

1 **Title**

2 Concurrent Validity and Reliability of a Semi-automated Approach to Measuring the Magnetic
3 Resonance Imaging Morphology of the Knee Joint in Active Youth

4
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1 **ABSTRACT**

2 Post-traumatic knee osteoarthritis is attributed to alterations in joint morphology, alignment, and
3 biomechanics triggered by injury. While magnetic resonance (MR) imaging-based measures of
4 joint morphology and alignment are relevant to understanding osteoarthritis risk, time consuming
5 manual data extraction and measurement limit the number of outcomes that can be considered
6 and deter widespread use. This paper describes the development and evaluation of a semi-
7 automated software for measuring tibiofemoral and patellofemoral joint architecture using MR
8 images from youth with and without a previous sport-related knee injury. After prompting users
9 to identify and select key anatomical landmarks, the software can calculate 37 (14 tibiofemoral,
10 23 patellofemoral) relevant geometric features (morphology and alignment) based on established
11 methods. To assess validity and reliability, 11 common geometric features were calculated from
12 the knee MR images (proton density and proton density fat saturation sequences; 1.5 Tesla) of 76
13 individuals with a 3–10-year history of youth sport-related knee injury and 76 uninjured controls.
14 Spearman’s or Pearson’s correlation coefficients (95% CI) and Bland-Altman plots were used to
15 assess the concurrent validity of the semi-automated software (novice rater) versus expert
16 manual measurements, while intra-class correlation coefficients (ICC_{2,1}; 95% CI), standard error
17 of measurement (95% CI), 95% minimal detectable change, and Bland-Altman plots were used to
18 assess the inter-rater reliability of the semi-automated software (novice versus resident
19 radiologist rater). Correlation coefficients ranged between 0.89 (0.84,0.92; Lateral Trochlear
20 Inclination) and 0.97 (0.96,0.98; Patellar Tilt Angle). ICC estimates ranged between 0.79
21 (0.63,0.88; Lateral Patellar Tilt Angle) and 0.98 (0.95,0.99; Bisect Offset). Bland-Altman plots
22 did not reveal systematic bias. These measurement properties estimates are equal, if not better
23 than previously reported methods suggesting that this novel semi-automated software is an
24 accurate, reliable, and efficient alternative method for measuring large numbers of geometric
25 features of the tibiofemoral and patellofemoral joints from MR studies.

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27 **Keywords:** Alignment, Biomechanics, Morphology, MRI, Patellofemoral, Tibiofemoral,

28 MATLAB

1 **INTRODUCTION**

2 Youth who suffer a sport-related knee injury are at increased risk of developing symptomatic
3 radiographic knee osteoarthritis.^{1,2} Alongside the inflammatory response to injury, it is
4 hypothesized that one of the contributing mechanisms underlying the elevated risk of post-
5 traumatic osteoarthritis are alterations in tibiofemoral and patellofemoral joint bone shape (i.e.,
6 morphology), alignment and subsequent biomechanics precipitated by injury.³

7
8 Knee joint geometry are commonly quantified as distances, angles and ratios measured from
9 Magnetic Resonance (MR) images.⁴ Traditionally, geometric values are manually generated by
10 an experienced rater with extensive knowledge of anatomy, radiology, and data manipulation,
11 using a Digital Imaging and Communications in Medicine (DICOM) image file viewing
12 application with measurement abilities.^{5,6} This resource intensive and time-consuming approach
13 restricts the types of geometric measurements that can be assessed (i.e., DICOM applications
14 typically only measure distances and angles), is prone to data transcription errors when data are
15 extracted for post-processing, and limits the number of measurements that can be assessed in
16 large MR datasets.

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18 A purpose built, user-friendly, semi-automated software for quantifying knee joint geometries,
19 that houses both measurement and post-processing functionalities could overcome the limitations
20 of the traditional manual approach to obtaining knee joint geometric measurements. A semi-
21 automated approach could also contribute to efforts to standardize how knee joint geometric
22 outcomes are named and quantified across studies, and homogenize MR image slice selection
23 and anatomical landmarks.^{7,8,9} On top of being faster, less prone to error due to data
24 manipulation, and standardizing measurements to enable data synthesis, a semi-automated
25 software could also enable less-experienced raters to perform accurate and reliable
26 measurements if it incorporated clear instructions. The objective of this research was to develop
27 a semi-automated software to quantify relevant tibiofemoral and patellofemoral geometric
28 measurements from MR images, and to assess the software's inter-rater reliability and concurrent
29 validity to a traditional manual approach using MR images of youth with and without a previous
30 sport-related knee injury.

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1 **METHODS**

2 **Identification of Geometric Parameters**

3 All knee joint geometric features potentially relevant to knee injury and osteoarthritis were
4 identified from existing systematic reviews and relevant studies.^{6, 7, 8, 9, 10, 11, 12, 13, 14, 15} This list
5 was narrowed to 37 parameters (14 tibiofemoral, 23 patellofemoral) based on discussions with an
6 experienced rater (EM) and a musculoskeletal fellowship trained radiologist with more than 15
7 years of imaging experience (JJ), who informed the design of the custom-built software. The
8 selected measures have all been previously reported and used to quantify MRI knee joint
9 geometries in studies that assess the relationship between knee joint geometry and MRI features
10 (e.g., cartilage damage or bone marrow lesions) or clinical outcomes (e.g., injury, osteoarthritis,
11 pain). As we narrowed down the list of candidate measures for this study, we placed emphasis on
12 measurements that have been shown to statistically differ between groups or conditions, as well
13 as commonly used measurements that have appeared across multiple studies. As part of the
14 selection process, the established methods for calculating the geometric features (exclusively
15 distances, angles, and ratios) were extracted. Table 1 and 2 summarizes the tibiofemoral and
16 patellofemoral features, respectively.

17

18 **Table 1. Tibiofemoral Geometric Features Calculated by the Semi-automated Software**

Outcome	Description	Reference points on Figures 2-4	MRI Slice (if applicable)
Tibiofemoral Angle	Angle formed by line bisecting femoral shaft and line bisecting tibial shaft	Angle between C17 → C18 and C20 → C19	Midline coronal slice ¹
Tibial Slope	Angle between a line perpendicular to the bisecting tibial axis and a line connecting the lateral and medial tibial plateau (<i>A negative value indicates the medial side of the plateau is more proximal than the lateral</i>).	Angle between C9 → C10 and C9 → C21	Midline coronal slice ¹
Medial Tibial Slope	Angle between the medial tibial slope and line perpendicular to the tibial bisecting axis (<i>Negative value = the anterior point of the medial tibial slope is more proximal than the posterior</i>).	Medial: Angle between B10 → B11 and B10 → B20	Midline coronal slice ¹
Lateral Tibial Slope	Angle between the lateral tibial slope and line perpendicular to tibial bisecting axis (<i>Negative value = the anterior point of the lateral tibial slope is more proximal than the posterior</i>).	Lateral: Angle between B10 → B11 and B10 → B20*	Midline coronal slice ¹
Intercondylar Notch Width	Distance from the most medial point of the intercondylar notch to the most lateral	C15 → C16	Slice with the most-pronounced popliteal groove ²

