



RESEARCH ARTICLE

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Key Points:

- We investigate and upscale the physical and transport properties of an exceptionally exposed carbonate-bearing normal fault in central Italy
- Physical and transport properties of the investigated fault zone are controlled by the protolith and the different deformation processes
- Laboratory physical and mechanical data are in good agreement with in situ measurements and well-match seismological data

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## Physical and Transport Property Variations Within Carbonate-Bearing Fault Zones: Insights From the Monte Maggio Fault (Central Italy)

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**Abstract** The physical characterization of carbonate-bearing normal faults is fundamental for resource development and seismic hazard. Here we report laboratory measurements of density, porosity,  $V_p$ ,  $V_s$ , elastic moduli, and permeability for a range of effective confining pressures (0.1–100 MPa), conducted on samples representing different structural domains of a carbonate-bearing fault. We find a reduction in porosity from the fault breccia (11.7% total and 6.2% connected) to the main fault plane (9% total and 3.5% connected), with both domains showing higher porosity compared to the protolith (6.8% total and 1.1% connected). With increasing confining pressure,  $P$  wave velocity evolves from 4.5 to 5.9 km/s in the fault breccia, is constant at 5.9 km/s approaching the fault plane and is low (4.9 km/s) in clay-rich fault domains. We find that while the fault breccia shows pressure sensitive behavior (a reduction in permeability from  $2 \times 10^{-16}$  to  $2 \times 10^{-17}$  m<sup>2</sup>), the cemented cataclaste close to the fault plane is characterized by pressure-independent behavior (permeability  $4 \times 10^{-17}$  m<sup>2</sup>). Our results indicate that the deformation processes occurring within the different fault structural domains influence the physical and transport properties of the fault zone. In situ  $V_p$  profiles match well the laboratory measurements demonstrating that laboratory data are valuable for implications at larger scale. Combining the experimental values of elastic moduli and frictional properties it results that at shallow crustal levels,  $M \leq 1$  earthquakes are less favored, in agreement with earthquake-depth distribution during the L’Aquila 2009 seismic sequence that occurred on carbonates.

### 1. Introduction

Fault rocks and related properties such as permeability, frictional behavior, fluid content, and lithology exert a significant control on fault structure (Cowie & Scholz, 1992; Faulkner et al., 2010; and others), earthquake rupture nucleation, propagation and arrest (Ben-Zion & Sammis, 2003; Boatwright & Cocco, 1996), fluid flow (Caine, 1996; Evans et al., 1997; Mitchell & Faulkner, 2012), and variations in the stress field around brittle crustal faults (Faulkner et al., 2006). Fault structure is generally represented by one or more high strain slip zones (the fault core) surrounded by a highly heterogeneous region characterized by fracture sets, secondary faults, joints, and veins (damage zone). The intensity of deformation in the damage zone decays away from the fault into relatively undeformed host rocks (Caine, 1996; Chester & Logan, 1986; Faulkner et al., 2010; Savage & Brodsky, 2011). The described fault zone architecture has mainly been reconstructed from field examples of faults cutting across crystalline basement rocks (e.g., Chester & Logan, 1986; Mitchell & Faulkner, 2009). However, within fault zones crosscutting sedimentary rocks, the mechanical properties are significantly influenced by sedimentary facies, with different mineralogical characteristics that primarily affect grain size, grain distribution, and porosity (Hugman & Friedman, 1979; Riley et al., 2010; Shipton et al., 2006). Nonetheless, at first approximation, the typical fault zone structure where slip localizes along a fault core with distributed deformation in the damage zone, has also been documented also for carbonate-bearing faults (e.g., Agosta & Kirschner, 2003; Billi et al., 2003; Collettini et al., 2014a; Demurtas et al., 2016; Ferrill et al., 2011; Fondriest et al., 2012; Micarelli et al., 2006) with some notable differences highlighted in the width and in the mechanical processes acting on the damage zones (De Paola et al., 2008; Ferrill et al., 2011; Micarelli et al., 2006).

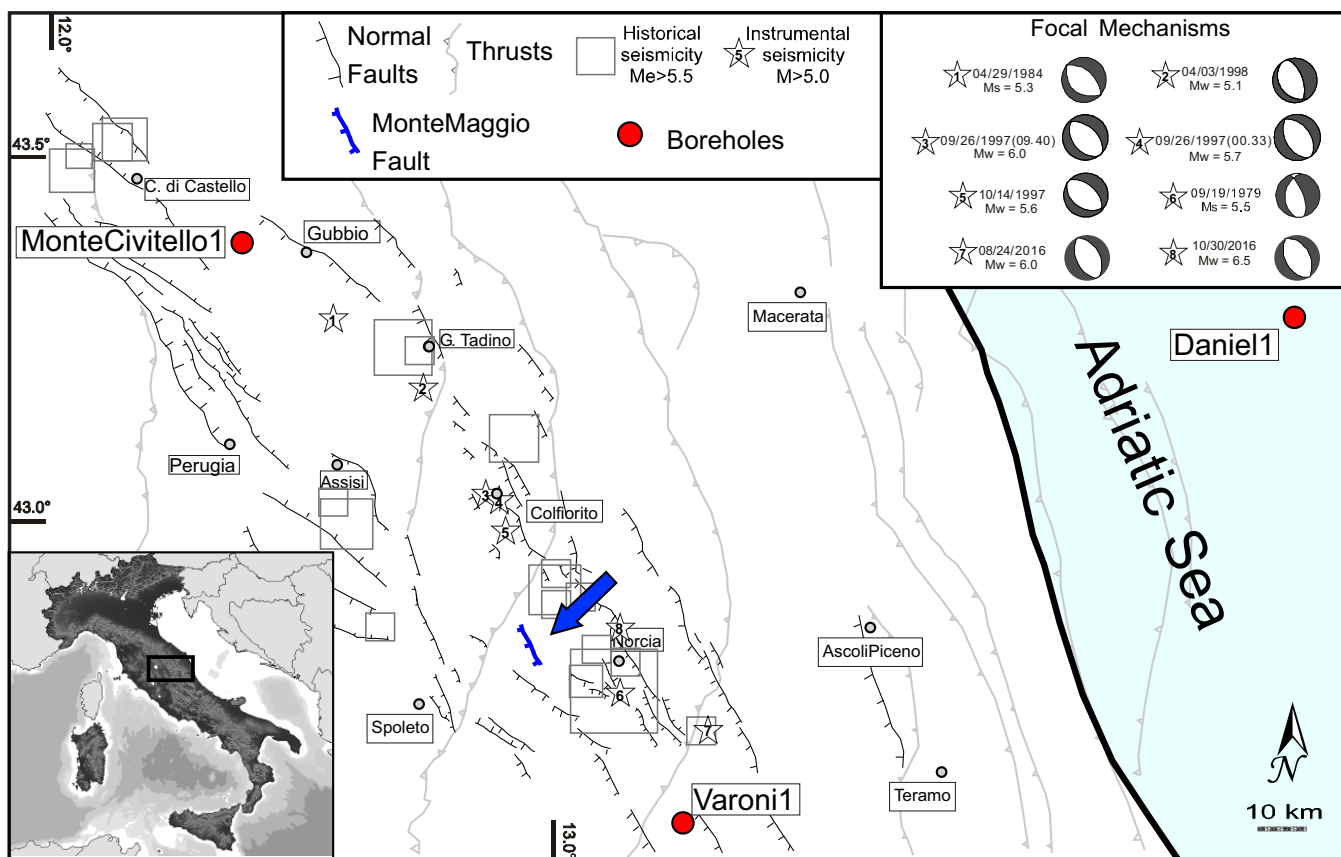
Carbonate-bearing faults represent important structures for numerous reasons, including: (1) faulted and fractured carbonate reservoirs contain approximately two thirds of the world’s oil and gas reserves (Al-Anzi

et al., 2003), and (2) significant earthquakes, both natural (i.e., Miller et al., 2004) or human-induced (i.e., Improta et al., 2015) nucleate and/or propagate through thick sequences of carbonates that dominate upper-crustal sedimentary sequences (Burchfiel et al., 2008; Chiaraluze, 2012; Govoni et al., 2014; Nissen et al., 2014; Mirabella et al., 2008). For these reasons, the characterization of carbonate-bearing faults is fundamental to improve our understanding of reservoir characterization and seismic risk in active tectonic areas. In particular, the transport and mechanical properties of carbonate-bearing faults at crustal conditions have received increased attention (e.g., Agosta, 2008; Baud et al., 2009; Bussolotto et al., 2015; Michie, 2015; Michie & Haines, 2016; Rath et al., 2011) together with the characterization of the frictional properties (e.g., Carpenter et al., 2014, 2016; De Paola et al., 2015; Scuderi et al., 2016; Smith et al., 2013; Tesei et al., 2014; Violay et al., 2013; Verberne et al., 2010, 2014, 2015).

