

# Prediction of energy dissipation in violent sloshing flows simulated by Smoothed Particle Hydrodynamics

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- Smoothed Particle Hydrodynamics (SPH) in brief
- SPH for sloshing flows and its current limitations
- A new SPH model for the SLOWD sloshing test case
- Energy balance and analysis of the fluid dissipation mechanisms
- Conclusions and perspectives



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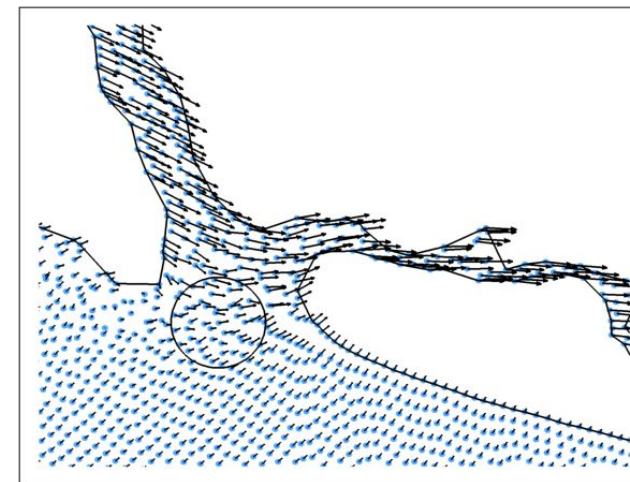
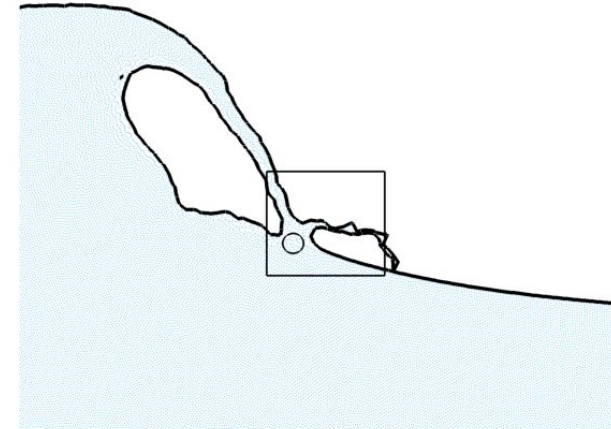
SPH is a meshless numerical method for discretizing Lagrangian PDEs

### SPH for fluids

**Meshless character:** a fluid described through a set of unconnected fluid blobs called “particles” (small fluid volumes)

**Lagrangian character:** each blob is followed in the flow according to its own motion obeying fluid dynamics equations

**Hamiltonian character:** essential conservation properties (of mass, momentum, energy) are guaranteed



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Positioning with respect to other numerical methods for free-surface flows:

	<i>Eulerian</i> (Interface Capturing/tracking) (Level Set, VOF, MAC, CIP)	<i>Lagrangian</i>
<i>Mesh Based</i>	FD Method, FEM, FVM	Particle in Cell (PIC) P-FEM
<i>Meshless</i>	FEM based on Integral Interpolation, RKPM	<b>(SPH, MPS ...)</b>



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Mathematical model: **Lagrangian formulation of N-S equations** for a barotropic fluid

$$\left\{ \begin{array}{l} \frac{D\rho}{Dt} = -\rho \operatorname{div}(\mathbf{u}) \\ \rho \frac{D\mathbf{u}}{Dt} = -\nabla p + \operatorname{div} \mathbb{V} + \rho \mathbf{g} \\ \frac{D\mathbf{r}}{Dt} = \mathbf{u}, \quad p = F(\rho) \end{array} \right.$$

- Single phase approximation (only the liquid phase is modelled)
- Surface tension is neglected
- Liquid is modelled as a **Weakly-compressible** medium ( $\text{Ma} < 0.1$ )  
→ Linearized state equation

$$p = c_0^2 (\rho - \rho_0)$$

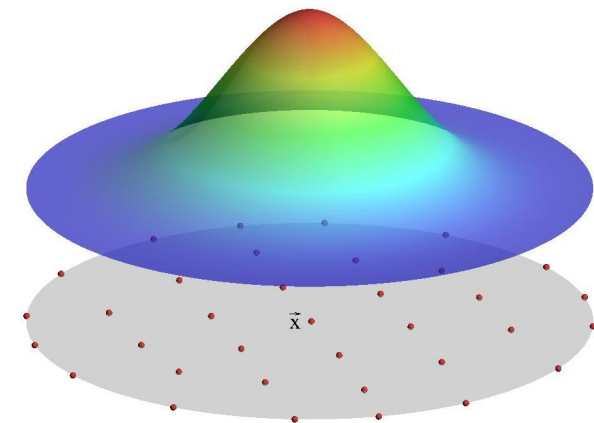




### Standard discrete SPH equations

$$\left\{ \begin{array}{l} \frac{D\rho_i}{Dt} = -\rho_i \sum_j \frac{m_j}{\rho_j} (\mathbf{u}_j - \mathbf{u}_i) \cdot \nabla_i W_{ij} \\ \frac{D\mathbf{u}_i}{Dt} = -\sum_j \frac{m_j}{\rho_i \rho_j} (p_j + p_i) \nabla_i W_{ij} + \mu \sum_j \frac{m_j}{\rho_i \rho_j} \pi_{ij} \nabla_i W_{ij} + \mathbf{g} \\ \frac{D\mathbf{r}_i}{Dt} = \mathbf{u}_i(t), \quad p = c_0^2(\rho - \rho_0) \end{array} \right.$$

Differential operators are computed as a **sum of particle interactions** weighted through a Kernel function **W**



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Advanced model  **$\delta$ -LES-SPH**: SPH with **LES filtering** for turbulence modelling

$$\begin{cases} \frac{D\rho_i}{Dt} = -\rho_i \sum_j (\mathbf{u}_j - \mathbf{u}_i) \cdot \nabla_i W(\mathbf{r}_{ij}) V_j + \sum_j \nu_{ij}^\delta \mathcal{D}_{ij} \cdot \nabla_i W(\mathbf{r}_{ij}) V_j, \\ \frac{D\mathbf{u}_i}{Dt} = \mathbf{g}_i - \frac{1}{\rho_i} \sum_j (p_i + p_j) \nabla_i W(\mathbf{r}_{ij}) V_j + \sum_j (\nu_i + \nu_{ij}^T) \pi_{ij} \nabla_i W(\mathbf{r}_{ij}) V_j, \\ \frac{D\mathbf{r}_i}{Dt} = \mathbf{u}_i, p_i = c_0^2 (\rho_i - \rho_0) \end{cases}$$

Classical Smagorinsky closure is adopted:  $\nu_T = (C_S \sigma)^2 \|\tilde{\mathbf{D}}\|$ ,

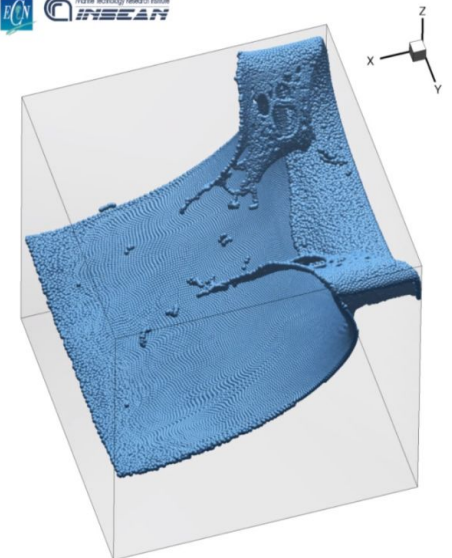
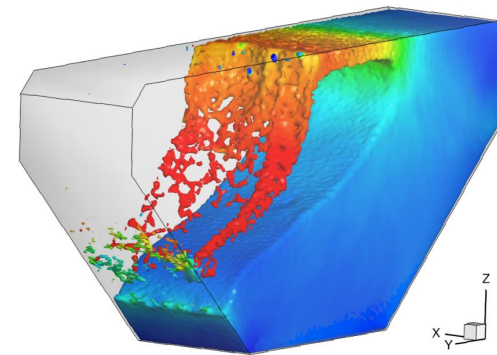
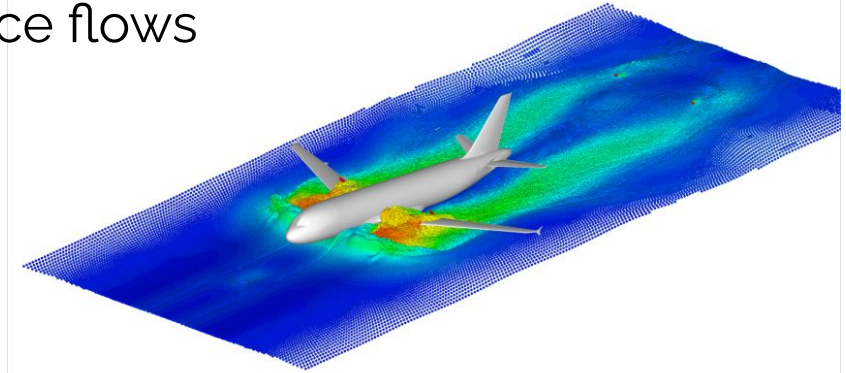
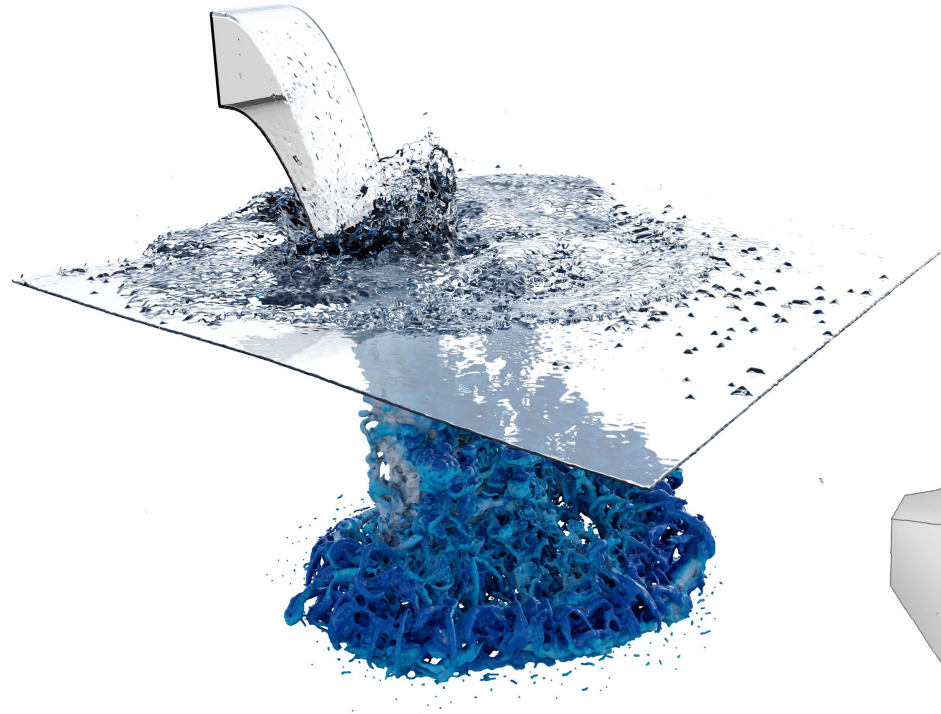
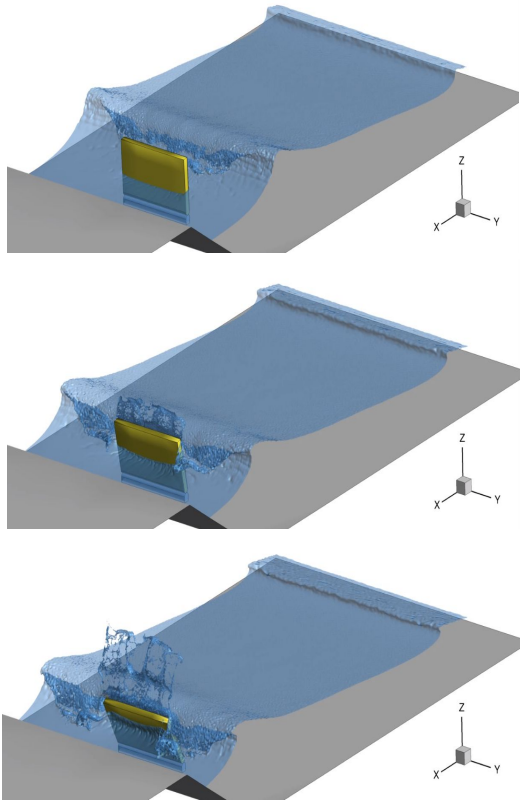
**"Smoothed Particle Hydrodynamics method  
from a large eddy simulation perspective."  
Di Mascio et al. Physics of Fluids (2017)**



