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# Advancements in biofilm carriers and gas-permeable membranes: assessment of zeolite technologies for shortcut nitrogen removal applications in wastewater

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1     **Advancements in biofilm carriers and gas-permeable membranes:**  
2     **assessment of zeolite technologies for shortcut nitrogen removal**  
3     **applications in wastewater**

4  
5     *Anndee L. Huff Chester<sup>\*1,2</sup>, Santiago Romero-Vargas Castrillón,<sup>3</sup> Paige J. Novak<sup>1\*</sup>*

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7  
8     <sup>1</sup>Department of Civil, Environmental, and Geo- Engineering, University of Minnesota, 500  
9     Pillsbury Drive SE, Minneapolis, Minnesota 55455

10  
11    <sup>2</sup>Brown and Caldwell, 370 Wabasha St N, Suite 500, St. Paul, Minnesota 55102

12  
13    <sup>3</sup>School of Engineering, The University of Edinburgh, William Rankine Building, Thomas Bayes  
14    Road, Edinburgh EH9 3FG, United Kingdom

15  
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20    \*authors to whom correspondence should be addressed:

21    ALHC: phone: 612-626-9846; email: [huffx063@umn.edu](mailto:huffx063@umn.edu)

22    PJN: phone: 612-626-9846; email: [novak010@umn.edu](mailto:novak010@umn.edu)

23 **Abstract**

24 The partial nitrification-anammox (PNA) process and other shortcut nitrogen removal processes  
25 have been widely studied because of their potential to offer cost savings during wastewater  
26 treatment; nevertheless, sustainable examples of full-scale mainstream shortcut nitrogen removal  
27 are lacking. The recent development of novel biofilm supports, specifically, zeolite-coated  
28 hollow fiber membranes and zeolite-coated biofilm carriers, that locally concentrate ammonium  
29 are promising for enhancing mainstream PNA. The ideal application of these technologies is yet  
30 to be determined, however. In this study, zeolite-coated carriers were tested in flow-through  
31 reactors under both anaerobic and aerobic conditions and zeolite-coated hollow fiber membranes  
32 were tested in a membrane-aerated flow-through configuration with varying operating times,  
33 lumen oxygen concentrations, and with the presence and absence of amended nitrite. Under  
34 anaerobic conditions, reactors containing zeolite-coated carriers had significantly greater  
35 ammonium and total nitrogen removal ( $84.0 \pm 16.2\%$  and  $89.4 \pm 17.1\%$ , respectively) compared  
36 to reactors containing control carriers ( $P = 0.005$ ). Anammox-specific 16S rRNA (*Amx*) genes  
37 and two genes associated with denitrifiers (*nirS* and *nosZ*) were preferentially retained in the  
38 bulk liquid and in the carrier biofilms in zeolite-coated carrier reactors at a statistically  
39 significant level. Genes specific to aerobic ammonium oxidizers (*amoA* genes) were  
40 preferentially retained in the bulk liquid of the zeolite-coated carrier reactors. The aerated  
41 zeolite-coated carrier reactors also had higher ammonium removal rates ( $83.8 \pm 10.9\%$ ) and  
42 higher TN removal rates ( $69.1 \pm 16.1\%$ ) compared to the aerated control reactors ( $30.8 \pm 23.4\%$ ,  
43  $P = 0.002$  and  $37.4 \pm 27.4\%$ ,  $P = 0.05$  for ammonia and TN, respectively). Again, despite  
44 aeration, *amoA* genes were only preferentially retained in the liquid of the reactors containing  
45 zeolite-coated carriers. In experiments with zeolite-coated membranes, *Amx* genes were

46 preferentially retained at significantly higher quantities under only two of the experimental  
47 conditions: two-week operation with 100% oxygen delivered in the membrane lumen and two-  
48 week operation with nitrite supplemented in the influent. Overall, the zeolite-coated carriers  
49 present promising potential for deployment in both anaerobic and aerated environments to  
50 enhance nitrogen removal and in particular, the retention of anammox bacteria. The zeolite-  
51 coated membranes require more study before their optimal deployment strategy is clear.

52

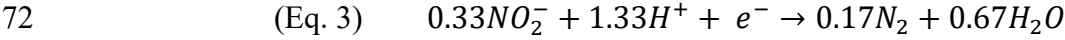
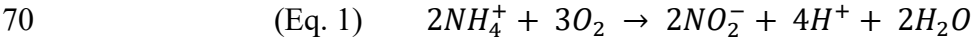
### 53 **Introduction**

54 Nitrogen removal is an important part of wastewater treatment and protects the environment  
55 from excess nutrients. Wastewater technologies have been designed to remove both ammonium  
56 and nitrite/nitrate, forming harmless nitrogen gas, typically through the application of combined  
57 nitrification and denitrification processes. Although effective, these processes are energy and  
58 resource intensive, resulting in an industry shift towards implementing lower cost “shortcut”  
59 nitrogen removal processes.<sup>1,2</sup>

60

61 Shortcut nitrogen removal can make use of a variety of microbial metabolic processes, with the  
62 ultimate goal of streamlining microbiological oxidation and reduction for lower oxygen, carbon,  
63 and/or alkalinity requirements.<sup>3-5</sup> In general, shortcut nitrogen removal combines nitrification,  
64 anammox, and denitrification processes. Partial nitrification is the process of converting half of  
65 the influent ammonium to nitrite via the activity of aerobic ammonia oxidizing bacteria (AOB)  
66 (Eq. 1).<sup>6</sup> Subsequently, ammonium and nitrite are converted to nitrogen gas by anaerobic  
67 ammonium oxidizing (anammox) bacteria (Eq. 2).<sup>7</sup> Combined, this process is referred to as

68 partial nitrification-anammox (PNA). Alternatively, the nitrite produced by AOB can be  
69 converted to nitrogen gas by nitrite-consuming denitrifiers (Eq. 3).<sup>6</sup>



73 Implementing shortcut nitrogen removal processes substantially reduces operating costs  
74 compared to conventional nitrification and denitrification. The anammox process reduces oxygen  
75 demand by approximately 60% with overall operating cost savings estimated at 60 to 90% if  
76 implemented for mainstream treatment.<sup>3,5,8</sup> Nitrite shunt, or nitrification/denitrification, can reduce  
77 oxygen demand by 25% and reduce overall energy costs by 60%.<sup>4</sup> Additional benefits associated  
78 with shortcut nitrogen removal are the elimination or reduction of carbon or alkalinity addition, a  
79 reduction in sludge production, and the potential decrease in reactor footprint.<sup>1,4,8</sup> Nevertheless,  
80 the implementation of such processes for mainstream treatment have presented challenges  
81 because typical mainstream conditions do not allow for the retention of certain microorganisms,  
82 such as anammox.<sup>1</sup>

83  
84 One way to improve shortcut nitrogen removal for mainstream wastewater treatment is the use of  
85 biofilm. Biofilm growth decouples the solids retention time and the hydraulic retention time  
86 (HRT) to retain slow growing, autotrophic microorganisms.<sup>9</sup> In some cases, specific biofilm  
87 carriers are used to further improve performance.<sup>10</sup> As biofilms develop and aerobic and  
88 anaerobic zones are created, complete nitrogen removal can occur in a single biofilm.<sup>10-12</sup>  
89 Technologies that take advantage of these benefits include integrated fixed film activated sludge  
90 (IFAS) and moving bed biofilm reactors (MBBR).<sup>13</sup> Membrane aerated biofilm reactors

91 (MABR) supply oxygen at the membrane base of the biofilm, creating a unique substrate profile  
92 that may enhance total nitrogen removal within a single biofilm.<sup>14</sup> Many studies have shown that  
93 biofilm technologies work well for shortcut nitrogen removal processes, but that there is still  
94 room for improvement, particularly with respect to enhancing the colonization and retention of  
95 anammox biomass.<sup>10,13,15-17</sup>

96  
97 Because of their ability to sorb and therefore concentrate ammonium, zeolite-coated membranes  
98 and biofilm carriers could improve current biofilm technologies for shortcut nitrogen removal by  
99 improving the rate at which anammox bacteria colonize solid supports as well as their retention,  
100 and potentially retaining AOB as well.<sup>16,18,19</sup> In previous work, we showed that zeolite  
101 technologies can attract and retain anammox bacteria under mainstream conditions.<sup>18</sup> With  
102 enough zeolite in the system, anammox bacteria were retained and outperformed systems  
103 without zeolite amendment with respect to both ammonium and total nitrogen (TN) removal. The  
104 wastewater conditions under which zeolite-coated carriers or membrane technologies can be  
105 applied for enhanced performance has yet to be explored, however. Aerated zeolite-coated  
106 membranes with anaerobic bulk conditions might encourage simultaneous AOB and anammox  
107 growth if biofilm growth enables anaerobic zones on the outer biofilm layers. Under aerated  
108 conditions, it is possible that AOB and anammox could coexist on carriers colonized with thick  
109 biofilms. Regardless of the bulk conditions, both zeolite-coated carrier and membrane  
110 technologies should concentrate ammonium at the base of the biofilm and therefore retain and  
111 enrich anammox bacteria, if oxygen concentrations are not too high. The overall AOB and  
112 anammox bacteria retention will likely depend on bulk conditions, the mass of zeolite

113 incorporated into these biofilm supports, and the oxygen permeance of the zeolite-coated  
114 membranes<sup>9,18,20-23</sup>.

115

116 In this study, we explored how operating conditions impact the performance of novel zeolite-  
117 coated biofilm support technologies with respect to nitrogen removal and microbial  
118 enrichment/retention. We hypothesized that anammox bacteria will be preferentially retained in  
119 the presence of zeolite coatings and low oxygen concentrations, whereas AOB will be  
120 preferentially retained on zeolite-coated membranes that are able to supply oxygen and sorb  
121 ammonium. This research clarifies how one can implement these novel zeolite-coated biofilm  
122 supports for enhanced wastewater nitrogen removal and suggests other applications for these  
123 supports.

124

## 125 **Experimental**

126 ***Biofilm attachment materials.*** Several methods of attaching zeolite onto a support were tested in  
127 this research to create a material that maximized ammonium removal per support surface area.  
128 Detailed methods describing these processes are provided in the SI or in previous  
129 publications.<sup>18,19,24,25</sup> Briefly, for development of zeolite-coated membranes, attachment onto a  
130 polymer surface was tested with four different methods of surface functionalization,<sup>24-29</sup> one  
131 method of embedding the zeolite into the polymer membrane, and one method of growing zeolite  
132 on alumina hollow fibers, which we have tested previously and is described in Huff Chester et  
133 al.<sup>18</sup> For development of porous zeolite-coated carriers, deposition into a porous polyethylene  
134 (PE) matrix was tested, also described previously (Feinberg et al.).<sup>19</sup> Control materials without  
135 zeolite were generated for some of these zeolite-coated supports as previously described.<sup>18,19</sup>

136 Scanning electron microscope (SEM) images were taken using methods described in Huff  
137 Chester et al.<sup>18</sup>

138

139 ***Synthetic wastewater and seed.*** Three types of synthetic wastewater with ammonium  
140 concentrations of 35 mg-N/L were used, depending on the experimental objectives. One  
141 wastewater contained carbon at 200 mg/L and nitrite at 21 mg-N/L, modified from Huff Chester  
142 et al.,<sup>18</sup> and was intended to mimic mainstream wastewater in which partial nitrification (PN)  
143 was active. The second synthetic wastewater was identical to this but did not contain nitrite,  
144 mimicking mainstream wastewater influent.<sup>18</sup> A third synthetic wastewater was prepared without  
145 carbon and was modified from Peterson et al.<sup>30</sup> to limit the potential for heterotrophic activity.  
146 Tables S1 and S2 detail the synthetic wastewater contents. Wastewater was autoclaved and  
147 sealed until used. The activated sludge and anammox sludge inoculum and their storage  
148 conditions were described previously.<sup>18</sup>

149

## 150 ***Experimental set-up and operation***

151 *Sorption measurements and isotherm tests.* Sorption tests were carried out on membranes and  
152 carriers as described by Huff Chester et al.<sup>18</sup> Areas of membranes were measured using a calipers  
153 to determine ammonium removal per area of membrane. Carrier surface area was calculated as  
154 the apparent surface area, and not the surface area of the internal porous network. Sorption tests  
155 were also conducted for isotherm fitting, also described in Huff Chester et al.<sup>18</sup> Briefly, carriers  
156 were added to 10 mL of autoclaved synthetic wastewater amended with varying ammonium  
157 concentrations and then mixed on a rotator for 48 hours. Ammonium measurements were taken  
158 with an ammonium probe (Orion, Thermo Scientific). Ammonium sorbed per unit mass of



159 membrane or per carrier ( $q_e$ ) and liquid equilibrium ammonium concentration were fit to  
160 Langmuir (Eq. 4), Freundlich (Eq. 5), and linear isotherms (Eq. 6) using the R nonlinear least  
161 squares function (nls). Constants are described in Table S3.

