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3 **INFLUENCE OF THERMAL PRETREATMENTS ON DIMENSIONAL**
4 **CHANGE AND HUMIDITY SENSITIVITY OF DENSIFIED SPRUCE AND**
5 **POPLAR WOOD**
6
7

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23 **ABSTRACT**

24
25 The effect of thermal pretreatments on the dimensional change and humidity sensitivity
26 of densified spruce (*Picea orientalis*) and poplar (*Populus nigra*) wood were investigated.
27 A thermal pretreatment was applied on the wood specimens at 140 °C, 160 °C, 180 °C,
28 and 200 °C for 7 h and 9 h. Wood specimens were then compressed at ratios of 20 % and
29 40 % at a temperature of 150 °C. The results showed that spring-back and thickness
30 swelling increased in all specimens (thermally pre-treated and untreated) depending on
31 the increase in compression ratio. However, set-recovery was determined higher at 20 %
32 compression ratio. The equilibrium moisture content values of untreated specimens and
33 thermally pre-treated specimens at low temperatures (140 °C and 160 °C) were found
34 lower than uncompressed specimens. The impact of compression ratio on equilibrium
35 moisture content was not clear. Thermal pretreatments significantly affected the
36 dimensional stability and hygroscopicity of densified specimens (especially poplar
37 wood). Depending on the increase in thermal pretreatment temperature and duration,
38 spring-back, set-recovery and thickness swelling in wood specimens decreased up to 31
39 %, 67 % and 62 %, respectively. In addition, equilibrium moisture content and water
40 absorption decreased with the increase in thermal pretreatment temperature and duration.
41 Moreover, the thermal treatment temperature was more important than duration on the
42 investigated properties.
43

44 **Keywords:** Densification, dimensional stability, hygroscopicity, thermal treatment,
45 wood material.
46

47 **INTRODUCTION**

48 The numerous superior properties of wood make it usable in many structural and non-
49 structural applications. However, since wood is a natural material, it can be easily
50 degraded by various environmental factors (biotic and abiotic). On the other hand, the
51 difficulties in finding wood with good characteristics and the increase in less durable and
52 faster growing species have accelerated the modification studies aimed at improving
53 wood properties (Rowell 2012, Sandberg *et al.* 2017). In wood modification processes, it
54 is aimed to produce materials that are non-toxic during use and do not create any toxic
55 residues when disposed of at the end of its life. Wood modification is essentially methods
56 applied to improve some undesirable characteristics of wood such as low resistance to
57 biodegradation, hygroscopic structure, low dimensional stability, low hardness and low
58 resistance to weathering (Hill 2006, Gérardin 2016, Jones *et al.* 2019).

59 Density is an important parameter for determining suitable usage areas of wood
60 and giving an idea about many properties of wood. In structural applications and where
61 resistance is important, high-density wood species are generally preferred because of their
62 high mechanical properties. However, wood species with these properties are difficult to
63 obtain due to their limited and high cost. Wood densification, an alternative modification
64 method, it gives improved new properties to wood materials with low-quality and
65 insufficient strength characteristics. Thus, the economic value and usage area of wood
66 species that are less used in the sector can be increased (Sandberg *et al.* 2013, Song *et al.*
67 2018, Fang *et al.* 2019, Laskowska 2020). There is a growing interest in the use of
68 densified wood. Increased wood density is achieved by compressing the wood material,
69 usually in the radial direction and under suitable conditions (moisture and temperature)
70 to improve its especially mechanical properties. The main purpose of wood densification
71 processes is to improve the hardness and mechanical strength properties of wood species

72 with particularly low density (Laine *et al.* 2013, Báder *et al.* 2018, Cencin *et al.* 2021, Xu
73 *et al.* 2021). In addition to the compression process, wood material can be densified by
74 filling the cavity structure of wood impregnated with different resins or by combining
75 compression and impregnation (Seborg *et al.* 1962, Kollmann *et al.* 1975, Inoue *et al.*
76 1993, Fukuta *et al.* 2008, Gabrielli and Kamke 2010, Lykidis *et al.* 2020, Pelit and
77 Emiroglu 2020). However, the densified wood obtained by these methods may contain
78 toxic effects depending on the resin properties. The most important issue associated with
79 wood densified by compressing is the fixation of the compressed thickness. Compressed
80 wood produced without any deformation fixation treatment is sensitive to moisture. After
81 compression, the densified wood has a tendency to return to its initial dimensions when
82 exposed to liquid water or humid environments. This undesirable phenomenon is defined
83 as set-recovery and is the main disadvantage of compressed wood (Morsing 2000, Navi
84 and Heger 2004, Rautkari *et al.* 2010, Kutnar and Kamke 2012, Gao *et al.* 2019).

85 Thermal modification is a generally accepted procedure used to improve some
86 undesirable properties of wood at a temperature greater than 160 °C, without chemical
87 additives and in a limited oxygen environment (Militz 2005, Torniainen *et al.* 2021). The
88 thermal modification of wood is accepted environmentally friendly and is known as the
89 most commercial wood modification process to date (Sandberg *et al.* 2021). Thermal
90 treatments are a physical process. However, it causes chemical changes of the basic
91 components of wood (cellulose, hemicelluloses and lignin), which affects properties such
92 as hygroscopicity, dimensional stability, permeability, and decay resistance in wood
93 (Boonstra 2016). Thermal treatments are a widely used wood modification method,
94 especially to increase dimensional stability and decay resistance (Esteves and Pereira
95 2009, Ünsal *et al.* 2009, Sandberg *et al.* 2017, Hill *et al.* 2021). The equilibrium moisture
96 content (EMC) of thermally treated wood is reduced and stability resistance is

97 significantly increased by decreasing shrinking and swelling due to ambient conditions
98 (Militz 2002, Bekhta and Niemz 2003, Esteves *et al.* 2007, Korkut and Guller 2008,
99 Kaygin *et al.* 2009, Aydemir *et al.* 2011, Kocaefe *et al.* 2015, Boonstra 2016). This
100 property change is mainly associated with the thermal degradation of hemicelluloses and
101 generally the changes persist as the temperature increases (Hill 2006). In addition to
102 dimensional stability, wood's resistance to biodegradation increases as a result of thermal
103 treatment, especially its resistance to fungi (Boonstra *et al.* 2007a, Dubey *et al.* 2012,
104 Lekounougou and Kocaefe 2014, Yalçın and Şahin 2015, Ayata *et al.* 2017). Moreover,
105 the color of the thermally treated wood can be changed homogeneously to more
106 interesting dark tones (Thompson *et al.* 2005, González-Peña and Hale 2009,
107 Pleschberger *et al.* 2014, Toker *et al.* 2016, Pelit 2017, Sikora *et al.* 2018, Sivrikaya *et al.*
108 2019, Torniainen *et al.* 2021). However, as an important disadvantage, mechanical
109 strength properties of thermally treated wood generally decreases and wood becomes
110 more fragile and rigid, depending on the processing conditions (treatment temperature,
111 treatment time, ambient condition), wood species, and properties of its anatomical
112 structure, or the moisture content of the wood (Poncsák *et al.* 2006, Yıldız *et al.* 2006,
113 Boonstra *et al.* 2007b, Korkut *et al.* 2008, Perçin *et al.* 2016, Pelit and Yorulmaz 2019).
114 The reduced mechanical strength limits the use of thermally treated wood, especially in
115 structural applications (Esteves and Pereira 2009).

116 In our previous study, the effect of densification modification on the mechanical
117 properties of thermally treated wood specimens was studied (Pelit and Yorulmaz 2019).
118 The results showed that the hardness and mechanical strength, which were reduced by
119 thermal treatment, improved significantly due to the compression ratio after densification.
120 The goal of this study presented was to investigate the effect of thermal pretreatments on
121 the dimensional stability and hygroscopicity behaviors of densified wood specimens. For

122 this reason, poplar and spruce woods were thermally treated at four different temperatures
123 and at two different durations were densified with two different compression ratios.
124 Spring-back, thickness swelling, set-recovery, equilibrium moisture content (EMC) and
125 water absorption tests were performed to determine the stability and hygroscopicity
126 properties of wooden specimens in this condition.

127 MATERIALS AND METHOD

128 Wood material

129 In this study, Eastern spruce (*Picea orientalis* (L.) Link.) and black poplar (*Populus nigra*
130 L.) wood, which have relatively low densities, were used. Wood materials were supplied
131 as round wood from a timber company in Istanbul, Turkey. Round wood was cut from
132 the sapwood with a band sawing machine taking into account the study methodology.
133 Wood materials were subjected to natural drying (approximately 12 % moisture content),
134 and then cut with a tolerance of 15 % to 20 % from the draft dimensions of the specimens
135 to be used for densification.

136 Thermal treatment of wood specimens

137 Thermal treatments were conducted in a laboratory-type oven and at atmospheric
138 pressure. The oven used has a capacity of 48 liters and internal dimensions of 420 × 350
139 × 330 mm. Sixty test specimens were subjected to heat treatment at one time. Thermal
140 treatment processes of wood specimens are given in Table 1.

141 **Table 1:** Thermal treatment processes.

