



A theory of physiological similarity in muscle-driven motion

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Muscle contraction is the primary source of all animal movement. I show that the maximum mechanical output of such contractions is determined by a characteristic dimensionless number, the “effective inertia,” Γ , defined by a small set of mechanical, physiological, and anatomical properties of the interrogated musculoskeletal complex. Different musculoskeletal systems with equal Γ may be considered physiologically similar, in the sense that maximum performance involves equal fractions of the muscle’s maximum strain rate, strain capacity, work, and power density. It can be demonstrated that there exists a unique, “optimal” musculoskeletal anatomy which enables a unit volume of muscle to deliver maximum work and power simultaneously, corresponding to Γ close to unity. External forces truncate the mechanical performance space accessible to muscle by introducing parasitic losses, and subtly alter how musculoskeletal anatomy modulates muscle performance, challenging canonical notions of skeletal force–velocity trade-offs. Γ varies systematically under isogeometric transformations of musculoskeletal systems, a result which provides fundamental insights into the key determinants of animal locomotor performance across scales.

locomotion | scaling | motor | dimensional analysis

Muscle, the “prime mover” of the animal kingdom, is used for acts of tender kindness, devastating brutality, and astonishing grace. By conversion of chemical into mechanical energy, it enables contractions long-lasting and cyclical, actions fast and forceful, and movements precise and reflexive. Whether an animal swims, runs, crawls, or flies; whether it is smaller than the tip of a sharp pencil or heavier than 15 school buses; whether it first appeared millions or only thousands of years ago—muscle is what gets it about (1–4).

Juxtaposed to this diversity stands the observation that many functional, physiological, and ultrastructural features of muscle vary remarkably little (1, 5, 6), suggesting the existence of general limits to what it can achieve. Identification of these limits, and assessment of their consequences for locomotor performance and musculoskeletal anatomy, has a long history in biomechanics and muscle physiology (e.g., refs. 7–24). A particularly successful and thus popular approach in comparative studies of animal locomotion has been the notion of similarity indices, derived via dimensional analysis, and introduced to biology in the hope to replicate the success it afforded in the physical sciences (e.g., refs. 11, 13, 14, and 25). Remarkably, the two dominant similarity indices for animal movement—the Froude and the Strouhal number—consider elastic and gravitational forces as the agents of motion (3). The scarcity of similarity theories which make explicit reference to muscle (e.g., refs. 9, 16, 17, 21, and 22) may be partially explained by the complexity of muscle as a motor: Muscle force, work, and power output depend in a nontrivial fashion on muscle strain rate (26), strain (27), and contractile history (28). Appropriate assessment of muscle performance thus requires coupling these characteristic properties with both internal and external forces, in order to avoid results that are mechanically possible, but physiologically prohibited (29–31); a task rarely addressed and so challenging that it typically requires numerical resolution (e.g., refs. 15, 19, 32–34).

In this text, I investigate how the interaction between physical constraints, muscle physiology, and the anatomy of musculoskeletal systems places bounds on the mechanical performance space accessible to muscle. It will be demonstrated analytically that the maximal mechanical output of every muscle contraction is governed by the competition between two distinct limits, which arise from physiological and anatomical constraints. The relative importance of these constraints characterises the degree of “physiological similarity” of muscle contractions, a metric defined by a dimensionless number that enables direct comparison of musculoskeletal systems across size, and physiological and anatomical make-up.

Significance

Muscle is the ancient biological motor. The contractile mechanism and physiology of muscle are remarkably conserved, suggesting that its maximum mechanical performance may be bound by similar constraints in animals of different sizes, and across locomotor modes. I show that this similarity can be captured by a dimensionless number, the “effective inertia.” The effective inertia quantifies the relative importance of strain and strain rate in limiting muscle mechanical output, and the extent to which muscle can access its maximum power and work density; muscle contractions with equal effective inertia may thus be considered “physiologically similar.” The effective inertia varies systematically with body size for geometrically similar animals, with profound consequences for our understanding of the scaling of animal locomotion.

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Two Speed Limits for Muscle-Driven Motion

Consider the seemingly simple example of a muscle with constant gear ratio G , capable of exerting a maximum force F_{max} , as it contracts to accelerate an object of mass m .^{*} What is the maximum speed it can impart in a single contraction? Mass, maximum force, and gear ratio together determine the net acceleration (a), $a = F_{max}Gm^{-1}$, of dimension length per time squared [$L t^{-2}$]. Identifying a maximum speed v of dimension length per time [$L t^{-1}$] thus requires specification of either a time (t), $v_t \sim at$, or a displacement (δ), $v_\delta \sim \sqrt{a\delta}$. These results may be recognized as the first time- and path-integrals of Newton's 2nd law, respectively, which link the speed imparted to the delivered impulse (p), $mv \sim p \sim \int F_{max}Gdt$, or the work done (W), $mv^2 \sim W \sim \int F_{max}Gd\delta$. Unfortunately, this analysis does not yet yield the maximum speed the muscle can impart, for Newtonian mechanics alone provides no information about what the appropriate displacement or time might be. Because no muscle can contract in perpetuity, both boundary conditions may be identified through introduction of appropriate physiological and anatomical constraints.

In order to develop some intuition for how such constraints enter the problem, consider the joyful if simplistic analogy of riding a bicycle: If the gear is much too small, it is impossible to increase speed because the muscle cannot contract quickly enough to accelerate the pedals; the best it can do is to keep them spinning at their current speed. If the gear is much too large, in turn, the muscle will accelerate the pedals rather slowly, so that the speed imparted at the end of a single contraction cycle will be miniscule. Both scenarios are manifestations of two limits to the speed of muscle-driven motion: how fast a muscle can contract, and by how much it can shorten. The axiomatic limit on muscle strain rate, $\dot{\epsilon}$, and the anatomical limit on muscle strain, ϵ , can inform the mechanical analysis, for they each impose a distinct limit on the maximum impulse muscle can deliver, and on the maximum work that it can do.

The maximum distance δ_{max} available for acceleration must be some fraction of the muscle fiber length l_m , $\delta_{max} = l_m \epsilon_{max} G^{-1}$, where the maximum strain ϵ_{max} is considered to be independent of the gear ratio. This distance is covered in a time $t_{max,\delta} \sim \sqrt{2\delta_{max}a^{-1}}$ (the factor two arises from integration). Where work and impulse are limited by the strain capacity of muscle, the maximum speed then follows from either maximum distance or time as:

$$v_{Bo} = \sqrt{2 \frac{W_{max}}{m}} = \sqrt{\frac{2}{m} V_m \hat{\sigma}_{max} \epsilon_{max}}, \quad [1]$$

where $W_{max} = V_m \hat{\sigma}_{max} \epsilon_{max}$ is the maximum work, defined by the muscle volume V_m , and the maximum average stress, $\hat{\sigma}_{max}$, the muscle can exert as it shortens by ϵ_{max} .[†] In recognition of the pioneering work of GA Borelli, who first derived an equivalent result (7), I will refer to Eq. 1 as the Borelli limit to speed and define the Borelli number, $Bo \propto v (2W_{max}m^{-1})^{-1/2}$.

Consider next the case where muscle work and impulse are limited by the maximum shortening speed of muscle instead. Let

^{*}An exact analysis would need to consider separately the mass of the object and of the muscle. For simplicity, I here lump both into one term. This lumping will introduce an error in calculations where the muscle mass is comparable to the external mass that is moved by the muscle, but this error will only change the result in magnitude, and not in principle, because the distributed mass of the muscle can be taken into account with an "effective mass"-term that is a fixed fraction of the total muscle mass (35).

[†]For a muscle which generates a constant force throughout the contraction, $\hat{\sigma}_{max} = \sigma_{max}$. But this is not true for "real" muscle, for which the force varies with both strain and strain rate as discussed in more detail later.

this maximum shortening speed be $v_{max} = l_m \dot{\epsilon}_{max}$, where $\dot{\epsilon}_{max}$ is the maximum strain rate in units of muscle lengths per second. Reaching $\dot{\epsilon}_{max}$ requires accelerating the mass over a distance $\delta_{max,\dot{\epsilon}} \sim 1/2 (l_m \dot{\epsilon}_{max})^2 a^{-1} G^{-2}$, which takes a time $t_{max,\dot{\epsilon}} \sim l_m \dot{\epsilon}_{max} a^{-1} G^{-1}$. The speed imparted then follows from either as:

$$v_{Hi} = \frac{l_m \dot{\epsilon}_{max}}{G}, \quad [2]$$

which I will call the Hill limit to speed, with the associated Hill number, $Hi \propto vG (l_m \dot{\epsilon}_{max})^{-1}$, in recognition of AV Hill's groundbreaking contributions to our understanding of the force-velocity properties of muscle (26). The Hill limit may also be derived through a simpler argument: In the absence of series elasticity, the speed of the mass must equal the muscle shortening speed divided by the gear ratio at any time; the mass thus cannot move faster than $v_{Hi} = \frac{l_m \dot{\epsilon}_{max}}{G}$.

