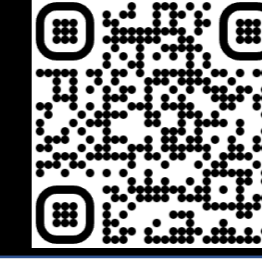


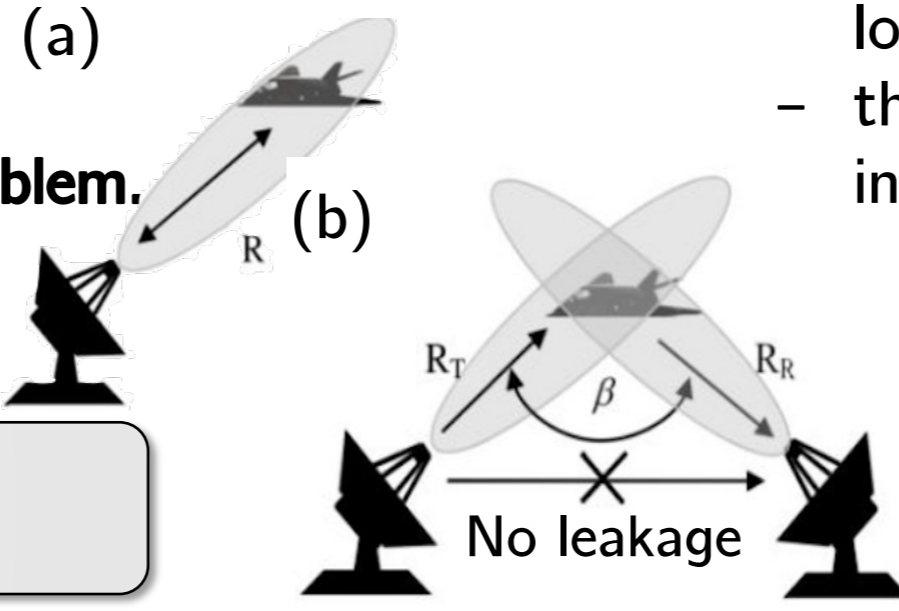
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## Background

- Mono-static:
  - Relative simplicity due to the known transmit (dual-function) waveform at the receiver.
  - Suffering from leakage (self interference).
  - **Most ISAC studies underestimate this leakage problem.**
- Bistatic:
  - Overhead cost associated with reference sharing.



## Full-duplex Setup

- Physical separation of TX and RX antennas may not entirely solve the echo-miss problem (SI can be 100dB larger than thermal noise).
- To achieve ISAC, the transceiver should work in the full-duplex (FD) mode.

## Challenge: Echo-miss

- **Echo-miss:** For a mono-static ISAC transceiver,
  - signal transmission durations (3GPP 38.211) are typically much longer than the radar echo round-trip times,
  - the radar returns are drowned by the strong residual self interference (SI) from the transmitter.