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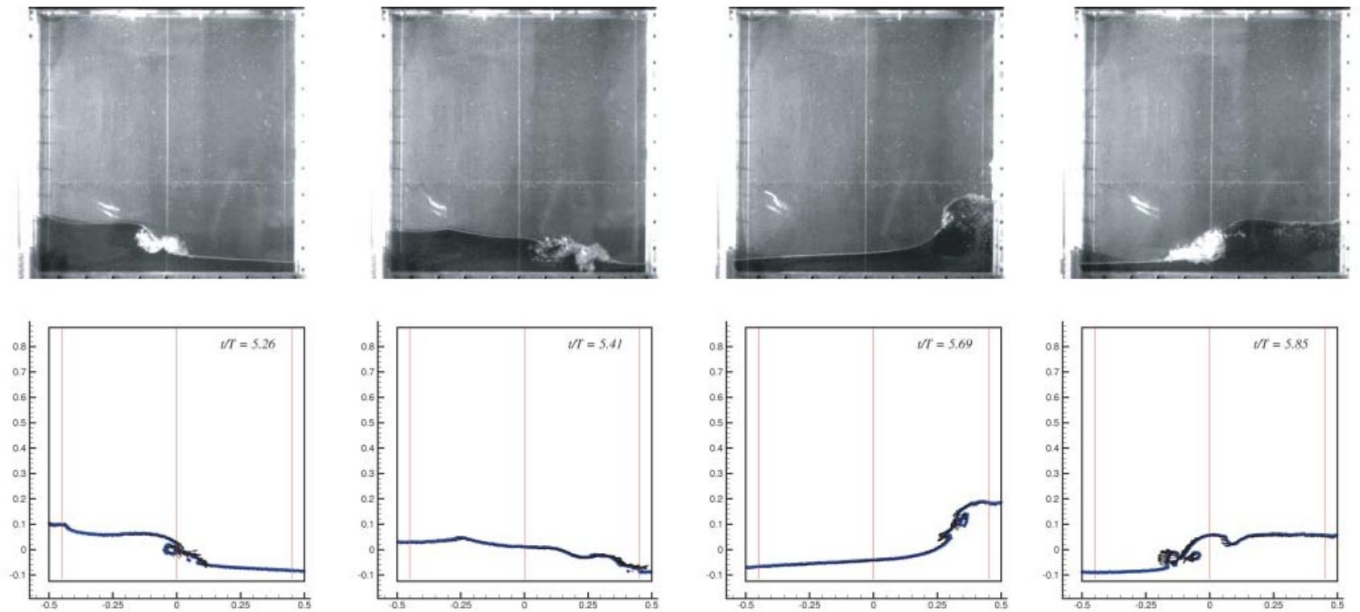
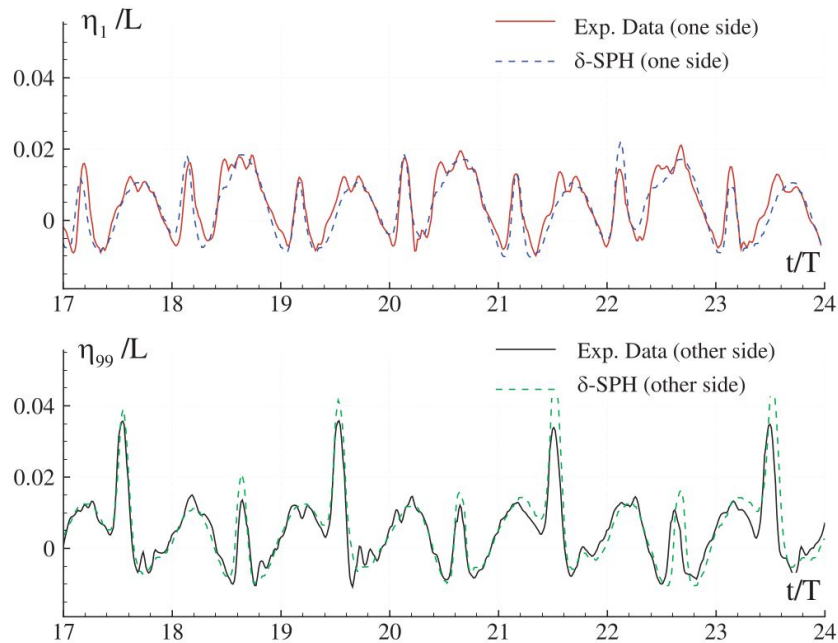
This model is particularly effective in simulating free-surface flows



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SPH has been thoroughly validated on simulation of sloshing flows

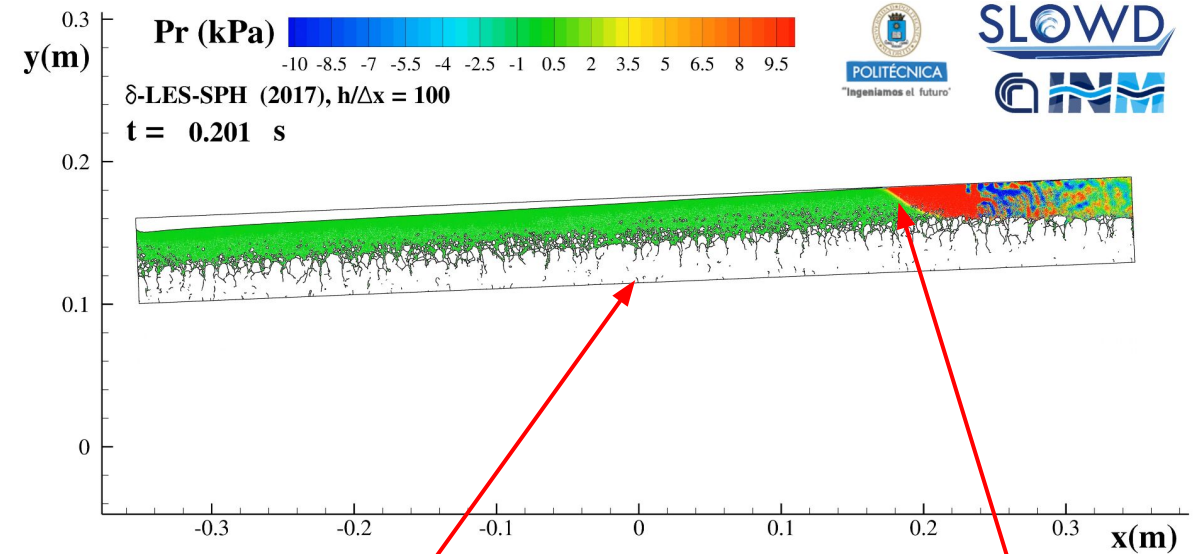
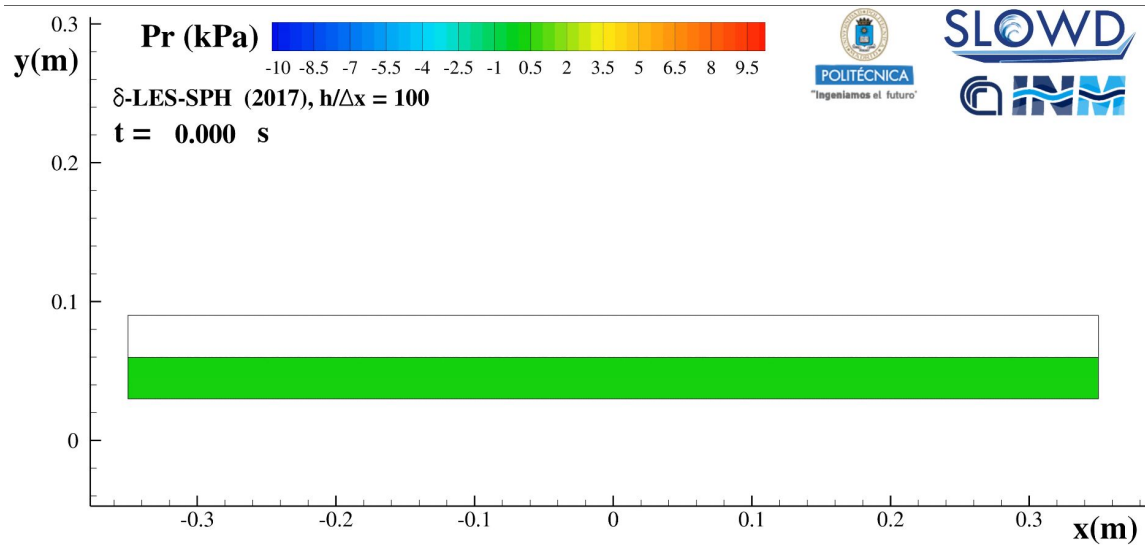


**Numerical and experimental investigation of nonlinear shallow water sloshing.**  
*Bouscasse et al . International Journal of Nonlinear Sciences and Numerical Simulation, 14(2), 2013*



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However, for very high vertical accelerations, intense negative pressure develops and “**numerical cavitation**” occurs:



Detachment of the fluid from the bottom, linked to the negative pressure value (tensile instability)