The Borelli and Hill number are dimensionless numbers which may be interpreted as indices of dynamic similarity in muscle-driven motion: Where muscle does equal amounts of mass-specific work, movements will have equal Borelli numbers; equality of Hill numbers, in turn, implies equal ratios between the muscle contraction speed and the musculoskeletal gear ratio. But which number is appropriate to assess the limit which binds maximum speed?

To answer this question, I once more borrow from the versatile toolbox of dimensional analysis: The ratio between a characteristic speed and a characteristic displacement depends on the acceleration via $v^2 \delta^{-1} \sim a$. Thus, for vanishing acceleration, the speed gained per unit displacement is negligible, and the muscle will have shortened maximally long before it has reached its maximum shortening speed; the contraction is quasi-static relative to the maximum strain rate. If the acceleration is large, in turn, the maximum speed is reached with minimum length change of the muscle, and within miniscule time; the contraction is quasi-instantaneous. Thus, in general, a muscle that contracts against a sufficiently small mass is bound by the Hill limit (Fig. 1 A and B); the impulse and work it can deliver, and thus the speed it can impart, are limited by its maximum strain rate. In contrast, a muscle that contracts against a sufficiently large mass is Borelli-limited (Fig. 1 C and D); the impulse, work, and speed it can deliver are limited by its strain capacity.

This dimensional argument is simple, but unsatisfying—How large is a sufficiently large, and how small is a sufficiently small mass? To render the qualitative argument quantitative, I next normalize the mass with the relevant physiological properties of muscle, with the aim to find the "effective inertia" of the musculoskeletal system.

The Effective Inertia of a Muscle Contraction

The Borelli and Hill limit are absolute: A muscle that has exhausted its strain capacity cannot increase the speed of the mass further, even if it could contract faster still; a muscle contracting with its maximum strain rate can no longer accelerate the mass, even if it has not yet shortened by the maximum possible amount. The maximum speed muscle can impart is thus determined by whichever of the two speeds is lower (Fig. 1A), so that the relevant limit can be identified by consideration of the ratio between the Hill and the Borelli limit:

$$\Gamma = \left[\frac{v_{Hi}}{v_{Bo}} \right]^2 = \frac{1}{2} \left[\frac{l_m^2}{G^2} \right] \left[\frac{\dot{\epsilon}_{max}^2}{\hat{\sigma}_{max} \epsilon_{max}} \right] \left[\frac{m}{V_m} \right]. \quad [3]$$

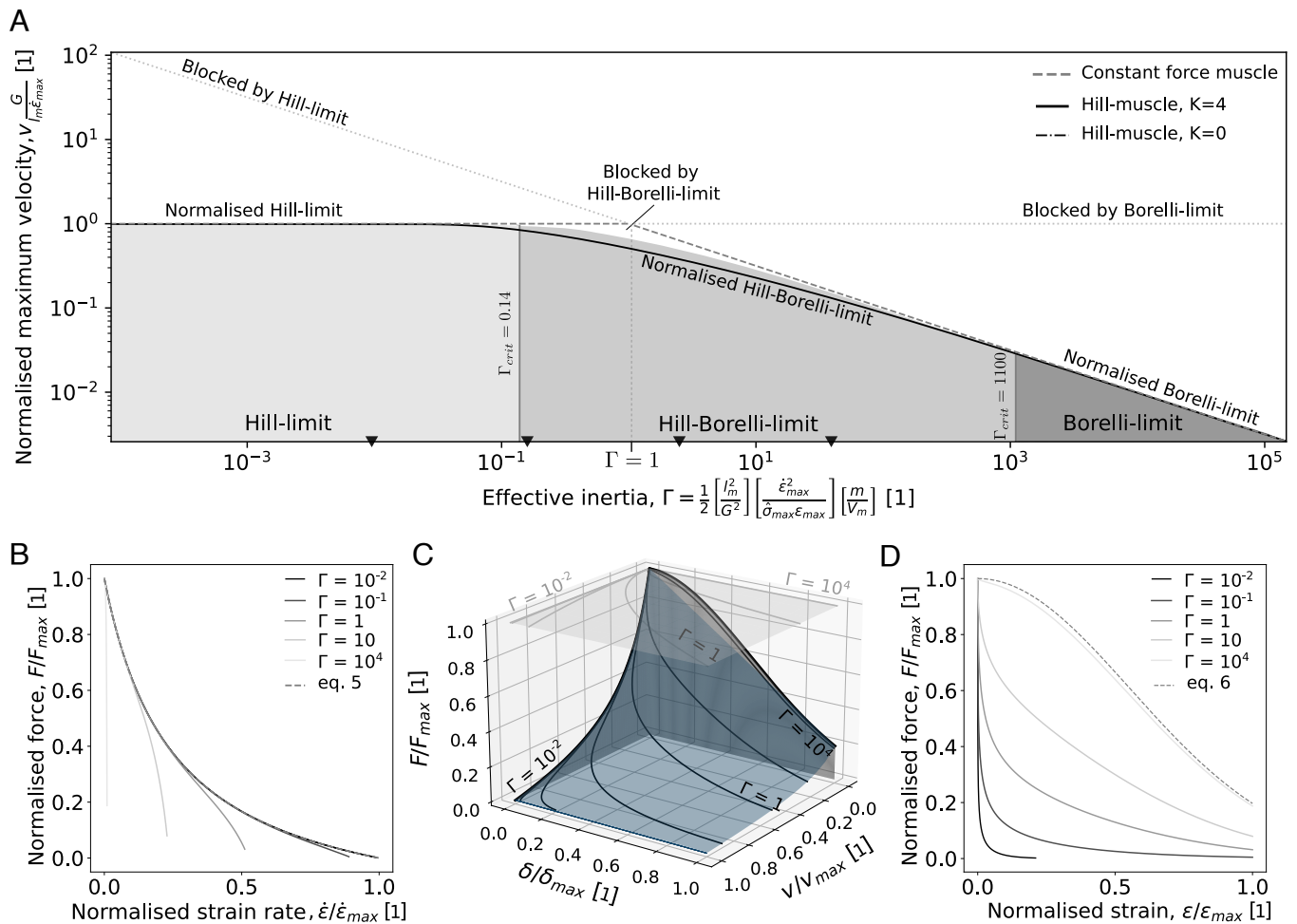


Fig. 1. (A) The maximum speed that muscle can impart in a single contraction depends on the effective inertia, Γ , of the mass-musculoskeletal system. For $\Gamma < 1$, the speed is bound by the Hill limit (Eq. 2), which arises because muscle has a finite maximum strain rate, $\dot{\epsilon}_{max}$. For $\Gamma > 1$, the speed is bound by the Borelli limit (Eq. 1), which arises because muscle can only shorten by a fraction of its length, $\epsilon_{max}l_m$. For a constant force muscle, the Hill and the Borelli limit are exact expressions for the maximum speed (dark gray dashed line), and the transition between both occurs abruptly at $\Gamma = 1$. For a Hill muscle (black solid & dashed lines), where the force depends both on muscle strain rate and strain, the Hill and the Borelli limit are asymptotic, reasonably accurate only below or above a critical value Γ_{crit} (SI Appendix); for intermediate values of Γ , the speed is bound by the Hill-Borelli limit instead, which reflects reductions in work capacity due to the strain-rate dependence of the muscle force. Black triangles at the Bottom indicate an estimate for the effective inertia of the hindlimb of a generalized tetrapod with a body mass of 10 g, 1 kg, 100 kg, and 10 ton, respectively (Left to Right, see text for details). (B) The effective inertia controls the fraction of the maximum strain rate that muscle can access. For vanishing Γ , the contraction may be considered quasi-instantaneous, and the relation between force and velocity is described solely by the FV relationship of the muscle (cf. to (D), and Eq. 5). (C) The solutions of all possible equations of motion can be visualized on a 3D landscape which relates the normalized force to the normalized displacement and velocity. For a constant force muscle, the resulting contractile landscape is a horizontal plane (gray, on top), but for a Hill muscle, it describes a complex 3D envelope (blue), shaped by the projections of the FV and FL relationships, respectively. A muscle with small Γ operates in the Hill limit and contracts close to the FV plane; a muscle with large Γ operates in the Borelli limit and contracts close to the FL plane. (D) The effective inertia determines the fraction of the maximum strain over which muscle can accelerate. For diverging Γ , the relation between force and displacement approaches the FL relationship (dashed line), and the contraction may thus be considered quasi-static with respect to the maximum relative speed (cf. to (B), and Eq. 6).

