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To the Graduate Council:
I am submitting herewith a thesis written by Yeon-Joo Yu entitled "Impact and shock attenuation during landing activities from different heights on different surfaces." I have examined the final electronic copy of this thesis for form and content and recommend that it be accepted in partial fulfillment of the requirements for the degree of Master of Science, with a major in Human Performance and Sport Studies.

Songning Zhang, Major Professor
We have read this thesis and recommend its acceptance:
Wendell Liemohn, David R. Bassett
Accepted for the Council:
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I am submitting herewith a thesis written by Yeon-Joo Mu entitled "Impact and shock attenuation during landing activities from different heights on different surfaces." I have examined the final copy of this thesis for form and content and recommend that it be accepted in partial fulfillment of the requirements for the degree of Master of Science, with a major in Human Performance and Sports Studies.


We have read this thesis and recommend its acceptance:


Wendell Liemohn


Accepted for the Council:


# Impact and shock attenuation during landing activities from different heights on different surfaces 

A Thesis<br>Presented for the<br>Master of Science<br>Degree<br>The University of Tennessee, Knoxville

Yeon-Joo Yu
May 2001

## DEDICATION

I would like to dedicate this thesis to my parents Jin-Hae Yu and Han-Sook Kim and my brother Choul-Ho Yu. Their love and support have always encouraged and guided me through the better or worse times in my life.

## ACKNOWLEDGMENTS

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#### Abstract

The purpose of this study was to examine impact shock attenuation during landing activities from different heights on different surfaces. Thirteen healthy and active subjects performed five trials of step-off landing from four different heights $(30,45,60$, and 75 cm ) in shod and barefoot. Ground reaction forces (GRF), accelerations of the tibia and forehead, and kinematic data were sampled simultaneously. Increased heights caused increases in angular kinematic variables (range of motions, contact and maximum angular velocities of the ankle, knee, and hip joints). Few significant changes in kinematics were observed across the surface conditions. The first maximum GRF (F1) showed a trend of greater values in the shoe landing than that in the barefoot landing, with significant difference found at 75 cm . The second maximum GRF (F2) demonstrated a trend of greater values in the barefoot conditions than those in the shoe conditions. Greater F 1 and F 2 values were observed with increases in landing heights. The maximum head acceleration (AccHead) showed few significant changes in across the heights and surfaces. The first tibia acceleration (AccTibial) was generally greater in the shoe conditions than that in the barefoot conditions. On the other hand, the second tibia acceleration (AccTibia2) displayed a trend of greater values in the barefoot conditions than that in the shod conditions, with significant difference found at 60 and 75 cm . The shock attenuation index (AtteIndex) in the barefoot conditions was significantly greater than that in the shoe conditions at all landing heights. The results suggested that the shoe provided an additional cushion to minimize impact forces and attenuate impact shock during the landing activities.


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## Chapter I

## Introduction

Jumping and landing are integral parts of many sport activities such as basketball, volleyball, and gymnastics. Many injuries of the lower extremity occur during the landing phase. According to a 1995 study by Kujala et al. [18], lower extremity injuries were most common in soccer, volleyball, and basketball athletes. With 54,186 sports injuries reported in Finland during a five-year investigation, the knee was reported as the most vulnerable joint. This result was in agreement with the studies of Arendat et al. [2] and Garrick [11]. Arendt et al. [2] found that knee injuries were the most prevalent injury in soccer and basketball using data obtained from the National College Athletic Association Injury Surveillance System. Garrick [11] examined 11,141 sports injuries in 1985, and reported that the knee joint was a commonly injured site. More than two thirds of injuries were due to overuse. In a study by Ferretti et al. [8], frequent knee injuries were often found in landing from a jump in volleyball players.

During landing, the human body experiences tremendous impact forces. Studies in biomechanics frequently focus on mechanisms and prevention of lower extremity injuries by investigating vertical ground reaction force (VGRF). Dufek and Bates [7] examined effects of heights, distances, and techniques on impact forces during landing. Increases in landing stiffness and landing heights were associated with increases of peak VGRF. These results were in agreement with Mizrahi et al. [25] who also found that greater VGRF was associated with greater landing heights. The first peak VGRF (F1) in
toe-heel landing was significantly greater than in toe landings from the lower height. In addition, the toe-heel landing from the higher height produced greater ranges of motion for the hip, knee, and ankle joints than from the lower height.

Another aspect of biomechanical studies in dynamic activities is related to impact shock attenuation of the human body. Many studies have examined the shock attenuation capacity in walking and running. Only a few studies have addressed shock attenuation during landing activities, especially using information obtained from accelerometers. In a study conducted by Gross and Nelson [13], shock attenuation at the ankle was examined using two uniaxial accelerometers during barefoot landing from a vertical jump. No significant difference was found for peak calcaneal and tibial accelerations across the three surfaces (a midsole foam, a tartan rubber, and a cast aluminum). There was no significant difference between the peak calcaneal and tibial accelerations across all landing techniques (toe and toe-heel landing). The toe landing technique attenuated more peak VGRF and therefore was considered as a preferable landing technique for injury prevention.

Cavanagh et al. [3] examined VGRF during walking barefoot and in shoes. During barefoot walking, Fl was significantly greater and the time to F1 was shorter than the three footwear conditions. These results confirmed that differences of VGRF existed between the barefoot and shoe conditions. Wit et al. [38] examined GRF and kinematics during barefoot and shoe running. Nine long distance runners ran at three different velocities of $3.5,4.5$, and $5.5 \mathrm{~m} / \mathrm{s}$. The barefoot running produced significantly greater peak VGRF and loading rate, and shorter time to F1 than the shoe running. Barefoot
running also showed greater plantarflexion and knee flexion compared to the shoe running.

## Problem Statement

The purpose of the study was to investigate impact force and shock attenuation during landings on two different surface conditions and from different heights. Studies in biomechanics of landing have mainly focused on measuring impact forces during the landing using different experimental manipulations of landing techniques, heights, surfaces, and distances. However, very few studies have investigated shock attenuation using accelerometers in landing activities in shoe and barefoot conditions. By investigating the shock attenuation at the tibia and head using accelerometers while changing the surface and the height conditions, one could determine mechanisms of shock attenuation throughout the body during landing activities.

The results of this research may provide better understanding of performance enhancement, injury mechanisms, shock attenuation properties of shoes, and prevention of sport injuries during landing related activities.

## Hypotheses

The following hypothesis were tested:

1) There are no differences in GRF during landings in barefoot and shoe conditions.
2) There are no differences in GRF during landings from different heights.
3) There are no differences in accelerations at the tibia and the head in the barefoot and shoe conditions.
4) There are no differences in accelerations at the tibia and the head from the different heights. •
5) There are no differences in kinematic variables of the hip, knee, and ankle joints during landings in the barefoot and shoe conditions, as well as from the different heights.

## Delimitations

The study was conducted within the following delimitations:

1) Thirteen active and healthy male subjects were selected from the student population at The University of Tennessee. They had no impairments of the lower extremities.
2) Eight test conditions included step-off landings with shoes from four different heights ( $30,45,60$, and 75 cm ) and step-off landings without shoes from the same four different heights.
3) Biomechanical signals were collected and analyzed for duration from 100 ms prior to the contact to the end of the landing phase for each trial.
4) Data were collected at 1200 Hz from a force platform (AMTI), two accelerometers (A353B17, Piezotronics Inc.), and at 60 Hz from a video camera (AG-188U, Panasonic) for each trial of the landing activity.

## Limitations

The study was limited by the following factors:

1) Subjects were limited to the student population at The University of Tennessee.
2) Possible errors from placements of reflective markers.
3) Potential errors from the force platform, the accelerometers, and the video camera.
4) Possible errors due to the digitization of video.
5) The difference in the sampling frequency of the force platform $(1200 \mathrm{~Hz})$ and the video camera $(60 \mathrm{~Hz})$.

## Assumptions

The following assumptions were made for this study:

1) Step-off landings could be modeled mechanically.
2) Biomechanical measurements used were sufficient for analyzing effects of step-off landings with different landing heights and surfaces.
3) Biomechanical instruments used were accurate.
4) All subjects were free of injuries of lower extremities at the time of testing.
5) The performance of the subjects was symmetrical, so therefore only the right side was assessed for the kinematics, GRF, and acceleration.

## Chapter II

## Literature Review

The purpose of this study was to investigate impact force and shock attenuation during landings on different surface conditions and from different heights. The intent of this literature review is to present research findings regarding biomechanics and impact attenuation during landing activities. Relevant research on walking, running, and pendulum experiments is also reviewed. The literature review is presented under these sub-titles: ground reaction force, acceleration, other relevant studies, and summary.

## Ground Reaction Force

Gross et al. [13] investigated vertical ground reaction force (VGRF) during barefoot landing from a vertical jump. Eleven male recreational basketball players were divided into two groups according to two different landing styles: four subjects were involved in landings with toe; seven subjects were involved in landings with toe-heel. Three different surfaces (an aluminum force plate surface, a 9.0 mm thick tartan rubber surface, and a 13.0 mm thick midsole foam surface) were used to examine VGRF. The VGRF data were collected with a force platform (Kistler Type 9261A) at 1000 Hz . The magnitude of VGRF with the toe landing was reduced by $22 \%$, compared with the toeheel landing. The VGRF data showed no significant differences among the landing surfaces. The findings suggest that the toe landing was more favorable in impact attenuation and potentially in injury prevention.

Stacoff et al. [34] studied the effects of landing techniques on impact force in landings during volleyball blocks. The VGRF data were collected and sampled at 500 Hz using a force platform. The peak VGRF of toe landings ranged from 1000 to 2000 N . In toe-heel landings, the VGRF values ranged from 1000 to 6500 N . The kinematic results also showed that the degree of knee flexion was closely associated with the reduction of VGRF.

Ozguven et al. [29] evaluated impact forces during human landings. In the first experiment three gymnasts performed 10 typical landings starting from a hanging position on a horizontal bar ( 2.55 m above the floor) onto a $2.5 \times 3.0 \mathrm{~m}$ mat placed on a force platform ( 150 Hz ). In the second experiment, two male and two female gymnasts were asked to land normally from a 0.45 m height onto the force platform. During both experiments, the subjects did not wear shoes. The VGRF values ranged from 8.2 to 11.7 $\mathrm{BW}(10.6 \pm 1.1 \mathrm{BW})$ and 5.0 to $7.0 \mathrm{BW}(5.9 \pm 0.6 \mathrm{BW})$ in the first and second experiments, respectively.

Dufek and Bates [7] examined effects of height, distance, and technique on impact forces during landing. The mean peak VGRF (F1 and F2) and the mean time to F1 and F2 were used in analyses. Data were collected using a force platform (Type 9281-B, Kistler) and a high-speed film camera (Redlake Corporation). Three male subjects performed landings in test conditions with a combination of three landing distances ( 40,70 , and 100 cm ), and three landing heights ( 40,60 , and 100 cm ) using three landing techniques (stiff knee, slightly-flexed knee, and fully-flexed knee). The subjects performed three landing trials per condition for a total of 81 trials. Increases in landing stiffness and landing height were associated with increases of the peak VGRF.

These results were in agreement with Mizrahi et al. [25] who also found that greater VGRF was associated with greater landing heights. In their study, five subjects landed from two hanging positions on rings with arms either straight or flexed. Subjects performed both with toe-heel and toe only landings from the lower position ( 0.5 m above the floor), and toe landings from the higher position (1 m above the floor). The peak VGRF ( F 1 and F 2 ) and the range of motion for the hip, knee, and ankle joints were examined. The F1 magnitude in toe-heel landings was significantly greater than in toe landings from the lower height. In addition, the toe-heel landings from the higher height produced greater ranges of motion for the hip, knee, and ankle joints than the toe-heel landings from the lower height.

Panzer et al. [30] examined VGRF acting on six elite gymnasts during single back somersaults (SBS) and double back somersaults (DBS). The VGRF data were collected with two Kistler force platforms and sampled at 500 Hz . To obtain kinematic data, five reflective markers (gleno-humeral joint, greater trochanter, femoral condyle, lateral malleolus, and fifth metatarsal-phalangeal joint) were placed along the side of subjects and performances were recorded with a high-speed film camera. The values of peak VGRF for DBS ranged from 8.8 to 14.4 BW for single-leg landings; the peak VGRF in DBS was 6.7 BW higher than in SBS.

Ricard and Veatch [31] investigated impact forces of two aerobic dance movements: the low impact front knee lift (LFKL) and the high impact front knee lift (HFKL). The variables included peak impact force, time to peak impact force, and peak loading rate. The mean peak impact force was 0.98 and 1.98 BW for LFKL and HFKL, respectively. The time to peak impact force in LFKL was significantly longer than in

HFKL. The mean peak-loading rate was 42.55 and $14.38 \mathrm{BW} / \mathrm{s}$ for HFKL and LFKL, respectively. Based on these results, it can be observed that LFKL produced significantly lower impact forces than HFKL.

## Acceleration

## Landing

In a study conducted by Gross and Nelson [13], shock attenuation at the ankle was examined during barefoot landing from a vertical jump. The experiment conditions included landing from vertical jumps with two landing techniques (toe and toe-heel) onto three different landing surfaces (a midsole foam, a tartan rubber, and a cast aluminum). Two uniaxial accelerometers (Endevco 2222B.) were used to measure accelerations at the tibia and the calcaneus. In pilot data, damping factors of 0.239 and 0.552 were determined for the calcaneus and the tibia, respectively. These values showed that the acceleration measurement at the tibia was more attenuated than at the calcaneus. The average of peak accelerations at the calcaneus and tibia across the three surfaces were 20.8 and 14.3 g , respectively. However, no significant difference was found between the peak calcaneal and tibial accelertions across the three surfaces. There was also no significant difference between the peak calcaneal and tibial accelerations between the two landing techniques.

## Walking

In the study performed by Voloshin et al. [37], the ability of shock absorption was investigated among healthy subjects and subjects with degenerative changes in bones
and/or joints. The data were collected using accelerometers (Type 4371, Bruel and Kjaer) attached to the tibial tuberosity and forehead of each subject during walking at speed of $4.2 \mathrm{~km} / \mathrm{hr}$. Shock absorption capacity, K , was calculated with the following formula:

## Amplitude on tibial tuberosity <br> $\mathrm{K}=$ <br> Amplitude on forehead

The healthy subjects had significantly higher K values than the patients. The higher K value indicated greater shock attenuation capacity in the healthy subject group. This result confirmed that the lower values of the shock-absorbing capacity of the human locomotor system were related to degenerative changes in bones and/or joints.

Wosk and Voloshin [39] examined the shock attenuation between the forehead and tibial tuberosity in 39 healthy subjects. Miniature accelerometers (Type 4371, Bruel \& Kjaer) were mounted on the forehead and the tibial tuberosity of the subjects. The subjects performed walking without shoes at speed of $4.0 \mathrm{~km} / \mathrm{hr}$. Twenty-three subjects showed approximately symmetrical value of the peak-to-peak acceleration in the first cycle (PP1). Sixteen subjects showed asymmetrical values of PP1, whereas a symmetrical value was considered as $10 \%$ or less in difference of PP1 values between the right and left heel strikes. Using the same formula [37], K was used for evaluating the shock attenuation between the knee and the forehead. The asymmetrical subjects showed a $25 \%$ lower K ratio than the symmetrical subjects, implying a lack of shock absorbing capacity of the hip-knee-joint system. Even though all subjects were healthy
and reported no orthopedic diseases, the authors suggested the development of degenerative joint diseases in the asymmetrical subjects.

## Running

Shorten and Winslow [33] examined impact shock attenuation during treadmill running. Twelve healthy subjects performed running at different speeds ( 2 to $5 \mathrm{~m} / \mathrm{s}$ ). A piezo-resistive accelerometer (EGA-125-250D) was mounted on the skin of the medialanterior aspect of the tibia to measure shock of the tibia. In order to measure shock of the head, an accelerometer attached to a bite-bar was affixed to the teeth of the subjects. As the treadmill speed increased, the amplitude and frequency of the leg acceleration increased. However, the peak head acceleration did not show any significant changes due to the increase of the treadmill speed. At higher frequencies (above 6 Hz ), the acceleration of the head showed no significant peak power. The results suggested that the body served as a low-pass filter, attenuating the impact shock of higher frequencies.

Hamill et al. [15] examined the relationship between stride frequencies and shock attenuation during treadmill running. Two accelerometers (PCB Piezotronics) were mounted on the antero-medial distal aspect of the left tibia and the frontal bone of the head. Ten healthy male subjects ran at $-20 \%,-10 \%, 0 \%,+10 \%$, and $+20 \%$ of a preferred stride frequency at a preferred running speed. A power spectral analysis displayed two peaks of power for the leg acceleration. One was at 5 to 7 Hz and the other at 10 to 15 Hz , respectively. A single peak for the head acceleration was found below 10 Hz . The head acceleration was constant across the stride frequency conditions. The
powers and frequencies at which the peaks occurred for the leg and the head were similar to the findings of Shorten and Winslow [33].

Lafortune and Hennig [19] examined accelerations obtained from a bone-mounted accelerometer during walking and running. A bone-pin was inserted into the proximal end of the right tibia with a triaxial accelerometer. Six subjects performed 5 trials of running at $4.5 \mathrm{~m} / \mathrm{s}$, and three components of accelerations and ground reaction forces were collected at 1000 Hz . One of the subjects performed three trials of walking. The acceleration signal was analyzed using a power spectrum analysis. The average values of peak tibial axial acceleration (At) were 3.1 and 5.3 g for walking and running, respectively, whereas the average peak tibial axial acceleration (Ai) estimated from ground reaction forces were 2.6 and 10.3 g for walking and running, respectively. No significant differences were observed in times to At and Ai during between walking and running.

## Pendulum Experiment

Lafortune et al. $[21,22]$ conducted two studies using a pendulum device. The first study [21] examined relationships among GRF, impact shock, knee joint angles, and different surfaces in the pendulum experiment. The pendulum device was composed of a lightweight bed and a Kistler force platform (Model \#9281B11) mounted on a wall. All subjects laid supine with the right leg extended and the left leg flexed on the bed. The subjects positioned the right leg so that it barely touched the force platform. A uniaxial accelerometer (EGA-100D, Entran) was mounted on the antero-medial of the shank 15 cm proximal to the medial malleolus. The velocity at the time of impact with the force
platform was set to $1.0 \mathrm{~m} / \mathrm{s}$. Nine different test conditions were conducted with combinations of three initial knee angles (IKA) of 0,20 , and 40 degrees and three surfaces of barefoot, soft (a 2.5 cm thick layers of EVA form with Asker C of 40), and hard (a 2.5 cm thick layers of EVA form with Asker C of 60 ) contact materials. The variables included peak impact force, time to the peak impact force, peak acceleration, and time to the peak acceleration. The results demonstrated that larger IKA were associated with reduction of initial peak impact force, and larger IKA increased peak shank acceleration on the three different surfaces. The soft surface caused reduction of peak shank acceleration at the three IKA. Increases in IKA were associated with shorter times to the peak impact force and the peak shank acceleration except at the barefoot condition with the 0 and $40^{\circ} \mathrm{IKA}$. The soft surface produced longer times to the peak impact force and the peak shank acceleration at the all three IKAs.

In the second study [22], the authors focused on shock transmission of the body using the same pendulum impact device. Test conditions included combinations of three different impact velocities of $0.9,1.05$, and $1.20 \mathrm{~m} / \mathrm{s}$, and two different surfaces of soft ( 2.5 cm thick layers of 40 Asker C) and hard ( 2.5 cm thick layers of 60 Asker C) materials. Two biaxial accelerometers were mounted on the head and the shank to obtain impact shock of the seventeen male subjects. Right knee angle was kept $20^{\circ}$ flexion during the impact. Peaks and times to peaks of head and shank accelerations were obtained. The peak shock transmission of the body was calculated as a ratio of the head and shank peaks. In addition, the time to the shock transmission was calculated from interval between the head peak and shank peak acceleration. With increases in the impact velocity, the peak shock and the time to the peak shock were increased in
magnitude and decreased in time for both head and shank accelerations. The hard surface was linked to greater peak shock and shorter times to peak shock for the head and the shank. Significant differences in the body shock transmissions were found among the three different velocities; there was a significant difference in the body shock transmissions between the soft and the hard surfaces. The soft surface introduced greater shock transmission than the hard surface.

## Other relevant studies

## Landing

In the study conducted by Dufek et al. [6], two peaks of VGRF (F1 and F2) were examined in four different shoe conditions: two basketball shoes (Cland C2), a running shoe (C3), and a volleyball shoe (C4). Five male subjects landed from a $60-\mathrm{cm}$ height onto a force platform $(1000 \mathrm{~Hz})$. Four variables were obtained from the GRF data, including forefoot impact force (F1), rearfoot impact force (F2), time to the occurrence of F1 (T1), and time to the occurrence of F 2 (T2). The average values for F 1 and F 2 were 1.21 and 3.00 BW , respectively. The average T 1 and T 2 were 14.8 and 56.5 ms , respectively. The first basketball shoe $(\mathrm{Cl})$ produced statistically lower values as well as shorter time of both F1 and F2 than the second basketball shoe (C2). Comparing shoe conditions across the subjects, Cl caused less values of F 1 for all subjects.

Gross and Bunch [12] investigated VGRF in the thickness of the different midsole materials during landings from a jump. Three midsole materials were used: a 2 mm thick rigid paperboard as a stiff spring (STS), polyurethane as a subordinate spring/dominant damper (SS/DD), and ethyl vinyl acetate as a dominant spring/subordinate damper
(DS/SD). The three midsole materials were inserted into basketball shoes. Nine male subjects performed five vertical jumps in each of the three different midsole conditions. A kistler force plate (Type SN $9807,333 \mathrm{~Hz}$ ) was used to measure VGRF. The peak VGRF did not show any significant difference among the midsole materials.

Fukoda [10] analyzed muscle power and joint kinematics in landings on surfaces of different stiffness. Four male subjects landed from a 0.2 m height onto surfaces of two different stiffnesses ( $\mathrm{K} 1 ; 49.0 \mathrm{kN} / \mathrm{m}, \mathrm{K} 2 ; 392.0 \mathrm{kN} / \mathrm{m}$ ). The peak power at the knee joint during landing on K 2 was significantly larger than when landing on K 1 . There was no significant difference for the peak power at the ankle between two surfaces. The results suggested that increases in surface hardness produced increases in the impact load on the knee extensors.

## Walking

Cavanagh et al. [3] examined VGRF and kinematic data during walking barefoot and in shoes. Ten male subjects (Mean body weight $=693.3 \mathrm{~N}$ ) performed five trials of walking at a speed of $1.32 \mathrm{~m} / \mathrm{s}$ in barefoot and three shoe conditions (army boots, leather street shoes, and crepe soled casual shoes). Force platform ( 1580 Hz ) and a high-speed kinematic data $(200 \mathrm{~Hz})$ were collected for three trials for each subject. During the barefoot walking, F1 was significantly greater and the time to F1 was shorter than the three footwear conditions. During the barefoot walking, the ankle was significantly more dorsiflexed than shoe walking during the swing phase. However, there was no significant difference in the posture at contact between the conditions. Only the knee was fully
flexed at contact during the barefoot walking. These results confirmed that differences in VGRF exist between barefoot and shoe walking.

Lafortune et al. [20] studied VGRF and acceleration in walking in different types of footwear. A 6-g triaxial Entran piezoresistive accelerometer was inserted into the proximal right tibia of five subjects using a bone pin. Both VGRF (9281 Kistler) and tibial acceleration data were sampled at 1000 Hz . The subjects performed three trials of walking at $1.5 \mathrm{~m} / \mathrm{s}$ in three footwear conditions (barefoot, leather-soled street shoe, and athletic shoe). The variables examined included initial peak ground reaction force (IPF), initial peak tibial acceleration (IPA), force loading rate (FLR), and acceleration transient rate (ATR). FLR and ATR was calculated with the following formulas:
$\mathrm{FLR}=0.7 \mathrm{IPF} / \Delta \mathrm{t}_{\mathrm{F}}$, where $\Delta \mathrm{t}_{\mathrm{F}}$ are the time from 0.2 IPF to 0.9 IPF.
$\mathrm{ATR}=0.7 \mathrm{IPA} / \Delta \mathrm{t}_{\mathrm{A}}$, where $\Delta \mathrm{t}_{\mathrm{A}}$ are the time from 0.2 IPA to 0.9 IPA.
The barefoot condition produced higher IPF and faster FLR than the shoe conditions ( $\mathrm{p}<0.05$ ). Significant differences ( $\mathrm{p}<0.05$ ) were also found for IPA and ATR among all three footwear conditions. The barefoot condition produced higher IPA and ATR than the street shoes, and the street shoes produced higher IPA and ATR than the athletic shoes. Difference in IPF and FLR between walking barefoot and in shoes implied that the shoes were responsible for the reduction of the impact force and loading rate. The lower values of IPA and ATR in athletic shoes explained that both heel fat pad and compliant soles were involved in cushioning of the impact shock.

Fredrick et al. [9] determined effects of shoe design parameters on impact loads. These parameters included hardness of midsole materials, heel height, and angle of midsole flare. They found that shoe design parameters played a role in shock attenuation
reflected in kinematic and kinetic data. This observation indicated that shoes could either prevent injuries or cause injuries.

A study conducted by Denoth and Nigg [5] examined the difference of the partial load on the ankle and knee joint using different surfaces during walking and running. A partial load on the ankle and knee joint was defined as the mechanical load of the ankle and knee joint. The partial loads of the ankle and knee was calculated with the following formulas:

$$
\begin{aligned}
& \mathrm{f}_{\text {foot }}^{\prime}=m * \cdot v_{0} \cdot \sqrt{\frac{f_{\text {floor }} \cdot f_{\text {heel }}}{m * \cdot\left(f_{\text {floor }}+f_{\text {heel }}\right)}} \\
& \mathrm{f}_{\mathrm{knee}}=\left(m^{*}-m_{\text {tibia }}\right) \cdot v_{0} \cdot \sqrt{\frac{f_{\text {floor }} \cdot f_{\text {heel }}}{m^{*} \cdot\left(f_{\text {floor }}+f_{\text {heel }}\right)}}
\end{aligned}
$$

where, $\mathrm{v}_{0}=$ velocity of the effective mass ( $\mathrm{m}^{*}$ ) before impact (vertical)
$\mathrm{f}_{\text {floor }}, \mathrm{f}_{\text {heel }}=$ spring constant of floor and heel
The partial loads of both knee and ankle joint were greater on synthetic floors than on grass. It was observed that knee and ankle joints were vulnerable to injury on synthetic floors. This study showed the importance of playing surface in sports events such as jumping, walking and running.

## Running

Wit et al. [38] examined spatio-temporal variables of GRF and kinematics during barefoot and shoe running. Nine long distance runners (body mass: $70 \pm 9 \mathrm{~kg}$; shoe size: UK $8.9 \pm 1.5$ ) ran at velocities of $3.5,4.5$, and $5.5 \mathrm{~m} / \mathrm{s}$. Among nine subjects, seven subjects performed additional barefoot running at $4.5 \mathrm{~m} / \mathrm{s}$. The three components of GRF
and foot movement data were collected using a Kistler force platform and two high-speed video cameras: The GRF data were obtained from 10 trials and the kinematic data were analyzed from 5 trials of running. The barefoot running produced significantly greater loading rate and shorter time to F 1 than the shoe running. The barefoot running also showed greater plantarflexion and knee flexion, compared to the shoe running.

During the examination of the human heel pad, De Clercq et al. [4] found that there were differences in peak VGRF in barefoot and shoe running. In barefoot running, the F1 and the loading rate of F1 were higher than the shoe running. In addition, the time to F1 was shorter in the barefoot running compared to the shoe running.

Nigg et al. [27] investigated effects of midsole hardness and running velocities on VGRF during toe-heel running. Three pairs of shoes (size 9) were provided to fourteen subjects. The midsole was altered to 25,35 , and 45 shore for soft, normal and hard hardness. Subjects were asked to run at velocities of $3,4,5$, and $6 \mathrm{~m} / \mathrm{s}( \pm 0.2 \mathrm{~m} / \mathrm{s})$. Variables included peak impact force, time to peak impact force, and peak active force. In order to obtain these variables, a force platform ( 1020 Hz ) and a high-speed camera $(200 \mathrm{~Hz})$ were used. Increases in running velocities caused an increase in the peak impact force and a decrease in the time to peak impact force. As the velocity increased from $3 \mathrm{~m} / \mathrm{s}$ to $6 \mathrm{~m} / \mathrm{s}$, the peak active force increased from 1.86 kN to 2.26 kN . Increases in midsole hardness slightly decreased the peak impact force. However, it was not statistically significant. The time to peak impact force was significantly decreased as the midsole hardness increased from soft to normal.

Nigg and Liu [26] examined effects of soft and hard midsole during running. The mean peak VGRF was 1339 N and 1187 N for the hard and the soft shoe. The hard
midsole shoe produced significantly higher VGRF than the soft midsole shoe. This result was in an agreement with another study by Nigg et al. in 1981 [28]. Nigg and his colleagues [28] reported that soft sole shoes produced lower VGRF than hard sole shoes during $5 \mathrm{~m} / \mathrm{s}$ running. Furthermore, the peak VGRF was higher in a spike shoe than in a soft midsole training shoe during a vertical jump.

Valiant et al. [36] examined the acceleration at the tibia during barefoot and shoe running. An accelerometer was mounted on the anteromedial distal tibia; four subjects ran five trials in each condition. In the shoe condition, the peak acceleration and the time to the peak acceleration were $6.1 \mathrm{~g}( \pm 2.5 \mathrm{~g})$ and $8.3 \mathrm{~ms}( \pm 1.8 \mathrm{~ms})$, respectively. The peak acceleration and the time to the peak acceleration were $7.2 \mathrm{~g}( \pm 2.5 \mathrm{~g})$ and 6.0 ms $( \pm 1.6 \mathrm{~ms})$ for the barefoot condition. Only the time to the peak acceleration for the barefoot condition demonstrated a significantly lower value.

## Summary

This chapter illustrates biomechanics and impact attenuation during landing and other activities. The emphasis in the literature was placed on evaluating VGRF and acceleration during walking, running and landing. However, research addressing shock attenuation on different surfaces during landing activities is quite limited. Further investigations of shock attenuation on different surface conditions and from different heights during landing activities are warranted.

## Chapter III

## Research Methods

## Experimental Methods

Experiments were conducted to investigate attenuation of impact force and shock during landing from different heights on different surfaces. The protocol for the experiment consisted of a warm-up, anthropometric measurements, and eight test conditions. Five trials of step-off landings in each of eight different conditions, for a total of 40 trials, were performed by each subject.

## Subjects

All subjects signed an informed consent form approved by the Institutional Review Board at The University of Tennessee (Appendix G) prior to their participation in the study. Subjects were recruited from the student population at The University of Tennessee. Thirteen healthy and physically active male subjects volunteered to participate in the study. A healthy and physically active male subject was defined for this study as one who had no history of impairments to his lower extremities and who participated in recreational sports 2-3 times a week. All subjects were briefed on the purpose, procedures, risks, and benefits of this study before their participation. Subject information is provided in Appendix $B$.

## Instrumentation

All testing was conducted in the Biomechanics/Sports Medicine Lab, Room 135, HPER Building at The University of Tennessee. The biomechanical instrument used in this study included a force platform (OR6-7, AMTI), two accelerometers (A353B17, Piezotronics Inc.), a video camera (AG-188U, Panasonic), lab shoes, a trigger device, a reference frame, reflective markers, an analog/digital (A/D) converter, and an Ariel Performance Analysis System (APAS, Ariel Dynamics, Inc.) for data collection and processing.

## Kinematics

A video camera (AG-188U, Panasonic) was used to obtain kinematic data from the right sagittal view of the subjects during the test. The camera ( 60 Hz ) was set parallel to the floor and the shutter speed was set at $1 / 1000 \mathrm{sec}$. A reference frame (width= 140.97 cm , length $=186.69 \mathrm{~cm}$ ) was used to obtain scale factors in order to convert anatomical coordinates of the reflective markers. The reference frame has four coplanar reflective markers placed on the four comers of the structure.

Reflective markers were placed on the right side of the body at the shoulder, hip, knee, ankle, heel, and the head of the fifth metatarsal (Figure 1). Using the Ariel system, the recorded video images were digitized to obtain coordinates of these markers throughout during the activity. The digitized coordinates were then imported into a customized program to determine the time-history and discrete events of linear and angular positions, velocities, and accelerations.


Figure1. Placement of reflective markers

## Force Platform

A force platform (OR6-7, AMTI) flush with the surrounding floor was used to measure ground reaction forces (GRF) and moments during the test. The GRF data included Fx , Fy , and Fz , representing medial-lateral, anterior-posterior and vertical forces respectively. $\mathrm{Mx}, \mathrm{My}$, and Mz represented moments applied about $\mathrm{Fx}, \mathrm{Fy}$, and Fz axes. Signals from the force platform were sampled for 1.5 sec at a frequency of 1200 Hz and amplified before being stored in the APAS computer through the A/D converter.

## Accelerometer

Two miniature accelerometers (A353B17, Piezotronics, Inc.) were used to measure accelerations at the forehead and distal tibia of the subjects. Signals from the accelerometers were also sampled at a frequency of 1200 Hz using the APAS. The accelerometer has a range of 500 g and a resolution of 0.005 g . Two accelerometers were securely fastened to the tolerance of the subject, on the forehead and the anteromedial surface of distal tibia of the subject with adhesive tape and Velcro straps.

## Synchronization

The force platform, the accelerometers, and the sagittal view video were simultaneously recorded during the experiment. The synchronization between the kinematic and analog signals (the force platform and the accelerometers) was achieved by using a customized trigger device with a light emitting diode (LED).

[^0]

## Ariel

Performance
Analysis
System


Video Camera

Figure 2. Diagram of experimental setup

## Experimental Protocol

Prior to their participation in this study, subjects were briefed on the purpose and the procedures of the study by the principal investigator. On the test day, the subjects were further informed about the purpose, the number of conditions, the number of repetitions, and performance requirements of the study. The test session took approximately 1.0 hour including practice and familiarity with the testing protocol. Forty trials of step-off landing were performed by the subjects in eight conditions. The eight test conditions included landings with and without shoes from four different heights: 30 , 45,60 and 75 cm .

A pilot study was conducted to determine the appropriate highest height for the barefoot landing. Two subjects performed landings from four different heights (30, 45, 60 and 75 cm ) with and without shoes. They were able to land from the 75 cm height in barefoot without changing their landing techniques. The subjects did not show significant changes either in range of motion (ROM) of lower extremity joints or in peak VGRF at the different landing heights across the two surface conditions. The subjects reported the 75 cm landing was within their tolerance. Therefore, the 75 cm was chosen as the highest height for the experiment.

The subject began the test session with a warm-up by riding a stationary bike for five minutes. The retro-reflective markers were placed on the acromioclavicular joint, the greater trochanter, the tibial epicondyle, the lateral malleolus, the heel, and the head of the fifth metatarsal. In the shoe conditions, the last two markers were affixed to the corresponding sites on the lateral side of the shoe. These markers were used to obtain right sagittal kinematics of the subjects during the landing activities.

Anthropometric measurements were obtained before the actual testing. The proximal and distal circumferences and length of lower extremity segments were measured three times (Table 1); the mean value of these measurements was used in the subsequent analyses. The anthropometric measurements were used to estimate inertia characteristics and center of gravity (COG) of each lower extremity segment, and the location of COG of the total body using a mathematical model [16].