In this work, we investigate the physical properties of carbonate samples collected along the Monte Maggio Normal Fault (MMNF), a regional-scale normal fault zone located in the active extensional system of the Northern Apennines (Italy). We developed laboratory experiments to characterize the petrophysical properties of the different domains identified across the fault zone. Results are discussed to (1) infer the evolution of the fault physical properties during deformation; (2) compare laboratory determinations of  $V_p$  with field measurements; and (3) provide further constraints for earthquake nucleation on carbonate-bearing faults.

## 2. Field Study Area—The Monte Maggio Normal Fault

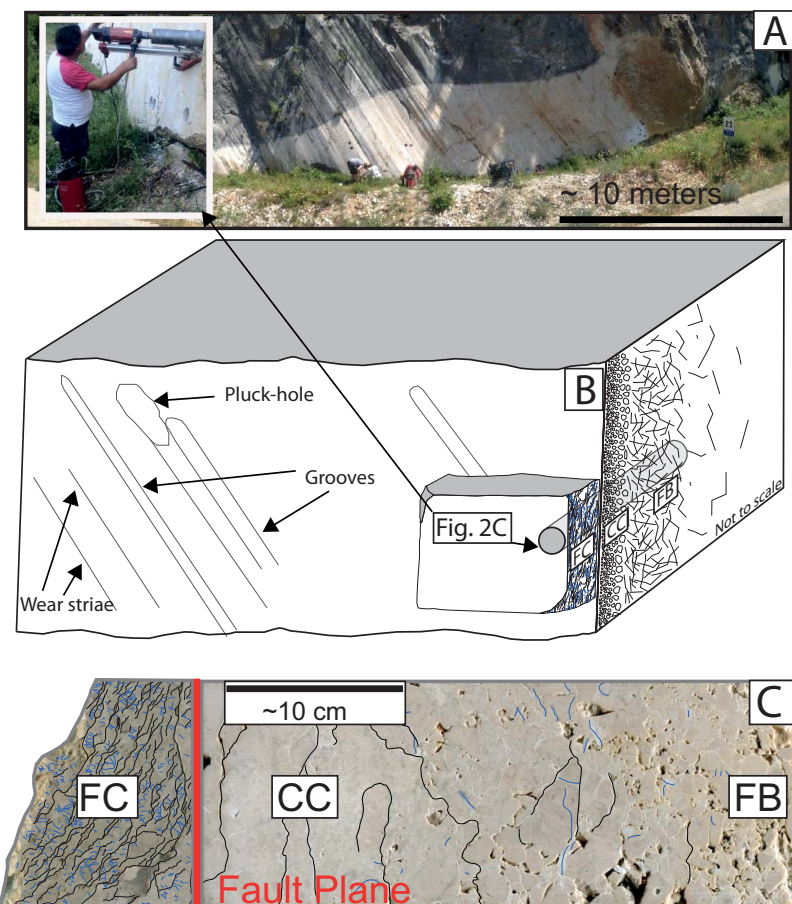
The study area (Figure 1) is located within the Northern Apennines (Italy), a thrust-and-fold belt resulting from the convergence between the Alpine orogen and the continental lithosphere of the African plate (e.g., Doglioni et al., 1998, and references therein). While convergence is still active beneath the Po River plain and along the Adriatic coast (Anderlini et al., 2016; Frepoli & Amato, 1997), extensional tectonics have



**Figure 1.** Simplified map of the Umbria–Marche Apennines of central Italy, with locations of the Monte Maggio Fault and of the boreholes analyzed for the comparison of measured  $V_p$  in Laboratory (modified after Lavecchia et al., 1994; Colletini et al., 2014b).

characterized the axial zone of the Northern Apennines since the upper Pliocene (Barchi et al., 1998; Collettini et al., 2006). The resulting extension is mainly accommodated by high-angle W-dipping normal faults, which are responsible for the major earthquakes of the area (e.g., Boncio & Lavecchia, 2000; Chiarabba et al., 2009; Chiaraluca et al., 2005, 2017; Collettini et al., 2003).

The Monte Maggio Normal Fault (MMNF) is a spectacularly exposed (Figure 2a), high-angle W-dipping normal fault outcropping near the town of Spoleto (central Italy). The MMNF is located in an area where regional uplift and erosion override sedimentation, therefore Quaternary basin filling sediments in the hanging-wall are absent. Slip on the fault results in the juxtaposition of carbonate formations of the Umbria-Marche sequence. We thus interpret the MMNF as an exhumed analogue of the active structures that, in the same area, are responsible for the recorded seismicity like the 1997 Colfiorito ( $M_w = 6.0$ ), the 2009 ( $M_w = 6.3$ ) L'Aquila and the 2016 Amatrice ( $M_w = 6.0$ ) and Norcia ( $M_w = 6.5$ ) earthquakes (Amato et al., 1998; Chiarabba et al., 2009; Chiaraluca et al., 2005, 2017; Mirabella et al., 2008; Tinti et al., 2016). The fault extends for a length of 10 km consisting of five subparallel segments with a maximum distance between overlapping fault segments of about 1.5 km. The maximum displacement (370–650 m) of each fault segment is partitioned along subparallel slipping zones extending for a total width of about 50 m (Collettini et al., 2014a). These slipping zones, developed within the calcareo massiccio formation, are characterized by a prominent slip surface with different slip surface phenomena, including pluck-holes, grooves,



**Figure 2.** (a) Outcrop picture of the Monte Maggio Normal Fault and coring method (top left inset). (b) Schematic illustration of fault architecture. The slip surface shows grooves and striations at different scales. Fault plane juxtaposes a foliated cataclasite and a very thin ultracataclasite rock where this latter results from the comminution of a thicker cemented cataclastic layer. The cemented cataclasite evolves in a fault breccia with an exponential decrease in damage into the protolith. (c) Slabbed core, drilled perpendicular through the fault zone (from Collettini et al., 2014). The foliated cataclasite (FC) shows hydrofractures and pressure solution seams. The footwall block is mainly characterized by 2–10 cm thick cemented cataclasite (CC) and by a thicker (up to few meters) highly fractured fault breccia (FB) shading into the protolith.

wear striae, circular cracks, and comb fractures (Collettini et al., 2014a; Tesi et al., 2017) as shown in Figures 2a and 2b.

In the hanging-wall block, fault rock derived from a calcareous-marly protolith (91.7% carbonate and 8.3% clay), is represented by a carbonate-rich foliated cataclasite (Figure 2c, left), where clay-rich pressure solution seams (stylolites) and calcite-rich veins with mutual crosscutting relationships are observed. These structural features indicate that during fault activity, deformation processes such as cataclasis, pressure solution, and hydrofracturing with cementation were active in the slip zone of the hanging-wall block (Collettini et al., 2014a).

Moving away from the slip surface, the footwall block is characterized by a thin zone, <2 cm, of ultracataclasite (see Carpenter et al., 2014, and Collettini et al., 2014a, for details) followed by a 2–10 cm thick cataclastic layer and fault breccia (Figure 2c). Both the ultracataclasite and cataclasite form from the CM formation. The cataclasite layer has a thickness ranging from a few centimeters to about 10 cm and is characterized by a fine-grained texture with a few principal slip surfaces and calcite veins. One prominent feature of this layer is its strong cohesion, likely related to cementation processes (healing and sealing) that occurred within the fault zone. Fault breccia (Figure 2c, right) is represented by clasts of calcareo massiccio separated by visible open fractures, calcite-rich veins and limited pressure solution seams with fractures that often reopen pre-existing calcite-filled cracks. A characteristic of fault breccia is larger clast dimensions in comparison to the cataclasite and ultracataclasite layers. In some portions of the slip zone, Collettini et al. (2014a, 2014b) documented small displacement (<1 cm) fault planes both synthetic and antithetic to the major slip surface that merge into it.

