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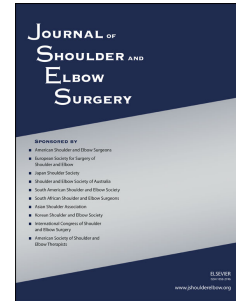
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Elbow Joint Loads during Simulated Activities of Daily Living: Implications for Formulating Recommendations after Total Elbow Arthroplasty

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1 **Elbow Joint Loads during Simulated Activities of Daily Living: Implications for** 2 **Formulating Recommendations after Total Elbow Arthroplasty**

3

4 **Abstract**

5 Background: Overloading of the elbow joint prosthesis following total elbow arthroplasty can
6 lead to implant failure. Joint moments during daily activities are not well-contextualized for a
7 prosthesis' failure limits and the effect of the current postoperative instruction on elbow joint
8 loading is unclear. This study investigates the difference in elbow joint moments between
9 simulated daily tasks and between flexion-extension, pronation-supination, varus-valgus
10 movement directions. Additionally, the effect of the current postoperative instruction on
11 elbow joint load is examined.

12 Methods: Nine healthy participants (age 45.8 ± 17 years, 3 males) performed eight tasks;
13 driving a car, opening a door, rising from chair, lifting, sliding, combing hair, drinking,
14 emptying cup, without and with the instruction "not lifting more than 1 kg". Upper limb
15 kinematics and hand contact forces were measured. Elbow joint angles and net moments were
16 analyzed using inverse dynamic analysis, where the net moments are estimated from
17 movement data and external forces.

18 Results: Peak elbow joint moments differed significantly between tasks ($p < 0.01$) and
19 movement directions ($p < 0.01$). The most and least demanding tasks were, rising from a chair
20 (13.4 Nm extension, 5.0 Nm supination, 15.2 Nm valgus) and sliding (4.3 Nm flexion, 1.7
21 Nm supination, 2.6 Nm varus). Net moments were significantly reduced after instruction only
22 in the chair task ($p < 0.01$).

23 Conclusion: This study analyzed elbow joint moments in different directions during daily
24 tasks. The outcomes question whether postoperative instruction can lead to decreasing elbow

25 loads. Future research might focus on reducing elbow loads in the flexion-extension and
26 varus-valgus directions.

27

28 Keywords: elbow joint loading, joint moments, elbow prosthesis, TEA, biomechanical
29 analysis, varus-valgus, inverse dynamics.

30 Level of Evidence: Basic Science Study; Kinesiology

31

32 Total elbow arthroplasty (TEA) is a surgical procedure that is performed to reduce pain
33 and regain function in patients with a variety of debilitating elbow pathologies, such as
34 inflammatory or post-traumatic arthritis and complex fractures [38]. Though the use of TEA is
35 growing, it remains a relatively uncommon orthopedic procedure, with 3,146 TEAs performed
36 over a 5-year period in the USA [41]. In the Netherlands, the number of TEAs rose from 67 in
37 2017 to 73 in 2022 [19]. It is performed more often in women than in men [7, 13].
38 Unfortunately, elbow prosthesis survival rates following TEA are low compared to those
39 following hip and knee arthroplasties. The current TEA survival rate in the range of 7.5-14.2
40 years is 71-87% [31, 37, 38] compared to a 10 year survival rate of 90-95% for hip and knee
41 arthroplasty [8, 17, 33].

42 The most important factor determining poor survival rates of elbow arthroplasty is
43 aseptic loosening of the humeral component [31, 32, 36-38]. Retrieval studies showed that
44 aseptic loosening results from different mechanisms. First, overloading of the prosthesis during
45 activities of daily living (ADL) causes polyethylene (PE) wear [26, 32], bringing loose particles
46 to the proximity of the bone-prosthesis interface, ultimately leading to bone destruction and
47 inflammation [4, 12, 32]. Revision surgery becomes necessary as a result of aseptic loosening.
48 A second mechanism of failure may be inadequate cement fixation [22], where excessive
49 stresses at the bone-cement-prosthesis interface leads to micromotion and consequent failure of

50 the implant. Last, joint replacements face greater durability requirements as lifespan lengthens.
51 It has been observed that patients following TEA stay active for a longer period, and are less
52 inclined to restrict their lifestyle to safeguard the prosthesis' lifetime [2]. In the long term, this
53 behavior may lead to overloading of the implant during activities of daily living [21].

54 In vitro tests to analyze elbow joint biomechanics have provided insight into the failure
55 mechanisms of TEA. Lo and Lipman examined retrieved Coonrad Morrey ulnar components,
56 demonstrating that varus-valgus (VV) moments in the ulnohumeral joint as high as 5 Nm would
57 lead to loads exceeding the PE's theoretical yield strength of the Coonrad-Morrey prosthesis
58 and consequently to irreversible plastic deformation [18]. Furthermore, elbow joint loading of
59 three different types of TEAs while holding a 2.3-kg weight exceeded the yield strength of PE
60 when the shoulder was abducted at 45° and 90° [15]. However, these results are not easily
61 generalizable to ADL tasks, as it isn't known what the specific loads during different ADL tasks
62 are and which tasks could lead to a potential overload of the elbow joint.

63 To reduce overloading of the elbow, common clinical practice is to instruct patients not
64 to perform daily activities that regularly exceed lifting 1 kg weight and incidentally up to 5 kg
65 [5, 9]. However, this guideline lacks specificity since it is unclear which ADL tasks or specific
66 movements would exceed the 1-5-kg limits and should thus be avoided [5]. Depending on the
67 type of movement and how it is executed, similar weights can lead to different loads on the
68 elbow [15, 20]. It is therefore crucial to know whether the current clinical instruction brings
69 about a detectable reduction in elbow joint loads.