Table 1. Anthropometric measurement and definitions

| Anthropometric Measurement |
| :--- |
| FDC $~=~ F o o t ~ D i s t a l ~ C i r c u m f e r e n c e ~$ |
| FPH = Height of lateral malleolus |
| FL = Foot Length |
| LDC = Leg Distal Circumference |
| LPC = Leg Proximal Circumference |
| LL = Leg Length |
| TDC = Thigh Distal Circumference |
| TPC = Thigh Proximal Circumference |
| TL = Thigh Length |
| AMA = Ankle Moment Arm |
| Measurement Definition |
| FDC = Circumferential measurement from the head of first metatarsal to the fifth metatarsal |
| FPH = Height measurement from floor to center of the lateral malleolus |
| FL = Léngth measurement from the lateral malleolus to the head of the fifth metatarsal marker |
| LDC = Circumferential measurement of the ankle superior to the mallelus |
| LPC = Circumferential measurement of widest girth of the leg |
| LL = Length measurement from the ankle to the tibial epicondyle marker |
| TDC = Circumferential measurement of the femur just superior to the femoral epicondyle |
| TPC = Circumferential measurement of the widest girth of the thigh |
| TL = Length measurement from the tibial epicondyle marker to the hip marker |
| AMA = Length measurement from center of the heel marker to midline of the Achille's tendon |

Prior to the experiment, the body weight was measured on the force platform. During the test, the subject was instructed to land with the right foot on the force platform with the left foot on the adjacent floor in a symmetrical manner. The subject performed five step-off landings in each of the eight conditions. The order of the surface conditions was randomized for each height and the height was changed from low $(30 \mathrm{~cm})$ to high ( 75 cm ) height.

## Data Processing

The data processing procedure was divided into two categories: kinematic and kinetic data.

## Kinematic Data

Images collected from the video camera were used to obtain kinematic variables. The data were processed in four steps: capturing, digitizing, decoding/smoothing, and computing. First, a total of 60 frames of video images was captured and stored for each trial on the APAS, with 10 frames prior to and 50 frames following the foot contact with the force platform. Second, the reflective markers were digitized using the APAS. The reference frame was also digitized to obtain scale factors to convert the coordinates of digitized reflective markers from a screen reference system to a lab reference system. The third step involved decoding, smoothing and reconstructing the digitized coordinates using a customized computer program written in Microsoft Visual Basic 6.0. The digitized coordinates were smoothed using an algorithm to obtain optimal cutoff frequencies individually for x and y coordinates of each reflective marker [17]. A

Shannon algorithm was used to reconstruct the video signal from 60 Hz to 240 Hz [14]. In the fourth step, the decoded time-history file was imported into the second customized program to compute linear and angular kinematic variables and determine corresponding discrete events. These variables included contact position/velocity, maximum and time to maximum position/velocity, and minimum and time to minimum position/velocity for the hip, knee, and ankle joints.

## Kinetic Data

Data collected from the force platform and the accelerometers were analyzed in two steps. Analog data file stored on the APAS file was decoded using another Visual Basic program to obtain ASCII time-history of GRF and acceleration data. Second, using the fourth Visual Basic program, the decoded data files were imported to compute and obtain GRF and acceleration variables. These variables included the first (F1) and second (F2) maximum and vertical GRF and the times (T1 and T2) at which they occurred as well as the first and second maximum acceleration values for the head and the tibia and the times at which they occurred.

## Statistical Analysis

Descriptive statistics (means and standard deviations) were calculated for each kinematic and kinetic variable. A two-way (surface $\times$ height, $2 \times 4$ ) analysis of variance (ANOVA) was employed for selected variables with using a statistical package SAS (SAS Institute, Inc., Cary, NC, USA). Post-hoc comparisons were performed using slicing interactions in SAS [32]. The significance level was set at $\mathrm{p}<0.05$.

## Chapter IV

## Results

The purpose of this study was to investigate the shock and impact attenuation during landing activities from different height on different surfaces. The results of the kinematic and kinetic data were obtained for eight different conditions: C1-30 cm with shoe, C2-45 cm with shoe, C3-60 cm with shoe, C4-75 cm with shoe, C5-30 cm without shoe, C6-45 cm without shoe, C7-60 cm without shoe, and C8-75 cm without shoe. Kinematic and kinetic data were collected and analyzed for thirteen male subjects. Among the thirteen subjects, ten subjects landed with a toe-heel landing technique (Group 1) and three subjects landed with a flatfoot landing technique (Group 2) during the experiment. The individual subject results of kinematics, VGRF, and acceleration are provided in Appendix C, D, and E. The following sections mainly focus on the kinematic and kinetic data for Group 1.

## Kinematics

Kinematic variables included the followings of the ankle, knee, and hip joint: contact angle (Cont), maximum angle (Max) and minimum angle (Min), time to Max (Tmax) and Min (Tmin), range of motion (ROM), contact velocity (ContVel), maximum velocity (MaxVel), and time to maximum velocity (TmaxVel). The contact angle is indicative of the joint position at the moment the foot contacts the ground. The maximum joint angle reflects the greatest angle of the joint during the landing phase.

The minimum joint angle reflects the smallest angle during the landing phase. The time to the maximum and minimum joint angle represents how long it takes to reach the maximum and minimum angle. The range of motion is defined as the difference between the maximum and minimum angles during the landing phase. The contact velocity reflects the velocity at the moment the foot contacts the ground. The maximum velocity represents the highest velocity achieved during the landing phase. The time to maximum velocity reflects the time associated with the maximum velocity.

## Ankle Joint

Representative curves of the ankle joint angle and angular velocity are provided in Figure 3. Representative curves of the ankle joint for barefoot at 60 cm are provided in Appendix F. The ankle joint angle was changed from a negative angle at the contact to a positive angle afterwards. A positive angle indicates dorsiflexion and a negative angle indicates plantar flexion. A minimum angle was associated with forefoot contact. A positive ankle angular velocity is associated with dorsiflexion while a negative velocity is associated with plantarflexion.

## Group 1

The two-way ANOVA showed a significant omnibus F for ankle angular ContVel ( $\mathrm{F}=3.47, \mathrm{p}<0.05$ ) and $\operatorname{MaxVel}(\mathrm{F}=8.67, \mathrm{p}<0.05)$. A significant main effect of height was found for the ankle angular ContVel and MaxVel. No significant surface main effect and interactions (surface $\times$ height) were found for these variables. No significant differences were found for the ankle Cont, Max, Min, Tmax, Tmin, ROM, and TmaxVel.

(a) Joint angle

(b) Joint angular velocity

Figure 3. Representative ankle joint curves for shoe at 60 cm (Group 1).

The post-hoc comparison showed that the ContVel at 60 and 75 cm with shoe and barefoot conditions produced significantly higher than the ContVel at 30 cm (Table 2). The post-hoc comparison for the ankle angular MaxVel in the shoe conditions revealed significant differences between 30 and 60 cm , between 30 and 75 cm , between 45 and 60 cm , and between 45 and 75 cm . The ankle angular MaxVel in the shoe conditions at the lower height was smaller than that at the higher height. The ankle angular maximum velocities at 60 and 75 cm with barefoot were significantly greater than that at 30 cm .

## Group 2

The two-way ANOVA showed significant omnibus $F$ for the ankle joint ROM ( $F$ $=4.71, \mathrm{p}<0.05)$, ContVel $(\mathrm{F}=17.92, \mathrm{p}<0.05), \mathrm{MaxVel}(\mathrm{F}=16.47 ; \mathrm{p}<0.05)$, and TmaxVel ( $F=4.90, p<0.05$ ). Significant main of height and surface effects was found for the ankle joint ROM, ContVel, MaxVel, and TmaxVel. No interactions were found for those variables.

The post-hoc comparison for ROM revealed significant differences between 30 and 75 cm in both shoe and barefoot conditions (Table 3). At the heights of 45 and 60 cm , the ankle joint ROM with barefoot were significantly greater than those at the same height with shoes.

Table 2. Means and standard deviations of ankle joint kinematic variables (Group 1).

| Surface | Height | Cont | Max | Tmax | Min | Tmin | ROM | ContVel | MaxVel | Tma |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Shoe | 1 | -14.897 |  | 0.229 | -15.580 | 0.038 | 38.359 | 470.028 | 683.756 |  |
|  |  | (11.25) | (6.900) | (0.091) | (10.476) | (0.095) | (8.854) | (116.647) | (174.354) | (0.006) |
|  | 2 | -16.348 | 25.396 | 0.211 | -16.359 | 0.012 | 41.755 | 634.729 | 835.153 | 0.015 |
|  |  | (10.058) | (7.679) | (0.059) | (10.050) | 0.038) | (7.678) | (71.833) | (118.392) | (0.005) |
|  | 3 | -18.567 | 25.211 | 0.213 | -18.718 | 0.024 | 43.929 | $684.497^{\text {b }}$ | $985.048^{\text {b,d }}$ | 0.015 |
|  |  | (10.72 | (8.311) | (0.055) | (10.356) | (0.076) | (7.882) | (163.268) | (132.952) | (0.007) |
|  | 4 | -17 | 25.73 | 0.205 | -17.503 | 0.031 | 43. | 813.144 | 083.614 | 0.013 |
|  |  | (10.359) | (9.257) | (0.058) | (10.015) | (0.068) | (5.733) | (143.039) | (160.296) | (0.004) |
| Barefoot | 1 | -20.748 | 21.387 | 0.211 | -21.296 | 0.035 | 42.684 | 494.517 | 738.705 | 0.020 |
|  |  | (10.252) | (6.226) | (0.084) | (9.637) | (0.056) | (7.927) | (70.479) | (90.671) | (0.007) |
|  | 2 | -21.694 | 22.047 | 0.214 | -21.694 | 0.000 | 43.741 | 558.961 | 856.479 | 0.020 |
|  |  | (8.576) | (6.896) | (0.083) | (8.576) | (0.000) | (7.434) | (98.373) | (94.936) | (0.006) |
|  | 3 | -19.586 | 22.939 | 0.212 | -19.602 | 0.012 | 42.541 | $694.116^{\text {b }}$ | $952.677^{\text {b }}$ | 0.016 |
|  |  | (8.825) | (7.904) | (0.076) | (8.817) | (0.037) | (5.831) | (138.759) | (83.654) | (0.006) |
|  | 4 | -20.589 | 22.826 | 0.215 | -20.976 | 0.035 | 43.802 | $688.142^{\text {c }}$ | $991.694^{\text {c }}$ | 0.017 |
|  |  | (8.055) | (7.710) | (0.057) | (7.729) | (0.079) | (5.479) | (83.651) | (90.597) | (0.005) |

Note: Angle and ROM units are in degrees and units of time are in s.
Velocity units are in deg/s.
Standard deviation values are in parenthesis.
${ }^{a}$ denotes significant difference between heights 1 and 2 .
${ }^{b}$ denotes significant difference between heights 1 and 3 .
${ }^{\text {c }}$ denotes significant difference between heights 1 and 4.
${ }^{d}$ denotes significant difference between heights 2 and 3.
${ }^{e}$ denotes significant difference between heights 2 and 4.
${ }^{\mathbf{r}}$ denotes significant difference between heights 3 and 4.

* denotes significant difference between the shoe and barefoot conditions on the same landing height.
The definitions of variables are in appendix A.

Table 3. Means and standard deviations of ankle joint kinematic variables (Group 2).

| Surface | Height | Cont | Max | Tmax | Min | Tmin | ROM | ContVel | MaxVel | TmaxVel |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Shoe | 1 | -1.997 | 19.841 | 0.220 | -3.131 | 0.199 | 22.972 | 73.699 | 257.141 | 0.033 |
|  |  | (2.981) | (1.076) | (0.055) | (2.009) | (0.183) | (3.076) | (25.665) | (28.459) | (0.004) |
|  | 2 | -1.319 | 21.585 | 0.193 | -2.032 | 0.157 | 23.617 | 205.781 | 326.495 | 0.036 |
|  |  | (3.833) | (1.125) | (0.041) | (3.854) | (0.059) | (2.730) | (58.986) | (44.121) | (0.017) |
|  | 3 | -5.622 | 21.562 | 0.215 | -5.622 | 0.000 | 27.184 | $389.584^{\text {b,d }}$ | $473.690^{\text {b }}$ | $0.021{ }^{\text {d }}$ |
|  |  | (5.170) | (2.318) | (0.049) | (5.170) | (0.000) | (3.221) | (19.957) | (24.790) | (0.007) |
|  | 4 | -7.835 | 22.390 | 0.196 | -8.771 | 0.080 | $31.162^{\text {c,e }}$ | $548.367{ }^{\text {c, }}$ | $660.024^{\text {c,e, }}$ | $0.010^{\text {c,e }}$ |
|  |  | (8.190) | (3.747) | (0.057) | (6.726) | (0.139) | (3.813) | (185.545) | (170.389) | (0.008) |
| Barefoot | 1 | -6.972 | 21.381 | 0.195 | -7.591 | 0.031 | 28.972 | 290.611* | 435.643 * | 0.020 |
|  |  | (6.652) | (3.700) | (0.036) | (7.164) | (0.052) | (3.674) | (118.810) | (77.052) | (0.007) |
|  | 2 | -11.075 | 21.694 | 0.240 | -11.075 | 0.000 | 32.768 * | $531.685^{\text {a, * }}$ | $630.789^{\text {a, * }}$ | 0.012 * |
|  |  | (4.853) | (2.836) | (0.081) | (4.853) | (0.000) | (2.291) | (40.062) | (65.700) | (0.001) |
|  | 3 | -14.247 | 21.649 | 0.170 | -14.247 | 0.000 | 35.896* | $650.912^{\text {b, * }}$ | $807.347^{\text {b, d, }}$ * | 0.011 |
|  |  | (4.192) | (4.468) | (0.052) | (4.192) | (0.000) | (7.080) | (12.591) | (121.239) | (0.004) |
|  | 4 | -15.754 | 21.823 | 0.178 | -15.754 | 0.000 | $37.577^{\text {c }}$ | $666.482^{\text {c }}$ | $858.314^{\text {ce, } *}$ | 0.014 |
|  |  | (7.846) | (3.121) | (0.043) | (7.846) | (0.000) | (5.936) | (87.387) | (110.575) | (0.004) |

Note: Angle and ROM units are in degrees and units of time are in s.
Velocity units are in deg/s.
Standard deviation values are in parenthesis.
${ }^{\text {a }}$ denotes significant difference between heights 1 and 2 .
${ }^{b}$ denotes significant difference between heights 1 and 3.
${ }^{\text {c }}$ denotes significant difference between heights 1 and 4.
${ }^{\text {d }}$ denotes significant difference between heights 2 and 3 .
${ }^{\mathbf{e}}$ denotes significant difference between heights 2 and 4.
${ }^{\mathrm{f}}$ denotes significant difference between heights 3 and 4 .

* denotes significant difference between the shoe and barefoot conditions on the same landing height.
The definitions of variables are in appendix $A$.

All heights with barefoot for the MaxVel were significantly different except for comparison between 60 and 75 cm . The landing barefoot at each height produced significantly greater maximum angular velocity than landing shoe at the same height. The barefoot landing at 45 cm showed significantly faster time to reach the MaxVel than the shoe condition at the same height.

## Knee Joint

Representative curves of the knee joint angle and angular velocity are provided in Figure 4. Representative curves of the knee joint for barefoot landing at 60 cm are provided in Appendix F. An increasing knee angle indicates knee flexion and a decreasing knee angle indicates knee extension. Positive knee joint angular velocities are associated with angular knee flexion velocity and negative knee joint angular velocities are associated with knee joint extension velocity.

## Group 1

A significant omnibus F was found for knee joint $\operatorname{Max}(\mathrm{F}=2.75, \mathrm{p}<0.05$ ), ROM $(\mathrm{F}=3.80, \mathrm{p}<0.05)$, and $\operatorname{MaxVel}(\mathrm{F}=6.74, \mathrm{p}<0.05)$. Significant main effect of height was found for Max, ROM, and MaxVel. Only MaxVel showed interactions between height and surface conditions. No significant omnibus. $F$ was found for Cont, Min, Tmax, Tmin, ContVel, and TmaxVel.


Figure 4. Representative knee joint curves for shoe at 60 cm (Group 1).

Increased Max knee angles were observed with increased landing heights. The post-hoc comparison revealed that the Max knee angle with shoes was significantly different between 30 and 75 cm , between 45 and 60 cm , and between 45 and 75 cm (Table 4). The Max angle at 30 cm with barefoot was significantly smaller than that at 60 and 75 cm . The post-hoc comparison showed the height of 75 cm in the shoe conditions produced significantly larger ROM than the heights of 30 and 45 cm . The ROM at 30 cm with barefoot was significantly smaller than that at 60 and 75 cm . MaxVel of 60 and 75 cm in the shoe conditions were greater than those of 30 and 45 cm . The heights of 60 and 75 cm with barefoot produced significantly greater MaxVel than 30 cm . The barefoot landing at 45 cm showed significantly greater MaxVel than the shoe landing at the same height.

## Group 2

The ANOVA results demonstrated a significant omnibus F for the knee joint Max angle ( $F=2.68, \mathrm{p}<0.05$ ). A significant main effect of height was found for Max (Appendix H), no interactions and surface main effect were seen that. The post-hoc comparison showed that the height of 75 cm in both shoe and barefoot conditions revealed greater Max angle than the height of 30 cm (Figure 5).

Table 4. Means and standard deviations of knee joint kinematic variables (Group 1).

| Surface | Height | Cont | Max | Tmax | Min | Tmin | ROM | ContVel | MaxVel | TmaxVel |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Shoe | 1 | 29.615 | 81.749 | 0.205 | 22.061 | 0.324 | 59.688 | 332.804 | 612.710 | 析 |
|  |  | (8.036) | (10.269) | (0.075) | (9.945) | (0.226) | (6.640) | (67.268) | (70.457) | (0.014) |
|  | 2 | 32.322 | 91.096 | 0.207 | 26.801 | 0.265 | 64.295 | 385.639 | 661.908 | 0.04 |
|  |  | (6.981) | (11.694) | (0.056) | (11.32) | (0.251) | (7.82) | (62.77) | (65.531) | (0.009) |
|  | 3 | 31.602 | $94.776^{\text {d }}$ | 0.204 | 26.477 | 0.255 | $68.299^{\text {d }}$ | 383.067 | $772.220^{\text {b, }}$ | 0.044 |
|  |  | (7.984) | (11.331) | (0.049) | (10.17 | (0.252) | (7.025) | (86.178) | (90.488) | (0.009) |
|  | 4 | 33.061 | $97.793^{\text {ce }}$ | 0.207 | 27.042 | 0.272 | $70.751^{\text {ce }}$ | 435.266 | $814.584^{\text {ce }}$ | 0.039 |
|  |  | (6.67) | (11.051) | (0.054) | (8.654) | (0.247) | (6.911) | (88.664) | (93.679) | $(0.008)$ |
| Barefoot | 1 | 26.953 | 79.051 | 0.190 | 20.744 | 0.297 | 58.308 | 321.236 | 575.618 | 0.047 |
|  |  | (7.612) | (11.029) | (0.063) | (6.991) | (0.214) | (7.852) | (52.380) | (64.592) | (0.008) |
|  | 2 | 28.032 | 86.785 | 0.193 | 22.103 | 0.293 | 64.682 | 357.270 | 661.327* | 0.047 |
|  |  | (6.541) | (11.454) | (0.048) | (9.057) | (0.233) | (8.077) | (56.445) | (68.570) | (0.007) |
|  | 3 | 31.483 | 94.789 ${ }^{\text {b }}$ | 0.204 | 23.679 | 0.296 | $71.110^{\text {b }}$ | 418.455 | $705.492{ }^{\text {b }}$ | 0.043 |
|  |  | (5.218) | (12.383) | (0.052) | (9.109) | (0.312) | (9.156) | (78.355) | (67.067) | (0.007) |
|  | 4 | 32.344 | $97.660^{\text {c }}$ | 0.198 | 24.359 | 0.287 | $73.301{ }^{\text {c }}$ | 426.975 | $751.067^{\text {c }}$ | 0.043 |
|  |  | (5.280) | (12.786) | (0.048) | (8.935) | (0.288) | (9.790) | (67.232) | (80.036) | (0.007) |

Note: Angle and ROM units are in degrees and units of time are in s.
Velocity units are in deg/s.
Standard deviation values are in parenthesis.
${ }^{\text {a }}$ denotes significant difference between heights 1 and 2 .
${ }^{\mathbf{b}}$ denotes significant difference between heights 1 and 3.
${ }^{\text {c }}$ denotes significant difference between heights 1 and 4.
${ }^{d}$ denotes significant difference between heights 2 and 3.
${ }^{\text {e }}$ denotes significant difference between heights 2 and 4.
${ }^{\mathrm{r}}$ denotes significant difference between heights 3 and 4.

* denotes significant difference between the shoe and barefoot conditions on the same landing height.
The definitions of variables are in Appendix A.


Note: Same shadow of the bar denotes significant difference ( $p<0.05$ ).
Figure 5. Maximum knee joint angle in the shoe conditions (Group 2).

## Hip Joint

Representative curves of the hip joint angle and angular velocity are provided in Figure 6. Representative curves of the hip joint in the barefoot conditions at 60 cm are provided in Appendix F. An increasing hip angle indicates hip flexion and a decreasing hip angle indicates hip extension. Positive hip joint angular velocities are associated with hip angular flexion velocity and negative angular velocities are associated with hip joint extension velocity.

(a) Joint angle

(b) Joint angular velocity

Figure 6. Representative hip joint curves for shoe at 60 cm (Group 1).

## Group 1

The ANOVA results showed significant omnibus F for hip joint $\operatorname{Max}(\mathrm{F}=3.37$, $\mathrm{p}<0.05), \operatorname{ROM}(\mathrm{F}=7.23, \mathrm{p}<0.05)$, ContVel $(\mathrm{F}=2.78, \mathrm{p}<0.05)$, and $\operatorname{MaxVel}(\mathrm{F}=10.35$, $\mathrm{p}<0.05$ ). Significant main effect of height was found for Max, ROM, ContVel, and MaxVel. No interactions and surface main effect were found for those variables. No significant omnibus F was found for Cont, Min, Tmax, Tmin, and TmaxVel.

The post-hoc comparison showed that the Max angle at 75 cm with shoes was greater than that at 30 and 45 cm (Table 5). The height of 30 cm in the barefoot conditions produced significantly smaller Max angle than the heights of 60 and 75 cm . The ROM at 75 cm with shoes was significantly greater than that at 30,45 , and 60 cm . The height of 75 cm in the barefoot conditions produced significantly greater ROM than the heights of 30 and 45 cm . The ROM at 60 cm with barefoot was significantly greater than that at 30 cm .

The ContVel at 75 cm with shoes was significantly greater than that at 45 cm . The height of 75 cm with barefoot produced significantly greater ContVel than the heights of 30 and 45 cm . The ContVel at 30 cm in the barefoot conditions was significantly smaller than that at 60 cm . The MaxVel at 75 cm in the shoe conditions was significantly greater velocity than that at 30 and 45 cm . The height of 60 cm with shoes produced greater MaxVel than the heights of 30 and 45 cm . The height of 75 cm with barefoot was significantly greater MaxVel than the heights of 30 and 45 cm . The MaxVel at 60 cm with barefoot was significantly greater than that at 30 cm .

Table 5. Means and standard deviations of hip joint kinematic variables (Group 1).

| Surface | Height | Cont | Max | Tmax | Min | Tmin | ROM | ContVel | MaxVel | TmaxVel |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Shoe | 1 | 35.214 | 73.058 | 0.232 | 29.889 | 0.286 | 43.169 | 146.057 | 397.449 | 0.052 |
|  |  | (8.718) | (14.024) | (0.087) | (9.198) | (0.258) | (8.708) | (76.674) | (68.837) | (0.016) |
|  | 2 | 36.052 | 80.990 | 0.237 | 31.866 | 0.250 | 49.124 | 160.387 | 438.061 | 0.054 |
|  |  | (5.878) | (16.121) | (0.07) | (9.033) | (0.3) | (10.09) | (47.573) | (77.743) | (0.014) |
|  | 3 | 34.125 | 88.382 | 0.248 | 30.073 | 0.238 | 58.309 b,d | 167.530 | $551.804^{\text {b, d }}$ | 0.053 |
|  |  | (7.324) | (17.923) | (0.093) | (9.035) | (0.269) | (11.757) | (54.013) | (81.491) | (0.010) |
|  | 4 | 35.864 | $97.105^{\text {ce }}$ | 0.264 | 31.741 | 0.241 | $65.364^{\text {ce }}$ | $204.956^{\text {e }}$ | $601.838^{\text {ce }}$ | 0.049 |
|  |  | (6.541) | (17.799) | (0.102) | (6.941) | (0.266) | (14.833) | (38.062) | (80.375) | (0.009) |
| Barefoot | 1 | 34.427 | 74.281 | 0.225 | 29.325 | 0.294 | 44.956 | 130.537 | 382.572 | 0.062 |
|  |  | (9.115) | (20.443) | (0.080) | (8.889) | (0.227) | (13.439) | (65.566) | (67.295) | (0.023) |
|  | 2 | 35.281 | 85.381 | 0.237 | 30.518 | 0.252 | 54.863 | 158.447 | $470.516^{\text {a }}$ | 0.056 |
|  |  | (8.786) | (19.293) | (0.064) | (11.205) | (0.274) | (10.337) | (51.287) | (75.402) | (0.009) |
|  | 3 | 35.254 | $92.921^{\text {b }}$ | 0.244 | 29.586 | 0.300 | $63.336^{\text {b }}$ | $200.924{ }^{\text {b }}$ | $529.044^{\text {b }}$ | 0.055 |
|  |  | (6.823) | (17.951) | (0.069) | (8.437) | (0.316) | (11.057) | (58.425) | (76.214) | (0.013) |
|  | 4 | 36.470 | $102.492^{\text {c }}$ | 0.251 | 31.942 | 0.252 | $70.5511^{\text {c,e }}$ | $229.292^{\text {c e }}$ | $601.722^{\text {c,e }}$ | 0.054 |
|  |  | (8.055) | (19.137) | (0.067) | (8.582) | (0.285) | (13.467) | (52.245) | (75.804) | (0.010) |

Note: Angle and ROM units are in degrees and units of time are in s.
Velocity units are in deg/s.
Standard deviation values are in parenthesis.
${ }^{\text {a }}$ denotes significant difference between heights 1 and 2.
${ }^{\text {b }}$ denotes significant difference between heights 1 and 3 .
${ }^{c}$ denotes significant difference between heights 1 and 4.
${ }^{d}$ denotes significant difference between heights 2 and 3.
${ }^{\mathbf{e}}$ denotes significant difference between heights 2 and 4.
${ }^{\mathrm{f}}$ denotes significant difference between heights 3 and 4 .

* denotes significant difference between the shoe and barefoot conditions on the same landing height.
The definitions of variables are in Appendix A.


## Group 2

A significant omnibus F was found for hip angular $\operatorname{MaxVel}(\mathrm{F}=6.22, \mathrm{p}<0.05) . \mathrm{A}$ significant main effect of height was found for the MaxVel. The post-hoc comparison showed that the MaxVel at 75 cm in the shoe and the barefoot conditions were significantly greater than that at 30 and 45 cm . The height of 60 cm in the shoe and the barefoot conditions produced greater MaxVel than the height of 30 cm . Descriptive statistics for hip joint variables are listed in Appendix H.

## Kinetics

## Vertical Ground Reaction Force

In this section, vertical ground reaction force and acceleration data are presented. Vertical GRF variables included the first ( F 1, forefoot contact) and the second ( F 2, heel contact) maximum VGRF, the time to F 1 (T1) and F2 (T2), the loading rate of F1 (LrateF1) and F2 (LrateF2), and impulse of VGRF from contact to 100 ms (Imp100ms). F1 loading rate was computed as a ratio of F1 and T1. F2 loading rate was computed as ratio of (F2-Fmin)/(T2-Tmin). Representative VGRF curves are shown in Figure 7.

## Group 1

Significant omnibus F was found for $\mathrm{F} 1(\mathrm{~F}=26.15, \mathrm{p}<0.05), \mathrm{F} 2(\mathrm{~F}=4.01$, $\mathrm{p}<0.05$ ), LrateF1 ( $\mathrm{F}=3.95, \mathrm{p}<0.05$ ), and Imp100ms ( $\mathrm{F}=4.55, \mathrm{p}<0.05$ ). Significant main height and surface effects were found for F1,F2, LrateF1, and Imp100ms. No significant omnibus was found for $\mathrm{T} 1, \mathrm{~T} 2$, and LrateF2.

(a) VGRF curve for shoe at 60 cm

(b) VGRF curve for barefoot at 60 cm

Figure 7. Representative VGRF curves (Group 1).

Increased landing heights in the shoe and the barefoot landing were showed to cause significantly greater magnitude of F 1 . The height of 75 cm with shoes produced significantly greater F1 than the same height with barefoot (Figure 8). F2 at 75 cm with shoes and barefoot produced significantly greater forces than that at 30 cm .

LrateF1 at 75 cm in the shoe conditions revealed significantly greater loading rate than that at 30 cm . LrateF1 at 30 cm in the barefoot conditions was significantly smaller than that at 45,60 , and 75 cm . Imp 100 ms at 75 cm with shoes produced significantly greater impulse than that at 30 and 45 cm . Imp 100 ms at 60 cm with shoes was significantly greater than that at 30 cm . For the barefoot, Imp100 ms at 45,60 , and 75 cm was significantly greater than that at 30 cm (Table 6).

## Group 2

Subjects who landed with the flatfoot landing technique did not reveal $\mathrm{F} 1, \mathrm{~T} 1$, and LrateF1 during the experiment. A significant omnibus F was found for $\mathrm{F} 2(\mathrm{~F}=3.59$, $\mathrm{p}<0.05)$ and $\mathrm{T} 2(\mathrm{~F}=2.86, \mathrm{p}<0.05)$. Significant main effects of height and surface were found for F 2 while significant main effect of surface was observed for T 2 (Appendix H ).

The post-hoc comparison showed that the barefoot conditions at 30 cm produced greater magnitude of F 2 than the shoe conditions at the same height (Figure 9). T 2 with shoes at 30,45 , and 60 cm was significantly faster than that with barefoot at each same landing height (Figure 10).


Figure 8. Mean F1 values at different heights (Group 1)
Significant difference was found between the surface conditions at each landing height.

Table 6. Means and standard deviations of vertical ground reaction force variables
(Group 1).

| Surface | Height | F1 | T1 | F2 | T2 | LrateF1 | LrateF2 | Imp 100 ms |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Shoe | 1 | 13.424 | 0.007 | 54.273 | 0.042 | 1953.058 | 1831.765 | 2.525 |
|  |  | (5.039) | (0.004) | (10.071) | (0.014) | (1086.067) | (952.811) | (0.327) |
|  | 2 | $21.460{ }^{\text {a }}$ | 0.008 | 59.279 | 0.044 | 2922.792 | 1965.419 | 2.671 |
|  |  | (3.432) | (0.003) | (13.118) | (0.013) | (1039.659) | (915.225) | (0.368) |
|  | 3 | $29.558^{\text {b,d }}$ | 0.009 | 65.403 | 0.041 | 3592.578 | 2168.216 | $2.911{ }^{\text {b }}$ |
|  |  | (4.774) | (0.003) | (10.030) | (0.009) | (814.218) | (781.164) | (0.377) |
|  | 4 | $36.863^{\text {c, e, }, ~}$ | 0.009 | $75.902^{\text {c }}$ | 0.039 | $4546.078^{\text {c }}$ | 2771.090 | $3.123^{\text {c e }}$ |
|  |  | (7.415) | (0.002) | (17.894) | (0.008) | (1030.121) | (1184.135) | $(0.460)$ |
| Barefoot | 1 | 13.104 | 0.007 | 65.202 | 0.050 | 2623.742 | 1692.260 | 2.237 |
|  |  | (3.590) | (0.004) | (18.683) | (0.012) | (1667.453). | (811.473) | (0.267) |
|  | 2 | $19.415^{\text {a }}$ | 0.006 | 76.169 | 0.045 | $4370.646^{2}$ | 2126.449 | $2.603{ }^{\text {a }}$ |
|  |  | (4.476) | (0.003) | (21.535) | (0.010) | (2605.665) | (937.333) | (0.372) |
|  | 3 | $25.992^{\text {b,d }}$ | 0.007 | 80.965 | 0.045 | $5095.213^{\text {b }}$ | 2305.932 | $2.775^{\text {b }}$ |
|  |  | (5.848) | (0.003) | (27.035) | (0.009) | (3215.794) | (1162.897) | (0.382) |
|  | 4 | 30.897 c,e, ¢, * | 0.008 | $91.241^{\text {c }}$ | 0.043 | $5338.847^{\text {c }}$ | 2857.155 | $2.879^{\text {c }}$ |
|  |  | (6.236) | (0.004) | (27.029) | (0.007) | (2564.041) | (1262.236) | (0.584) |

Note: Force unit is in $\mathrm{N} / \mathrm{kg}$ and time unit is in s .
Loading rate unit is in $\mathrm{N} / \mathrm{kg} / \mathrm{s}$.
Impulse unit is in ( $\mathrm{N} / \mathrm{kg}$ ).s.
Standard deviation values are in parenthesis.
${ }^{a}$ denotes significant difference between heights 1 and 2.
${ }^{\mathbf{b}}$ denotes significant difference between heights 1 and 3.
${ }^{\mathrm{c}}$ denotes significant difference between heights 1 and 4.
${ }^{d}$ denotes significant difference between heights 2 and 3 .
${ }^{e}$ denotes significant difference between heights 2 and 4.
${ }^{\text {f }}$ denotes significant difference between heights 3 and 4.

* denotes significant difference between the shoe and barefoot conditions on the same landing height.
The definitions of variables are in Appendix A.


Figure 9. Mean F2 values at different heights (Group 2)
Significant difference was found between the surface conditions at each landing height.


Figure 10. Mean T2 values at different heights (Group 2)
Significant difference was found between the surface conditions at each landing height.

## Acceleration

Acceleration variables included maximum head acceleration (AccHead), the time to AccHead (TaccHead), the first (AccTibia1) and second (AccTibia2) maximum tibia accelerations, the time to AccTibial (TaccTibial) and AccTibia2 (TaccTibia2), and shock attenuation index (AtteIndex). The AtteIndex is calculated as:

$$
\text { AtteIndex }=\left(1-\frac{\text { AccHead }}{\text { AccTibia } 2}\right) \times 100
$$

Typical head and tibia acceleration curves with shoes at 60 cm are provided in Figure 11; Representative head and tibia acceleration curves with barefoot at 60 cm are provided in Appendix F .

## Group 1

Significant omnibus $F$ was found for AccHead ( $F=4.41, \mathrm{p}<0.05$ ), AccTibial ( F $=12.03, \mathrm{p}<0.05)$, AccTibia2 $(\mathrm{F}=8.10, \mathrm{p}<0.05)$, and AtteIndex $(\mathrm{F}=6.24, \mathrm{p}<0.05)$.

Significant main effects of height and surface were found for AccHead, AccTibial, and AccTibia2. Significant main of surface effect was found for AtteIndex.

For the shoe condition, the post-hoc comparison showed that the AccHead at 75 cm was significantly greater than that at 30 and 45 cm (Table 7). The maximum head acceleration at 75 cm in the shoe conditions was significantly greater than that in the barefoot conditions at the same height.

(a) Head acceleration

(b) Tibia acceleration

Figure 11. Representative acceleration curves for shoe at 60 cm (Group 1).