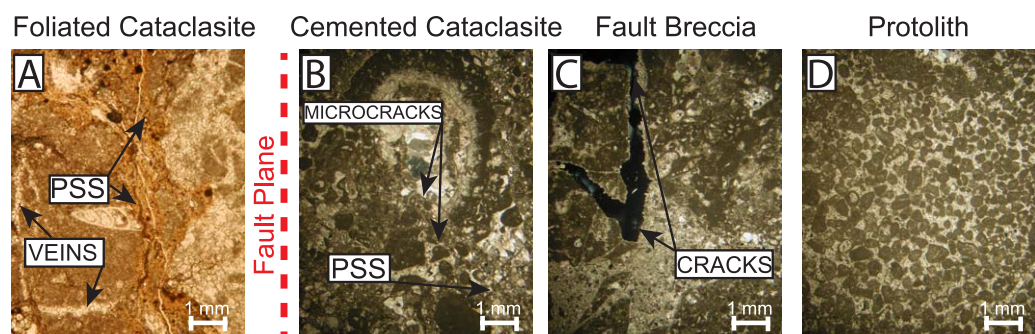
### 2.1. Investigated Samples

We collected large cores (100 mm in diameter and up to 20 cm in length), drilled perpendicular to the fault plane (Figures 2b and 2c). These cores were then subsampled to obtain smaller cores (38 mm in diameter and 38 mm in length). Following the fault zone architecture described above, we classified the fault rock samples as: foliated cataclasite (FC in Figure 2c) that represents the clay-rich domain of the fault core, cemented cataclasite (CC in Figure 2c) or the carbonate-rich fault core, and fault breccia (FB in Figure 2c) or the damage zone. For comparison, we also collected samples from the protolith (P).

Optical microscope analyses of the clay-rich domain displays a cataclasite with abundant pressure solution surfaces and calcite-rich veins, in agreement with mesoscale observations. Microcracks are also present with orientations that seem to follow both grain boundaries and pressure solutions seams (Figure 3a).

The cemented cataclasite consists of randomly oriented, subcentimetric angular clasts of calcareo massiccio formation, dispersed within a fine-grained calcite-rich ground mass (Figure 3b). Microcracks between clasts are abundant whilst very few open cracks and pressure solution seams are present.

The footwall fault breccia shows a high variability of clast dimensions ranging from a few microns to some centimeters. Open cracks that often reopen preexisting calcite-filled cracks are the prominent features of this portion of the fault footwall block (Figure 3c).

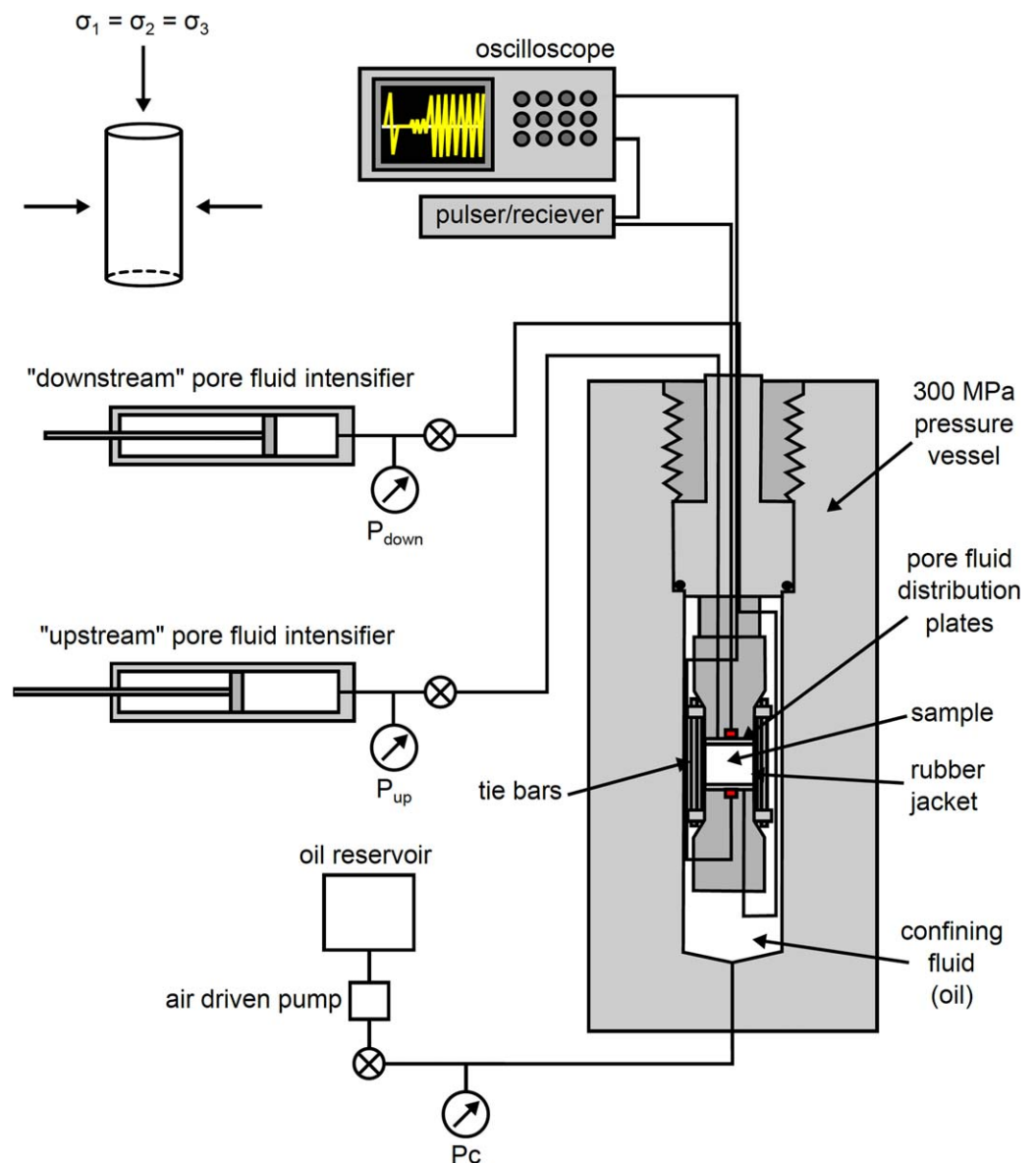


**Figure 3.** Representative microstructures of the test samples from thin sections: (a) Foliated and clay-rich cataclasite located in the hanging-wall of the fault plane with abundant calcite-filled veins, and pressure solution surfaces (bottom inset). (b) Cemented cataclasite with submillimeter-scale clasts and abundant microcracks. (c) Fault breccia showing clasts with variable dimensions, and abundant open cracks. (d) Protolith (calcareo massiccio limestone) showing the undeformed classical oolitic grainstone texture.

The protolith shows the typical oolitic grainstone microscopic textures of the calcareo massiccio limestone (e.g., Santantonio, 1994). At the microscale, this tight limestone is characterized by the absence of cracks, microcracks, and pores (Figure 3d).

### 3. Experimental Methodology

We tested 16 cylindrical core samples representative of the main structural domains of the fault (Figure 2), i.e., clay-rich foliated cataclasite (FC), cemented carbonate-bearing cataclasite (CC), fault breccia (FB), and the protolith (P). For all the samples, we measured density, porosity, and  $P$  and  $S$  wave velocity at ambient pressure under dry conditions. Seismic wave velocities were also measured at effective confining pressures ranging up to 100 MPa. All experiments were performed at the HP-HT Laboratory of Experimental Volcanology and Geophysics of the Istituto Nazionale di Geofisica e Vulcanologia in Rome (Italy). Samples consist of



**Figure 4.** Schematic diagram (from Heap et al., 2014b) of the servo-controlled permeameter equipped for measurements of  $V_p$ ,  $V_s$  and permeability up to confining pressures of 100 MPa at the High Pressure High Temperature (HPHT) Laboratory, Istituto Nazionale di Geofisica e Vulcanologia (INGV), Rome. The sample size is 38 mm in diameter and 38 mm in length.

cylinders, 38 mm in diameter and 38 mm long, with their end faces ground flat and parallel to  $\pm 0.02$  mm. Density measurements were performed on samples that had been dried in an oven at 60°C for a minimum of 24 h. This modest temperature is used to preclude any possibility of thermal cracking in the samples prior to measurement (Fredrich & Wong, 1986; Glover et al., 1995). The porosity for each sample was measured using a helium pycnometer (AccuPyc II 1340) with an analytical accuracy of  $\pm 0.001\%$ . Initial elastic wave velocity measurements were made axially on dry samples under ambient laboratory conditions using the pulse transmission technique (Birch, 1960, 1961). A 900 V pulse generator was used to excite a 1 MHz resonant frequency piezo-electric transmitting transducer, and the resulting waveforms were recorded using an identical receiving transducer. After preamplification, signals were recorded and displayed on a digital storage oscilloscope.

