



## Boundary Layer Flow of Williamson Hybrid Ferrofluid over A Permeable Stretching Sheet with Thermal Radiation Effects

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### ABSTRACT

This research investigated the convective boundary layer flow and heat transfer of Williamson hybrid ferrofluid over a permeable stretching sheet with thermal radiation effects. Human blood is employed as a based fluid while magnetite (Fe<sub>3</sub>O<sub>4</sub>) and copper (Cu) are taken as the hybrid ferroparticle. The study started with transforming the non-linear partial differential equation system that governed the model to a more convenience non-linear dimensionless ordinary differential equations using the similarity transformation. The transformed equations obtained then are solved numerically using the Runge-Kutta-Fehlberg (RKF45) method in Maple software. The characteristics and effects of stretching parameter, permeability parameter, thermal radiation parameter as well as the ferroparticle volume fraction in the Williamson hybrid ferrofluid towards the temperature profiles, velocity profiles as well as the Nusselt number and the skin friction coefficient are analysed and discussed. The result of this research for various pertinent parameter varies differently. It can be concluded that the increase in magnetic parameter, the Williamson parameter, the stretching parameter, and the permeability rate parameter increase the skin friction and reduced the velocity profile. Furthermore, the increase in stretching parameter, thermal radiation parameter and the permeability rate results to the increase in the Nusselt number.

## 1. Introduction

The illustration flow of pseudoplastic using model equation was proposed by Williamson [1]. It is a straightforward model which simulates the viscoelastic shear-thinning characteristics. Named as the Williamson fluid, it has a shear-thinning property where the rate of shear stress increases, the viscosity of fluid decreases which can be characterised as a fluid since the Newton's law of viscosity is disobeyed. Blood flow is one of the related examples to a Williamson fluid model. Nadeem *et al.*,

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[2-6] have extended the Williamson model to fluid flow over stretching sheet, heated surface over a stretching sheet and peristaltic flow in asymmetrical channel.

Ferrofluid was introduced early in the days to help the astronaut to travel into space. NASA invented the fluid to overcome the zero gravity in space by mixed together with fuel (base fluid) so that the fuel can be injected into the combustion chamber using magnetic force [7]. Due to the fluid characteristic which can be moved with the presence of magnetic force, it attracts researcher to further study and extend the fluid capability including fluid interaction and heat transfer. The effect of frictional and joule heating on ferrofluid are studied by Reddy *et al.*, [8] which they include both Casson and Williamson models in constructing the basic flow equations in their study. Jiao *et al.*, [9] found in their studies found that to achieve the best result of heat transfer of ferrofluid the concentration of particle and external magnetic effect has to be controlled. Saeed *et al.*, [10] claimed velocity profile gradient decrease as ferrofluid and viscosity parameter increase. Ferrofluid is also used to create new smart fluid and solar application like [11-14].

There are many researcher who are interested in researching the fluid flow past a permeable stretching sheet and credit to Crane *et al.*, [15] who was the first to studied the boundary layer flow on stretching sheet. Investigating incompressible viscous fluid flow over a stretching plate, Crane discovered that the boundary layer for fluid velocity varied linearly using analytical solution. Kumaran *et al.*, [16] stated that the researchers extended Crane studies and obtained closed form solutions. They also concluded that the wall shear stress reduction is caused by the shear thinning property of the fluid. Jusoh *et al.*, [17] found that ferrofluid exert drag force when rotation parameter increases on the stretching surface. They also claimed increase gradient of velocity profile which translate that skin friction increase when suction, magnetic and nanoparticle volume fraction parameter increase. Jahan *et al.*, [18] found in their research of boundary layer flow of nanofluid on permeable stretching/shrinking sheet that increase of suction parameter is linear with heat transfer rate. Naramgari *et al.*, [19] also stated the same founding.