Bicondylar Width	Distance from the most lateral point of the lateral femoral condyle to the most medial point of the medial femoral condyle	C11 → C12	Slice with the most-pronounced popliteal groove ²
Medial Condylar Width	Distance from the most medial/lateral point of the medial femoral condyle to the medial side of the intercondylar notch	C12 → C18	Slice with the most-pronounced popliteal groove ²
Lateral Condylar Width	Distance from the most medial/lateral point of the lateral femoral condyle to the lateral side of the intercondylar notch	C11 → C15	Slice with the most-pronounced popliteal groove ²
Medial Compartment Ratio	Ratio of medial femoral condylar width and medial tibial plateau width	Medial: (B13 → B12)/(B10 → B11)	Slice with the most-pronounced popliteal groove ²
Lateral Compartment Ratio	Ratio of lateral femoral condylar width and lateral tibial plateau width	Lateral: (B13 → B12)/(B10 → B11)	Slice with the most-pronounced popliteal groove ²
Medial Plateau Concavity	Ratio of medial tibial plateau depth (<i>line perpendicular to a line that connects the anterior and posterior points of the medial tibial plateau and runs through the deepest point of the medial tibial plateau</i>) and the medial tibial plateau length	Medial: (B14 → B18)/(B10 → B11)	Midline coronal slice ¹
Lateral Plateau Convexity	Ratio of lateral tibial plateau height (<i>line perpendicular to a line that connects the anterior and posterior points of the lateral tibial plateau and runs through the highest point of the lateral tibial plateau</i>) and the lateral tibial plateau length	Lateral: (B14 → B18)/(B10 → B11)	Midline coronal slice ¹
Medial Condylar Convexity	Ratio of the medial condylar width and a line perpendicular to the line that runs through the most anterior and posterior points of the medial femoral condyle and runs through the deepest point of the medial femoral condyle	Medial: (B15 → B19)/(B12 → B13)	Midline coronal slice ¹
Lateral Condylar Convexity	Ratio of the lateral condylar width and a line perpendicular to the line that runs through the most anterior and posterior points of the lateral femoral condyle and runs through the deepest point of the lateral femoral condyle	Lateral: (B15 → B19)/(B12 → B13)	Midline coronal slice ¹

1 ¹MRI slice located halfway between the most posterior slice containing the tibia and femur, and the slice containing the most posterior aspect of the patella.

2 ²The most-pronounced popliteal slice is the MRI slice where the patellar groove has the greatest area and extends the furthest medially.

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6 **Table 2. Patellofemoral Geometric Features Calculated by the Semi-automated Software**

Outcome	Description	Reference points on Figures 2-4	MRI Slice (as applicable)
Insall-Salvati Ratio	Ratio of the distance from the patellar tendon tibial attachment to the most distal point of the patella, and the distance line connecting the most proximal point of the patella and the most distal.	(B6 → B7)/ (B5 → B6)	Midline patellar sagittal slice ¹
Modified Insall-Salvati Ratio	Ratio of the distance from the patellar tendon tibial attachment to the most distal point of the patellar articular surface, and the distance line connecting	(B9 → B7)/ (B8 → B9)	Midline patellar sagittal slice ¹

	the most proximal point of the patellar articular surface and the most distal.		
Blackburne-Peel Index	Ratio of the distance between the distal and proximal points of the patellar articular surface, and the distance between the distal point of the patellar articular surface and a point created from a line that is perpendicular to the medial tibial slope line, that also runs through the distal point of the patellar articular surface.	(B8 → B9)/ (B9 → B21)	Midline patellar sagittal slice ¹
Caton-Deschamps Index	Ratio of the distance between the distal and proximal points of the patellar articular surface, and the distance between the distal point of the patellar articular surface and the anterior point of the medial tibial plateau	(B8 → B9)/ (B9 → B10)	Midline patellar sagittal slice ¹
Lateral Displacement 1	Percent of patellar length that lies lateral to the anterior point of the lateral femoral trochlea	(A6 → A18)/ (A6 → A7)*100	Slice with greatest mediolateral patellar diameter ²
Lateral Displacement 2	Distance between a line perpendicular to the posterior condylar line and a line that runs through the most anterior point of the medial femoral trochlea and the most medial point of the patella	A7 → A20	Slice with greatest mediolateral patellar diameter ²
Bisect Offset	Percent of the patella length that lies lateral to the line perpendicular to the posterior condylar line that runs through the deepest point of the trochlea	(A6 → A14)/ (A7 → A14)*100	Slice with greatest mediolateral patellar diameter ²
Medial Trochlear Inclination Angle	Angle between the posterior condylar line and the medial trochlea	Angle between A3 → A4 and A5 → A1	Femoral condylar slice ³
Lateral Trochlear Inclination Angle 1	Angle between the posterior condylar line and the lateral trochlea	Angle between A3 → A4 and A5 → A2	Femoral condylar slice ³
Lateral Trochlear Inclination Angle 2	Angle between the posterior condylar line and the lateral trochlea	Angle between A3 → A4 and A5 → A2	Most proximal axial slice showing complete cartilage coverage of the trochlea
Lateral Patellofemoral Angle	Angle between the anterior condylar line and the lateral articular surface of the patella (<i>Negative = the most lateral point of the patellar articular surface is posterior to the most medial point of the patellar articular surface</i>)	Angle between A1 → A2 and A9 → A8	Slice with greatest mediolateral patellar diameter ²
Sulcus Angle	Angle between the medial and lateral trochlea	Angle between A5 → A1 and A5 → A1	Femoral condylar slice ³
Trochlear Angle	Angle between the posterior condylar line and anterior condylar line (<i>Negative = the most anterior point of the medial trochlea is anterior to the most anterior point of the lateral trochlea</i>)	Angle between A3 → A4 and A1 → A2	Femoral condylar slice ³