Table7. Means and standard deviations of acceleration variables (Group 1).

| Surface | Height | AccHead | TaccHead | AccTibial | TaccTibial | AccTibia2 | TaccTibi | AtteIndex |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Shoe | 1 | $\begin{gathered} 2.571 \\ (0.763) \end{gathered}$ | $\begin{gathered} 0.052 \\ (0.011) \end{gathered}$ | $\begin{gathered} 7.821 \\ (5.219) \end{gathered}$ | $\begin{gathered} 0.013 \\ (0.007) \end{gathered}$ | $\begin{aligned} & 18.251 \\ & (8.170) \end{aligned}$ | $\begin{gathered} 0.045 \\ (0.012) \end{gathered}$ | $\begin{aligned} & 84.363 \\ & (5.829) \end{aligned}$ |
|  | 2 | $\begin{gathered} 3.301 \\ (1.079) \end{gathered}$ | $\begin{gathered} 0.053 \\ (0.014) \end{gathered}$ | $\begin{aligned} & 12.073 \\ & (4.424) \end{aligned}$ | $\begin{gathered} 0.016 \\ (0.005) \end{gathered}$ | $\begin{aligned} & 23.816 \\ & (9.582) \end{aligned}$ | $\begin{gathered} 0.046 \\ (0.009) \end{gathered}$ | $\begin{aligned} & 85.235 \\ & (4.131) \end{aligned}$ |
|  | 3 | $\begin{aligned} & 3.631^{b} \\ & (0.974) \end{aligned}$ | $\begin{gathered} 0.050 \\ (0.010) \end{gathered}$ | $\begin{gathered} 17.965^{\mathrm{b}, \mathrm{~d}} \\ (6.074) \end{gathered}$ | $\begin{gathered} 0.016 \\ (0.005) \end{gathered}$ | $\begin{aligned} & 28.508 \\ & (6.705) \end{aligned}$ | $\begin{gathered} 0.044 \\ (0.007) \end{gathered}$ | $\begin{gathered} 87.009 \\ (3.167) \end{gathered}$ |
|  | 4 | $\begin{gathered} 4.463^{\mathrm{c} e} \\ (1.180) \end{gathered}$ | $\begin{gathered} 0.045 \\ (0.006) \end{gathered}$ | $\begin{gathered} 22.840^{c, e, e, ~} \\ (7.631) \\ \hline \end{gathered}$ | $\begin{gathered} 0.016 \\ (0.004) \\ \hline \end{gathered}$ | $\begin{gathered} 38.240^{\mathrm{c}, \mathrm{e}} \\ (9.410) \end{gathered}$ | $\begin{gathered} 0.043 \\ (0.007) \end{gathered}$ | $\begin{aligned} & 88.099 \\ & (2.844) \end{aligned}$ |
| Barefoot | 1 | $\begin{gathered} 2.305 \\ (1.010) \end{gathered}$ | $\begin{gathered} 0.059 \\ (0.013) \end{gathered}$ | $\begin{gathered} 7.473 \\ (2.382) \end{gathered}$ | $\begin{gathered} 0.017 \\ (0.006) \end{gathered}$ | $\begin{gathered} 30.101 \\ (12.868) \end{gathered}$ | $\begin{gathered} 0.054 \\ (0.008) \end{gathered}$ | $\begin{gathered} 90.608 \text { * } \\ (5.625) \end{gathered}$ |
|  | 2 | 2.687 | 0.052 | 10.843 | 0.016 | 37.688 | 0.050 | 91.730* |
|  |  | (1.141) | (0.009) | (2.991) | (0.005) | (15.471) | (0.008) | (4.874) |
|  | 3 | 2.961 | 0.050 | $14.656{ }^{\text {b }}$ | 0.016 | $47.494^{\text {b }}$ * | 0.049 | 92.076* |
|  |  | (1.108) | (0.011) | (4.278) | (0.005) | (24.881) | (0.007) | (4.567) |
|  | 4 | 3.220 * | 0.047 | $17.454^{\text {c,e, } *}$ | 0.017 | $63.943^{\text {c,e, }, ~}$, | 0.047 | 93.958* |
|  |  | (0.936) | (0.007) | (3.962) | (0.005) | (27.666) | (0.005) | (3.010) |

Note: Acceleration unit is in $g$ and time unit is in $s$.
Shock attenuation index unit is in \%.
Standard deviation values are in parenthesis.
${ }^{a}$ denotes significant difference between heights 1 and 2.
${ }^{\text {b }}$ denotes significant difference between heights 1 and 3 .
${ }^{c}$ denotes significant difference between heights 1 and 4.
${ }^{d}$ denotes significant difference between heights 2 and 3.
${ }^{e}$ denotes significant difference between heights 2 and 4.
${ }^{\text {f }}$ denotes significant difference between heights 3 and 4.

* denotes significant difference between the shoe and barefoot conditions on the same landing height.
The definitions of variables are in Appendix A.

Increased landing heights caused increased AccTibial values. The AccTibial at all heights in the shoe conditions was significantly different except for comparisons between 30 and 45 cm . AccTibial with barefoot at 75 cm was significantly greater than that at 30 and 45 cm . The barefoot at 60 cm produced greater AccTibial than the barefoot at 30 cm . The shoe condition at 75 cm produced greater AccTibial than the barefoot condition at the same height.

The AccTibia2 at 75 cm in the shoe conditions was significantly greater than that at 30 and 45 cm . For the barefoot condition, the height of 75 cm produced significantly greater AccTibia2 than 30, 45, and 60 cm . AccTibia2 at 60 and 75 cm with barefoot were significantly greater than those with shoes at each same height. The shock attenuation index with barefoot at all heights were significantly greater than those with shoes at each height (Figure 12).


Figure 12. Mean shock attenuation index values at different heights (Group 1)
Significant difference was found between the surface conditions at each landing height.

## Group 2

A significant omnibus $F$ was found for AccTibia2 $(F=5.51, p<0.05)$ and TaccTibia2 ( $\mathrm{F}=3.04, \mathrm{p}<0.05$ ). Significant main effects of height and surface were found for AccTibia2. A significant surface effect was also found for TaccTibia2.

For the barefoot condition, the post-hoc comparison showed that the AccTibia2 at 30 cm was significantly smaller than that at 60 and 75 cm (Appendix H). The barefoot conditions at 60 and 75 cm produced significantly greater AccTibia2 than the shoe conditions at the same height (Figure 13). The TaccTibia2 with shoes at 45 and 60 cm were significantly less than those with barefoot at the same height.


Figure 13. Mean AccTibia2 values at different heights (Group 2)
Significant difference was found between the surface conditions at each landing height.

## Chapter V

## Discussion and Conclusions

## Discussion

The purpose of this study was to investigate impact force and shock attenuation during landings from different heights on different surface conditions. The vertical ground reaction force, accelerometer data, and kinematic variables were examined and analyzed. In this chapter only the results of group 1 will be discussed.

The first maximum VGRF (F1) significantly varied with increased heights and changed surface conditions. The F1 values at all landing heights were significantly different from each other for both surface conditions. F1 increased from $13.42 \mathrm{~N} / \mathrm{kg}$ at 30 cm to $36.86 \mathrm{~N} / \mathrm{kg}$ in the shoe conditions, and from $13.10 \mathrm{~N} / \mathrm{kg}$ at 30 cm to $30.90 \mathrm{~N} / \mathrm{kg}$ at 75 cm in the barefoot conditions (Table 6). The effect of shoe condition for F1 was statistically significant at 75 cm level. At the other heights, F 1 did not show significant changes, but demonstrated a trend of greater values in the shoe conditions than that in the barefoot conditions. This result is initially counterintuitive and greater $F 1$ values for the barefoot are expected since impact forces are expected to increase without shoe protection. The occurrence of F1 is associated with the forefoot contact with the ground. The contact and maximum ankle angular velocities may indicate how the forefoot and ankle joint are controlled at and after the touchdown. Further examinations of the ankle angular kinematics suggest that the contact and maximum angular velocities at 75 cm . with the shoe landing were greater than those with the barefoot landing (Table 2). These
data may indicate that the ankle plantarflexors are less active in the shoe conditions. This result may also suggest that the subjects were sensitive to the changes of surfaces at the forefoot contact, and were able to cope with such changes with neuromuscular intervention.

The present study presented a different F1 pattern than has been previously reported in walking and running studies. Cavanagh et al. [3] examined impact force during walking with three different shoes (Army boot, Leather street shoe, and Crepe soled casual shoe) and barefoot. The first maximum VGRF in the barefoot condition ( 0.55 BW ) was significantly greater than that in any shoe conditions. F1 with army boots, leather street shoes, and crepe soled casual shoes were $0.37,0.27$, and 0.25 BW , respectively. Lafortune et al. [20] reported a significant difference for the initial peak of VGRF between the barefoot and shoe conditions (street shoes and athletic shoes) during walking. F1 with the barefoot ( 0.69 BW ) was significantly greater than that with the street shoes ( 0.48 BW ) as well as with the athletic shoes ( 0.44 BW ). However, F1 did not show any significance between shoe and barefoot in running studies. F1 in barefoot running (2.25 BW ) was slightly higher than that in the shoe running ( 2.11 BW ) for one subject [4]. Wit et al. [38] found that the difference F1 was not significant, but F1 in the barefoot running showed slightly higher magnitude than that in the shoe running.

The second maximum VGRF (F2) demonstrated a different trend across the surface conditions compared with the changes of F1. Even though they were not significant, the F2 values for the barefoot were generally greater than those for the shoe conditions (Table 6). The F2 event occurs at the time of heel contact with the ground after the initial forefoot contact. It was found that VGRF with barefoot was 1.1 times
(4.3 BW) greater than that with shoes during netball landings [35]. This reversal of responses of the shoe and barefoot was not observed in running studies. In the study conducted by Wit et al. [38], the F2 values between shoe and barefoot running were same (2.9 BW) at a speed of $4.5 \mathrm{~m} / \mathrm{s}$.

An explanation of the mechanisms of different VGRF responses at the forefoot contact and heel contact in the shoe and barefoot conditions are attempted below. F1 with shoe was slightly greater than that with barefoot whereas F2 with barefoot was slightly greater than that with shoes. Impact forces in landing usually occur within 50 ms that is beyond the human reaction time. Any attempt to reduce impact forces during the impact phase is preprogrammed by the neuromuscular system prior to the touchdown [23]. The preset neuromuscular program intension is rather effective in reducing F1 in the barefoot conditions. The heel contact occurs at a later time than forefoot contact. The neuromuscular intervention may be therefore, less effective reducing F2 at the heel contact than at the forefoot contact. The reaction of kinematic variables could be indicative of muscular responses. In this study, the contact angle and the range of motion of the ankle, knee, and hip joints did not show any significant differences across surface conditions. It is, therefore, suggested that the shoe provided an additional capacity to attenuate impact forces.

The loading rate of F1 (LrateF1) indicates how fast mechanical load is applied to the body from contact to F1. LrateF1 at 75 cm with shoes was significantly faster than that at 30 cm (Table 6). Even though there was no statistical difference for LrateF1 across surface conditions, LrateF1 in the barefoot conditions presented a trend of greater values than that in the shoe conditions. This result is in agreement with the running
studies conducted by Wit et al. [38] and De Clercq et al. [4]. The barefoot running produced greater F1 loading rate than the shoe running.

As mentioned early, increased first and second maximum VGRF were observed with increased landing heights. In the study conducted by Dufek and Bates [7], the landing height was a significant main effect for $F 1$. F 1 values at 40,60 , and 100 cm were 1.23, 1.31, and 2.15 BW, respectively. McNitt-Gray [24] reported increased VGRF magnitude with increased landing height. The VGRF was $4.2,6.4$, and 9.1 BW for recreational athletes, and 3.9, 6.3, and 11.0 BW for gymnastic athletes landings from 32 , 72 , and 128 cm , respectively. Ozguven et al. [29] reported that greater VGRF values were associated with increased heights. Subjects landing from 2.55 m produced VGRF ranged from 8.2 to 11.7 BW whereas subjects who landing from 0.45 m produced VGRF ranged from 5.0 to 7.0 BW .

The maximum head acceleration (AccHead) significantly demonstrated minimum amount of changes with changes in heights and surfaces. AccHead ranged from 2.57 g at 30 cm to 4.46 g at 75 cm in the shoe conditions, and from 2.30 g at 30 cm to 3.22 g at 75 cm in the barefoot conditions. Only AccHead with shoes was statistically greater than that with barefoot at 75 cm . AccHead with shoe displayed statistically significant increases with increased height, however the increases were incredibly small. The AccHead values with barefoot remained relatively constant across heights. This finding is in partial agreement with several previous studies [15,33,39]. The maximum head acceleration was shown to be constant during barefoot walking [39]. During treadmill running, the maximum head acceleration did not change with increased treadmill speed
$[15,33]$. The constant AccHead values indicate that a body serves as a low pass filter and shock absorber during landings.

The first maximum tibia acceleration (AccTibial) demonstrated a similar trend as F1 of VGRF across surface and height conditions. AccTibial showed significantly greater changes with increased heights in the shoe and barefoot conditions. AccTibial with shoe demonstrated generally greater values than those with barefoot, with statistically significant difference found between the shoes and barefoot at 75 cm . AccTibial occurs at the forefoot contact when F1 is observed. As mentioned early, changes in surface conditions and corresponding preprogrammed neuromuscular responses could be responsible for the similar trends of AccTibial and F1 across the surface conditions.

The second maximum tibia acceleration (AccTibia2) revealed statistical differences across height and surface conditions. AccTibia2 occurs at the time of the heel contact when F2 is observed. The AccTibia2 values increased from 18.25 g at 30 cm to 38.24 g at 75 cm , and from 30.10 g at 30 cm to 63.94 g at 75 cm with shoe and barefoot, respectively. AccTibia2 displayed a different pattern compared with the AccTibial: the barefoot landing was significantly greater than the shoe landing at 60 and 75 cm . At the same time, kinematic results of lower extremity joints did not show any significant changes at these heights across the surface conditions. The contact angle and range of motion of ankle, knee, and hip joint did not change significantly across surface conditions. Due to the preset neuromuscular program, ankle plantarflexors were more active in the barefoot conditions than in the shoe conditions. Such a neuromuscular intervention has a greater effect on impact attenuation at the forefoot contact than at the heel contact
because the heel contact occurs at a much later time than the forefoot contact. The smaller AccTibia2 values with shoe at 60 and 75 cm indicated that shoes added additional cushioning capacity in comparison to the barefoot conditions. However, the peak calcaneal and tibial accelerations did not show any significant difference across the three surface conditions in the Gross and Nelson 's study [13]. The average of peak calcaneus and tibia accelerations across the three surfaces was 20.8 and 14.3 g , respectively. Because the subjects were asked to land from a vertical jump, the input energy and landing heights were not controlled in the study, which could influence the results.

The AccHead values were much lower than the AccTibia values. The AccHead and AccTibial with shoe were 4.46 and 22.84 g at 75 cm , respectively. Similar differences were found for the barefoot landings. Shorten and Winslow [33] reported that the head acceleration was much less than the tibia acceleration at higher frequencies (above 6 Hz ) whereas the head acceleration was much higher than the tibia acceleration at lower frequencies (below 6 Hz ). The peak head acceleration was constant across a range of impact shock levels. Wosk and Voloshin [39] also indicated that the peak forehead acceleration was less than the peak tibia acceleration. It was suggested that the body serves as a filter minimizing the impact shock transmitted to the head. The shock attenuation index (AtteIndex) indicates that how much impact shock is attenuated by the human body. A higher AtteIndex value indicates greater shock attenuation while a smaller AtteIndex indicates lesser shock attenuation. The result demonstrated that the AtteIndex with barefoot was significantly greater than those with shoe at all landing heights (Table 7). The AtteIndex, for example, was 87 and $92 \%$ for the shoe and barefoot at 60 cm , respectively. This result suggested that impact shock in the barefoot
condition was more attenuated than in the shoe conditions. It is logical to assume that the shoes can provide additional impact shock. Impact shock may be attenuated through passive structures such as bones and soft tissues [39]. Impact shock can also be minimized by active muscle contraction. Subjects may change their landing strategies in order to protect their body from injury in the barefoot landings. Even though the kinematic results did not show any significant changes across the surface conditions, they seemed to be more cautious in the barefoot conditions than in the shoe conditions.

## Conclusions

For the vertical ground reaction force, four variables (F1, F2, LrateF1, and Imp100ms) showed significant height effect. Greater values of these four variables increased with increased landing heights. F1 values with shoe were slightly greater than that of the barefoot conditions. On the other hand, the barefoot conditions produced greater F2 than the shoe conditions even though the results were not significant. The ankle, knee, and hip joint kinematic variables also showed a similar pattern. The range of motion and the maximum angular velocity of these joints increased with increased landing heights. At the forefoot contact, it is suggested that the ankle muscles were more active in the barefoot conditions than in the shoe conditions, therefore they played an important role in impact attenuation. It is also suggested that the shoes provided an additional cushion to minimize impact forces during landings.

The accelerometer results indicated four significant variables: AccHead, AccTibial, AccTibia2, and AtteIndex. These variables except for AccHead demonstrated greater values with increased heights. The increased values of the

AccHead were relatively small while the AccTibia changes were much more significant. It is suggested that the body serves as a filter minimizing impact shock transmission to the head. The values of the AccTibial with shoes were greater than those with barefoot conditions whereas the AccTibia2 values with shoes were smaller than those with barefoot. These results along with the results of VGRF suggest that the shoe added a substantial amount of cushion and impact shock attenuation. The AtteIndex values in the barefoot conditions were also greater than those in the shoe conditions.

Recommendations for further studies can be derived from the experiences of this study. An accelerometer needs to be carefully and securely attached to subjects. In this study, the accelerometers were attached to the tibia and forehead of the subjects using athletic tape and Velcro straps. During the experiment, repetitive landing performances sometimes caused the Velcro straps to loosen up, therefore induced noisy signals of accelerations. It would be ideal to find a better way to fix an accelerometer to the skin of subjects. Subject populations of this study were healthy and active, but some of them were not skilled in jumping and landing. It would be more interesting how skilled athletes would attenuate impact shock with using their consistent landing techniques.

This study presented accurate information of the impact force, accelerometer data, and kinematics regarding to different surface conditions from different heights during landings. Future studies need to explore neuromuscular changes of the human body in impact attenuation during landing activities. It is necessary to examine the relationship between muscle activities of lower extremity joints and impact shock attenuation during landing activities.

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## APPENDICES

## APPENDIX A

## DEFINITIONS OF VARIABLES

## DEFINITIONS OF VARIABLES

## Kinematics

| Cont | Contact joint angle at ground contact |
| :--- | :--- |
| Max | Maximum joint angle |
| Tmax | Time to maximum joint angle |
| Min | Minimum joint angle |
| Tmin | Time to minimum joint angle |
| ROM | Range of motion of joint |
| ContVel | Angular joint velocity at ground contact |
| MaxVel | Angular joint maximum velocity |
| TmaxVel | Time to angular joint maximum velocity |

## VGRF

F1 First maximum vertical ground reaction force
T1 : Time to first maximum vertical ground reaction force
F2 Second maximum vertical ground reaction force
T2 Time to second maximum vertical ground reaction force
LrateF1 Loading rate of the first maximum vertical ground reaction force
LrateF2 Loading rate of the second maximum vertical ground reaction force
Imp100ms Impulse of vertical ground reaction force from contact to 100 ms

## Acceleration

AccHead Maximum head acceleration
TaccHead Time to maximum head acceleration
AccTibial First maximum tibia acceleration
TaccTibial Time to the first maximum tibia acceleration
AccTibia2 Second maximum tibia acceleration
TaccTibia2 Time to the second maximum tibia acceleration
AtteIndex Shock attenuation index

## APPENDIX B

## SUBJECT INFORMATION

Table 8. Subject information

| Group | Subject | Age | Body Weight (kg) | Height (cm) |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 19 | 72.28 | 182.88 |
|  | 2 | 20 | 78.03 | 177.8 |
|  | 3 | 19 | 82.68 | 187.96 |
|  | 4 | 28 | 81.39 | 187.96 |
| 1 | 5 | 21 | 55.33 | 172.72 |
|  | 6 | 21 | 71.05 | 180.34 |
|  | 7 | 18 | 88.00 | 187.96 |
|  | 8 | 20 | 73.06 | 180.34 |
|  | 9 | 20 | 84.93 | 190.5 |
|  | 10 | 18 | 83.16 | 180.34 |
| Mean |  | 20.4 | 76.99 | 182.88 |
| S.D. |  | 2.88 | 9.52 | 5.61 |
|  | 1 | 30 | 72.38 | 180.34 |
| 2 | 2 | 21 | 86.38 | 175.26 |
|  | 3 | 21 | 74.94 | 182.88 |
| Mean |  | 24 | 77.90 | 179.49 |
| S.D. |  | 5.2 | 7.45 | 3.87 |

## APPENDIX C

## KINEMATIC DATA

Table 9. Subject means and standard deviations of ankle joint variables (Group 1).

| Subj | ond | Cont | Max | Tmax | Min | Tmin | ROM | ContVel | MaxVel | TmaxVel |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | $\begin{array}{\|l\|} \hline-21.158 \\ (4.674) \end{array}$ | $\begin{aligned} & 27.826 \\ & (2.254) \end{aligned}$ | $\begin{gathered} \hline 0.178 \\ (0.017) \end{gathered}$ | $\begin{aligned} & -21.158 \\ & (4.674) \end{aligned}$ | $\begin{gathered} \hline 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 48.984 \\ & (5.642) \end{aligned}$ | $\begin{gathered} 332.752 \\ (268.990) \end{gathered}$ | $\begin{gathered} 822.666 \\ (128.794) \end{gathered}$ | $\begin{gathered} 0.029 \\ (0.012) \end{gathered}$ |
|  | 2 | $\begin{aligned} & -13.057 \\ & (4.902) \end{aligned}$ | $\begin{aligned} & 31.486 \\ & (1.586) \end{aligned}$ | $\begin{gathered} 0.211 \\ (0.045) \end{gathered}$ | $\begin{aligned} & -13.057 \\ & (4.902) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 44.543 \\ & (3.410) \end{aligned}$ | $\begin{gathered} 593.577 \\ (121.814) \end{gathered}$ | $\begin{gathered} 702.967 \\ (39.084) \end{gathered}$ | $\begin{gathered} 0.016 \\ (0.008) \end{gathered}$ |
|  | 3 | $\begin{aligned} & -25.262 \\ & (6.180) \end{aligned}$ | $\begin{aligned} & 31.691 \\ & (1.572) \end{aligned}$ | $\begin{aligned} & 0.233 \\ & (0.072) \end{aligned}$ | $\begin{array}{r} -25.262 \\ (6.180) \end{array}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 56.953 \\ & (6.050) \end{aligned}$ | $\begin{gathered} 321.26 \\ (312.20 \end{gathered}$ | $\begin{aligned} & 1035.753 \\ & (53.295) \end{aligned}$ | $\begin{gathered} 0.030 \\ (0.007) \end{gathered}$ |
|  | 4 | $\begin{aligned} & -15.443 \\ & (12.287) \end{aligned}$ | $\begin{gathered} 38.147 \\ (14.832 \end{gathered}$ | $\begin{gathered} 0.281 \\ (0.111) \end{gathered}$ | $\begin{aligned} & -15.443 \\ & (12.287) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{gathered} 53.59 \\ (22.832) \end{gathered}$ | $\left(\begin{array}{c} 886.838 \\ (171.805) \end{array}\right.$ | $\begin{aligned} & 1185.902 \\ & (138.020) \end{aligned}$ | $\begin{gathered} 0.013 \\ (0.008) \end{gathered}$ |
|  | 5 | $\begin{aligned} & -19.952 \\ & (7.069) \end{aligned}$ | $\begin{aligned} & 26.390 \\ & (1.618) \end{aligned}$ | $\begin{gathered} 0.156 \\ (0.022) \end{gathered}$ | $\begin{aligned} & -19.952 \\ & (7.069) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 46.342 \\ & (6.519) \end{aligned}$ | $\begin{gathered} 523.228 \\ (245.541) \end{gathered}$ | $\begin{aligned} & 824.585 \\ & (30.028) \end{aligned}$ | $\begin{gathered} 0.020 \\ (0.014) \end{gathered}$ |
|  | 6 | $\begin{aligned} & -22.547 \\ & (5.420) \end{aligned}$ | $\begin{aligned} & 23.554 \\ & (1.505) \end{aligned}$ | $\begin{gathered} 0.176 \\ (0.034) \end{gathered}$ | $\begin{aligned} & -22.547 \\ & (5.420) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 46.101 \\ & (5.724) \end{aligned}$ | $\begin{gathered} 663.317 \\ (203.491 \end{gathered}$ | $\begin{aligned} & 943.682 \\ & (60.223) \end{aligned}$ | $\begin{gathered} 0.018 \\ (0.006) \end{gathered}$ |
|  | 7 | $\begin{aligned} & -14.673 \\ & (9.352) \end{aligned}$ | $\begin{aligned} & 27.664 \\ & (1.849) \end{aligned}$ | $\begin{gathered} 0.196 \\ (0.058) \end{gathered}$ | $\begin{aligned} & -14.673 \\ & (9.352) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{gathered} 42.337 \\ (10.284) \end{gathered}$ | $\begin{gathered} 954.680 \\ (112.418) \end{gathered}$ | $\begin{aligned} & 1077.978 \\ & (75.370) \end{aligned}$ | $\begin{gathered} 0.008 \\ (0.007) \end{gathered}$ |
|  | 8 | $\begin{aligned} & -25.392 \\ & (6.352) \end{aligned}$ | $\begin{aligned} & 27.832 \\ & (2.564) \end{aligned}$ | $\begin{gathered} 0.238 \\ (0.094) \end{gathered}$ | $\begin{aligned} & -25.392 \\ & (6.352) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{gathered} 53.224 \\ (5.928) \end{gathered}$ | $\begin{gathered} 693.255 \\ (221.926) \end{gathered}$ | $\begin{aligned} & 1096.425 \\ & (160.177) \end{aligned}$ | $\begin{gathered} 0.018 \\ (0.010) \end{gathered}$ |
| 2 | 1 | $\begin{aligned} & -31.363 \\ & (6.230) \end{aligned}$ | $\begin{gathered} 9.542 \\ (2.086) \end{gathered}$ | $\begin{gathered} 0.410 \\ (0.217) \end{gathered}$ | $\begin{aligned} & -31.363 \\ & (6.230) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 40.905 \\ & (6.942) \end{aligned}$ | $\begin{gathered} 541.859 \\ (124.115) \end{gathered}$ | $\begin{aligned} & 776.305 \\ & (94.946) \end{aligned}$ | $\begin{gathered} 0.018 \\ (0.003) \end{gathered}$ |
|  | 2 | $\begin{aligned} & -27.162 \\ & (6.059) \end{aligned}$ | $\begin{aligned} & 11.535 \\ & (1.813) \end{aligned}$ | $\begin{gathered} 0.226 \\ (0.098) \end{gathered}$ | $\begin{aligned} & -27.162 \\ & (6.059) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 38.697 \\ & (7.607) \end{aligned}$ | $\begin{aligned} & 717.213 \\ & (98.570) \end{aligned}$ | $\begin{aligned} & 894.856 \\ & (88.746) \end{aligned}$ | $\begin{gathered} 0.012 \\ (0.006) \end{gathered}$ |
|  | 3 | $\begin{aligned} & -31.898 \\ & (4.898) \end{aligned}$ | $\begin{aligned} & 10.284 \\ & (1.158) \end{aligned}$ | $\begin{gathered} 0.194 \\ (0.046) \end{gathered}$ | $\begin{aligned} & -31.898 \\ & (4.898) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 42.182 \\ & (5.655) \end{aligned}$ | $\begin{gathered} 607.041 \\ (190.901 \end{gathered}$ | $\begin{aligned} & 967.331 \\ & (45.531) \end{aligned}$ | $\begin{gathered} 0.018 \\ (0.007) \end{gathered}$ |
|  | 4 | $\begin{aligned} & -33.333 \\ & (5.851) \end{aligned}$ | $\begin{aligned} & 10.258 \\ & (0.730) \end{aligned}$ | $\begin{gathered} 0.140 \\ (0.019) \end{gathered}$ | $\begin{aligned} & -33.333 \\ & (5.851) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 43.591 \\ & (5.635) \end{aligned}$ | $\begin{gathered} 856.430 \\ (155.240) \end{gathered}$ | $\begin{aligned} & 1217.495 \\ & (69.951) \end{aligned}$ | $\begin{gathered} 0.012 \\ (0.005) \end{gathered}$ |
|  | 5 | $\begin{aligned} & -32.733 \\ & (5.793) \end{aligned}$ | $\begin{aligned} & 11.099 \\ & (2.330) \end{aligned}$ | $\begin{gathered} 0.185 \\ (0.010) \end{gathered}$ | $\begin{aligned} & -32.733 \\ & (5.793) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 43.832 \\ & (6.898) \end{aligned}$ | $\begin{gathered} 516.166 \\ (141.659 \end{gathered}$ | $\begin{aligned} & 806.890 \\ & (68.132) \end{aligned}$ | $\begin{gathered} 0.019 \\ (0.008) \end{gathered}$ |
|  | 6 | $\begin{aligned} & -31.075 \\ & (4.013) \end{aligned}$ | $\begin{aligned} & 12.469 \\ & (2.024) \end{aligned}$ | $\begin{gathered} 0.169 \\ (0.015) \end{gathered}$ | $\begin{aligned} & -31.075 \\ & (4.013) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 43.544 \\ & (5.610) \end{aligned}$ | $\begin{gathered} 587.856 \\ (144.905) \end{gathered}$ | $\begin{aligned} & 912.277 \\ & (56.028) \end{aligned}$ | $\begin{gathered} 0.019 \\ (0.006) \end{gathered}$ |
|  | 7 | $\begin{aligned} & -33.208 \\ & (5.279) \end{aligned}$ | $\begin{aligned} & 11.403 \\ & (1.338) \end{aligned}$ | $\begin{gathered} 0.173 \\ (0.074) \end{gathered}$ | $\begin{aligned} & -33.208 \\ & (5.279) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 44.611 \\ & (4.498) \end{aligned}$ | $\left[\begin{array}{c} 733.103 \\ (158.991) \end{array}\right.$ | $\begin{aligned} & 1076.460 \\ & (83.295) \end{aligned}$ | $\begin{gathered} 0.015 \\ (0.007) \end{gathered}$ |
|  | 8 | $\begin{array}{\|l} -30.453 \\ (7.656) \\ \hline \end{array}$ | $\begin{array}{r} 12.811 \\ (11.021 \\ \hline \end{array}$ | $\begin{array}{r} 0.247 \\ \times(0.200) \\ \hline \end{array}$ | $\begin{array}{r} -30.453 \\ (7.656) \\ \hline \end{array}$ | $\begin{gathered} 0.000 \\ (0.000) \\ \hline \end{gathered}$ | $\begin{gathered} 43.264 \\ (16.195) \end{gathered}$ | $\begin{gathered} 621.042 \\ (220.235) \end{gathered}$ | $\begin{array}{r} 991.186 \\ +(131.139) \\ \hline \end{array}$ | $\begin{gathered} 0.017 \\ (0.010) \end{gathered}$ |

Table 9. (Continued).

| Subj | ond | Cont | Max | $\mathrm{T}_{\text {max }}$ | Min | Tmin | ROM | ContVel | MaxVel | TmaxVel |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | 1 | $\begin{gathered} -10.128 \\ (13.529) \end{gathered}$ | $\begin{aligned} & 22.353 \\ & (1.433) \end{aligned}$ | $\begin{gathered} 0.142 \\ (0.020) \end{gathered}$ | $\begin{aligned} & -11.657 \\ & (10.851) \end{aligned}$ | $\begin{gathered} 0.075 \\ (0.184) \end{gathered}$ |  | $\begin{aligned} & 637.59 \\ & (232.39 \end{aligned}$ | $\begin{aligned} & 745.427 \\ & (256.506) \end{aligned}$ | $\begin{gathered} \hline 0.008 \\ (0.009) \end{gathered}$ |
|  | 2 | $\begin{aligned} & -11.486 \\ & (6.815) \end{aligned}$ | $\begin{aligned} & 28.513 \\ & (2.231) \end{aligned}$ | $\begin{gathered} 0.193 \\ (0.048) \end{gathered}$ | $\begin{aligned} & -11.486 \\ & (6.815) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 39.998 \\ & (8.816) \end{aligned}$ | $\begin{gathered} 780.64 \\ (134.27 \end{gathered}$ | $\begin{aligned} & 893.862 \\ & (49.923) \end{aligned}$ | $\begin{gathered} 0.009 \\ (0.008) \end{gathered}$ |
|  | 3 | $\begin{aligned} & -20.110 \\ & (7.646) \end{aligned}$ | $\begin{aligned} & 29.176 \\ & (3.122) \end{aligned}$ | $\begin{gathered} 0.191 \\ (0.025) \end{gathered}$ | $\begin{aligned} & -20.110 \\ & (7.646) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 49.286 \\ & (8.525) \end{aligned}$ | $\begin{gathered} 677.182 \\ (136.799) \end{gathered}$ | $\begin{gathered} 1083.655 \\ (197.935) \end{gathered}$ | $\begin{gathered} 0.016 \\ (0.008) \end{gathered}$ |
|  | 4 | $\begin{gathered} -4.177 \\ (15.629) \end{gathered}$ | $\begin{aligned} & 30.736 \\ & (0.868) \end{aligned}$ | $\begin{gathered} 0.195 \\ (0.058) \end{gathered}$ | $\begin{gathered} -6.758 \\ (12.443) \end{gathered}$ | $\begin{gathered} 0.194 \\ (0.300) \end{gathered}$ | $\begin{gathered} 37.494 \\ (12.823) \end{gathered}$ | $\left.\right\|_{\mid 894.739} ^{(274.650}$ | $\begin{aligned} & 1040.554 \\ & (275.758) \end{aligned}$ | $\begin{gathered} 0.006 \\ (0.009) \end{gathered}$ |
|  | 5 | $\begin{aligned} & -21.339 \\ & (3.763) \end{aligned}$ | $\begin{aligned} & 22.611 \\ & (2.581) \end{aligned}$ | $\begin{gathered} 0.165 \\ (0.022) \end{gathered}$ | $\begin{aligned} & -21.339 \\ & (3.763) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 43.950 \\ & (5.076) \end{aligned}$ | $\left\lvert\, \begin{gathered} 518.145 \\ (139.267) \end{gathered}\right.$ | $\begin{aligned} & 784.843 \\ & (41.660) \end{aligned}$ | $\begin{gathered} 0.021 \\ (0.006) \end{gathered}$ |
|  | 6 | $\begin{aligned} & -25.854 \\ & (1.742) \end{aligned}$ | $\begin{aligned} & 26.870 \\ & (0.891) \end{aligned}$ | $\begin{gathered} 0.244 \\ (0.071) \end{gathered}$ | $\begin{aligned} & -25.854 \\ & (1.742) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 52.724 \\ & (2.262) \end{aligned}$ | $\begin{aligned} & 381.573 \\ & (38.834) \end{aligned}$ | $\begin{aligned} & 928.712 \\ & (33.454) \end{aligned}$ | $\begin{gathered} 0.027 \\ (0.002) \end{gathered}$ |
|  | 7 | $\begin{aligned} & -15.936 \\ & (11.237) \end{aligned}$ | $\begin{aligned} & 26.826 \\ & (2.246) \end{aligned}$ | $\begin{gathered} 0.278 \\ (0.073) \end{gathered}$ | $\begin{array}{r} -16.09 \\ (10.88 \end{array}$ | $\begin{gathered} 0.118 \\ (0.265) \end{gathered}$ | $\begin{aligned} & 42.926 \\ & (9.998) \end{aligned}$ | $\begin{gathered} 648.239 \\ (228.008) \end{gathered}$ | $\begin{aligned} & 933.262 \\ & (57.756) \end{aligned}$ | $\begin{gathered} 0.016 \\ (0.011) \end{gathered}$ |
|  | 8 | $\begin{aligned} & -14.552 \\ & (12.600) \end{aligned}$ | $\begin{aligned} & 24.586 \\ & (2.889) \end{aligned}$ | $\begin{gathered} 0.237 \\ (0.060) \end{gathered}$ |  |  |  | $\left\lvert\, \begin{gathered} 712.417 \\ (184.513) \end{gathered}\right.$ | $\begin{aligned} & 998.636 \\ & (99.815) \end{aligned}$ | $\begin{gathered} 0.014 \\ (0.010) \end{gathered}$ |
| 4 | 1 | $\begin{aligned} & -6.617 \\ & (6.403) \end{aligned}$ | $\begin{aligned} & 24.377 \\ & (1.817) \end{aligned}$ | $\begin{gathered} 0.249 \\ (0.048) \end{gathered}$ | $\begin{gathered} -6.617 \\ (6.403) \end{gathered}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 30.994 \\ & (6.337) \end{aligned}$ | $\begin{gathered} 468.096 \\ (117.612) \end{gathered}$ | $\begin{aligned} & 621.913 \\ & (57.395) \end{aligned}$ | $\begin{gathered} 0.013 \\ (0.010) \end{gathered}$ |
|  | 2 | $\begin{aligned} & -5.550 \\ & (4.165) \end{aligned}$ | $\begin{aligned} & 25.808 \\ & (0.637) \end{aligned}$ | $\begin{gathered} 0.200 \\ (0.045) \end{gathered}$ | $\begin{gathered} -5.550 \\ (4.165) \end{gathered}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 31.358 \\ & (3.991) \end{aligned}$ | $\begin{gathered} 614.959 \\ (184.017) \end{gathered}$ | $\begin{gathered} 705.155 \\ (115.606) \end{gathered}$ | $\begin{gathered} 0.009 \\ (0.008) \end{gathered}$ |
|  | 3 | $\begin{gathered} -9.762 \\ (3.076) \end{gathered}$ | $\begin{aligned} & 24.323 \\ & (1.627) \end{aligned}$ | $\begin{gathered} 0.195 \\ (0.047) \end{gathered}$ | $\begin{gathered} -9.762 \\ (3.076) \end{gathered}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 34.085 \\ & (3.155) \end{aligned}$ | $\left[\begin{array}{c} 709.430 \\ (209.281) \end{array}\right.$ | $\begin{aligned} & 846.530 \\ & (67.385) \end{aligned}$ | $\begin{gathered} 0.010 \\ (0.007) \end{gathered}$ |
|  | 4 | $\begin{aligned} & -15.889 \\ & (8.868) \end{aligned}$ | $\begin{gathered} 23.436 \\ (1.455) \end{gathered}$ | $\begin{gathered} 0.188 \\ (0.031) \end{gathered}$ | $\begin{aligned} & -15.889 \\ & (8.868) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 39.326 \\ & (8.820) \end{aligned}$ | $\begin{gathered} 644.512 \\ (166.002) \end{gathered}$ | $\begin{gathered} 983.773 \\ (128.938) \end{gathered}$ | $\begin{gathered} 0.014 \\ (0.009) \end{gathered}$ |
|  | 5 | $\begin{aligned} & -5.082 \\ & (12.425) \end{aligned}$ | $\begin{aligned} & 26.843 \\ & (2.633) \end{aligned}$ | $\begin{gathered} 0.192 \\ (0.056) \end{gathered}$ | $\begin{gathered} -7.216 \\ (8.070) \end{gathered}$ | $\begin{gathered} 0.120 \\ (0.268) \end{gathered}$ | $\begin{aligned} & 34.059 \\ & (8.691) \end{aligned}$ | $\left[\begin{array}{c} 540.994 \\ (133.073) \end{array}\right.$ | $\begin{gathered} 672.345 \\ (146.698) \end{gathered}$ | $\begin{gathered} 0.011 \\ (0.009) \end{gathered}$ |
|  | 6 | $\begin{aligned} & -10.198 \\ & (2.253) \end{aligned}$ | $\begin{gathered} 25.470 \\ (1.090) \end{gathered}$ | $\begin{gathered} 0.240 \\ (0.058) \end{gathered}$ | $\begin{aligned} & -10.198 \\ & (2.253) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 35.668 \\ & (3.057) \end{aligned}$ | $\begin{gathered} 523.750 \\ (155.690) \end{gathered}$ | $\begin{aligned} & 725.755 \\ & (54.578) \end{aligned}$ | $\begin{gathered} 0.016 \\ (0.007) \end{gathered}$ |
|  | 7 | $\begin{aligned} & -14.368 \\ & (5.657) \end{aligned}$ | $\begin{aligned} & 27.473 \\ & (2.064) \end{aligned}$ | $\begin{gathered} 0.254 \\ (0.038) \end{gathered}$ | $\begin{aligned} & -14.368 \\ & (5.657) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 41.841 \\ & (6.518) \end{aligned}$ | $\begin{aligned} & 541.721 \\ & (194.276) \end{aligned}$ | $\begin{aligned} & 891.336 \\ & (39.108) \end{aligned}$ | $\begin{gathered} 0.018 \\ (0.009) \end{gathered}$ |
|  | 8 | $\begin{aligned} & -19.768 \\ & (3.624) \\ & \hline \end{aligned}$ | $\begin{gathered} 27.227 \\ (1.519) \\ \hline \end{gathered}$ | $\begin{gathered} 0.277 \\ (0.088) \\ \hline \end{gathered}$ | $\begin{array}{r} -19.768 \\ (3.624) \\ \hline \end{array}$ | $\begin{gathered} 0.000 \\ (0.000) \\ \hline \end{gathered}$ | $\begin{aligned} & 46.995 \\ & (3.492) \\ & \hline \end{aligned}$ | $\begin{gathered} 651.380 \\ (161.554) \end{gathered}$ | $\begin{aligned} & 1030.238 \\ & (46.791) \\ & \hline \end{aligned}$ | $\begin{array}{cc} 8 & 0.018 \\ \quad(0.00 .6) \\ \hline \end{array}$ |