Experiments under fluid-saturated conditions were performed using a standard permeameter (Figure 4) that is equipped with three servo-controlled pressure intensifiers used to apply a confining pressure ( $P_c$ ), up to 100 MPa, and an upstream and downstream pore fluid pressure (maximum pressure 70 MPa). Confining pressure is applied using a hydrogenated paraffinic oil. For pore fluid, we used a calcium-rich water solution similar to the water circulating in carbonate-bearing faults. For the configuration of the testing apparatus, the confining pressure is applied isotropically to the sample (i.e.,  $\sigma_1 = \sigma_2 = \sigma_3$ ) and the effective stress results from  $\sigma_{\text{eff}} = P_c - P_f$ , where  $P_f$  is the fluid pressure. The sample assembly consists of two end-caps that sandwich the cylindrical core sample. Each end-cap is equipped with two 1 MHz resonant frequency piezo-electric transducers crystal, one for compressional ( $V_p$ ) and one for shear ( $V_s$ ) wave velocity measurements. During each experiment, we increased the effective pressure in steps of 10 MPa, under hydrostatic boundary conditions, until a maximum effective pressure of 100 MPa. For each pressure step, we measured axial  $P$  and  $S$  wave velocity and sample permeability. The accuracy of the  $P$  and  $S$  wave velocity is estimated as 1–2% for  $V_p$  and 2–4% for  $V_s$ . Sample permeability was measured by applying a constant head method that consist in applying a differential fluid pressure between the upstream and downstream reservoir (2 MPa for all measurements reported here) and measure the resulting flow rate. We subsequently determined sample permeability from the measured flow rates and the sample dimensions, by direct application of Darcy's law.

## 4. Results

### 4.1. Measurements at Ambient Pressure

In this section, we report results from measurements of bulk density, porosity, and axial  $P$  wave velocity made at ambient pressure (0.1 MPa): these results are listed in Table 1.

By averaging the values of each fault rock type (Table 1, bold) it results that the protolith,  $P$ , has an average porosity of 6.8%, formed predominantly by isolated pores since the connected porosity is only 1.1%. These values are in good agreement with microstructural observations and previous measurements on similar tight limestones (e.g., Agosta et al., 2007; Mavko et al., 2009). FB samples are characterized by the highest bulk porosity (11.7%) and a resulting connected porosity of 6.2%, whilst CC samples show lower bulk porosity (9.0%) and a connected porosity of 3.5%. It is worth noting that FB samples show a relatively wide range of both total (from 13.8% to 9.9%) and connected (from 12.9% to 2.5%) porosity values in comparison to CC samples that possess a narrow porosity range. The high heterogeneity of FB samples is related to the highly variable dimensions of the clasts observed at the microscale (from microns to some centimeters). The clay-rich cataclasite shows a bulk porosity of 7.7% and a connected porosity of 2.4%, both values being slightly lower with respect to CC samples.

Measured density values (2.47–2.69 g/cm<sup>3</sup>) are those typical for limestones (Mavko et al., 2009) where higher density is linearly related to lower porosity. Variations in density can, in fact, be only related to

**Table 1**  
Summary of the Physical Properties of the Fault Rocks Samples Measured at Ambient Pressure

Sample	Bulk density (g/cm <sup>3</sup> )	Total porosity (%)	Eff. porosity (%)	$V_p$ (km/s)	$V_s$ (km/s)	$V_p/V_s$
P01	2.66	7.4	1.7	6.12	3.19	1.92
P02	2.67	6.9	1.3	6.16	3.26	1.89
P03	2.66	7.1	1.4	6.53	3.20	2.04
P04	2.69	6.3	0.5	6.65	2.60	2.56
P05	2.68	6.4	0.7	6.13	2.84	2.16
<b>Average P</b>	<b>2.67</b>	<b>6.8</b>	<b>1.1</b>	<b>6.32</b>	<b>3.02</b>	<b>2.11</b>
FB01	2.53	11.6	6.3	4.59	2.95	1.56
FB02	2.47	13.8	12.9	5.55	2.68	2.07
FB03	2.50	12.7	2.5	5.77	2.78	2.08
FB04	2.57	10.2	4.6	5.21	2.91	1.79
FB05	2.58	9.9	4.4	4.90	2.67	1.84
FB06	2.52	12.1	6.7	5.53	2.47	2.24
<b>Average FB</b>	<b>2.53</b>	<b>11.7</b>	<b>6.2</b>	<b>5.26</b>	<b>2.74</b>	<b>1.93</b>
CC01	2.61	9.1	3.6	5.41	2.62	2.07
CC02	2.62	8.7	3.1	5.97	2.87	2.08
CC03	2.60	9.2	3.7	5.63	2.56	2.20
CC04	2.61	9.0	3.5	5.62	2.71	2.07
<b>Average CC</b>	<b>2.61</b>	<b>9.0</b>	<b>3.5</b>	<b>5.66</b>	<b>2.69</b>	<b>2.10</b>
<b>FC01</b>	<b>2.65</b>	<b>7.7</b>	<b>2.4</b>	<b>4.38</b>	<b>2.66</b>	<b>1.65</b>

Note. Bold line indicates the average values of each fault rock type. Eff. porosity is connected porosity,  $V_p$  is  $P$  wave velocity,  $V_s$  is  $S$  wave velocity where their ratio is reported in the last column

variation in porosity, in particular for pure limestone (CC, FB and P) samples, since no bulk mineralogical differences have been observed between these samples.

Axial  $P$  wave ( $V_p$ ) and  $S$  wave ( $V_s$ ) velocities measured at ambient pressure are listed in Table 1. The highest  $V_p$  values were recorded for the protolith samples (average  $V_p = 6.32$  km/s) whereas CC velocities (average  $V_p = 5.66$  km/s) are generally higher than FB velocities (average  $V_p = 5.26$  km/s). The higher velocities recorded for protolith samples are consistent with microstructural details showing higher density, lower porosity, and absence of cracks.

The clay-rich foliated cataclasite (FC) is characterized by the lowest velocity ( $V_p = 4.38$  km/s), likely related to (1) the more marly protolith, and (2) the presence of the abundant pressure solution seams, often reopened by microcracks almost perpendicular to the wave propagation direction.

The  $V_p/V_s$  ratios follow the same trend of  $V_p$  values being higher for protolith samples (2.11) and slightly lower for CC samples (2.10 on average). FB samples show the lower  $V_p/V_s$  ratio for footwall rocks (1.93) while the lowest value of the data set has been recorded for the FC samples (1.65).