Lateral Patellar Tilt Angle	Angle between the posterior condylar line and the lateral articular surface of the patella (<i>Negative = the most lateral point of the patellar articular surface is posterior to the most medial point of the patellar articular surface</i>)	Angle between A3 → A4 and A9 → A8	Femoral condylar slice ³
Patellar Tilt Angle	Angle between the posterior condylar line and a line that runs through the widest part of the patella (<i>Negative = the lateral point of the patella is anterior to the medial point</i>)	Angle between A3 → A4 and A6 → A7	Slice with greatest mediolateral patellar diameter ²
Tibial Tuberosity to Trochlear Groove Distance (TT-TG)	Distance between the tibial tubercle and the line that is perpendicular to the posterior condylar line that runs through the deepest part of the trochlea	A10 → A15	(1) Femoral condylar slice ³ (2) Most proximal axial slice including the tibial patellar tendon attachment
Trochlear Depth	Average of the distance from the posterior condylar line to the medial and lateral condyles, minus the distance from the deepest point of the trochlea to the posterior condylar line	$((A1 \rightarrow A16) + (A2 \rightarrow A17))/2 - (A5 \rightarrow A18)$	Slice with greatest mediolateral patellar diameter ²
Congruence Angle	Angle between the line that bisects the sulcus angle and a line that connects the deepest part of the trochlea with the most posterior point of the patella	Angle between A3 → A21* and A5 → A11	Femoral condylar slice ³
Patellar Angle	Angle between the medial and lateral patellar articular surfaces	Angle between A11 → A6 and A11 → A6	Slice with greatest mediolateral patellar diameter ²
Trochlear Width	Length of the anterior condylar line	A1 → A2	Femoral condylar slice ³
Axial Engagement Index	Ratio of the patellar width (greatest width) and the trochlear width (greatest width)	$(A6 \rightarrow A7)/(A1 \rightarrow A2)$	(1) Femoral condylar slice ³ (2) Slice with greatest mediolateral patellar diameter ²
Patellar Facet Asymmetry	Ratio of the medial and lateral patellar articular surface lengths	$(A8 \rightarrow A9)/(A12 \rightarrow A13)$	Slice with greatest mediolateral patellar diameter ²
Trochlear Facet Asymmetry	Ratio of the medial and lateral trochlear lengths	$(A5 \rightarrow A1)/(A5 \rightarrow A2)$	Femoral condylar slice ³

1 *Note: Measurements in **Bold font** were used to assess the validity and reliability of the software*

2 ¹The middle MRI slice containing the patella (i.e., total number of MRI slices containing the patella divided by two)

3 ²The axial slice showing the greatest mediolateral patellar diameter

4 ³The axial slice with the most-prominent femoral condyles – the slice showing the greatest area of femoral condyles.

5

6 **Software Development**

7 Matlab (Matlab v. 2019b, MathWorks, USA) was used to develop a custom semi-automated
8 software (<https://bit.ly/KneeMorphSAM>)¹⁶ with a custom graphical user interface (GUI) for use
9 in conjunction with axial, coronal and sagittal proton density and proton density fat saturation
10 sequences, and balanced steady-state gradient echo pulse sequences.

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2 When the user initiates our software, they are prompted to select which of the 37 geometric
3 features they want to measure (i.e., all features, a subset of features, or an individual feature). As
4 geometric measurements of the knee are taken from individual MR image slices extracted from
5 MR sequences based on the presence of unique anatomical landmarks, users are prompted
6 through an anatomical point selection process of key morphological landmarks in the MR
7 sequences. For example, to select the appropriate midline axial slice (a common slice used across
8 multiple measurements), the user is prompted to identify both the most posterior slice containing
9 the tibia and femur, and the slice containing the most posterior aspect of the patella. Using this
10 information, the software then calculates and displays the exact slice representative of the
11 halfway point. While the software recommends the use of the displayed slice, the user has the
12 option to override the software if they believe the slice is not an accurate representation of the
13 slice in question, if there are resolution errors, or if slice mal alignment is present due to
14 technologist errors and variability. The anatomical point selection process is customized to
15 include only points and relevant MR sequences (e.g., frontal, sagittal and axial) required to
16 calculate the relevant geometric features (Tables 1 and 2, Figures 2, 3 and 4). To assist novice
17 users and facilitate standardization, the GUI provides detailed instructions to guide users as the
18 identify anatomical points. These instructions were developed with access to the source
19 publications. To help orientate the user, the main GUI window includes composite images which
20 overlay the selected MR sequence for conceptual visualization of the knee joint (Figure 1). The
21 GUI also has tools to adjust MR image brightness and contrast, add overlaying gridlines, and
22 zoom features. If the MR study does not include an axial sequence the software has an option to
23 generate an axial sequence based on a reformat of available high resolution minimal slice
24 thickness sagittal sequences.

25
26 PLACE FIGURE 1 HERE
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28 Once anatomical point selection is complete, the software calculates the selected distance, angle
29 and ratio geometric features using cartesian plane methods (Tables 1 and 2).^{6, 7, 8, 9, 10, 11, 12, 13, 14, 15}
30 The features and their values are then summarized and can be exported as an Excel spreadsheet
31 (Microsoft Corporation, Redmond, WA). A detailed standard operating procedure

1 (<https://bit.ly/KneeMorphSAM>)¹⁶ was also developed to guide users and describe all
2 functionalities of the software application.

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PLACE FIGURE 2 HERE

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10 **Software Evaluation**

11 **Participants:** Participants included a sub-sample of the Alberta Youth Prevention of Early-
12 Osteoarthritis (PrE-OA) cohort study with sagittal 3D gradient echo FIESTA MR sequences
13 (repetition time 10.5 ms, echo time 4.2 ms, slice thickness 1.0 mm, flip angle 55°, matrix
14 512x512; 1.5 Tesla). This included 76 youth who experienced a sport-related intra-articular knee
15 injury 3-10 years prior to undergoing MR images, and 76 uninjured controls of similar age, sex
16 and sporting history.¹⁷ Balanced steady-state gradient echo pulse sequences (FIESTA MR
17 sequences) were used for the present study because the slice thickness was smaller in comparison
18 to other sequences obtained in the parent PrE-OA study, and the pixel resolution was higher and
19 isotropic, allowing for high quality axial image reformatting. Information regarding participant
20 recruitment and eligibility for the PrE-OA cohort study is detailed elsewhere.¹⁸ Ethics approval
21 was granted by the local Conjoint Health Research Ethics Board (CHREB, ETHICS ID # E-
22 25075).

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Procedures: A sub-set of 11 of the 37 features was selected to assess the software performance
due to time and resource restraints associated with manual measurements. These 11 features
(Table 2) encompass distances, angles, and ratios, and were selected, based on their expected
relevance to the current cohort (i.e., youth with and without a knee injury).^{4, 5, 7, 15} Given that all
37 measures are performed and calculated with similar procedures for identifying anatomical
landmarks on MR images, there is no reason to believe the performance of the software would
differ for the remaining 26 features.

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1 Knee geometric measurements were assessed by three unique blinded raters. First, a novice rater
2 (Rater 1) used the semi-automated software to measure the subset of 11 geometric features
3 across all 152 participants. Second, a rater with nine years' experience (Rater 2) used an
4 established manual method in conjunction with OsiriX Lite 10.0 (Pixmeo SARL, Switzerland) to
5 estimate the same 11 geometric features across all 152 participants. Finally, a radiologist resident
6 (Rater 3) used the semi-automated software to estimate the 11 geometric features in a subset of
7 30 participants. These measurements were used to estimate concurrent validity (semi-automated
8 software, Rater 1 vs. manual measurement, Rater 2) and inter-rater reliability (Rater 1 vs. Rater
9 3, semi-automated software). Rater 1 developed the software, and embedded instructions based
10 on source publications for the established manual method used by Rater 2. Rater 1 had no
11 previous experience using the manual approach to perform the measurements. For this reason, it
12 can be assumed that Raters 1 and 2 differed on level experience but not access to the source
13 publications. Rater 3 only used the instructions embedded in the software and did not have
14 access to the source publications. Rater 3 is a trained radiologist, with experience performing
15 standard measurements on DICOM image viewing applications.