70 The low survival rates, combined with the lack of consensus on postoperative
71 management, emphasize the need for biomechanical studies focusing on elbow joint loading
72 during ADL. The aims of the current study are: first, to identify any differences in range of
73 motion and elbow joint moments between eight ADL tasks in a lab setting; second, to identify
74 differences in peak loads between the flexion-extension (FE), pronation-supination (PS), varus-

75 valgus (VV) movement; and last, examine whether the current instruction of “not lifting more
76 than 1 kg” leads to a decrease in elbow joint moments. We hypothesize that joint moments will
77 differ per task and that the instruction will not lead to a decrease in elbow joint load.

78

79 **Materials and Methods**

80 *Participants*

81 Nine healthy, able-bodied participants performed eight simulated ADL tasks. Exclusion
82 criteria were 1) mental or physical disability to meet study requirements; 2) insufficient
83 command of the Dutch language; 3) prior surgery in the upper extremity or other pathologies
84 affecting upper extremity function. Participants were informed about the procedures and signed
85 an informed consent. The study was approved by the Medical Ethical Committee of University
86 Medical Center Groningen, The Netherlands (METc2019/624). Anthropometric data are
87 presented in Table I.

88

89 *Procedure*

90 Basic anthropometric data (length, weight, arm length, shoulder width) and a maximum
91 voluntary contraction of the biceps and triceps were collected at entrance. After a static
92 calibration trial, participants performed a standardized series of eight ADL tasks in two
93 conditions (Figure 1). All tasks are explained in Table II. After one entire series (uninstructed
94 condition), another series followed with each task performed again (Figure 1), this time with a
95 verbal instruction comprising the recommendation to “not exceed lifting 1-kg weight and only
96 incidentally use up to 5 kg” (instructed condition). In both conditions, the tasks were performed
97 in the same fixed order (Table II).

98 The tasks were selected based on the expected amount of elbow movement, as well as
99 on patients’ frequently asked questions after TEA surgery [1]. In the seated tasks, the participant

100 sat on a height-adjustable chair without back support. A 75-cm high table was placed in front
101 of the participant, with a marked starting point. The height of the chair was adjusted so that the
102 elbow was flexed at 90° when the hand was placed on the table, and the upper arm was held in
103 vertical position (Figure 2). For each task, an initial position and aim were defined. After verbal
104 instruction and one test trial, each task was repeated five times. The participant was instructed
105 to move at a comfortable speed throughout the experiment. Between the different tasks, there
106 was a rest period of at least 30 seconds. All tasks were performed consecutively twice, i.e., in
107 two consecutive conditions.

108 In three ADL tasks (1, 2, 3), a force transducer was used to record generated external
109 reaction forces. During the steering wheel task, a constant force of 15N for the car task and 25N
110 for the door task was applied as resistance [16, 25].

112 *Instruments and Data Collection*

113 Body segment position of the upper extremity was collected at 100Hz using a 4-position
114 sensor motion capture system (Optotrak 320; Northern Digital Inc., Waterloo, ON, Canada).
115 Four infrared light-emitting markers were placed on bony landmarks of the upper limb and
116 thorax. Six rigid bodies were placed on the thorax and upper limb segments, which mapped 14
117 additional virtual markers. Last, one marker was placed on the center of the force transducer
118 and one marker on the 1-kg object. All marker positions are shown in Appendix A. The
119 coordinate system of the marker data was set on the table, with X forward, Z to the right, and
120 Y upward.

121 Force data were recorded with a force transducer (ME-Messysteme GmbH,
122 Henningsdorf, Germany) with an accuracy of 0.01 N. The force transducer was mounted on an
123 aluminum T-bar and could be set in different positions (Figure 2a/b). Both marker data and

124 force data were recorded with a frequency of 100 Hz. The motion capture system and the force
125 transducer were digitally synced to enable simultaneous recording.

126

127 *Data Analysis*

128 The force values in the local coordinate systems were converted into a global coordinate
129 system of the motion capture system using a customized MATLAB script (version 20a;
130 MathWorks Inc., Natick, MA, USA). The motion capture data and force data were filtered in
131 MATLAB using a 4th-order Butterworth filter with a 6Hz cut-off frequency. Data gaps were
132 reconstructed using piecewise cubic spline interpolation.

133

134 *Musculoskeletal model:*

135 OpenSim musculoskeletal modeling software (version 3.3; Stanford University,
136 Stanford, CA, USA) was used to run the dynamic Holzbauer model [11, 35]. This model
137 consists of 7 bone segments and 50 Hill-type muscle-tendon actuators, representing 32 muscles
138 and muscle compartments (Figure 2c). This model, which only allowed elbow joint moments
139 in the FE and PS direction calculation, was adjusted to include the VV moments. To analyze
140 the VV direction, an extra degree of freedom was computed in the humeroulnar joint. The
141 maximum VV range of motion was set from -11.2° valgus to 6.6° varus [29]. The model was
142 scaled in OpenSim to the body dimensions of the participant using data from the static
143 calibration trial. The anatomical locations and the segments' coordinate systems are in
144 accordance with the International Society of Biomechanics (ISB) recommendations [40].
145 Inverse kinematic analysis was accomplished by using the OpenSim application programming
146 interface in MATLAB [6]. Inverse dynamic analysis was performed in OpenSim software
147 interface. The external reaction forces were applied to the model's hand segment at the distal
148 end of the third metacarpal bone of the dominant hand. The gravitational force was applied to

149 the hand on the task where the 1-kg object was lifted. In the task where a 1-kg object was slid
150 across the table, a dynamic friction coefficient of 0.5 for polyethylene-on-polyethylene was
151 applied. Repetition 2, 3 or 4 was normalized over time from the start of the movement to the
152 end.