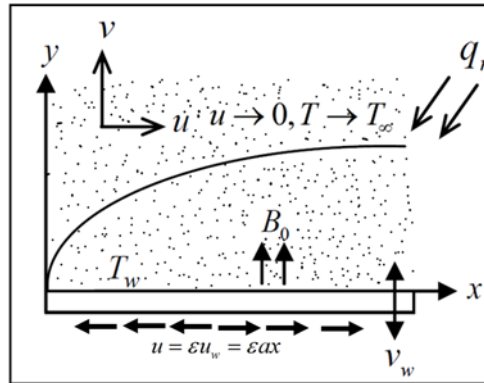
Other than conduction and convection, thermal radiation is another heat and energy transfer method, and it is the only heat transfer method that occurred without medium of transfer (vacuum). Surface temperature increases when received thermal radiation energy [20]. Since thermal radiation may affect the heat transfer on the surface, it is important to study the presence of it in this research. Recently, Kumar *et al.*, [21] analysed the impact of thermal radiation on nanofluid flow from an infinite vertical plate and establish that increasing thermal radiation parameter heightens both velocity and temperature profile. Abbas *et al.*, [22] and Megahed *et al.*, [23] both made the same claimed that skin friction and Nusselt number are in line with increasing radiation parameter. Other recent studies considering thermal radiation effects included the works by Mishra *et al.*, [24], Asghar *et al.*, [25], Daud *et al.*, [26] and Ismail *et al.*, [27].

In summary, studies on blood-based Williamson hybrid ferrofluid were not available to find. In this paper, the upgraded fluid called Williamson hybrid ferrofluid was investigated. A small amount of metal nanoparticles, copper (*Cu*) is blended with ferrofluid ( $Fe_3O_4$ ) together in Williamson fluid (blood) is believed to provide better thermal properties compared to its conventional ferrofluid. With this research it will provide fast and cheap theoretical knowledge of the upgraded fluid characteristics of heat transfer and surface interaction using mathematical formulation and numerical solution.

## 2. Mathematical Formulation

Figure 1 below illustrates a steady two-dimensional Williamson hybrid ferrofluid flow on a permeable stretching sheet with ambient temperature. Assuming that  $T = T_w$  is the wall temperature,  $u$  and  $v$  are the velocity components along the  $x$  and  $y$  axes, respectively. Next  $q_r$

is the radiative heat flux and  $B_0$  is the uniform magnetic field of strength that is assumed to be applied the positive  $y$ -directional normal to the flat plate.



**Fig. 1.** Physical model and the coordinate system

The Navier-Stoke equations that can be formed are [20,28-30]:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0, \quad (1)$$

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = \nu_{hmf} \frac{\partial^2 u}{\partial y^2} + \sqrt{2} \nu_{hmf} \Gamma \frac{\partial u}{\partial y} \frac{\partial^2 u}{\partial y^2} - \frac{\sigma B_0^2(x)}{\rho_{hmf}} u, \quad (2)$$

$$u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \frac{k_{hmf}}{(\rho C_p)_{hmf}} \frac{\partial^2 T}{\partial y^2} - \frac{1}{(\rho C_p)_{hmf}} \frac{\partial q_r}{\partial y}. \quad (3)$$

with boundary conditions:

$$\begin{aligned} u = \epsilon u_w = \epsilon ax, \quad v = v_w, \quad T = T_w \quad \text{at } y = 0 \\ u \rightarrow 0, \quad T \rightarrow T_\infty, \quad \text{as } y \rightarrow \infty \end{aligned} \quad (4)$$

$\epsilon$  is a stretching parameter and  $v_w$  is a plate permeability rate. Using the Rosseland approximation for radiation, the radiative heat flux is simplified as [31]:

$$q_r = -\frac{4\sigma^*}{3k^*} \frac{\partial T^4}{\partial y} \quad (5)$$

where  $\sigma^*$  and  $k^*$  are the Stefan-Boltzmann constant and the mean absorption coefficient, respectively. The hybrid ferrofluid kinematic viscosity, a dynamic viscosity, a density, and the electric conductivity are denoted as  $\nu_{hmf}$ ,  $\mu_{hmf}$ ,  $\rho_{hmf}$  and  $\sigma$  respectively. Furthermore,  $\Gamma$ ,  $k_{hmf}$  and  $(C_p)_{hmf}$  are the time constant, the thermal conductivity and the heat capacity of Williamson hybrid ferrofluid respectively. Other properties related to base fluid and the nanoparticles are denoted with subscript  $bf$  and  $s1,s2$  respectively. We assume that the temperature differences within the flow through the

fluid such as that the term  $T^4$  may be expressed as a linear function of temperature. Hence, expanding  $T^4$  in a Taylor series about  $T_\infty$  and neglecting higher-order terms, we get:

$$T^4 \cong 4T_\infty^3 T - 3T_\infty^4 \tag{6}$$

In view of Eq. (5) and Eq. (6), Eq. (3) reduces to

$$u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \left( \frac{k_{hmf}}{(\rho C_p)_{hmf}} + \frac{16\sigma^* T_\infty^3}{3(\rho C_p)_{hmf} k^*} \right) \frac{\partial^2 T}{\partial y^2}. \tag{7}$$