I squared the ratio for convenience, and split the equation into three terms to distinguish between distinct determinants of the effective inertia: the geometry of the musculoskeletal system, represented by the gear ratio and the allocation of a unit volume of muscle into fiber length versus cross-sectional area; the physiology of the muscle, represented by the maximum average stress, strain rate, and strain; and a characteristic density, m/V_m , which may be interpreted as a relative investment of muscle tissue compared to the mass that is to be moved. If $\Gamma < 1$, the muscle is Hill-limited, and if $\Gamma > 1$, the muscle is Borelli-limited; $\Gamma = 1$ corresponds to the unique special case for which a constant force muscle operates simultaneously at both limits.

I note that the specific parameter combination in Eq. 3 also falls out of more formal dimensional analyses as a dimensionless mass (see SI Appendix in refs. 33, 36, and SI Appendix in ref.

16 for a similar result for series elasticity). Throughout this work, I will discuss several possible interpretations of Γ . For example, Γ also follows as the ratio between the kinetic energy associated with a contraction at maximum strain rate, and the work done in a contraction to maximum strain (SI Appendix, Eq. S6). For $\Gamma < 1$, the muscle uses a fraction $\epsilon = \Gamma \epsilon_{max}$ of its strain capacity to reach its maximum strain rate (Fig. 1A and B). For $\Gamma > 1$, in turn, the muscle uses its entire strain capacity to accelerate to a fraction $\dot{\epsilon} = \Gamma^{-1/2} \dot{\epsilon}_{max}$ of its maximum strain rate (Fig. 1A and D). Dimensionless numbers such as Γ can be interpreted in a number of ways, and I submit that the effective inertia may best be thought of as a physiological similarity index a notion which combines all possible interpretations into one term, and on which I will expand on further below.

It is of obvious interest to estimate the effective inertia of “real” muscle and musculoskeletal systems. In *SI Appendix*, I derive two such estimates using published data (3, 37–40). First, for a representative vertebrate muscle contracting against itself, $\Gamma \approx 2/3 l_m^2$ meters⁻². Thus, even for a long muscle with a fiber length of 1 m, $\Gamma \approx 2/3 < 1$; for a fiber length of 1 cm, the effective inertia drops to $\Gamma \approx 2/3 \cdot 10^{-4}$. Second, for a generalized tetrapod hindlimb contracting to accelerate the body mass, $\Gamma \approx 4/25 m^{0.6}$ kg^{-0.6}. Thus, for a shrew with a body mass of 0.01 kg, $\Gamma \approx 0.01$; for a mole with a body mass of 0.1 kg, $\Gamma \approx 0.04$; for a cat with a body mass of 1 kg, $\Gamma \approx 0.16$; for a dwarf crocodile with a body mass of 10 kg, $\Gamma \approx 0.64$; for a caribou with a body mass of 100 kg, $\Gamma \approx 2.5$; for a rhinoceros with a body mass of 1,000 kg, $\Gamma \approx 10$; and for an elephant with a body mass of 10,000 kg, $\Gamma \approx 40$. The strong size-dependence of Γ is evident, and will be discussed in more detail below.

The Equations of Motion Landscape and the Hill-Borelli Transition for Real Muscle. The above analysis is valid for a muscle which generates a constant force throughout the contraction. In reality, however, muscle is more complex a motor, and the force it generates is a function of both its relative strain rate, $\dot{\epsilon}_{rel} = \dot{\epsilon} \dot{\epsilon}_{max}^{-1}$, and its relative length, $l_{rel} = l/l_{opt}$ (26, 27): Muscle produces maximum force during an isometric contraction, $\dot{\epsilon} = 0$, at “optimal” length, $l = l_{opt}$, and less force for any deviation from these conditions. Unfortunately, as the muscle contracts to accelerate the mass, it must change both its length and contractile speed; the net force it generates—and thus, the acceleration the mass experiences—consequently varies continuously throughout the contraction. In order to assess the effect of this dynamic complexity, I now introduce the force–length (FL) and force–velocity (FV) properties of muscle. Three simplifying assumptions: aid this analysis: The muscle activation time constant, t_{act} , is much smaller than the characteristic acceleration time, $t_{act} \ll t^* \sim v_m m F_m^{-1} G^{-2}$, so that the muscle can be considered fully activated throughout; I consider a single contraction from rest at the optimal length, so that the relative length can be reexpressed via the strain, $l_{rel} - 1 = \epsilon = \Delta l_m l_m^{-1}$; and the normalized FV and FL functions, $FV = f(\dot{\epsilon}_{rel})$ and $FL = f(\epsilon)$, respectively, are independent, and each modulate the generated muscle force such that it is equal to some fraction of its maximum value (dashed lines in Fig. 1 *B* and *D*). The muscle force may then be written as $F_m = F_{max} f(\dot{\epsilon}_{rel}) f(\epsilon)$.

In order to develop some intuition for the effect of FV and FL properties on muscle contraction dynamics, I briefly return to the simpler case of a muscle which generates a constant force throughout the contraction, i. e. $f(\dot{\epsilon}_{rel}) = f(\epsilon) = 1$, and thus $F_m = F_{max}$. The contraction dynamics—that is the change of speed and displacement with time—are governed by the equation of motion (EoM), $a = F_{max} G m^{-1}$. All possible solutions of this EoM can be visualized in a single plot of the normalized net force against the normalized displacement and velocity, respectively (Fig. 1*C*). Because the net force is constant throughout the contraction, all such solutions lie in a horizontal plane (gray plane at the top of Fig. 1*C*). Consider now the path inscribed onto this plane by contractions with different effective inertias; as an illustrative example, let the very same muscle contract against different masses. For any specific mass, the contraction describes a unique trajectory onto the EoM plane: If the mass is very small, Γ vanishes, and the mass thus gains normalized speed rapidly, and with minimum normalized displacement; the contractile trajectory is almost parallel to the FV-line. If the mass is large,

in turn, Γ diverges and the normalized speed remains small throughout the displacement; the contractile trajectory is almost parallel to the FL-line. For intermediate masses, corresponding to Γ close to unity, the contraction involves significant changes in both normalized speed and displacement and thus describes a more complex FVL trajectory (Fig. 1*C*).

Consider next the more complex case of a Hill muscle with FV and FL properties, governed by the EoM, $a = F_{max} G m^{-1} f(\dot{\epsilon}_{rel}) f(\epsilon)$. The two horizontal lines which defined the EoM plane for a constant-force muscle are now curves, and the EoM plane is thus transformed into a three-dimensional EoM landscape, shaped by their projection (Fig. 1*C*). The principal logic and interpretation, however, remain the same: If the muscle contracts against a vanishing mass, Γ is small, the acceleration is large, and the muscle reaches its maximum strain rate with a small change in length. The EoM of the contraction is defined solely by the muscle’s FV properties, $f(\epsilon) \approx 1$, so that the contractile trajectory is approximately equal to the FV-curve (Fig. 1 *B* and *C*). If the muscle contracts against a diverging mass, in turn, Γ is large, the acceleration is small, and the muscle will have shortened by its maximum amount long before it has reached its maximum strain rate. The EoM of the contraction is defined solely by the muscle’s FL properties, $f(\dot{\epsilon}_{rel}) \approx 1$, so that the contractile trajectory is approximately equal to the FL-curve (Fig. 1 *C* and *D*). The relative FV and FL functions may thus be interpreted as the sole contributors to the EoMs of two contractions which represent unphysical extremes: a quasi-instantaneous contraction which reaches the maximum strain rate with vanishing strain; and a quasi-static contraction, during which a muscle shortens by its maximum strain with a vanishing increase in strain rate.