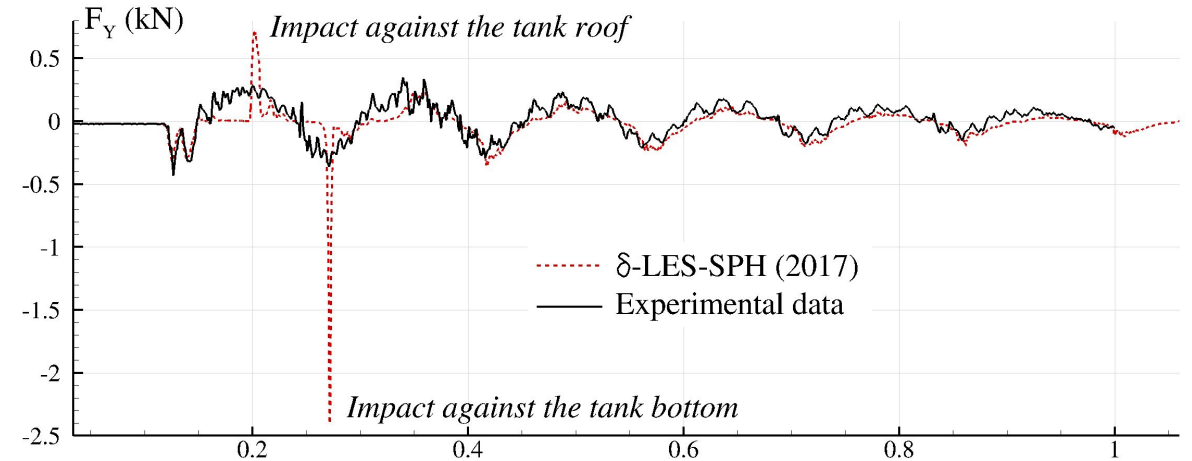
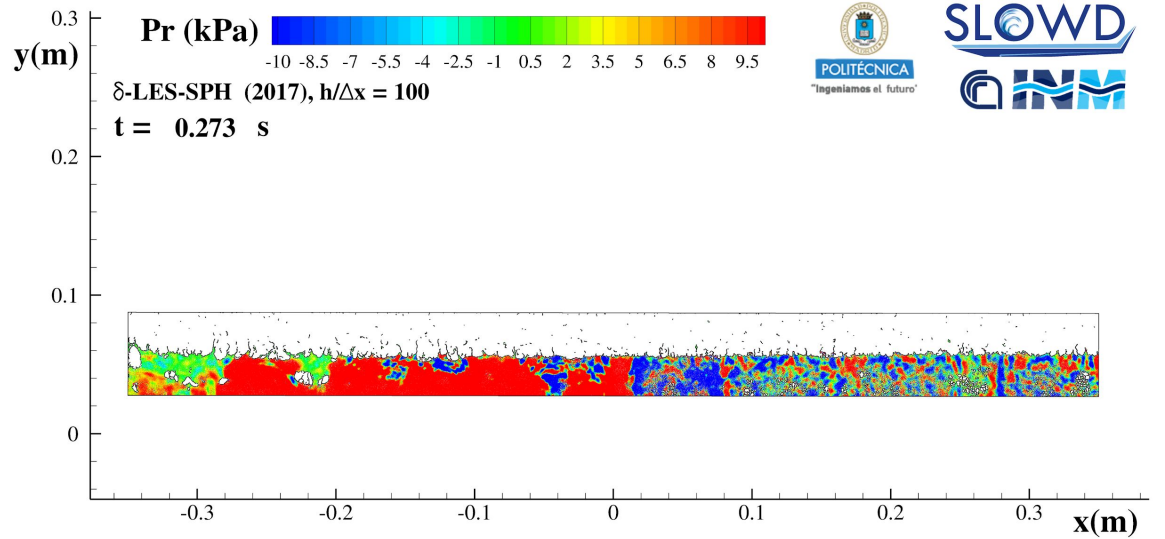
Violent pressure impact on the tank roof.



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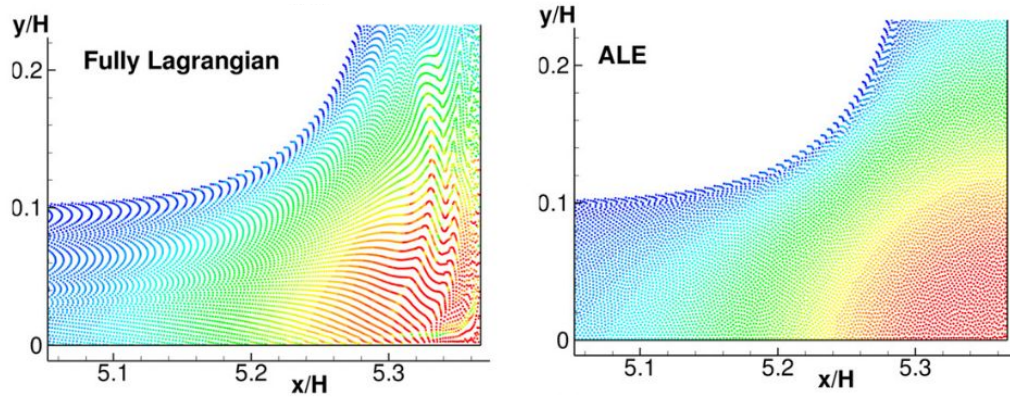
However, for very high vertical accelerations, intense negative pressure develops and “**numerical cavitation**” occurs:



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$\delta$ -LES-SPH model rewritten in an **Arbitrary Lagrangian Eulerian** framework (ALE)



Particles motion is made **quasi-Lagrangian** in order to keep particles uniformly distributed

**"SPH accuracy improvement through the combination of a quasi-Lagrangian shifting transport velocity and consistent ALE formalisms."**  
 Oger et al. *Journal of Computational Physics* 2016

$$\left\{ \begin{aligned} \frac{d\tilde{\rho}_i}{dt} &= -\tilde{\rho}_i \sum_j [(\tilde{\mathbf{u}}_j + \delta\tilde{\mathbf{u}}_j) - (\tilde{\mathbf{u}}_i + \delta\tilde{\mathbf{u}}_i)] \cdot \nabla_i W_{ij} V_j + \\ &\quad \sum_j (\tilde{\rho}_j \delta\tilde{\mathbf{u}}_j + \tilde{\rho}_i \delta\tilde{\mathbf{u}}_i) \cdot \nabla_i W_{ij} V_j + \sum_j \delta_{ij} \psi_{ji} \cdot \nabla_i W_{ij} V_j \\ \frac{d\tilde{\mathbf{u}}_i}{dt} &= -\frac{1}{\tilde{\rho}_i} \sum_j P_{ij} \nabla_i W_{ij} V_j + \frac{\rho_0}{\tilde{\rho}_i} K \sum_j \alpha_{ij} \pi_{ij} \nabla_i W_{ij} V_j + \\ &\quad \frac{\rho_0}{\tilde{\rho}_i} \sum_j (\tilde{\mathbf{u}}_j \otimes \delta\tilde{\mathbf{u}}_j + \tilde{\mathbf{u}}_i \otimes \delta\tilde{\mathbf{u}}_i) \cdot \nabla_i W_{ij} V_j \\ \frac{d\tilde{\mathbf{x}}_i}{dt} &= \tilde{\mathbf{u}}_i + \delta\tilde{\mathbf{u}}_i, \quad \tilde{p}_i = F(\tilde{\rho}_i), \quad V_i = \frac{m_i}{\tilde{\rho}_i}, \end{aligned} \right.$$

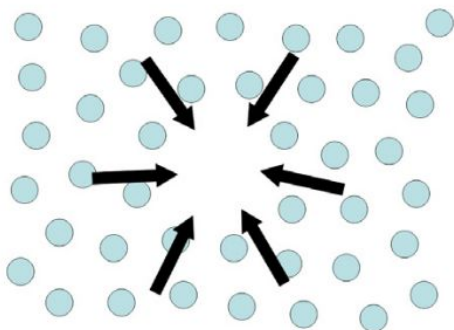


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Motion is corrected through a Particle Shifting Technique

$$\delta \hat{\mathbf{u}}_i = -M_a \ell c_0 \sum_j \left[ 1 + R \left( \frac{W_{ij}}{W(\Delta x)} \right)^n \right] \nabla_i W_{ij} V_j$$



$$\left\{ \begin{array}{l} \frac{d\tilde{\rho}_i}{dt} = -\tilde{\rho}_i \sum_j [(\tilde{\mathbf{u}}_j + \delta\tilde{\mathbf{u}}_j) - (\tilde{\mathbf{u}}_i + \delta\tilde{\mathbf{u}}_i)] \cdot \nabla_i W_{ij} V_j + \\ \sum_j (\tilde{\rho}_j \delta\tilde{\mathbf{u}}_j + \tilde{\rho}_i \delta\tilde{\mathbf{u}}_i) \cdot \nabla_i W_{ij} V_j + \sum_j \delta_{ij} \psi_{ji} \cdot \nabla_i W_{ij} V_j \\ \frac{d\tilde{\mathbf{u}}_i}{dt} = -\frac{1}{\tilde{\rho}_i} \sum_j P_{ij} \nabla_i W_{ij} V_j + \frac{\rho_0}{\tilde{\rho}_i} K \sum_j \alpha_{ij} \pi_{ij} \nabla_i W_{ij} V_j + \\ \frac{\rho_0}{\tilde{\rho}_i} \sum_j (\tilde{\mathbf{u}}_j \otimes \delta\tilde{\mathbf{u}}_j + \tilde{\mathbf{u}}_i \otimes \delta\tilde{\mathbf{u}}_i) \cdot \nabla_i W_{ij} V_j \\ \frac{d\tilde{\mathbf{x}}_i}{dt} = \tilde{\mathbf{u}}_i + \delta\tilde{\mathbf{u}}_i \quad \tilde{p}_i = F(\tilde{\rho}_i), \quad V_i = \frac{m_i}{\tilde{\rho}_i} \end{array} \right.$$





LES-Model for weakly-compressible SPH

$$\alpha_{ij} = \frac{\mu}{\rho_0} + 2 \frac{\nu_i^T \nu_j^T}{\nu_i^T + \nu_j^T}, \quad \delta_{ij} = 2 \frac{\nu_i^\delta \nu_j^\delta}{\nu_i^\delta + \nu_j^\delta}$$

$$\nu_i^T = (C_S \ell)^2 \|\tilde{\mathbf{D}}_i\|, \quad \nu_i^\delta = (C_\delta \ell)^2 \|\tilde{\mathbf{D}}_i\|$$