Thermal treatment stages	Temperature (°C)	Duration (h)	Total duration (h)
Drying	103	30 to 36	40 to 47
Thermal treatment	140, 160, 180, and 200	7 and 9	
Cooling	-	2 to 4	

142

143 The specimens were separately thermally treated at target temperatures for 7 h

144 and 9 h. After thermal treatment, wood specimens hold in a conditioning cabin (relative
145 humidity (RH) 65 ± 3 % and 20 ± 2 °C) until they reached a stable weight, and then they
146 were cut to the dimensions of 20 mm \times 320 mm (tangential direction \times longitudinal
147 direction) and thicknesses 20 mm (for non-compressed specimens), 25 mm, and 33,3 mm
148 (radial direction). Wood thicknesses were prepared differently in order to achieve the
149 targeted compression ratios (20 % and 40 %).

150 **Densification of wood specimens**

151 The thermally pre-treated specimens were densified *via* custom-made metal molds in
152 laboratory test press. The compression parameters used for the densification process of
153 the wood specimens are given in Table 2.

154 **Table 2:** Densification parameters.

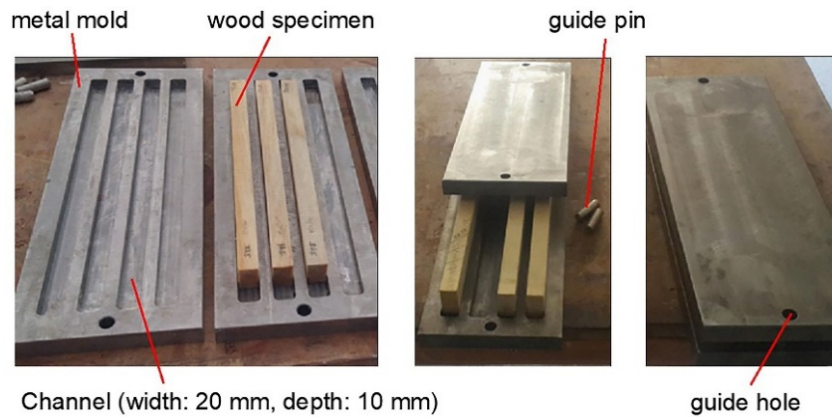
Parameter	Value
Compression temperature (°C)	150
Compression ratio (%)	20 and 40
Pre-heating time (min)	20
Closing rate (mm min ⁻¹)	60
Compressed holding time (min)	10

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156 The wood specimens were first placed in the channels opened on the surfaces of
157 the metal molds (Figure 1). Before compression, specimens were preheated for 20 min.
158 at target temperature. The specimens were then compressed with a speed of 60 mm min⁻¹
159 ¹ and in the radial direction. The load was applied until the metal molds made contact to
160 reach the target thickness of 20 mm in wood specimens (Figure 2). The compressed
161 spruce and poplar specimens were hold at 150 °C for 10 minutes. The specimens were
162 then cooled to room temperature under pressure to minimize the spring-back formation.

163 Densified specimens were conditioned at RH 65 % and 20 °C until they reached
164 a stable weight. The thermally pre-treated and densified specimens were then sized in line

165 with the standards of the applied tests and in a number providing ten repetitions ($n = 10$)
166 for each group.

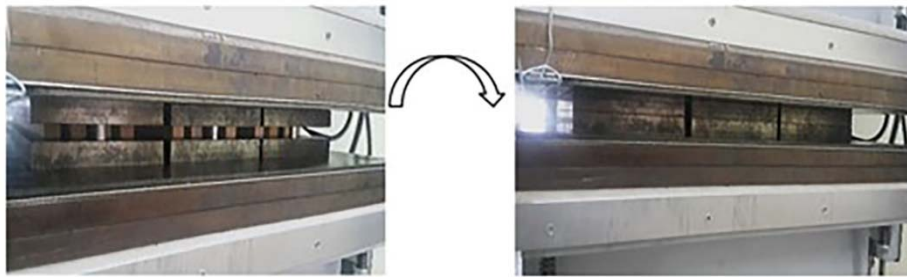
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Figure 1: Position of wood specimens in metal molds.



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Figure 2: Compression of wood specimens with metal molds in a hot press.

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173 **Determination of dimensional change and hygroscopicity properties**

174 Compressed wood tends to return to its initial dimensions after the opening of press due
175 to shape memory effect. This phenomenon is referred to as spring-back and causes a
176 change in the target compression ratio. The actual compression ratio (or compression-set)
177 of the compressed wood specimens was calculated using equation 1, and spring-back
178 values were calculated using equation 2:

$$179 \quad \text{Compression ratio (\%)} = \frac{T_0 - T_c}{T_0} \times 100 \quad (1)$$

180

$$181 \quad \text{Spring - back (\%)} = \frac{T_c - T_t}{T_t} \times 100 \quad (2)$$

182

183 where T_o is the initial thickness (mm) of specimens before compression, T_c is the
184 thickness (mm) of specimens kept at $20\text{ }^\circ\text{C} \pm 2\text{ }^\circ\text{C}$ and $65\% \pm 3\%$ RH for eight weeks
185 (until reaching a stable weight) after compression, T_i is the thickness (mm) under pressure
186 (target).

187 Equilibrium moisture content (EMC) was determined in line with ISO 13061-1
188 (ISO 2014), and calculated using by equation 3:

$$189 \quad \text{EMC (\%)} = \frac{W_c - W_d}{W_d} \times 100 \quad (3)$$

190 where W_c is the weight (g) of specimens conditioned at $20\text{ }^\circ\text{C} \pm 2\text{ }^\circ\text{C}$ and RH $65\% \pm 3\%$
191 for eight weeks and W_d is the weight (g) of specimens after keeping in a heated oven ($103\text{ }^\circ\text{C} \pm 2\text{ }^\circ\text{C}$)
192 for 72 h.

194 The set-recovery values of the densified specimens after soaking in water was
195 determined using equation 4:

$$196 \quad \text{Set - recovery (\%)} = \frac{T_m - T_c}{T_o - T_c} \times 100 \quad (4)$$

197 where T_m is the thickness (mm) of specimens after immersion in water for two weeks.

199 Thickness swelling of test specimens was analyzed in line with ISO 13061-15
200 (ISO 2017), and calculated using equation 5:

$$201 \quad \text{Thickness swelling (\%)} = \frac{T_m - T_d}{T_d} \times 100 \quad (5)$$

202 where T_d is the thickness (mm) of specimens after waiting at $103\text{ }^\circ\text{C} \pm 2\text{ }^\circ\text{C}$ for 72 h.

204 Water absorption was calculated using equation 6:

$$205 \quad \text{Water absorption (\%)} = \frac{W_m - W_d}{W_d} \times 100 \quad (6)$$

206 where W_m is the weight (g) of specimens after immersion in water for two weeks.

207 **Statistical analysis**

208 Analysis of variance (ANOVA) tests were performed to determine the impact of thermal
209 pretreatments on the dimensional stability and hygroscopicity of densified spruce and
210 poplar specimens at the 0,05 significance level. Then the mean values of the tested
211 properties of the modified wood specimens were compared separately.

212 **RESULTS AND DISCUSSION**

213 Thickness of the specimens before and after the compression, actual compression ratio,
214 spring-back and density values of thermally pre-treated and densified wood specimens
215 are given in Table 3 and Table 4. The results showed that spring-back occurred at different
216 rates depending on the thermal pretreatment conditions and compression ratios after the
217 pressing process in the densified specimens. There was a decrease in the targeted
218 compression ratios depending on the spring-back ratios in the wood specimens. Spring-
219 back values increased with increasing compression ratio in both thermally pre-treated and
220 untreated wood specimens. Spring-back increased by 68 % and 92 %, respectively, in 40
221 % compressed spruce and poplar specimens compared to 20 %. Due to the increase in
222 compression ratio, the internal stresses increase in densified wood, thus leading to higher
223 spring-back values (Laine *et al.* 2013, Nairn 2006, Pelit *et al.* 2014, Wolcott *et al.* 1989).

224 Thermal pretreatment conditions affected the springback ratios of the densified
225 wood specimens differently. At lower temperatures (140 °C and 160 °C), the springback
226 ratios of the thermally treated specimens generally tend to increase compared to the
227 untreated specimens. These results were similar to results obtained by Kariz *et al.* (2017).
228 However, as of the 180 °C limit, the spring-back values of the specimens decreased due
229 to the increase in thermal treatment temperature and time. Compared to the untreated
230 samples, the spring-back ratio decreased up to 10 % and 31 %, respectively, in the spruce
231 and poplar specimens that were thermally treated at 200 °C for 9 h (Table 3 and 4).
232 Reducing the internal stresses that occur in wood specimens due to the effect of high

233 pressure during the pressing stage by thermal pretreatments and the decrease in the EMC
 234 of the thermally pre-treated specimens may affect the results. Furthermore, previous
 235 studies noted that thermal degradations that occur especially in hemicellulose compound
 236 with the effect of temperature play a key role in the elimination of spring-back in densified
 237 wood (Dwianto *et al.* 1997, Heger *et al.* 2004, Morsing 2000).

238 Density values of densified wood specimens increased depending on thermal
 239 pretreatment conditions and compression ratio. As a result of the increase in the
 240 compression ratio, the density of the spruce and poplar specimens increased by 45 % and
 241 46 %, respectively, compared to the control samples (Tables 3 and 4). The rate of increase
 242 in the density of mechanically compressed wood generally depends on the level of
 243 compression, spring-back effect and characteristics of the wood species (Rautkari 2012,
 244 Pelit *et al.* 2014).