Although the introduction of FV and FL properties leaves the effect of variations in Γ qualitatively unaltered, there exists a material difference. For a constant-force muscle, the Hill and the Borelli limit are exact expressions for the maximum speed muscle can impart; the transition between both limits is sharp and occurs at $\Gamma = 1$, where the muscle reaches its maximum contraction velocity exactly when it has contracted to the maximum strain (Fig. 1*C*). For a Hill muscle, the Hill limit remains intact, but the Borelli limit is now only exact in the limit of diverging Γ , for which the contraction becomes quasi-static; the imparted speed is smaller than v_{Bo} for any other contraction to ϵ_{max} . This result may be understood qualitatively as follows: the Borelli limit is the speed that can be imparted during a contraction which involves the maximum possible work output, or, equivalently, the maximal possible area underneath the FL-trajectory. For a constant-force muscle, this area is maximized for any contraction to ϵ_{max} . For a Hill muscle, however, the area is maximal only for a quasi-static contraction; any increase in muscle strain rate reduces the muscle work output compared to this maximum Fig. 1*D* and ref. 19. Because the work output during realistic displacement-limited contractions is influenced by both the FL and the FV-function, I will refer to the corresponding speed limit as the Hill–Borelli limit, v_{Hi-Bo} .

Evaluation of the Hill–Borelli limit requires solution of the EoM $a = F_{max} G m^{-1} f(\dot{\epsilon}_{rel}) f(\epsilon)$. This EoM is a nonlinear differential equation, which can be solved by rewriting it as a path integral, which permits separation of variables (*SI Appendix* for detailed derivations and further discussion of the results which follow):

$$\int_0^{\delta_{max}} \frac{F_{max} G}{m} f(\delta) d\delta = \int_0^{v_{Hi-Bo}} \frac{v}{f(v)} dv, \quad [4]$$

where I used the coupling $\delta = l_m \varepsilon G^{-1}$ and $v = l_m \dot{\varepsilon} G^{-1}$, respectively, to reexpress the strain and strain rate in terms of the integration variables. Eq. 4 may be recognized as the Work–Energy theorem, which relates the work done by the muscle to the resulting change in the kinetic energy.

Up to this point, the exposition is agnostic to the form of the FL and FV relationship, and thus general.[‡] Further evaluation however requires a specific choice, which is not trivial, for there are no accepted first principle forms of the FL and the FV functions of striated muscle (but see ref. 41, for exciting recent developments). I proceed with two common forms, not to proclaim their superiority, but merely by way of example; the procedure laid out here may be followed just as well for any other choice. I describe the FV relationship with a normalized Hill relation (1, 26, see dashedline in Fig. 1B):

$$F_m = F_{max} \underbrace{\left[\frac{1 - \dot{\varepsilon}_{rel}}{1 + K \dot{\varepsilon}_{rel}} \right]}_{f(\dot{\varepsilon}_{rel})}. \quad [5]$$

Here, K is a dimensionless constant of order unity, which controls the curvature of the FV relationship (1). The FL relationship, in turn, may be written as (e.g., ref. 42, see dashed line in Fig. 1D):

$$F_m = F_{max} \underbrace{\left[\exp(-\beta \varepsilon^2) \right]}_{f(\varepsilon)}, \quad [6]$$

where β is a dimensionless shape parameter, which controls how quickly the force decays with strain.

The two integrals in Eq. 4 have a closed-form solution for these two choices, but an explicit writing in terms of v_{Hi-Bo} is only possible for a linear FV relationship, i.e., $K = 0$ (*SI Appendix*):

$$v_{Hi-Bo} = v_{Hi} \left[1 + \mathbb{W} \left(-\exp \left(-1 - \frac{1}{2\Gamma} \right) \right) \right], \quad [7]$$

where \mathbb{W} is the Lambert \mathbb{W} function. Although only exact for the special case $K = 0$, this solution captures all relevant physical (dimensional) parameters, and confirms that the effective inertia remains the key dimensionless number which governs muscle performance: For $\Gamma \rightarrow 0$, $v_{Hi-Bo} \rightarrow v_{Hi}$, and for $\Gamma \rightarrow \infty$, $v_{Hi-Bo} \rightarrow v_{Bo}$ (Fig. 1A. In *SI Appendix*, I derive limiting values Γ_{crit} , below or above which the Hill and the Borelli number are within 1% of v_{Hi-Bo} and may thus be considered reasonable approximations). I thus define the Hill–Borelli number, Hi-Bo $\propto v v_{Hi-Bo}^{-1}$, as dynamic similarity index which characterizes the maximum output of a Hill muscle across a broad range of Γ . It is instructive to compare the prediction via Eq. 7 to i) the result for a constant force muscle and ii) to a numerical result for $K = 4$ and $\beta = 6.5$ —reasonable values for animal muscle (refs. 3, 43, and *SI Appendix*). v_{Hi-Bo} remains within 30% of either result for any value of Γ and may thus be considered sufficiently accurate unless all experimental quantities are known with small error (Fig. 1A). All that follows nevertheless proceeds with the general form of the Hill relation to retain generality.

Finding an expression for the maximum speed that muscle can impart is, at first glance, a simple problem in Newtonian mechanics. But the simplicity of the governing equations is deceiving. No muscle can contract by more than ε_{max} , or faster

than with $\dot{\varepsilon}_{max}$. Because these boundary conditions compete and dynamically couple to the mass that is accelerated, and because muscle is a rather peculiar motor with complex FV and FL functions, the problem acquires considerable subtlety. It was demonstrated that the resulting complexity is suitably captured by a single characteristic dimensionless number: the effective inertia, or the physiological similarity index, Γ .

The Effective Work and Power Density of Muscle and the “Optimal” Geometry of Musculoskeletal Systems

Equipped with a first-order understanding of the relevance of the effective inertia in muscle contractions, one may next interrogate musculoskeletal “design.” A classic concept in the analysis of muscle performance is the notion of a characteristic work and power density; each unit mass of muscle can at most deliver an ostensibly fixed maximum amount of work and power, and these maxima represent putatively suitable metrics to characterize muscle performance limits (4, 7, 9, 10, 22, 33, 36). What determines whether a mass-musculoskeletal system operates close to these limits?

By definition, muscle operates with maximum work density, $W_{\rho,max}$, in the Borelli limit, where it contracts over the largest possible distance with the smallest possible increase in strain rate (Figs. 2A and 3); $W_{\rho,max}$ is a sole function of the muscle’s FL properties, the muscle density, ρ , and the maximum strain, $W_{\rho,max} \sim \hat{\sigma}_{max}(\varepsilon_{max}) \varepsilon_{max} \rho^{-1}$ (*SI Appendix*, Eqs. S12 and S16). As may be expected by analogy, muscle operates with maximum average power density in the Hill limit, where it reaches any strain rate with a minimum loss in force due to length changes (Fig. 2B); $P_{\rho,max}$ is a sole function of the muscle’s FV properties, its density, and a characteristic strain rate, $P_{\rho,max} \sim \hat{\sigma}_{max}(\dot{\varepsilon}_c) \dot{\varepsilon}_c \rho^{-1}$ (*SI Appendix*, Eqs. S13 and S20, and note that the stress is now time-averaged). For a muscle which generates constant force, maximum average power is delivered in contractions to $\dot{\varepsilon}_{max}$, but for a muscle with FV properties, average power is maximized when the contraction is terminated at a lower strain rate (about half of $\dot{\varepsilon}_{max}$ for $K = 4$; *SI Appendix* for a detailed calculation and refs. 44 and 45 for related results).[§]

To explore the implications of these observations for musculoskeletal design, consider first again the simpler case of a constant force muscle. A unit volume of muscle operates with $W_{\rho,max}$ in the Borelli limit and with $P_{\rho,max}$ in the Hill limit. It can thus only operate with both $W_{\rho,max}$ and $P_{\rho,max}$ if $\Gamma = 1$, the unique effective inertia at which the musculoskeletal system is simultaneously in both limits (Fig. 2C). For $\Gamma < 1$, muscle only delivers a fraction of its work density, equal to $W_{\rho,\%} = \Gamma$, and for $\Gamma > 1$, it delivers only a fraction of its power density, equal to $P_{\rho,\%} = \Gamma^{-1/2}$ (*SI Appendix*, and Fig. 2A–C). The product of the relative power and work densities thus takes a maximum value of unity at $\Gamma = 1$ and is equal to Γ for $\Gamma < 1$ and to $\Gamma^{-1/2}$ for $\Gamma > 1$. Somewhat fortuitously, Γ can thus also be interpreted as the fraction of the maximum work and average power density that muscle can deliver. Indeed, Γ may also be derived as the ratio between the average power and work density of the contracting muscle, $P_{\rho,max} W_{\rho,max}^{-1} = 1/2 \dot{\varepsilon}_{max} \varepsilon_{max}^{-1}$, which defines a characteristic physiological time scale; normalization of this time scale with the time it takes to accelerate to the maximum strain rate, $t_{max} = m \dot{\varepsilon}_{max} l_m \hat{F}_{max}^{-1} G^{-2}$, yields the effective inertia.