153 The data was further processed in MATLAB 20a to extract 1) the ROM in the FE and
154 PS directions, and 2) peak elbow joint moments in three different directions (FE, PS, VV). The
155 standard deviations of the peak elbow joint moments were calculated to quantify intersubject
156 variability.

157

158 *Statistical analysis:*

159 Peak joint moments were used to test the differences in elbow joint moments between
160 direction (FE, VV, PS), tasks (car, door, chair, etc.), and condition (instructed, uninstructed).
161 To analyze the data, IBM SPSS Statistics v 29 (IBM Corp., Armonk, NY, USA) was used for
162 linear mixed-model analysis. Bonferroni correction was used for post hoc tests. Cohen's d was
163 calculated to indicate the effect size of the post hoc tests. A p -value $< .01$ was considered
164 statically significant. Normality of data distribution was tested to allow parametric testing.

165 Since the joint moments were not normally distributed, the positively skewed
166 distribution of joint moments was normalized via a square root transformation (Appendix B) so
167 that the linear mixed model could be used.

168

169 **Results**

170 *Kinematic data*

171 The average ROM of all the participants is shown in Figure 3. Chair, door, and cup tasks
172 showed the largest FE-ROM (range 19° to 110°). The hair and drinking task corresponded with

173 the highest extension angles (126°). Large PS-ROM was observed during the cup task (range
174 38° to -59°). The greatest ROM variability was seen during the hair task.

175

176 *Joint Moments*

177 Figure 4 shows the normalized joint moments over time in the FE, PS, and VV
178 directions for the eight ADL tasks. Especially the chair, car, and door tasks show greater
179 intersubject variability. Peak elbow joint moments for the FE, PS, and VV direction are shown
180 in Table III. The overall highest peak moments were observed when rising from a chair (13.4
181 Nm extension, 5.0 Nm supination, 15.2 Nm varus), followed by steering a car (9.3 Nm
182 extension, 5.4 Nm supination, 15.2 Nm valgus). The slide task required the smallest elbow
183 moment (4.3 Nm flexion, 1.7 Nm supination, 2.6 Nm valgus). Table IV shows an overall
184 ranking of the eight tasks based on the joint moment magnitude and the externally applied force.
185 Greater elbow joint moments, in all directions, were present during those tasks with an external
186 reaction force applied on the hand.

187 Statistical outcomes are presented in Table V. Peak elbow joint moments were
188 significantly different between the tasks, $F(7,376) = 40.44$, $p < .001$. There was a significant
189 difference in elbow joint loads between the movement directions, $F(2,376) = 170.02$, $p < .001$.
190 Post-hoc test showed that VV moments ($p < .001$, *Cohen's d* = 1.3) and FE moments ($p < .001$,
191 *Cohen's d* = 1.3) were significantly higher than PS moments.

192 The instruction did not lead to a significant decrease in elbow joint load $F(1,376) = 2.07$
193 $p = 0.15$. However, a significant interaction effect of task and condition was found ($p < 0.01$).
194 This evidences that the instruction only had an effect on selected tasks. Follow-up analysis
195 showed that only during the chair task was there a significant decrease in elbow joint load when
196 the instruction was followed ($t(1,376) = 2.58$, $p < 0.01$). During this task, the participants lifted
197 their own body weight using a combination of arm and, possibly, leg movements.

198 **Discussion**

199 In this study, eight simulated ADL tasks were analyzed on range of motion and peak
200 joint moments in FE, PS, and VV direction, depending on the given verbal instruction of not
201 lifting more than 1 kg. Joint moments did differ between tasks and movement directions. FE
202 moments and VV moments were significantly higher compared to PS moments. The effect of
203 the instruction of 'not lifting more than 1 kg' was dependent of the tasks. Only during the chair
204 rise task did the instruction result in a significant decrease in elbow joint loads. These results
205 confirm our hypothesis that elbow joint moments differ per task, and indicate that the current
206 instruction might be reconsidered to emphasize the load demand per task based on
207 biomechanical evidence.

208 The tasks performed during this study give a good representation of elbow ROM needed
209 to naturally perform ADL. The findings of the FE-ROM (range 19°–126°) are in line with
210 earlier literature [27]. A review of Oosterwijk et al concluded that an FE-ROM 0°–150° is
211 required for ADL tasks, which is more than the generally used reference of 30°–130° [21, 34].
212 Mainly tasks needed for personal care and feeding needed a flexion angle > 135° [27]. FE angles
213 < 30° were observed during the door, cup, and lift tasks. A review of Kincaid and An shows
214 that especially peak bone-on-bone contact forces occur between 7° and 11° flexion (almost fully
215 extended) [14]. Muscle activity and therefore bone-on-bone contact forces would be higher
216 early in the flexion cycle due to the poor mechanical advantage of the prime movers: the
217 brachialis, biceps, and brachioradialis muscles [24]. The functional PS-ROM of -50° pronation
218 to 88° supination found in our study is higher than the PS-ROM found by Sardelli, who reported
219 a functional ROM between -65° ± 8° pronation and 77° ± 13° supination [34].