The hybrid ferrofluid properties are given as [32,33]

$$\begin{aligned} \nu_{hmf} &= \frac{\mu_{hmf}}{\rho_{hmf}}, \quad \rho_{hmf} = (1 - \phi_2) \left[ (1 - \phi_1) \rho_f + \phi_1 \rho_{s1} \right] + \phi_2 \rho_{s2}, \quad \mu_{hmf} = \frac{\mu_f}{(1 - \phi_1)^{2.5} (1 - \phi_2)^{2.5}}, \\ (\rho C_p)_{hmf} &= (1 - \phi_2) \left[ (1 - \phi_1) (\rho C_p)_f + \phi_1 (\rho C_p)_{s1} \right] + \phi_2 (\rho C_p)_{s2}, \\ \frac{k_{hmf}}{k_{bf}} &= \frac{k_{s2} + 2k_{bf} - 2\phi_2(k_{bf} - k_{s2})}{k_{s2} + 2k_{bf} + \phi_2(k_{bf} - k_{s2})}, \quad \frac{k_{bf}}{k_f} = \frac{k_{s1} + 2k_f - 2\phi_1(k_f - k_{s1})}{k_{s1} + 2k_f + \phi_1(k_f - k_{s1})} \end{aligned} \tag{8}$$

the similarity variable considered are as follows [29]:

$$\eta = \left( \frac{a}{v_f} \right)^{1/2} y, \quad \psi = (av_f)^{1/2} xf(\eta), \quad \theta(\eta) = \frac{T - T_\infty}{T_w - T_\infty}, \tag{9}$$

where  $\eta$ ,  $\psi$  and  $\theta$  is a non-dimensional variable, dimensional stream function and temperature, respectively. The similarity variables Eq. (9) satisfy the continuity Eq. (1) by definition Eq. (10)

$$u = \frac{\partial \psi}{\partial y} \text{ and } v = -\frac{\partial \psi}{\partial x}. \tag{10}$$

Next, substitute the similarity variables Eq. (9) and Eq. (10) into governing Eq. (2) and Eq. (3) gives the following transformed ordinary differential equations:

$$\frac{1}{(1 - \phi_1)^{2.5} (1 - \phi_2)^{2.5} \left[ (1 - \phi_2) + \left[ (1 - \phi_1) + \phi_1 (\rho_{s1} / \rho_f) \right] + \phi_2 (\rho_{s2} / \rho_f) \right]} f''' + ff'' + \lambda f'' f' - f'^2 - Mf' = 0, \tag{11}$$

$$\frac{k_{hmf} / k_f}{(1 - \phi_2) \left[ (1 - \phi_1) + \phi_1 (\rho C_p)_{s1} / (\rho C_p)_f \right] + \phi_2 (\rho C_p)_{s2} / (\rho C_p)_f} \left( 1 + \frac{4}{3} N_R \right) \theta'' + Pr f \theta' = 0. \tag{12}$$

The boundary conditions Eq. (4) become

$$\begin{aligned} f(0) = S, \quad f'(0) = \varepsilon, \quad \theta(0) = 1, \\ f'(\eta) \rightarrow 0, \quad \theta(\eta) \rightarrow 0, \text{ as } \eta \rightarrow \infty. \end{aligned} \tag{13}$$