[§]In fact, the power density goes to zero as the strain rate approaches $\dot{\varepsilon}_{max}$ because the Hill relation is asymptotic; (see *SI Appendix*).

[‡]But see *SI Appendix* for a discussion on the choice of the integration limits.

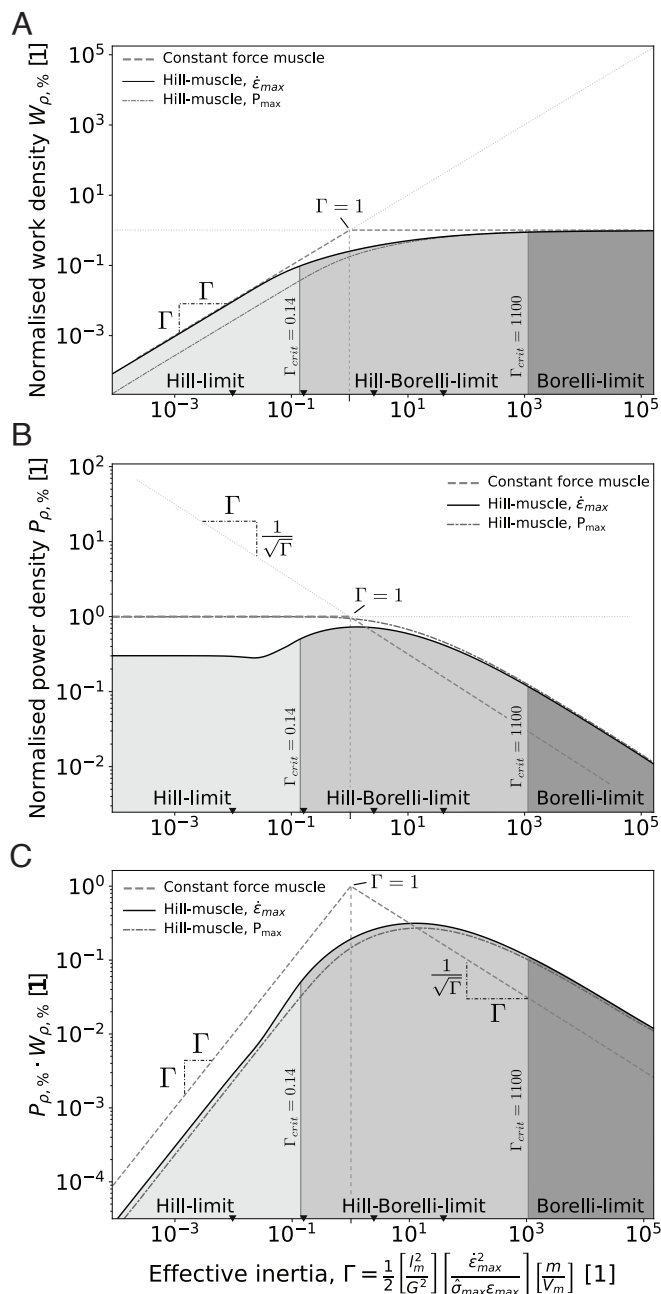


Fig. 2. A muscle delivers its maximum work density, $W_{\rho,max}$, in the Borelli limit (A), and its maximum power density, $P_{\rho,max}$, in the Hill limit (B). The effective inertia Γ is directly related to the fractions $W_{\rho,\%}$ and $P_{\rho,\%}$ delivered in the Hill and the Borelli limit, respectively, as indicated by the slopes. (C) Maximizing the product between $W_{\rho,\%}$ and $P_{\rho,\%}$ may be considered a design objective: A constant force muscle operating at $\Gamma = 1$ can deliver both its maximum work and power density simultaneously. For a Hill muscle, the maximum product is less than unity and occurs at $\Gamma > 1$. Dark gray lines show contractions which result in maximum average power output, P_{max} , as opposed to close to maximum strain rate, $0.99\dot{\epsilon}_{max}$ (SI Appendix, Text). Black triangles at the Bottom indicate an estimate for the effective inertia of the hindlimb of a generalized tetrapod with a body mass of 10 g, 1 kg, 100 kg, and 10 ton, respectively (Left to Right).

For a muscle with FV and FL properties, these results are no longer exact, but the scaling relations hold in the limit of small and large Γ , i.e., where the Hill–Borelli limit is close to the Hill and the Borelli limit, respectively (Fig. 2A–C). Although there no longer exists an effective inertia at which the muscle is simultaneously in both the Hill and the Borelli limit, an

equivalent optimum may still be defined as the value of Γ which maximizes the product between $W_{\rho,\%}$ and $P_{\rho,\%}$. This maximum product is now smaller than unity and occurs at an effective inertia larger than unity (Fig. 2C). An exploration of the exact value of Γ which corresponds to this putative optimum as a function of the FL and FV properties of muscle is beyond the scope of this work. However, the implication is clear: Operation with small or large Γ means operation with suboptimal work or power density, respectively (Fig. 2A–C).

It is instructive to note that although neither $W_{\rho,max}$ nor $P_{\rho,max}$ depend on the geometry of the musculoskeletal system, nor on the mass muscle contracts against, the ability of muscle to deliver either depends on both (Fig. 2A and B and Eq. 3). In the classic literature, the influence of mass on the ability of muscle to deliver $W_{\rho,max}$ or $P_{\rho,max}$ has rarely been explicitly considered (but see e.g., refs. 19–21, 24, 46, and 22), and variations in musculoskeletal anatomy are typically interpreted as controlling a trade-off between force and velocity. The above result demonstrates that this popular interpretation is correct only if muscle operates in the Hill limit (i.e. $\Gamma < 1$), where musculoskeletal geometry determines the extent to which a unit power is split into force versus velocity (Eq. 2). In sharp contrast, in the Borelli limit (i.e. $\Gamma > 1$), the maximum velocity is independent of the musculoskeletal geometry (Eq. 1), which instead merely determines the extent to which a unit amount of work is split into force and displacement, respectively; changing the gear ratio in the Borelli limit changes the force, but leaves the maximum velocity unaffected. Consider as an illustrative example a muscle operating close to an effective inertia of unity: Increasing the gear ratio results in a reduction of both the maximum achievable speed and the time it takes to reach this maximum speed; the power remains constant but the work done decreases. Decreasing the gear ratio, in turn, leaves the maximum speed unchanged but increases the time it takes to reach it; the work remains constant but the power decreases (see refs. (20) and (23) for other results indicating a work–power trade-off modulated by musculoskeletal geometry). At an effective inertia of unity, the musculoskeletal system imparts the maximum possible speed in the shortest possible time.

On the basis of these remarks, it is tempting to consider $\Gamma \approx 1$ as the “optimal design” for a musculoskeletal system. This may well be so, but the notion of a maximum speed, power, and work density as the sole design objective is likely overly simplistic for at least two reasons. First, where muscle is expected to move a range of masses in stereotypical scenarios, muscle performance is not suitably characterized by a single-valued effective inertia and will thus deviate by necessity from any putative optimum. Second, delivering the same amount of muscle mass-specific work or power in a different time may well be associated with a variation in efficiency, i.e., the amount of metabolic energy required to deliver a unit amount of mechanical energy. Such variation may then favor effective inertias smaller or larger than unity.

Parasitic Forces and the Truncation of the EoM Landscape

The above analysis is vulnerable to the reasonable criticism that it is concerned with a case of seemingly limited practical relevance—muscle is never the sole contributor to the net force that accelerates the mass. I will next demonstrate that the initial development, though restricted to a special case, constructed an conceptual framework strong enough to carry the burden of further complexity.