245 **Table 3:** Properties of thermally pre-treated and densified spruce wood ($n=10$).

Thermal treatment	Compression ratio (%)	Initial thickness (mm)	Final thickness (mm)	Actual compression ratio (%)	Spring-back (%)	Density (kg/m ³)	Increase in density (%)
Untreated	Non-compressed	20	20	-	-	382 (37)	-
	20	24,98 (0,22)	21,31 (0,17)	14,68 (0,74)	6,55 (0,84)	434 (27)	13,6
	40	32,86 (0,24)	22,03 (0,22)	32,94 (0,85)	10,16 (1,08)	555 (75)	45,3
140 °C / 7 h	20	24,87 (0,30)	21,29 (0,16)	14,38 (1,08)	6,46 (0,78)	426 (26)	11,5
	40	32,66 (0,25)	22,25 (0,21)	31,88 (1,02)	11,24 (1,07)	530 (59)	38,7
140 °C / 9 h	20	24,91 (0,25)	21,17 (0,12)	15,02 (1,11)	5,85 (0,59)	438 (24)	14,7
	40	32,56 (0,19)	22,14 (0,17)	32,01 (0,67)	10,69 (0,87)	541 (55)	41,6
160 °C / 7 h	20	24,84 (0,25)	21,33 (0,13)	14,13 (0,66)	6,67 (0,67)	432 (36)	13,1
	40	32,51 (0,36)	22,24 (0,20)	31,57 (1,04)	11,21 (0,98)	525 (74)	37,4
160 °C / 9 h	20	24,78 (0,24)	21,30 (0,09)	14,04 (0,98)	6,50 (0,43)	417 (48)	9,2
	40	32,62 (0,25)	22,16 (0,22)	32,07 (1,03)	10,79 (1,12)	516 (33)	35,1
180 °C / 7 h	20	24,81 (0,20)	21,28 (0,08)	14,22 (0,56)	6,41 (0,41)	417 (28)	9,2
	40	32,49 (0,55)	22,07 (0,20)	32,04 (1,47)	10,37 (1,00)	519 (27)	35,9
180 °C / 9 h	20	24,69 (0,25)	21,21 (0,10)	14,07 (0,72)	6,06 (0,49)	414 (25)	8,4
	40	32,37 (0,52)	22,08 (0,13)	31,76 (1,33)	10,39 (0,64)	512 (63)	34,0
200 °C / 7 h	20	24,64 (0,27)	21,23 (0,08)	13,86 (0,83)	6,14 (0,42)	411 (29)	7,6
	40	32,46 (0,41)	21,98 (0,19)	32,27 (0,67)	9,91 (0,95)	495 (45)	29,6
200 °C / 9 h	20	24,70 (0,21)	21,18 (0,07)	14,25 (0,78)	5,88 (0,34)	411 (41)	7,6
	40	32,49 (0,34)	22,00 (0,20)	32,27 (0,79)	10,02 (1,01)	492 (58)	28,8

All values are measurement results of specimens conditioned at RH 65 % and 20 °C.
 Values in parentheses are standard deviations.

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Table 4: Properties of thermally pre-treated and densified poplar wood ($n=10$).

Thermal treatment	Compression ratio (%)	Initial thickness (mm)	Final thickness (mm)	Actual compression ratio (%)	Spring-back (%)	Density (kg/m ³)	Increase in density (%)
Untreated	Non-compressed	20	20	-	-	404 (10)	-
	20	25,19 (0,15)	21,46 (0,09)	14,78 (0,55)	7,31 (0,46)	472 (22)	16,8
	40	33,39 (0,08)	22,65 (0,34)	32,18 (0,92)	13,23 (1,72)	589 (30)	45,8
140 °C / 7 h	20	25,09 (0,07)	21,44 (0,10)	14,52 (0,48)	7,22 (0,50)	463 (25)	14,6
	40	33,29 (0,13)	22,93 (0,33)	31,13 (0,98)	14,64 (1,63)	570 (29)	41,1
140 °C / 9 h	20	25,09 (0,04)	21,57 (0,09)	14,03 (0,41)	7,87 (0,46)	452 (19)	11,9
	40	33,21 (0,22)	22,90 (0,25)	31,05 (0,91)	14,49 (1,26)	573 (38)	41,8
160 °C / 7 h	20	25,02 (0,11)	21,42 (0,19)	14,37 (0,84)	7,11 (0,93)	461 (25)	14,1
	40	33,22 (0,12)	22,86 (0,28)	31,17 (0,76)	14,31 (1,39)	571 (23)	41,3
160 °C / 9 h	20	24,97 (0,12)	21,52 (0,11)	13,82 (0,77)	7,62 (0,54)	461 (28)	14,1
	40	33,21 (0,09)	22,78 (0,35)	31,42 (1,05)	13,89 (1,73)	560 (30)	38,6
180 °C / 7 h	20	24,92 (0,17)	21,32 (0,13)	14,45 (0,63)	6,60 (0,65)	461 (29)	14,1
	40	33,11 (0,10)	22,46 (0,26)	32,17 (0,79)	12,31 (1,29)	556 (29)	37,6
180 °C / 9 h	20	24,90 (0,12)	21,17 (0,14)	14,98 (0,44)	5,83 (0,71)	456 (24)	12,9
	40	33,06 (0,16)	22,40 (0,18)	32,26 (0,41)	11,99 (0,88)	557 (25)	37,9
200 °C / 7 h	20	24,69 (0,18)	21,06 (0,09)	14,68 (0,59)	5,32 (0,46)	438 (27)	8,4
	40	32,84 (0,18)	22,03 (0,17)	32,92 (0,52)	10,14 (0,85)	545 (25)	34,9
200 °C / 9 h	20	24,73 (0,11)	21,01 (0,08)	15,03 (0,45)	5,05 (0,40)	435 (30)	7,7
	40	32,85 (0,13)	21,96 (0,11)	33,15 (0,40)	9,78 (0,56)	535 (36)	32,4

All values are measurement results of specimens conditioned at RH 65 % and 20 °C.
 Values in parentheses are standard deviations.

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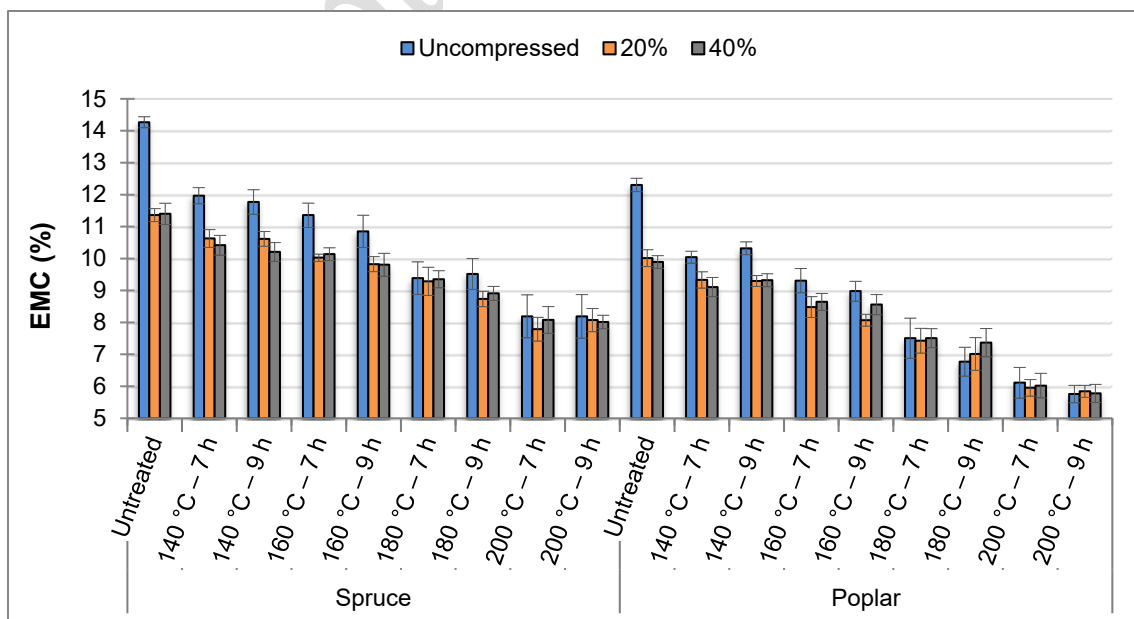
It was observed that the thermal pretreatment temperature and time affected the density values of the wood specimens. Density values generally tend to decrease with increasing temperature and time. This is more evident in 40 % compressed wood specimens. Compared to the untreated samples, the density of the densified spruce and poplar specimens, which were thermally pre-treated for 9 h at 200 °C, decreased by 11 % and 9 %, respectively (Table 3 and 4). The density reduction of thermally treated wood is mostly due to the destruction of hemicelluloses and mass losses as a result of evaporation of extractives (Boonstra 2008; Esteves and Pereira 2009). In addition, it can be said that the lower initial density and decreases in the EMC of thermally treated wood specimens has an effect on the air-dry density results (Kariz *et al.* 2017, Pelit and Yorulmaz 2019).