Table 9. (Continued).

| Subj | nd | Cont | Max | Tmax | Min | Tmin | ROM | ContVel | MaxVel | TmaxVel |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5 | 1 | $\begin{array}{\|c\|} \hline-8.764 \\ (8.657) \end{array}$ | $\begin{aligned} & 24.642 \\ & (2.919) \end{aligned}$ | $\begin{gathered} 0.213 \\ (0.032) \end{gathered}$ | $\begin{gathered} \hline-8.764 \\ (8.657) \end{gathered}$ | $\begin{gathered} \hline 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 33.406 \\ & (7.182) \end{aligned}$ | $\begin{aligned} & 467.725 \\ & (112.174) \end{aligned}$ | $\begin{aligned} & 594.003 \\ & (67.605) \end{aligned}$ | $\begin{gathered} 0.013 \\ (0.009) \end{gathered}$ |
|  | 2 | $\begin{array}{\|c} -9.854 \\ (11.000) \end{array}$ | $\begin{aligned} & 25.915 \\ & (1.164) \end{aligned}$ | $\begin{gathered} 0.163 \\ (0.023) \end{gathered}$ | $-9.959$ | $0.120$ | $\begin{gathered} 35.874 \\ (10.560) \end{gathered}$ | $\begin{gathered} 625.702 \\ (120.650) \end{gathered}$ | $\begin{gathered} 820.027 \\ (154.390) \end{gathered}$ | $\begin{gathered} 0.011 \\ (0.010) \end{gathered}$ |
|  | 3 | $\begin{array}{\|l} -14.157 \\ (9.626) \end{array}$ | $\begin{aligned} & 24.518 \\ & (1.553) \end{aligned}$ | $\begin{gathered} 0.170 \\ (0.057) \end{gathered}$ | $\begin{aligned} & -14.157 \\ & (9.626) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 38.675 \\ & (9.499) \end{aligned}$ | $\begin{gathered} 950.615 \\ (198.185) \end{gathered}$ | $\begin{aligned} & 142.011 \\ & 103.702) \end{aligned}$ | $\begin{gathered} 0.009 \\ (0.009) \end{gathered}$ |
|  | 4 | $\begin{aligned} & -20.614 \\ & (4.902) \end{aligned}$ | $\begin{aligned} & 22.595 \\ & (1.346) \end{aligned}$ | $\begin{gathered} 0.150 \\ (0.048) \end{gathered}$ | $\begin{aligned} & -20.614 \\ & (4.902) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 43.209 \\ & (5.043) \end{aligned}$ | $\begin{gathered} 986.265 \\ (270.130) \end{gathered}$ | $\begin{aligned} & 1273.975 \\ & (108.076) \end{aligned}$ | $\begin{gathered} 0.012 \\ (0.006) \end{gathered}$ |
|  | 5 | $\begin{aligned} & -12.107 \\ & (11.560) \end{aligned}$ | $\begin{aligned} & 19.237 \\ & (1.157) \end{aligned}$ | $\begin{gathered} 0.154 \\ (0.055) \end{gathered}$ | $\begin{aligned} & -14.591 \\ & (7.108) \end{aligned}$ | $\begin{gathered} 0.118 \\ (0.265) \end{gathered}$ | $\begin{aligned} & 33.828 \\ & (7.045) \end{aligned}$ | $\left\lvert\, \begin{gathered} 611.887 \\ (105.337) \end{gathered}\right.$ | $\begin{aligned} & 718.862 \\ & (96.693) \end{aligned}$ | $\begin{gathered} 0.010 \\ (0.010) \end{gathered}$ |
|  | 6 | $\begin{aligned} & -10.612 \\ & (8.675) \end{aligned}$ | $\begin{aligned} & 20.54 \\ & (1.68 \end{aligned}$ | $\begin{gathered} 0.136 \\ (0.037) \end{gathered}$ | $\begin{aligned} & -10.612 \\ & (8.675) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 31.152 \\ & (9.423) \end{aligned}$ | $\begin{gathered} 683.166 \\ (105.055) \end{gathered}$ | $\begin{aligned} & 811.301 \\ & (41.509) \end{aligned}$ | $\begin{gathered} 0.010 \\ (0.010) \end{gathered}$ |
|  | 7 | $\begin{gathered} -8.992 \\ (4.481) \end{gathered}$ | $\begin{aligned} & 20.871 \\ & (1.717) \end{aligned}$ | $\begin{array}{r} 0.15 \\ (0.06 \end{array}$ | $\begin{aligned} & -8.992 \\ & (4.481) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 29.863 \\ & (5.134) \end{aligned}$ | $\begin{aligned} & 864.726 \\ & (60.405) \end{aligned}$ | $\begin{gathered} 909.814 \\ (54.916) \end{gathered}$ | $\begin{gathered} 0.007 \\ (0.005) \end{gathered}$ |
|  | 8 | $\begin{aligned} & -14.867 \\ & (3.325) \end{aligned}$ | $\begin{aligned} & 21.406 \\ & (1.024) \end{aligned}$ | $\begin{gathered} 0.188 \\ (0.048) \end{gathered}$ | $\begin{aligned} & -14.867 \\ & (3.325) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 36.273 \\ & (4.061) \end{aligned}$ | $\begin{aligned} & 840.312 \\ & (98.886) \end{aligned}$ | $\begin{aligned} & 969.409 \\ & (54.560) \end{aligned}$ | $\begin{gathered} 0.011 \\ (0.004) \end{gathered}$ |
| 6 | 1 | $\begin{gathered} -2.690 \\ (8.707) \end{gathered}$ | $\begin{aligned} & 36.491 \\ & (2.181) \end{aligned}$ | $\begin{gathered} 0.248 \\ (0.017) \end{gathered}$ | $\begin{aligned} & -2.690 \\ & (8.707) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 39.181 \\ & (7.787) \end{aligned}$ | $\begin{aligned} & 507.984 \\ & (77.144) \end{aligned}$ | $\begin{gathered} 624.459 \\ (87.719) \end{gathered}$ | $\begin{gathered} 0.012 \\ (0.009) \end{gathered}$ |
|  | 2 | $\begin{gathered} -0.449 \\ (7.538) \end{gathered}$ | $\begin{aligned} & 39.818 \\ & (1.576) \end{aligned}$ | $\begin{gathered} 0.238 \\ (0.022) \end{gathered}$ | $\begin{aligned} & -0.449 \\ & (7.538) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 40.266 \\ & (6.479) \end{aligned}$ | $\begin{aligned} & 622.882 \\ & (70.214) \end{aligned}$ | $\begin{aligned} & 732.861 \\ & (73.718) \end{aligned}$ | $\begin{gathered} 0.009 \\ (0.008) \end{gathered}$ |
|  | 3 | $\begin{gathered} 4.992 \\ (9.622) \end{gathered}$ | $\begin{aligned} & 41.909 \\ & (1.606) \end{aligned}$ | $\begin{gathered} 0.233 \\ (0.059) \end{gathered}$ | $\begin{gathered} 3.482 \\ (7.816) \end{gathered}$ | $\begin{gathered} 0.240 \\ (0.329) \end{gathered}$ | $\begin{aligned} & 38.428 \\ & (9.122) \end{aligned}$ | $\begin{gathered} 672.474 \\ (113.589) \end{gathered}$ | $\begin{aligned} & 768.222 \\ & (94.434) \end{aligned}$ | $\begin{gathered} 0.008 \\ (0.008) \end{gathered}$ |
|  | 4 | $\begin{gathered} 2.282 \\ (8.421) \end{gathered}$ | $\begin{aligned} & 41.741 \\ & (3.228) \end{aligned}$ | $\begin{gathered} 0.221 \\ (0.043) \end{gathered}$ | $\begin{gathered} 2.237 \\ (8.345) \end{gathered}$ | $\begin{gathered} 0.120 \\ (0.268) \end{gathered}$ | $\begin{aligned} & 39.504 \\ & (8.540) \end{aligned}$ | $\begin{aligned} & 719.162 \\ & (97.686) \end{aligned}$ | $\begin{aligned} & 855.159 \\ & (97.440) \end{aligned}$ | $\begin{gathered} 0.009 \\ (0.006) \end{gathered}$ |
|  | 5 | $\begin{gathered} -9.608 \\ (2.637) \end{gathered}$ | $\begin{aligned} & 32.390 \\ & (1.376) \end{aligned}$ | $\begin{gathered} 0.249 \\ (0.011) \end{gathered}$ | $\begin{gathered} -9.608 \\ (2.637) \end{gathered}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 41.998 \\ & (3.660) \end{aligned}$ | $\begin{gathered} 476.753 \\ (103.688) \end{gathered}$ | $\begin{gathered} 649.904 \\ (29.288) \end{gathered}$ | $\begin{gathered} 0.018 \\ (0.006) \end{gathered}$ |
|  | 6 | $\begin{gathered} -9.841 \\ (4.522) \end{gathered}$ | $\begin{aligned} & 36.388 \\ & (3.427) \end{aligned}$ | $\begin{gathered} 0.258 \\ (0.048) \end{gathered}$ | $\begin{gathered} -9.841 \\ (4.522) \end{gathered}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 46.229 \\ & (2.797) \end{aligned}$ | $\begin{gathered} 633.126 \\ (125.229) \end{gathered}$ | $\begin{gathered} 826.227 \\ (72.644) \end{gathered}$ | $\begin{gathered} 0.014 \\ (0.005) \end{gathered}$ |
|  | 7 | $\begin{aligned} & -8.038 \\ & (5.434) \end{aligned}$ | $\begin{aligned} & 39.765 \\ & (2.315) \end{aligned}$ | $\begin{gathered} 0.252 \\ (0.038) \end{gathered}$ | $\begin{aligned} & -8.038 \\ & (5.434) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 47.803 \\ & (6.950) \end{aligned}$ | $\begin{gathered} 691.900 \\ (199.362) \end{gathered}$ | $\begin{aligned} & 924.892 \\ & (76.478) \end{aligned}$ | $\begin{gathered} 0.014 \\ (0.009) \end{gathered}$ |
|  | 8 | $\begin{aligned} & -6.659 \\ & (3.584) \end{aligned}$ | $\begin{aligned} & 40.211 \\ & (1.456) \end{aligned}$ | $\begin{gathered} 0.269 \\ (0.023) \end{gathered}$ | $\begin{aligned} & -6.659 \\ & (3.584) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 46.870 \\ & (4.196) \end{aligned}$ | $\begin{gathered} 756.699 \\ (144.880) \end{gathered}$ | $\begin{aligned} & 932.015 \\ & (69.257) \end{aligned}$ | $\begin{gathered} 0.013 \\ (0.005) \end{gathered}$ |

Table 9. (Continued).

| Subj | Cond | Cont | Max | Tmax | Min | Tmin | ROM | ContVel | MaxVel | TmaxVel |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7 | 1 | $\begin{array}{\|l\|} \hline-31.399 \\ (8.371) \end{array}$ | $\begin{aligned} & \hline 21.073 \\ & (4.196) \end{aligned}$ | $\begin{gathered} \hline 0.203 \\ (0.087) \end{gathered}$ | $\begin{aligned} & -31.399 \\ & (8.371) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{gathered} 52.471 \\ (11.843) \end{gathered}$ | $\begin{aligned} & 468.261 \\ & (263.881) \end{aligned}$ | $\begin{aligned} & 934.322 \\ & (66.596) \end{aligned}$ | $\begin{gathered} 0.023 \\ (0.012) \end{gathered}$ |
|  | 2 | $\begin{aligned} & -31.738 \\ & (1.876) \end{aligned}$ | $\begin{aligned} & 26.267 \\ & (2.876) \end{aligned}$ | $\begin{gathered} 0.265 \\ (0.060) \end{gathered}$ | $\begin{aligned} & -31.738 \\ & (1.876) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 58.005 \\ & (4.116) \end{aligned}$ | $\begin{aligned} & 647.831 \\ & (128.428) \end{aligned}$ | $\begin{aligned} & 991.332 \\ & (54.582) \end{aligned}$ | $\begin{gathered} 0.022 \\ (0.003) \end{gathered}$ |
|  | 3 | $\begin{aligned} & -29.702 \\ & (8.650) \end{aligned}$ | $\begin{aligned} & 25.003 \\ & (1.738) \end{aligned}$ | $\begin{gathered} 0.311 \\ (0.061) \end{gathered}$ | $\begin{aligned} & -29.702 \\ & (8.650) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 54.706 \\ & (8.796) \end{aligned}$ | $\begin{gathered} 684.122 \\ (244.455) \end{gathered}$ | $\begin{aligned} & 1070.717 \\ & (76.073) \end{aligned}$ | $\begin{gathered} 0.018 \\ (0.010) \end{gathered}$ |
|  | 4 | $\begin{aligned} & -22.901 \\ & (8.611) \end{aligned}$ | $\begin{aligned} & 23.905 \\ & (2.334) \end{aligned}$ | $\begin{gathered} 0.234 \\ (0.034) \end{gathered}$ | $\begin{aligned} & -22.901 \\ & (8.611) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 46.806 \\ & (7.918) \end{aligned}$ | $\begin{aligned} & 1019.425 \\ & (130.568) \end{aligned}$ | $\begin{aligned} & 1202.247 \\ & (94.061) \end{aligned}$ | $\begin{gathered} 0.010 \\ (0.007) \end{gathered}$ |
|  | 5 | $\begin{aligned} & -35.250 \\ & (4.211) \end{aligned}$ | $\begin{aligned} & 23.770 \\ & (1.118) \end{aligned}$ | $\begin{gathered} 0.310 \\ (0.093) \end{gathered}$ | $\begin{aligned} & -35.250 \\ & (4.211) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 59.021 \\ & (3.608) \end{aligned}$ | $\left\lvert\, \begin{gathered} 342.241 \\ (127.584) \end{gathered}\right.$ | $\begin{aligned} & 771.031 \\ & (70.658) \end{aligned}$ | $\begin{gathered} 0.034 \\ (0.008) \end{gathered}$ |
|  | 6 | $\begin{aligned} & -31.478 \\ & (3.074) \end{aligned}$ | $\begin{aligned} & 24.682 \\ & (1.721) \end{aligned}$ | $\begin{gathered} 0.248 \\ (0.033) \end{gathered}$ | $\begin{aligned} & -31.478 \\ & (3.074) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 56.160 \\ & (2.742) \end{aligned}$ | $\begin{gathered} 463.529 \\ (158.537) \end{gathered}$ | $\begin{aligned} & 926.376 \\ & (56.213) \end{aligned}$ | $\begin{gathered} 0.028 \\ (0.008) \end{gathered}$ |
|  | 7 | $\begin{aligned} & -30.363 \\ & (6.202) \end{aligned}$ | $\begin{array}{r} 20.866 \\ (3.734) \end{array}$ | $\begin{gathered} 0.179 \\ (0.099) \end{gathered}$ | $\begin{aligned} & -30.363 \\ & (6.202) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 51.228 \\ & (6.461) \end{aligned}$ | $\begin{gathered} 537.319 \\ (114.882) \end{gathered}$ | $\begin{aligned} & 987.743 \\ & (54.729) \end{aligned}$ | $\begin{gathered} 0.025 \\ (0.003) \end{gathered}$ |
|  | 8. | $\begin{aligned} & -27.817 \\ & (6.479) \end{aligned}$ | $\begin{aligned} & 19.936 \\ & (4.321) \end{aligned}$ | $\begin{gathered} 0.233 \\ (0.113) \end{gathered}$ | $\begin{aligned} & -27.817 \\ & (6.479) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 47.753 \\ & (5.773) \end{aligned}$ | $\begin{aligned} & 705.174 \\ & (263.055) \end{aligned}$ | $\begin{aligned} & 1064.637 \\ & (69.750) \end{aligned}$ | $\begin{gathered} 0.019 \\ (0.008) \end{gathered}$ |
| 8 | 1 | $\begin{array}{\|l} -21.251 \\ (6.323) \end{array}$ | $\begin{aligned} & 23.363 \\ & (1.266) \end{aligned}$ | $\begin{gathered} 0.356 \\ (0.118) \end{gathered}$ | $\begin{aligned} & -21.251 \\ & (6.323) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 44.613 \\ & (6.824) \end{aligned}$ | $\begin{aligned} & 543.391 \\ & (191.923) \end{aligned}$ | $\begin{gathered} 789.380 \\ (77.620) \end{gathered}$ | $\begin{gathered} 0.017 \\ (0.010) \end{gathered}$ |
|  | 2 | $\begin{aligned} & -26.169 \\ & (2.670) \end{aligned}$ | $\begin{aligned} & 23.298 \\ & (2.278) \end{aligned}$ | $\begin{gathered} 0.331 \\ (0.130) \end{gathered}$ | $\begin{aligned} & -26.169 \\ & (2.670) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 49.467 \\ & (4.821) \end{aligned}$ | $\begin{gathered} 605.652 \\ (195.936) \end{gathered}$ | $\begin{aligned} & 1036.727 \\ & (46.629) \end{aligned}$ | $\begin{gathered} 0.020 \\ (0.007) \end{gathered}$ |
|  | 3 | $\begin{aligned} & -24.196 \\ & (3.739) \end{aligned}$ | $\begin{aligned} & 22.626 \\ & (1.440) \end{aligned}$ | $\begin{gathered} 0.297 \\ (0.123) \end{gathered}$ | $\begin{aligned} & -24.196 \\ & (3.739) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 46.822 \\ & (4.573) \end{aligned}$ | $\begin{gathered} 797.179 \\ (185.562) \end{gathered}$ | $\begin{array}{r} 1141.000 \\ (119.335) \end{array}$ | $\begin{gathered} 0.015 \\ (0.006) \end{gathered}$ |
|  | 4 | $\begin{aligned} & -27.564 \\ & (3.896) \end{aligned}$ | $\begin{aligned} & 22.360 \\ & (0.953) \end{aligned}$ | $\begin{gathered} 0.315 \\ (0.158) \end{gathered}$ | $\begin{aligned} & -27.564 \\ & (3.896) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 49.923 \\ & (3.300) \end{aligned}$ | $\begin{gathered} 657.460 \\ (150.514) \end{gathered}$ | $\begin{aligned} & 1193.254 \\ & (16.362) \end{aligned}$ | $\begin{gathered} 0.019 \\ (0.005) \end{gathered}$ |
|  | 5 | $\begin{aligned} & -31.045 \\ & (4.673) \end{aligned}$ | $\begin{aligned} & 18.281 \\ & (1.226) \end{aligned}$ | $\begin{gathered} 0.394 \\ (0.104) \end{gathered}$ | $\begin{aligned} & -31.045 \\ & (4.673) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 49.326 \\ & (4.757) \end{aligned}$ | $\begin{aligned} & 503.249 \\ & (87.474) \end{aligned}$ | $\begin{aligned} & 892.443 \\ & (59.051) \end{aligned}$ | $\begin{gathered} 0.024 \\ (0.004) \end{gathered}$ |
|  | 6 | $\begin{aligned} & -29.365 \\ & (2.742) \end{aligned}$ | $\begin{gathered} 15.575 \\ (1.992) \end{gathered}$ | $\begin{gathered} 0.398 \\ (0.109) \end{gathered}$ | $\begin{aligned} & -29.365 \\ & (2.742) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 44.940 \\ & (2.670) \end{aligned}$ | $\begin{aligned} & 627.796 \\ & (74.317) \end{aligned}$ | $\begin{aligned} & 974.729 \\ & (91.483) \end{aligned}$ | $\begin{gathered} 0.019 \\ (0.002) \end{gathered}$ |
|  | 7 | $\begin{aligned} & -26.840 \\ & (4.929) \end{aligned}$ | $\begin{gathered} 15.453 \\ (0.993) \end{gathered}$ | $\begin{gathered} 0.362 \\ (0.192) \end{gathered}$ | $\begin{aligned} & -26.840 \\ & (4.929) \end{aligned}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 42.294 \\ & (4.982) \end{aligned}$ | $\begin{array}{\|c} 705.974 \\ (150.759) \end{array}$ | $\begin{aligned} & 985.538 \\ & (57.389) \end{aligned}$ | $\begin{gathered} 0.018 \\ (0.006) \end{gathered}$ |
|  | 8 | $\begin{aligned} & -29.756 \\ & (4.102) \\ & \hline \end{aligned}$ | $\begin{array}{r} 15.903 \\ (2.356) \\ \hline \end{array}$ | $\begin{gathered} 0.214 \\ (0.141) \\ \hline \end{gathered}$ | $\begin{array}{r} -29.756 \\ (4.102) \\ \hline \end{array}$ | $\begin{gathered} 0.000 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 45.659 \\ & (4.576) \end{aligned}$ | $\begin{gathered} 602.534 \\ (168.648) \end{gathered}$ | $\begin{aligned} & 1098.591 \\ & (40.423) \\ & \hline \end{aligned}$ | $\begin{gathered} 0.023 \\ (0.005) \\ \hline \end{gathered}$ |

Table 9. (Continued).

| Subj | Cond | Cont | Max | Tmax | Min | Tmin | ROM | ContVel | MaxVel | TmaxVel |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 9 | 1 | 0.516 | 17.909 | 0.166 | -4.786 | 0.301 | 22.694 | 22 | 296 | 1 |
|  |  | (9.168) | (1.109) | (0.029) | (3.344) | (0.277) | (4.125) | (97.885) | (161.249) | (0.027) |
|  | 2 | -19.016 | 16.580 | 0.169 | -19.016 | 0.000 | 35.596 | 626.380 | 833.704 | 0.014 |
|  |  | (3.748) | (1.486) | (0.005) | (3.748) | (0.000) | (3.311) | (186.997) | (68.770) | (0.007) |
|  | 3 | -17.259 | 17.854 | 0.159 | -17.259 | 0.000 | 35.113 | 802.352 | 963.577 | 0.010 |
|  |  | (4.100) | (2.231) | (0.015) | (4.100) | (0.000) | (5.415) | (139.033) | (51.272) | (0.007) |
|  | 4 | -17.356 | 17.612 | . 159 | -17.356 | 0.000 | 34.968 | 841.47 | 1076.706 | 0.010 |
|  |  | (11.169) | (3.873) | (0.022) | 1.169) | (0.000) | (9.049) | (283.088) | (85.170) | (0.010) |
|  | 5 | -15.705 | 17.076 | 0.185 | -16.577 | 0.112 | 33.653 | 470.571 | 624.141 | 0.013 |
|  |  | (11.061) | (1.444) | (0.025) | (9.139) | (0.250) | (9.493) | (97.161) | (126.558) | (0.009) |
|  | 6 | -21.879 | 17.183 | 0.163 | -21.879 | 0.000 | 39.063 | 5.285 | 816.241 | 0.018 |
|  |  | (4.436) | (0.964) | (0.014) | (4.436) | (0.000) | (4.324) | (91.430) | (83.613) | (0.006) |
|  | 7 | -18.033 | 19.112 | 0.183 | -18.033 | 0.000 | 37.144 | 723.740 | 937.654 | 0.012 |
|  |  | (8.870) | (0.956) | (0.021) | (8.870) | (0.000) | (9.351) | (198.514) | (47.743) | (0.010) |
|  | 8 | -13.163 | 19.126 | 0.160 | -16.426 | 0.233 | 35.552 | 744.214 | 938.301 | 0.010 |
|  |  | (14.528) | (1.357) | (0.013) | (9.361) | (0.320) | (9.774) | (130. | (132.658) | (0.010) |
| 10 | 1 |  |  |  |  |  | 36.328 | 2. | 632.592 | 0.019 |
|  |  | (2.111) | (1.127) | (0.010) | (2.111) | (0.000) | (2.262) | (64.584) | (16.337) | $(0.005)$ |
|  | 2 | -19.003 | 24.740 | 0.118 | -19.003 | 0.000 | 43.743 | 512.452 | 740.035 | 0.023 |
|  |  | (4.215) | (1.480) | (0.020) | (4.215) | (0.000) | (3.680) | (90.453) | (44.128) | (0.008) |
|  | 3 | -18.312 | 24.727 | 0.149 | -18.312 | 0.000 | 43.039 | 623.312 | 831.688 | 0.020 |
|  |  | (2.544) | (1.373) | (0.036) | (2.544) | (0.000) | (2.478) | (90.634) | (107.731) | (0.004) |
|  | 4 | -17.412 | 26.523 | 0.164 | -17.412 | 0.000 | 43.935 | 625.136 | 807.07 | 0.019 |
|  |  | (3.888) | (0.767) | (0.018) | (3.888) | (0.000) | (3.908) | (79.320) | (28.140) | (0.005) |
|  | 5 | -24.654 | 16.176 | 0.1 .17 | -24.654 | 0.000 | 40.830 | 441.937 | 642.009 | 0.027 |
|  |  | (2.447) | (1.570) | (0.007) | (2.447) | (0.000) | (3.706) | (80.232) | (32.252) | (0.007) |
|  | 6 | -24.095 | 17.737 | 0.109 | -24.095 | 0.000 | 41.832 | 470.209 | 699.486 | 0.027 |
|  |  | (3.925) | (1.397) | (0.028) | (3.925) | (0.000) | (4.178) | (37.760) | (44.982) | (0.004) |
|  | 7 | -25.404 | 19.962 | 0.088 | -25.404 | 0.000 | 45.366 | 539.756 | 802.093 | 0.026 |
|  |  | (3.238) | (0.707) | (0.007) | (3.238) | (0.000) | (3.562) | (54.402) | (36.788) | (0.003) |
|  | 8 | -23.461 | 19.219 | 0.085 | -23.461 | 0.000 | 42.681 | 554.390 | 797.501 | 0.025 |
|  |  | (3.560) | (1.934) | (0.007) | (3.560) | (0.000) | (2.777) | (116.390) | (54.068) | (0.005) |

Note: Angle and ROM units are in degrees and time unit is in s.
Velocity unit is in deg/s.
Standard deviation values are in parenthesis.
The definitions of variables are in Appendix A.

Table 10. Subject means and standard deviations of ankle joint variables (Group 2).


Table 10. (Continued).

| Subj Cond | Cont | Max | Tmax | Min | Tmin | ROM | ContVel | MaxVel | TmaxVel |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | 1 | -4.161 | 20.221 | 0.252 | -4.190 | 0.001 | 24.411 | 102.500 | 269.997 | 0.029 |
|  | $(3.732)$ | $(1.686)$ | $(0.044)$ | $(3.720)$ | $(0.002)$ | $(4.730)$ | $(136.842)$ | $(60.128)$ | $(0.013)$ |  |
|  | 2 | -1.249 | 21.505 | 0.231 | -2.206 | 0.126 | 23.711 | 140.599 | 312.757 | 0.034 |
|  | $(7.764)$ | $(2.600)$ | $(0.071)$ | $(7.226)$ | $(0.265)$ | $(6.417)$ | $(198.449)$ | $(158.310)$ | $(0.021)$ |  |
| 3 | -6.254 | 20.181 | 0.247 | -6.254 | 0.000 | 26.435 | 389.515 | 497.999 | 0.029 |  |
|  | $(8.340)$ | $(3.292)$ | $(0.059)$ | $(8.340)$ | $(0.000)$ | $(9.500)$ | $(255.688)$ | $(246.119)$ | $(0.035)$ |  |
| 4 | 4 | -15.381 | 20.169 | 0.222 | -15.381 | 0.000 | 35.550 | 601.254 | 796.131 | 0.011 |
|  | $(5.845)$ | $(2.179)$ | $(0.108)$ | $(5.845)$ | $(0.000)$ | $(7.023)$ | $(160.830)$ | $(156.762)$ | $(0.006)$ |  |
| 5 | -11.408 | 18.539 | 0.204 | -11.477 | 0.002 | 30.017 | 199.294 | 457.365 | 0.028 |  |
|  | $(9.048)$ | $(4.046)$ | $(0.060)$ | $(8.989)$ | $(0.004)$ | $(7.201)$ | $(260.137)$ | $(191.243)$ | $(0.011)$ |  |
| 6 | -10.260 | 23.089 | 0.276 | -10.260 | 0.000 | 33.348 | 577.615 | 705.028 | 0.011 |  |
|  | $(5.512)$ | $(1.441)$ | $(0.058)$ | $(5.512)$ | $(0.000)$ | $(6.844)$ | $(64.180)$ | $(77.912)$ | $(0.008)$ |  |
| 7 | -10.889 | 23.946 | 0.145 | -10.889 | 0.000 | 34.835 | 648.013 | 782.242 | 0.011 |  |
|  | $(5.376)$ | $(2.936)$ | $(0.020)$ | $(5.376)$ | $(0.000)$ | $(4.016)$ | $(102.629)$ | $(86.407)$ | $(0.004)$ |  |
| 8 | -6.964 | 23.808 | 0.157 | -6.964 | 0.000 | 30.772 | 737.067 | 850.866 | 0.009 |  |
|  | $(7.855)$ | $(2.220)$ | $(0.063)$ | $(7.855)$ | $(0.000)$ | $(6.820)$ | $(187.670)$ | $(175.943)$ | $(0.006)$ |  |

Note: Angle and ROM units are in degrees and time unit is in s.
Velocity unit is in deg/s.
Standard deviation values are in parenthesis.
The definitions of variables are in Appendix A.