16
17 ***Statistical Analysis:*** Data analyses were performed using Stata Version 14.2 (StataCorp LP,
18 College Station, TX). After assessing the distribution of all measurements by visual inspection
19 and Shapiro-Wilk normality tests, the mean, standard deviation (SD) and minimum and
20 maximum values for all 11 geometric features were calculated and summarized by rater.
21 Levene's test was evaluated to confirm homoscedasticity of samples.¹⁹

22
23 Concurrent validity can be assessed in the absence of a criterion measure or 'gold standard' and
24 is evaluated by comparing two measures on the same construct by different systems at relatively
25 similar times (i.e., concurrently). In the case of the current study we, evaluate the concurrent
26 validity of the newly developed semi-automated in comparison to a traditional manual
27 measurement approach. Similar performance, of the two measurement systems give confidence
28 that this novel method could be used in place of the traditional method, with the additional
29 benefit of being more standardized and taking less time.²⁰ The concurrent validity between the
30 semi-automated software and a traditional manual approach (criterion standard) was assessed
31 with Spearman's or Pearson's correlation coefficients as appropriate, and 95% limits of

1 agreement (mean difference between measurements ± 1.96 SD).^{20, 21} Bland-Altman plots were
 2 also used to assess for systematic bias, outliers, and relationships between the difference in
 3 values of parameters between methods.²² Further, these plots were visually assessed to ensure
 4 homoscedasticity (i.e., heteroscedasticity was considered present if the scatter of values changed
 5 progressively with increasing average values).²⁴ Bland-Altman plots for all reported measures
 6 are presented in Appendix A.

7
 8 Reliability is the extent to which a measurement system is consistent and free from error.²³ Inter-
 9 rater reliability refers to the agreement in measurements between two or more raters.²³ A subset
 10 of 30 studies were used to assess reliability. Agreement between novice and experienced raters
 11 (inter-rater reliability) using the semi-automated software was assessed with Intra-class
 12 Correlation Coefficients (ICC_{2,1}, 95% CI),²³ and measurement precision (Standard Error of
 13 Measurement; SEM; $SD * \sqrt{1 - ICC}$).²³ Model ICC_{2,1} was selected as the three raters in this
 14 study are expected to be representative of larger populations of raters (raters with minimal
 15 radiological experience, and raters with practicing radiologic history).²⁰ Finally, 95% Minimal
 16 Detectable Change (MDC₉₅), which represents the minimal change (in units of parameter) that
 17 must occur to be 95% confident that a true change has occurred, was calculated for each outcome
 18 as $1.96 * SEM * \sqrt{ICC}$ to assist in interpretation.²⁵

19
 20 **RESULTS**

21 The median participant age was 23 years (minimum-maximum 14-27) and 40% were female.
 22 Amongst previously injured participants the median age of injury was 16 years (11-19). The
 23 mean, SD and minimum and maximum values of all 11 geometric features by rater are
 24 summarized in Tables 3 and 4.

25
 26 **Table 3. Geometric Feature Measurements by Rater for Concurrent Validity Comparison**
 27 **(N = 152).**

Outcome	Rater 1¹ Mean±SD (min-max) (N = 152)	Rater 2² Mean±SD (min-max) (N = 152)
Insall-Salvati Ratio	1.1±0.2 (0.7-1.5)	1.1±0.2 (0.7-1.5)
Bisect Offset (%)	54.0±7.2 (37.0-84.4)	54.3±7.1 (37.1-86.4)
Medial Trochlear Inclination Angle (°)	28.6±5.4 (15.3-42.7)	29.6±5.7 (16.4-47.3)

Lateral Trochlear Inclination Angle 1 (°)	26.2±5.2 (14.7-43.4)	27.0±5.6 (12.2-44.4)
Lateral Trochlear Inclination Angle 2 (°)	19.5±5.9 (4.1-32.1)	18.9±6.0 (1.1-33.0)
Sulcus Angle (°)	126.7±9.0 (99.0-149.8)	126.0±9.6 (96.0-153.4)
Trochlear Angle (°)	1.7±2.3 (-4.5-8.7)	1.9±2.5 (-4.1-10.0)
Lateral Patellar Tilt Angle (°)	7.9±5.4 (-8.5-22.8)	8.5±5.6 (-6.3-24.8)
Patellar Tilt Angle (°)	9.3±4.5 (-2.0-19.9)	10.8±5.1 (-2.9-23.0)
TT-TG (mm)	8.6±4.2 (1.0-23.2)	8.0±3.9 (0.5-20.0)
Trochlear Depth (mm)	3.9±1.2 (1.4-8.9)	3.8±1.2 (0.9-8.1)

1 mm = millimeters, SD = standard deviation. TT-TG = Tibial Tuberosity to Trochlear Groove Distance.

2 ¹Novice rater using semi-automatic software method.

3 ²Experienced rater using manual method.

4

5 **Table 4. Geometric Feature Measurements by Rater for Reliability Comparison (N = 30).**

Outcome	Rater 1 ¹ Mean±SD (min-max) (N = 30)	Rater 3 ³ Mean±SD (min-max) (N = 30)
Insall-Salvati Ratio	1.1±0.2 (0.9-1.4)	1.1±0.2 (0.8-1.5)
Bisect Offset (%)	53.0±7.0 (37.0-68.8)	53.3±7.8 (35.7-71.1)
Medial Trochlear Inclination Angle (°)	25.1±5.4 (15.3-37.5)	23.4±5.4 (14.3-35.8)
Lateral Trochlear Inclination Angle 1 (°)	25.4±3.5 (18.9-31.9)	25.1±4.1 (17.3-32.0)
Lateral Trochlear Inclination Angle 2 (°)	18.8±5.4 (7.2-29.7)	18.9±5.9 (4.9-29.0)
Sulcus Angle (°)	129.5±8.5 (115.0-145.5)	130.0±8.4 (114.2-144.3)
Trochlear Angle (°)	2.5±2.3 (-3.8-6.3)	2.4±2.5 (-2.9-9.0)
Lateral Patellar Tilt Angle (°)	8.6±5.1 (-1.7-21.2)	7.2±4.9 (-3.5-16.0)
Patellar Tilt Angle (°)	8.1±5.5 (-2.0-19.9)	7.4±4.8 (-1.2-16.1)
TT-TG (mm)	8.5±3.7 (2.9-15.7)	8.1±4.2 (0.1-15.5)
Trochlear Depth (mm)	4.0±1.1 (1.7-6.1)	4.3±1.2 (2.1-6.9)

6 mm = millimeters, SD = standard deviation. TT-TG = Tibial Tuberosity to Trochlear Groove Distance.

