phase (compare Table VI), the high-frequency behavior of the red curve in the left plot of Fig. 12 is largely affected by this noise. Note that we add this noise to  $\Delta g$  when we subtract the TTL coupling.

For the comparison of the realignment strategy applied during the mission and the predictions of our analytical model [Eq. (2)], we computed the optimal TM alignment angles for cross-coupling suppression with this new model. Therefore, we replaced the  $C_{i,0}$  in Eq. (3) by the fitted coupling coefficients for the preengineering noise (Table VI) and solved Eq. (3) for the TM alignments for which the analytical coefficients  $C_i$  would be zero. By this, we found the angles shown in Table VII. The comparison with the rotations applied during the mission shows a large difference in the case of the angles  $\varphi_2$ ,  $\eta_1$ , and  $\eta_2$ . However, the  $\varphi_1$  angles as well as the differential  $\eta$  angles (considered in the computation of the coupling coefficient  $C_z$ ) are approximately the same. Hence,  $C_z$  was well suppressed (compare Fig. 12).

TABLE VI. TTL coupling coefficients during the pre- and postengineering phase. The first two columns show the fitted coefficients. The last column provides the coefficients computed by the analytical TTL noise model [Eq. (2)] for the post-engineering phase based on the preengineering fit-results. These predictions are close to the fit results.

Coefficients	[unit]	Pre-ED (fit)	Post-ED (fit)	Post-ED (analytical)
$C_\varphi$	[ $\mu\text{m}/\text{rad}$ ]	14.3	-0.7	-1.8
$C_\eta$	[ $\mu\text{m}/\text{rad}$ ]	-7.5	-6.7	-7.5
$C_y$	[ $10^{-6}$ ]	-50.2	-13.6	-12.5
$C_z$	[ $10^{-6}$ ]	7.6	1.1	0.6

TABLE VII. TM realignments for TTL suppression at the time of the ED derived via the analytical model [Eq. (2)] compared to the alignments performed at that time of the mission. These angles largely deviate. Only  $\varphi_1$  and the differential  $\eta$  angle are comparable.

DoF	[unit]	Mission	Analytical
$\varphi_1$	[ $\mu\text{rad}$ ]	-59.25	-60.3
$\varphi_2$	[ $\mu\text{rad}$ ]	-21.35	-10.3
$\eta_1$	[ $\mu\text{rad}$ ]	-3.5	15.8
$\eta_2$	[ $\mu\text{rad}$ ]	3.5	23.4

Next, we reproduced the TTL noise suppression we would have achieved with the analytical results. Since we could not repeat the measurements themselves, we computed the expected residual noise by adding the analytical model to the preengineering measurements. Note that this addition effectively reduces the noise as the analytical model explains how the coupling coefficients would change. For this, we inserted the analytically derived realignment angles into the analytical model (Eq. (3) with  $C_{i,0} = 0$ ) and added it to the preengineering  $\Delta g$ . We then find the residual noise provided by the dashed purple curve in the left-hand side of Fig. 13. It exceeds the noise floor we gain when subtracting the TTL noise via the fit model (1) (yellow curve) between 20 and 90 mHz. This noise almost only originates from the coupling of S/C accelerations along the optical axis ( $o_1$ -term). While we have no model

on hand describing this noise contribution, it showed a decrease when the overall TTL coupling decreases (e.g., Fig. 12). Therefore, we subtract it additionally from the data (together with the small stiffness terms), yielding the solid purple curve at the right-hand side of Fig. 13. This purple curve now coincides with the noise we get when subtracting the TTL coupling via the fit model (1). This shows that we could have achieved the after-fit sensitivity only by a realignment of the TMs in accordance with the new analytically predicted angles. Thereby, the increased noise at higher frequencies was only added due to the addition of the analytical model, which is affected by the GRS sensing noise. This noise increase does not show up when actually performing the realignments of the TMs by the analytically derived angles.