260 The ANOVA results for EMC, water absorption, thickness swelling, and set-
 261 recovery values of thermally pre-treated and densified specimens are shown in Table 5.
 262 According to the results, the effect of thermal treatment conditions and compression ratio
 263 on tested properties of spruce and poplar specimens was statistically significant ($p \leq$
 264 0,05). However, only for spruce wood, the effect of thermal treatment conditions on water
 265 absorption was no found to be significant (Table 5).

266 **Table 5:** ANOVA results for tested properties of thermally pre-treated and densified
 267 wood specimens.

Tests	Source	Spruce		Poplar	
		F ratio	p value	F ratio	p value
EMC	Thermal treatment (A)	458,5648	0,0000*	810,5218	0,0000*
	Compression ratio (B)	232,0087	0,0000*	99,0298	0,0000*
	Interaction (A×B)	20,0875	0,0000*	21,9468	0,0000*
Water absorption	Thermal treatment (A)	1,1963	ns	17,3151	0,0000*
	Compression ratio (B)	104,1394	0,0000*	48,6578	0,0000*
	Interaction (A×B)	0,8497	ns	0,4909	ns
Thickness swelling	Thermal treatment (A)	133,0360	0,0000*	339,3149	0,0000*
	Compression ratio (B)	11128,3401	0,0000*	11443,0455	0,0000*
	Interaction (A×B)	37,5094	0,0000*	101,9875	0,0000*
Set-recovery	Thermal treatment (A)	105,9681	0,0000*	483,6466	0,0000*
	Compression ratio (B)	62,1283	0,0000*	33,2390	0,0000*
	Interaction (A×B)	1,3664	ns	4,0171	0,0000*

*: significant at 95 % confidence level; ns: not significant



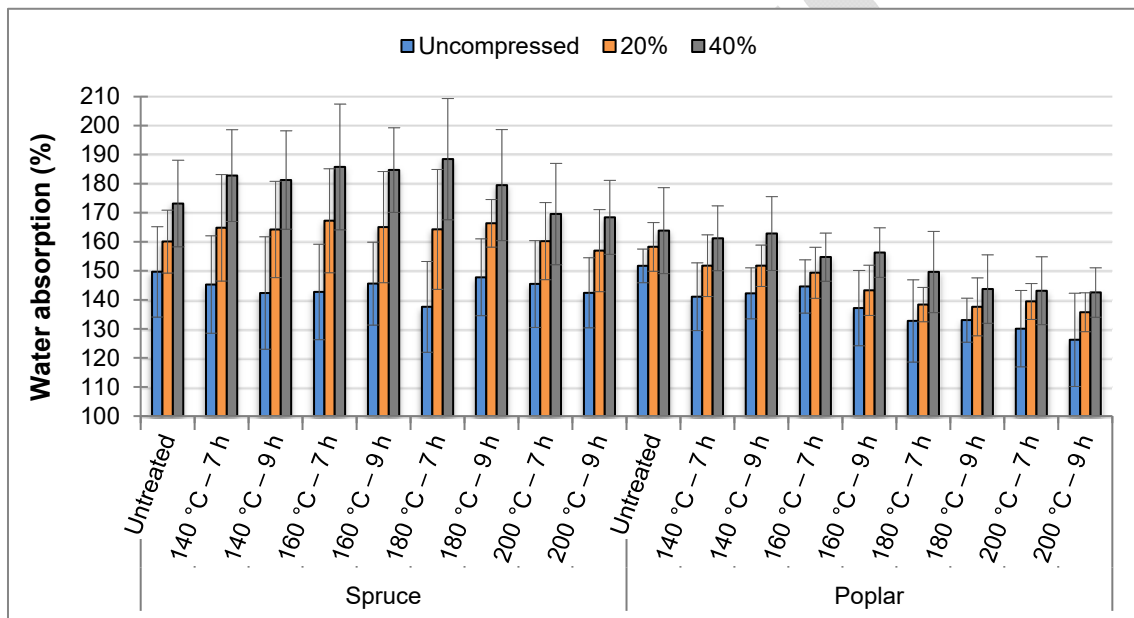
268 **Figure 3:** EMC values of thermally pre-treated and densified spruce and poplar specimens
 269 (n=10).
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271 Figure 3 results showed that EMC values were generally lower in densified
272 specimens compared to uncompressed specimens. This was quite evident in untreated and
273 thermally pre-treated specimens at low temperatures (140 °C and 160 °C). However, no
274 obvious difference was observed between the EMC values of the thermally pre-treated
275 uncompressed and densified specimens at 180 °C and especially at 200 °C. Also, the
276 compression ratio (20 % or 40 %) has no significant effect on the EMC values of both
277 thermally treated and untreated specimens (Figure 3).

278 On the other hand, EMC values of spruce and poplar specimens decreased with
279 increasing thermal pretreatment temperature and time. It was observed that the
280 temperature effect was more important than the time effect on the results. Thermal
281 treatment showed a similar effect in both uncompressed and densified wood specimens
282 (Figure 3). Compared to untreated specimens, the mean EMC of spruce and poplar wood
283 thermally treated at 200 °C decreased by 43 % and 52 % for uncompressed specimens,
284 and 30 % and 41 % for densified specimens, respectively. For EMC, the effect of thermal
285 pretreatment is more pronounced in poplar wood. The hygroscopic behavior of wood is
286 related to the -OH groups in the cell wall structure. -OH groups are present in
287 hemicelluloses, cellulose, and lignin as alcohols, as well as in lignin as phenolic groups.
288 Hemicelluloses are the component with the highest sorptive properties, followed by
289 cellulose and lignin. Thermal modification of wood causes a reduction of OH content
290 (mainly due to hemicelluloses degradation); therefore, it is expected that the EMC will
291 be lower compared to untreated wood (Boonstra 2016, Gérardin 2016, Hill *et al.* 2021).

292 According to Figure 4, water absorption of both thermally pre-treated and
293 untreated spruce and poplar specimens were higher than uncompressed specimens after
294 densification. In addition, water absorption was detected higher in specimens densified
295 with high compression ratio (40 %). This effect is more pronounced in spruce specimens.

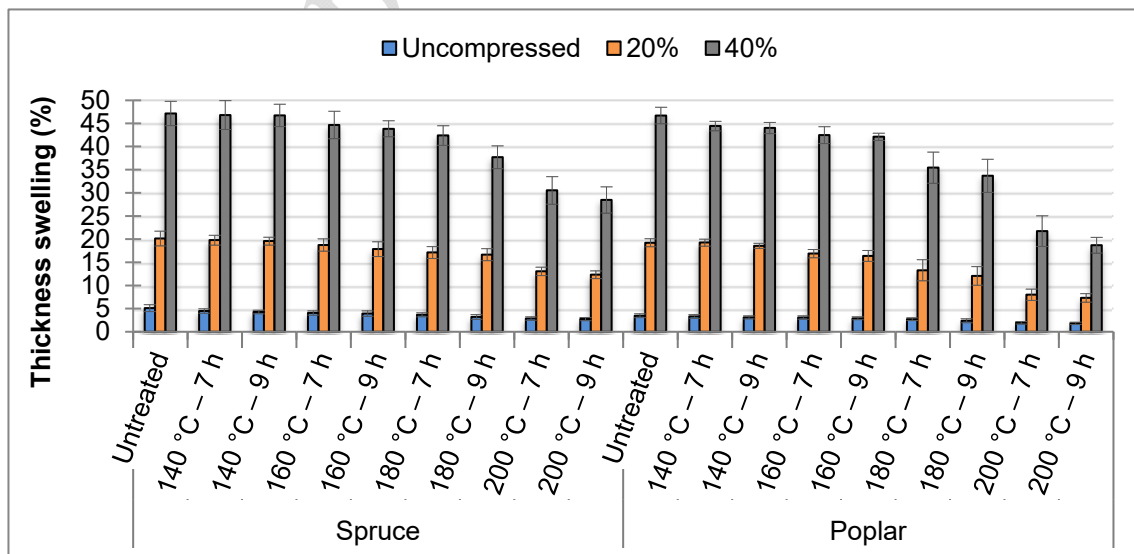
296 For both wood species, the effect of compression ratio on water absorption tended to
 297 decrease with the increase in thermal pretreatment temperature, and closer values were
 298 measured in both compression ratios. In the study reported by Pelit *et al.* (2016), thermal
 299 post-treatments were applied to thermo-mechanically densified fir and poplar wood
 300 specimens. Similarly, water absorption increased with increasing compression ratio in
 301 densified specimens. However, contrary to the present study, especially in specimens
 302 densified at high compression ratio, lower water absorption was obtained after thermal
 303 post-treatment. Thus, it has been observed that the thermal treatment application stage
 304 (before or after densification) affects the water absorption results.



305
 306 **Figure 4:** Water absorption values of thermally pre-treated and densified spruce and poplar
 307 specimens ($n=10$).