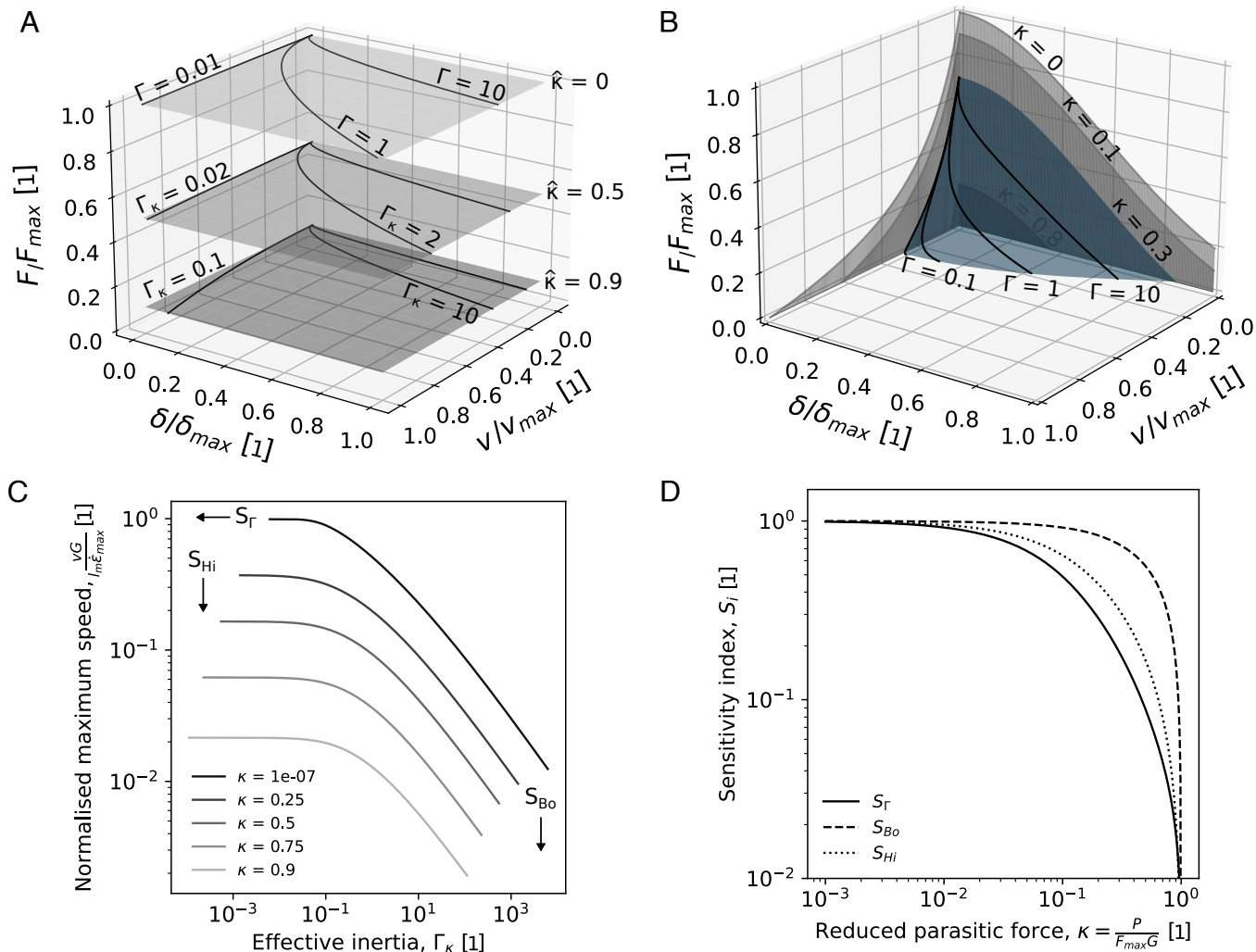


Fig. 3. External forces which oppose motion influence muscle dynamics in two distinct ways, distinguished in their generality by their dependence on the force-length (FL) and force-velocity (FV) relationship. (A) A constant opposing force, P , manifests its presence via a downward shift of the equation-of-motion (EoM) plane; P consumes part of the work done by muscle and may thus be considered “parasitic.” The amount of muscle work which flows into parasitic instead of kinetic energy is quantified by the reduced parasitic energy, $\hat{\kappa} = P\hat{F}_m^{-1}G^{-1}$, where \hat{F}_m is the muscle force averaged over the displacement, and G is the gear ratio. The effective inertia increases with $\hat{\kappa}$, as illustrated by the contractile trajectories on each EoM plane. (B) For a Hill muscle, the influence of parasitic forces is more complex. Because the FL and FV functions are now curves, the downward shift of the EoM plane results in a truncation of the accessible speed and displacement range. The extent of this truncation depends on the magnitude of the reduced parasitic force, $\kappa = PF_{max}^{-1}G^{-1}$, as illustrated by the FL and FV planes, and the EoM plane for $\kappa = 0.3$. (C) The net effect of a constant parasitic force is a decrease in both the maximum relative speed and the effective inertia. (D) The magnitude of these changes can be described by proportionality constants, S_i , which depend on κ and may thus serve as sensitivity indices that quantify the importance of external forces (Eqs. 11a–12): For $\kappa < 0.005$, $\kappa < 0.01$, and $\kappa < 0.05$, all $S_i \geq 0.95$, i. e., Γ_κ , $H_{i\kappa}$ and $B_{o\kappa}$ are within 5% of Γ , v_{Hi} , and v_{Bo} , respectively—the parasitic force may be neglected. The asymptote at $\kappa = PF_{max}^{-1}G^{-1} = 1$ is a force limit to muscle-driven motion. En route to this asymptote, all S_i decline steeply. For typical FL and FV relationships, the Hill number is more sensitive to parasitic forces than the Borelli number, as the muscle force declines more sharply with strain rate than with muscle strain.

The net force is the vector sum of all external forces. Where such forces oppose the muscle force, they will influence muscle dynamics in two distinct ways, distinguished in their generality by their dependence on the FV and FL relationships. Let a muscle contract against an opposing force P . The opposing force is “parasitic,” in the sense that it does negative work; it consumes part of the work done by muscle and, in doing so, redirects it from kinetic energy to other forms of energy—heat, gravitational potential energy, what have you. To evaluate the partitioning of muscle work into kinetic versus parasitic energy, one can find from conservation of energy:

$$\frac{E_{kin}}{W_m} = 1 - \frac{E_{para}}{W_m} = 1 - \hat{\kappa}, \quad [8]$$

where W_m is the work done by muscle. The reduced parasitic energy $\hat{\kappa} = P\hat{F}_m^{-1}G^{-1}$ is the fraction of muscle work consumed by the parasitic force, with the immediate consequence that $1 - \hat{\kappa}$ represents the fraction of muscle work which flows into kinetic energy. Because $\hat{\kappa}$ is the ratio of the work done by the parasitic and the driving force, which both act over the same displacement, it is, in general, a ratio of average forces. For $\hat{F}_m G = 10\hat{P}$, 90% of the work done by muscle flows into kinetic energy, and for $\hat{F}_m G = 2\hat{P}$, it is half. For $\hat{F}_m G = 20\hat{P}$, the error in neglecting the parasitic force in the energy balance is less than 5%, and for $\hat{F}_m G = \hat{P}$, muscle can do zero work; no acceleration is possible at all, and the system is in equilibrium. The reduced parasitic energy can be related to familiar dimensionless numbers, such as the Froude, Strouhal, or Reynolds number for gravitational, elastic,

or viscous parasitic forces, respectively, via $E_{kin}E_{para}^{-1} = \hat{\kappa}^{-1} - 1$ (note that these then differ from their definition in Alexander's sense, as gravitational and elastic energy are no longer the source of kinetic energy, but a sink for muscle work). I submit that their definition via a ratio of forces is preferable in problems of muscle dynamics because it places the focus on the agent which caused the change in energy: the contracting muscle.

For a constant force muscle, $\hat{\kappa}$ fully captures the influence of parasitic forces on muscle performance. The Hill number remains unchanged, but the Borelli number and thus the effective inertia gain an additional term, defined by Eq. 8. The net effect of the parasitic force is thus an increase of the effective inertia by a factor $\Gamma_{\kappa}\Gamma^{-1} = (1 - \hat{\kappa})^{-1}$; as $\hat{P} \rightarrow \hat{F}_m G$, the constant force muscle is increasingly likely to be Borelli-limited (Fig. 3A), and reaching a unit speed takes longer. The interpretations developed above remain valid, but now refer to the work that flows into kinetic energy, rather than the total muscle work.