After having demonstrated that we could have suppressed the TTL coupling noise using the new analytically predicted angles (Fig. 13), we confirmed our analytical model further with a second simulation: We reproduced the TTL coupling measured during the postengineering phase using the analytical model. Therefore, we inserted the alignment angles applied during the mission into Eq. (2) (setting the  $C_{i,0} = 0$ ) and add it to the preengineering noise (see Fig. 14). Additionally, we had to subtract the noise from the  $o_1$ -term, which was reduced due to the realignments. As shown at the right-hand side of Fig. 14, we then find the same relative accelerations as measured after the realignments (green curve). This simulation also supports our conclusion that the TM alignments applied during the LPF mission were not ideally chosen. Note that we see, as

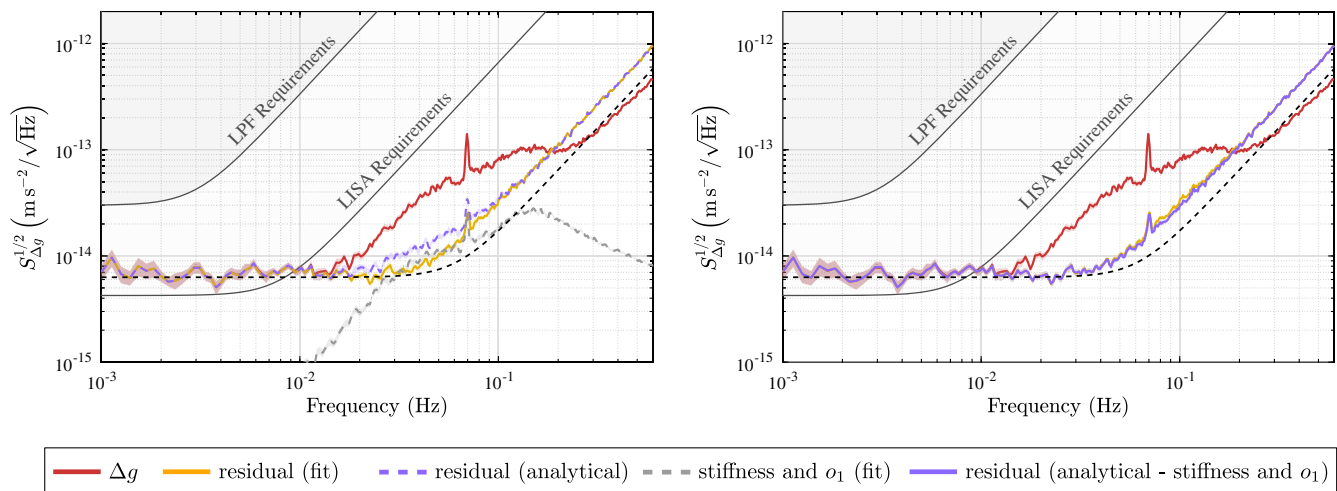


FIG. 13. Analytical modeling of the expected noise after realigning the TMs in accordance to the analytically derived angles (right hand side of Table VII). The results validate the analytical model [Eq. (2)]. Red curves: measured  $\Delta g$  before the realignment (preengineering data). Yellow curve: residual after the subtraction of the fit model [Eq. (1)] from the measured  $\Delta g$  before the realignment. Dashed black line: LPF performance model. Left figure: The analytical model [Eq. (2)] for the analytically derived realignment angles (Table VII) added to the preengineering noise (dashed purple line), and the sum of the fitted stiffness and  $o_1$ -noise contributions (dashed gray line). Right figure: The analytical model added to the preengineering noise minus the fitted stiffness and  $o_1$ -noise contributors (purple line). The overlap of the purple and the yellow curve indicates that a full TTL noise mitigation via realignment could have been achieved via the analytically derived TM angles. The noise added above 200 mHz originates from the measurement noise of the GRS scaled by the TTL coefficients. It would not be present if performing the realignment.