308 For spruce wood, thermal treatment applications caused a decrease in water
 309 absorption values of uncompressed specimens. However, water absorption tends to
 310 increase in densified spruce specimens as a result of the increase in thermal pretreatment
 311 temperature up to 200 °C. In spruce specimens pre-treated at 200 °C, water absorption
 312 was slightly decreased compared to untreated specimens (Figure 4). However, ANOVA
 313 results showed that the effect of thermal treatments on water absorption of spruce
 314

315 specimens was not significant (Table 5). For poplar wood, both uncompressed and
 316 densified specimens showed a decrease in water absorption values depending on increase
 317 in thermal treatment temperature (Figure 4). Compared to untreated specimens, water
 318 absorption was decreased by 17 % and 14 %, respectively, in uncompressed and densified
 319 poplar specimens thermally treated at 200 °C. In addition, it was determined that the
 320 thermal treatment time had a limited effect on the water absorption values of the
 321 specimens. The main components (cellulose, hemicelluloses and lignin) of the wood cell
 322 wall contain free hydroxyl groups (OH) that attract and hold water by hydrogen bonding.
 323 The accessibility of OH groups in the chemical components of wood (especially
 324 hemicelluloses) plays an important role in the desorption and water adsorption process
 325 (Boonstra 2016). Thermal treatment of wood results in a reduction in the accessible OH
 326 content and reduces the content of bound water held in the wood cell wall (Hill *et al.*
 327 2021). On the other hand, the most important parameters in thermal modification are
 328 treatment temperature and time, but on many wood properties, temperature is more
 329 dominant than treatment time (Bekhta and Niemz 2003, Tjeerdsma and Militz 2005,
 330 Kartal *et al.* 2007, Esteves *et al.* 2008).

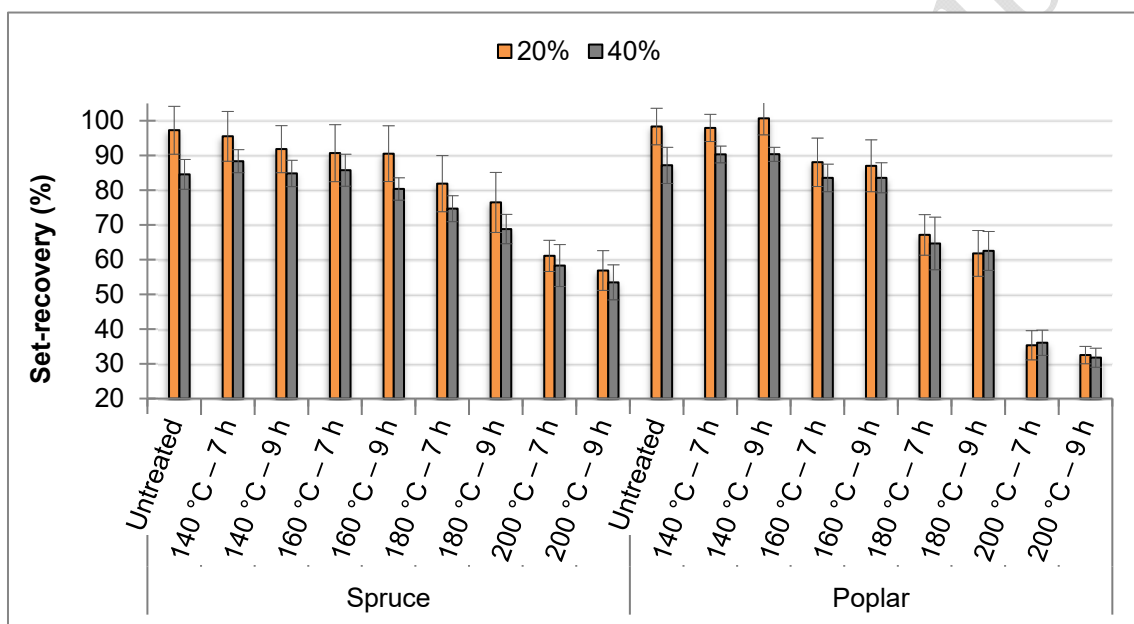


331 **Figure 5:** Thickness swelling values of thermally pre-treated and densified spruce and
 332 poplar specimens ($n=10$).
 333

334 Thickness swelling values were found to be significantly higher in densified wood
335 specimens compared to uncompressed specimens. Also, thickness swelling increased
336 with increasing compression ratio in all densified specimens (Figure 5). These determined
337 results are compatible with the findings of previous studies (Cai *et al.* 2013, Pelit *et al.*
338 2016, Pelit and Emiroglu 2020, Budakçı *et al.* 2021). It is known that the compressed
339 wood tends to revert to its initial dimensions before compression under high humidity
340 conditions or in contact with water. This is caused by the extension of the cell wall, the
341 relaxation of stresses occurring in the wood structure due to compression, and the
342 tendency of the cell wall to revert to its original state, especially due to shape memory
343 (Kollmann *et al.* 1975, Morsing 2000, Seborg *et al.* 1956).

344 The thickness swelling of both uncompressed and densified specimens decreased
345 and dimensional stability increased depending on the increase in thermal treatment
346 temperature and time. More successful results were obtained in thermally pre-treated
347 poplar specimens. In addition, it was determined that the temperature effect was more
348 significant on the thickness swelling than the thermal treatment time (Figure 5).
349 Compared to untreated specimens, thickness swelling was reduced by up to 40 % and 62
350 %, respectively, in spruce and poplar specimens that were thermally pre-treated for 9
351 hours at 200 °C. Kocaefe *et al.* (2015) reported several factors that cause an decrease in
352 the dimensional change of thermally treated wood. These include the mass loss of
353 hygroscopic hemicellulose polymers causing reduction of hydroxyl groups, cross-linking
354 of aromatic rings in lignin, and cross-linking or bridging of cellulose chains due to
355 separation of two hydroxyl groups on adjacent cellulose chains. Also, the overall swelling
356 of the wood is reduced as a result of the reduction in water absorption after thermal
357 treatment, thus increasing its dimensional stability (Boonstra 2016).

358 The set-recovery was higher in the specimens that were densified at 20 %
 359 compression ratio compared to the specimens densified with 40 % compression ratio in
 360 both untreated and thermally pre-treated wood specimens. The higher set-recovery at the
 361 lower compression ratio is similar to the results of previous studies reported (Kariz *et al.*
 362 2017, Pelit *et al.* 2016, Pelit and Emiroglu 2020). However, the effect of compression
 363 ratio on set-recovery decreased due to temperature increase in thermal pre-treated
 364 specimens and closer values were determined for both compression ratios (Figure 6).



365
 366 **Figure 6:** Set-recovery values of thermally pre-treated and densified spruce and poplar
 367 specimens (n=10).

368 Regarding the thermal pretreatment conditions, the set-recovery values of the
 369 untreated and low-temperature thermally treated specimens were found to be quite high,
 370 and the densified specimens almost completely reached their initial dimensions before
 371 compression. However, with the increase in thermal pretreatment temperature and time,
 372 set-recovery decreased significantly, especially in poplar wood specimens. As in the other
 373 test results, it was determined that the thermal treatment temperature had a more
 374 significant effect on the set-recovery than the thermal treatment time (Figure 6).
 375 Compared to untreated specimens, set-recovery was reduced by up to 42 % and 67 %,
 376

377 respectively, in spruce and poplar specimens that were thermally pre-treated for 9 hours
378 at 200 °C. It can be said that the break-down of the cross-links, which are responsible for
379 the shape memory of wood, by thermal treatments is effective on the results (Inoue *et al.*
380 2008, Laine *et al.* 2013, Navi and Heger 2004, Pelit *et al.* 2014). In addition, the fact that
381 the rate of internal stresses occurring in the wood during the pressing process is lower in
382 thermally pre-treated specimens may have an effect on the set-recovery.

383 CONCLUSIONS

384 In the present study, the impact of thermal pretreatments on the dimensional
385 change and humidity sensitivity of densified spruce and poplar wood specimens were
386 analyzed. Spring-back and thickness swelling values increased due to the increase in
387 compression ratio in both thermally pre-treated and untreated wood specimens. On the
388 other hand, set-recovery was determined higher in specimens densified at 20 %
389 compression ratio compared to 40 % compression ratio. However, the effect of
390 compression ratio on set-recovery decreased as the thermal pretreatment temperature
391 increased. Water absorption values increased significantly in all densified specimens
392 (especially spruce specimens) depending on the compression ratio. After densification,
393 the EMC of the untreated and thermally pre-treated specimens at low temperatures (140
394 °C and 160 °C) were significantly lower than the uncompressed samples. However, the
395 EMC values of the thermally pre-treated specimens (uncompressed ve densified),
396 especially at 200 °C, were found to be similar. In addition, compression ratio had no
397 significant effect on EMC values. After densification, the density of the spruce and poplar
398 specimens increased up to 45 % and 46 %, respectively, with the increase in compression
399 ratio.

400 Thermal pretreatments have a significant effect on the tested properties of
401 densified wood specimens. Spring-back, set-recovery and thickness swelling decreased

402 and dimensional stability of specimens (especially poplar) increased depending on the
403 increase in thermal pretreatment temperature and time. Compared to the untreated
404 specimens, spring-back decreased up to 10 % and 31 %, set-recovery up to 42 % and 67
405 %, and thickness swelling up to 40 % and 62 %, respectively, in the spruce and poplar
406 specimens, which were thermally pre-treated at 200 °C for 9 h. On the other hand, EMC
407 and water absorption values of spruce and poplar specimens decreased with increase in
408 thermal pretreatment temperature and time. However, water absorption tends to increase
409 in thermally pre-treated spruce samples at low temperatures. The mean EMC of thermally
410 pre-treated spruce and poplar wood at 200 °C decreased by 30 % and 41 %, respectively.
411 All test results showed that thermal treatment temperature has a more significant effect
412 than thermal treatment time.