162 (Eq. 4)  $q_e = \frac{q_{max} \cdot K \cdot C_f}{1 + K \cdot C_f} = \frac{41.56 \cdot 0.000946 \cdot C_f}{1 + 0.000946 \cdot C_f}$

163 (Eq. 5)  $q_e = k_f \cdot C_f^{\frac{1}{n}} = 0.0465 C_f^{\frac{1}{1.0588}}$

164 (Eq. 6)  $q_e = k_f \cdot C_f$

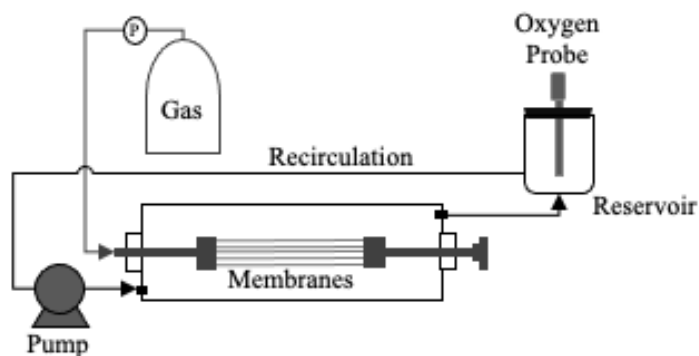
165 Testing of carriers for ammonium sorption through a developed biofilm. In addition to testing  
166 fresh membranes and carriers for ammonium sorption, carriers upon which a biofilm layer had  
167 developed were also tested for ammonium sorption to ensure that the zeolite deposited into the  
168 PE remained intact and ammonium could still exchange into the zeolite with biofilm present.  
169 Two sets of zeolite-coated and control carriers were tested for ammonium sorption post-biofilm  
170 growth: one set that was harvested at the end of an aerated flow-through experiment (described  
171 below) and a second set that was harvested after being submerged in a DEMON reactor  
172 (described previously by Peterson et al.<sup>30</sup>) for 14 days. Once harvested, carriers were subjected to  
173 925 Gy of gamma irradiation (GI) on a Cs-137 irradiator (JL Shepherd & Associates),<sup>31</sup> after  
174 which they were tested for abiotic ammonium sorption in an ammonium chloride solution (29.5  
175  $\pm$  0.4 mg-N/L), as previously described.<sup>19</sup>

176

177 Carrier bioavailability test. Carriers were formed such that the zeolite particles were entrapped  
178 in a porous structure of polyethylene. Carriers were tested to ensure that the ammonium sorbed  
179 to the zeolite particles within the porous network was accessible for microbial use, specifically  
180 for anaerobic ammonium oxidation. First, ammonium was exchanged into the zeolite in the  
181 carriers by adding 387 carriers to 2 L of 100 mg-N/L ammonium chloride solution for 72 hours,

182 after which the carriers were transferred to batch reactors. Control carriers were not pre-sorbed  
183 with ammonium. Carriers were then divided into three different reactor types: 1) zeolite-coated  
184 carriers to which an anammox enrichment culture was added, 2) zeolite-coated carriers amended  
185 with sodium azide (10 mM), as an abiotic control, and 3) control carriers to which an anammox  
186 enrichment culture was added. Serum bottles were used as reactors and contained 50 mL of  
187 headspace (97% N<sub>2</sub>:3% H<sub>2</sub>). Each reactor contained 43 carriers and 50 mL of synthetic carbon-  
188 free wastewater containing nitrite and was seeded with 2 mL of settled anammox biomass. This  
189 experiment was operated on a shake table (60 rpm) in a glove bag under anaerobic conditions at  
190 room temperature (21 ± 2°C). The only ammonium added to the systems was the ammonium  
191 sorbed to the carriers. Ammonium and nitrite were sampled every 4 hours to monitor ammonium  
192 and nitrite degradation.

193  
194 Oxygen transfer characteristics of hollow fiber membranes. Permeance testing of membranes  
195 was conducted for both zeolite-coated and uncoated alumina hollow fiber membranes using the  
196 methods described by Ahmed and Semmens.<sup>32</sup> To summarize, 10 membranes were potted in a  
197 long reactor, sealed on one end (dead-end configuration) (Figure 1).



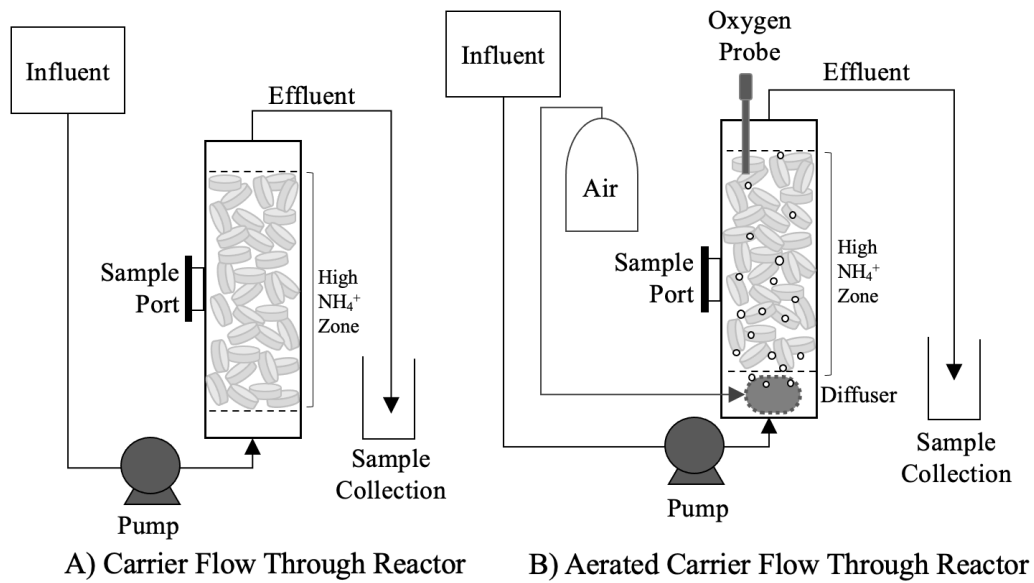
198  
199 **Figure 1. Schematic of membrane permeance test step-up**

200 Oxygen was fed to the membranes (lumen side) at 5 PSI and oxygen transfer occurred from the  
201 membrane into bulk reactor water as the water flowed over the membrane surface at 0.01  
202 cm/min. Prior to testing, the water was deoxygenated via an N<sub>2</sub> gas purge and recirculated in the  
203 reactor system until the oxygen probe (Unisense, Opto-3000) inserted in a reservoir at the end of  
204 the reactor measured <0.5 mg DO/L. Leakage tests with no oxygen fed through the membranes  
205 were also performed to enable the subtraction of oxygen leaking into the system from the oxygen  
206 permeating through the membranes. Once the oxygen mass transfer coefficient ( $k$ ) was  
207 determined, the mass flux of oxygen ( $J$ ) into the zeolite and control membrane reactors was  
208 calculated using Eq. 6. Here  $A$  is the area of the membrane,  $C^*$  is average equilibrium dissolved  
209 oxygen concentration in the membrane, and  $C_L$  is the oxygen concentration in the bulk liquid.

210 
$$(Eq. 6) \quad J = kA(C^* - C_L)$$

211 Carrier flow-through reactors - anaerobic and aerobic. Flow-through reactors were designed to  
212 test the nitrogen-removal performance of zeolite-coated and control carriers under mainstream  
213 wastewater treatment conditions, as well as their ability to attract and retain anammox bacteria  
214 and AOB. Triplicate carrier flow through reactors (CFTR) were packed with 100 zeolite-coated  
215 carriers to obtain a “high ammonium zone” of 10 mL. Triplicate control CFTRs were set up  
216 similarly but contained control carriers. The reactor set-up is shown in Figure 2. Synthetic  
217 wastewater containing carbon flowed through the reactors continuously, with a hydraulic  
218 residence time (HRT) of 17 hours. The experiment was operated twice, once without aeration  
219 and with synthetic wastewater amended with nitrite (CFTR), and once with aeration provided by  
220 a stone diffuser and synthetic wastewater with no nitrite added. Oxygen measurements were  
221 taken at the reactor exit periodically throughout the aerated carrier flow through reactor  
222 (ACFTR) experiment with an oxygen probe (Unisense, Opto-3000). Carrier and liquid biomass

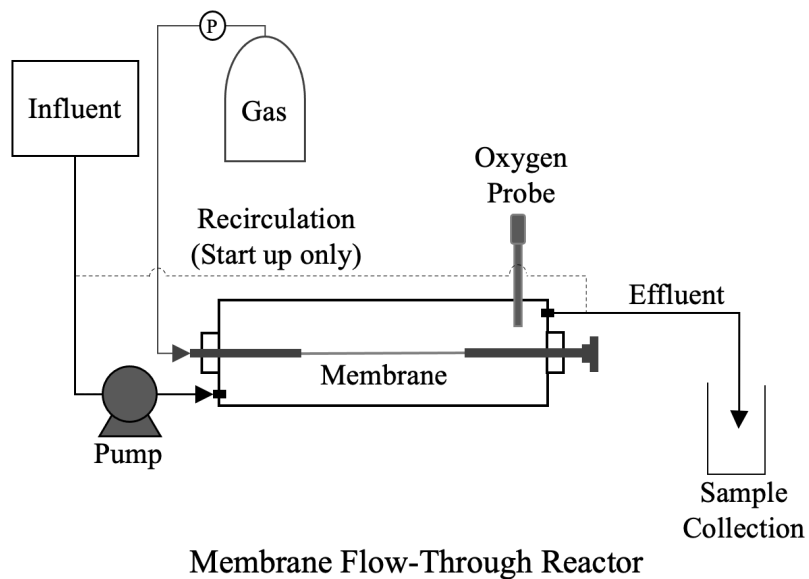
223 samples were harvested from a side port in the reactor for microbial analysis throughout the  
 224 experiment. Effluent was collected in a vial to which phosphoric acid was added so that the pH  
 225 of the effluent was adjusted to less than four to ensure that no biological reactions occurred after  
 226 collection but prior to analysis. Samples were immediately filtered (0.45  $\mu\text{m}$ ) and stored sealed  
 227 at 4°C until analyzed for COD, ammonium, total nitrogen, nitrate, and nitrite as described below.



228  
 229 **Figure 2. Schematic of CFTR and ACFTR reactor set-up**  
 230

231 Membrane aerated flow-through reactor. Zeolite-coated and alumina control membranes were  
 232 also tested in a flow-through configuration to assess the growth and retention of anammox  
 233 bacteria and AOB on the membranes. Carbon- and nitrite-free synthetic wastewater was fed  
 234 continuously into the reactors. Triplicate reactors were set up for both the zeolite-coated  
 235 membranes and the alumina control membranes. Reactors were 70 mL in volume and contained  
 236 a single potted membrane, as shown in Figure 3. Oxygen was introduced into the membrane  
 237 lumen from a compressed tank at 5 PSI in dead-end mode. Experiments were performed for 1, 7,

238 14, and 24 days to monitor colonization of the membranes; at the end of the experiment the  
239 membrane was harvested and biomass was extracted from the membrane surface (see below).  
240 Additional experiments were performed for 14 days in which N<sub>2</sub> or air were fed through the  
241 membrane. A final experiment was performed for 14 days in which nitrite was added to the  
242 synthetic wastewater fed to the system. For all experiments, 0.5 mL of activated sludge and 0.2  
243 mL of settled anammox sludge were added to the reactors at the start of the experiment. Reactor  
244 liquid was recirculated for 24 hours at 1.0 mL/min to encourage biofilm attachment. After 24  
245 hours, settled sludge was drained and the flow-through experiment was started with a wastewater  
246 HRT of 23 hours. At the end of each experiment membranes were carefully harvested and cut  
247 into equal sample lengths of 52 ± 3.4 mm for DNA extraction. Oxygen was monitored with an  
248 oxygen probe throughout the experiment; the bulk liquid of the reactors quickly became and  
249 stayed anaerobic during all experiments.