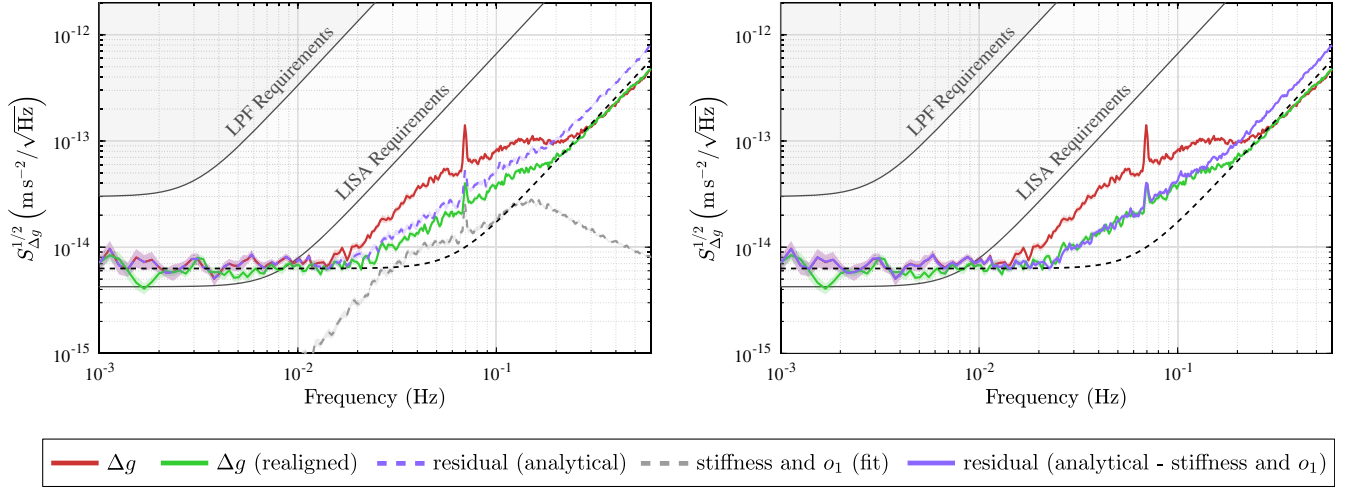


FIG. 14. Analytical modeling of the expected noise after realigning the TMs to the angles defined during the mission (left hand side of Table VII). The results further validate the analytical model [Eq. (2)]. Red curves: measured  $\Delta g$  before realignment. Green curve: measured  $\Delta g$  after the realignments. Dashed black line: LPF performance model. Left figure: The analytical model (2) evaluated for the realignments applied during the engineering days added to the preengineering noise (dashed purple line), and the sum of the fitted stiffness and  $o_1$ -noise contributions (dashed gray line). Right figure: Analytical model added to the preengineering noise minus the fitted stiffness and  $o_1$ -noise contributors (purple line). The overlap of the purple and the green curve indicates that the observed noise decrease due to the commanded realignment could have been predicted with the analytical model. In comparison to Fig. 13 we see that not the realignment angles defined during the mission but the new analytically derived ones would have yielded a suppression of TTL noise.

in Fig. 13, a noise increase at high frequencies due to the measurement noise included in the analytical model. Again, this is only an artefact of the modeling and would not occur in case of an actual realignment.

## B. TM realignments in June 2016

Since the TM realignments during the ED did not fully mitigate the TTL coupling, the realignment angles were corrected on 19th and 25th June 2016 to the angles shown in Table II. Like in the previous subsection concerning the realignment during the engineering days, we investigate here effect of these new alignments using the fit results and our analytical predictions. We first analyze the changes of the TTL noise contributors due to the realignments (Sec. VII B 2). Furthermore, we directly compare the angular realignments set in June 2016 with the analytically computed alignment angles (Sec. VII B 3) as well as the fitted and the analytically derived coupling coefficients (Sec. VII B 4).

### 1. Investigated timespans

For the computation of the TTL coefficients and the therefrom derived noise contributors, we considered the noise runs closest to the TM realignment times (Table II). The chosen noise runs all either ended about a day before or started about a day after the investigated realignment.

We could not use the result from the postengineering phase for the analysis of the first realignment in June 2016 since the coupling coefficients were found to drift for long timespans. This is further investigated in [34].

The noise run before the realignment on 19th June started on 15th June at 1:30 PM and lasted until 18th June at 8 AM UTC. Although no TM realignments were performed between this noise run and the postengineering phase, we found that the noise contributors changed in the meantime (compare Figs. 12 and 15, which is further discussed in the following subsection). These changes are most likely related to relaxations in the optical system [27]. A more detailed discussion can be found in [34].