413

414 **AUTHORSHIP CONTRIBUTIONS**

415 **H. P.:** Conceptualization, Formal Analysis, Funding acquisition, Investigation,
416 Methodology, Project administration, Resources, Supervision, Visualization, Writing –
417 original draft, Writing – review & editing. **R. Y.:** Investigation, Resources, Writing –
418 original draft, Writing – review & editing.

419

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423

424 **REFERENCES**

425 **Ayata, U.; Akcay, C.; Esteves, B. 2017.** Determination of decay resistance against
426 *Pleurotus ostreatus* and *Coniophora puteana* fungus of heat-treated scotch pine, oak and
427 beech wood species. *Maderas-Cienc Tecnol* 19(3): 309-316.
428 <https://doi.org/10.4067/S0718-221X2017005000026>

- 429 **Aydemir, D.; Gündüz, G.; Altuntaş, E.; Ertas, M.; Şahin, H.T.; Alma, M.H. 2011.**
430 Investigating changes in the chemical constituents and dimensional stability of
431 heat-treated hornbeam and Uludağ fir wood. *BioResources* 6(2): 1308-1321.
432 https://ojs.cnr.ncsu.edu/index.php/BioRes/article/view/BioRes_06_2_1308_Aydemir
433 [GAESA Changes Chem Phys Wood Heat Treat/924](https://doi.org/10.15376/biores.6.2.1308-1321)
434
- 435 **Báder, M.; Bak, M.; Németh, R.; Rousek, R.; Horníček, S.; Dömény, J.; Klímek, P.;**
436 **Rademacher, P.; Kudela, J.; Sandberg, D.; Neyses, B.; Kutnar, A.; Wimmer, R.;**
437 **Pfriem, A. 2018.** Wood densification processing for newly engineered materials. In 5th
438 International Conference on Processing Technologies for the Forest and Bio-based
439 Products Industries September 2018, Freising/Munich, Germany. [http://ltu.diva-](http://ltu.diva-portal.org/smash/get/diva2:1259102/FULLTEXT01.pdf)
440 [portal.org/smash/get/diva2:1259102/FULLTEXT01.pdf](http://ltu.diva-portal.org/smash/get/diva2:1259102/FULLTEXT01.pdf)
441
- 442 **Bekhta, P.; Niemz, P. 2003.** Effect of high temperature on the change in color,
443 dimensional stability and mechanical properties of spruce wood. *Holzforschung*
444 57(5): 539-546. <https://doi.org/10.1515/HF.2003.080>
445
- 446 **Boonstra, M.J. 2008.** A two-stage thermal modification of wood, Doctoral Thesis, Co-
447 supervised by Ghent University, Ghent, Belgium, and Université Henry Poincaré, Nancy,
448 France. <https://biblio.ugent.be/publication/468990/file/1880699.pdf>
449
- 450 **Boonstra, M.J. 2016.** Dimensional stabilization of wood and wood composites. Chapter
451 26. In: *Lignocellulosic Fibers and Wood Handbook: Renewable Materials for Today's*
452 *Environment*. Belgacem, N.; Pizzi, A. (eds.). Wiley, Hoboken, NJ, USA.
453 <https://doi.org/10.1002/9781118773727.ch26>
454
- 455 **Boonstra, M.J.; Van Acker, J.; Kegel, E.; Stevens, M. 2007a.** Optimisation of a two-
456 stage heat treatment process: durability aspects. *Wood Sci Technol* 41(1): 31-57.
457 <https://doi.org/10.1007/s00226-006-0087-4>
458
- 459 **Boonstra, M.J.; Van Acker, J.; Tjeerdsma, B.F.; Kegel, E.V. 2007b.** Strength
460 properties of thermally modified softwoods and its relation to polymeric structural wood
461 constituents. *Ann For Sci* 64(7): 679-690. <https://doi.org/10.1051/forest:2007048>
462
- 463 **Budakçı, M.; Şenol, S.; Korkmaz, M. 2021.** Effects of thermo-vibro-mechanic®
464 densification on the density and swelling of pre-treated uludağ fir and black poplar
465 wood. *BioResources* 16(1): 1581-1599. <https://doi.org/10.15376/biores.16.1.1581-1599>
466
- 467 **Cai, J.; Yang, X.; Cai, L.; Shi, S. Q. 2013.** Impact of the combination of
468 densification and thermal modification on dimensional stability and hardness of
469 poplar lumber. *Drying Technol* 31(10): 1107-1113.
470 <https://doi.org/10.1080/07373937.2013.775147>
471
- 472 **Cencin, A.; Zanetti, M.; Urso, T.; Crivellaro, A. 2021.** Effects of an innovative
473 densification process on mechanical and physical properties of beech and Norway spruce
474 veneers. *J Wood Sci* 67: 15(2021). <https://doi.org/10.1186/s10086-021-01948-w>
475
- 476 **Dwianto, W.; Inoue, M.; Norimoto, M. 1997.** Fixation of compressive deformation of
477 wood by heat treatment. *J Jpn Wood Res Soc* 43(4): 303-309.

- 478 [https://www.webofscience.com/wos/woscc/full-](https://www.webofscience.com/wos/woscc/full-record/WOS:A1997XD6540001?SID=D3I4CwJenYn9Z1okONA)
479 [record/WOS:A1997XD6540001?SID=D3I4CwJenYn9Z1okONA](https://www.webofscience.com/wos/woscc/full-record/WOS:A1997XD6540001?SID=D3I4CwJenYn9Z1okONA)
480
- 481 **Dubey, M.K.; Pang, S.; Walker, J. 2012.** Changes in chemistry, color, dimensional
482 stability and fungal resistance of *Pinus radiata* D. Don wood with oil heat treatment.
483 *Holzforschung* 66: 49–57. <https://doi.org/10.1515/HF.2011.117>
484
- 485 **Esteves, B.; Velez, M.A.; Domingos, I.; Pereira, H. 2007.** Influence of steam heating
486 on the properties of pine (*Pinus pinaster*) and eucalypt (*Eucalyptus globulus*) wood.
487 *Wood Sci Technol* 41(3): 193-207. <https://doi.org/10.1007/s00226-006-0099-0>
488
- 489 **Esteves, B.; Domingos, I.; Pereira, H. 2008.** Pine wood modification by heat treatment
490 in air. *BioResources* 3(1): 142-154.
491 [https://ojs.cnr.ncsu.edu/index.php/BioRes/article/view/BioRes_03_1_0142_Esteves_DP](https://ojs.cnr.ncsu.edu/index.php/BioRes/article/view/BioRes_03_1_0142_Esteves_DP_PineWoodMod/173)
492 [_PineWoodMod/173](https://ojs.cnr.ncsu.edu/index.php/BioRes/article/view/BioRes_03_1_0142_Esteves_DP_PineWoodMod/173)
493
- 494 **Esteves, B.M.; Pereira, H. M. 2009.** Wood modification by heat treatment: A review.
495 *BioResources* 4(1): 370-404. <https://doi.org/10.15376/biores.4.1.370-404>
496
- 497 **Fang, C.H.; Cloutier, A.; Jiang, Z.H.; He, J.Z.; Fei, B.H. 2019.** Improvement of
498 wood densification process *via* enhancing steam diffusion, distribution, and
499 evaporation. *BioResources* 14(2): 3278-3288.
500 [https://ojs.cnr.ncsu.edu/index.php/BioRes/article/view/BioRes_14_2_3278_Fang_Impro](https://ojs.cnr.ncsu.edu/index.php/BioRes/article/view/BioRes_14_2_3278_Fang_Improvement_Densification_Process_Steam/6721)
501 [vement_Densification_Process_Steam/6721](https://ojs.cnr.ncsu.edu/index.php/BioRes/article/view/BioRes_14_2_3278_Fang_Improvement_Densification_Process_Steam/6721)
502
- 503 **Gabrielli, C.P.; Kamke, F.A. 2010.** Phenol-formaldehyde impregnation of densified
504 wood for improved dimensional stability. *Wood Sci Technol* 44(1): 95–104.
505 <https://doi.org/10.1007/s00226-009-0253-6>
506
- 507 **Gao, Z.; Huang, R.; Chang, J.; Li, R.; Wu, Y. 2019.** Effects of pressurized
508 superheated-steam heat treatment on set recovery and mechanical properties of
509 surface-compressed wood. *BioResources* 14(1): 1718-1730.
510 [https://ojs.cnr.ncsu.edu/index.php/BioRes/article/view/BioRes_14_1_1718_Gao_Pressu](https://ojs.cnr.ncsu.edu/index.php/BioRes/article/view/BioRes_14_1_1718_Gao_Pressurized_Superheated_Steam_Treatment)
511 [rized_Superheated_Steam_Treatment](https://ojs.cnr.ncsu.edu/index.php/BioRes/article/view/BioRes_14_1_1718_Gao_Pressurized_Superheated_Steam_Treatment)
512
- 513 **Gérardin, P. 2016.** New alternatives for wood preservation based on thermal and
514 chemical modification of wood—a review. *Ann For Sci* 73(3): 559-570.
515 <https://doi.org/10.1007/s13595-015-0531-4>
516
- 517 **González-Peña, M.M.; Hale, M.D. 2009.** Colour in thermally modified wood of beech,
518 Norway spruce and Scots pine. Part 1: Colour evolution and colour changes.
519 *Holzforschung* 63: 385–393. <https://doi.org/10.1515/HF.2009.078>
520
- 521 **Fukuta, S.; Asada, F.; Sasaki, Y. 2008.** Manufacture of compressed wood fixed by
522 phenolic resin impregnation through drilled holes. *J Wood Sci* 54(2): 100–106.
523 <https://doi.org/10.1007/s10086-007-0920-x>
524
- 525 **Heger, F.; Groux, M.; Girardet, F.; Welzbacher, C.; Rapp, A.O.; Navi, P. 2004.**
526 Mechanical and durability performance of THM-densified wood. Proc. Final