250

251

252

**Figure 3. Schematic of MFTR reactor set-up**

253 **Analytical methods.** Analytical methods, specifically nitrogen measurement methods, were  
254 described previously in Huff Chester et al.<sup>18</sup> Briefly, ammonium concentrations for the sorption  
255 experiments were measured with an ammonium probe (Orion, Thermo Scientific). Ammonium  
256 and TN concentrations in reactor effluent samples were measured colorimetrically (Hach).  
257 Nitrite and nitrate concentrations in reactor effluent samples were measured with ion  
258 chromatography (930 Compact IC Flex, Metrohm). Dissolved organic carbon (DOC)  
259 measurements in reactor samples were analyzed using a TOC-L total organic carbon analyzer  
260 (Shimadzu) after first filtering samples through a 0.22 µm syringe filter. A 5-point calibration  
261 curve was generated from 500 mg/L stock solution ranging from 10 to 500 mg/L. Typical limits  
262 of detection were 2 mg/L.

263  
264 **Molecular methods.** DNA extractions and qPCR for Bacterial 16S rRNA, Anammox 16S rRNA,  
265 *amoA*, *nirK*, *nirS*, *nosZ*, and *nxrA* genes were performed as previously described in Huff Chester  
266 et al.<sup>18</sup>

267  
268 **Data and statistical analysis.** Ammonium removal was calculated for the ammonium sorption  
269 experiments using Eq. 7.

270 
$$(Eq. 7) \quad Removal = \frac{C_{initial} - C_{final}}{C_{initial}}$$

271 Non-parametric Wilcoxon rank sum tests were used to compare data from the CFTR and ACFTR  
272 experiments, namely the nitrogen concentrations, DOC concentrations, and the qPCR data for  
273 the zeolite-coated and control carrier reactors. Comparisons of the ammonium concentrations  
274 from the carrier-biofilm sorption tests were also performed using the non-parametric Wilcoxon  
275 rank sum test. Parametric paired Student t tests were used to compare the qPCR data in the

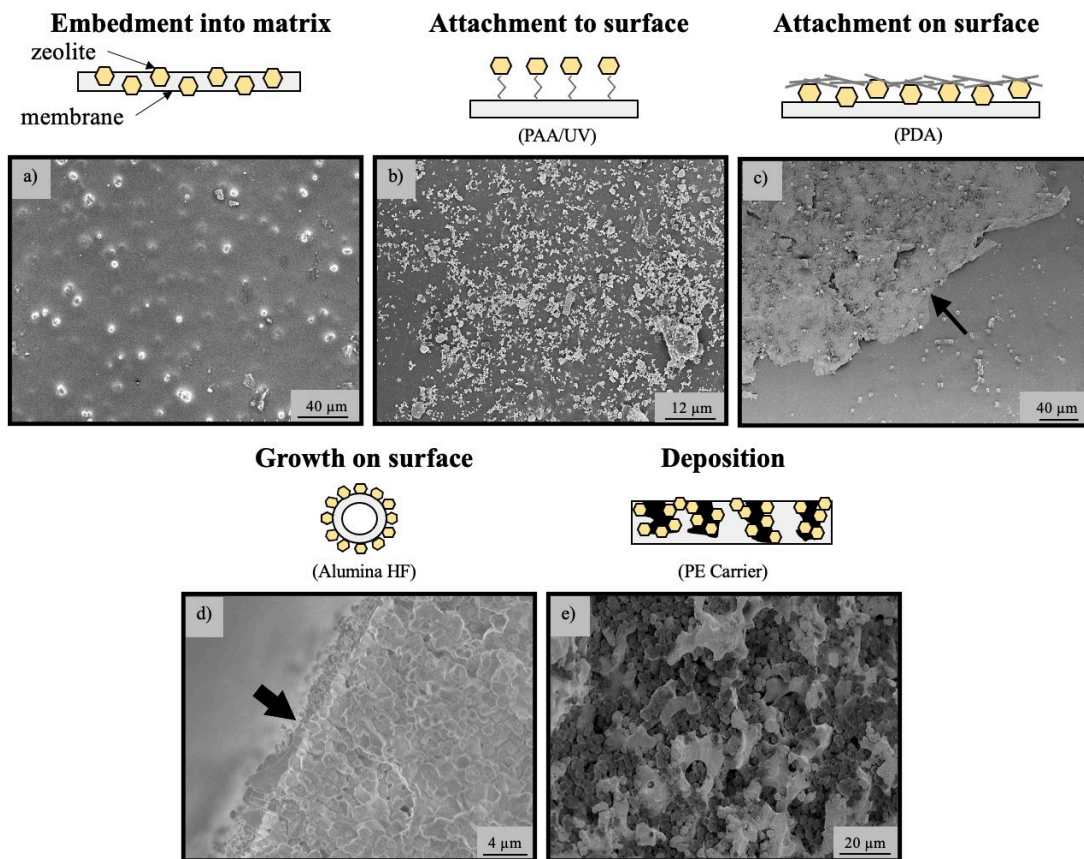
276 reactors containing zeolite-coated versus control membranes in the MFTR experiments after first  
277 checking for normality using the Shapiro-Wilk test. Typically, p-values less than 0.05 were  
278 considered significant, but p-values less than 0.1 were also reported and statistical significance  
279 with 90% confidence was clearly indicated. Statistical tests were performed with R software.

280

## 281 Results and Discussion

282 *Characterization of membranes and carriers for bioreactor deployment.* Materials prepared  
283 using different methods of zeolite attachment (described in the SI) were tested for ammonium  
284 sorption. SEM images of the developed materials are show in Figure 4.

285

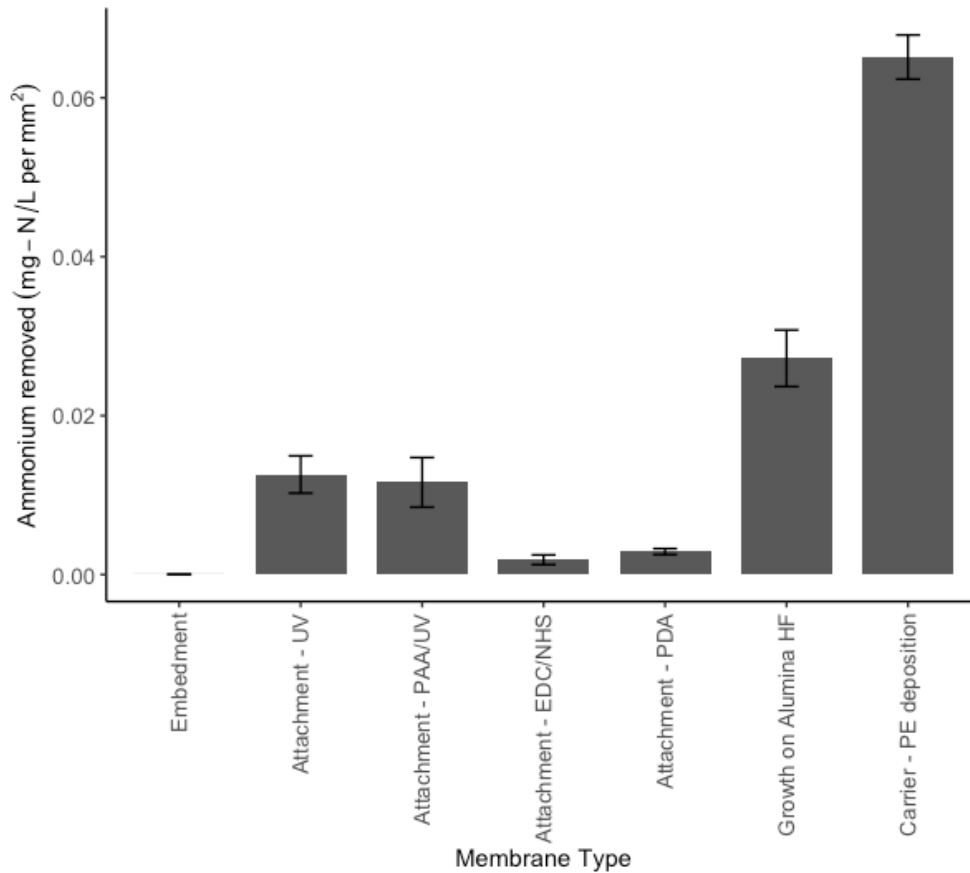


286

287 **Figure 4. SEM images of membrane and carrier surfaces.** a) Embedment into  
288 polymer membrane matrix, b) attachment to membrane surface using UV/PAA method,  
289 c) attachment to membrane using PDA method, d) growth of zeolite on alumina hollow  
290 fiber membrane, and e) deposition into porous PE carrier. Panel e is adapted with  
291 permission from Feinberg et al. Porous Polyethylene-Supported Zeolite Carriers for  
292 Improved Wastewater Deammonification. *ACS EST Eng.* 2021, 1 (7), 1104–1112.  
293 Copyright 2021 American Chemical Society.

294  
295 Ammonium sorption from synthetic wastewater as a function of carrier surface area is shown for  
296 each membrane and carrier type in Figure 5. Most of the zeolite coating methods were successful  
297 in attaching zeolite and facilitating at least some ammonium sorption from synthetic wastewater,  
298 except for the embedment method, which did not result in substantial ammonium removal  
299 ( $1.9 \times 10^{-5} \pm 4.1 \times 10^{-6}$  mg-N/L/mm<sup>2</sup>) (Figure 5). Membranes developed from the attachment  
300 methods all obtained some level of ammonium sorption ( $0.013 \pm 0.002$ ,  $0.012 \pm 0.003$ ,  $0.0019 \pm$   
301  $0.0006$ , and  $0.00029 \pm 0.0004$  mg-N/L/mm<sup>2</sup> for functionalization enabled by ultraviolet (UV),  
302 poly(acrylic acid)/UV, 1-ethyl-3-(3-dimethylaminopropyl)carbodiimide/N-hydroxysuccinimide,  
303 and polydopamine, respectively). The zeolite-coated alumina hollow fiber membranes had the  
304 highest ammonium sorption per mm<sup>2</sup> of membrane, removing  $0.029 \pm 0.004$  mg-N/L/mm<sup>2</sup>; these  
305 membranes were therefore selected for further testing, both with respect to their sorption  
306 capacity and their potential to transfer oxygen. Likewise, the zeolite-coated porous biofilm  
307 carriers also showed excellent ammonium sorption capability ( $0.065 \pm 0.03$  mg-N/L/mm<sup>2</sup>)  
308 (Figure 5) and were also studied further.





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**Figure 5. Ammonium removal from synthetic wastewater via sorption to zeolite-functionalized materials using zeolite attachment or coating methods.** Error bars

indicate the standard deviation of triplicate experiments. Note: For the porous carrier

within which the zeolite was deposited, the apparent surface area, excluding the internal

pore structure, was used for sorption calculations.

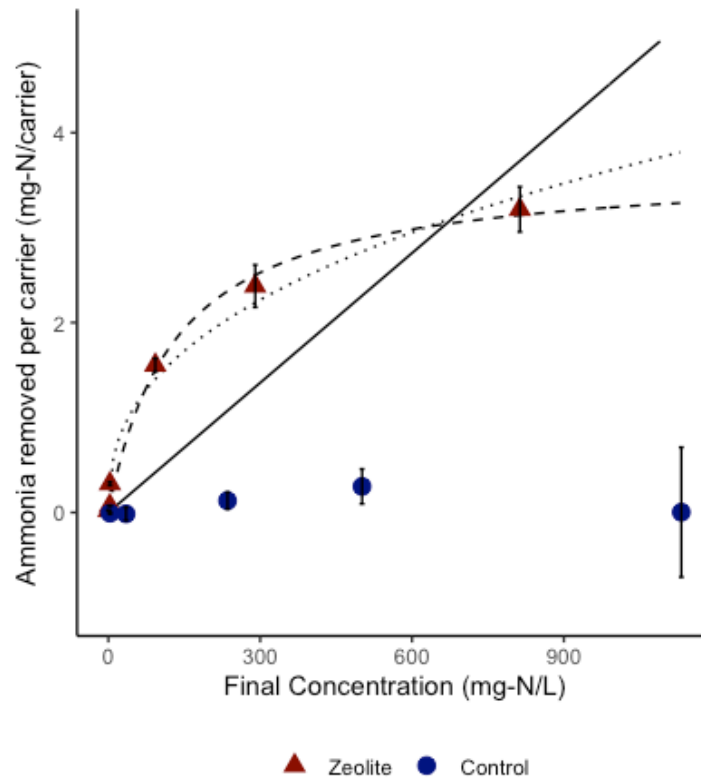
Isotherms for ammonium sorption of the zeolite-coated membranes and carriers were also

developed and were fit to linear, Langmuir, and Freundlich isotherm models.