#### 4.2. Measurements at Elevated Pressure

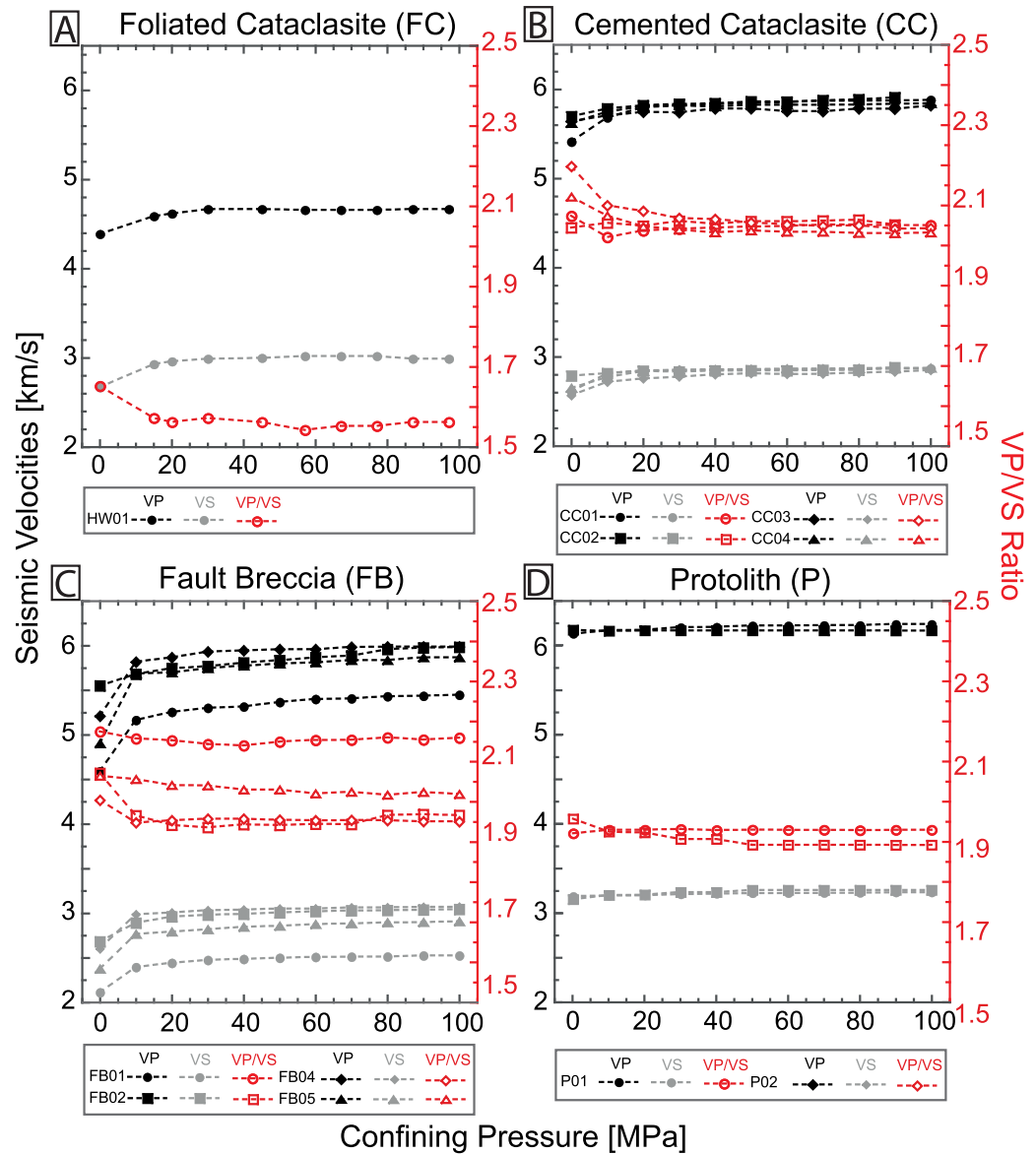
$V_p$  and  $V_s$  measurements were made on dry samples during pressurization from 0.1 to 100 MPa in 10 MPa increments, and during depressurization back to ambient pressure.

The results show that the velocities during pressurization and depressurization cycles are essentially similar, within measurement accuracy, and therefore the velocity hysteresis is negligible for all the tested samples with the exception of some FB samples. This suggests that, during pressurization, inelastic compaction acted only in FB samples. Since FB samples are highly fractured, as confirmed by high porosity at ambient pressure (Table 1) they are prone to compaction due to crack closure induced by pressurization. Due to this general absence of significant hysteresis, and for simplicity, we report only velocity measurements made during depressurization (Burke, 1987).

Variations in  $P$  and  $S$  wave velocity for dry samples as a function of the effective pressure are shown in Figure 5. All samples exhibit higher velocities at higher pressures, i.e.,  $>40$  MPa, due to the closure of cracks and the consequent decrease in porosity. Within this general trend, we observe that FB samples show a larger variability in velocities: 4.5–5.5 km/s at ambient pressure and 5.5–6 km/s at 100 MPa confining pressure. These samples also show the largest  $V_p$  increase: about 20% recorded within the first 40 MPa of applied confining pressure. Velocities are more pressure independent for the other rocks type, and absolute values show a narrower range (Figure 5). In particular, this trend is evident for CC and P samples (see Table 1) coherently with their meso-microstructural and petrophysical characteristics that show very low porosity, which is mostly not connected, i.e., primary porosity that is pressure independent. Moreover, the internal structure is homogeneous for all CC and P samples resulting in similar physical properties, which explains the recorded narrow range of velocities within these two groups. Clay-rich pressure solution seams are abundant in the foliated cataclasite (FC), decreasing the absolute velocities in respect to the pure limestone protolith. This effect is particularly evident at higher confining pressure where FC and P samples show a  $V_p$  of  $\sim 4.7$  and 6.2 km/s, respectively, resulting in a difference of 1.5 km/s.

For FB samples, the  $V_p/V_s$  ratio shows a large range,  $1.95 < V_p/V_s < 2.15$ , even at elevated pressures, whilst the other lithologies are more homogeneous resulting in a narrower range of  $V_p/V_s$  (red curves on Figure 5). For all the samples investigated, the evolution of the  $V_p/V_s$  ratio show a slight decrease at low confining pressures and becomes pressure independent above  $\sim 30$  MPa, in agreement with observations conducted on similar rock types such as dolomites (Trippetta et al., 2010).

Permeability measurements on water-saturated samples were performed at a constant pore fluid pressure ( $P_p$ ) of 10 MPa. Since the applied confining pressure ( $P_c$ ) must be equal to or greater than  $P_p$ , this means that measurements were necessarily conducted in the range of effective pressure, ( $P_e = P_c - P_p$ ) between 10 and 100 MPa. The clay-rich foliated cataclasite shows the lowest permeability (Figure 6) with a pressure-independent value of about  $6 \times 10^{-19}$  m<sup>2</sup>. This value is related to the presence of abundant clay-rich pressure solution seams arranged perpendicular to the fluid flow. Similar values of permeability have been recorded for the protolith, where the coupling between the very low porosity and the absence of fractures results in a very low permeability for this lithology. Our data are in agreement with those from Heap et al. (2014a) showing that when the fluid flow direction is perpendicular to pressure solution structures such as stylolites, the permeability is similar to that of the undeformed material.



**Figure 5.** Variation in axial  $P$  wave velocity (black),  $S$  wave velocity (grey), and  $V_p/V_s$  ratio (red) as a function of the effective confining pressure for all fault rocks: (a) foliated cataclasite; (b) cemented cataclasite; (c) fault breccia; and (d) footwall protolith.

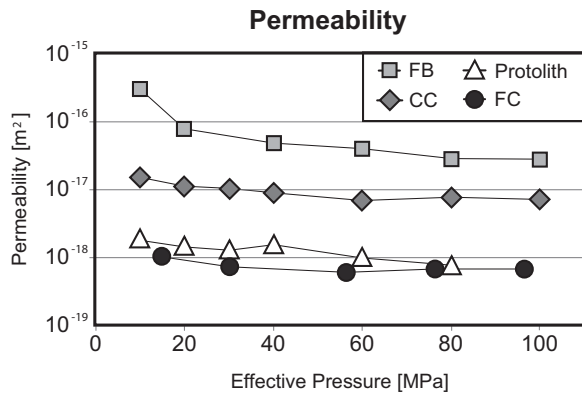
Permeability of the CC sample ( $\sim 4 \times 10^{-18} \text{ m}^2$ ) is higher than the protolith P ( $\sim 6 \times 10^{-19} \text{ m}^2$ ) and it is pressure independent. In contrast, the permeability of the FB sample is higher and pressure dependent showing values that decrease from  $\sim 2 \times 10^{-16} \text{ m}^2$  at ambient pressure to  $\sim 2 \times 10^{-17} \text{ m}^2$  at 100 MPa of confining pressure (Figure 6).