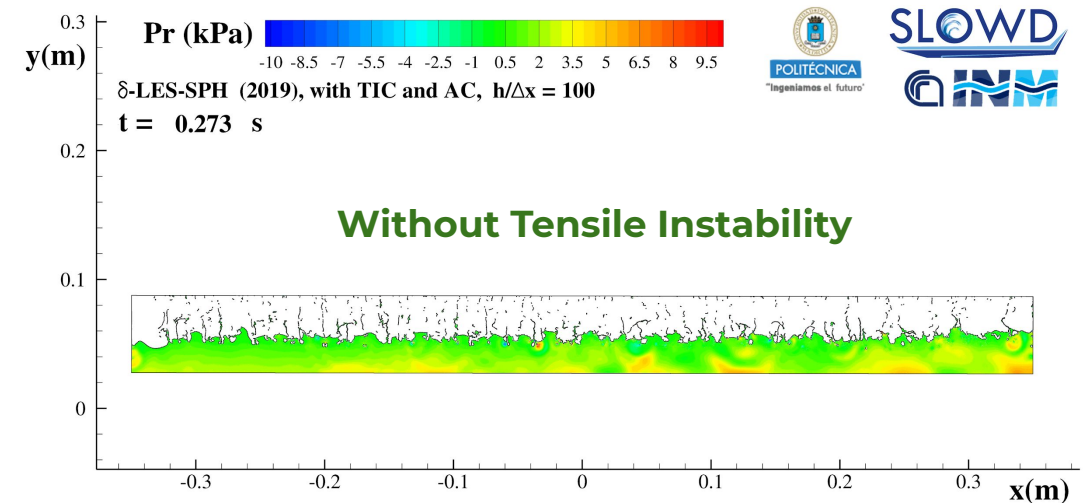
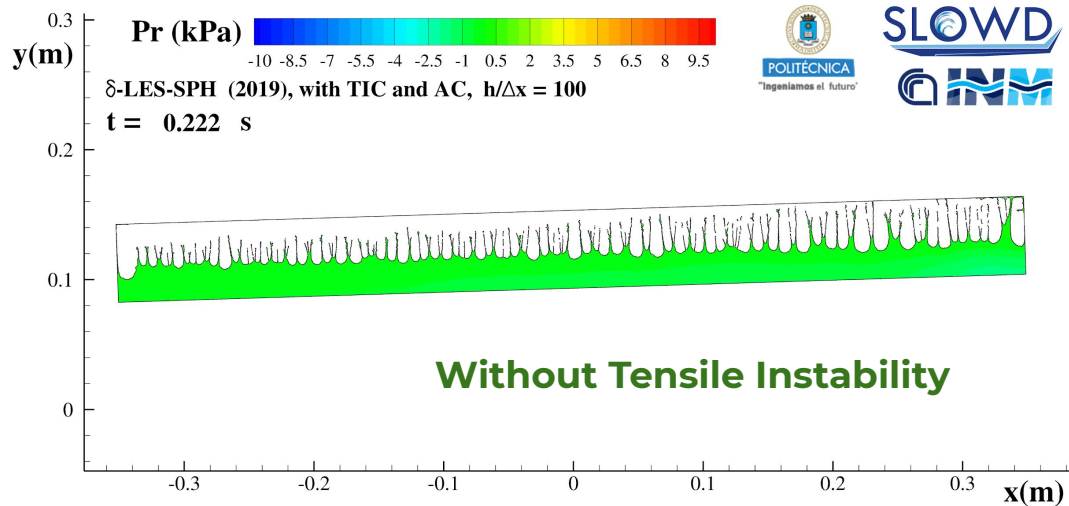
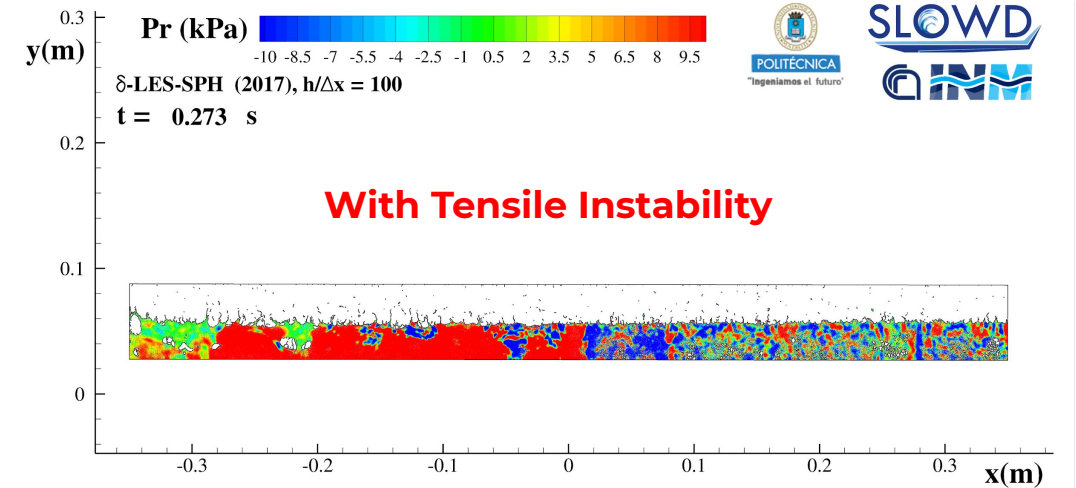
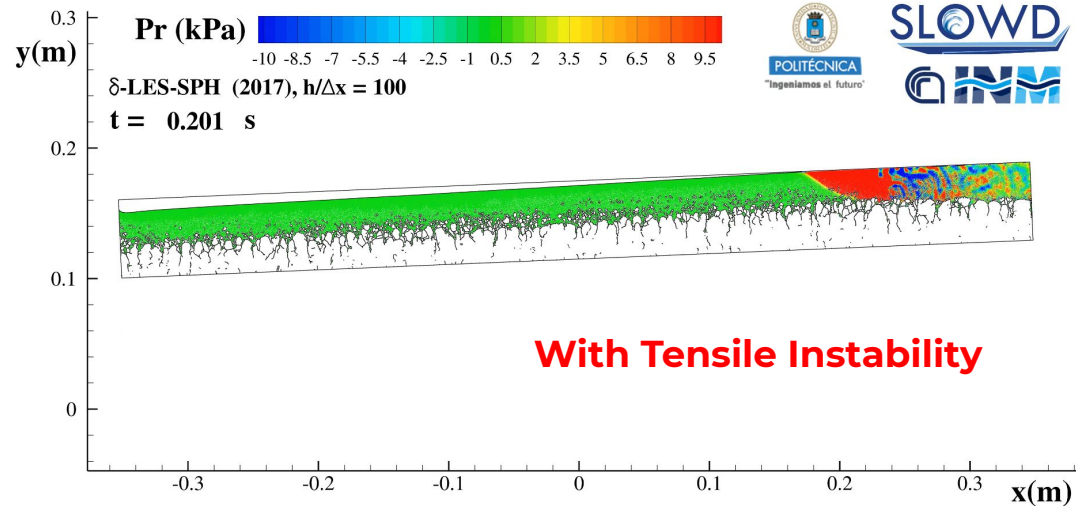
$$\left\{ \begin{aligned} \frac{d\tilde{\rho}_i}{dt} &= -\tilde{\rho}_i \sum_j [(\tilde{\mathbf{u}}_j + \delta\tilde{\mathbf{u}}_j) - (\tilde{\mathbf{u}}_i + \delta\tilde{\mathbf{u}}_i)] \cdot \nabla_i W_{ij} V_j + \\ &\quad \sum_j (\tilde{\rho}_j \delta\tilde{\mathbf{u}}_j + \tilde{\rho}_i \delta\tilde{\mathbf{u}}_i) \cdot \nabla_i W_{ij} V_j + \sum_j \delta_{ij} \psi_{ji} \cdot \nabla_i W_{ij} V_j \\ \frac{d\tilde{\mathbf{u}}_i}{dt} &= -\frac{1}{\tilde{\rho}_i} \sum_j P_{ij} \nabla_i W_{ij} V_j + \frac{\rho_0}{\tilde{\rho}_i} K \sum_j \alpha_{ij} \pi_{ij} \nabla_i W_{ij} V_j + \\ &\quad \frac{\rho_0}{\tilde{\rho}_i} \sum_j (\tilde{\mathbf{u}}_j \otimes \delta\tilde{\mathbf{u}}_j + \tilde{\mathbf{u}}_i \otimes \delta\tilde{\mathbf{u}}_i) \cdot \nabla_i W_{ij} V_j \\ \frac{d\tilde{\mathbf{x}}_i}{dt} &= \tilde{\mathbf{u}}_i + \delta\tilde{\mathbf{u}}_i, \quad \tilde{p}_i = F(\tilde{\rho}_i), \quad V_i = \frac{m_i}{\tilde{\rho}_i}, \end{aligned} \right.$$



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- Accuracy has been improved
- Tensile instability has been removed
- Numerical dissipation has been reduced
- The evaluation of energy dissipation terms is more complex due to the new particles interaction terms

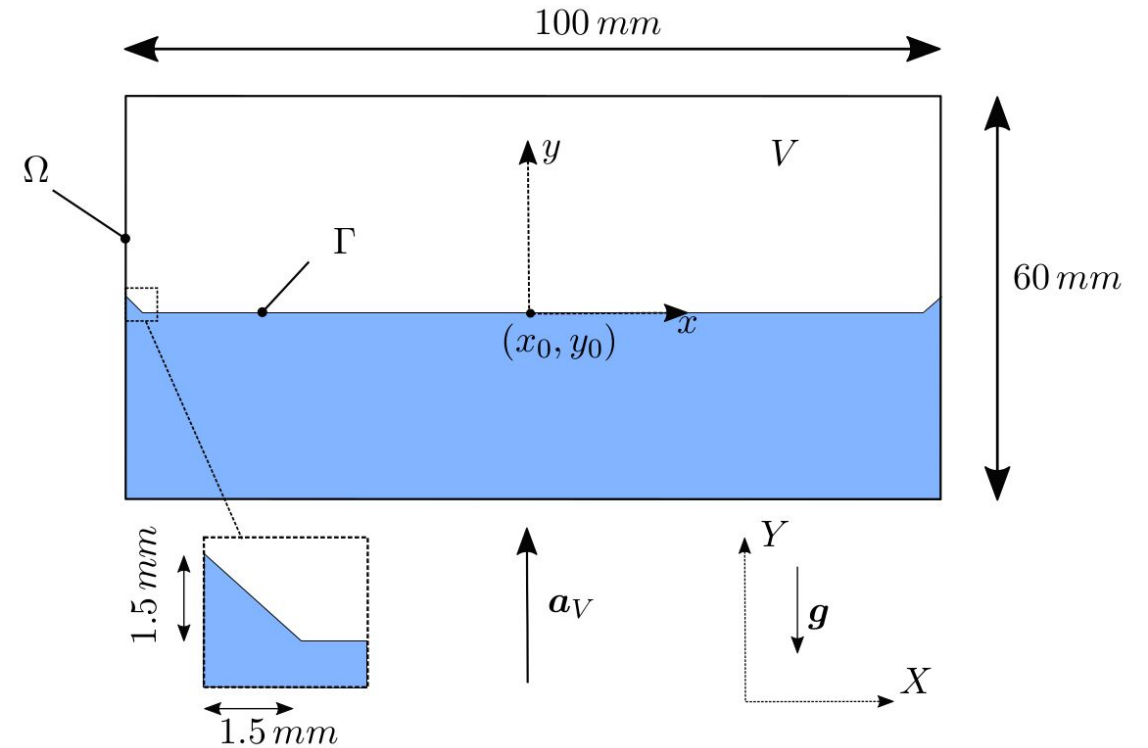
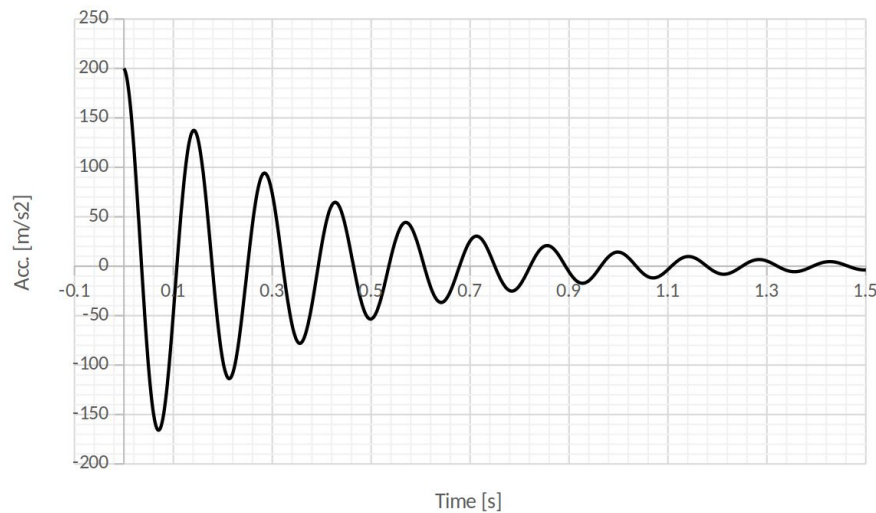
$$\left\{ \begin{aligned} \frac{d\tilde{\rho}_i}{dt} &= -\tilde{\rho}_i \sum_j [(\tilde{\mathbf{u}}_j + \delta\tilde{\mathbf{u}}_j) - (\tilde{\mathbf{u}}_i + \delta\tilde{\mathbf{u}}_i)] \cdot \nabla_i W_{ij} V_j + \\ &\quad \sum_j (\tilde{\rho}_j \delta\tilde{\mathbf{u}}_j + \tilde{\rho}_i \delta\tilde{\mathbf{u}}_i) \cdot \nabla_i W_{ij} V_j + \sum_j \delta_{ij} \psi_{ji} \cdot \nabla_i W_{ij} V_j \\ \frac{d\tilde{\mathbf{u}}_i}{dt} &= -\frac{1}{\tilde{\rho}_i} \sum_j P_{ij} \nabla_i W_{ij} V_j + \frac{\rho_0}{\tilde{\rho}_i} K \sum_j \alpha_{ij} \pi_{ij} \nabla_i W_{ij} V_j + \\ &\quad \frac{\rho_0}{\tilde{\rho}_i} \sum_j (\tilde{\mathbf{u}}_j \otimes \delta\tilde{\mathbf{u}}_j + \tilde{\mathbf{u}}_i \otimes \delta\tilde{\mathbf{u}}_i) \cdot \nabla_i W_{ij} V_j \\ \frac{d\tilde{\mathbf{x}}_i}{dt} &= \tilde{\mathbf{u}}_i + \delta\tilde{\mathbf{u}}_i, \quad \tilde{p}_i = F(\tilde{\rho}_i), \quad V_i = \frac{m_i}{\tilde{\rho}_i}, \end{aligned} \right.$$