By definition,  $Pr = \frac{v_f (\rho C_p)_f}{k_f}$  is a Prandtl number,  $S = -\frac{v_w}{(av_f)^{1/2}}$  is the permeability parameter at the plate surface, with  $S > 0$  and  $S < 0$  corresponds for suction and injection, respectively,  $\lambda = x\Gamma \sqrt{\frac{2a^3}{v_{mf}}}$  is the Williamson fluid parameter,  $\varepsilon = \frac{a}{b}$ , ( $\varepsilon > 0$ ) is a stretching parameter,  $N_R = \frac{4\sigma^* T_\infty^3}{k^* k_{mf}}$  is the thermal radiation parameter and  $M = \frac{\sigma B_o^2(x)}{a\rho_{mf}}$  is the magnetic parameter. The physical quantities of interest are the skin friction coefficient  $C_f$  and the local Nusselt number  $Nu_x$  are given by:

$$C_f = \frac{\tau_w}{\rho_f u_w^2}, Nu_x = \frac{xq_w}{k_f(T_w - T_\infty)}, \quad (14)$$

with the surface shear stress  $\tau_w$  and the surface heat flux  $q_w$  are given by

$$\tau_w = \mu_{mf} \left( \frac{\partial u}{\partial y} + \frac{\Gamma}{\sqrt{2}} \left( \frac{\partial u}{\partial y} \right)^2 \right)_{\bar{y}=0}, q_w = -k_{mf} \left( \frac{\partial T}{\partial y} \right)_{\bar{y}=0} + q_r, \quad (15)$$

Using variables in Eq. (6) and Eq. (14) give

$$C_f Re_x^{1/2} = \frac{1}{(1-\phi_1)^{2.5}(1-\phi_2)^{2.5}} \left( f''(0) + \frac{\lambda}{2} f''(0)^2 \right) \text{ and } Nu_x Re_x^{-1/2} = -\frac{k_{mf}}{k_f} \left[ 1 + \frac{4}{3} N_R \right] \theta'(0) \quad (16)$$

### 3. Results

The non-linear ordinary differential Eq. (11) and Eq. (12) with boundary conditions Eq. (13) were solved using Runge-Kutta-Fehlberg (RKF45) method programmed in Maple software. RKF45 is a method of order 4 with an error estimator of order 5 based on the large class of Runge-Kutta method. It was developed by German mathematician, Erwin Fehlberg. RKF (45) method is used because of its stability, well-known accuracy, and it does not require initial value profile.

In this research,  $Pr$  is set to 21 due to consideration of blood as a based fluid. Following Devi *et al.*, [32], initially 0.1 vol. solid nanoparticle of  $Fe_3O_4$  ( $\phi_1 = 0.1$ ) is added into blood to form  $Fe_3O_4$ /blood ferrofluid. Next, the 0.06 solid nanoparticle of  $Cu$  ( $\phi_2 = 0.06$ ) is added into  $Fe_3O_4$ /blood ferrofluid to form the hybrid ferrofluid namely  $Fe_3O_4$ - $Cu$ /blood hybrid ferrofluid. Table 1 shows the thermophysical properties of blood, magnetite ( $Fe_3O_4$ ) and copper ( $Cu$ ). To validate the numerical method accuracy, present result was compared with previous numerical result reported by Salleh *et al.*, [29] as shown in Table 2. The result of present research for  $-\theta'(0)$  with previous result was in good agreement.

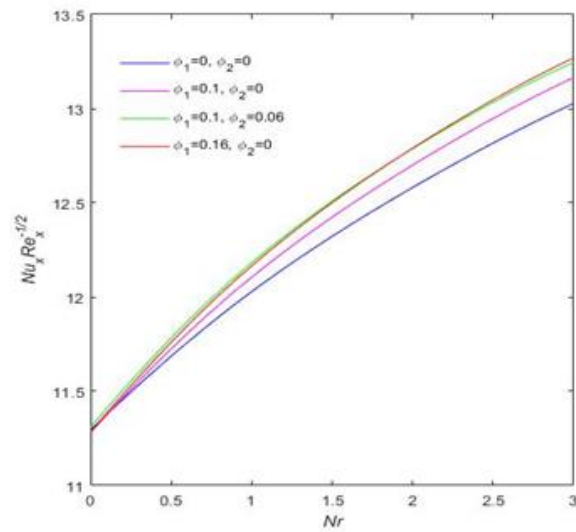
**Table 1**  
 Thermophysical properties of water, ferroparticles and copper particles [33]

Physical Properties	Blood	Magnetite ( $Fe_3O_4$ ), $\phi_1$	Copper ( $Cu$ ), $\phi_2$
$\rho$ (kg/m <sup>3</sup> )	1053	5180	8933
$C_p$ (J/kg·K)	3594	670	385
$k$ (W/m·K)	0.492	9.7	400