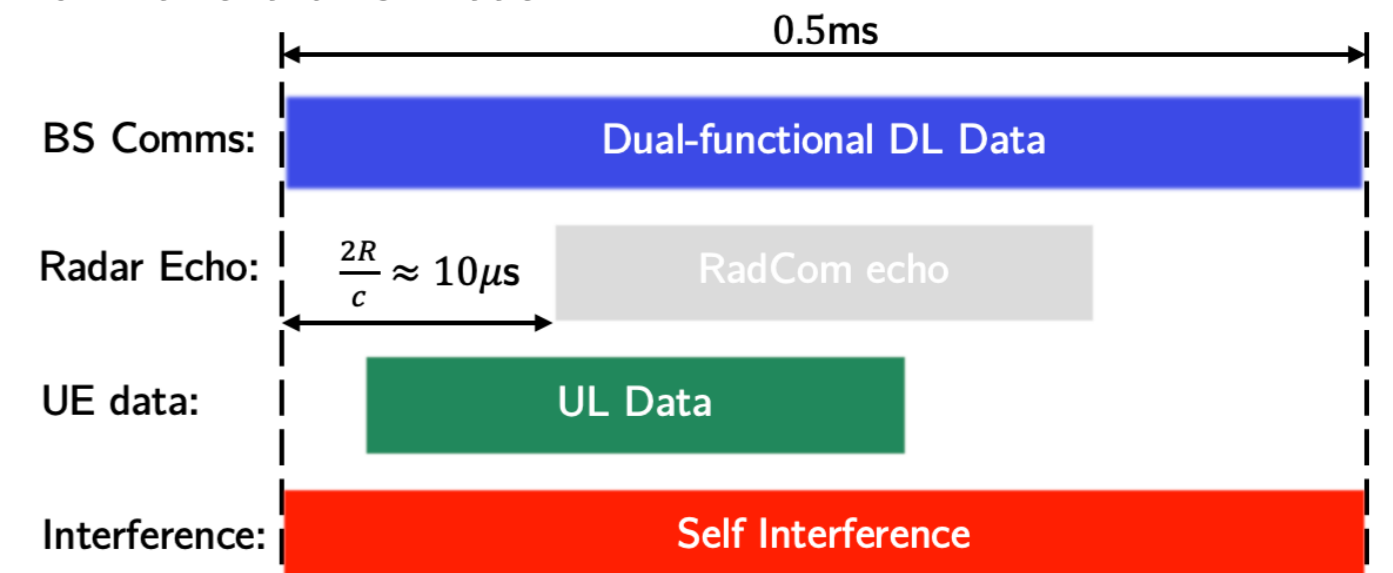
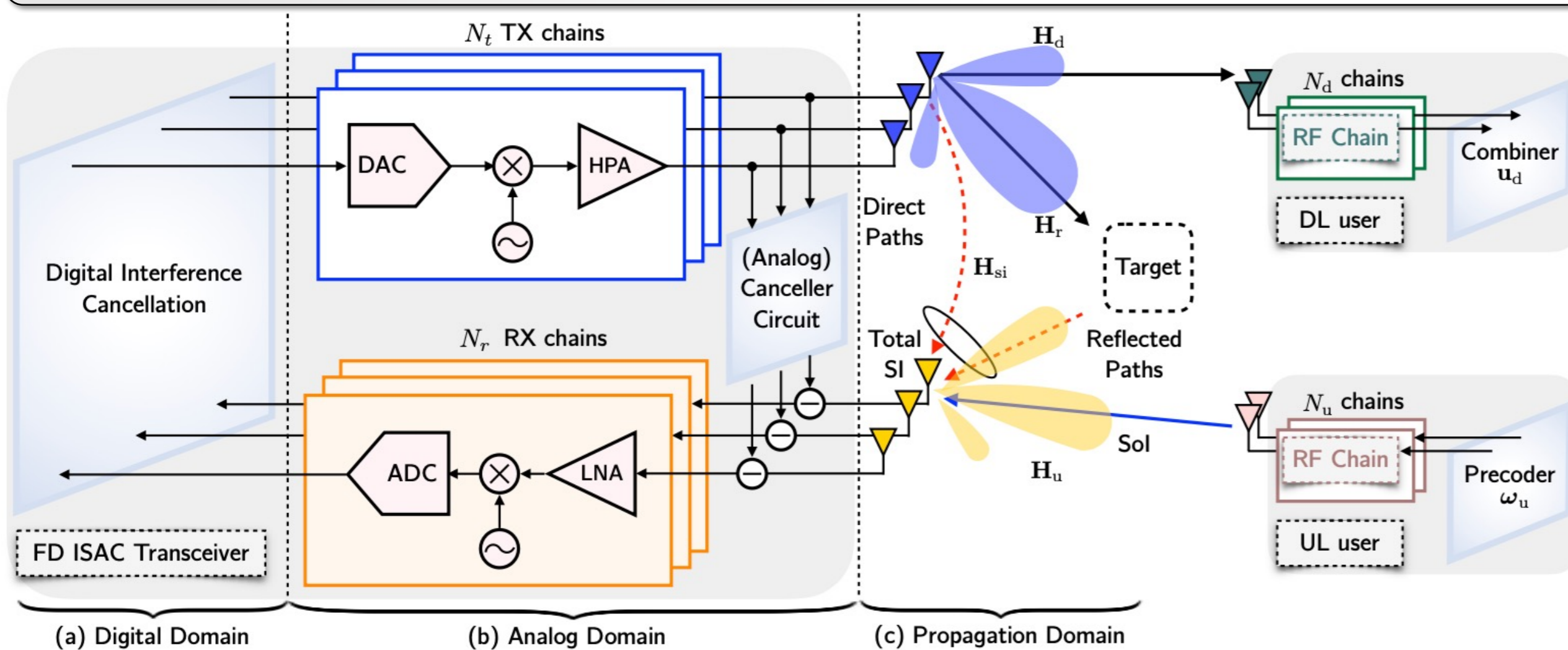


Fig: frames in a typical ISAC system.