Table 11. Subject means and standard deviations of knee joint variables (Group 1).

| Subj | Cond | Cont | Max | Tmax | Min | Tmin | ROM | ContVel | MaxVel | Tmax |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | 18.391 | 81.511 | 0.192 | 12.267 | 0.600 | 69.245 | 248.794 | 651.977 | , 67 |
|  |  | (3.493) | (4.67 | (0.016) | (5.456) | (0.000) | (3.050) | (93.326) | (59.959) | (0.013) |
|  | 2 | 28.624 | 92.493 | 0.192 | 21.120 | 0.480 | 71.373 | 425.865 | 685.800 | 0.043 |
|  |  | (3.366) | (4.922) | (0.008) | (7.493) | (0.268) | (3.727) | (97.807) | (48.004) | (0.009) |
|  | 3 | 19.782 | 96.393 | 0.207 | 18.787 | 0.240 | 77.606 | 262.198 | 881.855 | 0.060 |
|  |  | (4.284) | (4.303) | (0.009) | (4.956) | (0.329) | (4.854) | (107.966) | (46.717) | (0.015) |
|  | 4 | 30.480 | 104.573 | 0.209 | 28.925 | 0.360 | 75.648 | 485.215 | 941.848 | 0.039 |
|  |  | (6.549) | (4.057) | (0.020) | (5.897) | (0.329) | (7.122) | (174.125 | (57.883) | (0.013) |
|  | 5 | 20.117 | 71.286 | 0.143 | 12.391 | 0.360 | 58.895 | 286.684 | 634.761 | 0.057 |
|  |  | (4.224) | (1.535) | (0.005) | (5.327) | (0.329) | (6.494) | (90.852) | (78.551) | (0.012) |
|  | 6 | 19.321 | 79.940 | 0.158 | 8.595 | 0.600 | 71.345 | 336.240 | 785.069 | 0.048 |
|  |  | (2.689) | (3.551) | (0.018) | (3.377) | (0.000) | (2.137) | (100.864) | (82.600) | $(0.007)$ |
|  | 7 | 29.703 | 95.615 | 0.183 | 18.218 | 0.600 | 77.397 | 508.608 | 783.159 | 0.034 |
|  |  | (5.328) | (3.358) | (0.014) | (4.267) | (0.000) | (3.362) | (110.731) | (40.443) | (0.009) |
|  | 8 | 25.239 | 99.369 | 0.176 | 19.849 | 0.360 | 79.520 | 399.844 | 866.009 | 0.048 |
|  |  | (3.524) | (4.457) | (0.020) | (4.708) | (0.329) | (3.481) | (78.632) | (107.37 | (0.013) |
| 2 | 1 |  | 69.792 | 0.197 | 20 | 0.000 | 49.341 | 25 | 4 |  |
|  |  | (3.654) | (4.783) | (0.030) | (3.654) | (0.000) | (4.627) | (61.089) | (79.172) | (0.008) |
|  | 2 | 26.462 | 76.357 | 0.178 | 26.462 | 0.000 | 49.894 | 380.092 | 672.076 | 0.042 |
|  |  | (2.832) | (2.922) | (0.018) | (2.832) | (0.000) | (4.749) | (56.245) | (29.034) | (0.010) |
|  | 3 | 23.385 | 78.763 | 0.190 | 23.385 | 0.000 | 55.378 | 322.299 | 785.973 | 0.047 |
|  |  | (2.927) | (2.641) | (0.031) | (2.927) | (0.000) | (4.137) | (78.696) | (78.379) | (0.007) |
|  | 4 | 24.934 | 82.651 | 0.167 | 24.934 | 0.000 | 57.716 | 398.859 | 863.268 | 0.041 |
|  |  | (2.250) | (2.298) | (0.006) | (2.250) | (0.000) | (1.536) | (59.502) | (52.576) | $(0.005)$ |
|  | 5 | 19.077 | 64.674 | 0.163 | 19.077 | 0.000 | 45.597 | 258.641 | 569.730 | 0.057 |
|  |  | (2.674) | (1.812) | (0.022) | (2.674) | (0.000) | (2.837) | (53.406) | (38.402) | $(0.007)$ |
|  | 6 | 20.218 | 69.661 | 0.162 | 20.218 | 0.000 | 49.443 | 326.695 | 685.317 | 0.047 |
|  |  | (1.880) | (1.850) | (0.008) | (1.880) | (0.000) | (1.735) | (30.449) | (83.764) | (0.006) |
|  | 7 | 23.143 | 74.753 | 0.174 | 23.143 | 0.000 | 51.610 | 342.068 | 744.756 | 0.046 |
|  |  | (3.007) | (1.700) | (0.014) | (3.007) | (0.000) | (1.848) | (41.510) | (55.259) | (0.004) |
|  | 8 | 26.940 | 76.241 | 0.181 | 26.560 | 0.120 | 49.681 | 342.159 | 656.059 | 0.045 |
|  |  | (5.993) | (5.183) | (0.065) | (5.539) | (0.268) | (9.692) | (77.409) | (146.972) | (0.012) |

Table 11. (Continued).


Table 11. (Continued).

| Subj | Cond | Cont | Max | Tmax | Min | Tmin | ROM | ContVel | MaxVel | TmaxVel |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5 | 1 | 35.055 | 88.269 | 0.203 | 35.029 | 0.120 | 53.240 | 407.737 | 603.362 | 0.035 |
|  |  | (8.328) | (11.693) | ( 0.040 ) | (8.335) | (0.268) | (7.846) | (83.855) | (29.981) | (0.014) |
|  | 2 | 40.486 | 95.187 | 0.201 | 37.525 | 0.120 | 57.662 | 450.771 | 691.166 | 0.037 |
|  |  | (6.186) | (6.806) | (0.025) | (6.835) | (0.268) | (5.339) | (121 | 186) | (0.016) |
|  | 3 | 41.823 | 101.863 | 0.197 | 37.397 | 0.360 | 64.466 | 507.022 | 675.525 | 0.042 |
|  |  | (5.620) | (2.817) | (0.011) | (6.473) | (0.329) | (6.354) | (105.272) | (52.581) | (0.011) |
|  | 4 | 38.503 | 93.196 | 0.165 | 27.069 | 0.500 | 66.128 | 442.668 | 724.920 | 0.041 |
|  |  | (4.415) | (5.947) | (0.028) | 11.464) | (0.245) | (9.907) | (68.832) | (135.914) | (0.004) |
|  | 5 | 34.938 | 78.754 | 0.162 | 22.894 | 0.479 | 55.859 | 418.340 | 528.148 | 0.038 |
|  |  | (7.435) | (3.230) | (0.029) | . 05 | 0.268) | 11.581) | (66.412) | (43.910) | (0.016) |
|  | 6 | 36.479 | 88.167 | 0.175 | 26.208 | 0.360 | 61.959 | 465.651 | 637.470 | 0.034 |
|  |  | (4.727) | (6.005) | (0.029) | (7.517) | (0.329) | (9.453) | (104.009) | (45.763) | (0.014) |
|  | 7 | 38.022 | 93.515 | 0.169 | 17.912 | 0.600 | 75.603 | 495.444 | 726.717 | 0.030 |
|  |  | (3.038) | (6.480) | (0.016) | (7.265) | (0.000) | (2.858) | (62.184) | (55.017) | (0.006) |
|  | 8 | 39.828 | 96.891 | 0.173 | 16.949 | 0.600 | 79.943 | 404.661 | 700.100 | 0.037 |
|  |  | (2.838) | (5.172) | (0.013) | (2.656) | (0.000) | (3.506) | (49.876) | (24.970) | (0.005) |
| 6 | 1 | 37.275 | 97.553 | 0.237 | 30.310 | 0.360 | 67.243 | 331.363 | 676.304 | 0.0 |
|  |  | (7.018) | (2.710) | (0.012) | (8.626) | (0.329) | (8.396) | (78.866) | (42.877) | (0.012) |
|  | 2 | 40.640 | 104.436 | 60.228 | 39:418 | 0.240 | 65.018 | 413.049 | 720.687 | 0.034 |
|  |  | (4.489) | (3.108) | (0.012) | (3.051) | (0.329) | (2.113) | (120.393) | (37.300) | (0.010) |
|  | 3 | 43.235 | 108.932 | 20.232 | 37.360 | 0.240 | 71.571 | 510.144 | 834.586 | 0.028 |
|  |  | (6.279) | (5.037) | (0.037) | (7.284) | (0.329) | (5.413) | (188.201) | (30.471) | (0.013) |
|  | 4 | 41.665 | 111.658 | 80.231 | 38.357 | 0.360 | 73.302 | 409.812 | 880.947 | 0.032 |
|  |  | (5.481) | (5.376) | (0.022) | (3.461) | (0.329) | (4.905) | (156.394) | (104.468) | (0.010) |
|  | 5 | 32.396 | 92.079 | 0.225 | 27.608 | 0.480 | 64.471 | 278.578 | 650.994 | 0.043 |
|  |  | (2.679) | (3.492) | (0.013) | (6.104) | (0.268) | (2.847) | (53.400) | (51.106) | (0.008) |
|  | 6 | 37.325 | 101.738 | 8 0.245 | 37.325 | 0.000 | 64.413 | 386.597 | 627.662 | 0.040 |
|  |  | (2.534) | (5.059) | (0.022) | (2.534) | (0.000) | (5.815) | (53.457) | (40.821) | (0.008) |
|  | 7 | 39.527 | 109.475 | 50.262 | 39.527 | 0.000 | 69.948 | 406.803 | 680.469 | 0.042 |
|  |  | (4.133) | (2.386) | ) (0.021) | (4.133) | (0.000) | (5.893) | (53.985) | (35.179) | (0.008) |
|  | 8 | 38.620 | 113.564 | 40.248 | 38.620 | 0.000 | 74.945 | 432.375 | 800.514 | 0.040 |
|  |  | (2.807) | (3:029) | (0.016) | (2.807) | (0.000) | (4.632) | (30.254) | (48.260) | (0.005) |

Table 11. (Continued).

| Subj | Cond | Cont | Max Tmax | Min | Tmin | ROM | ContVel | MaxVel | TmaxVel |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7 | 1 | 27.319 | 81.0880 .200 | 20.119 | 0.360 | 60.970 | 273.268 | 481.812 | 0.067 |
|  |  | (4.537) | (11.627) (0.060) | (7.154) | (0.329) | (5.922) | (88.498) | (52.801) | (0.024) |
|  | 2 | 32.908 | 98.8510 .246 | 32.908 | 0.000 | 65.943 | 451.349 | 555.490 | 0.020 |
|  |  | (5.345) | (9.467) (0.032) | (5.345) | (0.000) | (6.590) | (46.641) | (63.781) | (0.004) |
|  | 3 | 35.503 | 107.2700 .262 | 35.503 | 0.000 | 71.767 | 450.167 | 655.089 | 0.039 |
|  |  | (8.503) | (6.129) (0.028) | (8.503) | (0.000) | (5.970) | (140.280) | (41.661) | (0.024) |
|  | 4 | 36.417 | 111.2140 .261 | 36.417 | 0.000 | 74.797 | 582.229 | 730.659 | 0.029 |
|  |  | (5.232) | (3.443) (0.011) | (5.232) | (0.000) | (6.981) | (93.013) | (99.937) | (0.028) |
|  | 5 | 23.087 | 88.1590 .259 | 21.729 | 0.120 | 66.430 | 276.256 | 468.031 | 0.054 |
|  |  | (6.087) | (7.027) (0.055) | (7.146) | (0.268) | (7.931) | (56.640) | (27.444) | (0.026) |
|  | 6 | 24.411 | 92.5550 .223 | 23.905 | 0.240 | 68.649 | 359.756 | 588.084 | 0.052 |
|  |  | (3.221) | (5.037) (0.022) | (2.841) | (0.329) | (5.523) | (48.146) | (22.486) | (0.019) |
|  | 7 | 30.094 | 113.5090 .298 | 30.094 | 0.000 | 83.415 | 446.464 | 638.920 | 0.055 |
|  |  | (4.685) | (8.761) (0.023) | (4.685) | (0.000) | (5.033) | (38.729) | (40.446) | (0.025) |
|  | 8 | 33.034 | 117.5450 .283 | 33.034 | 0.000 | 84.511 | 505.441 | 723.686 | 0.041 |
|  |  | (3.481) | (5.958) (0.024) | (3.481) | (0.000) | (7.994) | (82.339) | (115.025) | (0.014) |
| 8 | 1 | 21.374 | $85.627 \quad 0.384$ | 21.374 | 0.000 | 64.253 | 322.903 | 641.877 | 0.048 |
|  |  | (3.397) | (7.945) (0.128) | (3.397) | (0.000) | (7.854) | (29.765) | (32.844) | (0.008) |
|  | 2 | 25.244 | 103.1060 .336 | 25.244 | 0.000 | 77.862 | 360.460 | 689.507 | 0.056 |
|  |  | (2.543) | (9.938) (0.069) | (2.543) | (0.000) | (11.985) | (50.828) | (24.669) | (0.009) |
|  | 3 | 25.797 | 101.3560 .282 | 25.797 | 0.000 | 75.559 | 398.587 | 838.450 | 0.049 |
|  |  | (1.201) | (8.854) (0.085) | (1.201) | (0.000) | (8.968) | (80.714) | (110.591) | (0.006) |
|  | 4 | 24.410 | 102.8830 .309 | 24.410 | 0.000 | 78.473 | 338.331 | 845.843 | 0.054 |
|  |  | (2.367) | (4.991) (0.081) | (2.367) | (0.000) | (6.123) | (26.998) | (59.215) | (0.004) |
|  | 5 | 19.611 | 91.5600 .323 | 19.611 | 0.000 | 71.949 | 351.379 | 606.074 | 0.052 |
|  |  | (1.637) | (4.160) (0.062) | (1.637) | (0.000) | (3.416) | (28.918) | (82.770) | (0.010) |
|  | 6 | 24.704 | 100.2020 .282 | 24.704 | 0.000 | 75.498 | 414.317 | 715.485 | 0.052 |
|  |  | (1.025) | (4.961) (0.040) | (1.025) | (0.000) | (4.249) | (47.232) | (84.607) | (0.006) |
|  | 7 | 27.249 | 100.1060 .247 | 27.249 | 0.000 | 72.857 | 476.554 | 723.964 | 0.044 |
|  |  | (2.806) | (2.700) (0.036) | (2.806) | (0.000) | (3.935) | (53.006) | (26.120) | (0.008) |
|  | 8 | 26.406 | $100.708 \quad 0.243$ | 26.406 | 0.000 | 74.301 | 450.251 | 772.890 | 0.058 |
|  |  | (1.568) | (2.206) (0.032) | (1.568) | (0.000) | (3.356) | (38.439) | (77.425) | (0.014) |

Table 11. (Continued).

| Subj | Cond | Cont | Max | Tmax | Min | Tmin | ROM | ContVel | MaxVel | TmaxVel |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 9 | 1 | 36.434 | 76.652 | 0.141 | 12.385 | 0.538 | 64.267 | 401.998 | 713.104 | 0.024 |
|  |  | (15.398) | (2.403) | (0.030) | (6.466) | (0.023) | (7.222) | (247.106) | (40.946) | (0.022) |
|  | 2 | 23.837 | 74.111 | 0.145 | 5.581 | '0.546 | 68.529 | 272.979 | 720.542 | 0.044 |
|  |  | (3.205) | (3.013) | (0.009) | (5.572) | (0.027) | (5.313) | (97.056) | (26.592) | (0.006) |
|  | 3 | 27.206 | 80.174 | 0.141 | 9.501 | 0.549 | 70.673 | 385.388 | 862.942 | 0.039 |
|  |  | (1.027) | (3.669) | (0.020) | (7.864) | (0.033) | (11.043) | (150.688) | (115.351) | (0.009) |
|  | 4 | 26.994 | 80.500 | 0.128 | 7.908 | 0.544 | 72.592 | 420.064 | 864.912 | 0.037 |
|  |  | (6.055) | (3.848) | (0.030) | (7.671) | (0.035) | (5.695) | (170.640) | (38.658) | (0.013) |
|  | 5 | 31.395 | 80.507 | 0.173 | 19.553 | 0.477 | 60.954 | 354.453 | 616.594 | 0.036 |
|  |  | (8.314) | (1.825) | (0.024) | (4.522) | (0.267) | (5.930) | (153.145) | (31.968) | (0.018) |
|  | 6 | 28.270 | 78.243 | 0.157 | 14.828 | 0.472 | 63.415 | 328.715 | 665.984 | 0.044 |
|  |  | (2.451) | (2.305) | (0.007) | (9.070) | (0.264) | (10.609) | (65.739) | (78.642) | (0.005) |
|  | 7 | 30.619 | 82.680 | 0.152 | 10.830 | 0.564 | 71.850 | 428.749 | 686.340 | 0.039 |
|  |  | (5.619) | (4.326) | (0.015) | (7.878) | (0.056) | (11.603) | (125.075) | (94.923) | (0.013) |
|  | 8 | 34.748 | 86.136 | 0.136 | 10.803 | 0.591 | 75.333 | 532.746 | 790.841 | 0.031 |
|  |  | (8.502) | (2.757) | (0.019) | (7.944) | (0.021) | (9.633) | (167.870) | (39.778) | (0.016) |
| 10 | 1 | 26.012 | 68.089 | 0.120 | 9.456 | 0.563 | 58.633 | 326.827 | 508.970 | 0.044 |
|  |  | (1.766) | (1.358) | (0.004) | (2.323) | (0.040) | (2.052) | (56.095) | (30.315) | (0.007) |
|  | 2 | 27.740 | 75.661 | 0.143 | 14.870 | 0.600 | 60.791 | 341.802 | 529.628 | 0.047 |
|  |  | (2.064) | (4.499) | (0.016) | (2.549) | (0.000) | (3.660) | (60.064) | (18.488) | (0.012) |
|  | 3 | 28.418 | 80.395 | 0.127 | 17.524 | 0.588 | 62.871 | 360.287 | 625.797 | 0.048 |
|  |  | (3.588) | (2.710) | (0.005) | (2.042) | (0.026) | (3.477) | (41.297) | (64.976) | (0.004) |
|  | 4 | 30.049 | 89.008 | 0.168 | 23.659 | 0.360 | 65.349 | 440.177 | 641.177 | 0.048 |
|  |  | (2.774) | (2.691) | (0.024) | (7.620) | (0.329) | (5.663) | (25.914) | (29.143) | (0.005) |
|  | 5 | 22.270 | 62.452 | 0.118 | 9.448 | 0.545 | 53.004 | 317.997 | 475.834 | 0.046 |
|  |  | (1.387) | (1.872) | (0.011) | (2.220) | (0.076) | (3.535) | (46.580) | (40.097) | (0.010) |
|  | 6 | 25.123 | 71.229 | 0.122 | 11.437 | 0.540 | 59.792 | 324.723 | 540.035 | 0.050 |
|  |  | (3.080) | (2.236) | (0.008) | (1.727) | (0.085) | (2.684) | (32.841) | (61.530) | (0.008) |
|  | 7 | 26.817 | 80.676 | 0.134 | 14.306 | 0.597 | 66.370 | 396.745 | 569.644 | 0.052 |
|  |  | (1.700) | (1.798) | (0.006) | (3.657) | (0.008) | (5.023) | (40.895) | (19.549) | (0.006) |
|  | 8 | 28.705 | 83.857 | 0.142 | 14.542 | 0.600 | 69.315 | 425.395 | 600.279 | 0.048 |
|  |  | (2.713) | (1.157) | (0.013) | (2.813) | (0.000) | (2.794) | (36.686) | (10.504) | (0.011) |

Note: Angle and ROM units are in degrees and time unit is in s .
Velocity unit is in deg/s.
Standard deviation values are in parenthesis.
The definitions of variables are in Appendix A.

Table 12. Subject means and standard deviations of knee joint variables (Group 2).

| Subj | Cond | Cont | Max | Tmax | Min | Tmin | ROM | ContVel | MaxVel | TmaxVel |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | 26.626 | 82.613 | 0.207 | 8.991 | 0.599 | 73.622 | 290.447 | 600.116 | 0.048 |
|  |  | (4.718) | (5.590) | (0.011) | (3.960) | (0.002) | (2.078) | (43.996) | (19.795) | (0.008) |
|  | 2 | 30.396 | 84.431 | 0.186 | 10.504 | 0.595 | 73.927 | 370.154 | 647.645 | 0.039 |
|  |  | (5.264) | (1.638) | (0.027) | (8.364) | (0.011) | (8.035) | (51.695) | (51.014) | (0.009) |
|  | 3 | 31.329 | 86.945 | 0.188 | 11.453 | 0.599 | 75.492 | 404.171 | 685.845 | 0.035 |
|  |  | (4.170) | (7.633) | (0.034) | (4.374) | (0.002) | (3.405) | (94.297) | (31.011) | (0.009) |
|  | 4 | 32.517 | 90.142 | 0.202 | 13.263 | 0.600 | 76.879 | 383.773 | 692.780 | 0.037 |
|  |  | (4.655) | (2.387) | (0.009) | (5.789) | (0.000) | (4.450) | (82.731) | (38.363) | (0.009) |
|  | 5 | 32.153 | 79.856 | 0.172 | 8.204 | 0.568 | 71.652 | 393.660 | 565.341 | 0.035 |
|  |  | (4.517) | (3.261) | (0.013) | (2.735) | (0.028) | (2.434) | (65.386) | (25.522) | (0.009) |
|  | 6 | 29.396 | 82.438 | 0.213 | 9.580 | 0.598 | 72.859 | 391.494 | 596.918 | 0.036 |
|  |  | (5.234) | (4.693) | (0.026) | (8.494) | (0.004) | (6.721) | (45.001) | (31.744) | (0.005) |
|  | 7 | 34.729 | 84.056 | 0.159 | 11.334 | 0.595 | 72.722 | 466.637 | 618.304 | 0.028 |
|  |  | (3.990) | (3.421) | (0.024) | (3.104) | (0.005) | (6.277) | (41.153) | (28.460) | (0.004) |
|  | 8 | 30.294 | 82.967 | 0.156 | 11.614 | 0.585 | 71.353 | 424.749 | 635.179 | 0.037 |
|  |  | (3.761) | (8.940) | (0.028) | (5.969) | (0.016) | (13.402) | (78.040) | (62.785) | (0.009) |
| 2 | 1 | 27.920 | 73.408 | 0.142 | 20.965 | 0.360 | 52.443 | 396.488 | 757.030 | 29 |
|  |  | (2.680) | (2.518) | (0.011) | (7.847) | (0.329) | (6.681) | (132.575) | (38.639) | (0.008) |
|  | 2 | 30.102 | 80.930 | 0.158 | 28.515 | 0.360 | 52.415 | 401.773 | 879.926 | 0.029 |
|  |  | (4.313) | (2.469) | (0.013) | (4.410) | (0.329) | (5.702) | (177.420) | (135.065) | (0.007) |
|  | 3 | 30.245 | 85.297 | 0.161 | 30.245 | 0.000 | 55.052 | 448.194 | 887.314 | 0.031 |
|  |  | (2.844) | (3.048) | (0.005) | (2.844) | (0.000) | (1.364) | (125.867) | (20.184) | (0.007) |
|  | 4 | 32.556 | 89.677 | 0.158 | 23.396 | 0.360 | 66.280 | 577.185 | 1125.636 | 0.025 |
|  |  | (6.522) | (3.529) | (0.012) | (8.228) | (0.329) | (5.085) | (218.382) | (132.436) | (0.007) |
|  | 5 | 30.330 | 79.554 | 0.148 | 27.223 | 0.120 | 52.331 | 500.213 | 725.268 | 0.023 |
|  |  | (1.902) | (2.467) | (0.007) | (8.146) | (0.268) | (7.281) | (96.248) | (27.460) | (0.006) |
|  | 6 | 28.375 | 78.544 | 0.148 | 27.555 | 0.120 | 50.989 | 401.514 | 753.332 | 0.031 |
|  |  | (1.340) | (2.703) | (0.009) | (2.498) | (0.268) | (2.153) | (63.954) | '(57.746) | (0.005) |
|  | 7 | 24.709 | 81.515 | 0.169 | 24.709 | 0.000 | 56.806 | 341.009 | 878.317 | 0.041 |
|  |  | (3.480) | (3.353) | (0.014) | (3.480) | (0.000) | (3.093) | (94.206) | (121.100) | (0.008) |
|  | 8 | 25.384 | 86.163 | 0.162 | 23.267 | 0.360 | 62.896 | 379.099 | 943.781 | 0.040 |
|  |  | (4.832) | (4.479) | (0.006) | (5.360) | (0.329) | (2.254) | (85.913) | (74.933) | (0.007) |

Table 12. (Continued).

| Subj Cond | Cont | Max | Tmax | Min | Tmin | ROM | ContVel | MaxVel | TmaxVel |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | 1 | 27.772 | 80.003 | 0.220 | 27.772 | 0.000 | 52.231 | 286.030 | 637.149 | 0.033 |
|  |  | $(4.417)$ | $(8.028)$ | $(0.029)$ | $(4.417)$ | $(0.000)$ | $(4.037)$ | $(67.656)$ | $(40.376)$ | $(0.007)$ |
|  | 2 | 32.897 | 93.043 | 0.264 | 30.400 | 0.240 | 62.644 | 357.039 | 763.341 | 0.030 |
|  |  | $(5.187)$ | $(6.472)$ | $(0.042)$ | $(4.492)$ | $(0.329)$ | $(4.446)$ | $(116.161)$ | $(65.280)$ | $(0.006)$ |
|  | 3 | 33.061 | 95.099 | 0.249 | 33.061 | 0.000 | 62.037 | 353.942 | 808.088 | 0.034 |
|  | $(5.248)$ | $(3.442)$ | $(0.019)$ | $(5.248)$ | $(0.000)$ | $(6.467)$ | $(138.572)$ | $(54.878)$ | $(0.009)$ |  |
|  | 4 | 30.835 | 102.097 | 0.288 | 30.835 | 0.000 | 71.262 | 273.293 | 895.241 | 0.040 |
|  | $(2.798)$ | $(2.659)$ | $(0.043)$ | $(2.798)$ | $(0.000)$ | $(4.578)$ | $(58.036)$ | $(54.168)$ | $(0.006)$ |  |
| 5 | 21.123 | 66.712 | 0.203 | 21.123 | 0.000 | 45.589 | 278.076 | 607.630 | 0.038 |  |
|  | $(5.365)$ | $(12.683)$ | $(0.040)$ | $(5.365)$ | $(0.000)$ | $(7.914)$ | $(104.934)$ | $(70.824)$ | $(0.014)$ |  |
| 6 | 31.809 | 91.123 | 0.267 | 31.809 | 0.000 | 59.314 | 364.334 | 709.675 | 0.035 |  |
|  | $(3.757)$ | $(4.898)$ | $(0.033)$ | $(3.757)$ | $(0.000)$ | $(5.810)$ | $(142.502)$ | $(34.444)$ | $(0.012)$ |  |
|  | 7 | 34.724 | 90.258 | 0.228 | 34.710 | 0.120 | 55.549 | 321.884 | 678.267 | 0.037 |
|  | $(3.534)$ | $(3.958)$ | $(0.057)$ | $(3.520)$ | $(0.268)$ | $(2.731)$ | $(79.774)$ | $(35.814)$ | $(0.006)$ |  |
| 8 | 35.887 | 97.669 | 0.228 | 35.887 | 0.000 | 61.782 | 483.054 | 748.563 | 0.031 |  |
|  | $(4.275)$ | $(5.594)$ | $(0.053)$ | $(4.275)$ | $(0.000)$ | $(9.548)$ | $(103.643)$ | $(46.125)$ | $(0.010)$ |  |

Note: Angle and ROM units are in degrees and time unit is in s.
Velocity unit is in deg/s.
Standard deviation values are in parenthesis.
The definitions of variables are in Appendix A.

Table 13. Subject means and standard deviations of hip joint variables (Group 1).

| Subj | Cond | Cont | Max | Tmax | Min | Tmin | ROM | ContVel | MaxVe | TmaxVel |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | 19.018 | 55.194 | 0.195 | 11.511 | 0.600 | 43.684 | 113.611 | 384.047 | 0.071 |
|  |  | (3.343) | (6.488) | (0.015) | (4.467) | (0.000) | (2.861) | (27.888) | (51.135) | (0.012) |
|  | 2 | 26.825 | 65.719 | 0.193 | 19.441 | 0.600 | 46.278 | 240.927 | 417.453 | 0.045 |
|  |  | (1.170) | (5.066) | (0.013) | (7.456) | (0.000) | (6.506) | (62.577) | (29.780) | (0.010) |
|  | 3 | 19.136 | 67.100 | 0.210 | 17.330 | 0.360 | 49.771 | 119.028 | 549.531 | 0.064 |
|  |  | (4.571) | (6.107) | (0.009) | (5.306) | (0.329) | (2.951) | (51.181) | (22.815) | (0.008) |
|  | 4 | 25.389 | 84.231 | 0.258 | 25.282 | 0.120 | 58.948 | 223.257 | 643.214 | 0.045 |
|  |  | (2.936) | (3.986) | (0.028) | (2.925) | (0.268) | (6.411) | (117.326) | (37.501) | (0.012) |
|  | 5 | 16.178 | 42.947 | 0.139 | 10.475 | 0.480 | 32.472 | 102.235 | 376.795 | 0.062 |
|  |  | (2.836) | (1.919) | (0.027) | (3.736) | (0.268) | (4.215) | (51.111) | (45.015) | (0.012) |
|  | 6 | 17.186 | 57.564 | 0.171 | 8.073 | 0.600 | 49.491 | 176.533 | 511.322 | 0.052 |
|  |  | (1.534) | (6.166) | (0.020) | (4.562) | (0.000) | (3.144) | (48.791) | (31.807) | (0.006) |
|  | 7 | 24.027 | 70.403 | 0.198 | 18.471 | 0.600 | 51.932 | 231.784 | 523.673 | 0.042 |
|  |  | (3.968) | (1.791) | (0.015) | (1.338) | (0.000) | (2.487) | (75.181) | (36.900) | (0.009) |
|  | 8 | 20.703 | 78.908 | 0.247 | 19.706 | 0.240 | 59.202 | 187.773 | 584.934 | 0.055 |
|  |  | (1.380) | (4.361) | (0.032) | (1.656) | (0.329) | (3.455) | (46.229) | (75.299) | (0.017) |
| 2 | 1 | 31.792 | 73.988 | 0.273 | 31 | 0.000 | 42.196 | 93.595 | 452.127 | 0.060 |
|  |  | (3.610) | (6.931) | (0.056) | (3.610) | (0.000) | (6.058) | (42.601) | (22.101) | $(0.006)$ |
|  | 2 | 36.589 | 81.523 | 0.263 | 36.589 | 0.000 | 44.935 | 155.943 | 482.425 | 0.052 |
|  |  | (5.535) | (5.592) | (0.052) | (5.535) | (0.000) | (5.388) | (44.304) | (28.153) | (0.008) |
|  | 3 | 37.414 | 100.123 | 0.277 | 37.414 | 0.000 | 62.709 | 157.865 | 661.321 | 0.054 |
|  |  | (2.042) | (5.643) | (0.021) | (2.042) | (0.000) | (6.476) | (51.558) | (33.867) | (0.009) |
|  | 4 | 37.107 | 101.145 | 0.265 | 37.107 | 0.000 | 64.037 | 207.409 | 677.999 | 0.047 |
|  |  | (2.929) | (6.014) | (0.013) | (2.929) | (0.000) | (4.230) | (36.087) | (44.481) | $(0.005)$ |
|  | 5 | 33.262 | 71.811 | 0.265 | 33.262 | 0.000 | 38.549 | 55.783 | 433.632 | 0.066 |
|  |  | (4.632) | (7.846) | (0.032) | (4.632) | (0.000) | (4.456) | (44.947) | (51.506) | (0.008) |
|  | 6 | 36.316 | 88.530 | 0.266 | 36.316 | 0.000 | 52.214 | 138.168 | 552.153 | 0.056 |
|  |  | (1.210) | (6.271) | (0.021) | (1.210) | (0.000) | (6.019) | (30.003) | (68.485) | (0.006) |
|  | 7 | 36.503 | 94.636 | 0.258 | 36.503 | 0.000 | 58.132 | 141.958 | 612.886 | 0.053 |
|  |  | (1.845) | (7.764) | (0.022) | (1.845) | (0.000) | (7.701) | (23.183) | (37.792) | (0.005) |
|  | 8 | 43.481 | 106.786 | 0.255 | 43.481 | 0.000 | 63.306 | 202.930 | 671.995 | 0.056 |
|  |  | (4.269) | (4.764) | (0.030) | (4.269) | (0.000) | (3.809) | (48.631) | (63.873) | (0.010) |

Table 13. (Continued).

| Subj | Cond | Cont | Max | Tmax | Min | Tmin | ROM | ContVel | MaxVel | TmaxVel |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | 1 | 39.092 | 61.019 | 0.143 | 25.467 | 0.586 | 35.552 | 165.812 | 352.051 |  |
|  |  | (5.046) | (3.64) | (0.020) | (1.795) | (0.034) | (4.858) | (147.455) | (59.216) | (0.021) |
|  | 2 | 39.741 | 72.879 | 0.190 | 29.010 | 0.595 | 43.869 | 146.287 | 385.708 | 0.044 |
|  |  | (3.885) | (11.050) | (0.041) | (6.353) | (0.011) | (4.712) | (31.593) | (61.117) | (0.011) |
|  | 3 | 38.836 | 80.345 | 0.201 | 28.769 | 0.586 | 51.576 | 107.844 | 519.557 | 0.058 |
|  |  | (1.998) | (5.087) | (0.029) | (5.462) | (0.017) | (4.345) | (46.022) | (70.931) | (0.012) |
|  | 4 | 46.161 | 97.532 | 0.212 | 32.807 | 0.498 | 64.725 | 263.024 | 575.613 | 0.039 |
|  |  | (5.973) | (6.741) | (0.035) | (8.379) | (0.244) | (4.116) | (116.176) | (53.487) | (0.019) |
|  | 5 | 35.729 | 59.269 | 0.140 | 27.169 | 0.554 | 32.100 | 58.054 | 342.412 | 0.053 |
|  |  | (1.934) | (3.080) | (0.022) | (0.999) | (0.065) | (3.273) | (32.233) | (33.746) | (0.008) |
|  | 6 | 42.508 | 90.254 | 0.225 | 29.748 | 0.480 | 60.507 | 142.297 | 466.733 | 0.066 |
|  |  | (2.621) | (8.816) | (0.036) | (9.597) | (0.268) | (4.687) | (21.459) | (55.656) | (0.010) |
|  | 7 | 46.171 | 96.845 | 0.217 | 30.872 | 0.600 | 65.973 | 203.123 | 503.397 | 0.054 |
|  |  | (2.498) | (4.345) | (0.013) | (4.961) | (0.000) | (3.849) | (67.702) | (32.449) | (0.015) |
|  | 8 | 41.055 | 100.782 | 0.230 | 36.453 | 0.480 | 64.329 | 243.203 | 587.970 | 0.048 |
|  |  | (6.738) | (4.355) | (0.014) | (3.524) | (0.268) | (3.264) | (119.149) | (90.194) | (0.016) |
| 4 | 1 | 44.590 | 94 |  |  |  | 49.684 | 138.634 | 439.668 |  |
|  |  | (2.903) | (5.587) | (0.015) | (2.897) | (0.268) | (3.519) | (83.723) | (26.869) | (0.014) |
|  | 2 | 45.229 | 104.843 | 0.269 | 45.229 | 0.000 | 59.614 | 128.998 | 527.271 | 0.046 |
|  |  | (3.143) | (2.051) | (0.006) | (3.143) | (0.000) | (2.268) | (38.441) | (31.378) | (0.006) |
|  | 3 | 40.602 | 112.237 | 0.293 | 40.602 | 0.000 | 71.635 | 109.340 | 612.384 | 0.0 |
|  |  | (3.691) | (2.567) | (0.011) | (3.691) | (0.000) | (3.157) | (44.616) | (28.537) | (0.007) |
|  | 4 | 39.879 | 121.475 | 0.306 | 39.879 | 0.000 | 81.596 | 128.363 | 699.895 | 0.047 |
|  |  | (3.633) | (4.405) | (0.018) | (3.633) | (0.000) | (3.800) | (128.754) | (81.809) | (0.011) |
|  | 5 | 42.642 | 88.793 | 0.247 | 38.918 | 0.120 | 49.875 | 181.050 | 405.922 | 0.044 |
|  |  | (6.096) | (9.095) | (0.043) | (4.570) | (0.268) | (6.578) | (116.637) | $(21.521)$ | (0.022) |
|  | 6 | 39.724 | 101.121 | 0.271 | 39.724 | 0.000 | 61.397 | 105.339 | 539.864 | 0.052 |
|  |  | (2.633) | (2.509) | (0.018) | (2.633) | (0.000) | (2.736) | (54.024) | (26.713) | (0.005) |
|  | 7 | 38.870 | 115.880 | 0.291 | 38.870 | 0.000 | 77.010 | 102.225 | 634.420 | 0.055 |
|  |  | (1.573) | (3.406) | (0.011) | (1.573) | (0.000) | (2.484) | (35.628) | (35.518) | (0.007) |
|  | 8 | 41.635 | 126.560 | 0.299 | 41.635 | 0.000 | 84.925 | 127.027 | 662.525 | 0.054 |
|  |  | (3.208) | (5.225) | (0.015) | (3.208) | (0.000) | (2.991) | (53.177) | (27.182) | (0.004) |

Table 13. (Continued).