All isotherms fit the data for the zeolite-coated membranes well.<sup>18</sup> Zeolite carriers were tested

beyond the linear region. As a result, the Langmuir isotherm model provided the best fit, with an

320  $R^2$  of 0.992; the Freundlich isotherm model also provided a good fit to the data, with an  $R^2$  of  
321 0.981. The linear isotherm fit was poor, with an  $R^2$  of 0.85.



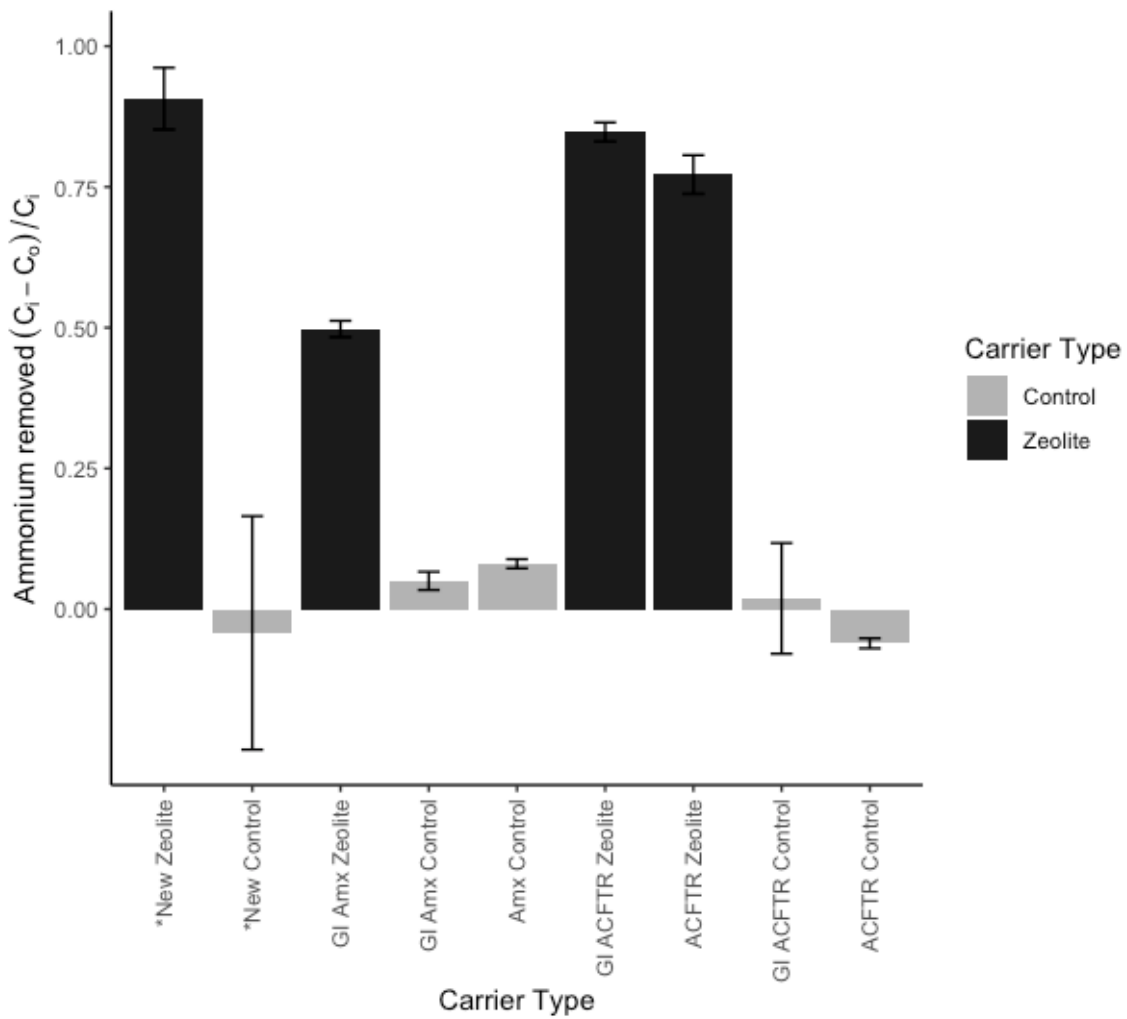
322

323 **Figure 6. Ammonium sorption isotherms for zeolite-coated and control carriers in**  
324 **synthetic wastewater.** Lines indicate model fits, with the solid line showing the linear  
325 isotherm fit, the dashed line showing the Langmuir isotherm fit, and the dotted line  
326 showing the Freundlich isotherm fit. Control membranes and carriers were not fit to  
327 isotherm curves, as they failed to sorb ammonium. Error bars indicate the standard  
328 deviation of triplicate experiments.

329

330 Carriers coated with biofilm were also tested for ammonium sorption to determine if biofilm  
331 growth created substantial blockage of ion exchange sites on the zeolite, as has been reported in  
332 other studies.<sup>29</sup> Zeolite-coated carriers, first gamma irradiated to inactivate the biofilm, showed

333 considerable ammonium removal (Figure 7) indicating that biofilm growth did not prevent  
 334 ammonium sorption on zeolite-coated carriers. In fact, all zeolite-coated carriers showed  
 335 ammonium sorption, removing significantly more ammonium compared to the control carriers ( $P$   
 336  $= 0.0035$ ). The GI-ACFTR zeolite-coated carriers removed more ammonium compared to the  
 337 GI-Amx zeolite-coated carriers ( $84.6 \pm 2\%$  vs.  $49.8 \pm 1\%$ , respectively,  $P < 0.0001$ ), which is  
 338 likely an indication that the GI-Amx biofilm was thicker than the GI-ACFTR biofilm and some  
 339 blockage of the exchange sites did occur upon growth of a thick enough biofilm.  
 340



341

342 **Figure 7. Ammonium removal  $[(C_i - C_f)/C_i]$  via sorption to biofilm-covered zeolite-**  
343 **coated and control carriers subjected to gamma irradiation; these were compared to**  
344 **pristine (no biofilm present) zeolite-coated and control carriers.** Amx indicates  
345 carriers submerged in an anammox enrichment reactor for biofilm growth. ACFTR  
346 indicates carriers sampled from the aerated CFTR experiment and also covered in biofilm  
347 growth. GI indicates gamma-irradiated carrier samples. Error bars indicate standard  
348 deviation of triplicate experiments.

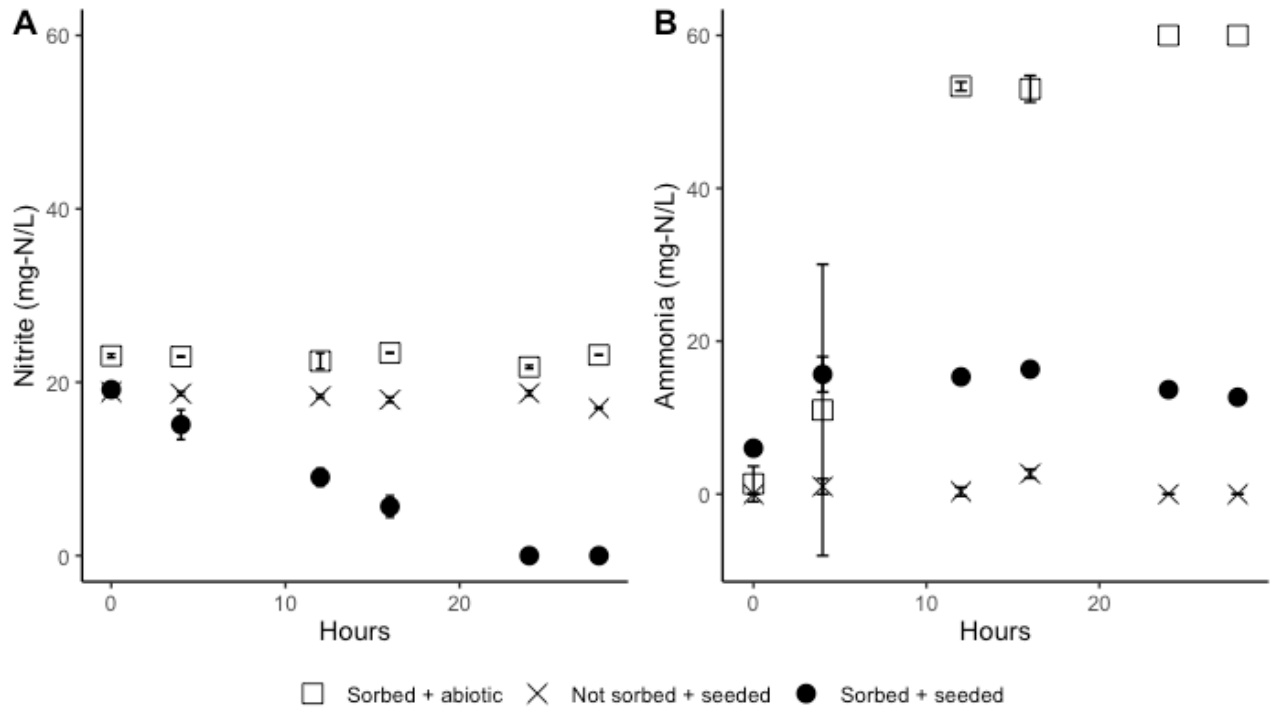
349

350 Permeance tests with zeolite-coated alumina hollow fibers showed that the fibers were capable of  
351 transferring oxygen to water, with mass transfer coefficients calculated to be  $6.3 \times 10^{-6}$  cm/s for  
352 the zeolite-coated membranes and  $2.8 \times 10^{-6}$  cm/s for the control membranes. It is unclear why the  
353 zeolite-coated membranes were capable of greater oxygen transfer, but it could have been a  
354 result of their different surface chemistry. Measurements of the zeta potential and hydrophobicity  
355 of the zeolite-coated and control membranes were attempted, the curvature of the hollow fiber  
356 surfaces, however, made these parameters impossible to measure. The reasons for the greater  
357 oxygen transfer rates with the zeolite-coated membranes, therefore, could not be confirmed. The  
358 mass flux of oxygen into the system was calculated from the mass transfer coefficients to be  
359  $2.4 \times 10^{-7}$  mg/s for pure oxygen and  $5.04 \times 10^{-8}$  mg/s for air fed to the lumen of the zeolite-coated  
360 membranes. For the control membranes, the mass flux was  $1.0 \times 10^{-7}$  mg/s for pure oxygen and  
361  $2.2 \times 10^{-8}$  mg/s for air.