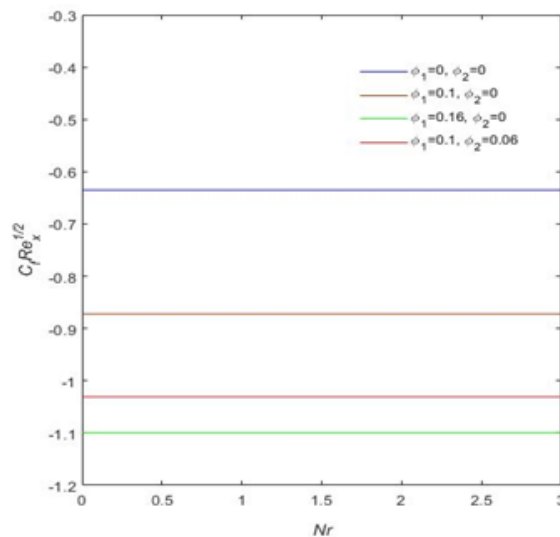
**Table 2**  
 Comparison values of  $-\theta'(0)(CWT)$  with previously published result when  $\phi_1 = \phi_2 = M = \lambda = \varepsilon = Nr = S = 0$

Pr	$-\theta'(0)$	
	Salleh <i>et al.</i> , [29]	Present Paper
0.72	0.46317	0.466972
1	0.58198	0.582663
3	1.16522	1.165164
10	2.30821	2.307950

The effects of thermal radiation parameter  $Nr$  as well as various nano particle volume fraction are illustrated in Figures 2 and 3. From Figure 2, it shows that the  $Fe_3O_4$ - $Cu$ /blood hybrid ferrofluid ( $\phi_1 = 0.1, \phi_2 = 0.06$ ) scored highest in  $Nu_x Re_x^{-1/2}$ . Physically,  $Fe_3O_4$ - $Cu$ /blood hybrid ferrofluid has better performance in heat transfer compared to blood-based viscous fluid ( $\phi_1 = \phi_2 = 0$ ) and  $Fe_3O_4$ /blood ferrofluid ( $\phi_1 = 0.1, \phi_2 = 0$ ). Its performance is almost similar with the concentrated  $Fe_3O_4$ /blood ferrofluid ( $\phi_1 = 0.16, \phi_2 = 0$ ) as  $Nr$  increases. Even though it has the same performance of heat transfer as concentrated ferrofluid, Figure 3 shows that the  $Fe_3O_4$ - $Cu$ /blood hybrid ferrofluid ( $\phi_1 = 0.1, \phi_2 = 0.06$ ) has lower skin friction compared to  $Fe_3O_4$ /blood ferrofluid ( $\phi_1 = 0.16, \phi_2 = 0$ ) but higher than blood-based viscous fluid and  $Fe_3O_4$ /blood ferrofluid ( $\phi_1 = 0.1, \phi_2 = 0$ ). This is because higher concentration of ferrofluid exert drag to the surface. Besides that, it is found that the increase of  $Nr$  does not affect the skin friction of  $Fe_3O_4$ /blood ferrofluid ( $\phi_1 = 0.1, \phi_2 = 0$ ), it produces constant  $C_f Re_x^{1/2}$  values throughout the parameter. This phenomenon is realistic where  $Nr$  has no relation with velocity term in Eq. (12). Noticed that the negative values stated in the Figure 3 refers to the opposing direction between fluid and the stretching sheet.



**Fig. 2.** Distribution of  $Nu_x Re_x^{-1/2}$  of different nano particle volume fractions for  $Nr$  when  $Pr = 21, M = 0.5, \lambda = 0.1, \varepsilon = 0.5, S = 1$



**Fig. 3.** Distribution of  $C_f Re_x^{1/2}$  of different nano particle volume fractions for  $Nr$  when  $Pr = 21, M = 0.5, \lambda = 0.1, \varepsilon = 0.5, S = 1$

Table 3 shows the result of  $Nu_x Re_x^{-1/2}$  and  $C_f Re_x^{1/2}$  for various values of magnetic parameter  $M$ . Increasing strength of magnetic effects causes inclination of  $C_f Re_x^{1/2}$  values and reduction in  $Nu_x Re_x^{-1/2}$  values. Magnetic parameter induces Lorentz force which slow down the fluid velocity via ferroparticles, thus opposes the flow and increase the skin friction values.