7 ¹Novice rater using semi-automatic software method.

8 ²Radiologist rater using semi-automated software.

9

10 **Concurrent Validity**

11 The correlation and limits of agreement of between values generated by rater 1 using the novel
 12 semi-automated software (target test) and rater 2 using a traditional manual approach are
 13 summarized in Table 4. Pearson Product-Moment Correlation Coefficient (95% CI) was
 14 estimated for normally distributed measurements (i.e., Insall-Salvati Ratio, Medial Trochlear
 15 Inclination, Lateral Trochlear Inclination 2, Sulcus Angle, Trochlear Angle, Lateral Patellar Tilt,
 16 Patellar Tilt), and Spearman Rank Correlation Coefficient for non-normally distributed
 17 measurements (i.e., Bisect Offset, Lateral Trochlear Inclination 1, Tibial Tuberosity to Trochlear

1 Groove Distance (TT-TG), and Trochlear Depth).²¹ Correlation coefficients ranged from 0.89
 2 (Lateral Trochlear Inclination 1) to 0.97 (Patellar Tilt Angle) for angled measurement
 3 measurements, from 0.92 (Insall-Salvati Ratio) to 0.95 (Bisect Offset) for ratio measurements,
 4 and from 0.95 (TT-TG) to 0.96 (Trochlear Depth) for linear distance measurements.

5
 6 Mean differences \pm 2 SD (95% limits of agreement) between rater 1 and 2 ranged from 0.17°
 7 (Trochlear Angle) to 1.44° (Patellar Tilt Angle) for angled measurement measurements, from
 8 0.003 (Bisect Offset) to 0.04 (Insall-Salvati Ratio) for ratio measurements, and from 0.295mm
 9 (Trochlear Depth) to 0.56mm (TT-TG) for linear distance measurements. Bland-Altman plots
 10 did not reveal any major systematic bias or relationships between the difference in magnitude
 11 between rater 1 and 2 and were reviewed to ensure homoscedasticity.

12
 13 **Table 5. Correlation and Agreement between Semi-automatic Software and Manual**
 14 **Approach (Rater 1 vs. 2) to Estimate Concurrent Validity (N = 152).**

Outcome	Pearson, or Spearman Correlation Coefficient (95% CI)	p-value	Mean Difference (95% CI), (LOA)
Insall-Salvati Ratio	0.92 ^a (0.89, 0.94)	< 0.001	0.04 (0.03 0.05), (-0.09, 0.17)
Bisect Offset (%)	0.95 ^b (0.92, 0.96)	< 0.001	0.28% (-0.59 0.04), (-4.21, 3.65)
Medial Trochlear Inclination Angle (°)	0.91 ^a (0.87, 0.93)	< 0.001	-1.02° (-1.41 -0.64), (-5.84, 3.79)
Lateral Trochlear Inclination Angle 1 (°)	0.89 ^b (0.84, 0.92)	< 0.001	0.75° (-1.12 -0.38), (-3.53, 4.30)
Lateral Trochlear Inclination Angle 2 (°)	0.91 ^a (0.88, 0.95)	< 0.001	0.64° (0.24 1.03), (-4.33, 5.60)
Sulcus Angle (°)	0.95. ^a (0.94, 0.97)	< 0.001	0.33° (-0.13 0.79), (-5.46, 6.12)
Trochlear Angle (°)	0.96 ^a (0.95, 0.98)	< 0.001	-0.17° (-0.27 -0.07), (-1.42, 1.08)
Lateral Patellar Tilt Angle (°)	0.95 ^a (0.94, 0.97)	< 0.001	-0.64° (-0.91 -0.37), (-4.04, 2.76)
Patellar Tilt Angle (°)	0.97 ^a (0.96, 0.98)	< 0.001	-1.44° (-1.65 -1.23), (-4.06, 1.18)
TT-TG (mm)	0.95 ^b (0.93, 0.97)	< 0.001	0.56mm (0.36 0.75), (-1.87, 2.93)
Trochlear Depth (mm)	0.96 ^b (0.93, 0.97)	< 0.001	-0.14mm (0.09 0.19), (-0.54, 0.82)

15 LOA = limits of agreement, mm = millimeters, SEM = Standard error of measurement, TT-TG = Tibial Tuberosity
 16 to Trochlear Groove Distance.

17 ^aPearson Correlation Coefficient

18 ^bSpearman Correlation Coefficient

19
 20 **Inter-rater Reliability**

21 Inter-rater reliability (ICC_{2,1} (95% CI)), SEM, MDC₉₅, mean differences and 95% limits of
 22 agreement (\pm 1.96 SD) between rater 1 and 3 using the semi-automated software are summarized
 23 in Table 5. ICC_{2,1} (95% CI) values ranged between 0.79 (95% CI 0.63, 0.88) for Lateral Patellar

1 Tilt Angle and 0.98 (0.95, 0.99) for Bisect Offset. SEM values ranged from 0.783° (Trochlear
 2 Angle) to 3.382° (Sulcus Angle) for angled measurement measurements, from 0.010 (Bisect
 3 Offset) to 0.054 (Insall-Salvati Ratio) for ratio measurements, and from 0.348mm (Trochlear
 4 Depth) to 1.109mm (TT-TG) for linear distance measurements. Bland-Altman plots showed
 5 homoscedasticity and did not reveal any significant systematic bias or relationships between the
 6 differences in magnitude between measurements.

7
 8 **Table 6. Correlation and Agreement between Novel Rater and Radiologist (Rater 1 vs. 3) to**
 9 **Estimate Reliability (N = 30).**

Outcome	ICC _{2,1} (95%CI)	SEM	MDC ₉₅	Mean Difference (95% CI), (LOA)
Insall-Salvati Ratio	0.89 (0.80, 0.94)	0.05	0.15	0.07 (-0.02 0.04), (-0.15, 0.17)
Bisect Offset (%)	0.98 (0.95, 0.99)	1.02%	2.82%	-0.27% (-0.88 0.33), (-3.52, 2.97)
Medial Trochlear Inclination Angle (°)	0.92 (0.86, 0.96)	1.52°	4.20°	1.77° (0.96 2.58), (-2.59, 6.13)
Lateral Trochlear Inclination Angle 1 (°)	0.86 (0.76, 0.93)	1.94°	5.37°	0.38° (-0.35 1.11), (-3.54, 4.30)
Lateral Trochlear Inclination Angle 2 (°)	0.89 (0.81, 0.94)	1.97°	5.46°	-0.04° (-1.02 0.93), (-5.27, 5.18)
Sulcus Angle (°)	0.86 (0.75, 0.92)	3.38°	9.37°	-0.50° (-2.16 1.16), (-9.37, 8.38)
Trochlear Angle (°)	0.90 (0.82, 0.95)	0.78°	2.05°	0.09° (-0.30 0.49), (-2.03, 2.21)
Lateral Patellar Tilt Angle (°)	0.81 (0.66, 0.89)	2.35°	6.53°	1.44° (0.30 2.58), (-4.68, 7.55)
Patellar Tilt Angle (°)	0.79 (0.63, 0.88)	2.08°	5.77°	0.68° (-0.57 1.92), (-5.99, 7.34)
TT-TG (mm)	0.93 (0.87, 0.96)	1.11mm	3.08mm	0.35mm (-0.21 0.90), (-2.61, 3.30)
Trochlear Depth (mm)	0.92 (0.86, 0.96)	0.35mm	0.97mm	-0.30mm (-0.46 -0.13), (-1.18, 0.59)

10 Abbreviations: LOA = limits of agreement, MDC₉₅ = Minimal detectable change, mm = millimeters, SEM =
 11 Standard error of measurement, TT-TG = Tibial Tuberosity to Trochlear Groove Distance.