362

363 Our previous work on the zeolite-coated alumina hollow fibers (Huff Chester et al),<sup>18</sup> as well as  
364 work by others,<sup>30,31</sup> has suggested that ammonium sorbed to zeolite is accessible to

365 microorganisms; nevertheless, given the sponge-like structure of the zeolite-coated carriers and  
366 the fact that porous materials of this kind have not been previously tested, the bioavailability of  
367 the sorbed ammonium with the zeolite-coated carriers was verified. As described in the methods,  
368 if the ammonium that was sorbed to the carriers was bioavailable, the nitrite in the bottles  
369 containing zeolite-coated carriers and anammox bacteria should degrade. Data presented in  
370 Figure 8 supports this view, with the nitrite concentrations in the zeolite-coated carrier treatments  
371 decreasing from  $19.16 \pm 0.5$  to  $0 \pm 0$  mg-N/L within 25 hours and no appreciable nitrite decrease  
372 in the control carrier treatments. Indeed, the rate of nitrite degradation in the zeolite-coated  
373 carrier treatments was significantly greater ( $0.97 \pm 0.04$  mg/L per hour) than that in the control  
374 carrier treatments ( $0.052 \pm 0.005$  mg/L per hour) ( $P = 0.027$ ). Additionally, negative control  
375 reactors containing zeolite-coated carriers amended with sodium azide showed an increase in  
376 ammonium to an average of  $56.6 \pm 3.7$  mg-N/L, as the ammonium desorbed into solution from  
377 the carriers and was not consumed biologically. These results clearly demonstrated the ability of  
378 the anammox culture to access sorbed ammonium from the zeolite-coated carriers.  
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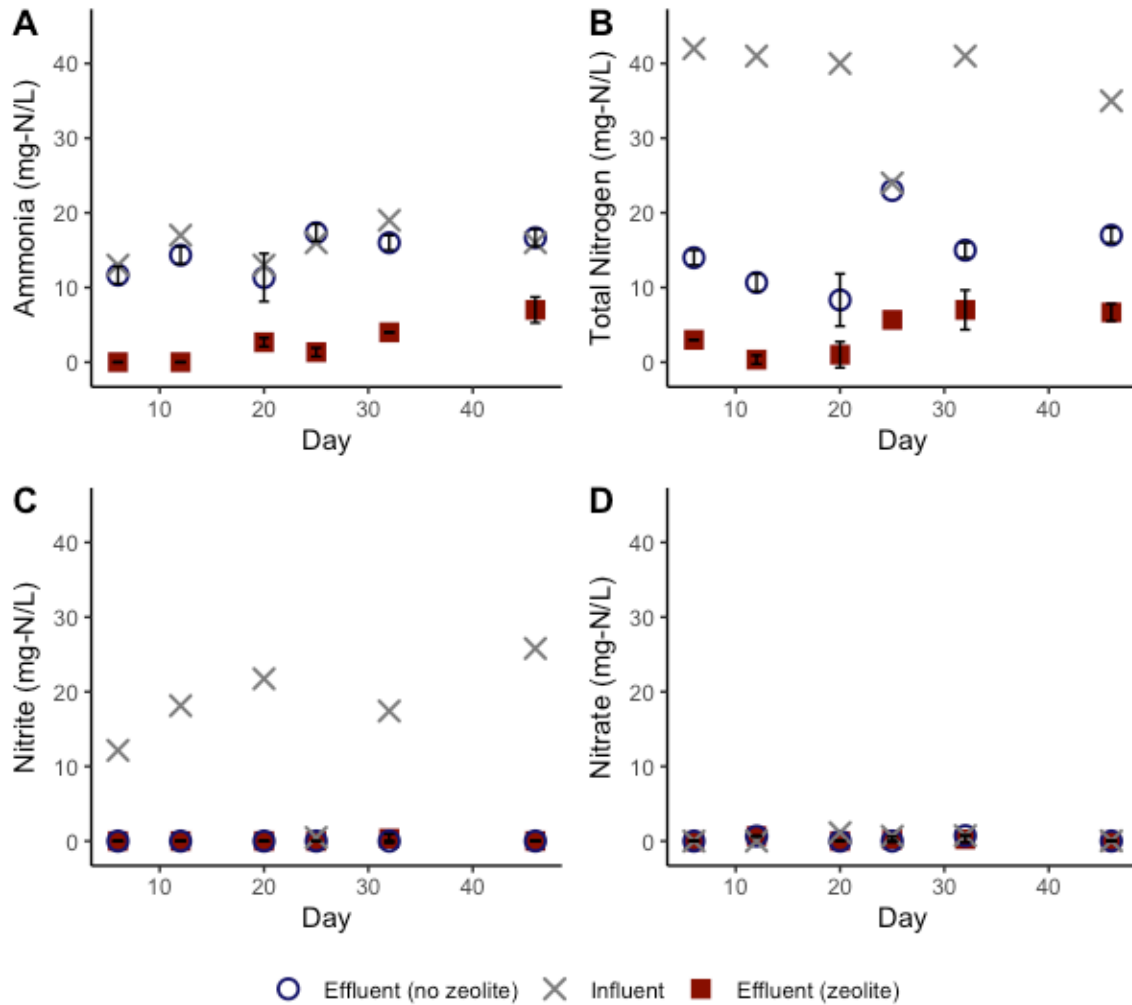
**Figure 8. Measured ammonium and nitrite concentrations over time from the bioavailability tests, indicating that the ammonium sorbed to the carriers was bioavailable.** Error bars show standard deviations of triplicate experimental replicates.

Overall, material testing was able to show that a variety of methods could be used to attach zeolite to supports and additional experiments with two of the most promising materials showed that ammonium sorption followed both a Langmuir and Freundlich sorption model. It was further shown that ammonium sorption occurred through a layer of biofilm, and ammonium exchanged into the zeolite-coated carriers was biologically accessible.

***Zeolite coated substrates demonstrate shortcut nitrogen removal in wastewater system.*** The results in the previous section suggested that both the zeolite-coated alumina hollow fiber membranes and PE carriers should be excellent candidates for deployment into mainstream

394 wastewater systems for enhanced shortcut nitrogen removal. We investigated these prospects in  
395 carrier flow-through bioreactors, aerated carrier flow-through bioreactors, and membrane flow-  
396 through bioreactors. Zeolite-coated and control carriers were tested in a flow-through system  
397 (Figure 1) fed with synthetic wastewater containing ammonium and nitrite at concentrations of  
398  $15.7 \pm 2.33$  mg-N/L and  $17.4 \pm 4.0$  mg-N/L, respectively, for a TN concentration of  $37.2 \pm 6.9$   
399 mg-N/L. The influent also contained DOC at a concentration of  $167.7 \pm 66.2$  mg/L. Influent and  
400 effluent concentrations of ammonium, TN, nitrite, and nitrate are shown in Figure 9. DOC  
401 influent and effluent concentrations are shown in Figure 10. As a result of an error, no nitrite was  
402 added to the influent on Day 25. This is evident in the results shown in Figure 9, where the  
403 influent concentration on Day 25 was 0.5 mg-N/L, compared to the average concentration on all  
404 other days of  $17.4 \pm 4.0$  mg-N/L.

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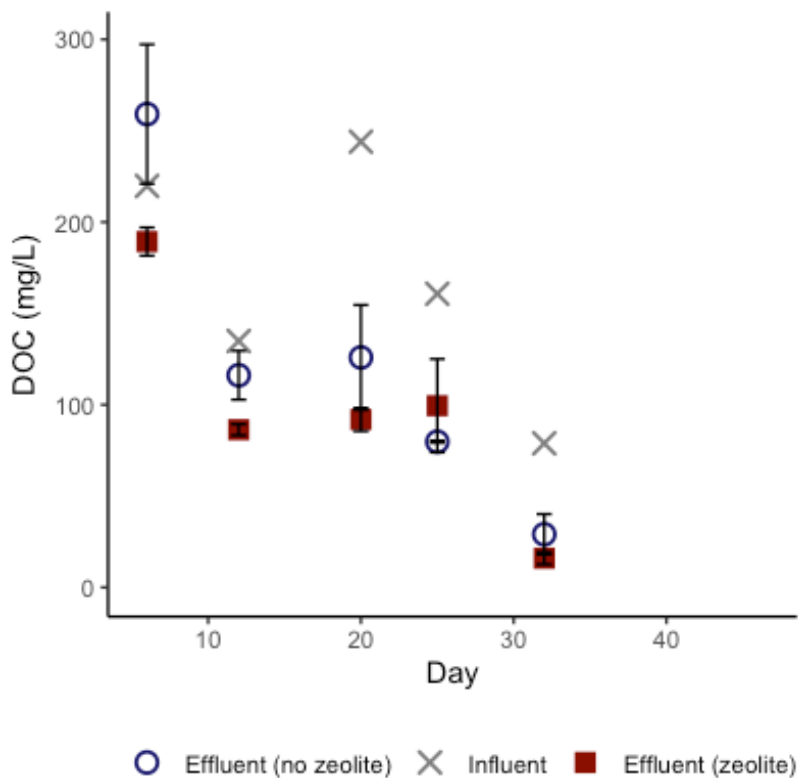
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**Figure 9. Influent and effluent concentrations of A) Ammonium, B) TN, C) Nitrite, and D) Nitrate in the CFTR experiment. Error bars indicate the standard deviation of triplicate reactors.**





410  
 411 **Figure 10. Influent and effluent DOC concentrations in the CFTR experiment.** Error  
 412 bars indicate standard deviation of triplicate reactors.

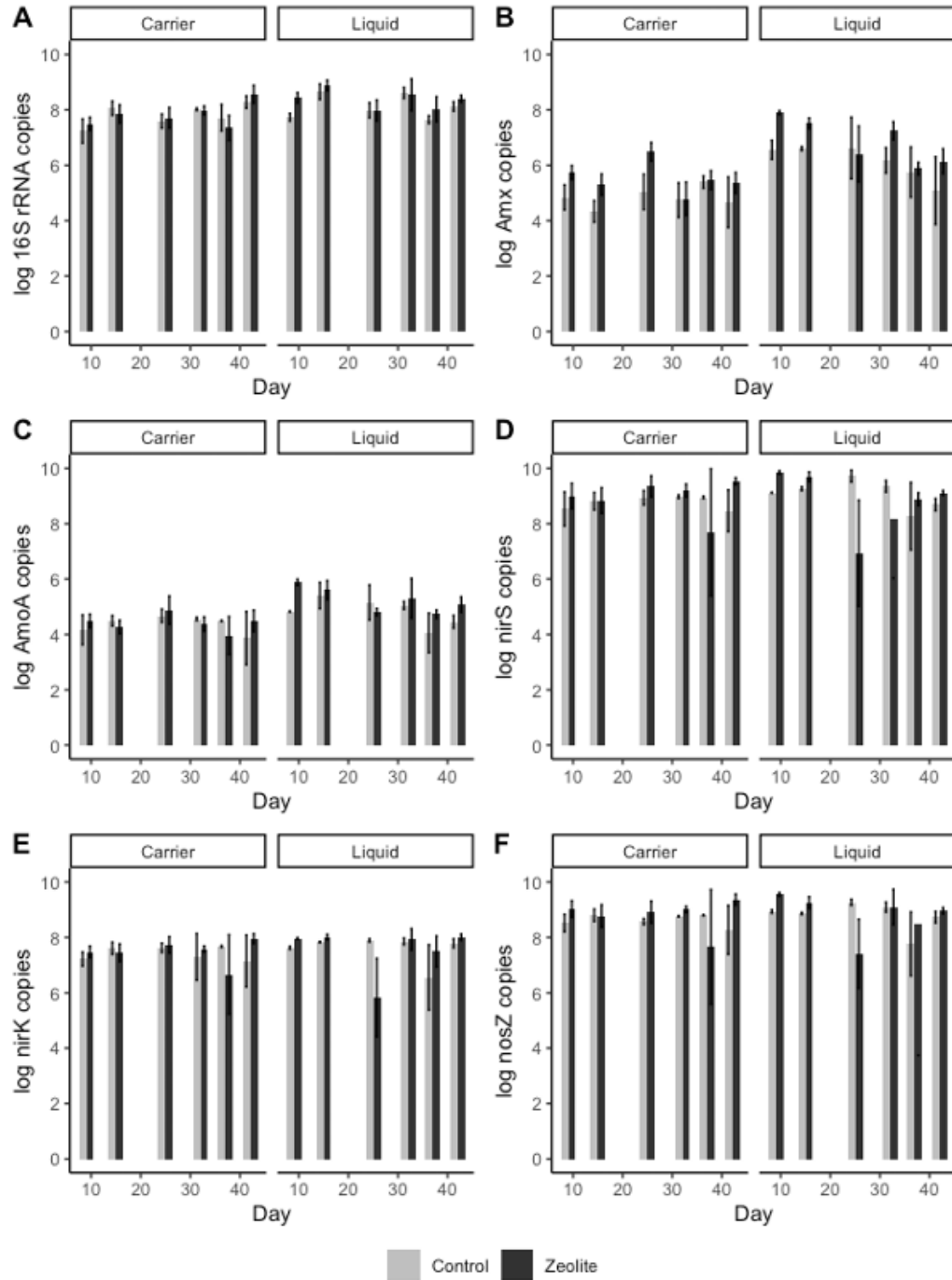
413  
 414 Over the course of the 46-day experiment, the reactors containing zeolite-coated carriers  
 415 removed significantly more ammonium ( $84.0 \pm 16.2\%$ ) and TN ( $89.4 \pm 17.1\%$ ) on average, and  
 416 therefore had much lower average effluent ammonium ( $2.50 \pm 2.62$  mg-N/L) and TN ( $3.94 \pm$   
 417  $2.98$  mg-N/L) concentrations compared to control reactors ( $14.56 \pm 2.79$  and  $14.7 \pm 5.37$  mg-N/L  
 418 for ammonium and TN, respectively) ( $P < 0.0001$  for both ammonium and TN) (Figure 9). It  
 419 cannot be determined from the chemical data alone whether this was a result of the  
 420 retention/enrichment of anammox bacteria on the zeolite-coated carriers and enhanced anammox  
 421 activity, or a result of abiotic ammonium sorption coupled with the denitrification of amended  
 422 nitrite. Examination of the microbial data, Figure 11, however, shows that retention of anammox

423 bacteria on the zeolite-coated carriers is at least partially responsible for the enhanced nitrogen  
424 removal in the reactors containing zeolite-coated carriers.