## Previous Approaches for SI Cancellation



- Taxonomy of SI cancellation techniques:
  - Propagation domain
  - Analog domain
  - Digital domain (e.g., modulo ADC [1], [2])

## Difficulty in FD ISAC

- Radar echoes are correlated with the SI
- Previous approaches may distort Sol

## Our Approach: Joint ISAC TX-RX Design

- We aim to design
  - $\mathbf{p}, \mathbf{w}$ : the transmit and receive beamformer at the transceiver,
  - $\omega_u$ : precoder at the uplink user,
  - $\mathbf{u}_d$ : combiner at the downlink user
- to simultaneously maximize
  - $R_u, R_d$ : the uplink and downlink rate,
  - $G_t, G_r$ : the transmit and receive radar beampattern power at the target, suppress the residual SI.

$$\begin{aligned} \max_{\mathbf{p}, \mathbf{w}, \omega_u, \mathbf{u}_d} \quad & \alpha_1 R_u + \alpha_2 R_d + \alpha_3 G_t + \alpha_4 G_r \\ \text{s.t.} \quad & \|\mathbf{p}\|_2^2 \leq P_d, \quad \|\mathbf{w}\|_2^2 = 1, \\ & \|\omega_u\|_2^2 \leq P_u, \quad \mathbf{w}^H \mathbf{H}_{si} \mathbf{p} = 0. \end{aligned}$$

- $R_u = \log_2(1 + \gamma_u)$
- $R_d = \log_2(1 + \gamma_d)$
- $\gamma_u = \frac{|\mathbf{w}^H \mathbf{H}_u \omega_u|^2}{|\mathbf{w}^H \mathbf{H}_p|^2 + \|\mathbf{w}\|^2 \sigma_u^2}$
- $\gamma_d = \frac{|\mathbf{u}_d^H \mathbf{H}_d \mathbf{p}|^2}{\|\mathbf{u}_d\|^2 \sigma_d^2}$
- $G_r = |\mathbf{w}^H \mathbf{a}(\theta_r)|^2$
- $G_t = |\mathbf{b}^H(\theta_r) \mathbf{p}|^2$
- $P_u, P_d$ : combiner at the downlink user

**Algorithm 1:** Proposed Penalty-based Joint Transmit and Receive Beamformer Design

**Input:**  $\mathbf{H}_d, \mathbf{H}_u, \mathbf{H}_r, \mathbf{H}_{si}, P_d, P_u$ .  
**Output:**  $\rho_u^*, \rho_d^*, \mathbf{p}^*, \mathbf{w}^*, \omega_u^*, \mathbf{u}_d^*$ .

- 1 Initialize  $\mathbf{p}, \mathbf{w}, \omega_u, \mathbf{u}_d$  randomly,  $\beta = 10^{-25}$ ;
- 2 **while** no convergence of objective function **do**
- 3     Update  $\rho_u^*$ . Complexity =  $\mathcal{O}(N_r^2)$ .
- 4     Update  $\rho_d^*$ . Complexity =  $\mathcal{O}(N_t N_d)$ .
- 5     Update  $\omega_u^*$ . Complexity =  $\mathcal{O}(I_1 N_r N_u)$ .
- 6     Update  $\mathbf{w}^*$ . Complexity =  $\mathcal{O}(N_r^3)$ .
- 7     Update  $\mathbf{u}_d^*$ . Complexity =  $\mathcal{O}(N_t N_d)$ .
- 8     Update  $\mathbf{p}^*$ . Complexity =  $\mathcal{O}(I_2 N_t^3)$ .
- 9 **end**
- 10 Normalize  $\mathbf{w}^*$ ;
- 11 Return  $\rho_u^*, \rho_d^*, \mathbf{p}^*, \mathbf{w}^*, \omega_u^*, \mathbf{u}_d^*$ .