220 In this study we found that overall peak FE moments and VV moments were higher
221 compared to the peak PS moments. Therefore, the focus in preventing overload should probably
222 be on reducing elbow moments, mainly in the FE and VV directions. The high VV-moments

223 found, especially during rising from a chair and steering a car, are likely due to the combination
224 of large external reaction forces and a relatively large moment arm.

225 Although no other study examined ADL tasks in all three directions, results of previous
226 research on FE and PS moments are comparable to our findings. For instance, the task
227 performed by Murray et al showed the same order of magnitude as those of our study, although
228 we used a 1-kg object compared to Murray's 0.5-kg object, resulting in higher FE moments
229 [23]. To illustrate: during the lifting task, Murray et al found a maximum FE moment of 5.8
230 Nm during the lifting of a block (~0.5 kg) to head height, while in our study, where the object
231 was placed at shoulder height, a flexion moment of 6.4 Nm was required. The results of Cheng
232 et al were comparable to ours, although they found higher moments in tasks where they used a
233 2-kg object compared to our results, where a 1-kg object was used [3].

234 For all participants, the highest peak moments, in FE direction, were achieved during
235 the rising phase of the chair task. The lowest elbow joint moments were observed during the
236 slide task. King et al showed that the amount of shoulder abduction affects the joint loading of
237 the elbow [15]. The variation in elbow moment is surprisingly low in the slide task compared
238 to the lifting and cup tasks (which show the same FE-ROM). This may indicate that all
239 participants used the same movement strategy during the slide task, which is initiated from the
240 shoulder. More research is needed to elucidate whether shoulder moments could partially
241 relieve elbow joint loading during selected tasks.

242 Altogether, the chair, door, and car tasks showed the highest risk of wear because of the
243 higher observed external reaction forces resulting from pushing and pulling. These findings
244 question whether the focus of the instruction should be on lifting an object ("not lifting 1 kg")
245 or on the presence of external reaction force, i.e., the amount of force required for a pulling or
246 pushing movement.

247

248 *Instruction*

249 No overall main effect of instruction was found; however, the p-value was low ($p = .15$).
250 The results show that the effect of the instruction is dependent on the tasks. During the chair
251 task a significant change was found after the instruction in FE moments (13.4 Nm to 10.3 Nm)
252 and VV moments (15.2 Nm to 11.1 Nm). This was the consequence of less pushing force against
253 the armrest, possibly combined with a greater leg pushing force.

254 Contrary to our expectations, during the door and lift tasks unexpected higher peak
255 flexion moments were found during the instructed condition, with a change in the minimal FE
256 angle during the door task (figure 3A). However, this kinematic change did not lead to a
257 significant decrease in elbow joint moments. This finding questions whether people can
258 accurately predict which changes in movement will lead to lower loads in the elbow.

259

260 *Implications for implant failure:*

261 Finite element studies indicated that VV moments of 5 Nm at the ulnohumeral joint
262 would possibly exceed the yield strength of PE. Surprisingly, the overall mean of the VV
263 moments found in this study (7.9 Nm) exceeded these failure limits, leading to permanent
264 deformation of the PE material. Moreover, during five (car, door, chair, lift, cup) of the eight
265 tasks, even higher external VV moments were observed (Table III).

266 Besides the loading, task frequency also plays an essential role in the risk of PE wear.
267 Many repetitions of a movement lead to erosion of the material. The frequency of the FE
268 movement associated with normal ADL is estimated to be 0.5 million cycles/year, while for
269 strenuous ADL with a significant weight in hand the frequency is approximately 7500
270 cycles/year [30]. It is therefore important to remember that there is not one specific
271 limit/threshold on whether a task can be performed, as it is also important to consider the
272 frequency of the task.

273

274 *Recommendation for clinical practice*

275 So far, it is known that high elbow loads lead to PE wear, which ultimately causes
276 permanent deformation of the prosthetic PE material. Based on the results of the current study,
277 we can now give a better indication of which tasks are more demanding. First, frequent
278 repetition of heavy tasks with a large amount of external load should be avoided or performed
279 differently than before the operation, for example rising from a chair without using the armrest
280 instead of pushing with whole-body weight. Hence external loads are not only the loads
281 resulting from lifting an object (i.e., a heavy book or groceries), but also from the reaction force
282 on the object. Plus, tasks further away from the body with an outstretched arm (e.g., reaching)
283 are more demanding than tasks closer to the body [20].

284

285 *Limitations and Future directions*

286 The musculoskeletal model used in the current study was based on a single cadaver
287 specimen. Individual differences could have led to soft-tissue artifacts or incorrectly-defined
288 joint centers in marker-scaled models, affecting the inverse dynamics results [10]. However,
289 the elbow axes and kinematics were defined in accordance with the ISB recommendations [40]
290 and therefore the effect of individual differences is subsequent to the correct anatomical
291 behavior. Future research could further investigate the effect of individual morphological
292 differences on the inverse dynamics estimations.

293 Second, although healthy participants were examined in this study, it is possible that
294 elbow motions following TEA are changed due to altered motion pathways (i.e., rotation axis),
295 proprioception, and muscle forces [2]. Future research should examine the changes in elbow
296 joint moments in TEA patients and incorporate the changes in prosthesis kinematics into the
297 musculoskeletal model. Computed tomography scans, combined with artificial intelligence

298 technology, have already been used to measure muscle elongations for different implants,
299 positions, and patient anatomies, and can therefore be used to personalize the model [28].