425

426 The log of the anammox gene copies per carrier or per mL was statistically greater in both the  
427 carrier biofilm samples and in the bulk liquid samples from the reactors containing zeolite-coated  
428 carriers, compared to the same samples taken from the reactors containing control carriers (P =  
429 0.002 for the carrier biofilm samples and P = 0.01 for the bulk liquid samples). The average log  
430 16S rRNA copies per mL or per carrier for anammox (Amx) in the zeolite-coated carrier reactor  
431 liquid and carrier biofilm samples were  $6.85 \pm 0.38/\text{mL}$  and  $5.53 \pm 0.38$  per carrier, respectively,  
432 compared to  $6.13 \pm 0.69/\text{mL}$  and  $4.84 \pm 0.54$  per carrier for the control reactor liquid and carrier  
433 biofilm samples, respectively. This equated to a statistically greater percent of Amx genes in the  
434 liquid of the zeolite-coated ( $10.02 \pm 9.91\%$ ) versus control carrier ( $4.64 \pm 5.90\%$ ) reactors (P =  
435 0.01557). There was also a greater percent of Amx genes in the carrier biofilm in the zeolite-  
436 coated ( $1.6 \pm 0.49\%$ ) versus control carrier ( $0.33 \pm 0.31\%$ ) reactors, but only at the 90%  
437 confidence level (P = 0.07359). When coupled with the chemical data, these results suggest that  
438 the zeolite-coated carriers were able to enhance the retention, and likely the activity, of the  
439 anammox bacteria in the system. Amx gene copies per mL decreased on Day 25 in the liquid of  
440 the zeolite-coated reactors, but not in the carrier biofilm samples. This was thought to be a result  
441 of the lack of nitrite in the feed on Day 25. The control reactors appeared to be less affected by  
442 the lack of nitrite, with no clear decline of Amx gene copies per mL occurring with the lack of  
443 nitrite addition.

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**Figure 11. qPCR results from the CFTR experiment for the A) 16S rRNA, B) Amx, C) *amoA*, D) *nirS*, E) *nirK*, and F) *nosZ* genes, showing the log number copies per carrier for the carrier biofilm samples and the log number copies per mL for the reactor liquid from CFTR. Light grey indicates samples from control carrier reactors and**

450 dark grey indicates samples collected from zeolite-coated carrier reactors. Error bars  
451 show the standard deviation of the reactors run in triplicate.

452

453 Both reactors also showed excellent nitrite removal and little nitrate production, with effluent  
454 nitrite concentrations of  $0.069 \pm 0.27$  mg-N/L and 0 mg-N/L for the zeolite-coated and control  
455 carrier reactors, respectively, and effluent nitrate concentrations of  $0.23 \pm 0.33$  mg-N/L and  $0.28$   
456  $\pm 0.35$  mg-N/L for the zeolite-coated and control carrier reactors, respectively (Figure 10). This  
457 suggests that denitrification was occurring in both treatments. Not surprisingly, denitrifiers,  
458 quantified by the number of *nirK*, *nirS* and *nosZ* gene copies per mL or per carrier present, were  
459 detected in the bulk liquid and carrier biofilm samples in both reactors. The *nirS* ( $P = 0.037$ ) and  
460 *nosZ* ( $P = 0.0071$ ) genes were significantly enriched in the reactors containing zeolite-coated  
461 carriers (Figure 11), with the carrier biofilm samples containing average log *nirS* and log *nosZ*  
462 gene copies of  $8.93 \pm 0.66$  and  $8.79 \pm 0.58$  per zeolite-coated carrier, respectively, compared to  
463  $8.78 \pm 0.34$  and  $8.62 \pm 0.26$  per control carrier, respectively (Figure 11). On Day 25, *nirK*, *nirS*,  
464 and *nosZ* copies per mL in the liquid decreased in the zeolite-coated carrier reactors, likely from  
465 the lack of nitrite in the influent. A similar decrease was not observed in the carrier biofilm  
466 samples, suggesting, as with the anammox bacteria, that the denitrifying communities on the  
467 carriers were more stable. Again, as observed with the Amx genes, a similar decrease was not  
468 observed in the control carrier reactors.

469

470 Another group of nitrogen-cycling bacteria that was analyzed in these reactors was the  
471 ammonium oxidizing bacteria, specifically, the *amoA* gene. Interestingly, even with no oxygen  
472 supplied to the reactors, the log *amoA* gene copies per mL in the bulk liquid of the zeolite-coated

473 carrier reactors ( $5.24 \pm 0.29/\text{mL}$ ) was significantly higher than that in the control reactors ( $4.83 \pm$   
474  $0.37/\text{mL}$ ) ( $P = 0.009$ ) (Figure 11). The carrier biofilm samples themselves did not have  
475 significantly different numbers of *amoA* gene copies per carrier ( $P = 0.50$ ), perhaps because of  
476 the lack of oxygen supply within the reactors. There was no significant difference in log 16S  
477 rRNA gene copies per mL or per carrier in either the bulk liquid or carrier biofilm samples  
478 between the zeolite-coated carrier and control carrier reactors ( $P = 0.9244$  for the carrier biofilm  
479 samples and  $P = 0.1810$  for the bulk liquid samples).

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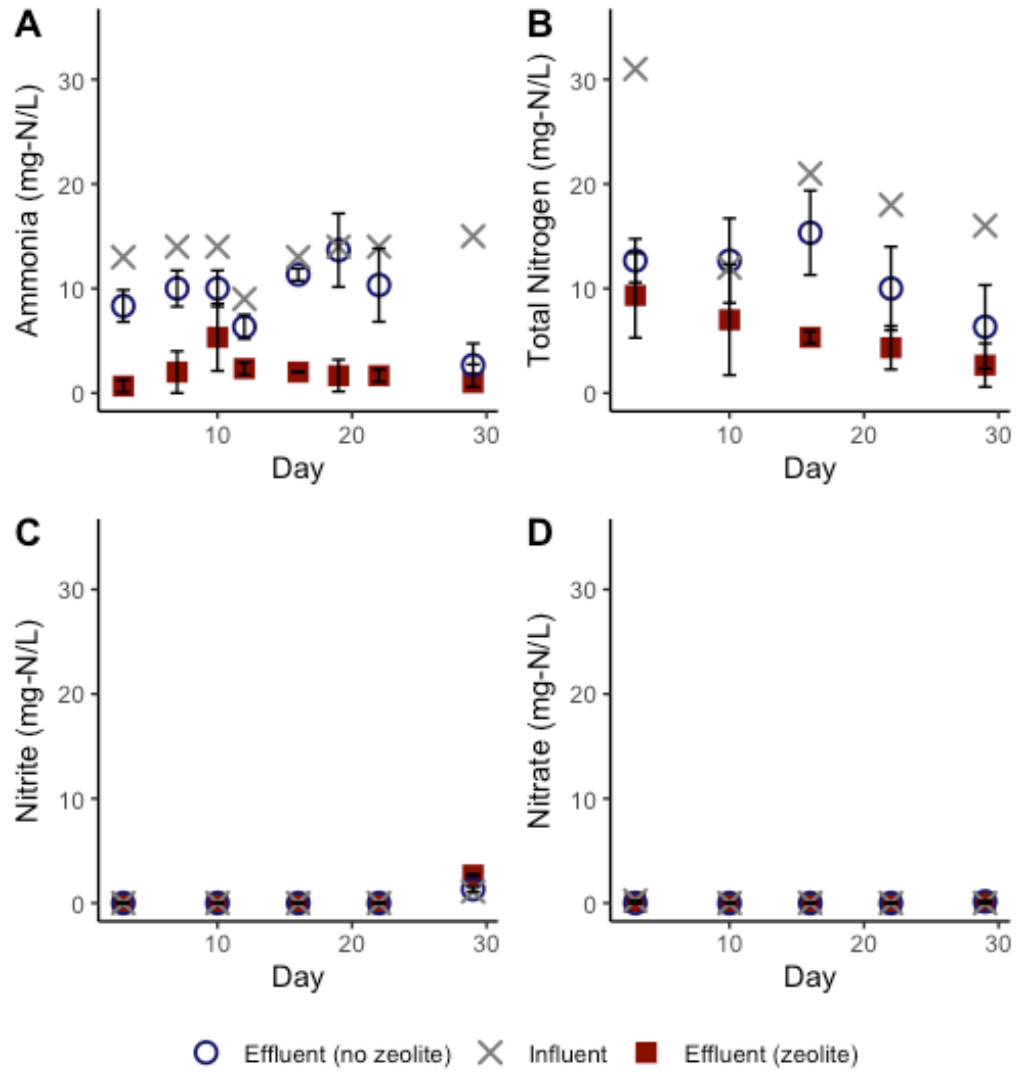
481 Overall, Amx genes were in higher abundance in the carrier biofilm samples and bulk liquid  
482 samples in the zeolite-coated carrier reactors compared to the control reactors, with some  
483 denitrifying genes, *nirS* and *nosZ*, also in greater abundance in these samples (Figure 11). The  
484 bulk liquid in the reactors containing zeolite-coated carriers also had higher numbers of *amoA*  
485 genes compared to the liquid in the control reactors. This indicates that the presence of the  
486 zeolite coating on these novel carriers did attract a unique microbial community, not only on the  
487 carrier surface, but also within the reactor bulk liquid. This provides evidence that the  
488 combination of zeolite-facilitated abiotic ammonium sorption with the apparent zeolite-enhanced  
489 retention/enrichment of N-cycling bacteria improves total nitrogen removal under mainstream-  
490 like operating conditions (Figure 9).

491

492 ***Aerated carrier flow-through reactors.*** To determine whether operating the system with active  
493 aeration would encourage more substantial colonization of AOB in the reactors containing  
494 zeolite-coated carriers, the experiment was repeated with no added nitrite in the influent and with  
495 active aeration within each reactor. DO levels were high in the bulk reactor liquid throughout the

496 experiment, with  $95.1 \pm 6.5\%$  and  $89.9 \pm 20.0\%$  of DO saturation measured in the zeolite-coated  
497 carrier and control carrier reactors, respectively. Over the course of the 30-day experiment, the  
498 reactors containing zeolite-coated carriers again removed significantly more ammonium and TN,  
499 and therefore had much lower effluent ammonium ( $2.1 \pm 1.9$  mg-N/L) and TN ( $6.5 \pm 3.6$  mg-  
500 N/L) concentrations compared to control reactors ( $9.1 \pm 3.7$  mg-N/L and  $12.7 \pm 3.7$  mg-N/L for  
501 ammonium and TN, respectively) ( $P < 0.0001$  for ammonium and  $P = 0.0012$  for TN) (Figure 11).  
502 As with the previous experiment, effluent nitrite and nitrate concentrations were low and very  
503 similar in the two types of reactors ( $P = 0.85$  and  $P = 0.83$  for nitrite and nitrate respectively),  
504 which suggests that either ammonium sorption or ammonium sorption, oxidation, and rapid  
505 denitrification on the carrier surface was occurring in the zeolite-coated carrier reactors (Figure  
506 12). Log *amoA* copies were  $5.55 \pm 0.24$ /mL and  $5.41 \pm 0.15$  per carrier in the reactor samples  
507 containing zeolite-coated carriers and  $5.20 \pm 0.40$ /mL and  $4.79 \pm 0.67$  per carrier in the control  
508 reactor samples (Figure 13). As with the CFTR experiments, the log *amoA* copies per mL or per  
509 carrier were only higher in the bulk liquid of the zeolite-coated carrier reactors, and at only a  
510 90% confidence interval, and not within the biofilm on the carriers ( $P = 0.065$  and  $P = 0.132$  for  
511 the liquid and carrier samples, respectively) (Figure 13), which suggests that ammonium  
512 oxidation was occurring in the bulk liquid, but was not significantly enhanced on the surface of  
513 the zeolite-coated carriers.