## Transformation and Penalty-based BCD Update

- Coupling Constraint Transformation by Penalty Term

Constraint  $\mathbf{w}^H \mathbf{H}_{si} \mathbf{p} = 0 \Rightarrow$  A penalty term  $-\frac{1}{2\beta} \|\mathbf{w}^H \mathbf{H}_{si} \mathbf{p}\|_2^2$  in the objective function

- Communication Rate Transformation by (weighted minimize mean square error) WMMSE

$$R_u \Rightarrow \log_2 \rho_u - \rho_u E_{BS} \quad R_d \Rightarrow \log_2 \rho_d - \rho_d E_d$$

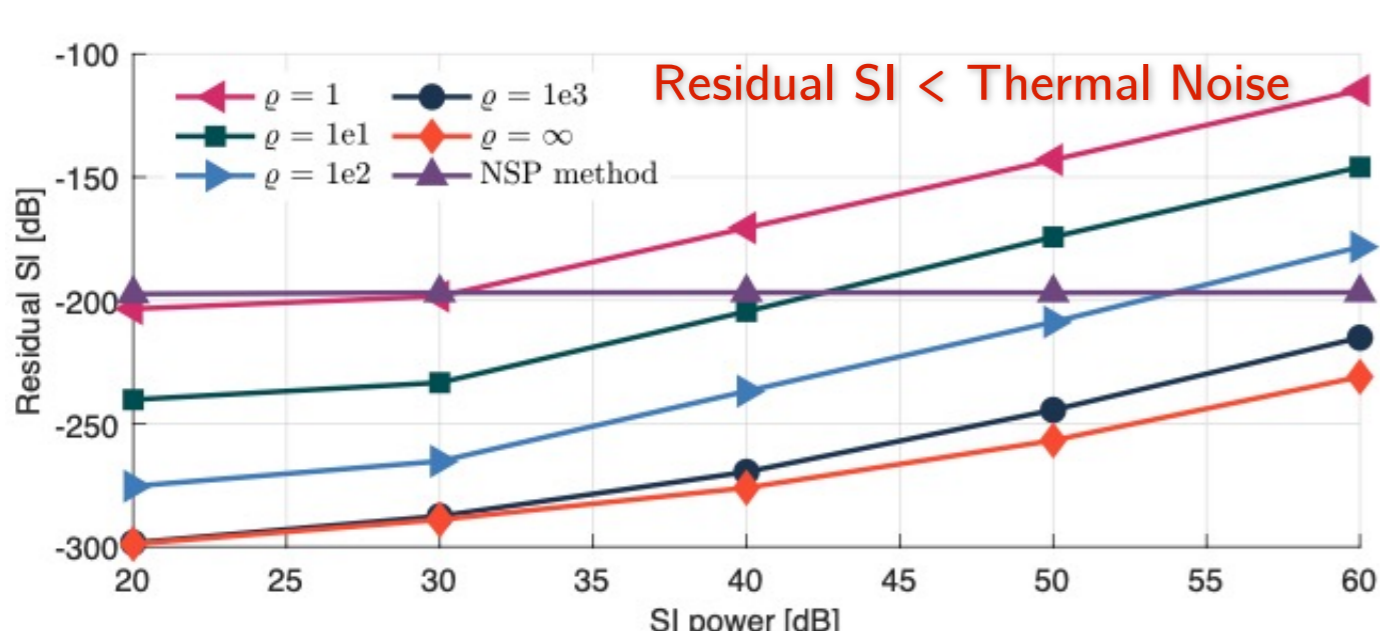
–  $\rho_u, \rho_d$ : auxiliary variables –  $E_{BS}, E_d$ : MSE matrices