Our analysis of the effect of the first TM realignment relies further on the noise run starting on 20th June at

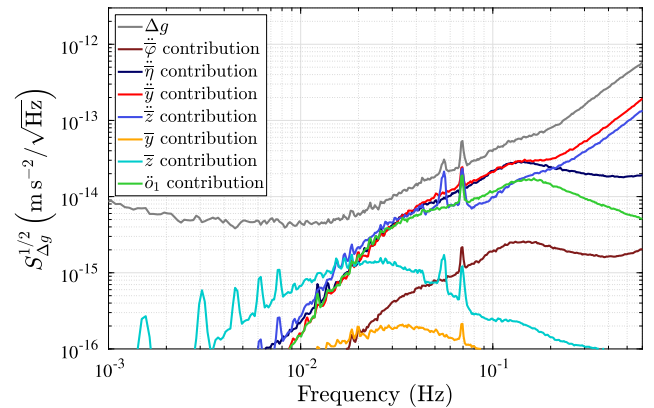


FIG. 15. Noise contributors during the noise run prior to the TM realignments in June 2016. The noise run started on 15th June and lasted almost three days until 18th June 2016. The coupling of the acceleration in  $y$  and  $\eta$  was the main cause of the TTL bump between 20 and 200 mHz.



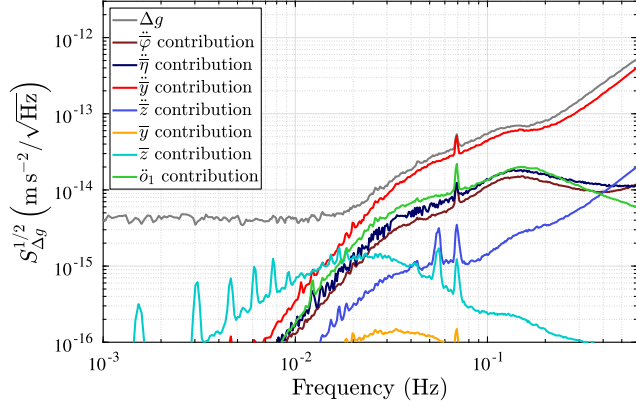


FIG. 16. Noise contributors during the noise run in between the two TM realignments in June 2016. It started a day after the realignment performed on 19th June 2016 and lasted for four days. In comparison to Fig. 15, we see a decrease of the  $\eta$ - and  $z$ -acceleration coupling but an increase of the  $\varphi$ - and  $y$ -acceleration noise. The overall TTL noise increased between 20 and 200 mHz.

8 AM, i.e. subsequent to the realignment. This noise run lasted until 8 AM at the day before the second and last alignment in June 2016.

Unfortunately, there was no dedicated noise run for the investigation of the effect of this last TM realignment. The earliest following noise run took place two weeks later during the disturbance reduction system (DRS) operations, and the measurements were additionally affected by temporary temperature increases [36]. As we show in [34], these also changed the coupling coefficients such that the data is not suited for testing how the realignment affected the TTL coupling noise. Therefore, we show here instead the results derived for a time segment of one hour (7:00–08:00 AM on 26th June 2016) shortly after the realignments, having low noise.

## 2. Noise contributor changes due to the realignments

In this subsection, we analyze the effect of the TM realignments performed in June 2016 on the TTL noise contributors. We start with comparing the noise contributions prior to the realignments (Fig. 15) with the noise contributors after the realignment on 19th June (Fig. 16). As can be seen in these figures, the noise due to the  $\varphi$ - and  $y$ -accelerations significantly increased while the coupling of the  $z$ -accelerations decreased. This increase was due to a sign error in the application of the changes. In total, it yielded larger TTL coupling noise (bump of the gray curve between 20 and 200 mHz). The ASD increased by almost 50% in this frequency regime.

Consequently, the TMs realignments were inverted on 25th June 2016. This led to a mitigation of the  $\varphi$ - and  $y$ -acceleration coupling but unfortunately increased the noise in the orthogonal plane again, i.e., mostly the  $z$ -acceleration coupling, see Fig. 17.

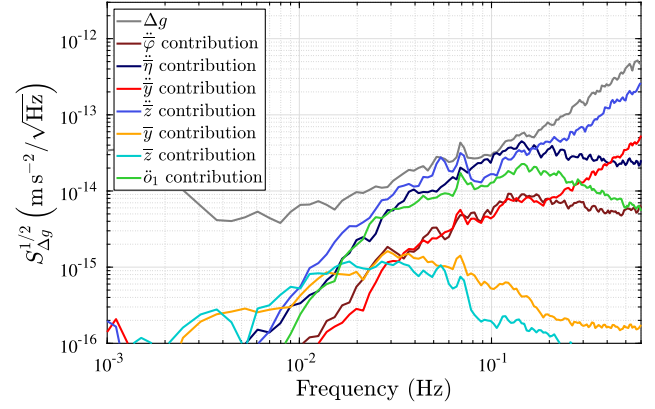


FIG. 17. Noise contributors after the realignment on 25th June 2016. Considered are data from 26th June 2016 from 7:00 to 8:00 AM UTC. Due to this realignment, the  $\varphi$ - and  $y$ -acceleration noise decreased, but the  $\eta$ - and  $z$ -acceleration coupling increased again. In sum, the TTL bump is smaller than before this realignment.