| Subj | ond | Cont | Max | Tmax | Min | Tmin | ROM | ContVel | MaxVel | TmaxVe |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5 | 1 | 34.709 | 71.232 | 0.217 | 34.709 | 0.000 | 36.522 | 225.805 | 385.121 |  |
|  |  | (8.403) | (17.90 | (0.046) | (8.403) | (0.000) | (10.346) | (69.801) | (42.095) | (0.013) |
|  | 2 | 35.618 | 76.517 | 0.208 | 34.818 | 0.120 | 41.699 | 244.617 | 480.312 | 0.041 |
|  |  | (7.000) | (5.413) | (0.025) | (6.791) | (0.268) | (3.664) | (111.626) | (59.427) | (0.016) |
|  | 3 | 33.748 | 80.479 | 0.206 | 30.682 | 0.120 | 49.797 | 249.023 | 508.797 | 0.047 |
|  |  | (6.100) | (2.822) | (0.016) | (3.153) | (0.268) | (4.239) | (65.764) | (23.642) | (0.011) |
|  | 4 | 35.619 | 76.602 | 0.175 | 27.554 | 0.600 | 49.047 | 211.253 | 538.795 | 0.048 |
|  |  | (3.344) | (8.268) | (0.026) | (8.354) | (0.000) | (6.674) | (48.483) | (99.970) | (0.007) |
|  | 5 | 35.327 | 68.222 | 0.188 | 29.503 | 0.360 | 38.719 | 233.727 | 368.075 | 0.043 |
|  |  | (2.456) | (5.050) | (0.031) | (8.269) | (0.329) | (7.137) | (57.244) | (33.932) | (0.016) |
|  | 6 | 36.182 | 81.163 | 0.201 | 30.797 | 0.360 | 50.367 | 286.260 | 476.535 | 0.040 |
|  |  | (3.816) | (9.146) | (0.031) | (4.961) | (0.329) | (7.744) | (78.002) | (21.018) | (0.015) |
|  | 7 | 33.492 | 80.785 | 0.181 | 21.437 | 0.600 | 59.348 | 309.272 | 548.932 | 0.037 |
|  |  | (4.904) | (5.398) | (0.016) | (6.090) | (0.000) | (4.333) | (41.543) | (52.098) | (0.007) |
|  | 8 | 42.199 | 95.287 | 0.181 | 25.275 | 0.600 | 70.012 | 282.645 | 590.034 | 0.042 |
|  |  | (2.530) | (4.961) | (0.014) | (2.541) | (0.000) | (2.572) | (28.023) | (19.779) | (0.005) |
| 6 | 1 | 42.382 | 84.845 | 0.252 | 40.884 | 0.2 | 43.961 |  | 428.782 |  |
|  |  | (4.095) | (5.129) | (0.021) | (6.524) | (0.329) | (6.822) | (45.621) | (39.729) | (0.012) |
|  | 2 | 43.987 | 94.753 | 0.254 | 43.987 | 0.000 | 50.766 | 169.371 | 467.925 | 0.043 |
|  |  | (3.048) | (2.418) | (0.024) | (3.048) | (0.000) | (3.899) | (78.998) | (25.139) | (0.011) |
|  | 3 | 43.360 | 98.349 | 0.248 | 40.949 | 0.120 | 57.401 | 257.163 | 563.733 | 0.035 |
|  |  | (4.450) | (7.012) | (0.038) | (4.644) | (0.268) | (6.868) | (110.396) | (35.037) | (0.012) |
|  | 4 | 41.882 | 104.191 | 0.249 | 41.171 | 0.120 | 63.019 | 205.460 | 641.516 | 0.039 |
|  |  | (2.160) | (5.969) | (0.015) | (0.943) | (0.268) | (5.622) | (98.691) | .(51.011) | (0.007) |
|  | 5 | 36.816 | 83.193 | 0.258 | 34.300 | 0.240 | 48.893 | 117.849 | 423.609 | 0.050 |
|  |  | (2.957) | (5.671) | (0.014) | (5.227) | (0.329) | (1.031) | (42.236) | (39.968) | (0.009) |
|  | 6 | 42.558 | 99.458 | 0.281 | 42.558 | 0.000 | 56.900 | 157.603 | 433.789 | 0.052 |
|  |  | (1.419) | (5.274) | (0.015) | (1.419) | (0.000) | (6.540) | (26.134) | (31.937) | (0.007) |
|  | 7 | 41.737 | 108.396 | 0.292 | 41.737 | 0.000 | 66.659 | 206.298 | 516.240 | 0.052 |
|  |  | (3.429) | (3.742) | (0.019) | (3.429) | (0.000) | (5.246) | (48.197) | (41.428) | (0.010) |
|  | 8 | 37.687 | 117.782 | 0.273 | 37.687 | 0.000 | 80.095 | 236.354 | 636.454 | 0.048 |
|  |  | (2.978) | (4.069) | (0.011) | (2.978) | ${ }^{\circ}(0.000)$ | (6.622) | (38.237) | (54.790) | (0.005) |

Table 13. (Continued).

| Subj | ond | Cont | Max Tmax | Min | Tmin | ROM | ContVel | MaxVel | TmaxVel |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7 | 1 | 29.672 | 64.2050 .241 | 27.536 | 0.240 | 36.670 | 40.05 | 324.887 | 0.078 |
|  |  | (3.277) | (13.723) (0.031) | (4.667) | (0.329) | (9.661) | (38.245) | (55.973) | (0.017) |
|  | 2 | 31.102 | $74.804 \quad 0.268$ | 31.102 | 0.000 | 43.703 | $148.931$ | 335.227 | 0.087 |
|  |  | (3.044) | (8.410) (0.015) | (3.044) | (0.000) | (6.012) | (35.716) | (13.267) | (0.016) |
|  | 3 | 38.231 | 100.2250 .269 | 38.231 | 0.000 | 61.994 | 196.462 | 485.190 | 0.073 |
|  |  | (2.452) | (2.848) (0.018) | (2.452) | (0.000) | (4.447) | (46.322) | (103.377) | (0.009) |
|  | 4 | 37.391 | 111.9710 .290 | 37.391 | 0.000 | 74.579 | 235.721 | 548.151 | 0.063 |
|  |  | (4.086) | (2.802) (0.009) | (4.086) | (0.000) | (5.150) | (37.796) | (84.478) | (0.009) |
|  | 5 | 29.273 | $71.560 \quad 0.275$ | 26.305 | 0.120 | 45.256 | 80.709 | 305.520 | 0.080 |
|  |  | (2.550) | (10.898) (0.051) | (6.039) | (0.268) | (12.096) | (36.008) | (19.804) | (0.016) |
|  | 6 | 29.480 | 78.8850 .269 | 29.480 | 0.000 | 49.406 | 110.662 | 397.962 | 0.074 |
|  |  | (4.377) | (8.258) (0.027) | (4.377) | (0.000) | (5.104) | (40.243) | (51.519) | (0.010) |
|  | 7 | 32.323 | 104.3540 .310 | 32.323 | 0.000 | 72.032 | 208.919 | 476.978 | 0.083 |
|  |  | (5.770). | (4.061) (0.015) | (5.770) | (0.000) | (3.444) | (24.866) | (32.861) | (0.015) |
|  | 8 | 37.426 | 117.5740 .292 | 37.426 | 0.000 | 80.149 | 232.406 | 589.337 | 0.071 |
|  |  | (4.518) | (11.237) (0.020) | 518) | (0.00 | 01 | (56.948) | (97.146) | (0.014) |
| 8 | 1. | 29.912 | 87.1830 .433 | 29.912 | 0.000 | 57.271 | 118.596 | 413.004 | 0.056 |
|  |  | (3.539) | (7.869) (0.090) | (3.539) | (0.000) | (5.745) | (20.798) | (17.045) | (0.011) |
|  | 2 | 32.983 | 105.8760 .394 | 32.983 | 0.000 | 72.894 | 125.107 | 494.279 | 0.065 |
|  |  | (2.479) | (5.387) (0.027) | (2.479) | (0.000) | (6.019) | (23.645) | (44.028) | (0.007) |
|  | 3 | 27.019 | 108.9810 .474 | 27.019 | 0.000 | 81.962 | 145.682 | 616.561 | 0.057 |
|  |  | (3.312) | (3.715) (0.089) | (3.312) | (0.000) | (6.023) | (34.484) | (94.387) | (0.005) |
|  | 4 | 25.364 | 120.5390 .520 | 25.364 | 0.000 | 95.176 | 157.203 | 644.420 | 0.063 |
|  |  | (1.912) | (5.170) (0.032) | (1.912) | (0.000) | (4.599) | (32.037) | (11.034) | (0.009) |
|  | 5 | 33.901 | 106.3910 .390 | 33.901 | 0.000 | 72.490 | 149.884 | 452.724 | 0.117 |
|  |  | (2.319) | (3.362) (0.023) | (2.319) | (0.000) | (5.107) | (17.503) | (58.837) | (0.121) |
|  | 6 | 37.768 | 114.8930 .353 | 37.768 | 0.000 | 77.124 | 160.531 | 526.750 | 0.063 |
|  |  | (3.990) | (3.649) (0.028) | (3.990) | (0.000) | (6.820) | (30.060) | (47.440) | (0.011) |
|  | 7 | 31.043 | 111.1100 .365 | 31.043 | 0.000 | 80.066 | 224.088 | 580.678 | 0.058 |
|  |  | (4.972) | (10.678) (0.062) | (4.972) | (0.000) | (10.287) | (38.604) | (27.622) | (0.005) |
|  | 8 | 29.062 | $121: 4150.388$ | 29.062 | 0.000 | 92.353 | 245.351 | 673.796 | 0.064 |
|  |  | (3.772) | (10.407) (0.058) | (3.772) | (0.000) | (7.166) | (36.074) | (34.599) | (0.013) |

Table 13. (Continued).

| Subj | Cond | Cont | Max | Tmax | Min | Tmin | ROM | ContVel | MaxVel | TmaxVel |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 9 | 1 | 48.886 | 83.628 | 0.161 | 28.410 | 0.471 | 55.218 | 316.574 | 517.802 | 0.02 |
|  |  | (11.039) | (6.891) | (0.032) | (9.740) | (0.264) | (8.669) | (183.230) | (7.692) | (0.022) |
|  | 2 | 37.683 | 76.080 | 0.166 | 27.621 | 0.593 | 48.459 | 145.904 | 497.921 | 0.050 |
|  |  | (6.076) | (6.696) | (0.005) | (6.164) | (0.017) | (10.022) | (55.082) | (29.494) | (0.004) |
|  | 3 | 34.299 | 75.377 | 0.162 | 21.122 | 0.600 | 54.254 | 187.311 | 617.036 | 0.045 |
|  |  | (2.472) | (4.721) | (0.028) | (4.156) | (0.000) | (7.156) | (82.343) | (96.501) | (0.010) |
|  | 4 | 35.638 | 76.265 | 0.152 | 21.129 | 0.596 | 55:136 | 217.920 | 619.480 | 0.042 |
|  |  | (2.387) | (1.504) | (0.014) | (3.344) | (0.009) | (3.622) | (89.232) | (25.449) | (0.011) |
|  | 5 | 51.419 | 99.609 | 0.219 | 39.419 | 0.480 | 60.190 | 229.054 | 463.513 | 0.043 |
|  |  | (6.061) | (6.203) | (0.031) | (3.894) | (0.268) | (7.558) | (118.355) | (24.043) | (0.018) |
|  | 6 | 45.557 | 90.342 | 0.200 | 36.653 | 0.480 | 53.689 | 177.838 | 495.598 | 0.052 |
|  |  | (3.884) | (6.293) | (0.027) | (8.631) | (0.268) | (4.793) | (32.771) | (42.309) | (0.004) |
|  | 7 | 40.721 | 84.291 | 0.172 | 27.380 | 0.600 | 56.911 | 235.346 | 530.081 | 0.047 |
|  |  | (6.104) | (10.229) | (0.015) | (4.244) | (0.000) | 11.630) | (91.477) | (76.203) | (0.014) |
|  | 8 | 44.309 | 91.062 | 0.168 | 28.502 | 0.600 | 62.560 | 319.547 | 607.871 | 0.040 |
|  |  | (4.685) | (6.548) | (0.025) | (8.320) | (0.000) | (9.385) | (130.270) | (34.966) | (0.016) |
| 10 | 1 | 32.090 | 55.043 | 0.134 | 24.111 | 0.600 | 30.932 | 112.664 | 276.996 |  |
|  |  | (1.778) | (4.334) | (0.008) | (3.377) | (0.000) | (5.978) | (37.132) | (40.218) | (0.006) |
|  | 2 | 30.760 | 56.911 | 0.159 | 17.885 | 0.600 | 39.026 | 97.794 | 292.088 | 0.065 |
|  |  | (4.004) | (5.653) | (0.017) | (3.207) | (0.000) | (3.156) | (30.666) | (21.156) | (0.010) |
|  | 3 | 28.608 | 60.609 | 0.143 | 18.614 | 0.600 | 41.995 | 145.587 | 383.931 | 0.056 |
|  |  | (2.851) | (3.685) | (0.021) | (3.014) | (0.000) | (2.871) | (32.275) | (37.201) | (0.002) |
|  | 4 | 34.207 | 77.104 | 0.210 | 29.723 | 0.480 | 47.381 | 199.952 | 429.297 | 0.059 |
|  |  | (2.058) | (4.662) | (0.025) | (6.047) | (0.268) | (2.551) | (15.650) | (15.957) | (0.006) |
|  | 5 | 29.723 | 51.017 | 0.133 | 20.002 | 0.585 | 31.015 | 97.021 | 253.519 | 0.064 |
|  |  | (2.868) | (4.959) | (0.021) | (4.071) | (0.034) | (4.529) | (33.001) | (10.416) | (0.014) |
|  | 6 | 25.528 | 51.599 | 0.130 | 14.060 | 0.600 | 37.540 | 129.234 | 304.457 | 0.058 |
|  |  | (2.223) | (6.364) | (0.010) | (2.365) | (0.000) | (4.452) | (42.264) | (51.559) | (0.006) |
|  | 7 | 27.654 | 62.512 | 0.159 | 17.219 | 0.600 | 45.293 | 146.223 | 363.156 | 0.069 |
|  |  | (3.755) | (5.439) | (0.014) | (1.291) | (0.000) | (4.790) | (26.244) | (21.789) | (0.008) |
|  | 8 | 27.145 | 68.768 | 0.178 | 20.192 | 0.600 | 48.576 | 215.687 | 412.300 | 0.062 |
|  |  | (2.731) | (5.206) | (0.025) | (2.126) | (0.000) | (6.178) | (24.935) | (13.046) | (0.006) |

Note: Angle and ROM units are in degrees and time unit is in s.
Velocity unit is in deg/s.
Standard deviation values are in parenthesis.
The definitions of variables are in Appendix A.

Table 14. Subject means and standard deviations of hip joint variables (Group 2).


Table 14. (Continued).

| Subj | ond | Cont | Max | Tmax | Min | Tmin | ROM | ContVel | MaxVel | TmaxVel |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | 1 | 25.475 | 62.955 | 0.234 | 25.475 | 0.000 | 37.480 | 213.160 | 446.945 | 0.035 |
|  |  | (4.961) | (12.9 | 0.043) | (4.961) | (0.000) | (8.179) | (60.199) | (38.535) | (0.007) |
|  | 2 | 30.816 | 87.384 | 0.268 | 30.600 | 0.240 | 56.784 | 264.241 | 589.015 | 0.033 |
|  |  | (1.890) | (8.527) | (0.036) | (1.738) | (0.329) | (8.165) | (121.494) | (29.824) | (0.009) |
|  | 3 | 35.064 | 109.710 | 0.304 | 35.064 | 0.000 | 74.646 | 236.247 | 674.542 | 0.041 |
|  |  | (3.238) | (2.206) | (0.017) | (3.238) | (0.000) | (2.894) | (113.872) | (28.659) | (0.008) |
|  | 4 | 32.429 | 129.211 | 0.338 | 32.429 | 0.000 | 96.782 | 229.616 | 749.451 | 0.044 |
|  |  | (2.571) | (3.718) | (0.025) | (2.571) | (0.000) | (5.089) | (50.795) | (27.111) | (0.005) |
|  | 5 | 24.506 | 60.086 | 0.224 | 24.506 | 0.000 | 35.580 | 156.773 | 448.068 | 0.042 |
|  |  | (3.785) | (11.270) | (0.039) | (3.785) | (0.000) | (8.740) | (107.965) | (52.746) | (0.015) |
|  | 6 | 36.456 | 114.331 | 0.323 | 36.456 | 0.000 | 77.876 | 237.734 | 591.653 | 0.041 |
|  |  | (5.193) | (4.298) | (0.025) | (5.193) | (0.000) | (7.814) | (116.662) | (48.636) | (0.012) |
|  | 7 | 35.724 | 118.676 | 0.293 | 35.724 | 0.000 | 82.952 | 218.277 | 608.543 | 0.043 |
|  |  | (5.979) | (1.840) | (0.011) | (5.979) | (0.000) | (5.140) | (42.259) | (17.280) | (0.004) |
|  | 8 | 39.684 | 137.730 | 0.332 | 39.684 | 0.000 | 98.046 | 344.366 | 699.641 | 0.041 |
|  |  | (6.735) | (7.368) | (0.046) | (6.735) | (0.000) | (5.772) | (77.210) | (42.666) | (0.009) |

Note: Angle and ROM units are in degrees and time unit is in s .
Velocity unit is in deg/s.
Standard deviation values are in parenthesis.
The definitions of variables are in Appendix A.

## APPENDIX D

## VERTICAL GROUND REACTION FORCE DATA

Table 15. Subject means and standard deviations of VGRF variables (Group 1).

| Subj Cond |  | FI | T1 | F2 | T2 | LrateFl | LrateF2 | Imp 100 ms |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | 14.100 | 0.009 | 53.537 | 0.051 | 1568.921 | 1343.100 | 2.691 |
|  |  | (2.600) | (0.002) | (8.404) | (0.008) | (175.864) | (447.434) | (0.311) |
|  | 2 | 20.014 | 0.008 | 63.453 | 0.041 | 2668.455 | 1953.229 | 2.810 |
|  |  | (1.407) | (0.000) | (7.266) | (0.001) | (187.533) | (274.141) | (0.413) |
|  | 3 | 29.960 | 0.007 | 67.047 | 0.037 | 4394.214 | 2119.323 | 2.946 |
|  |  | (1.297) | (0.000) | (10.945) | (0.002) | (297.932) | (525.330) | (0.428) |
|  | 4 | 36.965 | 0.007 | 77.008 | 0.036 | 5575.608 | 2618.059 | 3.040 |
|  |  | (1.827) | (0.001) | (8.009) | (0.002) | (498.744) | (559.858) | (0.299) |
|  | 5 | 12.902 | 0.009 | 59.966 | 0.057 | 1411.104 | 1222.301 | 2.128 |
|  |  | (0.864) | (0.001) | (16.309) | (0.003) | (117.148) | (436.699) | (0.272) |
|  | 6 | 16.102 | 0.006 | 99.206 | 0.045 | 2879.162 | 2629.775 | 3.260 |
|  |  | (5.465) | (0.002) | (15.348) | (0.008) | (824.214) | (985.798) | (0.291) |
|  | 7 | 19.104 | 0.005 | 111.290 | 0.041 | 3820.736 | 3425.548 | 2.905 |
|  |  | (4.406) | (0.000) | (14.473) | (0.002) | (881.200) | (552.017) | (0.319) |
|  | 8 | 21.454 | 0.005 | 113.428 | 0.039 | 4290.766 | 3704.182 | 3.168 |
|  |  | (8.778) | (0.000) | $(22.591)$ | (0.005) | (1755.629) | (1188.317) | (0.177) |
| 2 | 1 | 14.943 | 0.00 | 56 | 0.0 | 2 | 8 | 2.644 |
|  |  | (1.241) | (0.002) | (3.372) | (0.008) | (463.677) | (309.900) | (0.275) |
|  | 2 | 24.706 | 0.008 | 59.837 | 0.040 | 3169.560 | 1879.292 | 2.578 |
|  |  | (1.639) | (0.000) | (2.224) | (0.004) | (273.390) | (236.136) | (0.148) |
|  | 3 | 33.696 | 0.008 | 61.102 | 0.036 | 4142.645 | 2323.008 | 2.337 |
|  |  | (1.507) | (0.000) | (8.364) | (0.003) | (290.727) | (648.882) | (0.111) |
|  | 4 | 48.741 | 0.008 | 75.022 | 0.035 | 6106.236 | 3255.198 | 2.705 |
|  |  | (3.684) | (0.000) | (3.959) | (0.002) | (542.996) | (372.522) | (0.161) |
| 5 |  | 16.573 | 0.003 | 90.516 | 0.042 | 6291.708 | 2516.545 | 2.137 |
|  |  | (1.214) | (0.000) | (7.977) | (0.003) | (839.807) | (432.805) | (0.127) |
| 6 |  | 24.916 | 0.003 | 99.914 | 0.037 | 10138.654 | 3237.435 | 2.298 |
|  |  | (1.964) | (0.001) | (21.712) | (0.004) | (2984.841) | (1148.321) | (0.236) |
| 7 |  | 35.578 | 0.004 | 111.109 | 0.036 | 10077.746 | 3634.214 | 2.487 |
|  |  | (5.222) | (0.002) | (11.950) | (0.002) | (3898.535) | (467.727) | $(0.112)$ |
| 8 |  | 27.740 | 0.015 | 83.029 | 0.046 | 4018.672 | 2978.959 | 1.586 |
|  |  | (5.685) | (0.007) | (27.587) | (0.011) | (5721.221) | (1478.243) | (0.255) |

Table 15. (Continued).

| Subj | Cond | F1 | T1 | F2 | T2 | LrateF1 | LrateF2 | Imp 100 ms |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | 1 | $\begin{gathered} 16.972 \\ (1.475) \end{gathered}$ | $\begin{gathered} \hline 0.009 \\ (0.003) \end{gathered}$ | $\begin{aligned} & 62.357 \\ & (3.024) \end{aligned}$ | $\begin{gathered} 0.042 \\ (0.013) \end{gathered}$ | $\begin{aligned} & 2176.693 \\ & (756.347) \end{aligned}$ | $\begin{aligned} & 2023.216 \\ & (910.954) \end{aligned}$ | $\begin{aligned} & 2.831 \\ & (0.235) \end{aligned}$ |
|  | 2 | $\begin{gathered} 21.637 \\ (1.989) \end{gathered}$ | $\begin{gathered} 0.008 \\ (0.001) \end{gathered}$ | $\begin{aligned} & 67.879 \\ & (7.207) \end{aligned}$ | $\begin{gathered} 0.040 \\ (0.002) \end{gathered}$ | $\begin{aligned} & 2961.421 \\ & (273.365) \end{aligned}$ | $\begin{aligned} & 2355.103 \\ & (363.798) \end{aligned}$ | $\begin{gathered} 2.646 \\ (0.249) \end{gathered}$ |
|  | 3 | $\begin{aligned} & 29.154 \\ & (2.191) \end{aligned}$ | $\begin{gathered} 0.009 \\ (0.002) \end{gathered}$ | $\begin{gathered} 72.095 \\ (10.587) \end{gathered}$ | $\begin{gathered} 0.043 \\ (0.005) \end{gathered}$ | $\begin{aligned} & 3165.687 \\ & (420.962) \end{aligned}$ | $\begin{gathered} 2323.416 \\ (599.447) \end{gathered}$ | $\begin{gathered} 3.071 \\ (0.204) \end{gathered}$ |
|  | 4 | $\begin{aligned} & 33.588 \\ & (1.200) \end{aligned}$ | $\begin{gathered} 0.009 \\ (0.001) \end{gathered}$ | $\begin{aligned} & 70.654 \\ & (4.346) \end{aligned}$ | $\begin{gathered} 0.041 \\ (0.003) \end{gathered}$ | $\begin{aligned} & 3732.684 \\ & (244.717) \end{aligned}$ | $\begin{gathered} 2231.432 \\ (303.201) \end{gathered}$ | $\begin{gathered} 3.094 \\ (0.195) \end{gathered}$ |
|  | 5 | $\begin{gathered} 11.826 \\ (0.326) \end{gathered}$ | $\begin{gathered} 0.007 \\ (0.002) \end{gathered}$ | $\begin{gathered} 83.788 \\ (16.826) \end{gathered}$ | $\begin{gathered} 0.047 \\ (0.006) \end{gathered}$ | $\begin{aligned} & 1823.192 \\ & (496.826) \end{aligned}$ | $\begin{aligned} & 2170.859 \\ & (680.876) \end{aligned}$ | $\begin{gathered} 2.555 \\ (0.289) \end{gathered}$ |
|  | 6 | $\begin{aligned} & 16.612 \\ & (1.024) \end{aligned}$ | $\begin{gathered} 0.008 \\ (0.001) \end{gathered}$ | $\begin{aligned} & 57.034 \\ & (4.352) \end{aligned}$ | $\begin{gathered} 0.051 \\ (0.002) \end{gathered}$ | $\begin{aligned} & 1918.062 \\ & (101.953) \end{aligned}$ | $\begin{aligned} & 1288.435 \\ & (128.088) \end{aligned}$ | $\begin{gathered} 2.592 \\ (0.133) \end{gathered}$ |
|  | 7 | $\begin{aligned} & 21.876 \\ & (1.908) \end{aligned}$ | $\begin{gathered} 0.009 \\ (0.001) \end{gathered}$ | $\begin{gathered} 76.457 \\ (12.497) \end{gathered}$ | $\begin{gathered} 0.047 \\ (0.004) \end{gathered}$ | $\begin{aligned} & 2497.105 \\ & (304.448) \end{aligned}$ | $\begin{aligned} & 2037.871 \\ & (552.711) \end{aligned}$ | $\begin{gathered} 2.941 \\ (0.135) \end{gathered}$ |
|  | 8 | $\begin{aligned} & 28.438 \\ & (2.582) \end{aligned}$ | $\begin{gathered} 0.009 \\ (0.001) \end{gathered}$ | $\begin{gathered} 102.998 \\ (16.235) \end{gathered}$ | $\begin{gathered} 0.043 \\ (0.003) \end{gathered}$ | $\begin{aligned} & 3371.620 \\ & (360.208) \end{aligned}$ | $\begin{aligned} & 3122.584 \\ & (705.069) \end{aligned}$ | $\begin{gathered} 3.152 \\ (0.080) \end{gathered}$ |
| 4 | 1 | $\begin{gathered} 13.37 \\ (0.812) \end{gathered}$ | $\begin{gathered} 0.004 \\ (0.001) \end{gathered}$ | $\begin{aligned} & 46.163 \\ & (4.218) \end{aligned}$ | $\begin{gathered} 0.033 \\ (0.002) \end{gathered}$ | $\begin{gathered} 3043.1 \\ (561.968) \end{gathered}$ | $\begin{aligned} & 1843.852 \\ & (256.979) \end{aligned}$ | $\begin{gathered} 2.125 \\ (0.124) \end{gathered}$ |
|  | 2 | $\begin{gathered} 18.945 \\ (0.937) \end{gathered}$ | $\begin{gathered} 0.004 \\ (0.001) \end{gathered}$ | $\begin{aligned} & 60.008 \\ & (3.119) \end{aligned}$ | $\begin{gathered} 0.029 \\ (0.003) \end{gathered}$ | $\begin{gathered} 4413.816 \\ (1026.233) \end{gathered}$ | $\begin{gathered} 2954.634 \\ (378.426) \end{gathered}$ | $\begin{gathered} 2.374 \\ (0.190) \end{gathered}$ |
|  | 3 | $\begin{aligned} & 26.204 \\ & (1.295) \end{aligned}$ | $\begin{gathered} 0.006 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 74.364 \\ & (7.246) \end{aligned}$ | $\begin{gathered} 0.032 \\ (0.001) \end{gathered}$ | $\begin{aligned} & 4639.299 \\ & (358.633) \end{aligned}$ | $\begin{aligned} & 3314.515 \\ & (491.334) \end{aligned}$ | $\begin{gathered} 2.755 \\ (0.218) \end{gathered}$ |
|  | 4 | $\begin{aligned} & 29.719 \\ & (3.165) \end{aligned}$ | $\begin{gathered} 0.006 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 90.660 \\ & (9.644) \end{aligned}$ | $\begin{gathered} 0.030 \\ (0.003) \end{gathered}$ | $\begin{aligned} & 4959.301 \\ & (525.967) \end{aligned}$ | $\begin{aligned} & 4388.854 \\ & (874.266) \end{aligned}$ | $\begin{gathered} 2.966 \\ (0.212) \end{gathered}$ |
|  | 5 | $\begin{aligned} & 11.040 \\ & (1.175) \end{aligned}$ | $\begin{gathered} 0.005 \\ (0.001) \end{gathered}$ | $\begin{gathered} 68.385 \\ (10.688) \end{gathered}$ | $\begin{gathered} 0.040 \\ (0.004) \end{gathered}$ | $\begin{aligned} & 2395.213 \\ & (624.399) \end{aligned}$ | $\begin{aligned} & 2078.785 \\ & (484.826) \end{aligned}$ | $\begin{gathered} 2.234 \\ (0.158) \end{gathered}$ |
|  | 6 | $\begin{gathered} 15.040 \\ (0.695) \end{gathered}$ | $\begin{gathered} 0.004 \\ (0.001) \end{gathered}$ | $\begin{gathered} 75.603 \\ (16.962) \end{gathered}$ | $\begin{gathered} 0.035 \\ (0.003) \end{gathered}$ | $\begin{gathered} 4278.042 \\ (1101.549) \end{gathered}$ | $\begin{aligned} & 2571.014 \\ & (909.669) \end{aligned}$ | $\begin{gathered} 2.358 \\ (0.131) \end{gathered}$ |
|  | . 7 | $\begin{aligned} & 22.110 \\ & (2.365) \end{aligned}$ | $\begin{gathered} 0.006 \\ (0.002) \end{gathered}$ | $\begin{gathered} 89.865 \\ (11.501) \end{gathered}$ | $\begin{gathered} 0.037 \\ (0.003) \end{gathered}$ | $\begin{gathered} 4137.515 \\ (1819.490) \end{gathered}$ | $\begin{aligned} & 2919.104 \\ & (507.702) \end{aligned}$ | $\begin{gathered} 2.580 \\ (0.146) \end{gathered}$ |
|  | 8 | $\begin{array}{\|l} 31.039 \\ (0.793) \\ \hline \end{array}$ | $\begin{gathered} 0.008 \\ (0.000) \\ \hline \end{gathered}$ | $\begin{array}{r} 103.400 \\ (12.298) \\ \hline \end{array}$ | $\begin{gathered} 0.040 \\ (0.002) \end{gathered}$ | $\begin{array}{r} 4241.440 \\ (241.054) \\ \hline \end{array}$ | $\begin{array}{r} 3287.660 \\ (589.216) \\ \hline \end{array}$ | $\begin{gathered} 2.888 \\ (0.073) \\ \hline \end{gathered}$ |

Table 15. (Continued).

| Subj | Cond | F1 | T1 | F2 | T2 | LrateF1 | LrateF2 | Imp 100 ms |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5 | 1 | $\begin{array}{\|l} \hline 14.562 \\ (1.239) \end{array}$ | $\begin{gathered} 0.005 \\ (0.002) \end{gathered}$ | $\begin{aligned} & 65.036 \\ & (4.817) \end{aligned}$ | $\begin{gathered} 0.034 \\ (0.006) \end{gathered}$ | $\begin{gathered} 3945.385 \\ (3060.731) \end{gathered}$ | $\begin{aligned} & 2648.734 \\ & (582.603) \end{aligned}$ | $\begin{gathered} 2.897 \\ (0.177) \end{gathered}$ |
|  | 2 | $\begin{aligned} & 22.962 \\ & (3.005) \end{aligned}$ | $\begin{gathered} 0.005 \\ (0.002) \end{gathered}$ | $\begin{gathered} 76.882 \\ (10.574) \end{gathered}$ | $\begin{gathered} 0.035 \\ (0.006) \end{gathered}$ | $\begin{gathered} 4860.787 \\ (1752.020) \end{gathered}$ | $\begin{aligned} & 3350.633 \\ & (861.154) \end{aligned}$ | $\begin{gathered} 2.849 \\ (0.303) \end{gathered}$ |
|  | 3 | $\begin{aligned} & 30.806 \\ & (2.006) \end{aligned}$ | $\begin{gathered} 0.009 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 66.878 \\ & (5.234) \end{aligned}$ | $\begin{gathered} 0.045 \\ (0.003) \end{gathered}$ | $\begin{aligned} & 3301.938 \\ & (203.254) \end{aligned}$ | $\begin{aligned} & 1858.342 \\ & (217.557) \end{aligned}$ | $\begin{gathered} 3.049 \\ (0.088) \end{gathered}$ |
|  | 4 | $\begin{aligned} & 41.404 \\ & (2.912) \end{aligned}$ | $\begin{gathered} 0.008 \\ (0.001) \end{gathered}$ | $\begin{gathered} 94.274 \\ (11.798) \end{gathered}$ | $\begin{gathered} 0.040 \\ (0.004) \end{gathered}$ | $\begin{aligned} & 5017.981 \\ & (492.084) \end{aligned}$ | $\begin{aligned} & 3157.898 \\ & (772.834) \end{aligned}$ | $\begin{gathered} 3.620 \\ (0.299) \end{gathered}$ |
|  | 5 | $\begin{gathered} 12.800 \\ (1.993) \end{gathered}$ | $\begin{gathered} 0.005 \\ (0.003) \end{gathered}$ | $\begin{gathered} 78.248 \\ (26.315) \end{gathered}$ | $\begin{gathered} 0.047 \\ (0.006) \end{gathered}$ | $\begin{gathered} 3247.035 \\ (2128.701) \end{gathered}$ | $\begin{aligned} & 1887.616 \\ & (858.754) \end{aligned}$ | $\begin{gathered} 2.551 \\ (0.108) \end{gathered}$ |
|  | 6 | $\begin{aligned} & 17.633 \\ & (1.993) \end{aligned}$ | $\begin{gathered} 0.005 \\ (0.002) \end{gathered}$ | $\begin{aligned} & 109.725 \\ & (16.681) \end{aligned}$ | $\begin{gathered} 0.038 \\ (0.004) \end{gathered}$ | $\begin{gathered} 4221.010 \\ (2170.789) \end{gathered}$ | $\begin{aligned} & 3380.844 \\ & (871.950) \end{aligned}$ | $\begin{gathered} 2.788 \\ (0.332) \end{gathered}$ |
|  | 7 | $\begin{aligned} & 24.744 \\ & (1.234) \end{aligned}$ | $\begin{gathered} 0.007 \\ (0.001) \end{gathered}$ | $\begin{aligned} & 117.570 \\ & (24.434) \end{aligned}$ | $\begin{gathered} 0.038 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 3544.255 \\ & (252.293) \end{aligned}$ | $\begin{aligned} & 3835.116 \\ & (961.056) \end{aligned}$ | $\begin{gathered} 3.058 \\ (0.185) \end{gathered}$ |
|  | 8 | $\begin{aligned} & 30.113 \\ & (1.629) \end{aligned}$ | $\begin{gathered} 0.007 \\ (0.001) \end{gathered}$ | $\begin{aligned} & 142.469 \\ & (43.967) \end{aligned}$ | $\begin{gathered} 0.034 \\ (0.003) \end{gathered}$ | $\begin{aligned} & 4671.611 \\ & (527.599) \end{aligned}$ | $\begin{gathered} 5284.112 \\ (2371.338) \end{gathered}$ | $\begin{gathered} 3.259 \\ (0.239) \end{gathered}$ |
| 6 | 1 | $\begin{aligned} & 11.663 \\ & (1.802) \end{aligned}$ | $\begin{gathered} 0.005 \\ (0.002) \end{gathered}$ | $\begin{aligned} & 45.111 \\ & (5.972) \end{aligned}$ | $\begin{gathered} 0.034 \\ (0.005) \end{gathered}$ | $\begin{aligned} & 2586.656 \\ & (713.660) \end{aligned}$ | $\begin{aligned} & 1722.246 \\ & (379.658) \end{aligned}$ | $\begin{gathered} 2.010 \\ (0.307) \end{gathered}$ |
|  | 2 | $\begin{aligned} & 16.030 \\ & (1.033) \end{aligned}$ | $\begin{gathered} 0.007 \\ (0.001) \end{gathered}$ | $\begin{aligned} & 47.471 \\ & (3.256) \end{aligned}$ | $\begin{gathered} 0.035 \\ (0.002) \end{gathered}$ | $\begin{aligned} & 2477.842 \\ & (498.935) \end{aligned}$ | $\begin{aligned} & 1744.926 \\ & (162.674) \end{aligned}$ | $\begin{gathered} 2.132 \\ (0.168) \end{gathered}$ |
|  | 3 | $\begin{aligned} & 20.365 \\ & (1.122) \end{aligned}$ | $\begin{gathered} 0.005 \\ (0.000) \end{gathered}$ | $\begin{gathered} 63.254 \\ (2.590) \end{gathered}$ | $\begin{gathered} 0.028 \\ (0.002) \end{gathered}$ | $\begin{aligned} & 3953.572 \\ & (300.540) \end{aligned}$ | $\begin{aligned} & 3004.724 \\ & (258.031) \end{aligned}$ | $\begin{gathered} 2.453 \\ (0.082) \end{gathered}$ |
|  | 4 | $\begin{aligned} & 24.515 \\ & (2.844) \end{aligned}$ | $\begin{gathered} 0.006 \\ (0.001) \end{gathered}$ | $\begin{aligned} & 71.292 \\ & (5.983) \end{aligned}$ | $\begin{gathered} 0.027 \\ (0.003) \end{gathered}$ | $\begin{aligned} & 4533.446 \\ & (854.673) \end{aligned}$ | $\begin{aligned} & 3707.704 \\ & (445.048) \end{aligned}$ | $\begin{gathered} 2.670 \\ (0.214) \end{gathered}$ |
|  | 5 | $\begin{gathered} 9.751 \\ (1.005) \end{gathered}$ | $\begin{gathered} 0.003 \\ (0.001) \end{gathered}$ | $\begin{gathered} 66.401 \\ (21.102) \end{gathered}$ | $\begin{gathered} 0.037 \\ (0.004) \end{gathered}$ | $\begin{gathered} 4479.308 \\ (1340.487) \end{gathered}$ | $\begin{aligned} & 2051.657 \\ & (785.300) \end{aligned}$ | $\begin{gathered} 1.920 \\ (0.267) \end{gathered}$ |
|  | 6 | $\begin{aligned} & 17.248 \\ & (2.525) \end{aligned}$ | $\begin{gathered} 0.003 \\ (0.000) \end{gathered}$ | $\begin{gathered} 79.330 \\ (15.824) \end{gathered}$ | $\begin{gathered} 0.037 \\ (0.003) \end{gathered}$ | $\begin{gathered} 6908.570 \\ (2362.890) \end{gathered}$ | $\begin{aligned} & 2391.694 \\ & (640.695) \end{aligned}$ | $\begin{gathered} 2.070 \\ (0.207) \end{gathered}$ |
|  | 7 | $\begin{aligned} & 24.222 \\ & (1.262) \end{aligned}$ | $\begin{gathered} 0.003 \\ (0.001) \end{gathered}$ | $\begin{aligned} & 86.874 \\ & (9.992) \end{aligned}$ | $\begin{gathered} 0.036 \\ (0.003) \end{gathered}$ | $\begin{array}{r} 11729.940 \\ (3692.451) \end{array}$ | $\begin{aligned} & 2655.882 \\ & (454.028) \end{aligned}$ | $\begin{gathered} 2.159 \\ (0.285) \end{gathered}$ |
|  | 8 | $\begin{array}{r} 27.184 \\ (2.444) \\ \hline \end{array}$ | $\begin{gathered} 0.003 \\ (0.000) \\ \hline \end{gathered}$ | $\begin{gathered} 91.132 \\ (24.307) \\ \hline \end{gathered}$ | $\begin{gathered} 0.034 \\ (0.003) \\ \hline \end{gathered}$ | $\begin{array}{r} 11550.483 \\ (3837.962) \\ \hline \end{array}$ | $\begin{gathered} 3195.038 \\ (1160.427) \\ \hline \end{gathered}$ | $\begin{gathered} 2.413 \\ (0.080) \\ \hline \end{gathered}$ |