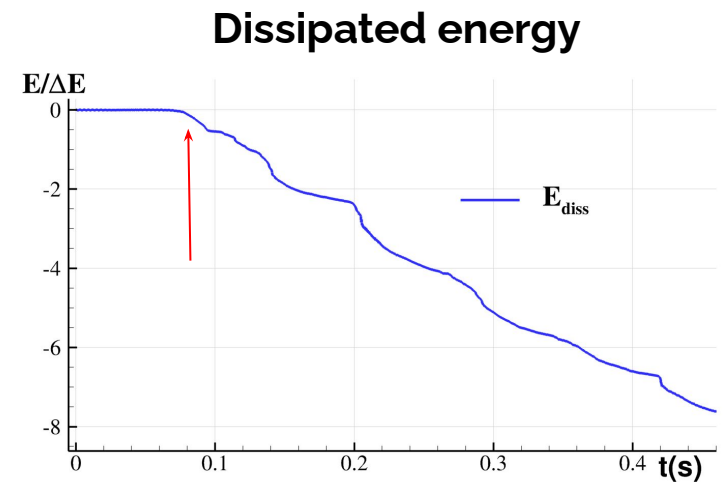
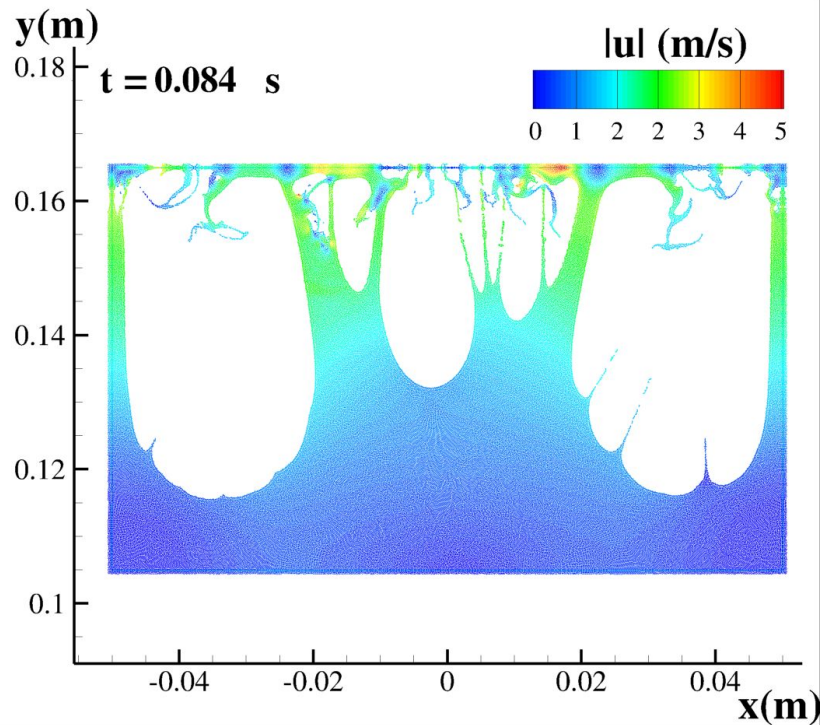
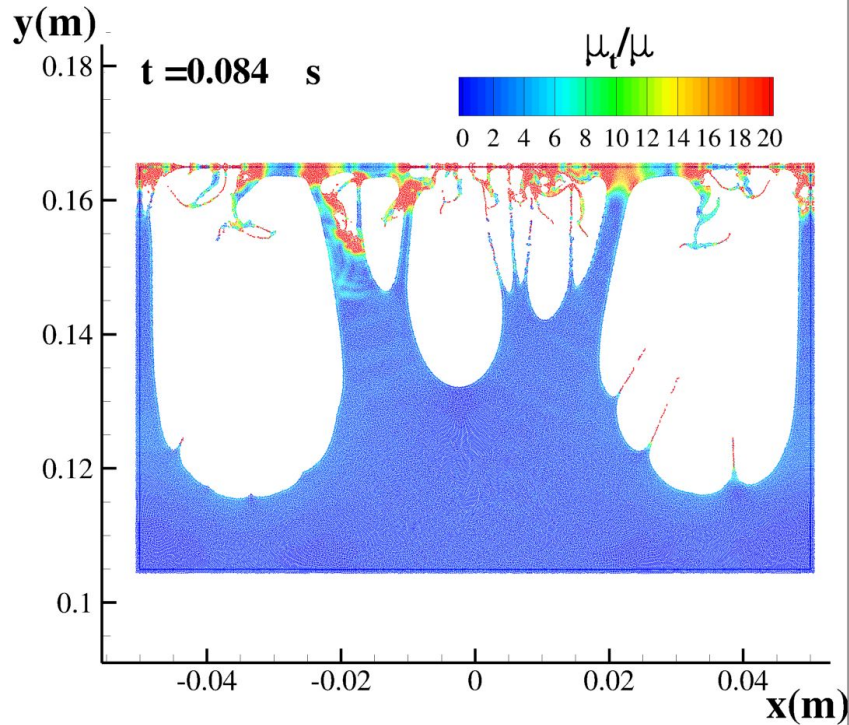
Analytical law of the tank motion

$$a(t) = a_0 e^{\lambda t} \cos(\omega t)$$

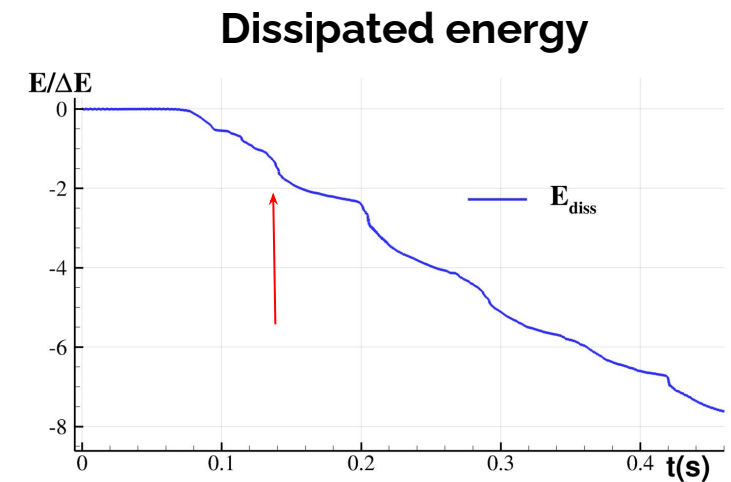
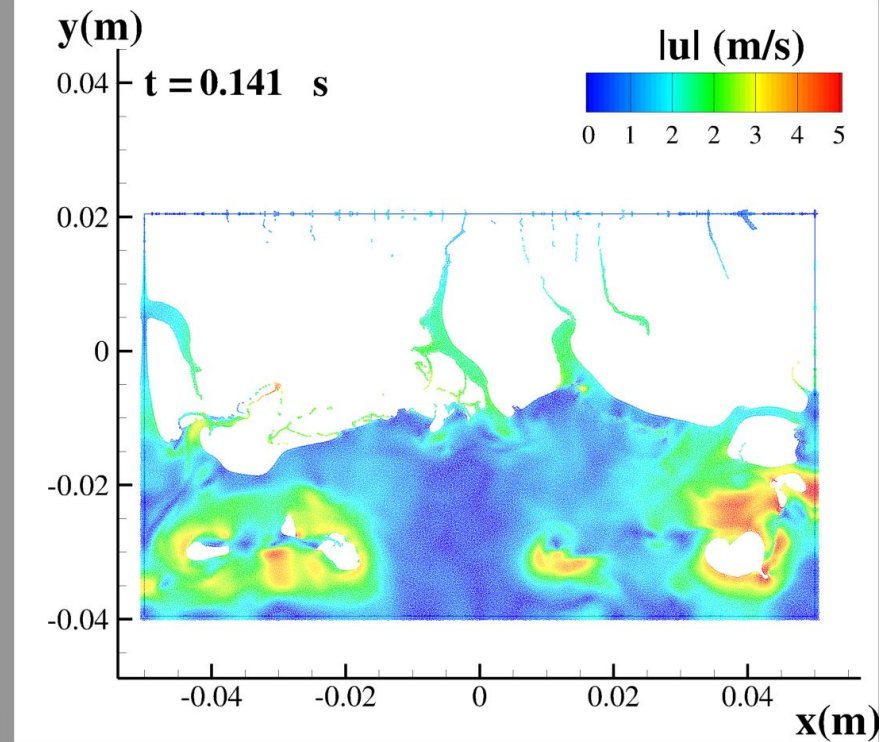
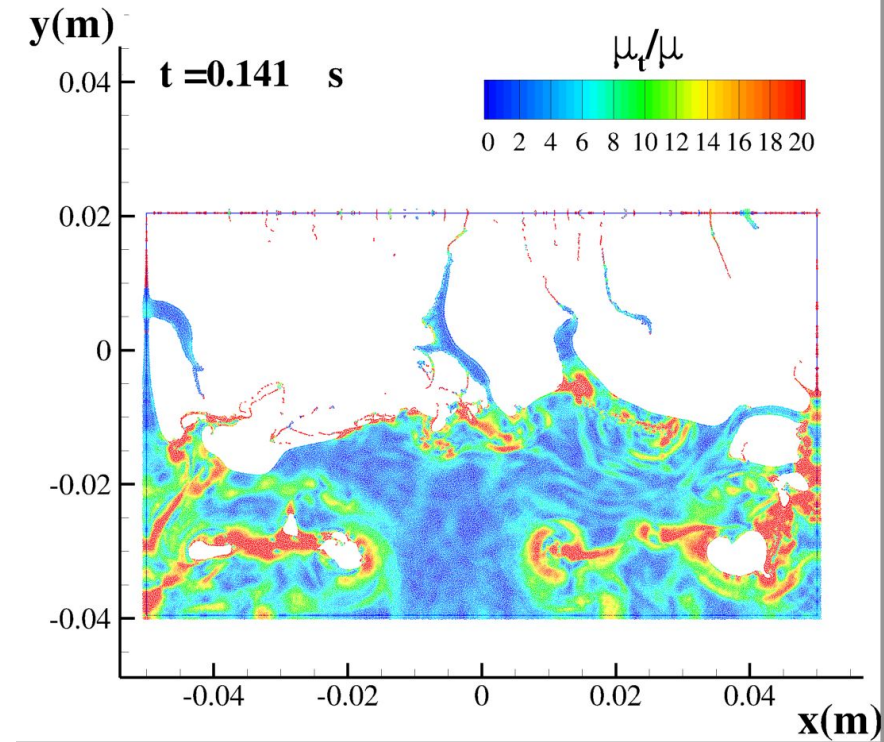