300 Last, we do not know if the observed elbow loads of the current study lead to failure of
301 the material of the elbow prosthesis. So far, we could only compare one feature of the elbow
302 load (VV moments) to the reported failure, i.e. permanent deformation and limits of the PE
303 material of one specific elbow prosthesis. Besides, different types of prostheses may have
304 different failure mechanisms and limits [39]. To compare the in vivo elbow load to the loads
305 that exceed the failure limits of the prosthetic material, future research should focus on failure
306 limits and elbow joint load in both elbow joint moments and internal bone-on-bone contact
307 forces [20].

308

309 **Conclusion**

310 Results of the current study provide insight into elbow joint loading during ADL tasks.
311 Tasks that include pushing and pulling result in higher joint loads, especially in the FE and VV
312 direction. Surprisingly, the VV moments found in this study exceeded the failure limits, leading
313 to permanent deformation of the prosthetic material. The current found joint moments could
314 provide a loading range for in-vitro testing of prostheses during the design stage. To avoid
315 overloading the elbow prosthesis, the current postoperative instruction does not appear to be
316 sufficient. The outcomes of this study can be used as a first step in formulating evidence-based
317 and specific instruction. However, bone-on-bone contact forces and elbow joint moments (VV,
318 PS, and FE direction) in both healthy adults and patients following TEA need to be further
319 analyzed to draw more definitive conclusions on elbow joint loading in ADL.

320

321

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456 **Appendix**

457 Appendix A: Marker position for 3D marker tracking.

Type	Segment	Location on body
Rigid body	Sternum	Jugular incision
Virtual marker	Xiphoid process	Xiphoid process
Virtual marker	Clavicle	Incisura jugularis
Single body + virtual marker	C7 vertebra	Spinal process of C7 vertebra
Single body + virtual marker	Non-dominant shoulder	Acromion
Rigid body	Right upper arm	Lateral upper right arm, 1/4 on the line between acromion and lateral epicondyle of humerus
Virtual marker	Right elbow lateral	Lateral epicondyle of humerus
Virtual marker	Right elbow medial	Medial epicondyle of humerus
Rigid body	Right forearm	Lower lateral surface of right forearm, one finger width proximal of styloid process of the radius and ulna
Single body + virtual marker	Right wrist ulnar	Styloid process of ulna (opposite each other!)
Single body + virtual marker	Right wrist radial	Styloid process of radius
Rigid body + virtual marker	3 rd MCP of finger	3 rd MCP of hand
Virtual marker	5 th MCP of finger	5 th MCP of hand
Rigid body	Sacrum	Sacrum
Virtual marker	Right posterior superior iliac	Right posterior superior spine of ilium
Virtual marker	Left posterior superior iliac	Left posterior superior spine of ilium
Virtual marker	Right anterior superior iliac	Right anterior superior spine of ilium

Virtual marker	Left anterior superior iliac	Left anterior superior spine of ilium
Virtual marker	T10 vertebra	Spinal process of T10 vertebra
Rigid body + virtual marker	Right shoulder	Dominant acromion
virtual marker	Right shoulder	Acromion angle
virtual marker	Right shoulder	Inferior angle
virtual marker	Right shoulder	Trigonum spinae
virtual marker	Right shoulder	Coracoid process
virtual marker	Right shoulder	AC most dorsal point
	1-kg object – Force transducer	Center of rotation (UP steering, SIDE door)

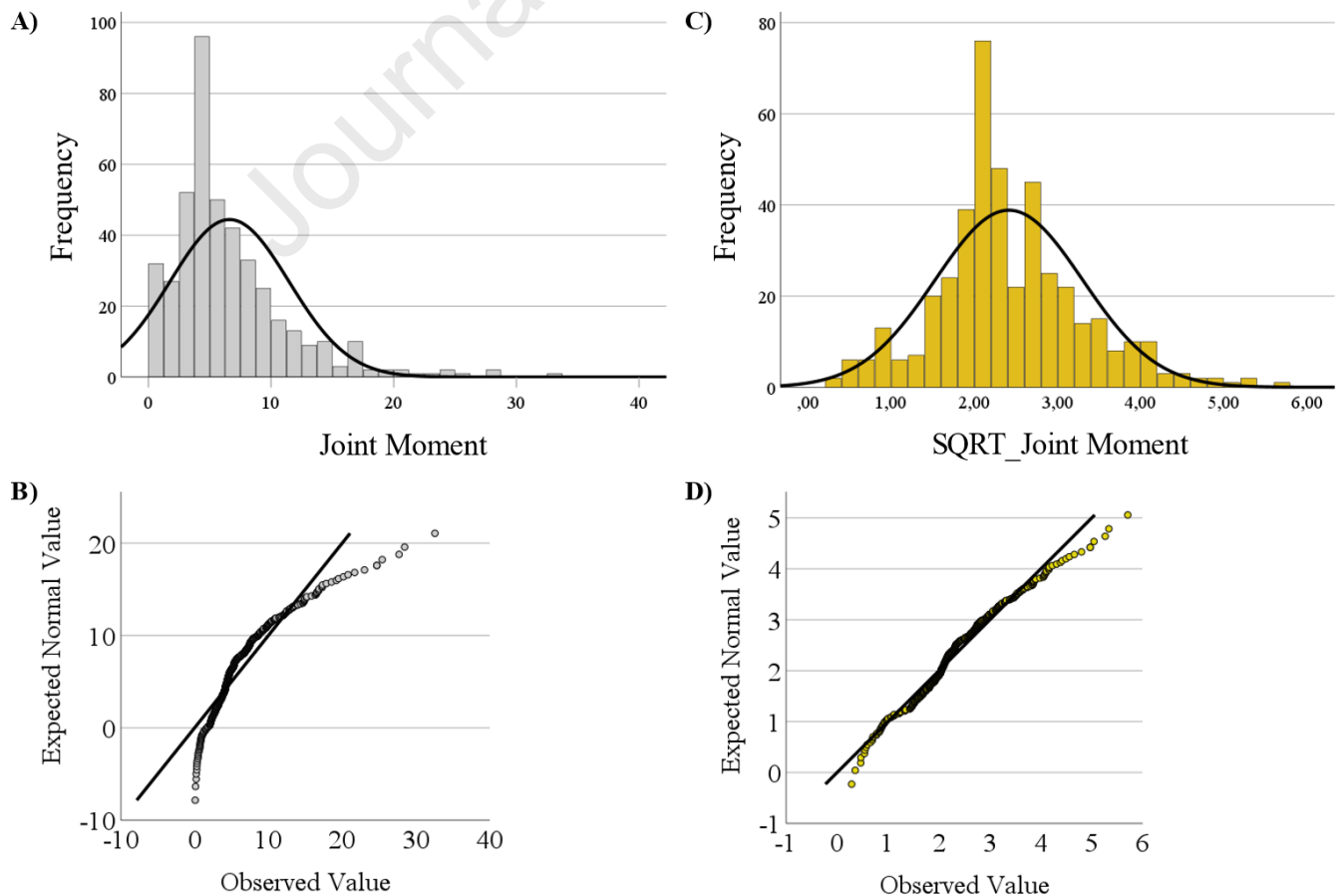
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459 APPENDIX B:

460 Distribution of joint moments before (A and B) and after (C and D) square root

461 transformation. Before the square root transformation, the histogram does not match with the

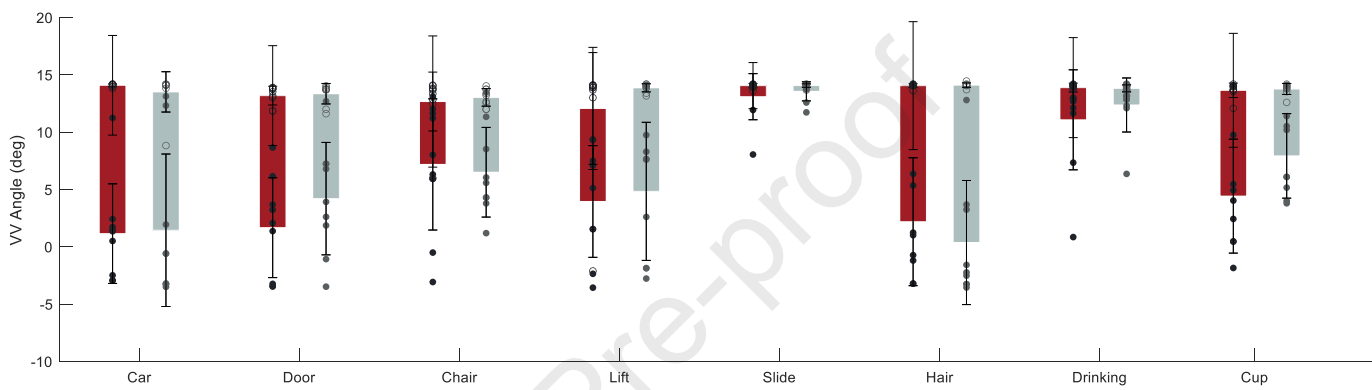
462 normal curve.



463

464 APPENDIX C:

465 Average (N=9) range of motion in varus-valgus direction for eight simulated activities of
 466 daily living. Negative angle is in the varus direction and positive angle is in the valgus
 467 direction. Without instruction (red) and with instruction (grey) of not lifting more than 1 kg.
 468 Dots represent minimal individual angles (filled) and maximal angles (empty). Angle in
 469 degrees. Error bars represent the standard error for the maximum angle (upper end) and
 470 minimal angle (lower end).



471

472 **Figures and Tables**473 **Table I:** Participant demographics mean +/- SD474 ^a Measured from acromion- acromion.475 ^b Measured from dominant acromion to 3 red MCP of dominant arm.476 ^c Handedness was analysed using the Edinburgh inventory (Oldfield et al 1971).

477

478 **Figure 1:** Research protocol. Each symbol illustrates an ADL task. Participants first
479 performed a series of eight ADL tasks. Next, there was the instruction of “not lifting more
480 than 1 kg”. Then the second series was performed. The instruction was repeated before each
481 task.

482

483 **Table II:** Description of activities of daily living and order of execution.

484 Note: AL: arm length, measured from acromion to 3rd MCP of the dominant hand. SW:
485 shoulder width, measured acromion-to-acromion, SH: shoulder height, SP: starting point. The
486 T-bar is an aluminum bar connected to the force transducer. Each activity was repeated 5
487 times, all within 35 seconds.

488

489 **Figure 2:** Schematic overview of experimental set-up for car task with the force transducer
490 (15 N resistance force). (A) sagittal view of the lab setting. (B) view of the geometry of the
491 musculoskeletal model. (C) view during the car task. The markers are in pink, the muscles in
492 red, the green arrow represents the external reaction force (force from T-bar to hand).