Table 15. (Continued).

| Subj Cond |  | F1 | T1 | F2 | T2 | LrateF1 | LrateF2 | Impl00ms |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7 | 1 | $\begin{array}{\|c\|} \hline 15.307 \\ (1.843) \end{array}$ | $\begin{gathered} \hline 0.014 \\ (0.001) \end{gathered}$ | $\begin{aligned} & 41.901 \\ & (7.159) \end{aligned}$ | $\begin{gathered} 0.068 \\ (0.007) \end{gathered}$ | $\begin{aligned} & 1109.878 \\ & (160.203) \end{aligned}$ | $\begin{gathered} 691.569 \\ (219.679) \end{gathered}$ | $\begin{gathered} 2.293 \\ (0.207) \end{gathered}$ |
|  | 2 | $\begin{aligned} & 19.020 \\ & (1.824) \end{aligned}$ | $\begin{gathered} 0.013 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 37.567 \\ & (8.174) \end{aligned}$ | $\begin{gathered} 0.076 \\ (0.010) \end{gathered}$ | $\begin{aligned} & 1408.890 \\ & (131.655) \end{aligned}$ | $\begin{gathered} 499.472 \\ (291.522) \end{gathered}$ | $\begin{gathered} 2.369 \\ (0.201) \end{gathered}$ |
|  | 3 | $\begin{aligned} & 28.075 \\ & (7.126) \end{aligned}$ | $\begin{gathered} 0.013 \\ (0.001) \end{gathered}$ | $\begin{aligned} & 43.882 \\ & (9.033) \end{aligned}$ | $\begin{gathered} 0.062 \\ (0.010) \end{gathered}$ | $\begin{aligned} & 2055.335 \\ & (522.697) \end{aligned}$ | $\begin{gathered} 781.966 \\ (394.273) \end{gathered}$ | $\begin{gathered} 2.680 \\ (0.236) \end{gathered}$ |
|  | 4 | $\begin{aligned} & 35.312 \\ & (1.370) \end{aligned}$ | $\begin{gathered} 0.012 \\ (0.001) \end{gathered}$ | $\begin{aligned} & 47.606 \\ & (6.391) \end{aligned}$ | $\begin{gathered} 0.053 \\ (0.004) \end{gathered}$ | $\begin{aligned} & 2895.718 \\ & (382.013) \end{aligned}$ | $\begin{aligned} & 1010.950 \\ & (312.622) \end{aligned}$ | $\begin{gathered} 2.696 \\ (0.143) \end{gathered}$ |
|  | 5 | $\begin{aligned} & 11.707 \\ & (2.891) \end{aligned}$ | $\begin{gathered} 0.018 \\ (0.003) \end{gathered}$ | $\begin{gathered} 34.278 \\ (15.119) \end{gathered}$ | $\begin{gathered} 0.076 \\ (0.007) \end{gathered}$ | $\begin{gathered} 671.358 \\ (179.650) \end{gathered}$ | $\begin{gathered} 445.292 \\ (248.799) \end{gathered}$ | $\begin{gathered} 1.984 \\ (0.371) \end{gathered}$ |
|  | 6 | $\begin{array}{\|l} 19.368 \\ (2.692) \end{array}$ | $\begin{gathered} 0.013 \\ (0.001) \end{gathered}$ | $\begin{gathered} 49.276 \\ (17.247) \end{gathered}$ | $\begin{gathered} 0.065 \\ (0.009) \end{gathered}$ | $\begin{aligned} & 1525.884 \\ & (262.909) \end{aligned}$ | $\begin{gathered} 835.132 \\ (536.589) \end{gathered}$ | $\begin{gathered} 2.479 \\ (0.109) \end{gathered}$ |
|  | 7 | $\begin{aligned} & 23.666 \\ & (2.639) \end{aligned}$ | $\begin{gathered} 0.012 \\ (0.002) \end{gathered}$ | $\begin{gathered} 41.515 \\ (11.007) \end{gathered}$ | $\begin{gathered} 0.063 \\ (0.009) \end{gathered}$ | $\begin{array}{r} 1994.662 \\ (176.021) \end{array}$ | $\begin{gathered} 674.427 \\ (319.665) \end{gathered}$ | $\begin{gathered} 2.353 \\ (0.143) \end{gathered}$ |
|  | 8 | $\begin{aligned} & 32.609 \\ & (3.983) \end{aligned}$ | $\begin{gathered} 0.011 \\ (0.001) \end{gathered}$ | $\begin{gathered} 46.573 \\ (23.282) \end{gathered}$ | $\begin{gathered} 0.054 \\ (0.009) \end{gathered}$ | $\begin{aligned} & 2978.313 \\ & (351.086) \end{aligned}$ | $\begin{gathered} 929.230 \\ (731.633) \end{gathered}$ | $\begin{gathered} 2.481 \\ (0.227) \end{gathered}$ |
| 8 | 1 | $\begin{array}{\|l} 18.087 \\ (1.904) \end{array}$ | $\begin{gathered} 0.009 \\ (0.001) \end{gathered}$ | $\begin{aligned} & 57.483 \\ & (8.113) \end{aligned}$ | $\begin{gathered} 0.046 \\ (0.006) \end{gathered}$ | $\begin{aligned} & 1915.375 \\ & (271.563) \end{aligned}$ | $\begin{aligned} & 1598.794 \\ & (624.209) \end{aligned}$ | $\begin{gathered} 2.419 \\ (0.149) \end{gathered}$ |
|  | 2 | $\begin{aligned} & 26.983 \\ & (2.516) \end{aligned}$ | $\begin{gathered} 0.009 \\ (0.001) \end{gathered}$ | $\begin{aligned} & 46.366 \\ & (7.572) \end{aligned}$ | $\begin{gathered} 0.048 \\ (0.002) \end{gathered}$ | $\begin{aligned} & 2860.967 \\ & (403.270) \end{aligned}$ | $\begin{gathered} 971.276 \\ (309.023) \end{gathered}$ | $\begin{gathered} 2.498 \\ (0.124) \end{gathered}$ |
|  | 3 | $\begin{aligned} & 38.655 \\ & (2.362) \end{aligned}$ | $\begin{gathered} 0.010 \\ (0.001) \end{gathered}$ | $\begin{gathered} 62.989 \\ (14.475) \end{gathered}$ | $\begin{gathered} 0.045 \\ (0.004) \end{gathered}$ | $\begin{aligned} & 3943.224 \\ & (316.405) \end{aligned}$ | $\begin{gathered} 1568.769 \\ (657.310) \end{gathered}$ | $\begin{gathered} 2.955 \\ (0.148) \end{gathered}$ |
|  | 4 | $\begin{aligned} & 47.447 \\ & (1.922) \end{aligned}$ | $\begin{gathered} 0.010 \\ (0.001) \end{gathered}$ | $\begin{gathered} 64.744 \\ (10.880) \end{gathered}$ | $\begin{gathered} 0.043 \\ (0.004) \end{gathered}$ | $\begin{aligned} & 4884.911 \\ & (636.899) \end{aligned}$ | $\begin{aligned} & 1694.861 \\ & (539.250) \end{aligned}$ | $\begin{gathered} 3.060 \\ (0.123) \end{gathered}$ |
|  | 5 | $\begin{gathered} 18.117 \\ (1.680) \end{gathered}$ | $\begin{gathered} 0.008 \\ (0.002) \end{gathered}$ | $\begin{gathered} 42.601 \\ (11.736) \end{gathered}$ | $\begin{gathered} 0.053 \\ (0.010) \end{gathered}$ | $\begin{aligned} & 2373.732 \\ & (366.812) \end{aligned}$ | $\begin{gathered} 859.657 \\ (359.883) \end{gathered}$ | $\begin{gathered} 2.072 \\ (0.080) \end{gathered}$ |
|  | 6 | $\begin{aligned} & 24.643 \\ & (2.090) \end{aligned}$ | $\begin{gathered} 0.007 \\ (0.001) \end{gathered}$ | $\begin{gathered} 60.529 \\ (17.661) \end{gathered}$ | $\begin{gathered} 0.048 \\ (0.007) \end{gathered}$ | $\begin{aligned} & 3587.370 \\ & (867.007) \end{aligned}$ | $\begin{aligned} & 1520.868 \\ & (726.567) \end{aligned}$ | $\begin{gathered} 2.375 \\ (0.142) \end{gathered}$ |
|  | 7 | $\begin{array}{\|l} 32.564 \\ (4.090) \end{array}$ | $\begin{gathered} 0.007 \\ (0.002) \end{gathered}$ | $\begin{aligned} & 48.962 \\ & (9.898) \end{aligned}$ | $\begin{gathered} 0.045 \\ (0.003) \end{gathered}$ | $\begin{gathered} 4932.338 \\ (2051.122) \end{gathered}$ | $\begin{aligned} & 1130.369 \\ & (217.343) \end{aligned}$ | $\begin{gathered} 2.757 \\ (0.147) \end{gathered}$ |
|  | 8 | $\begin{array}{r} 41.145 \\ (5.655) \\ \hline \end{array}$ | $\begin{gathered} 0.007 \\ (0.001) \end{gathered}$ | $\begin{gathered} 68.975 \\ (24.834) \end{gathered}$ | $\begin{gathered} 0.047 \\ (0.006) \end{gathered}$ | $\begin{gathered} 5943.835 \\ (1075.417) \end{gathered}$ | $\begin{array}{r} 1806.626 \\ (951.399) \end{array}$ | $\begin{gathered} 2.886 \\ (0.103) \end{gathered}$ |

Table 15. (Continued).

| Subj Cond |  | F1 | T1 | F2 | T2 | LrateF1 | LrateF2 | Imp 100 ms |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 9 | 1 | 0.000 | 0.000 | 71.288 | 0.018 | 0.000 | 4042.692 | 2.948 |
|  |  | (0.000) | (0.000) | (4.629) | (0.005) | (0.000) | (962.541) | (0.182) |
|  | 2 | 19.164 | 0.008 | 78.063 | 0.039 | 2417.948 | 2777.770 | 3.367 |
|  |  | (1.171) | (0.001) | (6.107) | (0.002) | (209.164) | (395.065) | (0.230) |
|  | 3 | 27.707 | 0.008 | 81.600 | 0.038 | 3746.693 | 2918.404 | 3.623 |
|  |  | (1.616) | (0.001) | (10.735) | (0.000) | (600.696) | (468.009) | (0.369) |
|  | 4 | 34.895 | 0.008 | 108.610 | 0.036 | 4673.834 | 4266.028 | 4.145 |
|  |  | (0.533) | (0.000) | (7.496) | (0.002) | (346.059) | (622.202) | $(0.165)$ |
|  | 5 | 7.704 | 0.006 | 79.341 | 0.039 | 1418.502 | 2890.295 | 2.097 |
|  |  | (0.532) | (0.001) | (18.392) | (0.005) | (194.850) | (909.732) | (0.146) |
|  | 6 | 15.382 | 0.003 | 79.367 | 0.039 | 5590.590 | 2566.586 | 2.692 |
|  |  | $(1.800)$ | $(0.000)$ | $(18.312)$ | (0.005) | (1329.696) | (968.098) | (0.112) |
|  | 7 | 21.913 | 0.005 | 67.997 | 0.043 | 4795.974 | 1853.689 | 3.088 |
|  |  | (2.735) | (0.001) | (12.353) | (0.003) | (947.578) | (458.033) | (0.252) |
|  | 8 | 27.745 | 0.003 | 93.808 | 0.037 | 7731.527 | 2989.882 | 3.391 |
|  |  | (4.059) | (0.001) | (26.252) | (0.001) | (1842.901) | (1028.213) | (0.198) |
| 10 | 1 |  | 0.011 |  | 0.0 | 1402.322 | 902.399 | 2.391 |
|  |  | (0.892) | (0.002) | (4.545) | (0.004) | (262.201) | (228.746) | (0.180) |
|  | 2 | 25.144 | 0.013 | 55.261 | 0.053 | 1988.238 | 1167.860 | 3.087 |
|  |  | (1.143) | (0.000) | (14.374) | (0.004) | (108.515) | (508.307) | (0.411) |
|  | 3 | 30.957 | 0.012 | 60.824 | 0.047 | 2583.175 | 1469.694 | 3.237 |
|  |  | (2.398) | (0.001) | (7.330) | (0.002) | (184.627) | (331.738) | (0.363) |
|  | 4 | 36.044 | 0.012 | 59.150 | 0.047 | 3081.058 | 1379.921 | 3.238 |
|  |  | $(0.697)$ | (0.001) | (3.793) | (0.004) | (386.999) | (164.557) | $(0.111)$ |
|  | 5 | 18.620 | 0.009 | 48.500 | 0.059 | 2126.267 | 799.596 | 2.695 |
|  |  | (0.530) | (0.001) | (4.410) | (0.005) | (220.703) | (149.638) | $(0.144)$ |
|  | 6 | 27.200 | 0.010 | 51.703 | 0.058 | 2659.117 | 842.706 | 3.121 |
|  |  | (1.081) | $(0.001)$ | (11.548) | (0.006) | (324.828) | (302.109) | (0.298) |
|  | 7 | 34.146 | 0.010 | 58.016 | 0.058 | 3421.858 | 893.098 | 3.417 |
|  |  | (1.739) | (0.001) | (5.772) | (0.002) | (227.472) | (180.576) | (0.135) |
|  | 8 | 41.501 | 0.009 | 66.597 | 0.053 | 4590.208 | 1273.276 | 3.559 |
|  |  | (2.558) | (0.001) | (17.501) | (0.006) | (733.097) | (573.207) | (0.195) |

Note: Force unit is in $\mathrm{N} / \mathrm{kg}$ and time unit is in s .

Standard deviation values are in parenthesis.
The definitions of variables are in Appendix A.

Table 16. Subject means and standard deviations of VGRF variables (Group 2).

| Subj Cond |  | F1 | T1 | F2 | T2 | LrateF1 | LrateF2 | $\frac{\operatorname{Imp} 100 \mathrm{~ms}}{2.650}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 |  | - | 64.951 | 0.017 | - | $3574.580$ |  |
|  |  |  |  | (7.300) | (0.004) |  | (900.658) | (0.133) |
|  | 2 | - | - | 79.137 | 0.025 | - | 3223.487 | 2.826 |
|  |  |  |  | (6.139) | (0.006) |  | (783.105) | (0.124) |
|  | 3 | - | - | 99.651 | 0.026 | - | 3856.677 | 2.996 |
|  |  |  |  | (11.195) | $(0.002)$ |  | (649.984) | (0.204) |
|  | 4 | - | - | 114.337 | 0.024 | - | 4728.326 | 3.235 |
|  |  |  |  | (12.455) | (0.003) |  | (879.176) | (0.157) |
|  | 5 | - | - | 82.997 | . 0.034 | -. | 2427.334 | 2.141 |
|  |  |  |  | $(13.681)$ | $(0.005)$ |  | (664.898) | $(0.070)$ |
|  | 6 | - | - | 91.006 | 0.038 | - | 2403.052 | 2.656 |
|  |  |  |  | (14.172) | (0.004) |  | (550.052) | (0.288) |
|  | 7 | - | - | 124.216 | 0.035 | - | 3671.220 | 2.904 |
|  |  |  |  | $(31.324)$ | $(0.005)$ |  | (1351.040) | $(0.166)$ |
|  | 8 | - | - | 113.656 | 0.027 | - | 9054.827 | 3.094 |
|  |  |  |  | (40.701) | (0.014) |  | (11560.677) | (0.131) |
| 2 | 1 | - | ${ }^{\circ}$ | 85.584 | 0.018 | - | 4674.473 | 3.230 |
|  |  |  |  | (6.012) | (0.002) |  | (295.120) | (0.131) |
|  | 2 | - | - | 98.984 | 0.017 | - | 5843.073 | 3.021 |
|  |  |  |  | (8.605) | (0.002) |  | (1216.387) | (0.193) |
|  | 3 | - | - | 126.379 | 0.017 | - | 8109.881 | 3.648 |
|  |  |  |  | (5.915) | $(0.006)$ |  | (2658.625) | (0.275) |
| 4 |  | - | - | 121.316 | 0.023 | - | 5826.274 | 3.389 |
|  |  | (13.845) |  | (0.008) | (2304.413) |  | $(0.221)$ |  |
| 5 |  |  | - | - | 111.165 | 0.011 | - | 10017.021 | 3.111 |
|  |  | (4.825) |  |  | $(0.002)$ | (1632.941) |  | (0.284) |
| 6 |  | - | - | 129.995 | 0.021 | - | 6169.147 | 2.945 |
|  |  | $(0.000)$ |  | $(0.002)$ | (692.029) |  | (0.319) |  |
| 7 |  |  | - | $-$ | 129.995 | 0.028 | - | 4840.354 | 3.015 |
|  |  | (0.000) |  |  | $(0.006)$ | (1110.457) |  | (0.281) |
| 8 |  | - | - | 129.259 | 0.026 | - | 5091.495 | 3.143 |
|  |  | (1.646) |  | (0.006) | (1093.276) |  | (0.070) |  |

Table 16. (Continued).

| Subj Cond |  | F1 | T1 | F2 | T2 | LrateF1 | LrateF2 | Imp 100ms |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | 1 | - | - | 61.319 | 0.019 | - | 3239.655 | 2.666 |
|  |  |  |  | (13.054) | (0.006) |  | (1032.743) | (0.464) |
|  | 2 | - | - | 70.519 | 0.020 | - | 4088.330 | 2.291 |
|  |  |  |  | (17.190) | (0.008) |  | (2118.153) | (0.509) |
|  | 3 | - | - | 78.344 | 0.021 | - | 4331.668 | 2.423 |
|  |  |  |  | (8.724) | (0.009) |  | (2192.099) | (0.171) |
|  | 4 | - | - | 86.988 | 0.029 | - | 3058.721 | 2.721 |
|  |  |  |  | (11.291) | $(0.004)$ |  | (668.868) | $(0.201)$ |
|  | 5 | - | - | 101.204 | 0.024 | - | 5614.674 | 2.783 |
|  |  |  |  | (12.520) | (0.012) |  | (3663.238) | (0.557) |
|  | 6 | - | - | 99.186 | 0.031 | - | 3202.253 | 1.954 |
|  |  |  |  | (17.269) | (0.003) |  | (875.424) | (0.169) |
|  | 7 | - | - | 113.739 | 0.031 | - | 3679.241 | 2.284 |
|  |  |  |  | (10.251) | (0.003) |  | (531.847) | (0.084) |
|  | 8 | - | - | 116.255 | 0.030 | - | 4278.815 | 2.431 |
|  |  |  |  | (23.642) | (0.008) |  | (2264.801) | (0.179) |

Note: Force unit is in $\mathrm{N} / \mathrm{kg}$ and time unit is in s .
Loading rate unit is in $\mathrm{N} / \mathrm{kg} / \mathrm{s}$ and Impulse unit is in ( $\mathrm{N} / \mathrm{kg}$ ) $\cdot \mathrm{s}$.
Standard deviation values are in parenthesis.
The definitions of variables are in Appendix A.

- indicates no value present.


## APPENDIX E

## ACCELERATION DATA

Table 17. Subject means and standard deviations of acceleration variables (Group 1).


Table 17. (Continued).

| Subj | Cond | Acchead | Tacchead | AccTibial TaccTibial AccTibia2 TaccTibia2 |  |  |  | AtteIndex |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | 1 | $\begin{gathered} \hline 3.992 \\ (0.912) \end{gathered}$ | $\begin{gathered} \hline 0.051 \\ (0.012) \end{gathered}$ | $\begin{gathered} 20.544 \\ (11.362) \end{gathered}$ | $\begin{gathered} \hline 0.014 \\ (0.003) \end{gathered}$ | $\begin{aligned} & 14.238 \\ & (5.560) \end{aligned}$ | $\begin{gathered} 0.049 \\ (0.004) \end{gathered}$ | $\begin{gathered} 60.701 \\ (39.465) \end{gathered}$ |
|  | 2 | $\begin{gathered} 5.296 \\ (0.641) \end{gathered}$ | $\begin{gathered} 0.052 \\ (0.001) \end{gathered}$ | $\begin{aligned} & 23.183 \\ & (1.908) \end{aligned}$ | $\begin{gathered} 0.013 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 39.829 \\ & (7.094) \end{aligned}$ | $\begin{gathered} 0.046 \\ (0.002) \end{gathered}$ | $\begin{aligned} & 86.441 \\ & (2.289) \end{aligned}$ |
|  | 3 | $\begin{gathered} 4.770 \\ (0.925) \end{gathered}$ | $\begin{gathered} 0.044 \\ (0.010) \end{gathered}$ | $\begin{aligned} & 33.776 \\ & (7.754) \end{aligned}$ | $\begin{gathered} 0.015 \\ (0.002) \end{gathered}$ | $\begin{aligned} & 34.079 \\ & (8.903) \end{aligned}$ | $\begin{gathered} 0.047 \\ (0.004) \end{gathered}$ | $\begin{aligned} & 85.703 \\ & (1.795) \end{aligned}$ |
|  | 4 | $\begin{gathered} 4.303 \\ (0.531) \end{gathered}$ | $\begin{gathered} 0.044 \\ (0.009) \end{gathered}$ | $\begin{aligned} & 40.048 \\ & (3.245) \end{aligned}$ | $\begin{gathered} 0.015 \\ (0.001) \end{gathered}$ | $\begin{aligned} & 44.840 \\ & (7.321) \end{aligned}$ | $\begin{gathered} 0.046 \\ (0.002) \end{gathered}$ | $\begin{aligned} & 90.299 \\ & (1.051) \end{aligned}$ |
|  | 5 | $\begin{gathered} 3.577 \\ (0.764) \end{gathered}$ | $\begin{gathered} 0.059 \\ (0.005) \end{gathered}$ | $\begin{aligned} & 11.178 \\ & (0.765) \end{aligned}$ | $\begin{gathered} 0.011 \\ (0.002) \end{gathered}$ | $\begin{gathered} 42.856 \\ (14.731) \end{gathered}$ | $\begin{gathered} 0.053 \\ (0.006) \end{gathered}$ | $\begin{aligned} & 91.106 \\ & (2.155) \end{aligned}$ |
|  | 6 | $\begin{gathered} 2.081 \\ (0.285) \end{gathered}$ | $\begin{gathered} 0.051 \\ (0.014) \end{gathered}$ | $\begin{gathered} 13.700 \\ (0.676) \end{gathered}$ | $\begin{gathered} 0.013 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 26.008 \\ & (2.597) \end{aligned}$ | $\begin{gathered} 0.057 \\ (0.002) \end{gathered}$ | $\begin{aligned} & 91.909 \\ & (1.526) \end{aligned}$ |
|  | 7 | $\begin{gathered} 2.748 \\ (0.259) \end{gathered}$ | $\begin{gathered} 0.039 \\ (0.004) \end{gathered}$ | $\begin{aligned} & 17.736 \\ & (1.409) \end{aligned}$ | $\begin{gathered} 0.013 \\ (0.001) \end{gathered}$ | $\begin{gathered} 43.058 \\ (14.974) \end{gathered}$ | $\begin{gathered} 0.052 \\ (0.004) \end{gathered}$ | $\begin{aligned} & 92.973 \\ & (2.445) \end{aligned}$ |
|  | 8. | $\begin{gathered} 3.415 \\ (0.348) \end{gathered}$ | $\begin{gathered} 0.051 \\ (0.010) \end{gathered}$ | $\begin{aligned} & 23.587 \\ & (1.488) \end{aligned}$ | $\begin{gathered} 0.013 \\ (0.001) \end{gathered}$ | $\begin{gathered} 76.349 \\ (20.686) \end{gathered}$ | $\begin{gathered} 0.048 \\ (0.002) \end{gathered}$ | $\begin{aligned} & 95.322 \\ & (0.975) \end{aligned}$ |
| 4 | 1 | $\begin{gathered} 2.804 \\ (0.754) \end{gathered}$ | $\begin{gathered} 0.047 \\ (0.002) \end{gathered}$ | $\begin{gathered} 7.445 \\ (1.150) \end{gathered}$ | $\begin{gathered} 0.014 \\ (0.003) \end{gathered}$ | $\begin{aligned} & 25.100 \\ & (3.556) \end{aligned}$ | $\begin{gathered} 0.037 \\ (0.002) \end{gathered}$ | $\begin{aligned} & 88.780 \\ & (3.000) \end{aligned}$ |
|  | 2 | $\begin{gathered} 4.239 \\ (0.991) \end{gathered}$ | $\begin{gathered} 0.042 \\ (0.003) \end{gathered}$ | $\begin{gathered} 9.160 \\ (1.046) \end{gathered}$ | $\begin{gathered} 0.015 \\ (0.005) \end{gathered}$ | $\begin{aligned} & 33.171 \\ & (4.150) \end{aligned}$ | $\begin{gathered} 0.033 \\ (0.005) \end{gathered}$ | $\begin{aligned} & 86.980 \\ & (3.904) \end{aligned}$ |
|  | 3 | $\begin{gathered} 3.896 \\ (0.454) \end{gathered}$ | $\begin{gathered} 0.043 \\ (0.002) \end{gathered}$ | $\begin{gathered} 12.490 \\ (0.971) \end{gathered}$ | $\begin{gathered} 0.013 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 40.132 \\ & (4.368) \end{aligned}$ | $\begin{gathered} 0.035 \\ (0.002) \end{gathered}$ | $\begin{aligned} & 90.187 \\ & (1.665) \end{aligned}$ |
|  | 4 | $\begin{gathered} 4.765 \\ (0.618) \end{gathered}$ | $\begin{gathered} 0.041 \\ (0.002) \end{gathered}$ | $\begin{aligned} & 12.691 \\ & (4.229) \end{aligned}$ | $\begin{gathered} 0.014 \\ (0.003) \end{gathered}$ | $\begin{gathered} 52.138 \\ (13.267) \end{gathered}$ | $\begin{gathered} 0.033 \\ (0.004) \end{gathered}$ | $\begin{aligned} & 90.459 \\ & (2.454) \end{aligned}$ |
|  | 5 | $\begin{gathered} 2.207 \\ (0.709) \end{gathered}$ | $\begin{gathered} 0.049 \\ .(0.003) \end{gathered}$ | $\begin{gathered} 4.620 \\ (0.276) \end{gathered}$ | $\begin{gathered} 0.020 \\ (0.004) \end{gathered}$ | $\begin{gathered} 38.013 \\ (17.428) \end{gathered}$ | $\begin{gathered} 0.047 \\ (0.003) \end{gathered}$ | $\begin{aligned} & 92.307 \\ & (6.514) \end{aligned}$ |
|  | 6 | $\begin{gathered} 2.834 \\ (0.621) \end{gathered}$ | $\begin{gathered} 0.043 \\ (0.004) \end{gathered}$ | $\begin{gathered} 8.656 \\ (1.619) \end{gathered}$ | $\begin{gathered} 0.024 \\ (0.002) \end{gathered}$ | $\begin{gathered} 29.539 \\ (15.617) \end{gathered}$ | $\begin{gathered} 0.042 \\ (0.002) \end{gathered}$ | $\begin{aligned} & 87.923 \\ & (8.249) \end{aligned}$ |
|  | 7 | $\begin{gathered} 2.824 \\ (0.563) \end{gathered}$ | $\begin{gathered} 0.044 \\ (0.003) \end{gathered}$ | $\begin{aligned} & 10.876 \\ & (2.786) \end{aligned}$ | $\begin{gathered} 0.025 \\ (0.001) \end{gathered}$ | $\begin{aligned} & 58.493 \\ & (8.957) \end{aligned}$ | $\begin{gathered} 0.043 \\ (0.002) \end{gathered}$ | $\begin{aligned} & 95.069 \\ & (1.253) \end{aligned}$ |
|  | 8 | $\begin{array}{r} 2.470 \\ (0.413) \\ \hline \end{array}$ | $\begin{gathered} 0.042 \\ (0.005) \\ \hline \end{gathered}$ | $\begin{array}{r} 12.187 \\ (1.733) \end{array}$ | $\begin{gathered} 0.024 \\ (0.002) \end{gathered}$ | $\begin{gathered} 80.587 \\ (14.543) \end{gathered}$ | $\begin{gathered} 0.045 \\ (0.002) \end{gathered}$ | $\begin{aligned} & 96.878 \\ & (0.601) \\ & \hline \end{aligned}$ |

Table 17. (Continued).