A **simplified liquid meniscus** at wall is added

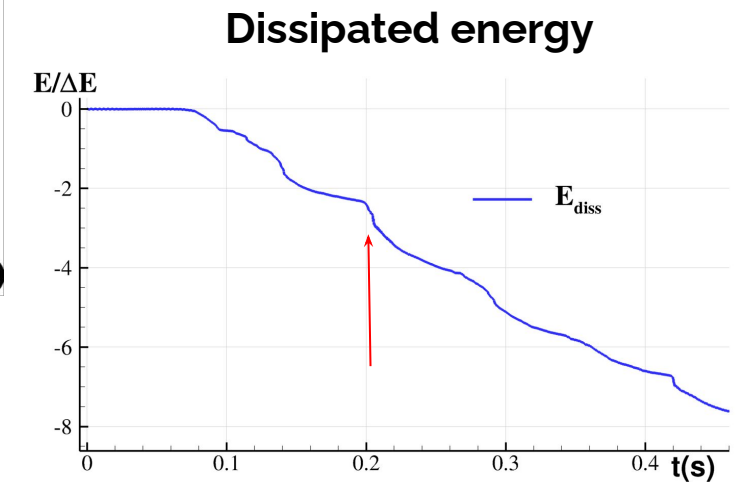
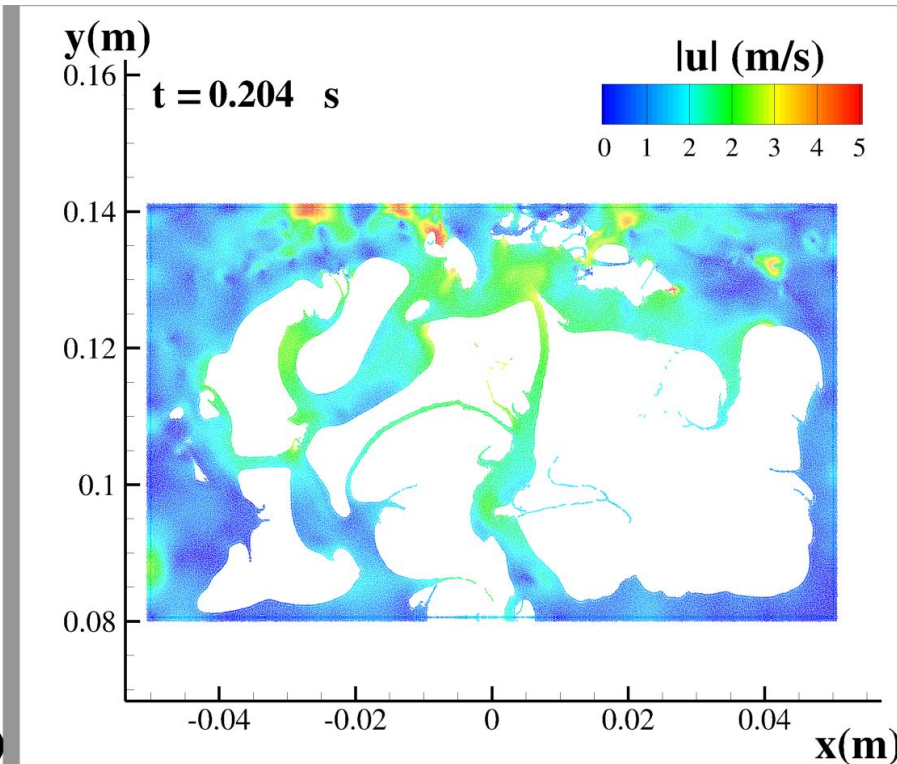
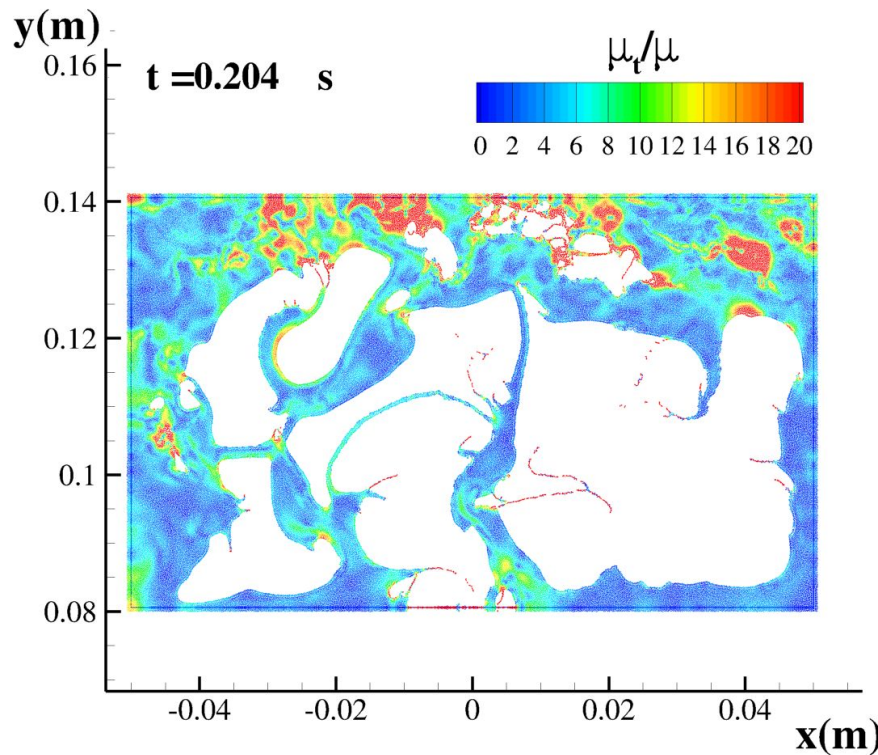
→ initial flow instability is triggered



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$$-\mathcal{P}_{ext} + \dot{\mathcal{E}}_M + \dot{\mathcal{E}}_C = \mathcal{P}_V + \mathcal{P}_V^{turb} + \mathcal{P}_N \leq 0$$

Power related to **external forces**

Time derivative of the fluid **mechanical energy**

Time derivative of reversible **compressible energy**

$$\mathcal{P}_C := - \int_{\Omega} p \operatorname{div}(\mathbf{u}) dV$$

→ generally negligible

Power related to laminar and turbulent **viscous dissipation**

Power related to **numerical dissipation**

A. Colagrossi, B. Bouscasse, S. Marrone, *Energy decomposition analysis for viscous free-surface flows*, Phys. Rev. E, Vol. **92**, pp. 053003-13, (2015).



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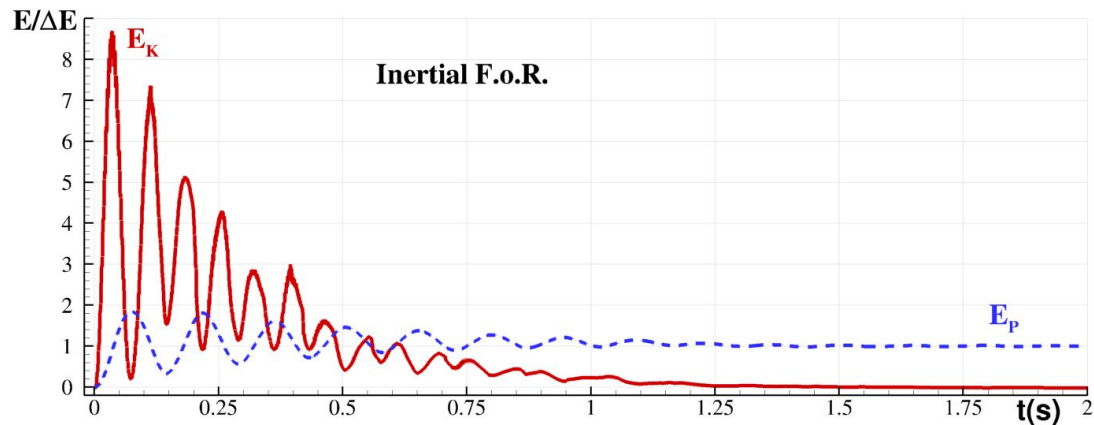
Dependency on the Frame of Reference of the simulation:

$$-\mathcal{P}_{ext} + \dot{\mathcal{E}}_M + \dot{\mathcal{E}}_C = \mathcal{P}_V + \mathcal{P}_V^{turb} + \mathcal{P}_N \leq 0$$

Invariant for rigid motions of the F.o.R.

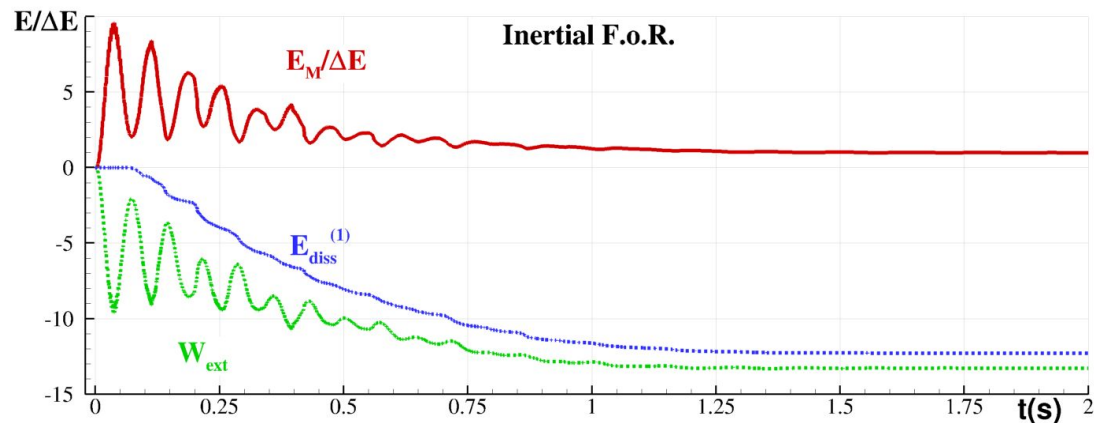


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Simulation in the **inertial** Frame of Reference

Kinetic and Potential Energy



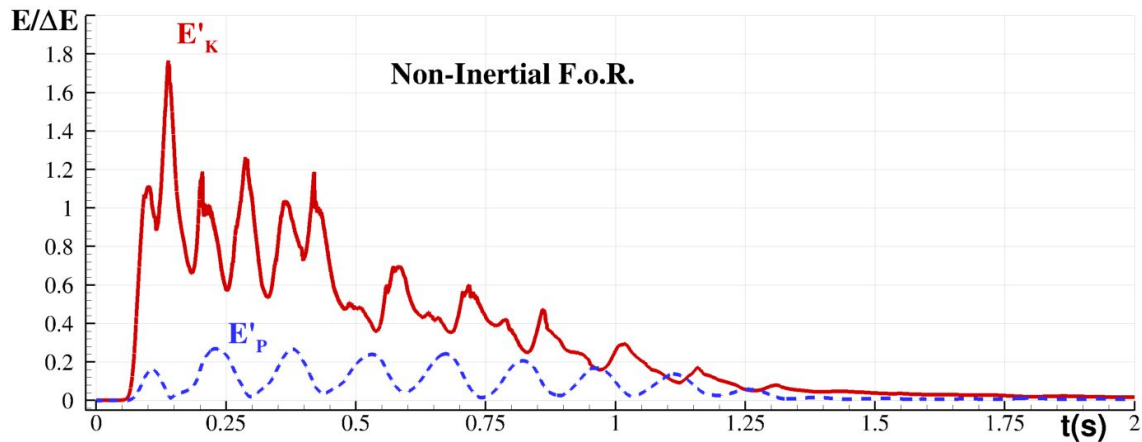
Mechanical energy (**EM**) and Work done by solid walls (**Wext**)

$$-\mathcal{P}_{ext} + \dot{E}_M + \dot{E}_C = \mathcal{P}_V + \mathcal{P}_V^{turb} + \mathcal{P}_N$$