- Beampattern Power Transformation to make it concave in the objective function

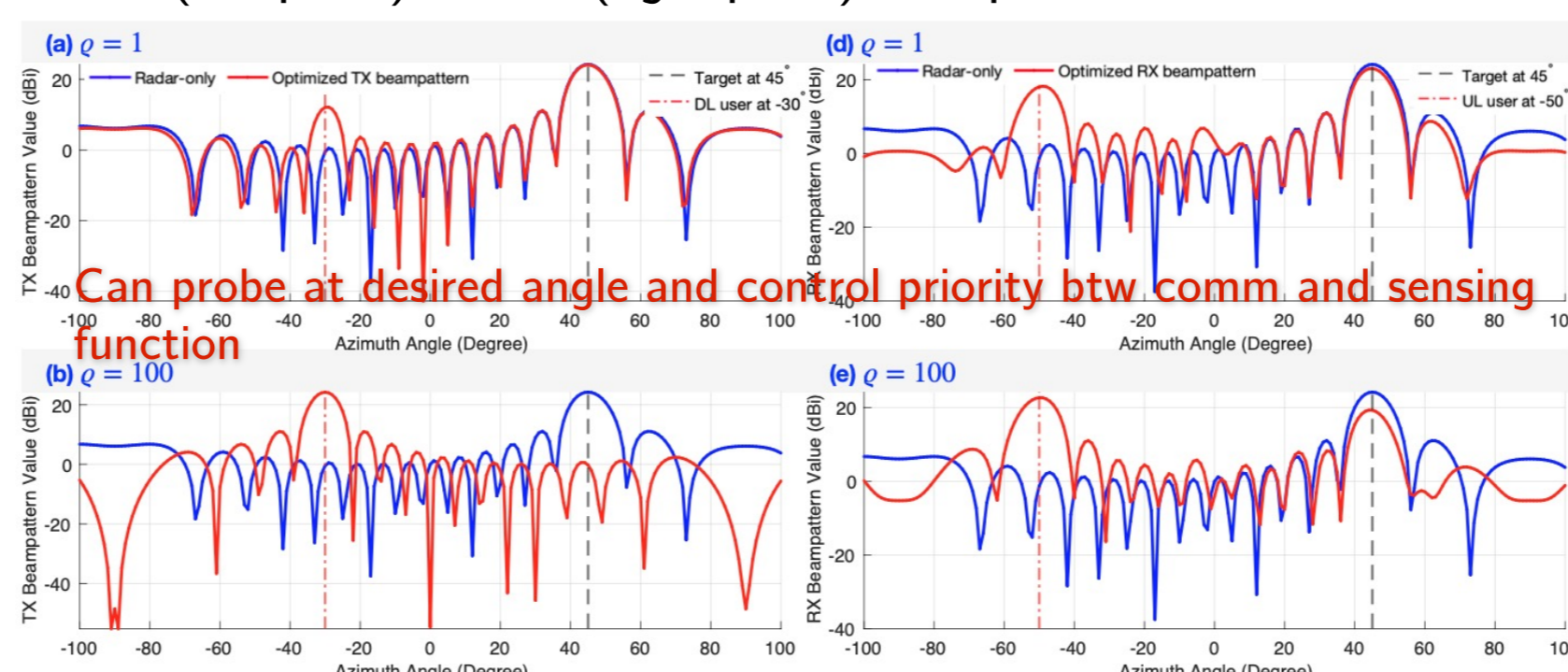
$$\begin{aligned} \max_{\{\mathbf{p}, \mathbf{w}\}, \{\omega_u, \mathbf{u}_d\}, \{\rho_u, \rho_d\}} \quad & \alpha_1 (\log_2 \rho_u - \rho_u E_{BS}) + \alpha_2 (\log_2 \rho_d - \rho_d E_d) + \alpha_3 \mathbf{p}^H \mathbf{Z}_t(\theta_t) \mathbf{p} + \alpha_4 \mathbf{w}^H \mathbf{Z}_r(\theta_r) \mathbf{w} - \frac{1}{2\beta} \|\mathbf{w}^H \mathbf{H}_{si} \mathbf{p}\|_2^2 \\ \text{s.t.} \quad & \|\mathbf{p}\|_2^2 \leq P_d, \quad \|\omega_u\|_2^2 \leq P_u, \quad \|\mathbf{w}\|_2^2 = 1. \end{aligned}$$