493

494 **Figure 3:** Average (N=9) range of motion in (A) flexion-extension (0° is fully extended) and
495 (B) pronation-supination (90° is fully pronated). direction for eight simulated activities of
496 daily living. Without instruction (red) and with instruction (grey) of not lifting more than 1
497 kg. Dots represent minimal individual angles (filled) and maximal angles (empty). Angle in
498 degrees. Error bars represent the standard error for the maximum angle (upper end) and
499 minimal angle (lower end).

500

501 **Figure 4:** Average (N=9) (dark) and individual (light) normalized elbow joint moment for the
502 selected ADL tasks (one of 5 repetitions). Red: uninstructed condition, blue: instructed
503 condition. (A) Elbow joint FE moment. Negative values indicate extension moment, positive
504 values flexion moment. (B) Elbow joint PS moment. Negative values indicate supination
505 moment, positive values pronation moment. (C) Elbow joint VV moments. Negative values

506 indicate varus, positive values valgus. One of 5 repetitions of every task was normalized over
507 time.

508

509 **Table III:** Peak elbow joint moments (N=9) in an uninstructed and instructed condition for
510 eight simulated activities of daily living

511 ^a Peak flexion and extension elbow joint moment for instructed and uninstructed task in Nm,
512 negative value indicates extension, positive flexion.

513 ^b Peak pronation and supination elbow joint moment in Nm for the instructed and uninstructed
514 task. A positive value indicates a pronation moment, a negative value indicates a supination
515 moment.

516 ^c Peak varus and valgus elbow joint moment in Nm for the instructed and uninstructed task, a
517 positive value indicates a varus moment, a negative value indicates a valgus moment.

518

519 **Table IV:** Ranking for each tasks based on joint moments and external force

520 Note: Lower values indicate a higher risk of polyethylene wear.

521 ^a Elbow joint moments in flexion-extension (FE), pronation-supination (PS), and varus-valgus
522 (VV) direction, ranked from high to low, higher joint moments indicate a higher risk of
523 polyethylene wear.

524 ^b Total external reaction force, calculated with output force transducer or gravitational/friction
525 force. Higher external load indicates a higher risk of PE wear.









526

527 **Table V:** Statistical outcomes of the linear mixed models. Joint moments were compared
528 between different tasks, directions, and conditions

529 Note: p -value $< .01$ was considered as statically significant; df = degrees of freedom.

		N	Mean	SD
Age (years)		9	45.8	17.4
Height (cm)		9	178	7.4
Weight (kg)		9	74.9	5.4
Shoulder width (cm) ^a		9	44.4	2.1
Arm length (cm) ^b		9	65.9	2.8
Gender	Male	3		
	Female	6		
Dominance (%) ^c	Right	8	86.1	12.4
	Left	1	-90	

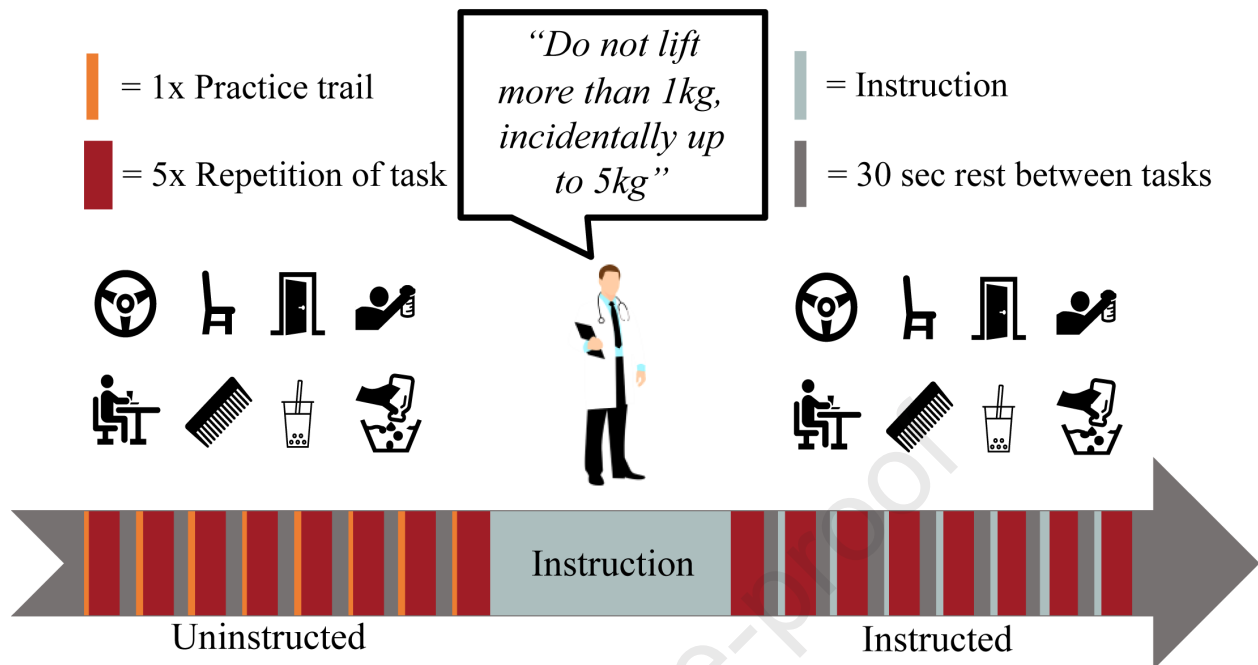
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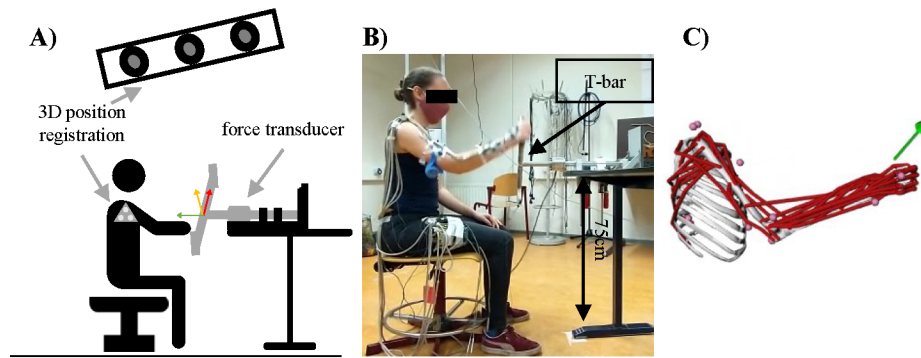
	Activity	Initial position	Aim
	1. Steering a car wheel (T-bar horizontal on the table).	Table placed in front of participant, at 1 AL. Chair is lowered, legs stretched. Dominant hand on T-bar, non-dominant hand on the leg.	Turn T-bar, using the handle, from 10 o'clock to 4 o'clock and turn it back to 10 o'clock.
	2. Opening and closing a door (T-bar vertical on the table).	Participant stands in front of the door, with elbow at 90°, hand resting on the handle.	Push T-bar to 90° using the handle. Close the door, back to starting position.
	3. Rising from a chair (T-bar in armrest).	Seated, both hands on armrests.	Rise from the chair using armrests, sit down again.
	4. Lifting 1-kg object	Target X on the platform (SH) placed 1 AL and 1 SW from dominant arm. Hold 1-kg object at SP.	SP, place object at target X, back to SP.
	5. Sliding 1-kg object	Target X at 1 SW on the non-dominant side, 1 AL with the dominant arm. Hold 1-kg object at SP.	SP, slide target to target X, and back to SP.
	6. Combing hair	Rest a hand on SP.	SP, combing hair in the midline back and forth, SP.
	7. Drinking (1 kg)	Hold 1-kg object at SP.	SP, simulate drinking, SP.
	8. Emptying a cup (1 kg)	Target one full AL in front of participant. Hold 1-kg object at SP.	SP, stretch arm toward target, 180° rotation counterclockwise, then back, SP.