12
 13 **DISCUSSION**

14 The traditional manual approach to quantify the geometry of the knee joint from MR images is
 15 resource intensive, time-consuming, and can be prone to data transcription errors. This study
 16 reports the development and preliminary evaluation (validity and inter-reliability) of a semi-
 17 automated approach for measuring tibiofemoral and patellofemoral joint geometry using MR
 18 images from youth with and without a previous sport-related knee injury. The novel semi-
 19 automated software, which guides users to select anatomical landmarks associated with desired
 20 geometrics features demonstrates strong concurrent validity and inter-rater reliability for
 21 measuring linear distance, angle, and ratio measurements suggesting that it is an accurate,

1 reproducible, and efficient alternative method for measuring large numbers of tibiofemoral and
2 patellofemoral geometric features from MR studies. Although the current study only assessed the
3 validity and reliability of a sub-set of varied geometric features, there is no reason to suggest that
4 the performance of the custom software would yield inferior results for the remaining features as
5 the measurement process is consistent.

6

7 To understand the relationship between measurements made with the target and criterion
8 standard test we estimated the monotonic association between measurements from the two
9 methods with a correlation coefficient,²¹ calculated mean differences (95% limits of agreements)
10 and employed Bland-Altman plots to assess for systematic bias.²² All monotonic associations
11 assessing concurrent validity exceeded 0.89 which suggests a good to excellent correlation
12 between the measurements made with the semi-automated software and traditional manual
13 approach.²¹ Mean differences less than 1.5° for angular measurements, 1mm for linear distance
14 measurements, and 5% for ratio measurements, as well as absence of systematic bias provide
15 further evidence of the promising accuracy of the semi-automated software. To provide a brief
16 context for these reported mean difference values, several studies were identified which
17 produced statistically significant differences, and compared knee joint geometry with MRI
18 features (e.g., cartilage damage or bone marrow lesions) or clinical outcomes (e.g., injury,
19 osteoarthritis, pain). Crossley et al. 2009²⁶ reported the following mean differences between a
20 population with patellofemoral joint OA and an uninjured control group: 19.86% for Bisect
21 Offset, -1.31 for Lateral Patellar Tilt Angle. Ali et al. 2010²⁷ reported the following mean
22 differences between an under 40-year-old population with severe cartilage defects and an
23 uninjured control group: -8.1° for Lateral Trochlear Inclination 1, 22° for Sulcus Angle, -
24 3.39mm for Trochlear Depth, 0.09 for Insall-Salvati Ratio. Stefanik et al. 2012²⁸ reported the
25 following ranges between quartiles with a low and high prevalence of patellofemoral joint
26 cartilage damage and bone marrow lesions, respectively: <4.96° and <0.8° for the Trochlear
27 Angle. Macri et al. 2018⁵ reported mean differences for the following: 3.6% for Bisect Offset,
28 and 4.9° for Sulcus Angle.

29

30 To evaluate inter-rater reliability between a novice and experienced rater using the semi-
31 automated software we assessed the association between rater measurements (ICC),

1 measurement precision (SEm) and examined Bland-Altman plots. All ICC estimates exceeded
2 0.79 which suggests good to excellent reliability.²⁹ SEm estimates less than 3.5° for angular
3 measurements, 1.2mm for linear measurements, and 0.5% for ratio measurements, as well as
4 absence of systemic bias suggest raters of all levels can generate relatively consistent
5 measurements of angular, linear and ratio measurements with the semi-automated software.
6 MDC and SEm values are somewhat appreciable, provided the subtlety of quantifiable
7 morphological changes precipitated by a knee injury, which infers differences between groups
8 may go overlooked by the current iteration of the software, if there are multiple raters. Similarly,
9 many clinical measures (e.g., strength testing, range of motion testing) have relatively high
10 MDCs, so it is typically recommended that measures on an individual patient are made by the
11 same rater to enhance interpretation of the values. Our results suggest that interpretation of some
12 of the measures made with the custom software will also benefit from a measurement system that
13 includes the same rater particularly if longitudinal comparison is desired. That withstanding,
14 when evaluating group differences, in research settings, it is recommend that MDC is calculated
15 as $\frac{MDC}{\sqrt{N}}$, which would result in a much smaller group MDC value that supports the usefulness of
16 these measures.²⁵

17
18 The error associated with appreciable MDC values is likely attributed to rater experience and
19 skill. To ameliorate this potential source of error, instructions to the software could be
20 supplemented by source publications with more elaborate measurements descriptions. This
21 source of error may also be compounded by pixel resolution. The pixel resolution for the sagittal
22 MR images used in this study was 0.293mm in both the x and y axis. However, as the software
23 created the axial reformats for measures in requiring an axial viewing plane, this distance
24 increased to 1mm in the y direction which may have led to greater between rater differences and
25 margin of error in terms of real-world distances. Furthermore, the custom software only allows
26 for selection of the center of the pixel. DICOM image viewing applications typically make use of
27 interpolation formulas for this reason, and future iterations of the custom software should apply
28 interpolation formulas to increase the resolution in this direction, thereby minimizing this error
29 of measurement. Future studies should clarify these discrepancies with a more robust study
30 design, where intra-rater reliability is assessed, and resultant values between injured and

1 uninjured groups are compared between the custom software and established traditional
2 approaches with standardized experience levels.

3

4 We were unable to identify previous studies that assessed geometric features of the knee joint
5 from MRI measurements with, or assessed the concurrent validity of, semi-automated methods.
6 One of the most crucial criteria for establishing concurrent validity is the validity of the criterion
7 standard. For this study, the criterion or “gold” standard was a manual method employing an
8 image processing application for DICOM images (DICOM viewing applications) to extract
9 distances and angles, and Microsoft Excel® (Microsoft, USA) for data manipulation and
10 analysis. Although measurements of this manual approach have not been compared to real-
11 world, in-situ bone geometry measurements, it has been used on numerous occasions to measure
12 and assess the relationship of knee geometrics to clinical features.^{5, 15, 30, 31} The novel semi-
13 automated software developed in this study produced virtually identical measurements to this
14 established manual method. It is interesting to note that Rater 2 (EM) estimated that the process
15 of measuring and calculating the 11 geometric measurements using the established manual
16 method took on an average 20 minutes per participant compared to approximately 10 minutes per
17 participants with the semi-automated approach. Given that the semi-automatic approach allows
18 investigators to measure up to 37 geometric features in approximately half of the time, while
19 eliminating opportunities for data transcription errors, suggests that it is a promising alternative.