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**Figure 12. Influent and effluent concentrations of A) Ammonium, B) TN, C) Nitrite,**

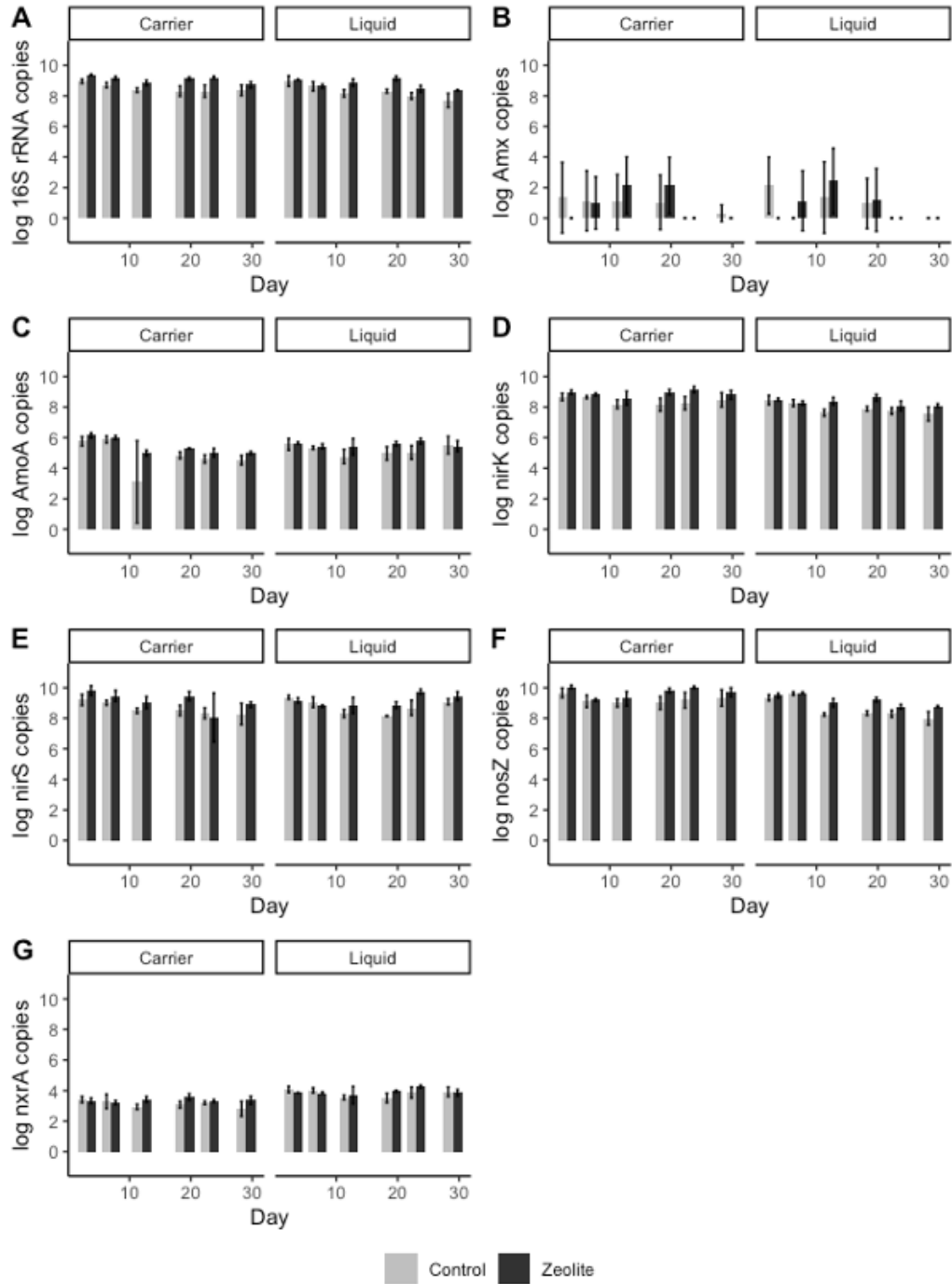
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**and D) Nitrate in the ACFTR experiment.** Error bars indicate the standard deviation of

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triplicate reactors.

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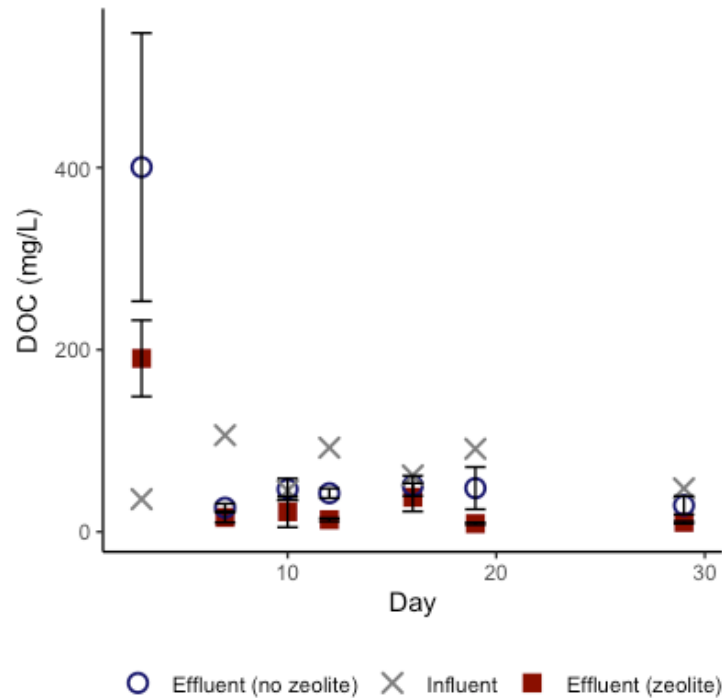
**Figure 13. qPCR results from the ACFTR experiment for the A) 16S rRNA, B) Amx, C) *amoA*, D) *nirK*, E) *nirS*, F) *nosZ*, and G) *nxrA* genes, showing the log number copies per carrier for the carrier biofilm samples and the log number copies per mL for the reactor liquid from ACFTR. Light grey indicates samples from control**



525 carrier reactors and dark grey indicates samples collected from zeolite-coated carrier  
526 reactors. Error bars show the standard deviation of the reactors run in triplicate.  
527  
528 Unexpectedly, 16S rRNA gene copies per carrier were significantly higher in the carrier biofilm  
529 and were also higher at the 90% confidence interval in the reactor bulk liquid in samples taken  
530 from the reactors containing zeolite-coated carriers compared to samples taken from control  
531 reactors ( $P = 0.0087$  and  $P = 0.065$  and for carrier biofilm and reactor liquid samples,  
532 respectively) (Figure 13). In addition, the zeolite-coated carriers had higher quantities of *nirK* ( $P$   
533  $= 0.009$ ), *nosZ* ( $P = 0.026$ ), and *nxrA* ( $P = 0.0411$ ) per carrier than the control carriers (Figure  
534 13). In the liquid samples, only *nirK* was in higher quantities per mL, and only at a 90%  
535 confidence interval, in the zeolite-coated carrier reactors compared to the control reactors ( $P =$   
536  $0.065$ ). Consistent with these higher biomass numbers, effluent DOC was significantly lower  
537 ( $P < 0.0001$ ) in the zeolite-coated carrier reactors ( $18.1 \pm 13.0$  mg/L) compared to that in the  
538 control carrier reactors ( $40.6 \pm 14.3$  mg/L) (Figure 14).  
539  
540 The higher DOC and HRT of 17 hours might not have facilitated substantial autotrophic  
541 ammonium oxidation (Figure 12) in this experiment but did appear to lead to abundant  
542 heterotrophic growth. Indeed, the zeolite-coated carriers did accumulate greater quantities of  
543 bacteria when compared to the control carriers, and this community included denitrifiers and  
544 nitrite oxidizing bacteria. More research is needed to understand exactly how best to use the  
545 zeolite-coated carriers under aerated conditions to enhance the enrichment, retention, and activity  
546 of AOB, nitrite oxidizing bacteria, and denitrifiers to enhance shortcut nitrogen removal under  
547 highly aerobic conditions that are less amenable to anammox activity. Nevertheless, these

548 zeolite-coated carriers appear to be promising for deployment in both anaerobic and aerated  
549 environments.

550



551

552 **Figure 14. Influent and effluent DOC concentrations in the ACFTR experiment.**

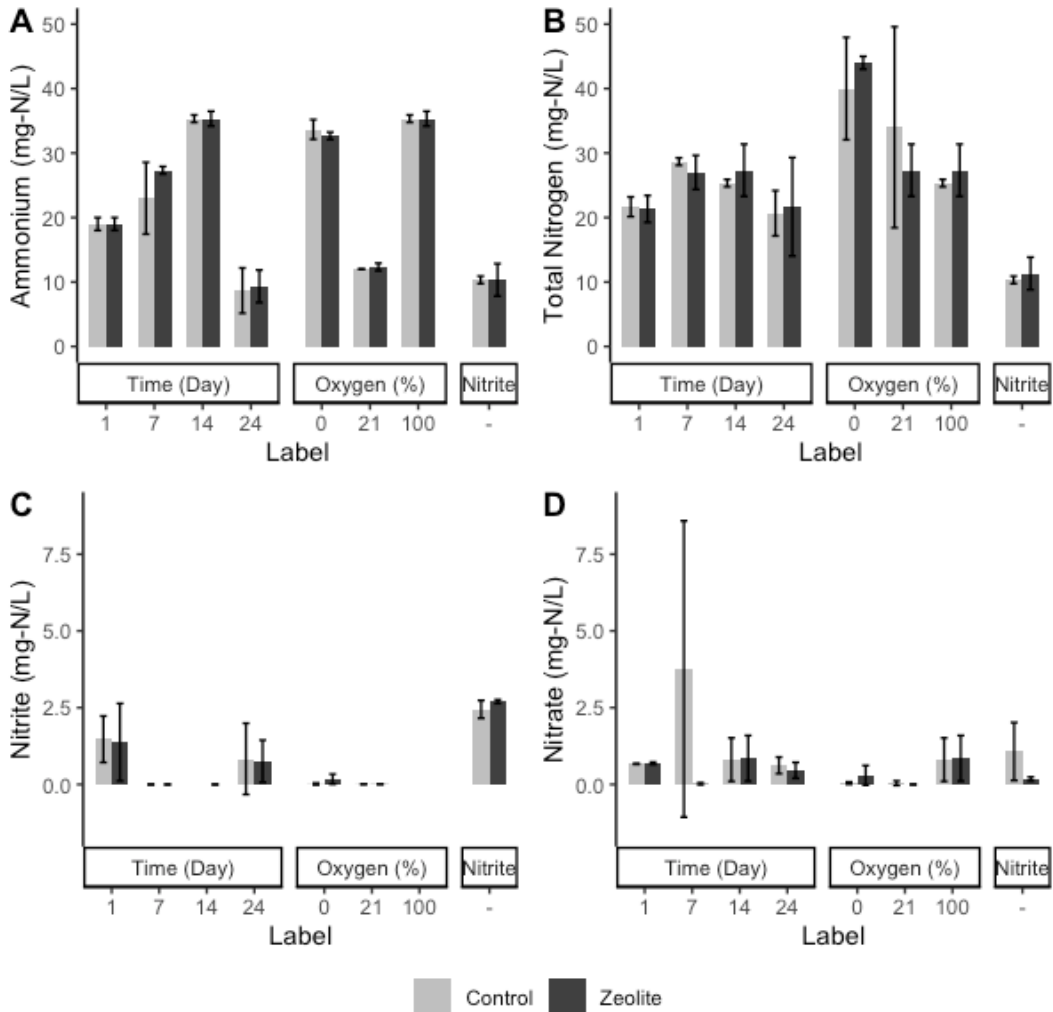
553 Error bars indicate standard deviation of triplicate experiments.