$E_{diss}^{(1)}$

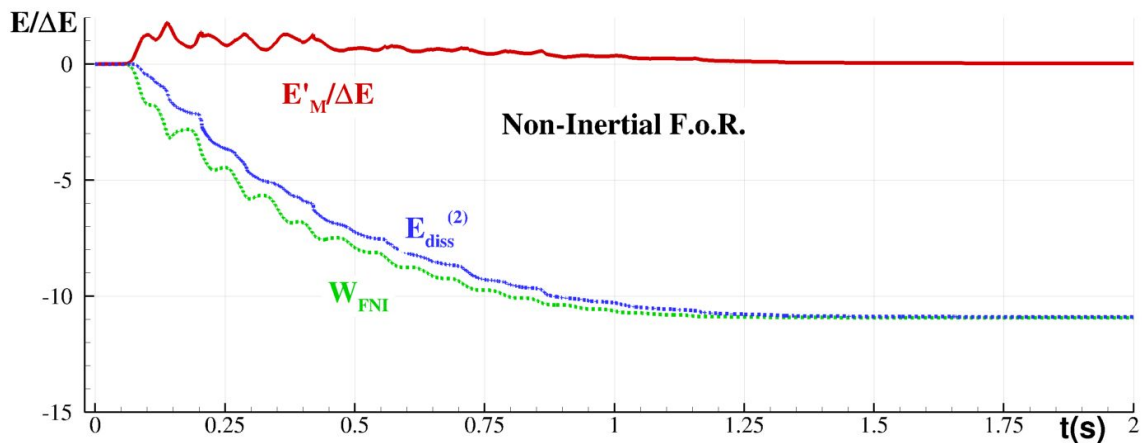


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Simulation in the **non-inertial** Frame of Reference

Kinetic and Potential Energy



Mechanical energy (**EM**) and Work done by non-inertial Forces (**FNI**)

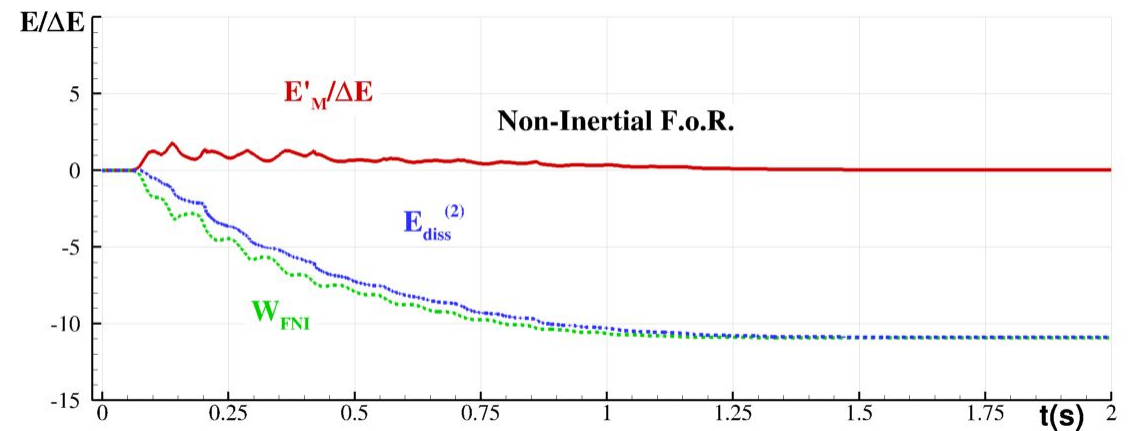
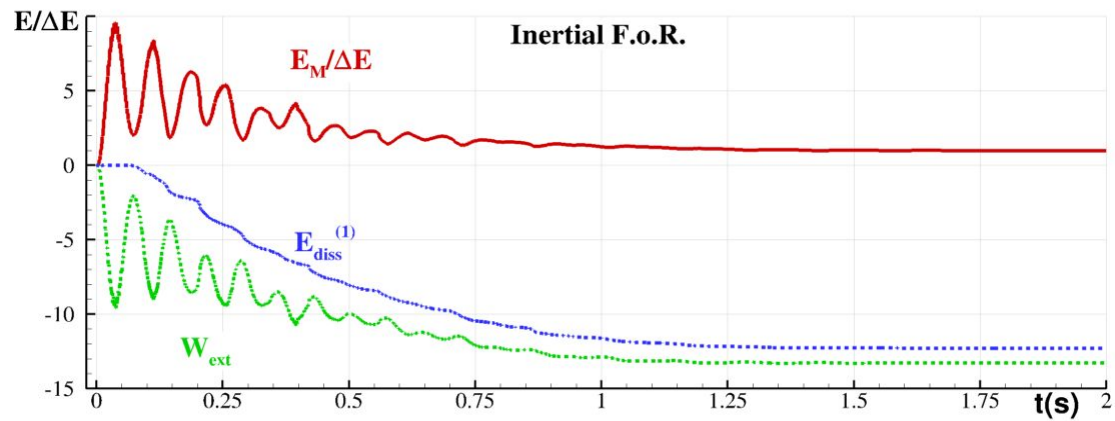
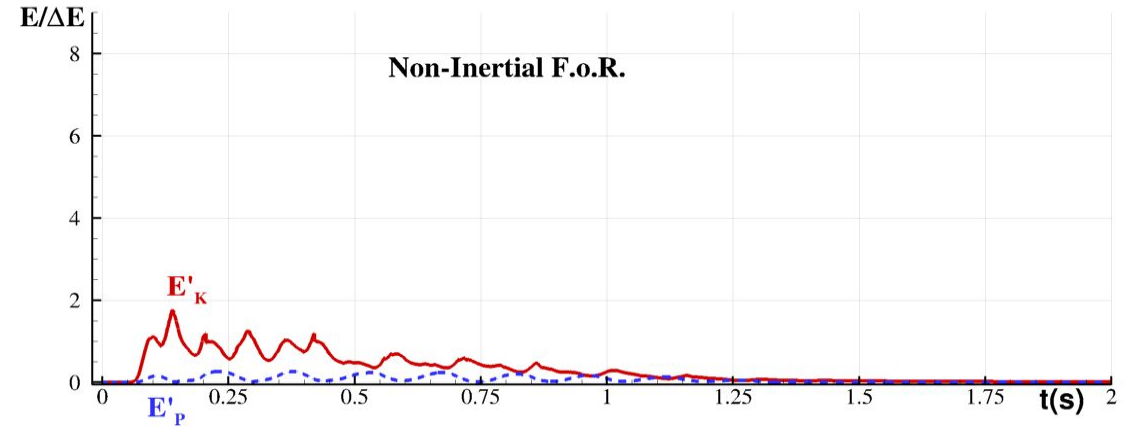
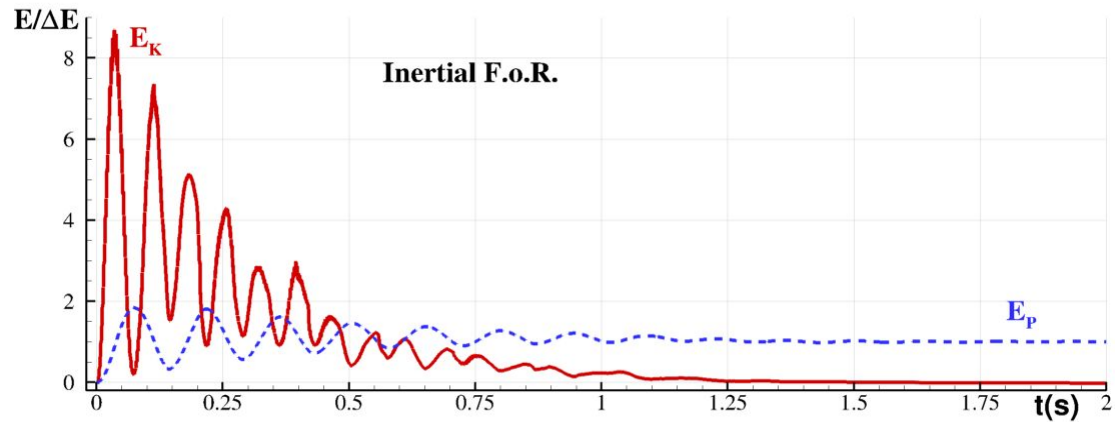
$$-\mathcal{P}_{ext} + \dot{E}_M + \dot{E}_C = \mathcal{P}_V + \mathcal{P}_V^{turb} + \mathcal{P}_N$$

The term  $\dot{E}_{diss}^{(2)}$  is circled in blue in the original image.



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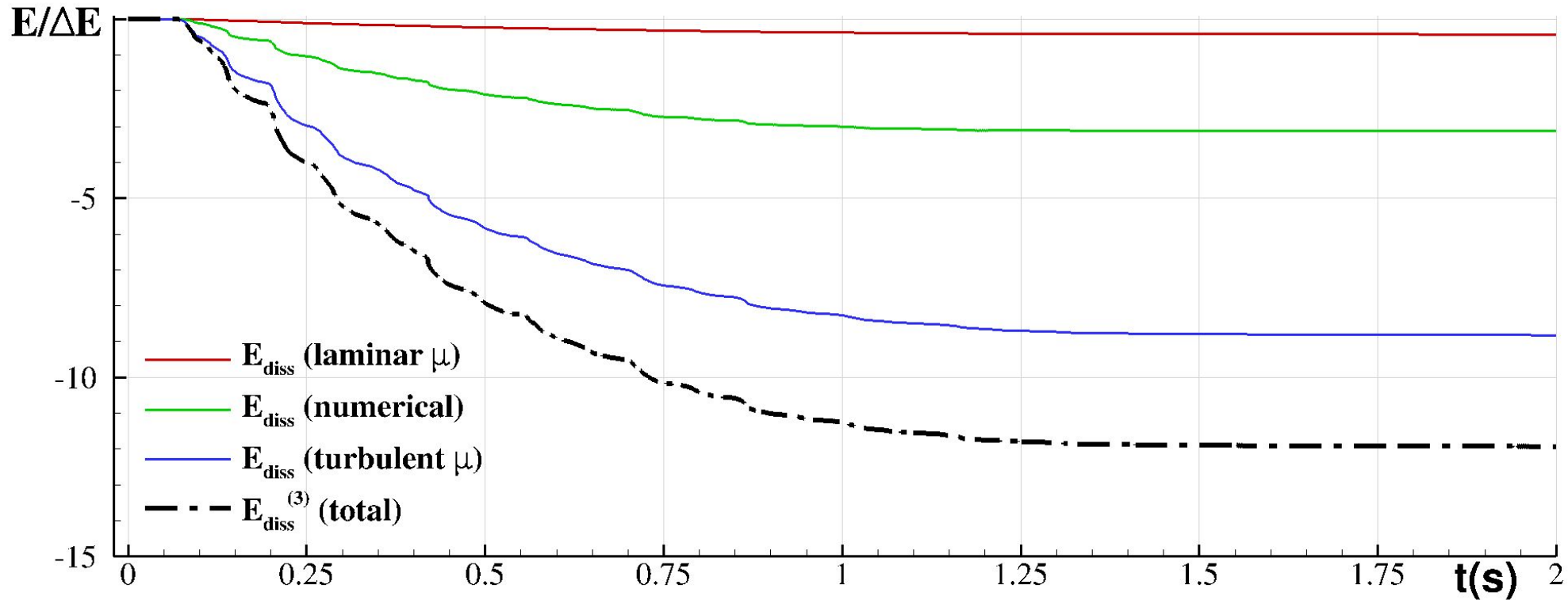