Imagining a TM alignment corresponding to the final  $\varphi$ -angles but the  $\eta$ -angle after the first June alignment, the full TTL coupling noise would have been smaller than for each of the applied alignment settings (combine the brown/red curves in Fig. 17 and blue curves in Fig. 16). From this observation, we conclude that an almost complete TTL suppression via realignment could have been achieved during the mission if the TMs would not have been realigned in  $\eta$  on 25th June 2016.

## 3. Comparison of the angular realignments set during the mission and derived analytically

Since the cross-coupling of the  $z$ -accelerations into the  $\Delta g$  readout increased in between the ED and the realignments in June 2016 (see Figs. 12 and 15), the differential  $\eta$  angle must have increased, too. Therefore, the analytically derived TM alignment angles shown in Table VII are outdated. We rederived these TM realignment angles. Analogously to before, we computed by Eq. (3) the TM alignments needed to counteract the fitted TTL coefficients for the noise run prior to the realignments. This computation took the coupling coefficients into account, that were

TABLE VIII. Comparison of the TM realignment angles set in June 2016 for TTL suppression with the alignment angles derived analytically based on the TTL coupling during the noise run before both alignments (15.06. 13:30 until 18.06. 8:00). Times are given in UTC.

DoF	[unit]	19.06. 8:20	25.06. 8:00	Analytical
$\varphi_1$	[ $\mu$ rad]	-56.32	-61.2	-63.75
$\varphi_2$	[ $\mu$ rad]	-33.01	-9.7	-13.05
$\eta_1$	[ $\mu$ rad]	-2.14	-4.9	8.3
$\eta_2$	[ $\mu$ rad]	10.3	-3.3	21.6

fitted to the prior noise run with TM rotation angles as set during the ED. Therefore, these angles are then added to these previous TM alignments. The sum yields the total realignment angles, respectively. The result is shown in the right column of Table VIII.

The differential analytical  $\eta$ -angle ( $\eta_1 - \eta_2$ ) differs less than  $1 \mu\text{rad}$  from the differential  $\eta$ -angle after the first realignment in June 2016 (cf.  $\eta_1 - \eta_2$  in the first and third value columns of Table VIII). Due to this realignment, the  $z$ -acceleration noise was well suppressed [cf. Fig. 16 and Eq. (3d)]. Likewise, the differential  $\varphi$ -angles ( $\varphi_2 - \varphi_1$ ) derived analytically and set on 25th June during the mission differ by less than  $1 \mu\text{rad}$ . Correspondingly, the  $y$ -acceleration noise contribution was well suppressed [cf. Fig. 17 and Eq. (3c)].

However, the individual analytical angles significantly differed from the ones set during the mission. E.g., the analytically derived  $\eta$ -angles are both approximately  $10 \mu\text{rad}$  larger than the angles set on 19th June. This difference increased even further after the last TM realignment. Consequently, the S/C-jitter coupling in  $\eta$  was not well suppressed after both realignments [see Figs. 16 and 17, compare with Eq. (3b)], which supports our analytical result. The  $\varphi$ -angles after the last TM alignment differ by about  $3 \mu\text{rad}$  from the corresponding analytical computations. By Eq. (3a), a small decrease of the  $\varphi$ -acceleration noise would have been possible by an adaption of these alignment angles. However, the  $\varphi$ -acceleration noise was already low due to the chosen alignment angles.

#### 4. Comparison of the fitted and the analytical coupling coefficients

For further confirmation of the analytical TTL model [Eq. (2)], we compare the coupling coefficients fitted after the TM realignments with their analytical prediction. The latter was derived by replacing the constant coefficient offsets  $C_{i,0}$  in Eq. (3) by the fitted coupling coefficients computed for the time before the realignments. Moreover, the TM alignment angles in Eq. (3) were substituted by the angles in Table II.