Task	FE-Moment (Nm) ^a				PS-Moment (Nm) ^b				VV-Moment (Nm) ^c			
	Extension (-)		Flexion (+)		Pronation(+)		Supination(-)		Varus(+)		Valgus(-)	
	Uninst(SD)	Inst(SD)	Uninst(SD)	Inst(SD)	Uninst(SD)	Inst(SD)	Uninst(SD)	Inst(SD)	Uninst(SD)	Inst(SD)	Uninst(SD)	Inst(SD)
1. Steering a car wheel	-8.6(4)	-9.3(4)	9.1(2)	8.5(2)	2.5(2)	3.3(3)	-4.8(3)	-5.4(4)	8.1(3)	8.0(3)	-14.2(4)	-15.2(6)
2. Opening and closing a door	-4.1(4)	-3.7(5)	7.2(2)	8.1(2)	1.8(1)	2.1(2)	-3.1(2)	-1.8(2)	7.7(2)	7.8(2)	-10.2(2)	-11.0(4)
3. Rising from chair	-13.4 (6)	-10.3(7)	6.4(3)	3.1(2)	1.3(1)	0.6(1)	-5.0(3)	-3.4(2)	15.2(10)	11.1(6)	-5.6(3)	-3.0(1)
4. Lifting 1-kg object	-	-	7.5(2)	7.7(2)	2.7(1)	1.1(2)	-0.1(2)	-1.6(2)	-	-	-5.2(1)	-5.3(1)
5. Sliding 1-kg object	-	-	4.2(1)	4.3(1)	0.4(2)	-	-1.7(3)	-1.4(2)	-	-	-2.6(1)	-2.6(1)
6. Combing hair	-3.2(1)	-3.2(1)	5.6(1)	5.2(3)	1.5(2)	1.4(3)	-2.0(3)	-1.6(3)	0.4(1)	0.1(1)	-4.2(1)	-4.2(2)
7. Drinking	-0.3(2)	-0.6(3)	8.4(2)	7.7(3)	1.7(2)	0.9(2)	-0.6(2)	-0.9(2)	-	-	-4.4(1)	-4.3(2)
8. Emptying cup	-1.3(3)	-	8.0(2)	7.7(2)	1.8(2)	1.9(2)	-2.6(2)	-2.6(2)	-	-	-7.8(1)	-7.7(1)

Task	FE Moments ^a	PS Moments ^a	VV Moments ^a	External load ^b	Overall total
1. Steering a car wheel	2	1	1	2	6
3. Rising from chair	1	2	2	1	6
2. Opening and closing a door	3	3	3	3	12
8. Emptying cup	5	4	4	4	17
7. Drinking	4	7	6	4	21
4. Lifting 1-kg object	6	6	5	4	21
6. Combing hair	7	5	7	8	27
5. Sliding 1-kg object	8	8	8	7	31

	df	F	P
Tasks	7	40.44	< .001
Direction	2	170.02	< .001
Condition	1	2.07	0.151
Direction * Condition	2	0.08	0.992
Condition * Tasks	7	3.04	< .001
Task * Direction	14	6.29	< .001
Tasks * Direction * Condition	14	0.31	0.993





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