20

21 Although we were unable to identify any studies that have assessed the reliability of semi-
22 automated approaches that measure geometric features of the knee, there are studies that examine
23 the reliability of traditional manual measurement approaches. An example subset of six such
24 studies have estimated ICC values for inter and or intra-rater reliability for the traditional manual
25 approach.^{4, 11, 15, 30, 31, 32} Using the picture archiving software Centricity® (General Electric
26 Healthcare, USA), Sebro et al. 2017¹¹ reported intra-rater ICC estimates ranging from 0.54-0.93,
27 while Mundy et al. 2016³² reported intra-rater ICCs between (0.78-0.90), and inter-rater ICCs
28 between (0.81-0.96), both in pediatric populations. Stefanik et al. 2010³¹ and 2012³⁰, using
29 OsiriX (Pixmeo, SARL, Switzerland), reported ranges of intra and inter-rater ICCs values across
30 several geometric features of the knee in the MOST cohort (adults with or at increased risk of
31 osteoarthritis) greater than 0.90, and 0.70, respectively. Macri et al. 2017⁴ and 2018¹⁵ reported

1 estimates of reliability across several geometric features of the knee in both the Framingham
2 Community cohort and in a population 1 year after anterior cruciate ligament reconstruction
3 surgery - presenting intra-rater ICCs between 0.89-0.99, and inter-rater ICCs between 0.85-0.98.
4 Given the susceptibility of ICCs to be inflated with samples containing large variance, stability
5 and agreement of a measurement system should also be considered.²⁰ In relation to the reliability
6 of established methods, the ICC estimates of inter-rater reliability of the semi-automated
7 software presented in this paper are directly comparable, if not superior to, previously
8 established methods.

9
10 **Limitations:** The findings of this study demonstrate that a novel semi-automated software for
11 measuring geometric features of the knee is valid and reliable for measuring 11 features
12 including linear, angular and ratio measurements. Similarly, only MR images from a subset of 30
13 participants were used to estimate inter-rater reliability, which could mask variability – although
14 Tables 3 and 4 present similar magnitudes of descriptive statistics between different sample
15 sizes, suggesting that the subset of 30 participants could be extrapolated. A larger sample size
16 may result in different estimates of reliability and should be evaluated in future studies to
17 confirm reproducibility. Despite being small, the clinical relevance, if any, of the mean
18 difference in measurements generated with the traditional manual and novel semi-automated
19 software has yet to be determined officially. To further assess clinical relevance, reported
20 measurements using the custom software between an injured and uninjured control population
21 could be evaluated for statistical relationships between study groups, and then compared to the
22 results of the same measurements using an established manual method - thus ensuring the mean
23 differences do not have a substantial influence when assessing measurements between injured
24 and uninjured populations. Further, it is important to note that the imaging processing software
25 OsiriX may prove to be more sophisticated and precise in interpreting data from high resolution
26 images than the novel semi-automated software developed in this study, which is limited by the
27 fact that the user is only able to select the center of a pixel, where each pixel represents a real-
28 world dimension that is provided in the DICOM (MRI) file.

29
30 It is important to recognize that both measurement systems assessed in this study (software and
31 manual) included a rater, and that it is impossible to compare these systems without considering

1 the level of rater experience. Although there would be less potential for variability in scores if we
2 had compared the two measurement systems using the same experienced rater, we would not
3 have been able to inform the real-world in-situ use of the software and understand if it could
4 walk an inexperienced user through the measurement process and successfully generate knee
5 joint measurements.

6

7 The cohort with which MRI sequences were drawn for this study was well-standardized in terms
8 of imaging protocol, meaning all MR images used to perform measurements were produced on
9 the same equipment at the same site. While this is a benefit for validating the software, the
10 reproducibility of these results has not yet been tested on other equipment, at different testing
11 sites, at different time points, upon patient repositioning, or with other patient populations. In its
12 current iteration, and without the use of interpolation formulas to increase pixel resolution, the
13 software measurements would likely change with larger slice thicknesses, or poorer MR image
14 resolutions. With that said, the primary source of information required by the software to
15 perform measurements is the pixel-spacing attribute found in DICOM image files, which
16 suggests that the software could be used for all MR image studies using the same file format and
17 regardless of equipment used – although fluctuations based on resolution could still occur.

18

19 **CONCLUSIONS**

20 This study describes the development and preliminary evaluation of a novel semi-automated
21 method for characterizing knee joint geometry using anatomical landmark features from MRI.
22 We found the software showed concurrent validity and inter-rater reliability equivalent or better
23 than previously reported methods for measuring geometric features, with accuracy,
24 reproducibility, and efficiency potentially suitable for measuring large numbers of tibiofemoral
25 and patellofemoral features from MRI. This method provides a viable alternative measurement
26 approach to the resource intensive, time consuming traditional manual approach, and may be of
27 interest to investigators interested in considering multiple geometric features of the knee joint in
28 large MR datasets. Although the results are promising, further studies are still required to
29 officially validate the clinical capabilities of the software.

30

31 ***Future Directions:***

1 Future evaluation of the novel semi-automated software developed in this study could include
2 further feasibility and acceptability measurements including the time saved in using it compared
3 to traditional manual approaches, and feedback from both naïve and expert users. Future
4 functionality related to use with other sagittal and frontal MR sequences and measurements that
5 exploit the three-dimensional nature of MR sequence data vs individual two-dimensional slices.
6 Finally, future studies are required to assess differences in the geometric features of the knee as
7 well as the relationship between these features and clinical measurements in youth with and
8 without a past intra-articular knee injury, as well as other clinical populations (e.g., knee
9 osteoarthritis).

10

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12 software, T.B., G.K., and J.J.; validation, T.B., E.M., and A.P.; formal analysis, T.B.;
13 investigation, T.B., E.M., and A.P.; resources, C.E., J.R.; data curation, T.B. and A.P.; writing—
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17

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24

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1 **FIGURE CAPTIONS**

2

3 Figure 1. Illustration of anatomical points included in the calculation of geometric outcomes, for
4 the axial viewing plane. Points labeled with an asterisk are not included in the point selection
5 process of the custom software, as outlined in the Software Development section of this report
6 and are therefore interpreted by the software to calculate outcomes. All other points are included
7 in the point selection process. Points were labeled for reference for Tables 1 and 2, that describe
8 the outcomes included in the custom software.