Instead of plotting the resulting noise reduction by the analytical model as shown in Fig. 14, we compare here the coupling coefficients directly. If both are close to each other, the TTL reduction during the mission and the analytical prediction would agree.

Both, the fitted and the analytically derived coupling coefficients, are summarized in Table IX. In the first column, we show the result for the noise run prior to the realignments. Here, only the fitted coefficients are given. The two following columns contain the computations for the noise run between the June realignments and the timespan of one hour after the last TM realignment. The analytical coefficients show how the coefficients are expected to change due to the TM rotations with respect to the fitted coefficients before the corresponding realignment.

TABLE IX. Comparison of the fitted (left) and analytically computed (right) cross-coupling coefficients for timespans prior, in between and after the TM realignments in June 2016 (Table II). The analytical coefficients were computed via the Eqs. (3), where the constant offsets of the coefficients were substituted by the respective fitted coefficient prior to these realignments (first column) and the angular TM alignment changes due to the realignments were inserted for the TM angles. Times are given in UTC.

Start time	TTL coefficients [fitted   analytical]		
	15.06. 13:30	20.06. 08:00	26.06. 07:00
End time	18.06. 08:00	24.06. 08:00	26.06. 08:00
$C_\varphi$ [ $\mu\text{m}/\text{rad}$ ]	-0.6 -	-3.3 -2.1	1.9 1.2
$C_\eta$ [ $\mu\text{m}/\text{rad}$ ]	-5.7 -	-3.5 -4.2	-7.5 -7.2
$C_y$ [ $10^{-6}$ ]	-12.8 -	-27.7 -27.5	3.3 0.7
$C_z$ [ $10^{-6}$ ]	6.4 -	0.9 0.9	11.8 11.8

The deviation between both sets of coefficients is in general small. The largest deviation occurs for the  $C_y$  coefficients computed for the one-hour timespan after the last realignment. However, also this deviation would lie within the variations observed for the fitted  $C_y$  coefficients during the noise run after the LXE (Table I). Although this noise run took place several months after the realignments, the  $C_y$ -coefficient has not changed much. Therefore, we assume the deviations to be applicable here.

In conclusion, the analytical model predicts within the 95% confidence interval the correct TTL noise coupling reduction due to the applied TM realignments. Thus, we expect that a TTL coupling suppression down to the fundamental noise limit would have been possible using the analytically computed alignment angles in Table VIII.

## VIII. SUMMARY

In this work, we presented an extensive analysis of the TTL coupling in LPF with focus on the LXE and the TTL coupling reduction by realignment. We described the coupling dependencies on the test mass alignment parameters. This has been done using two different TTL coupling models.

The analytical model we presented is the first TTL model successfully explaining the dependency of the TTL coupling into the  $\Delta g$  measurement on the TM alignment angles. Using this model, we have shown why the applied TM realignments failed to fully mitigate TTL coupling and derived alignment angles, which could have suppressed the TTL coupling *a priori*. This would have made the subtraction of the coupling in post-processing redundant (as long as the coefficients do not change over long timescales).

While the linear fit model used during the mission was sufficient for TTL subtraction in noise runs, we find higher-order noise peaks in experiments with injected TTL

noise. The analytical analysis has shown that the models can be easily extended to second-order models, adding only two additional coupling terms. Also, the additional coupling terms are stable and therefore need only to be computed once and can then be applied during the entire mission duration.

The derivation of the analytical model for LPF was complex and time-consuming. Within this work, we have introduced an alternative computation of an alignment-dependent model. By evaluating the relation of the fitted coupling coefficients for the twelve subexperiments on the corresponding TM alignment, a model equivalent to the analytical model was found. Such a procedure can also be applied in future missions like LISA, yielding the physical dependency of the measured TTL coupling on certain alignment parameters. Mind that the larger number of jittering components in LISA would also make a higher number of subexperiments with different realignments each necessary. However, from the analysis of the TTL coefficient changes due to the TM realignments in March and June 2016 using noise run data, we deduce that the injections applied during the LXE would not have been necessary for the fit of the changing coupling coefficients. Hence, a comparable calibration scheme in LISA does not necessarily interrupt the scientific measurements.

In conclusion, we have now understood the TTL coupling in LPF to a large extent. This drives our confidence that the TTL suppression strategies planned for future missions will be successful.

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