For a Hill muscle, the influence of parasitic forces is more complex, which may be illustrated by returning to the notion of the EoM landscape. For a constant force muscle, the presence of a constant parasitic force manifests itself in a downward shift of the EoM plane (Fig. 3A). The net force is reduced, but the maximum possible relative speed and displacement remain unchanged because the muscle force is independent of muscle strain and strain rate; the relative FL and FV functions are equal and constant. For a Hill muscle, the FL and FV functions are curves. As a consequence of the downward shift of the normalized net force, these curves may now intersect with the zero plane at a shortening velocity smaller than $l_m \dot{\epsilon}_{max}$ and at a finite displacement smaller than $l_m \epsilon_{max}$; parasitic forces truncate the EoM landscape (Fig. 3B and refs. 30, 31, 47–51). The extent of this truncation can, in principle, be quantified through an exercise in equilibrium mechanics (refs. 30, 47, 50, and 51): The maximum relative displacement over which the muscle can accelerate, and the maximum strain rate it can contract with are reached when the net force is zero, i.e., when the muscle force balances the parasitic force. For constant P , analytical evaluation of the fraction of the strain rate and strain that is accessible is straightforward: Each fraction corresponds to the point on the FL and FV curves at which the muscle force is equal to P . Setting P equal to the FV and FL functions defined by Eqs. 5 and 6 yields:

$$\epsilon_{\kappa} = \begin{cases} \epsilon_{max} & \text{if } \sqrt{\log(\kappa)(-\beta)^{-1}} \geq \epsilon_{max} \\ \sqrt{\log(\kappa)(-\beta)^{-1}} & \text{otherwise} \end{cases}, \quad [9]$$

$$\frac{\dot{\epsilon}_{\kappa}}{\dot{\epsilon}_{max}} = \frac{1 - \kappa}{1 + K\kappa}, \quad [10]$$

where I introduced the reduced parasitic force, $\kappa = PF_{max}^{-1}G^{-1}$. Because the parasitic force truncates both the strain rate and strain range, both the Hill and Borelli limit are altered and follow from combination of Eqs. 9 and 10 with Eqs. 1 and 2, respectively:

$$v_{Hi,\kappa} = v_{Hi} \underbrace{\left[\frac{1 - \kappa}{1 + K\kappa} \right]}_{S_{Hi}}, \quad [11a]$$

$$v_{Bo,\kappa} = v_{Bo} \underbrace{\left[C \left(\sqrt{\frac{\pi}{4\beta}} \operatorname{erf}(\sqrt{\beta}\epsilon_{\kappa}) - \kappa\epsilon_{\kappa} \right) \right]^{0.5}}_{S_{Bo}}. \quad [11b]$$

Here, erf is the error function, C is a constant that depends on β and ϵ_{max} (SI Appendix, Eq. S25), and S_i are sensitivity indices

which quantify the importance of the parasitic force (see below and Fig. 3D). Both the Hill and the Borelli limit now approach an asymptote of zero speed at a critical reduced parasitic force $\kappa = 1$; a “force limit” to muscle-driven motion. Close to this limit, both the Hill and the Borelli limit drop rapidly (Fig. 3C and D). The effective inertia follows immediately as the squared ratio of the Hill and the Borelli number:

$$\Gamma_{\kappa} = \Gamma \left[\frac{(1 - \kappa)^2}{(1 + K\kappa)^2 C \left(\sqrt{\frac{\pi}{4\beta}} \operatorname{erf}(\sqrt{\beta}\epsilon_{\kappa}) - \kappa\epsilon_{\kappa} \right)} \right]. \quad [12]$$

For $G = 4$ and $\beta = 6.5$, Eq. 12 is a decreasing function of κ (Fig. 3C and D).

The integration of parasitic forces into the definition of the effective inertia, and the visualization of its effect via the EoM landscape are conceptually simple. But even for the trivial case of a constant parasitic force, the increase in mathematical complexity is noticeable. Indeed, analytical evaluation of the Hill and the Borelli number in the presence of parasitic forces will only rarely be possible, first because of the complex form of the FV and FL relationships, and second because parasitic forces may depend on speed (viscous dissipation), or displacement (structural dissipation), resulting in nontrivial interactions with muscle contraction dynamics. A thorough evaluation of the above results and their generalization to characteristic nonconstant forces will have to await further work. However, from the cursory analysis presented here emerge two points of note.

First, for a given reduced parasitic force, Γ_{κ} , $v_{Bo,\kappa}$, and $v_{Hi,\kappa}$ are constant multiples of Γ , v_{Hi} , and v_{Bo} . The proportionality constants, S_i , which link both definitions (see bracketed terms in Eqs. 11a, b and 12), are thus suitable indices for the sensitivity to parasitic forces: For $\kappa < 0.005$, $\kappa < 0.01$, and $\kappa < 0.05$, all $S_i \geq 0.95$ (Fig. 3D). In other words, Γ_{κ} , $v_{Hi,\kappa}$, and $v_{Bo,\kappa}$ are within 5% of Γ , v_{Hi} , and v_{Bo} , respectively, and the parasitic force may be neglected in leading order analyses. To illustrate the utility of this simple analysis, consider briefly a long-standing observation in comparative biomechanics: Small animals are seemingly untroubled by the presence of gravity, and only change locomotor speed slightly, if at all, between running on horizontal or vertical surfaces. In contrast, larger animals generally slow down significantly when moving up inclines (52–55). The relevant parasitic force is the gravitational force, $F_g = mg$, and the reduced parasitic force thus reads $\kappa_g = mgF_{max}^{-1}G^{-1}$, and a ratio between kinetic and parasitic energy—the Froude number of the contraction— $Fr = \kappa_g^{-1} - 1$. An approximate limit $\kappa_g \geq 0.05 m^{1/3} kg^{-1/3}$, where m is the body mass in kilograms, was estimated from published data by Alexander (56). Thus, animals with a body mass $m < 1$ g, $m < 10$ g and $m < 1$ kg may be considered “gravitationally indifferent” in terms of their effective inertia, their Hill and their Borelli number, respectively, in robust agreement with the scarce experimental data (52–54). The work done by the muscle of small animals against the gravitational force is negligible, because the reduced parasitic force is small, and the muscle Froude number is large (see also ref. 18).

Second, the role of musculoskeletal anatomy, represented by the ratio between muscle fiber length and skeletal gear ratio, $l_m G^{-1}$, needs careful reinterpretation. In the absence of parasitic forces, the Borelli number is agnostic to musculoskeletal anatomy because all work flows into kinetic energy, irrespective of whether

it is done by displacing a large force over a small distance, or a small force over a long distance (see above and Eq. 1). Musculoskeletal anatomy does however control the speed in the Hill limit, which is maximal for maximum values of $l_m G^{-1}$ (Eq. 2). In the presence of parasitic forces, both results change fundamentally (Eq. 11a and b). In the Borelli limit, the split of a unit work into force versus displacement now matters because it controls the partitioning into parasitic versus kinetic energy; minimizing $l_m G^{-1}$ minimizes the reduced parasitic energy, $\hat{\kappa} = \hat{P}\hat{\sigma}_{max}^{-1}V_m^{-1}l_m G^{-1}$. In the Hill limit, in turn, maximizing $l_m G^{-1}$ will now minimize speed because it increases the reduced parasitic force, $\kappa = P\sigma_{max}^{-1}V_m^{-1}l_m G^{-1}$, so amplifying the truncation of the accessible contractile speed range (refs. 48 and 50; the analogous result holds for the truncation of the strain range in the Borelli-limit). Thus, in both the Hill and the Borelli limit, increasing the gear ratio or decreasing the muscle fiber length may now increase not only the net force but also the maximum possible velocity and displacement, in noteworthy contrast to their canonical interpretation as parameters which control putative force–velocity or force–displacement trade-offs (see above and refs. 57–59, for a recent controversial discussion of this topic). This force–velocity trade-off is now more complex: If $l_m G^{-1}$ is too small, the mass can only reach a fraction of its theoretical maximum possible speed, and the muscle only has access to a fraction of its work density; if it is too large, in turn, muscle performance is reduced by parasitic losses instead (Fig. 3 C and D). The optimum anatomy thus likely corresponds to intermediate values of $l_m G^{-1}$ that result in effective inertias close to the transition between the Hill and the Borelli limit; around this transition, the absolute speed, and relative effective work and effective power density are all close to their theoretical maximum (Figs. 1 and 2). Realizing this optimum will require a different anatomy for a physiologically identical muscle contracting against varying parasitic force (Fig. 3 C and D). Some reduced parasitic forces, for example, those due to gravity, will vary systematically with animal size, $\kappa_g \propto m^{1/3}$ (assuming geometric similarity). It follows at once that there now exists an incentive to depart from geometric similarity via systematic variation of musculoskeletal anatomy, for example, due to posture variation (20, 38), in order to remain close to the putative optimum: A systematic increase of the gear ratio with size can attenuate the decrease in the Froude number, and keep a larger fraction of the dynamic muscle performance space accessible.

A Theory of Physiological Similarity in Muscle-Driven Motion

Muscle is a motor with a complexity to baffle any mind, but its operation is eventually restricted to a space bound by the laws of physics. In the above, an attempt was made to analyse how these laws interact with some of the key physiological and anatomical idiosyncrasies of muscle, in an effort to delineate fundamental bounds on its mechanical performance. From this analysis emerged three dimensionless parameters—the effective inertia Γ , the reduced parasitic energy $\hat{\kappa}$, and the reduced parasitic force κ —which quantify the relative importance of different physiological and physical constraints on a continuous scale.