#### 4.3. Elastic Moduli

In order to assess the influence of the different structural domains of the fault zone on elastic moduli, we determined Young's modulus ( $E_d$ ) and Poisson's ratio ( $\nu_d$ ) values for each fault rock (P, FB, CC, and FC) at 0.1, 10, and 100 MPa. The dynamic moduli ( $E_d$  and  $\nu_d$ ) were calculated from measurements of  $V_p$  and  $V_s$  using the equations:

$$E_d = \rho \frac{V_s^2 (3V_p^2 - 4V_s^2)}{V_p^2 - V_s^2} \quad (1)$$





$$v_d = \frac{1}{2} \frac{V_p^2 - 2V_s^2}{V_p^2 - V_s^2} \tag{2}$$

**Figure 6.** Variation of permeability with increasing effective pressure up to 100 MPa for clay-rich foliated cataclasite (FC, circles), cemented cataclasite (CC, diamonds), fault breccia (FB, squares), and footwall protolith (P, triangles).

where  $\rho$  is rock density and  $V_p$  and  $V_s$  are the compressional and shear elastic wave velocities, respectively. Results are summarized in Table 2. As the confining pressure increases, the Young’s modulus ( $E_d$ ) increases and the Poisson’s ratio ( $v_d$ ) decreases (Figure 7), in agreement with similar data previously reported in the literature (Heap & Faulkner, 2008). The protolith exhibits the highest Young’s modulus and the lowest Poisson’s ratio of the footwall rocks. Within the fault zone  $E_d$  values are lower in FB than in CC. However, this difference vanishes with increasing confining pressure (Figure 7). This highlights the important role played by the open fractures, contained within FB, in controlling  $E_d$  at low confining pressure in agreement with previous data on similar fractured rocks (Trippetta et al., 2013b). Dynamic Poisson’s ratio is higher for FB with respect to CC indicating that the tested FB samples are weaker (more radially deformable) than CC samples. This is particularly

true at low confining pressure due the presence of a great number of cracks (see Figure 3 and section 2). In general, from the fault breccia to the cemented cataclasite, Young’s modulus decreases and Poisson’s ratio increases, with a nonlinear trend. For the clay-rich foliated cataclasite,  $E_d$  is in the range of FB and CC values whereas  $v_d$  is significantly lower. This could be related to several factors including: (1) the different protolith (see section 2) and (2) the presence of many pressure solution seams resulting in a strong anisotropy of the sample. In addition, due to the impossibility of obtaining samples parallel to the foliation, we have been able to test only samples drilled perpendicularly to the foliation. By measuring velocity perpendicular to the fault plane  $V_p$  tends to decrease due to the presence of several discontinuities that affect  $V_p$  more than  $V_s$ . For this reason, we observe a reduction in both  $E_d$  and  $v_d$  values with respect to the footwall fault rocks.

## 5. Discussion

### 5.1. Evolution of Fault Zone Physical Properties During Deformation

The petrophysical characterization of distinct carbonates rocks that are representative of different structural domains of a fault zone allowed us to draw a quantitative picture of the processes acting on a carbonate-bearing fault.

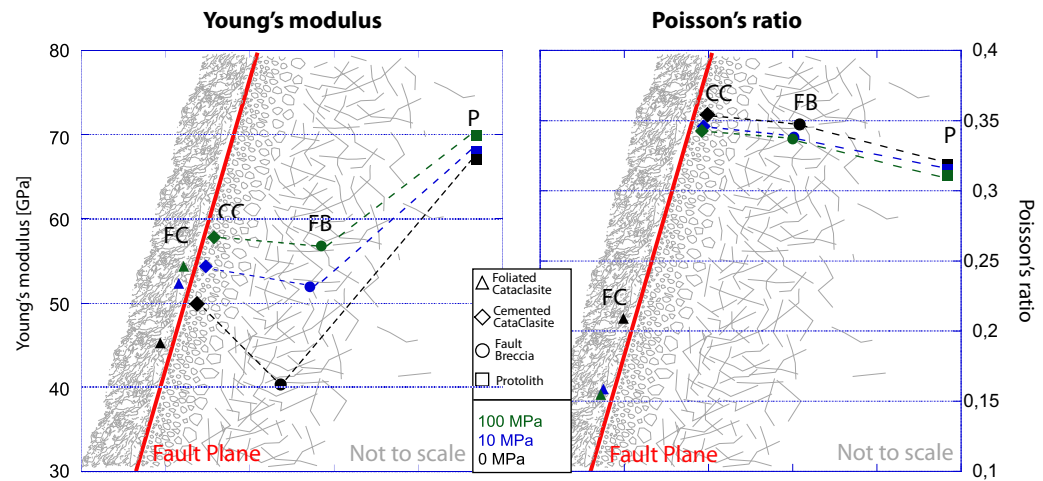
Porosity variations measured between P, FB, and CC samples suggests that starting from the protolith, fracturing would increase both the total porosity (from ~7% to ~12%) and the connected porosity (from ~1% to ~6%); thus, new pores with high aspect ratio should form during this process. Accordingly, permeability of FB samples is higher,  $V_p$  is lower with respect to the protolith, and both are pressure dependent.

Once the FB is formed, cataclasis and grain size reduction acting near the fault plane, together with healing and sealing processes, would tend to decrease porosity, both total (from ~12% to 9%) and connected (from ~6% to 3.5%), producing the cemented cataclasite, CC. These microstructural changes within the CC are highlighted by the lower permeability values and higher  $V_p$  velocities with respect to FB samples (Figures 5 and 6); in addition, permeability and  $V_p$  are pressure independent. The pressure dependency of permeability for FB (Figure 6) highlights that cracks tend to close at relatively low confining pressure (i.e., above 40 MPa). However, this crack closure is not enough to inhibit the role of fractures in increasing permeability, making FB the structural domain where crustal fluids can easily flow, even at seismogenic crustal depths (4–8 km). To be noted that our laboratory results are applicable to the current state of cementation within the fault zone, while the state of cementation may vary during the seismic cycle. Results from previous laboratory studies indicate that the permeability of similar carbonate-fault rocks ranges from  $10^{-16}$  to

**Table 2**  
Measured Mechanical Properties (Young’s Modulus, YM, and Poisson’s Ratio, PR) of the Tested Samples at 0.1, 10, and 100 MPa of Confining Pressure

Sample	0.1 MPa		10 MPa		100 MPa	
	YM (GPa)	PR	YM (GPa)	PR	YM (GPa)	PR
P01	65.47	0.32	65.52	0.32	68.42	0.32
P02	67.65	0.32	69.28	0.32	71.27	0.31
<b>Average P</b>	<b>66.56</b>	<b>0.32</b>	<b>67.40</b>	<b>0.32</b>	<b>69.85</b>	<b>0.31</b>
FB01	39.26	0.35	53.15	0.34	58.37	0.34
FB02	47.83	0.35	54.68	0.33	60.63	0.33
FB04	46.44	0.33	60.67	0.32	64.12	0.32
FB05	30.84	0.37	39.59	0.36	43.99	0.36
<b>Average FB</b>	<b>41.10</b>	<b>0.35</b>	<b>52.02</b>	<b>0.34</b>	<b>56.78</b>	<b>0.34</b>
CC01	47.87	0.35	55.19	0.34	57.61	0.34
CC02	54.61	0.34	55.75	0.35	58.41	0.34
CC03	46.98	0.37	52.04	0.35	56.74	0.34
CC04	50.38	0.36	54.76	0.35	58.58	0.34
<b>Average CC</b>	<b>49.96</b>	<b>0.35</b>	<b>54.43</b>	<b>0.35</b>	<b>57.84</b>	<b>0.34</b>
FC01	<b>45.29</b>	<b>0.21</b>	<b>52.31</b>	<b>0.16</b>	<b>54.32</b>	<b>0.15</b>

Note. Bold line indicates the average values of each fault rock type.



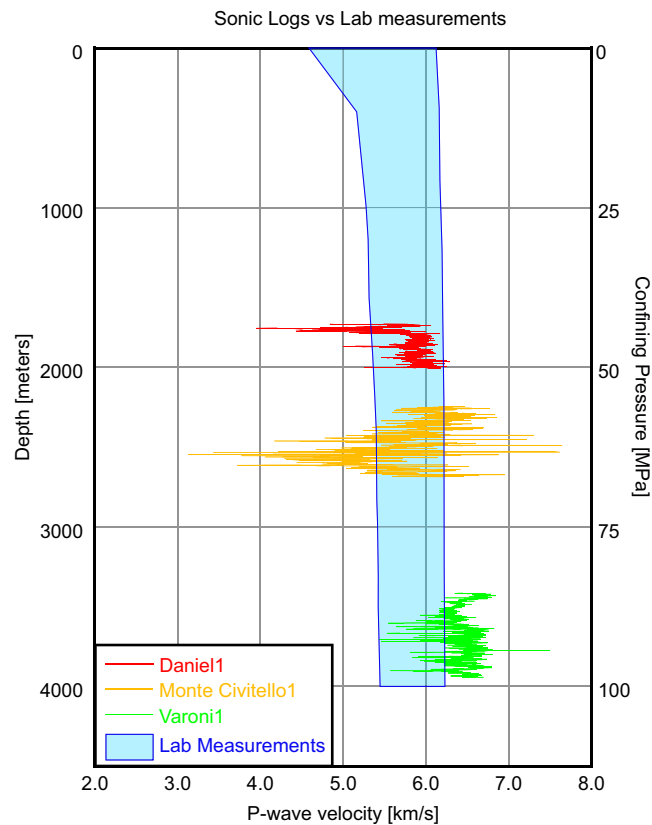
**Figure 7.** Variation of (a) Young's modulus and (b) Poisson's ratio as a function of the fault zone architecture. The elastic parameters of foliated cataclasite (FC, circles), cemented cataclasite (CC, diamonds), fault breccia (FB, squares), and protolith (P, triangles) are reported at effective pressures of up to 0.1 MPa (black), 10 MPa (blue), and 100 MPa (green).