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$$\mathcal{P}_{ext} + \dot{E}_M + \dot{E}_C = \mathcal{P}_V$$

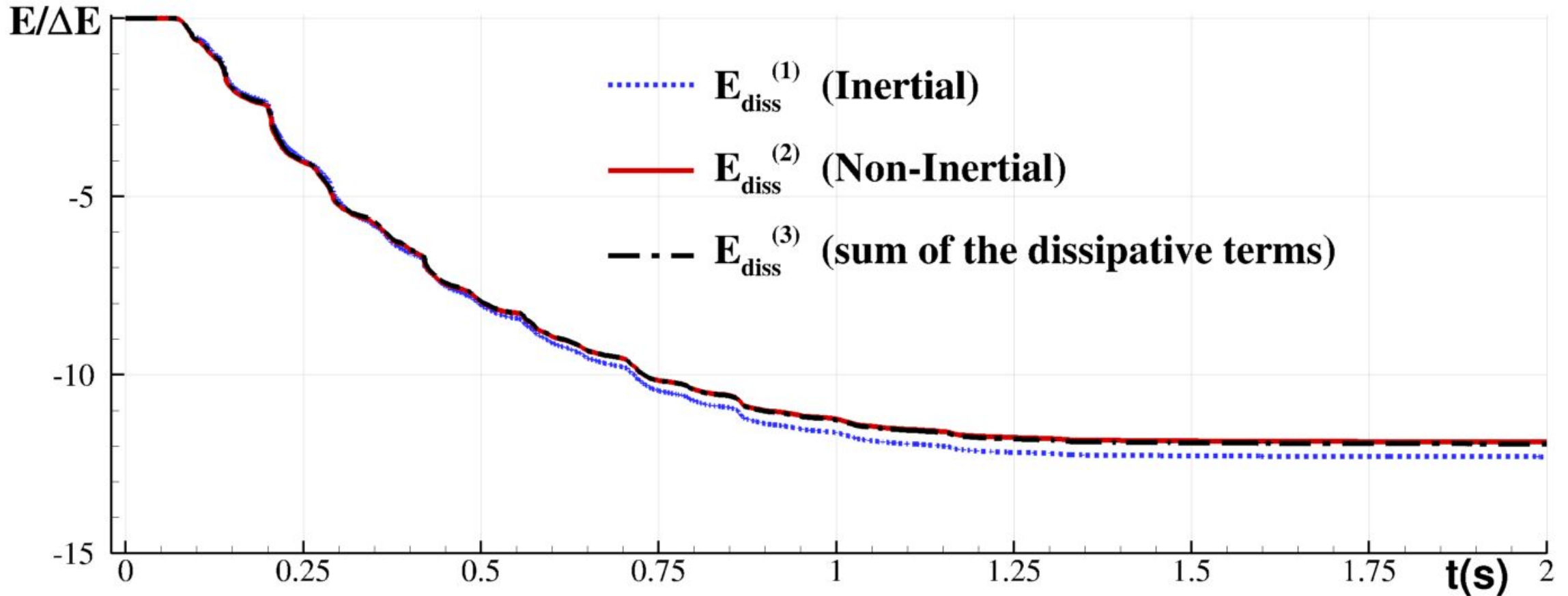


## Purely dissipative terms



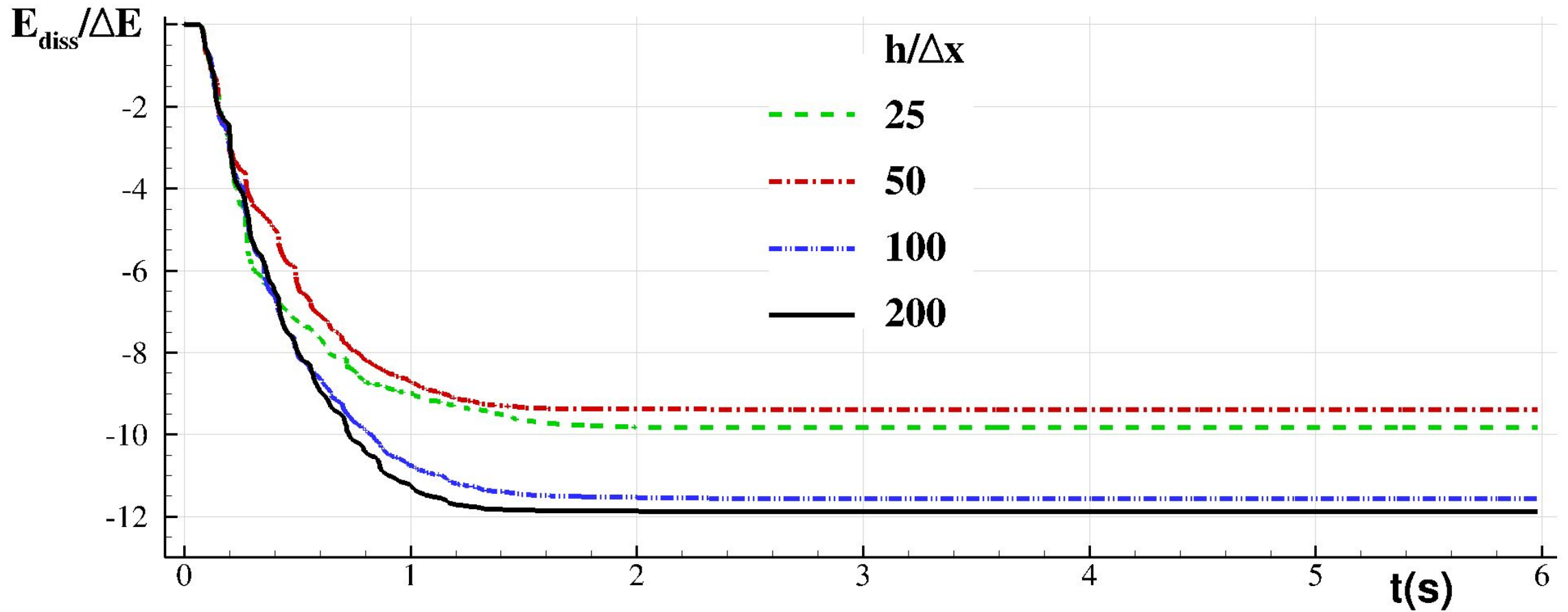
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$$-\mathcal{P}_{ext} + \dot{\mathcal{E}}_M + \dot{\mathcal{E}}_C \in \underbrace{\mathcal{P}_V + \mathcal{P}_V^{turb} + \mathcal{P}_N}_{E_{diss}^{(3)}}$$

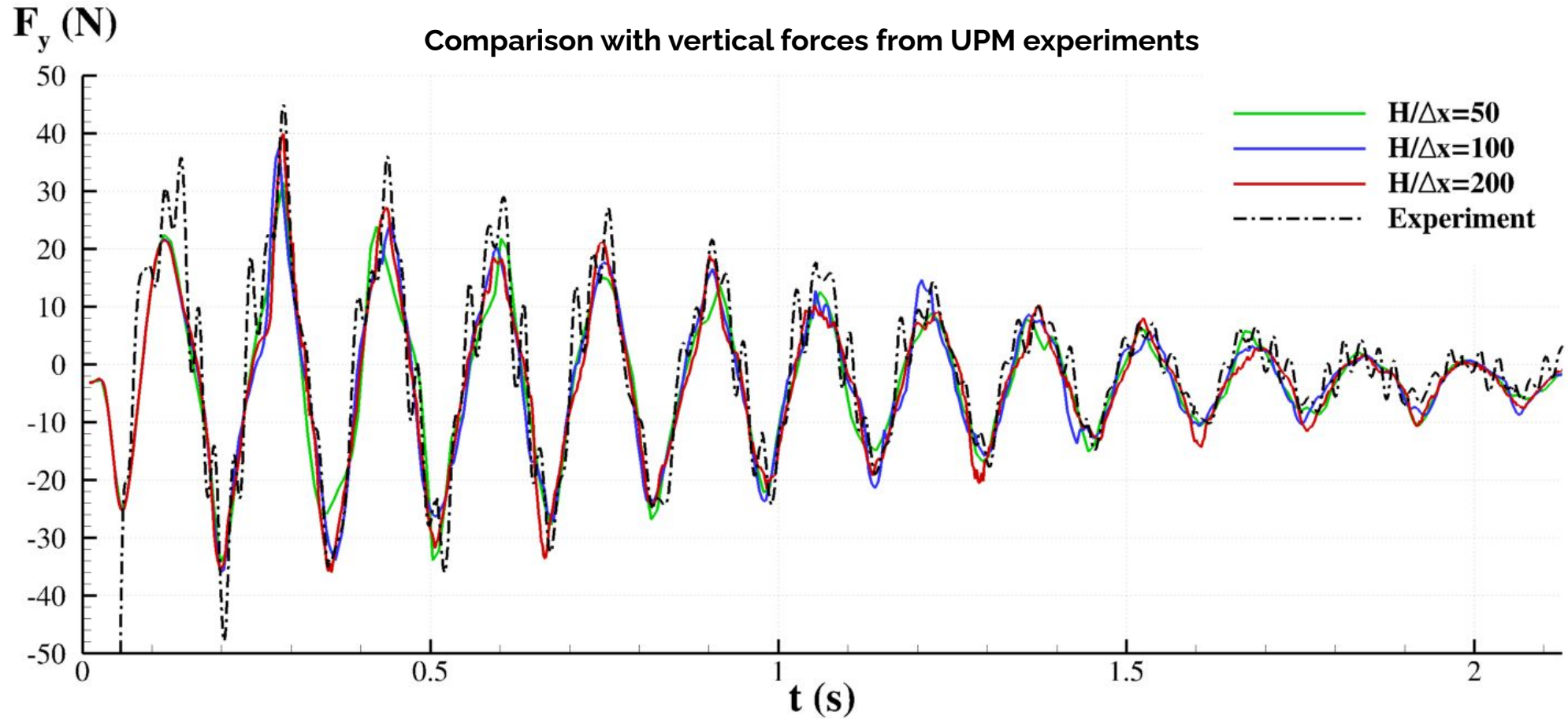


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$$\mathcal{P}_{ext} + \dot{\mathcal{E}}_M + \dot{\mathcal{E}}_C = \mathcal{P}_V + \mathcal{P}_V^{turb} + \mathcal{P}_N$$



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- the SPH model has been applied to a violent sloshing flow in pure heave motion
- standard SPH schemes exhibit tensile instability issues due to intense negative pressure in the first acceleration stage
- a new SPH model has been proposed to eliminate this issue and increase accuracy
- closure of the different energy terms has been shown for different choices of the frame of reference
- most of the energy drops seem related to impact stage
- an in-depth validation is still needed due to the complexity of the problem



**Thanks for your attention**



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