## Numerical Evaluation

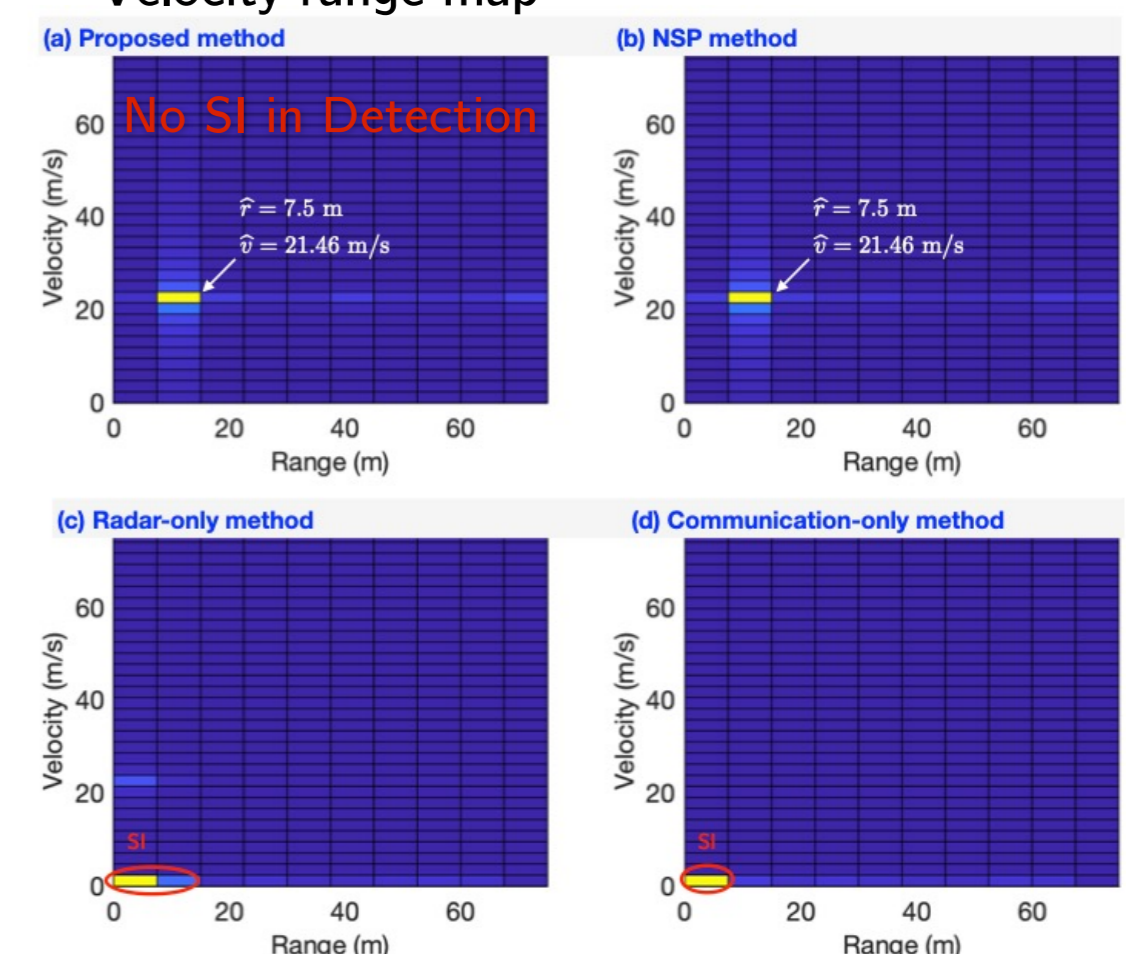
- SI cancellation performance



- Tx (left panel) and Rx (right panel) beampattern



- Velocity range map



## Conclusion

- Our proposed joint TX-RX beamformer design method can effectively achieve up to 60 dB digital-domain SI cancellation, a higher average sum-rate, and more accurate radar parameter estimation compared with previous ISAC FD studies.

[1] Z. Liu, A. Bhandari, and B. Clerckx, "λ – MIMO: Massive MIMO via modulo sampling," accepted to *IEEE Trans. Commun.*  
 [2] A. Bhandari, F. Kraemer, and R. Raskar, "On unlimited sampling and reconstruction," *IEEE Trans. Sig. Proc.*, vol. 69, pp. 3827–3839, Dec. 2020.