**Table 3**  
 Results for various values of  $M$  with  $Pr = 21, \lambda = 1,$   
 $\varepsilon = 0.5, Nr = 1, S = 0.5$

$M$	$Nu_x Re_x^{-1/2}$	$C_f Re_x^{1/2}$
0	12.2803016	-0.8688633
1	12.1087018	-1.2784927
2	11.9985094	-1.5645186
5	11.7891222	-2.1759994
10	11.5872789	-2.8826120

Next, Table 4 shows results for  $Nu_x Re_x^{-1/2}$  and  $C_f Re_x^{1/2}$  with various values of Williamson parameter. Both  $Nu_x Re_x^{-1/2}$  and  $C_f Re_x^{1/2}$  shows small changes when the Williamson parameter increases.

**Table 4**  
 Results for various values of  $\lambda$   
 with  $Pr = 21, M = 0.5, \varepsilon =$   
 $0.5, Nr = 1, S = 0.5$

$\lambda$	$Nu_x Re_x^{-1/2}$	$C_f Re_x^{1/2}$
0.1	12.1819220	-1.0990131
0.2	12.1709190	-1.1342526
0.3	12.1586059	-1.1759510
0.4	12.1446026	-1.2269258

Table 5 shows the effects of a stretching parameter  $\varepsilon$  on both  $Nu_x Re_x^{-1/2}$  and  $C_f Re_x^{1/2}$ . As  $\varepsilon$  increases, it is observed that both  $Nu_x Re_x^{-1/2}$  and  $C_f Re_x^{1/2}$  increases. Physically, as  $\varepsilon$  increases, the stretching velocity increases, thus drag the fluid together with the plate. This situation raised the temperature gradient, physically known as the reduced Nusselt number.

**Table 5**  
 Results for various values of  $\varepsilon$   
 with  $Pr = 21, M = 0.5, \lambda =$   
 $0.1, Nr = 1, S = 0.5$

$\varepsilon$	$Nu_x Re_x^{-1/2}$	$C_f Re_x^{1/2}$
0.6	12.490567	-1.362532
0.8	13.059310	-1.923475
1	13.576097	-2.523478
1.2	14.051215	-3.155929
1.4	14.491423	-3.814647

Lastly, Table 6 shows the effects of a permeability rate parameter  $S$  on both  $Nu_x Re_x^{-1/2}$  and  $C_f Re_x^{1/2}$  values. Noted that  $(S < 0)$  and  $(S > 0)$  are the injection and suction parameters respectively. It can be concluded that increasing the  $S$  parameter results to the increase in both quantities. This result is in line with the claim from Jahan *et al.*, [18] and Naramgari *et al.*, [19]. Result for permeability injection rate  $(S < 0)$  will be the opposite of permeability suction rate  $(S > 0)$  where skin friction and



Nusselt number value are decreasing. Noticed that the large injection rate effect may promote to pure conduction heat transfer process ( $Nu_x Re_x^{-1/2} \approx 0$ ).

**Table 6**  
 Results for various values of  $S$  with  $Pr = 21, M = 0.5, \varepsilon = 0.5, \lambda = 0.1, Nr = 1$

$S$	$Nu_x Re_x^{-1/2}$	$C_f Re_x^{1/2}$
-0.8	0.000123	-0.542655
-0.6	0.015589	-0.601733
-0.4	0.332867	-0.669632
-0.2	1.611840	-0.747152
0	3.933716	-0.834844
0.5	12.181922	-1.099013
1	21.683097	-1.420965
1.2	25.607000	-1.562865
1.4	29.568223	-1.710816

#### 4. Conclusions

The effects of the magnetic parameter, the Williamson parameter, the stretching parameter, the permeability rate parameter, and the thermal radiation parameter on the Nusselt number and the skin friction coefficient of blood-based Williamson hybrid ferrofluid is numerically studied. Below shows the summary of the results:

- i. The hybrid ferrofluid has same performance of heat transfer with ferrofluid with the same volume of nanoparticle volume fraction, but it provided lower values of skin friction coefficient which physically gave less erosion on surface.
- ii. Increasing all parameter resulted the increased in skin friction coefficient except for the thermal radiation parameter.
- iii. Enhancing stretching parameter, permeability rate parameter and the thermal radiation parameter raised the Nusselt number while the magnetic parameter and the Williamson parameter developed oppositely.

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