$10^{-20}$  m<sup>2</sup> at effective pressure up to 50 MPa, depending on fault rock type (Agosta et al., 2007). Our results are in agreement with these data, showing permeability down to  $10^{-19}$  m<sup>2</sup> for undeformed rocks and up to  $10^{-16}$  m<sup>2</sup> for the most intensely fractured rocks (FB). Permeability of granular fault gouges, obtained from crushing and sieving a protolith similar to the one analyzed here, show values in the range of  $5 \times 10^{-17}$ – $7 \times 10^{-18}$  m<sup>2</sup> (Scuderi & Collettini, 2016).

The tested clay-rich foliated cataclasite is affected by different deformation mechanisms as shown by numerous pressure solution seams with clay concentration along the stylolites. This fabric leads to lower the permeability ( $1 \times 10^{-18}$ – $9 \times 10^{-19}$  m<sup>2</sup>) and porosity, and a reduction in *P* wave velocities, which influences the elastic parameters and hence, the mechanical behavior of this portion of the fault zone.

### 5.2. Comparison Between Laboratory-Scale and Field-Scale *P* Wave Measurements

We have estimated synthetic *P* wave sonic logs profiles as a function of depth (Figure 8) by (1) supposing a general lithostatic stress gradient of 25 MPa/km, and (2) reporting the recorded values of *P* wave velocities of carbonate samples analyzed in this work (CC, FB, and P):  $V_p$  of FB (FB01 sample, cf. Table 1) represents the lower boundary of the synthetic profile whilst  $V_p$  of the P01 sample (Table 1) marks the upper boundary. These data, derived from the laboratory experiments, have been compared with digitalized *P* wave sonic logs from three boreholes that drilled the calcareo massiccio FM in Italy: Daniel1, Monte Civitello1, and Varoni1 (<http://unmig.sviluppoeconomico.gov.it/vidempi/vidempi.asp>). Figure 8 shows the relationship between the synthetic profile and the sonic log profiles reported in the boreholes composite log; the three boreholes locations are reported in Figure 1. In the laboratory versus in situ comparison, we report only the sonic log data for those portions of the wells that passed through the calcareo massiccio formation and laboratory data from footwall samples since they pertain to the same formation (cf. also section 2). All of the reported sonic logs are highly scattered as commonly observed for similar measurements and for data acquired in the 1980s (e.g., Latorre et al., 2016; Smeraglia et al., 2014; Trippetta et al., 2010, 2013). This is due to technical issues related to the acquisition tool and fluctuations of fluid pressures during the acquisition, thus anomalous high or low velocities can be considered as biased. The Daniel1 well penetrated the calcareo massiccio formation from about 1,750 to 2,015 m depth, and the lithology consists of highly fractured, pure limestone. The sonic log indicates a  $V_p$  in the range of 5.8 to 6.2 km/s. Recorded velocities mostly fall in the laboratory range whilst spikes in the upper part of the log indicates lower velocities. The Monte Civitello1 well-encountered calcareo massiccio formation over the depth range 2,250–2,700 m. The composite log highlights the presence of Packstone-Wackestone (Dunham, 1962) textures for the whole interval. Recorded values range from 4.0 to 7.5 km/s particularly in the depth range 2,450–2,600 m, however, most values fall between 5.5 and 6.2 km/s. In agreement with Daniel1 data, *P* wave velocities are mostly consistent with laboratory results.



**Figure 8.** Comparison between synthetic  $V_p$  depth profile derived from the laboratory  $P$  wave velocity measurements reported in this study and in situ  $V_p$  measurements from sonic logs through the calcare massiccio (<http://unmig.sviluppoeconomico.gov.it/videpi/videpi.asp>). See text for details of the method used for the calculation of the synthetic profile.

The Varoni 1 well penetrated the calcare massiccio formation from 3,418 to 4,400 m, where dolomitized Packstone-Grainstone textures are reported in the composite log for this interval. The sonic log records stop at depth of 3,947 m due to technical problems, for this reason we report  $V_p$  in the interval 3,418–3,947 m.  $V_p$  recorded on this well are mostly in the range 6.1–6.8 km/s. These velocities are higher with respect to what we recorded in the laboratory and higher with respect to any laboratory value for pure carbonates (e.g., Mavko et al., 2009).

The comparison of velocity data from sonic logs and laboratory measurements shows that most of the sonic log data agree with laboratory measurements. Moreover, both lab and in situ data clearly show that for the calcare massiccio formation the confining pressure (depth) does not influence velocity at the investigated depths. In addition, in situ data show some lower velocities with respect to laboratory measurements. This can be well explained by the presence of in situ mesoscale fractures not reproducible in laboratory (Trippetta et al., 2013a; Vinciguerra et al., 2006). For the Varoni1 borehole, we also observed the unusual situation of higher in situ velocities with respect to laboratory measurements. However, these higher in situ velocities are associated with a dolomitized portion of the calcare massiccio formation. The dolomitization of a pure limestone can progressively increase its initial velocity (Mavko et al., 2009) up to 7.3 km/s (Trippetta et al., 2010). On the other hand, mesoscale fracturation can reduce  $V_p$  values down to the observed values at the Varoni1 well (average  $V_p \sim 6.7$  km/s). We then suggest that both physical (mesoscale fractures) and chemical (dolomitization) processes are crucial for the propagation of seismic waves in carbonates at crustal scales. In general, the agreement between laboratory and in situ data indicates that the elastic moduli derived from laboratory  $V_p$  measurements represent a good estimate for the elastic properties of natural carbonate-bearing fault zone structures at seismogenic crustal levels.

**5.3. Implications for Earthquake Nucleation on Carbonate-Bearing Faults**

Once a fault has been formed, its further motion and slip behavior, seismic or aseismic, is controlled by the frictional properties of the sliding surface and the elastic properties of the medium surrounding the fault. In this paragraph, we integrate our data on Elastic moduli (the fault surrounding medium) with fault frictional properties derived from the literature, to discuss earthquake nucleation on carbonate-bearing faults.

Earthquake nucleation and the mechanics of frictional sliding can be evaluated for a 1-D fault obeying rate- and state-friction (Dieterich, 1979; Marone, 1998; Ruina, 1983) by considering the elastic stiffness of the surrounding medium,  $k$ , and the fault frictional properties, which can be written in terms of a critical rheologic stiffness  $k_c$  (Gu et al., 1984). The condition for instability, when sliding velocity is still low, can be written as:

$$k < k_c = \frac{(\sigma_n P_f)(b-a)}{D_c} \tag{3}$$

where  $\sigma_n$  is the normal stress,  $P_f$  is the pore fluid pressure,  $(b-a)$  is the friction rate parameter, and  $D_c$  is the critical slip distance. Numerical studies (Gu et al., 1984) and recently laboratory data (Ikari et al., 2015; Leeman et al., 2016; McLaskey & Yamashita, 2017; Scuderi et al., 2016) confirmed the theoretical criterion of equation (3). For a two- or three-dimensional case, the stiffness  $k$  must be inversely proportional to a length scale (Kanamori & Brodsky, 2004; Scholz, 2002). If the slipping region is treated as an elliptical crack, the stiffness  $k$  is:

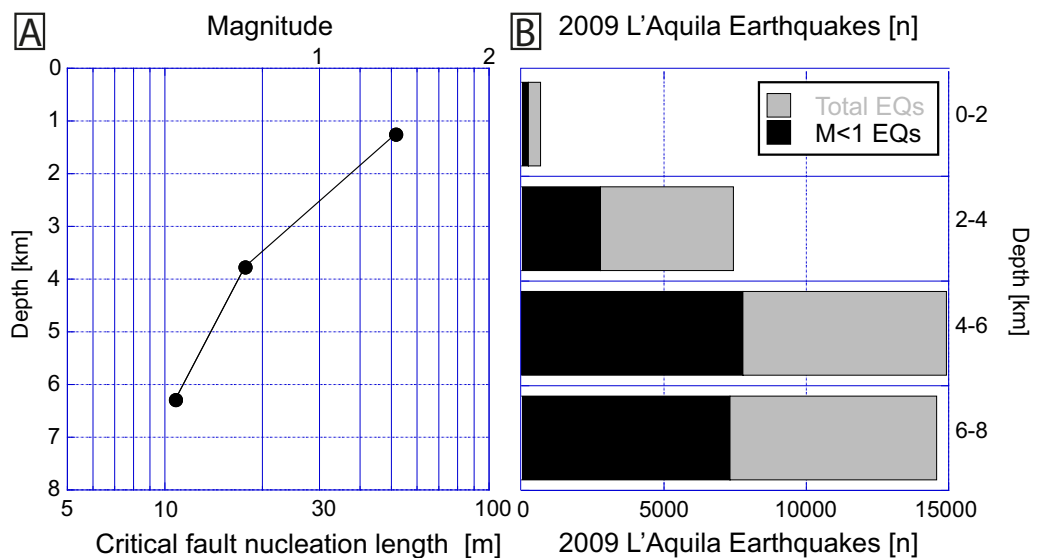
$$k = \frac{E}{2(1-\nu^2)L} \tag{4}$$

where  $L$  is the length of the slipping region,  $E$  is the Young's modulus, and  $\nu$  is the Poisson's ratio. Combining equation (3) with equation (4) results that the stability transition occurs at a critical length of the slipping region,  $L_c$ , given by:

$$L_c = \frac{ED_c}{(1-\nu^2)\sigma_n(b-a)} \tag{5}$$

Equation (5) predicts that stable sliding will occur during a nucleation stage until the slipping region grows to  $L_c$  and then, the earthquake instability occurs.

To evaluate  $L_c$  for carbonate-bearing faults, we used the elastic moduli of the Monte Maggio Fault, i.e., CC and FB that represent the fault loading medium (paragraph 4.3). The effective pressures of the laboratory



**Figure 9.** Comparison between: (a) the calculated critical nucleation length  $L_c$  with increasing depth (horizontal axis reported the critical nucleation length,  $L_c$ , and the equivalent minimum earthquake magnitude,  $M$ ) and (b) the totale (grey) and  $M \leq 1$  (black) earthquake depth-distribution of the 2009 L'Aquila sequence (Chiarialuze et al., 2011) showing an increase of both total and  $M < 1$  earthquakes above  $\sim 4$  km.

**Table 3**  
Imposed Confining and Fluid Pressures With Corresponding Depths and Normal Stresses, Used in Equation (5) to Calculate  $L_c$  of Figure 9a

Confining pressure (MPa)	Pore fluid factor	Equivalent depth (m)	Sigma n (MPa)	YM (GPa)	PR	$D_c$ (m)	b-a (m)
20	0.4	1258	10	54.72	0.3406	0.00005	0.003
60	0.4	3775	30	56.36	0.3396	0.00005	0.003
100	0.4	6292	50	57.31	0.3398	0.00005	0.003

Note. Young's Modulus (YM) and Poisson's Ratio (PR) at respective confining pressures have been obtained by averaging FB and CC data from this work. The values of 0.003 for b-a represents an average respect to the range of 0.001–0.006 reported in literature (Carpenter et al., 2016; Colletini et al., 2014a; Verberne et al., 2010, 2015). Similarly  $D_c$  value of  $50 \times 10^{-6}$  m represent an average respect to the range of  $10 \times 10^{-6}$ – $100 \times 10^{-6}$  m derived from previous works (Carpenter et al., 2014; Scuderi & Colletini, 2016).

experiments have been converted to crustal depths assuming a hydrostatic fluid pressure represented by a pore fluid factor of  $\lambda = P_f/\rho g z = 0.4$ , where  $\rho$  is the rock density,  $g$  is the acceleration due to gravity, and  $z$  is the crustal depth. For the frictional properties, we used data from the Monte Maggio Fault (Carpenter et al., 2014) and other data on carbonates at different boundary conditions (Carpenter et al., 2016; Scuderi et al., 2016; Verberne et al., 2010, 2015). The data used to estimate  $L_c$  (Figure 9a) are reported in Table 3. The  $L_c$  values evolve from about 50 m at shallow crustal levels to 12 m below 6 km. This is a rough estimate of  $L_c$  that can increase or decrease based on changes in the different parameters of equation (5). In particular, a reduction of  $D_c$  induced by fluid overpressure (Scuderi & Colletini, 2016) can reduce  $L_c$  as well as a more pronounced velocity weakening behavior favored by the increase of temperature (Verberne et al., 2010, 2015). On the other hand, a less pronounced velocity weakening behavior at low normal stresses (Carpenter et al., 2016) or due to fault rock heterogeneities (Carpenter et al., 2014) favors an increase  $L_c$ . Taking into account the variability mentioned above, the analysis on  $L_c$  suggests that: (1) within the seismogenic layer, earthquake occurrence should increase with depth since  $L_c$  decreases (Figure 9); (2) at shallow crustal levels,  $M \leq 1$  earthquakes are unlikely since the critical nucleation length is larger than the earthquake rupture radius estimated from elastic dislocation theory considering the fault as a circular crack with a stress drop of 3 MPa (Kanamori & Anderson, 1975; Sibson, 1989). To test these hypotheses, in Figure 9b, we have reported the frequency-depth distribution of total earthquakes and those with magnitudes  $M \leq 1$  recorded during the 2009 L'Aquila seismic sequence (Chiaraluce et al., 2011) that occurred on carbonates similar of those tested in this study (Valoroso et al., 2014). The increase of earthquake occurrence with depth agrees with the reduction of  $L_c$  with depth. The reduction of the percentage of earthquakes at shallow crustal levels is consistent with the mechanical prediction that  $L_c$  is larger than the dimension of a  $M \leq 1$  earthquake at such a depth. In addition, the presence of  $M \leq 1$  at shallow crustal levels can be addressed by several factors including the mentioned variations in the rate and state friction parameters that would reduce  $L_c$  and stress transfer processes induced by the larger events (e.g., Boatwright & Cocco, 1996; Stein et al., 1992).

## 6. Conclusions

Physical and transport properties of the investigated fault zone are controlled by the different deformation processes. Fracturing in the fault breccia results in high porosity (11% total and 6.2% connected), low and pressure-dependent  $V_p$  (4.9–5.9 km/s), and relatively high and pressure-dependent permeability ( $10^{-16}$ – $10^{-17}$  m<sup>2</sup>). Grain size reduction and cementation process near the fault plane reduce porosity (9% total and 3.5% connected), increase  $V_p$  (5.9 km/s), and decrease permeability ( $9 \times 10^{-18}$  m<sup>2</sup>). Fault rocks affected by pressure solution processes show significantly different physical properties: low porosity (7.7% total and 2.4% connected), low  $V_p$  (4.4 km/s), and low permeability ( $8 \times 10^{-19}$  m<sup>2</sup>).

The comparison between laboratory  $V_p$  measurements and with in situ sonic logs shows a general agreement for the two data sets. Lower in situ  $P$  wave velocities ( $\sim 5$  km/s at 2,500 meters in the M. Civitello1 borehole) in comparison to laboratory measurements (5.5–6.2 km/s at equivalent depth) are likely related to mesoscale fractures that cannot be captured in experiments conducted on centimeter samples. Higher in situ  $P$  wave velocities ( $\sim 6.5$  km/s at 3,800 m in the Varoni1 borehole) in comparison to laboratory measurements (5.5–6.2 km/s at equivalent depth) can be explained by the dolomitization documented in the borehole report.

The characterization of the fault critical nucleation length,  $L_c$ , obtained from elastic moduli and frictional properties suggests that at shallow crustal levels,  $M \leq 1$  earthquakes are less favored, since the critical nucleation length is larger than the earthquake rupture radius. Considering the influence of the frictional parameters in estimating  $L_c$  at first approximation, our results are consistent with the small number of  $M \leq 1$  earthquakes recorded at shallow crustal depth during the L'Aquila 2009 seismic sequence occurring on carbonates.

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