| Subj | Cond | AccHead | TaccHead | AccTibia | TaccTibia | AccTibia | TaccTibia | AtteIndex |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5 | 1 | $\begin{gathered} \hline 3.134 \\ (0.713) \end{gathered}$ | $\begin{gathered} 0.043 \\ (0.004) \end{gathered}$ | $\begin{gathered} \hline 4.883 \\ (1.426) \end{gathered}$ | $\begin{gathered} 0.015 \\ (0.003) \end{gathered}$ | $\begin{aligned} & 23.244 \\ & (3.542) \end{aligned}$ | $\begin{gathered} \hline 0.036 \\ (0.004) \end{gathered}$ | $\begin{aligned} & 86.316 \\ & (3.507) \end{aligned}$ |
|  | 2 | $\begin{gathered} 4.287 \\ (0.765) \end{gathered}$ | $\begin{gathered} 0.044 \\ (0.007) \end{gathered}$ | $\begin{aligned} & 11.037 \\ & (1.934) \end{aligned}$ | $\begin{gathered} 0.017 \\ (0.003) \end{gathered}$ | $\begin{gathered} 35.653 \\ (10.941) \end{gathered}$ | $\begin{gathered} 0.039 \\ (0.005) \end{gathered}$ | $\begin{aligned} & 86.571 \\ & (6.537) \end{aligned}$ |
|  | 3 | $\begin{gathered} 3.377 \\ (0.469) \end{gathered}$ | $\begin{gathered} 0.048 \\ (0.009) \end{gathered}$ | $\begin{aligned} & 17.393 \\ & (1.833) \end{aligned}$ | $\begin{gathered} 0.020 \\ (0.002) \end{gathered}$ | $\begin{aligned} & 28.591 \\ & (5.302) \end{aligned}$ | $\begin{gathered} 0.048 \\ (0.002) \end{gathered}$ | $\begin{gathered} 88.007 \\ (1.675) \end{gathered}$ |
|  | 4 | $\begin{gathered} 5.369 \\ (1.040) \end{gathered}$ | $\begin{gathered} 0.043 \\ (0.003) \end{gathered}$ | $\begin{aligned} & 24.454 \\ & (1.650) \end{aligned}$ | $\begin{gathered} 0.020 \\ (0.001) \end{gathered}$ | $\begin{gathered} 52.601 \\ (10.317) \end{gathered}$ | $\begin{gathered} 0.042 \\ (0.004) \end{gathered}$ | $\begin{aligned} & 89.768 \\ & (0.718) \end{aligned}$ |
|  | 5 | $\begin{gathered} 2.497 \\ (0.604) \end{gathered}$ | $\begin{gathered} 0.054 \\ (0.008) \end{gathered}$ | $\begin{gathered} 5.690 \\ (0.575) \end{gathered}$ | $\begin{gathered} 0.018 \\ (0.004) \end{gathered}$ | $\begin{gathered} 34.846 \\ (18.546) \end{gathered}$ | $\begin{gathered} 0.053 \\ (0.006) \end{gathered}$ | $\begin{aligned} & 91.516 \\ & (3.544) \end{aligned}$ |
|  | 6 | $\begin{gathered} 3.417 \\ (0.600) \end{gathered}$ | $\begin{gathered} 0.046 \\ (0.004) \end{gathered}$ | $\begin{gathered} 8.111 \\ (1.453) \end{gathered}$ | $\begin{gathered} 0.019 \\ (0.002) \end{gathered}$ | $\begin{gathered} 63.900 \\ (21.107) \end{gathered}$ | $\begin{gathered} 0.044 \\ (0.004) \end{gathered}$ | $\begin{aligned} & 94.009 \\ & (2.962) \end{aligned}$ |
|  | 7 | $\begin{gathered} 4.085 \\ (0.685) \end{gathered}$ | $\begin{gathered} 0.046 \\ (0.001) \end{gathered}$ | $\begin{aligned} & 12.550 \\ & (1.530) \end{aligned}$ | $\begin{gathered} 0.019 \\ (0.001) \end{gathered}$ | $\begin{gathered} 77.520 \\ (35.026) \end{gathered}$ | $\begin{gathered} 0.044 \\ (0.001) \end{gathered}$ | $\begin{aligned} & 94.285 \\ & (1.323) \end{aligned}$ |
|  | 8 | $\begin{gathered} 4.540 \\ (1.391) \end{gathered}$ | $\begin{gathered} 0.041 \\ (0.002) \end{gathered}$ | $\begin{gathered} 15.072 \\ (1.256) \end{gathered}$ | $\begin{gathered} 0.018 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 104.456 \\ & (33.325) \end{aligned}$ | $\begin{gathered} 0.040 \\ (0.003) \end{gathered}$ | $\begin{aligned} & 95.555 \\ & (0.777) \end{aligned}$ |
| 6 | 1 | $\begin{gathered} 1.706 \\ (0.165) \end{gathered}$ | $\begin{gathered} 0.048 \\ (0.008) \end{gathered}$ | $\begin{gathered} 9.377 \\ (1.128) \end{gathered}$ | $\begin{gathered} 0.013 \\ (0.000) \end{gathered}$ | $\begin{aligned} & 20.575 \\ & (3.296) \end{aligned}$ | $\begin{gathered} 0.040 \\ (0.006) \end{gathered}$ | $\begin{aligned} & 91.592 \\ & (1.185) \end{aligned}$ |
|  | 2 | $\begin{gathered} 2.262 \\ (0.346) \end{gathered}$ | $\begin{gathered} 0.045 \\ (0.003) \end{gathered}$ | $\begin{aligned} & 12.303 \\ & (0.553) \end{aligned}$ | $\begin{gathered} 0.015 \\ (0.001) \end{gathered}$ | $\begin{aligned} & 22.493 \\ & (2.693) \end{aligned}$ | $\begin{gathered} 0.040 \\ (0.003) \end{gathered}$ | $\begin{aligned} & 89.754 \\ & (2.431) \end{aligned}$ |
|  | 3 | $\begin{gathered} 2.950 \\ (0.449) \end{gathered}$ | $\begin{gathered} 0.040 \\ (0.001) \end{gathered}$ | $\begin{aligned} & 17.145 \\ & (0.451) \end{aligned}$ | $\begin{gathered} 0.013 \\ (0.001) \end{gathered}$ | $\begin{aligned} & 35.305 \\ & (6.931) \end{aligned}$ | $\begin{gathered} 0.033 \\ (0.001) \end{gathered}$ | $\begin{aligned} & 91.480 \\ & (1.591) \end{aligned}$ |
|  | 4 | $\begin{gathered} 4.679 \\ (0.287) \end{gathered}$ | $\begin{gathered} 0.039 \\ (0.003) \end{gathered}$ | $\begin{aligned} & 25.620 \\ & (4.418) \end{aligned}$ | $\begin{gathered} 0.015 \\ (0.005) \end{gathered}$ | $\begin{gathered} 34.296 \\ (20.427) \end{gathered}$ | $\begin{gathered} 0.033 \\ (0.005) \end{gathered}$ | $\begin{gathered} 17.386 \\ (159.292) \end{gathered}$ |
|  | 5 | $\begin{gathered} 1.595 \\ (0.558) \end{gathered}$ | $\begin{gathered} 0.049 \\ (0.004) \end{gathered}$ | $\begin{gathered} 7.360 \\ (0.797) \end{gathered}$ | $\begin{gathered} 0.018 \\ (0.001) \end{gathered}$ | $\begin{gathered} 33.792 \\ (15.344) \end{gathered}$ | $\begin{gathered} 0.044 \\ (0.004) \end{gathered}$ | $\begin{aligned} & 95.001 \\ & (1.056) \end{aligned}$ |
|  | 6 | $\begin{gathered} 1.747 \\ (0.195) \end{gathered}$ | $\begin{gathered} 0.045 \\ (0.004) \end{gathered}$ | $\begin{gathered} 9.983 \\ (0.553) \end{gathered}$ | $\begin{gathered} 0.018 \\ (0.000) \end{gathered}$ | $\begin{gathered} 49.126 \\ (13.935) \end{gathered}$ | $\begin{gathered} 0.044 \\ (0.003) \end{gathered}$ | $\begin{aligned} & 96.227 \\ & (1.076) \end{aligned}$ |
|  | 7 | $\begin{gathered} 2.121 \\ (0.517) \end{gathered}$ | $\begin{gathered} 0.044 \\ (0.005) \end{gathered}$ | $\begin{aligned} & 11.597 \\ & (0.916) \end{aligned}$ | $\begin{gathered} 0.015 \\ (0.003) \end{gathered}$ | $\begin{gathered} 67.285 \\ (17.617) \end{gathered}$ | $\begin{gathered} 0.043 \\ (0.003) \end{gathered}$ | $\begin{aligned} & 96.819 \\ & (0.451) \end{aligned}$ |
|  | 8 | $\begin{array}{r} 2.505 \\ (0.323) \\ \hline \end{array}$ | $\begin{gathered} 0.038 \\ (0.001) \\ \hline \end{gathered}$ | $\begin{array}{r} 13.816 \\ (0.748) \\ \hline \end{array}$ | $\begin{gathered} 0.016 \\ (0.003) \\ \hline \end{gathered}$ | $\begin{gathered} 70.211 \\ (21.331) \\ \hline \end{gathered}$ | $\begin{gathered} 0.040 \\ (0.003) \\ \hline \end{gathered}$ | $\begin{array}{r} 96.222 \\ (0.981) \\ \hline \end{array}$ |

Table 17. (Continued).

| Subj Cond |  | AccHead | Tacchead | AccTibial TaccTibial AccTibia2 TaccTibia2 |  |  |  | AtteIndex |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7 | 1 | $\begin{gathered} \hline 1.579 \\ (0.422) \end{gathered}$ | $\begin{gathered} \hline 0.069 \\ (0.010) \end{gathered}$ | $\begin{gathered} \hline 6.623 \\ (0.844) \end{gathered}$ | $\begin{gathered} \hline 0.028 \\ (0.001) \end{gathered}$ | $\begin{aligned} & 10.053 \\ & (3.577) \end{aligned}$ | $\begin{gathered} 0.063 \\ (0.010) \end{gathered}$ | $\begin{aligned} & \hline 82.284 \\ & (8.819) \end{aligned}$ |
|  | 2 | $\begin{gathered} 2.064 \\ (0.472) \end{gathered}$ | $\begin{gathered} 0.092 \\ (0.005) \end{gathered}$ | $\begin{gathered} 8.338 \\ (1.887) \end{gathered}$ | $\begin{gathered} 0.027 \\ (0.004) \end{gathered}$ | $\begin{gathered} 8.842 \\ (6.557) \end{gathered}$ | $\begin{gathered} 0.066 \\ (0.016) \end{gathered}$ | $\begin{gathered} 70.681 \\ (12.529) \end{gathered}$ |
|  | 3 | $\begin{gathered} 1.983 \\ (0.510) \end{gathered}$ | $\begin{gathered} 0.076 \\ (0.010) \end{gathered}$ | $\begin{aligned} & 14.290 \\ & (4.241) \end{aligned}$ | $\begin{gathered} 0.028 \\ (0.001) \end{gathered}$ | $\begin{gathered} 17.014 \\ (13.848) \end{gathered}$ | $\begin{gathered} 0.057 \\ (0.007) \end{gathered}$ | $\begin{aligned} & 83.444 \\ & (9.448) \end{aligned}$ |
|  | 4 | $\begin{gathered} 2.428 \\ (0.237) \end{gathered}$ | $\begin{gathered} 0.055 \\ (0.004) \end{gathered}$ | $\begin{aligned} & 19.536 \\ & (1.204) \end{aligned}$ | $\begin{gathered} 0.025 \\ (0.004) \end{gathered}$ | $\begin{gathered} 28.212 \\ (14.996) \end{gathered}$ | $\begin{gathered} 0.055 \\ (0.002) \end{gathered}$ | $\begin{aligned} & 89.616 \\ & (4.716) \end{aligned}$ |
|  | 5 | $\begin{gathered} 1.275 \\ (0.637) \end{gathered}$ | $\begin{gathered} 0.089 \\ (0.035) \end{gathered}$ | $\begin{gathered} 5.614 \\ (0.983) \end{gathered}$ | $\begin{gathered} 0.031 \\ (0.003) \end{gathered}$ | $\begin{gathered} 6.220 \\ (6.264) \end{gathered}$ | $\begin{gathered} 0.066 \\ (0.008) \end{gathered}$ | $\begin{gathered} 72.608 \\ (15.007) \end{gathered}$ |
|  | 6 | $\begin{gathered} 1.518 \\ (0.202) \end{gathered}$ | $\begin{gathered} 0.069 \\ (0.016) \end{gathered}$ | $\begin{gathered} 8.742 \\ (0.829) \end{gathered}$ | $\begin{gathered} 0.026 \\ (0.004) \end{gathered}$ | $\begin{gathered} 16.712 \\ (15.874) \end{gathered}$ | $\begin{gathered} 0.065 \\ (0.004) \end{gathered}$ | $\begin{gathered} 81.059 \\ (13.480) \end{gathered}$ |
|  | 7 | $\begin{gathered} 1.599 \\ (0.184) \end{gathered}$ | $\begin{gathered} 0.071 \\ (0.016) \end{gathered}$ | $\begin{aligned} & 11.365 \\ & (1.986) \end{aligned}$ | $\begin{gathered} 0.023 \\ (0.005) \end{gathered}$ | $\begin{gathered} 14.290 \\ (11.853) \end{gathered}$ | $\begin{gathered} 0.061 \\ (0.004) \end{gathered}$ | $\begin{gathered} 82.841 \\ (10.228) \end{gathered}$ |
|  | 8 | $\begin{gathered} 2.003 \\ (0.647) \end{gathered}$ | $\begin{gathered} 0.052 \\ (0.006) \end{gathered}$ | $\begin{gathered} 19.032 \\ (2.726) \end{gathered}$ | $\begin{gathered} 0.018 \\ (0.001) \end{gathered}$ | $\begin{gathered} 20.848 \\ (16.682) \end{gathered}$ | $\begin{gathered} 0.052 \\ (0.002) \end{gathered}$ | $\begin{aligned} & 86.304 \\ & (7.176) \end{aligned}$ |
| 8 | 1 | $\begin{gathered} 2.675 \\ (0.908) \end{gathered}$ | $\begin{gathered} 0.057 \\ (0.010) \end{gathered}$ | $\begin{gathered} 6.860 \\ (0.798) \end{gathered}$ | $\begin{gathered} 0.008 \\ (0.003) \end{gathered}$ | $\begin{aligned} & 18.563 \\ & (3.574) \end{aligned}$ | $\begin{gathered} 0.049 \\ (0.005) \end{gathered}$ | $\begin{aligned} & 85.882 \\ & (2.263) \end{aligned}$ |
|  | 2 | $\begin{gathered} 1.927 \\ (0.774) \end{gathered}$ | $\begin{gathered} 0.047 \\ (0.009) \end{gathered}$ | $\begin{gathered} 8.777 \\ (1.354) \end{gathered}$ | $\begin{gathered} 0.016 \\ (0.006) \end{gathered}$ | $\begin{aligned} & 17.655 \\ & (5.889) \end{aligned}$ | $\begin{gathered} 0.051 \\ (0.002) \end{gathered}$ | $\begin{aligned} & 88.969 \\ & (2.528) \end{aligned}$ |
|  | 3 | $\begin{gathered} 3.100 \\ (1.203) \end{gathered}$ | $\begin{gathered} 0.049 \\ (0.014) \end{gathered}$ | $\begin{aligned} & 16.343 \\ & (1.798) \end{aligned}$ | $\begin{gathered} 0.016 \\ (0.001) \end{gathered}$ | $\begin{gathered} 28.853 \\ (14.000) \end{gathered}$ | $\begin{gathered} 0.047 \\ (0.002) \end{gathered}$ | $\begin{aligned} & 88.800 \\ & (1.698) \end{aligned}$ |
|  | 4 | $\begin{gathered} 3.635 \\ (0.287) \end{gathered}$ | $\begin{gathered} 0.041 \\ (0.003) \end{gathered}$ | $\begin{aligned} & 22.497 \\ & (4.418) \end{aligned}$ | $\begin{gathered} 0.016 \\ (0.005) \end{gathered}$ | $\begin{gathered} 33.897 \\ (20.427) \end{gathered}$ | $\begin{gathered} 0.045 \\ (0.005) \end{gathered}$ | $\begin{gathered} 88.543 \\ (159.292) \end{gathered}$ |
|  | 5 | $\begin{gathered} 1.351 \\ (0.219) \end{gathered}$ | $\begin{gathered} 0.049 \\ (0.004) \end{gathered}$ | $\begin{gathered} 10.794 \\ (1.488) \end{gathered}$ | $\begin{gathered} 0.014 \\ (0.001) \end{gathered}$ | $\begin{gathered} 18.361 \\ (10.709) \end{gathered}$ | $\begin{gathered} 0.060 \\ (0.010) \end{gathered}$ | $\begin{aligned} & 89.237 \\ & (8.786) \end{aligned}$ |
|  | 6 | $\begin{gathered} 1.674 \\ (0.469) \end{gathered}$ | $\begin{gathered} 0.049 \\ (0.009) \end{gathered}$ | $\begin{gathered} 14.427 \\ (1.070) \end{gathered}$ | $\begin{gathered} 0.012 \\ (0.001) \end{gathered}$ | $\begin{gathered} 37.428 \\ (21.557) \end{gathered}$ | $\begin{gathered} 0.053 \\ (0.007) \end{gathered}$ | $\begin{aligned} & 93.685 \\ & (4.856) \end{aligned}$ |
| . | 7 | $\begin{gathered} 2.109 \\ (0.382) \end{gathered}$ | $\begin{gathered} 0.040 \\ (0.003) \end{gathered}$ | $\begin{aligned} & 18.260 \\ & (3.357) \end{aligned}$ | $\begin{gathered} 0.014 \\ (0.004) \end{gathered}$ | $\begin{gathered} 19.572 \\ (9.906) \end{gathered}$ | $\begin{gathered} 0.049 \\ (0.005) \end{gathered}$ | $\begin{aligned} & 86.422 \\ & (7.590) \end{aligned}$ |
|  | 8 | $\begin{gathered} 2.877 \\ (0.419) \\ \hline \end{gathered}$ | $\begin{gathered} 0.037 \\ (0.003) \\ \hline \end{gathered}$ | $\begin{array}{r} 24.212 \\ (4.260) \\ \hline \end{array}$ | $\begin{gathered} 0.013 \\ (0.001) \\ \hline \end{gathered}$ | $\begin{gathered} 41.564 \\ (32.918) \\ \hline \end{gathered}$ | $\begin{gathered} 0.049 \\ (0.004) \\ \hline \end{gathered}$ | $\begin{aligned} & 88.395 \\ & (9.003) \\ & \hline \end{aligned}$ |

Table 17. (Continued).

| Subj | Cond | AccHead | Tacchead | AccTibial TaccTibial AccTibia2 TaccTibia2 |  |  |  | AtteIndex |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 9 | 1 | 3.282 | 0.034 | 0.000 | 0.000 | 35.744 | 0.022 | 90.463 |
|  |  | (1.117) | (0.004) | (0.000) | (0.000) | (6.600) | (0.002) | (3.642) |
| 2 |  | 3.009 | 0.052 | 12.439 | 0.009 | 19.501 | 0.044 | 84.268 |
|  |  | (0.876) | (0.002) | (0.618) | (0.001) | (2.920) | (0.004) | (5.294) |
| 3 |  | 3.636 | 0.051 | 13.549 | 0.008 | 23.537 | 0.043 | 84.638 |
|  |  | (0.854) | (0.002) | (1.093) | (0.001) | (1.747) | (0.002) | (3.044) |
| 4 |  | 5.092 | 0.049 | 14.558 | 0.011 | 34.028 | 0.041 | 85.189 |
|  |  | (1.339) | (0.002) | (0.748) | (0.004) | (3.138) | (0.002) | (2.821) |
| 5 |  | 1.250 | 0.050 | 7.193 | 0.015 | 41.695 | 0.045 | 96.829 |
|  |  | (0.409) | (0.004) | (0.765) | (0.001) | (9.184) | (0.004) | (1.310) |
| 6 |  | 1.978 | 0.048 | 9.614 | 0.012 | 45.429 | 0.045 | 95.104 |
|  |  | (0.369) | (0.004) | (2.128) | (0.002) | (14.718) | (0.004) | (2.231) |
| 7 |  | 2.322 | 0.049 | 13.650 | 0.012 | 37.963 | 0.049 | 93.636 |
|  |  | (0.468) | $(0.002)$ | (0.916) | (0.002) | (11.147) | (0.003) | (1.501) |
| 8 |  | 3.262 | 0.047 | 17.181 | 0.009 | 80.940 | 0.044 | 95.257 |
|  |  | (0.658) | (0.003) | (2.355) | (0.001) | (41.180) | (0.001) | (2.152) |
| 10 | 1 | 79 | 0.059 | 8.838 | 0.017 | 10.351 | 0.053 | 80.673 |
|  |  | (0.271) | (0.008) | (1.381) | (0.001) | (3.027) | (0.003) | (6.142) |
| 2 |  | 3.264 | 0.056 | 15.092 | 0.017 | 16.505 | 0.054 | 78.966 |
|  |  | (0.503) | (0.004) | (1.315) | (0.001) | (6.315) | (0.001) | (4.516) |
| 3 |  | 3.779 | 0.054 | 20.843 | 0.017 | 24.878 | 0.051 | 83.324 |
|  |  | (1.092) | (0.003) | (1.934) | (0.001) | (12.003) | (0.002) | (4.633) |
| 4 |  | 3.638 | 0.053 | 26.694 | 0.017 | 24.374 | 0.053 | 85.117 |
|  |  | (0.612) | (0.001) | (3.142) | (0.001) | (2.906) | (0.002) | (1.161) |
| 5 |  | 2.303 | 0.066 | 10.048 | 0.015 | 12.873 | 0.065 | 81.337 |
|  |  | (0.261) | (0.004) | (0.844) | (0.001) | (3.476) | (0.004) | (3.960) |
| 6 |  | 3.173 | 0.066 | 16.706 | 0.017 | 15.799 | 0.054 | 71.088 |
|  |  | $(0.690)$ | (0.006) | (1.695) | (0.002) | (12.265) | $(0.006)$ | (15.391) |
| 7 |  | 3.284 | 0.067 | 24.273 | 0.017 | 18.119 | 0.061 | 79.366 |
|  |  | (0.465) | (0.003) | (1.769) | (0.001) | (6.235) | (0.001) | (9.264) |
| 8 |  | 2.891 | 0.060 | 18.451 | 0.019 | 28.052 | 0.055 | 83.710 |
|  |  | (1.135) | (0.003) | (2.749) | (0.001) | (22.142) | $(0.003)$ | (8.999) |

Note: Acceleration unit is in $g$ and time unit is in $s$.
AtteIndex unit is in \%.
Standard deviation values are in parenthesis.
The definitions of variables are in Appendix A.

Table 18. Subject means and standard deviations of acceleration variables (Group 2).


Table 18. (Continued).

| Subj | Cond | Acchead | TaccHead | AccTibial TaccTibial AccTibia2 TaccTibia2 |  |  |  |  | AtteIndex |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | 1 | 2.453 | 0.029 | - | - | - | 24.460 | 0.021 | 89.171 |
|  |  | (1.278) | (0.007) |  |  |  | (5.673) | (0.005) | (6.326) |
|  | 2 | 5.020 | 0.030 | - | - | - | 46.553 | 0.023 | 88.726 |
|  |  | (1.099) | (0.005) |  |  |  | (11.019) | (0.007) | (3.663) |
|  | 3 | 6.072 | 0.031 | - | - | - | 66.730 | 0.024 | 90.824 |
|  |  | (1.006) | (0.009) |  |  |  | (8.998) | (0.009) | (1.617) |
|  | 4 | 6.193 | 0.038 | - | - | - | 69.051 | 0.031 | 90.669 |
|  |  | (1.569) | (0.004) |  |  |  | (19.761) | (0.003) | (2.714) |
|  | 5 | 2.655 | 0.036 | - | - | - | 44.031 | 0.030 | 93.425 |
|  |  | (0.549) | (0.014) |  |  |  | (12.343) | (0.012) | (2.542) |
|  | 6 | 3.342 | 0.044 | - | - | - | 91.346 | 0.036 | 96.213 |
|  |  | (0.988) | (0.002) |  |  |  | (27.184) | (0.003) | (1.000) |
|  | 7 | 4.262 | 0.039 | - | - | - | 111.422 | 0.036 | 96.095 |
|  |  | (0.974) | (0.004) |  |  |  | (22.145) | (0.003) | (0.932) |
|  | 8 | 4.373 | 0.038 | - | - | - | 130.590 | 0.036 | 96.572 |
|  |  | (1.721) | (0.007) |  |  |  | (44.476) | (0.009) | (1.246) |

Note: Acceleration unit is in g and time unit is in s . AtteIndex unit is in \%.
Standard deviation values are in parenthesis.
The definitions of variables are in Appendix A.

- indicates no value present.


## APPENDIX F

## REPRESENTATIVE CURVES



Figure 14. Representative ankle joint curves for barefoot at 60 cm (Group 1).


Figure 15. Representative knee joint curves for barefoot at 60 cm (Group 1).


Figure 16. Representative hip joint curves for barefoot at 60 cm (Group 1).

(a) Head acceleration

(b) Tibia acceleration

Figure 17. Representative acceleration curves for barefoot at 60 cm (Group 1).

## APPENDIX G

## INFORMED CONSENT FORM

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You are invited to participate in a research study entitled "Shock attenuation at the tibia and head during landing activities" which examines the impact force and impact shock in different surface conditions during landings from different heights.

You are aware that the test session will take approximately one hour including practice and familiarity with the testing protocol. The test session will begin with a warm-up riding a stationary bike for five minutes. The girth and length of lower extremity segments will be measured and recorded afterwards. Reflective markers will be placed on the right side of the shoulder, hip, knee, ankle, heel, and toe. Two miniature accelerometers will be placed on the lower leg and the forehead using double-sided adhesive tapes and Velcro straps. You will perform 40 step-off landings onto a force platform, 5 trials in each of eight experimental conditions. These conditions will include landings from four predetermined heights ( $11.8,17.7,23.6$, and 29.5 inches) with and without shoes. You will wear shoes provided by Biomechanics and Sports Medicine Lab during the shoe conditions. The presentation order of different surfaces (shoes and no shoes) and heights will be randomized. During the testing, data from the force platform, the accelerometers, and a video camera will be simultaneously recorded.

## Potential Risks and Benefits

The potential risks include an ankle sprain and a muscular strain of the lower extremity from landing in an unbalanced fashion. These risks will be minimized through proper warm-up and sufficient practice before the test. Painful heel pad could be another risk during the barefoot conditions. A pilot study was conducted to determine the appropriate highest height within the tolerance of subjects. It showed that 29.5 -inches was tolerable: no performance changes and complaints were reported by the subjects. All tests will be conducted and the equipment handled by the qualified research personnel in the Biomechanics and Sports Medicine Lab. You will be encouraged to warm up actively prior to the testing session so that you feel physically prepared to perform effectively and thus minimize any chances of injuries. In an event of physical injuries resulting from the test, standard first aid procedures will be administered as necessary. At least one researcher with a basic knowledge of athletic training and/or first aid procedures will be present at each test session. The University of Tennessee does not
automatically provide reimbursement for medical care or other compensation. Your benefits from participating in this study include better understanding of ground reaction force and impact shock in landing performance. You are welcome to make an appointment to review the data from your test. In addition, if you wish to have a copy of the results of the study, please let the investigator know.

## Confidentiality

Your identity as a subject will be held in a strict confidential manner during and after the study. The description of your data will be coded numerically and will be referred to by a subject number. Only the principal investigator, her advisor and qualified Biomechanics and Sports Medicine Lab personnel will have access to subject information and data. Data will be stored on hard drives of computers in the Biomechanics and Sports Medicine Lab during the study, and will be backed up onto zip disks/CDs and erased from the hard drives after the completion of the study. Subject information sheets, videotapes, and backup data cartridges will be stored in a locked file cabinet in the office of the principal investigator's advisor.

If you have questions at any time about the study or the procedures, or experience adverse effects as a result of participating in this study, you may contact Yeon-Joo Yu at (865) 974-2091 or Songning Zhang at (865) 974-1271. If you have questions about your rights as a participant, contact the Compliance Section of the Office of Research at (865) 974-3466. Your participation is completely voluntary and your decision regarding whether or not to participate will involve no penalty or loss of benefits to which you are otherwise entitled. If you withdraw from the study before data collection is completed, your data will be destroyed.

I have read the above information and agree to participate in this study. I have received a copy of this form.

## Participant's name

Participant's signature Date
Investigator
Date

## APPENDIX H

## TABLES FOR GROUP 2

Table 19. Means and standard deviations of knee joint kinematic variables (Group 2).

| Surface | Height | Cont | Max | Tmax | Min | Tmin | ROM | ContVel | MaxVel | TmaxVel |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Shoe | 1 | 27.439 | 78.675 | 0.190 | 19.243 | 0.320 | 59.432 | 324.322 | 664.765 | 0.037 |
|  |  | (0.708) | (4.744) | (0.042) | (9.508) | (0.302) | (12.289) | (62.537) | (82.022) | (0.010) |
|  | 2 | 31.132 | 86.135 | 0.203 | 23.140 | 0.398 | 62.995 | 376.322 | 763.637 | 0.033 |
|  |  | (1.536) | (6.234) | (0.055) | (10.983) | (0.181) | (10.760) | (22.996) | 116.141) | (0.006) |
|  | 3 | 31.545 | 89.114 | 0.199 | 24.920 | 0.200 | 64.194 | 402.103 | 793.749 | 0.034 |
|  |  | (1.420) | (5.248) | (0.045) | (11.747) | (0.346) | (10.389) | (47.160) | 101.497) | (0.002) |
|  | 4 | 31.96 | $93.972^{\text {c }}$ | 0.216 | 22.498 | 0.320 | 71.474 | 411.4 | 904.552 | 0.034 |
|  |  | (0.983) | (7.040) | (0.066) | (8.820) | (0.302) | (5.303) | (153.820) | $(216.578)$ | $(0.008)$ |
| Barefoot | 1 | 27.869 | 75.374 | 0.174 | 18.850 | 0.229 | 56.524 | 390.64 | 632.746 | 0.032 |
|  |  | (5.913) | (7.503) | (0.028) | (9.711) | (0.299) | (13.528) | (111.099) | (82.869) | (0.008) |
|  | 2 | 29.860 | 84.035 | 0.210 | 22.981 | 0.239 | 61.054 | 385.780 | 686.642 | 0.034 |
|  |  | (1.763) | (6.440) | (0.060) | (11.799) | (0.317) | (11.038) | (19.237) | (80.711) | (0.003) |
|  | 3 | 31.387 | 85.276 | 0.185 | 23.584 | 0.238 | 61.692 | 376.510 | 724.963 | 0.035 |
|  |  | (5.784) | (4.498) | (0.038) | (11.728) | (0.315) | (9.573) | (78.636) | (136.151) | ( 0.006 ) |
|  | 4 | 30.52 | $88.933^{\text {c }}$ | 0.182 | 23.589 | 0.315 | 65.344 | 428.967 | 775.841 | 0.036 |
|  |  | (5.255) | (7.733) | (0.040) | (12.140) | (0.295) | (5.234) | (52.106) | (156.099) | (0.005) |

Note: Angle and ROM units are in degrees and units of time are in s.
Velocity units are in deg/s.
Standard deviation values are in parenthesis.
${ }^{\text {a }}$ denotes significant difference between heights 1 and 2 .
${ }^{\mathbf{b}}$ denotes significant difference between heights 1 and 3 .
${ }^{\mathrm{c}}$ denotes significant difference between heights 1 and 4.
${ }^{d}$ denotes significant difference between heights 2 and 3 .
${ }^{\mathbf{e}}$ denotes significant difference between heights 2 and 4.
${ }^{\mathrm{f}}$ denotes significant difference between heights 3 and 4 .

* denotes significant difference between the shoe and barefoot conditions on the same landing height.
The definitions of variables are in Appendix A.

Table 20. Means and standard deviations of hip joint kinematic variables (Group 2).

| Surface | Height | Cont | Max | Tmax | Min | Tmin | ROM | ContVel | MaxVel | TmaxVel |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Shoe | 1 | 29.421 | 64.607 | 0.191 | 20.814 | 0.320 | 43.793 | 197.083 | 452.207 | 0.040 |
|  |  | (3.530) | (7.722) | (0.043) | (10.998) | (0.302) | (18.639) | (21.276) | (6.897) | (0.012) |
|  | 2 | 31.141 | 75.847 | 0.212 | 25.238 | 0.279 | 50.609 | 233.947 | 539.897 | 0.036 |
|  |  | (1.127) | (10.233) | (0.048) | (10.879) | (0.300) | (13.184) | (30.508) | (55.119) | (0.005) |
|  | 3 | 33.281 | 89.294 | 0.238 | 27.097 | 0.200 | 62.198 | 245.508 | $603.101^{\text {b }}$ | 0.040 |
|  |  | (1.546) | (18.071) | (0.059) | (11.615) | (0.346) | (16.950) | (18.742) | (66.955) | (0.004) |
|  | 4 | 32.569 | 99.234 | 0.248 | 27.205 | 0.240 | 72.029 | 280.767 | $684.730^{\text {ce }}$ | 0.038 |
|  |  | (1.555) | (25.961) | (0.078) | (10.530) | (0.317) | (23.424) | (48.756) | (103.808) | (0.009) |
| Barefoot | 1 | 29.701 | 63.074 | 0.184 | 20.557 | 0.273 | 42.517 | 221.016 | 430.368 | 0.037 |
|  |  | (4.587) | (5.299) | (0.038) | (11.842) | (0.291) | (17.055) | (57.417) | (15.440) | (0.009) |
|  | 2 | 33.022 | 88.584 | 0.243 | 26.010 | 0.240 | 62.574 | 222.831 | 514.753 | 0.040 |
|  |  | (3.000) | (22.867) | (0.070) | (13.471) | (0.317) | (20.052) | (46.131) | (68.195) | (0.004) |
|  | 3 | 34.116 | 94.939 | 0.237 | 26.515 | 0.200 | 68.424 | 212.795 | $560.161^{\text {b }}$ | 0.043 |
|  |  | (1.515) | (20.560) | (0.051) | (13.430) | (0.346) | (16.816) | (98.502) | (59.580) | (0.004) |
|  | 4 | 34.468 | 105.962 | 0.246 | 29.002 | 0.200 | 76.960 | 271.607 | $651.353^{\text {ce }}$ | 0.045 |
|  |  | (4.612) | (27.515) | (0.074) | (12.995) | (0.346) | (20.270) | (107.168) | (65.461) | (0.003) |

Note: Angle and ROM units are in degrees and units of time are in s.
Velocity units are in deg/s.
Standard deviation values are in parenthesis.
${ }^{2}$ denotes significant difference between heights 1 and 2.
${ }^{\mathrm{b}}$ denotes significant difference between heights 1 and 3.
${ }^{\text {c }}$ denotes significant difference between heights 1 and 4.
${ }^{\text {d }}$ denotes significant difference between heights 2 and 3.
${ }^{e}$ denotes significant difference between heights 2 and 4.
${ }^{\mathrm{f}}$ denotes significant difference between heights 3 and 4.

* denotes significant difference between the shoe and barefoot conditions on the same landing height.
The definitions of variables are in Appendix A.

Table 21. Means and standard deviations of vertical ground reaction force variables (Group 2).

| Surface | Height | Fl | T1 | F2 | T2 | LrateFl | LrateF2 | Imp 100 ms |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Shoe | 1 | - | - | 70.618 | 0.018 | - | 3829.569 | 2.849 |
|  |  |  |  | (13.088) | (0.001) |  | (750.627) | (0.330) |
|  | 2 | - | - | 82.880 | 0.021 | - | 4384.963 | 2.713 |
|  |  |  |  | (14.597) | (0.004) |  | (1334.748) | (0.378) |
|  | 3 | - | - | $101.458^{\text {b }}$ | 0.021 | - | 5432.742 | 3.022 |
|  |  |  |  | (24.068) | (0.004) |  | (2330.603) | (0.613) |
|  | 4 | - | - | $107.547^{\text {c }}$ | 0.025 | - | 4537.773 | 3.115 |
|  |  |  |  | (18.143) | (0.003) |  | (1393.582) | (0.349) |
| Barefoot | 1 | - | - | 98.456* | 0.023 * | - | 6019.677 | 2.678 |
|  |  |  |  | (14.283) | (0.012) |  | (3811.018) | (0.493) |
|  | 2 | - | - | 106.729 | 0.030* | - | 3924.817 | 2.518 |
|  |  |  |  | (20.560) | (0.008) |  | (1984.299) | (0.510) |
|  | 3 | - | - | 122.650 | 0.031 * | - | 4063.605 | 2.734 |
|  |  |  |  | (8.240) | (0.003) |  | (672.696) | (0.394) |
|  | 4 | - | - | 119.723 | 0.028 | - | 6141.712 | 2.889 |
|  |  |  |  | (8.360) | (0.002) |  | (2555.345) | (0.398) |

Note: Force unit is in $\mathrm{N} / \mathrm{kg}$ and time unit is in s .
Loading rate unit is in $\mathrm{N} / \mathrm{kg} / \mathrm{s}$.
Impulse unit is in ( $\mathrm{N} / \mathrm{kg}$ )•s.
Standard deviation values are in parenthesis.
${ }^{\text {a }}$ denotes significant difference between heights 1 and 2 .
${ }^{b}$ denotes significant difference between heights 1 and 3.
${ }^{\text {c }}$ denotes significant difference between heights 1 and 4.
${ }^{\text {d }}$ denotes significant difference between heights 2 and 3.
${ }^{\text {e }}$ denotes significant difference between heights 2 and 4.
${ }^{\mathrm{r}}$ denotes significant difference between heights 3 and 4.

* denotes significant difference between the shoe and barefoot conditions on the same landing height.
- denotes no value present.

The definitions of variables are in Appendix A.

Table 22. Means and standard deviations of acceleration variables (Group 2).


Note: Acceleration unit is in g and time unit is in $s$.
Shock attenuation index unit is in \%.
Standard deviation values are in parenthesis.
${ }^{\text {a }}$ denotes significant difference between heights 1 and 2 .
${ }^{\mathrm{b}}$ denotes significant difference between heights 1 and 3.
${ }^{c}$ denotes significant difference between heights 1 and 4.
${ }^{\text {d }}$ denotes significant difference between heights 2 and 3.
${ }^{e}$ denotes significant difference between heights 2 and 4.
${ }^{\prime}$ denotes significant difference between heights 3 and 4.

* denotes significant difference between the shoe and barefoot conditions on the same landing height.
- denotes no value present.

The definitions of variables are in Appendix A.

Yeon-Joo Yu was borm in In-Cheon, Korea on November 17, 1973. After she graduated In Myung women's high school in February of 1992, she attended Sang Myung University in Seoul, Korea. She received her Bachelor of Physical Education degree in February of 1996. In March of that same year she began to work in Han-Yang Trading Co., Ltd as a secretary. In January of 1999 she began her graduate studies in Exercise Science with a concentration in Sports Medicine and Biomechanics at the University of Tennessee, Knoxville. As a graduate student, she was involved in several projects including analysis of shock attenuation of the human body during landings and biomechanical analysis of energy attenuation strategy in landings. Upon completion of her thesis, she received the Master of Science degree in human Performance and Sport Studies in May of 2001.


[^0]:    Shoe
    Subjects wore lab shoes (Noveto, Adidas) provided by the Biomechanics/Sports Medicine Lab. The midsole and outsole of the shoe consisted of lightstrike EVA and minimal carbon rubber. The diagram of experimental setup is shown in Figure 2.