- 527 Workshop COST Action E22 Environmental Optimization of Wood Protection
528 Lisbon, Portugal.
529
- 530 **Hill, C.A.S. 2006.** *Wood Modification: Chemical, Thermal and Other Processes*, John
531 Wiley & Sons, Chichester, United Kingdom. <https://doi.org/10.1002/0470021748>
532
- 533 **Hill, C.; Altgen, M.; Rautkari, L. 2021.** Thermal modification of wood—A review:
534 Chemical changes and hygroscopicity. *J Mater Sci* 56: 6581–6614.
535 <https://doi.org/10.1007/s10853-020-05722-z>
536
- 537 **Inoue, M.; Ogata, S.; Kawai, S.; Rowell, R.M.; Norimoto, M. 1993.** Fixation of
538 compressed wood using melamine-formaldehyde resin. *Wood Fiber Sci* 25(4): 404-410.
539 <https://wfs.swst.org/index.php/wfs/article/view/623>
540
- 541 **Inoue, M.; Sekino, N.; Morooka, T.; Rowell, R.M.; Norimoto, M. 2008.** Fixation of
542 compressive deformation in wood by pre-steaming. *J Trop For Sci* 20(4): 273-281.
543 https://www.fpl.fs.fed.us/documnts/pdf2008/fpl_2008_inoue001.pdf
544
- 545 **International Organization for Standardization. 2014.** Physical and mechanical
546 properties of wood – Test methods for small clear wood specimens – Part 1:
547 Determination of moisture content for physical and mechanical tests. ISO 13061-1. ISO.
548 Geneva, Switzerland. <https://www.iso.org/standard/60063.html>
549
- 550 **International Organization for Standardization. 2017.** Physical and mechanical
551 properties of wood – Test methods for small clear wood specimens – Part 15:
552 Determination of radial and tangential swelling. ISO 13061-15. ISO. Geneva,
553 Switzerland. <https://www.iso.org/standard/60077.html>
554
- 555 **Jones, D.; Sandberg, D.; Goli, G.; Todaro, L. 2019.** *Wood modification in Europe: A*
556 *state-of-the-art about processes, products, applications*. Firenze University Press,
557 Florence, Italy. <https://doi.org/10.36253/978-88-6453-970-6>
558
- 559 **Kariz, M.; Kuzman, M.K.; Sernek, M.; Hughes, M.; Rautkari, L.; Kamke, F.A.;**
560 **Kutnar, A. 2017.** Influence of temperature of thermal treatment on surface
561 densification of spruce. *Eur J Wood Prod* 75(1): 113-123.
562 <https://doi.org/10.1007/s00107-016-1052-z>
563
- 564 **Kartal, S.N.; Hwang, W.J.; Imamura, Y. 2007.** Water absorption of boron-treated and
565 heat-modified wood. *J Wood Sci* 53(5): 454-457. [https://doi.org/10.1007/s10086-007-](https://doi.org/10.1007/s10086-007-0877-9)
566 [0877-9](https://doi.org/10.1007/s10086-007-0877-9)
567
- 568 **Kaygın, B.; Gündüz, G.; Aydemir, D. 2009.** Some physical properties of heat treated
569 paulownia (*Paulownia elongata*) wood. *Drying Technol* 27(1): 89-93.
570 <https://doi.org/10.1080/07373930802565921>
571
- 572 **Kocaefe, D.; Huang, X.; Kocaefe, Y. 2015.** Dimensional stabilization of wood. *Curr*
573 *For Rep* 1(3): 151-161. <https://doi.org/10.1007/s40725-015-0017-5>
574
- 575 **Kollmann, F.F.P.; Kuenzi, E.W.; Stamm, A.J. 1975.** *Principles of wood science and*
576 *technology. Wood based materials*, II ed. Springer, New York, U.S.A.

- 577 <https://doi.org/10.1007/978-3-642-87931-9>
578
- 579 **Korkut, S.; Kök, M.S.; Korkut, D.S.; Gürleyen, T. 2008.** The effects of heat treatment
580 on technological properties in red-bud maple (*Acer trautvetteri* Medw.)
581 wood. *Bioresour Technol* 99(6): 1538-1543.
582 <https://doi.org/10.1016/j.biortech.2007.04.021>
583
- 584 **Korkut, D.S.; Guller, B. 2008.** The effects of heat treatment on physical properties and
585 surface roughness of red-bud maple (*Acer trautvetteri* Medw.) wood. *Bioresour Technol*
586 99(8): 2846-2851. <https://doi.org/10.1016/j.biortech.2007.06.043>
587
- 588 **Kutnar, A.; Kamke, F.A. 2012.** Influence of temperature and steam environment on set
589 recovery of compressive deformation of wood. *Wood Sci Technol* 46(5): 953-964.
590 <https://doi.org/10.1007/s00226-011-0456-5>
591
- 592 **Laine, K.; Rautkari, L.; Hughes, M.; Kutnar, A. 2013.** Reducing the set-recovery of
593 surface densified solid Scots pine wood by hydrothermal post-treatment.
594 *Eur J Wood Prod* 71(1): 17-23. <https://doi.org/10.1007/s00107-012-0647-2>
595
- 596 **Laskowska, A. 2020.** The influence of ultraviolet radiation on the colour of thermo-
597 mechanically modified beech and oak wood. *Maderas-Cienc Tecnol* 22:55-68.
598 <https://doi.org/10.4067/S0718-221X2020005000106>
599
- 600 **Lekounougou, S.; Kocaefe, D. 2014.** Durability of thermally modified *Pinus banksiana*
601 (Jack pine) wood against brown and white rot fungi. *Int Wood Prod J* 5(2): 92-97.
602 <https://doi.org/10.1179/2042645313Y.0000000057>
603
- 604 **Lykidis, C.; Kotrotsiou, K.; Tsihlakis, A. 2020.** Reducing set-recovery of
605 compressively densified poplar wood by impregnation–modification with melamine–
606 formaldehyde resin. *Wood Mater Sci Eng* 15(5): 269-277.
607 <https://doi.org/10.1080/17480272.2019.1594365>
608
- 609 **Militz, H. 2002.** Thermal treatment of wood: European processes and
610 their background. In The International Research Group on Wood
611 Preservation February 2012, Cardiff, U.K.
612
- 613 **Militz, H. 2005.** Preface of the second European conference on wood modification, In
614 Proceedings for the 2th European Conference on Wood Modification October 2005,
615 Gottingen, Germany.
616
- 617 **Morsing, N. 2000.** Densification of wood - The influence of hygrothermal treatment on
618 compression of beech perpendicular to the grain, Doctoral Thesis, Technical University
619 of Denmark, Lyngby, Denmark.
620 <https://backend.orbit.dtu.dk/ws/portalfiles/portal/5301406/Morsing.pdf>
621
- 622 **Nairn, J.A. 2006.** Numerical simulations of transverse compression and densification in
623 wood. *Wood Fiber Sci* 38(4): 576-591. <https://wfs.swst.org/index.php/wfs/article/view/2>
624
- 625 **Navi, P.; Heger, F. 2004.** Combined densification and thermo-hydro-mechanical
626 processing of wood. *MRS Bull* 29(5): 332-336. <https://doi.org/10.1557/mrs2004.100>