554

555 **Membrane flow-through bioreactors.** The zeolite-coated hollow fiber membranes offer another  
556 material that shows promise with respect to its ability to sorb ammonium and retain anammox  
557 bacteria.<sup>18</sup> The ability of these materials to enrich and retain anammox bacteria as well as AOB  
558 under a variety of operating conditions, however, is important for understanding how best to  
559 deploy and utilize these fibers for enhancing shortcut nitrogen removal in mainstream  
560 wastewater treatment. These experiments were not designed to achieve substantial nitrogen  
561 removal, with an HRT=bulk SRT of 23 hr and a single membrane serving as the only mechanism

562 for aerating the reactor, but rather, to determine whether differential microbial growth,  
563 particularly of AOB, could occur on the membrane surface because of the membrane's ability to  
564 both sorb ammonium and transfer oxygen. Nitrogen removal results from the final day of each  
565 experiment (Figure 15) suggest that there is perhaps some nitrification occurring, although  
566 neither the nitrite nor the nitrate effluent concentrations correlate with experiment duration or  
567 membrane lumen oxygen concentration. Additionally, there was no difference in performance  
568 between the reactors containing zeolite-coated versus plain alumina membranes. In a full-scale  
569 application, a much larger quantity of membrane surface area would need to be added to  
570 stimulate substantial ammonium oxidation.

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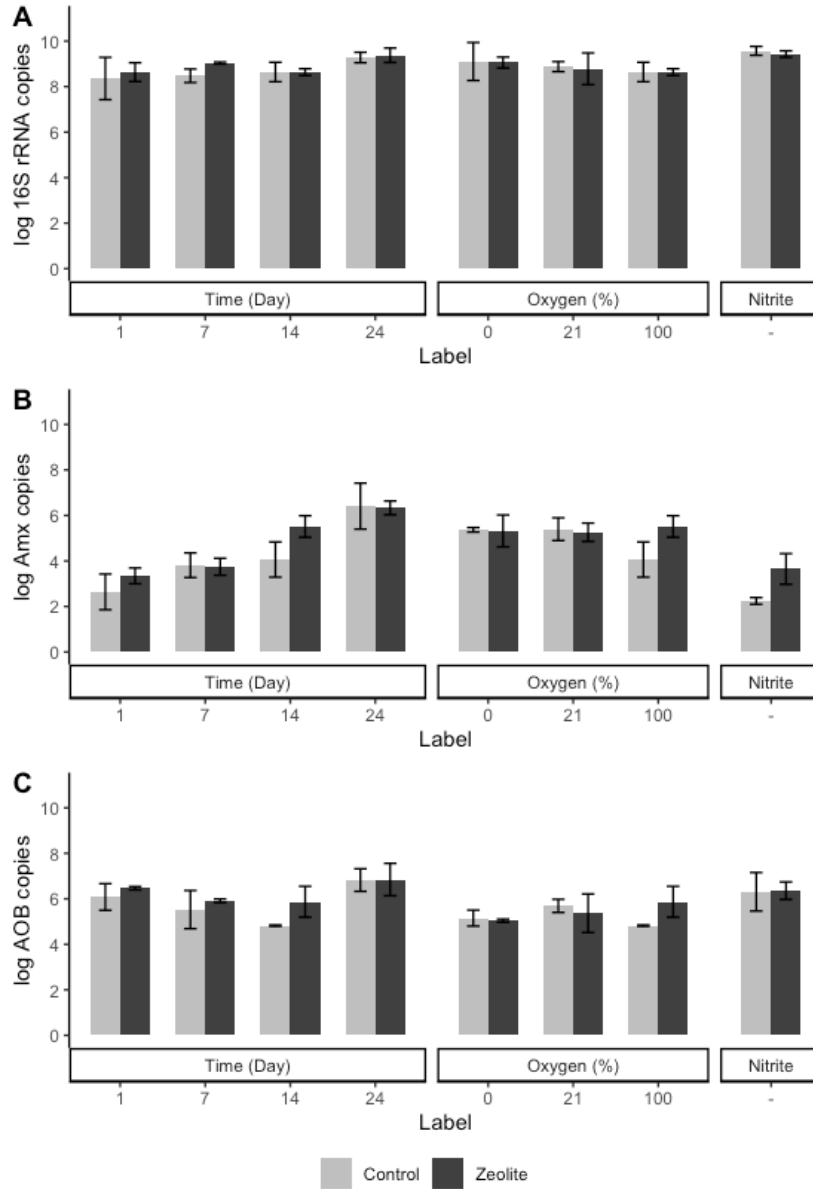
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**Figure 15. Effluent concentrations of A) Ammonium, B) TN, C) Nitrite, and D) Nitrate at the end of each of the MFTR experiments.** Labels at the bottom of each panel indicate the experiment performed. “Time (days)” indicates experiments operated for different durations of time, “Oxygen (%)” indicates the oxygen concentration supplied to the membrane lumen, and “Nitrite” indicates the experiment in which nitrite was added to the influent. The data from the 14 day and 100% oxygen experiments are the same. Light grey indicates samples from control membranes and dark grey indicates samples collected from zeolite-coated membranes. Error bars show the standard deviation of the reactors run in triplicate.

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With respect to biomass growth on the membrane surface, the results are varied, with the zeolite-coated membranes only having higher quantities of total bacteria (16S rRNA gene copies per membrane) in one experiment, the 1-week experiment ( $P = 0.044$ ), and only having higher quantities of *amoA* copies at the 90% confidence interval ( $P = 0.056$ ) in the two-week, 100% oxygen experiment (Figure 16). The quantities of anammox bacteria generally increased in both the plain alumina membrane reactors and in the zeolite-coated membrane reactors with operation time (Figure 16). As observed previously,<sup>18</sup> anammox bacteria were generally retained/enriched on the zeolite-coated membranes, with higher quantities measured in the 1-day experiment ( $P = 0.09195$ ) and significantly higher quantities measured in the two-week experiment ( $P = 0.02704$ ), as well as in the two-week experiment to which nitrite was added ( $P = 0.04128$ ). As observed with the carrier experiments, the zeolite coating only retained anammox bacteria and did not preferentially retain AOB.



596

597

**Figure 16. qPCR results from the MFTR experiments for the A) 16S rRNA, B)**

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**Amx, and C) *amoA* genes, showing the log number copies per membrane.**

599

Experiments included varied operation time, varied membrane lumen oxygen

600

concentrations, and an experiment to which nitrite was added in the influent. Light grey

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indicates samples from control membranes (plain alumina hollow fibers) and dark grey

602

indicates samples from zeolite-coated membranes (alumina hollow fiber core with zeolite

603

coating). The data from the 14-day experiment and the 100% oxygen experiment are the

604 same but are shown twice for comparison to other experiments. Error bars show the  
605 standard deviation of triplicate experimental replicates.

606

607 ***Implications for the use of biofilm supports incorporating zeolite coatings.*** Under most of the  
608 conditions tested, anammox bacteria were retained/enriched at higher quantities on zeolite-  
609 coated surfaces compared to control surfaces. This was likely a result of the zeolite-coatings  
610 concentrating ammonium at their surface as the ammonium exchanged into the zeolite cages.  
611 Anammox bacteria were also retained to a greater degree and under more experimental  
612 conditions than AOB. Even though the half saturation constant ( $K_s$ ) for anammox bacteria is low  
613 ( $0.07 \text{ g N/m}^3$ )<sup>7</sup> compared to that for AOB ( $2.4 \text{ g N/m}^3$ ),<sup>32</sup> anammox bacteria seem to grow much  
614 more effectively on surfaces with high ammonium concentrations. A possible explanation for the  
615 different behavior of anammox bacteria and AOB is the strong tendency for anammox to grow in  
616 biofilms or granules, which may have predisposed these organisms to form biofilm on the  
617 zeolite-coated carriers and membranes.<sup>33</sup> Additionally, while the half saturation constant for  
618 AOB is slightly higher than that for anammox bacteria, it is still low, indicating AOB can  
619 function well in low ammonium environments. An unexpected finding from this work was the  
620 apparent preferential retention/enrichment of denitrifiers on zeolite-coated carriers under both  
621 aerated and anaerobic conditions. This indicates that these zeolite-coated carriers should  
622 facilitate a range of shortcut nitrogen processes, including the bypass of nitrate production and  
623 denitrification via the nitrite shunt, as long as PN can be encouraged. More work is needed to  
624 better understand why denitrifying communities are retained and under what conditions AOB  
625 can be enriched and retained on zeolite-coated surfaces.

626

627 Others have also investigated zeolite particles<sup>16,34-36</sup> and carriers containing zeolite particles<sup>37</sup> as  
628 a way to retain anammox bacteria in target environments and have reported results similar to  
629 those of our study. When zeolite particles were added as media for a continuous-flow fixed bed  
630 biofilter, not only was an increase in the retention of anammox bacteria observed, but consistent,  
631 high rates of nitrogen removal (95%) were achieved and maintained over the course of 570  
632 days.<sup>36</sup> Another study added zeolite particles to sequencing batch reactors, and again, not only  
633 was anammox biomass retention improved, but the specific anammox activity in the system also  
634 increased.<sup>16</sup> A study using small spherical cages as biofilm carriers with zeolite particles inside  
635 also found increased retention of anammox bacteria compared to control carriers when operating  
636 a PNA system.<sup>37</sup> AOB were also successfully retained in this system, making up 19% of the total  
637 biomass in the attached biofilm. In our work we were specifically trying to create surfaces that  
638 could be economically mass produced (*e.g.*, PE carriers) (Feinberg et al.)<sup>19</sup> and also could be  
639 easily retained within a system that might otherwise allow zeolite particles to wash out.  
640 Nevertheless, the results of other researchers<sup>16,34-37</sup> are consistent with our findings and offer  
641 additional exciting possibilities for the application of zeolite-modified surfaces for enhanced  
642 nitrogen removal.

643

644 Potential applications for these biofilm support technologies are systems with low ammonium  
645 concentrations that would benefit from the localized concentration of ammonium and increased  
646 retention of anammox bacteria, such as mainstream wastewater treatment operated at low DO  
647 concentrations. The carbon amended in these experiments did not appear to negatively affect the  
648 selection and retention of anammox on zeolite surfaces, in fact, it appeared to facilitate greater  
649 growth of the overall carrier-supported biomass and the retention of denitrifiers. IFAS systems



650 may be of particular interest for this type of zeolite-coated carrier, providing the recycling of  
651 solids, and therefore AOB, along with the carrier biofilm-based retention of anammox bacteria.<sup>13</sup>  
652 Such systems could be retrofitted into existing activated sludge processes, reducing the need to  
653 continuously bioaugment anammox sludge for full-scale mainstream anammox nitrogen  
654 removal, as well as improve start up times for anammox activity, as biofilm carriers would be  
655 expected to be retained in the system with screens. Of course, it will be important to further test  
656 this promising novel technology with real wastewater, as contaminants in wastewater and  
657 variations in the C:N ratio could have an impact on nitrogen removal (Li et al., 2020; Madeira  
658 and de Araújo, 2021). It is possible that other applications where ammonium concentrations are  
659 low, such as in some treatment wetlands or stormwater systems, could also benefit from the use  
660 of zeolite-coated biofilm supports and the retention of anammox and denitrifying bacteria.<sup>1</sup>  
661 These systems typically are anoxic,<sup>38</sup> indicating they would also be an ideal setting for  
662 application of this technology. Nevertheless, work is needed to verify this, as the conditions for  
663 stormwater treatment (highly variable flows, periods of drying, very low ammonium  
664 concentrations) may not be consistent with biological nitrogen removal in this manner.

665

## 666 **Conclusions**

667 Zeolite-coated biofilm carriers were able to increase the removal of ammonium and total  
668 nitrogen compared to reactors containing control carriers under both aerobic and anaerobic  
669 operating conditions. In addition, under anaerobic conditions anammox bacteria and denitrifiers  
670 were preferentially retained in the bulk liquid and in the carrier biofilms in zeolite-coated carrier  
671 reactors. Aerobic ammonium oxidizers were preferentially retained in the bulk liquid of the  
672 zeolite-coated carrier reactors under both aerobic and anaerobic conditions. The zeolite-coated

673 carriers retained their ability to adsorb ammonium even when coated with biofilm, though thick  
674 biofilm did appear to block some sorption sites. The adsorbed ammonium was bioavailable.  
675 Results with zeolite-coated hollow fiber membranes were less definitive. The membranes were  
676 able to transfer oxygen and in some cases were able to preferentially retain anammox bacteria,  
677 but this was not always the case such as when 0% and 21% oxygen were fed to the membrane  
678 lumen. This suggests that additional research is needed to be able to apply such zeolite-coated  
679 hollow fiber membranes reliably to support mainstream anammox. Overall, the application of  
680 zeolite-coated carriers for promoting anammox activity and short-cut nitrogen removal in  
681 mainstream wastewater appears promising, with potential applications in other areas, such as  
682 stormwater treatment, as well.

683

#### 684 **Conflicts of interest**

685 There are no conflicts to declare.

686

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