9

10 Figure 2. Illustration of anatomical points included in the calculation of architectural outcomes,
11 for the sagittal viewing plane. Points labeled with an asterisk are not included in the point
12 selection process of the custom software, as outlined in the Software Development section of this
13 report and are therefore interpreted by the software to calculate outcomes. All other points are
14 included in the point selection process. Points were labeled for reference for Tables 1 and 2, that
15 describe the outcomes included in the custom software.

16

17 Figure 3. Illustration of anatomical points included in the calculation of geometric outcomes, for
18 the coronal viewing plane. Points labeled with an asterisk are not included in the point selection
19 process of the custom software, as outlined in the Software Development section of this report
20 and are therefore interpreted by the software to calculate outcomes. All other points are included
21 in the point selection process. Points were labeled for reference for Tables 1 and 2, that describe
22 the outcomes included in the custom software.

23

24 Figure 4. Composite renderings created by the custom software used to assist the rater with
25 orientation and visualizations. The user has the option to view one of the three renderings at a
26 time. From left to right: a simple Composite Overlay of each MR image in the sequence, an
27 Average Intensity Projection (AIP) is an image of the average intensity values of pixels between
28 all MR images in the sequence, and a Maximal Intensity Projection (MIP) is an image of the
29 maximum intensity value of pixels between all MR images in the sequence.

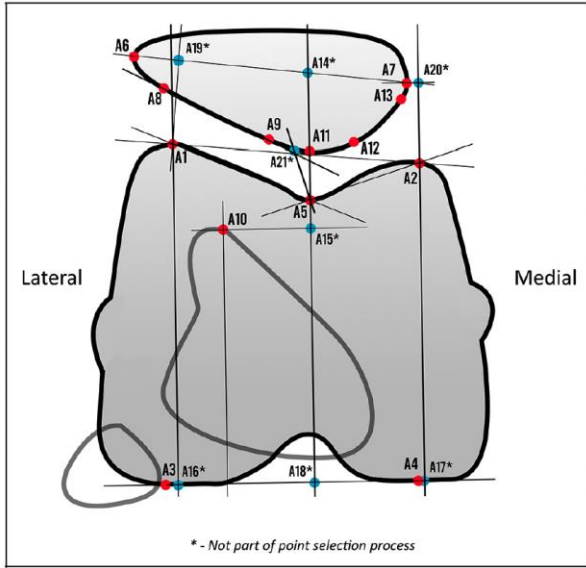
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1 FIGURES

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3 Figure 1

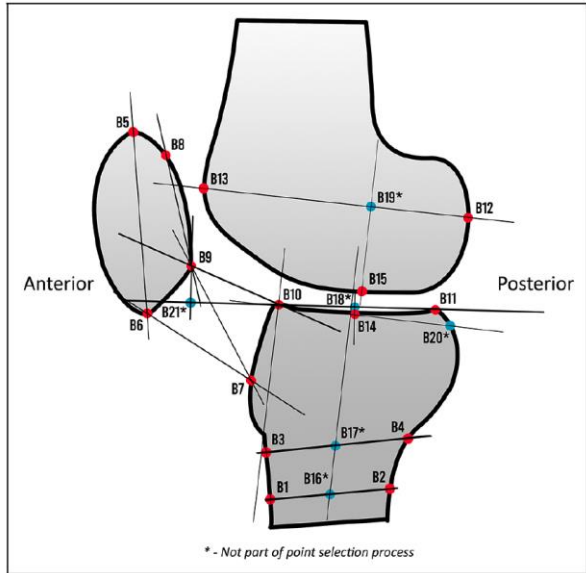
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7 Figure 2



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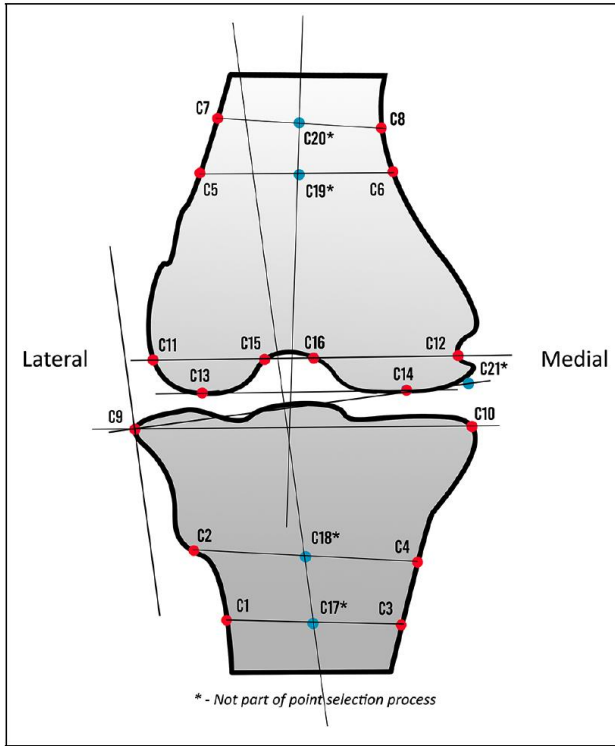
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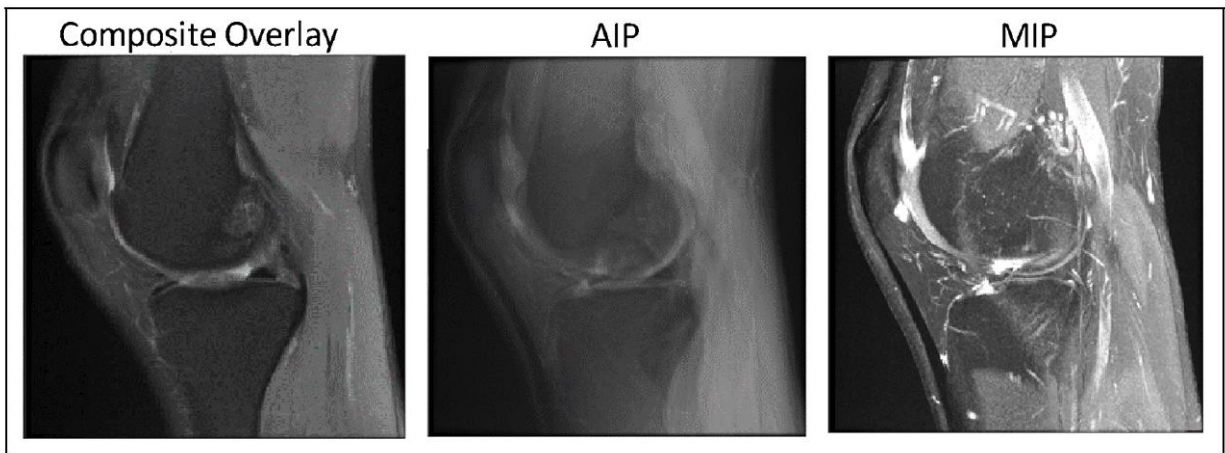
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1 Figure 3



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Figure 4



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