- 627 **Pelit, H. 2017.** The effect of different wood varnishes on surface color properties of heat
628 treated wood materials. *J Fac For Istanbul U* 67(2): 262-274.
629 <https://doi.org/10.17099/jffiu.300010>
630
- 631 **Pelit, H.; Budakçı, M.; Sönmez, A. 2016.** Effects of heat post-treatment on dimensional
632 stability and water absorption behaviours of mechanically densified Uludağ fir and black
633 poplar woods. *BioResources* 11(2): 3215-3229.
634 <https://doi.org/10.15376/biores.11.2.3215-3229>
635
- 636 **Pelit, H.; Emiroglu, F. 2020.** Effect of water repellents on hygroscopicity and
637 dimensional stability of densified fir and aspen woods. *Drv Ind* (1): 29-40.
638 <https://doi.org/10.5552/drvind.2020.1901>
639
- 640 **Pelit, H.; Sönmez, A.; Budakçı, M. 2014.** Effects of ThermoWood® process combined
641 with thermo-mechanical densification on some physical properties of Scots pine (*Pinus*
642 *sylvestris* L.). *BioResources* 9(3): 4552-4567. [https://doi.org/10.15376/biores.9.3.4552-](https://doi.org/10.15376/biores.9.3.4552-4567)
643 [4567](https://doi.org/10.15376/biores.9.3.4552-4567)
644
- 645 **Pelit, H.; Yorulmaz, R. 2019.** Influence of densification on mechanical properties of
646 thermally pretreated spruce and poplar wood. *BioResources* 14(4): 9739-9754.
647 [https://bioresources.cnr.ncsu.edu/resources/influence-of-densification-on-mechanical-](https://bioresources.cnr.ncsu.edu/resources/influence-of-densification-on-mechanical-properties-of-thermally-pretreated-spruce-and-poplar-wood/)
648 [properties-of-thermally-pretreated-spruce-and-poplar-wood/](https://bioresources.cnr.ncsu.edu/resources/influence-of-densification-on-mechanical-properties-of-thermally-pretreated-spruce-and-poplar-wood/)
649
- 650 **Perçin, O.; Peker, H.; Atılgan, A. 2016.** The effect of heat treatment on the some
651 physical and mechanical properties of beech (*Fagus orientalis* lipsky) wood. *Wood Res*
652 61(3): 443-456. <http://www.woodresearch.sk/wr/201603/10.pdf>
653
- 654 **Pleschberger, H.; Teischinger, A.; Müller, U.; Hansmann, C. 2014.** Change in
655 fracturing and colouring of solid spruce and ash wood after thermal modification. *Wood*
656 *Mater Sci Eng* 9(2): 92-101. <https://doi.org/10.1080/17480272.2014.895418>
657
- 658 **Poncsák, S.; Kocaefe, D.; Bouazara, M.; Pichette, A. 2006.** Effect of high temperature
659 treatment on the mechanical properties of birch (*Betula papyrifera*). *Wood Sci*
660 *Technol* 40(8): 647-663. <https://doi.org/10.1007/s00226-006-0082-9>
661
- 662 **Rautkari, L. 2012.** Surface modification of solid wood using different techniques.
663 Doctoral Thesis, Aalto University, Espoo, Finland.
664 [https://aaltodoc.aalto.fi/bitstream/handle/123456789/5259/isbn9789526044651.pdf?seq-](https://aaltodoc.aalto.fi/bitstream/handle/123456789/5259/isbn9789526044651.pdf?sequence=1&isAllowed=y)
665 [uence=1&isAllowed=y](https://aaltodoc.aalto.fi/bitstream/handle/123456789/5259/isbn9789526044651.pdf?sequence=1&isAllowed=y)
666
- 667 **Rautkari, L.; Properzi, M.; Pichelin, F.; Hughes, M. 2010.** Properties and set-recovery
668 of surface densified Norway spruce and European beech. *Wood Sci Technol* 44(4): 679–
669 691. <https://doi.org/10.1007/s00226-009-0291-0>
670
- 671 **Rowell, R.M. 2012.** *Handbook of wood chemistry and wood composites*. CRC Press,
672 Boca Raton, U.S.A.
673 [https://www.taylorfrancis.com/books/mono/10.1201/b12487/handbook-wood-](https://www.taylorfrancis.com/books/mono/10.1201/b12487/handbook-wood-chemistry-wood-composites-roger-rowell)
674 [chemistry-wood-composites-roger-rowell](https://www.taylorfrancis.com/books/mono/10.1201/b12487/handbook-wood-chemistry-wood-composites-roger-rowell)
675

- 676 **Sandberg, D.; Haller, P.; Navi, P. 2013.** Thermo-hydro and thermo-hydro-mechanical
677 wood processing: An opportunity for future environmentally friendly wood
678 products. *Wood Mater Sci Eng* 8(1): 64-88.
679 <https://doi.org/10.1080/17480272.2012.751935>
680
- 681 **Sandberg, D.; Kutnar, A.; Mantanis, G. 2017.** Wood modification technologies-a
682 review. *Iforest* 10(6): 895-908. <https://doi.org/10.3832/ifor2380-010>
683
- 684 **Sandberg, D.; Kutnar, A.; Karlsson, O.; Jones, D. 2021.** *Wood Modification*
685 *Technologies. Principles, Sustainability, and the Need for Innovation.* CRC Press, Boca
686 Raton, U.S.A.
687 [https://www.taylorfrancis.com/books/mono/10.1201/9781351028226/wood-](https://www.taylorfrancis.com/books/mono/10.1201/9781351028226/wood-modification-technologies-dick-sandberg-andreja-kutnar-olov-karlsson-dennis-jones)
688 [modification-technologies-dick-sandberg-andreja-kutnar-olov-karlsson-dennis-jones](https://www.taylorfrancis.com/books/mono/10.1201/9781351028226/wood-modification-technologies-dick-sandberg-andreja-kutnar-olov-karlsson-dennis-jones)
689
- 690 **Seborg, R.M.; Millett, M.A.; Stamm, A.J. 1956.** *Heat-stabilized compressed wood*
691 *(Staypak)*, USDA Forest Service, Forest Products Laboratory, Report No: 1580, Madison,
692 Wisconsin, U.S.A. <https://www.fpl.fs.fed.us/documnts/fplr/fplr1580.pdf>
693
- 694 **Seborg, R.M.; Tarkow, H.; Stamm, A.J. 1962.** *Modified woods.* USDA Forest Service,
695 Forest Products Laboratory, Report No: 2192 (revised), Madison, Wisconsin, U.S.A.
696
- 697 **Sikora, A.; Kačík, F.; Gaff, M.; Vondrová, V.; Bubeníková, T.; Kubovský, I. 2018.**
698 Impact of thermal modification on color and chemical changes of spruce and oak wood. *J*
699 *Wood Sci* 64(4): 406-416. <https://doi.org/10.1007/s10086-018-1721-0>
700
- 701 **Sivrikaya, H.; Tesařová, D.; Jeřábková, E.; Can, A. 2019.** Color change and emission
702 of volatile organic compounds from Scots pine exposed to heat and vacuum-heat
703 treatment. *J Build Eng* 26: 100918. <https://doi.org/10.1016/j.jobe.2019.100918>
704
- 705 **Song, S.; Chen, C.; Zhu, S.; Zhu, M., Dai, J.; Ray, U.; Li, Y.; Kuang, Y.; et al. 2018.**
706 Processing bulk natural wood into a high-performance structural material. *Nature* 554:
707 224-228. <https://doi.org/10.1038/nature25476>
708
- 709 **Thompson, D.W.; Kozak, R.A.; Evans, P.D. 2005.** Thermal modification of color in
710 red alder veneer. I. Effects of temperature, heating time, and wood type. *Wood Fiber*
711 *Sci* 37(4): 653-661. <https://wfs.swst.org/index.php/wfs/article/download/1039/1039/0>
712
- 713 **Tjeerdsma, B.; Militz, H. 2005.** Chemical changes in hydrothermal treated wood: FTIR
714 analysis of combined hydrothermal and dry heat-treated wood. *Holz Roh Werkst* 63(2):
715 102-111. <https://doi.org/10.1007/s00107-004-0532-8>
716
- 717 **Toker, H.; Baysal, E.; Kötekli, M.; Türkoğlu, T.; Kart, Ş.; Şen, F.; Peker, H. 2016.**
718 Surface characteristics of Oriental beech and Scots pine woods heat-treated above 200°C.
719 *Wood Res* 61(1): 43-54. <http://www.woodresearch.sk/wr/201601/05.pdf>
720
- 721 **Torniainen, P.; Jones, D.; Sandberg, D. 2021.** Colour as a quality indicator for
722 industrially manufactured ThermoWood®. *Wood Mater Sci Eng* 16(4): 287-289.
723 <https://doi.org/10.1080/17480272.2021.1958920>
724

- 725 **Ünsal, O.; Büyüksarı, U.; Ayrılmış, N.; Korkut, S. 2009.** Properties of wood and
726 wood based materials subjected to thermal treatments under various conditions.
727 In: Proceedings of International Wood Science and Engineering Conference in the Third
728 Millennium – ICWSE June 2009, Braşov, Romania.
729
- 730 **Wolcott, M.P.; Kasal, B.; Kamke, F.A.; Dillard, D.A. 1989.** Testing small wood
731 specimens in transverse compression. *Wood Fiber Sci* 21(3): 320-
732 329. <https://wfs.swst.org/index.php/wfs/article/download/966/966/0>
733
- 734 **Xu, B.H.; Yu, K.B.; Wu, H.C.; Bouchaïr, A. 2021.** Mechanical properties and
735 engineering application potential of the densified poplar. *Wood Mater Sci Eng* Published
736 online: 13 May 2021, 1-9. <https://doi.org/10.1080/17480272.2021.1924857>
737
- 738 **Yalçın, M.; Şahin, H.İ. 2015.** Changes in the chemical structure and decay
739 resistance of heat-treated narrow-leaved ash wood. *Maderas-Cienc Tecnol* 17(2):
740 435-446. <https://doi.org/10.4067/S0718-221X2015005000040>
741
- 742 **Yıldız, S.; Gezer, E.D.; Yıldız, Ü.C. 2006.** Mechanical and chemical behavior of spruce
743 wood modified by heat. *Build Environ* 41(12): 1762-1766.
744 <https://doi.org/10.1016/j.buildenv.2005.07.017>
745