The effective inertia, Γ , provides a direct measure of the extent to which the contractile performance of a unit volume of muscle is limited by muscle strain rate versus strain capacity, and thus of the fraction of the maximum power and work muscle can deliver. Analogous to how seemingly different problems in fluid

dynamics are considered hydrodynamically similar if they occur with equal Reynolds number, problems in muscle-driven motion may be considered physiologically similar if they involve equal Γ : The involved muscles will operate with comparable fractions of their maximum strain rate and strain capacity, follow similar contractile trajectories along the EoM landscape, and deliver a similar fraction of their maximum power and work density. A unit volume of muscle has access to its maximum performance space if the musculoskeletal geometry is such that contractions occur with an effective inertia close to unity. For much smaller or much larger Γ , muscle contractions may be considered quasi-instantaneous or quasi-static, and are effectively governed by the power or work density of muscle, or—equivalently—its FV or FL relationship, respectively. Analytical expressions for the maximum possible speed in these limits are available in the form of the Hill, the Hill–Borelli, and the Borelli number, which shed light on the distinct relevant “design” features of the musculoskeletal system in each regime.

The reduced parasitic energy and force, $\hat{\kappa}$ and κ , quantify the relative importance of parasitic forces which oppose muscle contraction, consume muscle work, and truncate the accessible mechanical performance space. In the presence of parasitic forces, the Hill and the Borelli number, and thus the effective inertia, gain additional terms which may serve as sensitivity indices. For $\kappa < 0.005$, parasitic forces may be ignored to first order; for $\kappa > 0.005$, they alter the dynamics by more than a few percent. Large parasitic forces can decrease both the effective inertia of the contraction and the maximum speed muscle can impart, and can fundamentally change how musculoskeletal anatomy modulates canonical trade-offs between force and velocity or force and displacement. It stands to reason that any investigation of muscle performance, and any assessment of musculoskeletal design, ought to explicitly consider the magnitude of Γ , κ , and $\hat{\kappa}$; ignoring them is to accept considerable risk of erroneous conclusions.

Up to this point, the text may have been heavy in theoretical thought, but arguably light in demonstrated practical consequence. Contractions at different Γ and κ may well be governed by rather different physiological and physical constraints, but what range of Γ and κ does real muscle find itself in? I note that both Γ and typical κ such as κ_g are size dependent: Under the parsimonious assumption of geometric similarity, all lengths scale as $L \propto m^{1/3}$, all areas as $A \propto m^{2/3}$, and all volumes as $V \propto m$. It follows that, for an isogeometric musculoskeletal system moving an isogeometric mass, $\Gamma \propto m^{2/3}$ and $\kappa_g \propto m^{1/3}$. Evolution has thus involuntarily conducted a control experiment in one of the world’s largest laboratories: the animal kingdom. Animals vary by at least 13 orders of magnitude in mass, so that, assuming geometric similarity, Γ should vary by a factor about $(10^{13})^{2/3} \approx 10^8$, and $1/\kappa_g$ should vary by a factor of $(10^{13})^{1/3} \approx 10^4$. Without allowing for nontrivial departures from geometric similarity, or systematic changes in muscle physiology, it is hard to avoid the conclusion that muscle of animals of different size operates in most substantially different physiological regimes, and with markedly different gravitational sensitivity.

The immediate implications of the influence and size-dependence of Γ and κ are profound and diverse: Characterisation of the maximum intrinsic muscle shortening speed via experiments on isolated muscle fibers is only sound if the contraction occurs in the Hill limit (ref. 35); extrapolation of such single-fiber experiments to whole muscle or in vivo performance can be misleading, as it is typically associated

with changes in Γ ; musculoskeletal geometry plays a more complex role than its canonical interpretation as a parameter that controls a force–velocity or force–displacement trade-off would have one believe, so that conclusions from comparative analyses of musculoskeletal functional morphology across species may need to be carefully reconsidered (see refs. 57 and 59); isogeometric animals of different sizes neither have access to the same (maximum) work density, nor to the same (maximum) power density per unit volume of muscle, and are suffering to different extents from parasitic losses to gravitational potential energy—three assertions which challenge the classic scaling theories in animal locomotion (3, 4, 7–9, 17, 21, 22, 33, 60, but ref. 24), and extrapolation of data on extant animals to infer muscle-driven locomotor performance of larger extinct animals may have to explicitly introduce the size dependence of Γ and κ to avoid physically possible but physiologically prohibited inference. Analyses framed in terms of Γ and κ may also provide inspiration for the design of legged robots and in sports biomechanics: Electrical motors have characteristic torque–rounds-per-minute relationships, akin to a FV function; many sports may be characterized by specific κ , which interacts with the muscle anatomy and physiology of the competing athlete. Some sports may provide dynamic control over κ , for example, gears in bicycles or oars in rowing, suggesting the possibility of optimal athlete-specific configurations (see ref. 50 for a similar suggestion). Whether future work verifies or rejects what at this point are mere hypotheses is immaterial to their potential to advance our understanding of muscle-driven motion, and of the design of musculoskeletal systems.

The insights provided by the theory of physiological similarity should not belie the fact that the list of tasks which need to be completed before it can be considered comprehensive is

1. T. A. McMahon, *Muscles, Reflexes, and Locomotion* (Princeton University Press, 1984), vol. 10.
2. M. H. Dickinson *et al.*, How animals move: An integrative view. *Science* **288**, 100–106 (2000).
3. R. M. Alexander, *Principles of Animal Locomotion* (Princeton University Press, 2003).
4. A. Biewener, S. Patek, *Animal Locomotion* (Oxford University Press, 2018).
5. S. L. Lindstedt, T. McGlothlin, E. Percy, J. Pifer, Task-specific design of skeletal muscle: Balancing muscle structural composition. *Comp. Biochem. Physiol. B, Biochem. Mol. Biol.* **120**, 35–40 (1998).
6. A. A. Biewener, Locomotion as an emergent property of muscle contractile dynamics. *J. Exp. Biol.* **219**, 285 (2016).
7. G. A. Borelli, *De Motu Animalium* (Angelo Bernabo, Rome, 1680).
8. D. A. W. Thompson, *On Growth and Form* (Cambridge University Press, 1917), vol. 2.
9. A. V. Hill, The dimensions of animals and their muscular dynamics. *Sci. Prog.* (1933) **38**, 209–230 (1950).
10. H. C. Bennet-Clark, "Scale effects in jumping animals" in *Scale Effects in Animal Locomotion*, T. J. Pedley, Ed. (Academic Press, London/New York, NY, 1977), pp. 185–201.
11. T. McMahon, Size and shape in biology: Elastic criteria impose limits on biological proportions, and consequently on metabolic rates. *Science* **179**, 1201–1204 (1973).
12. N. C. Heglund, C. R. Taylor, T. A. McMahon, Scaling stride frequency and gait to animal size: Mice to horses. *Science* **186**, 1112–1113 (1974).
13. R. McN. Alexander, A. S. Jayes, A dynamic similarity hypothesis for the gaits of quadrupedal mammals. *J. Zool.* **201**, 135–152 (1983).
14. R. Blickhan, R. J. Full, Similarity in multilegged locomotion: Bouncing like a monopode. *J. Comp. Physiol. A* **173**, 509–517 (1993).
15. R. McN. Alexander, Leg design and jumping technique for humans, other vertebrates and insects. *Philos. Trans. R. Soc. Lond., B, Biol. Sci.* **347**, 235–248 (1995).
16. A. Galantiss, R. C. Woledge, The theoretical limits to the power output of a muscle-tendon complex with inertial and gravitational loads. *Proc. R. Soc. B: Biol. Sci.* **270**, 1493–1498 (2003).
17. A. Bejan, J. H. Marden, Unifying constructal theory for scale effects in running, swimming and flying. *J. Exp. Biol.* **209**, 238–248 (2006).
18. M. N. Scholz, M. F. Bobbert, A. J. K. Van Soest, Scaling and jumping: Gravity loses grip on small jumpers. *J. Theor. Biol.* **240**, 554–561 (2006).
19. M. F. Bobbert, Effects of isometric scaling on vertical jumping performance. *PLoS ONE* **8**, e71209 (2013).
20. J. R. Usherwood, Constraints on muscle performance provide a novel explanation for the scaling of posture in terrestrial animals. *Biol. Lett.* **9**, 20130414 (2013).
21. N. Meyer-Vernet, J.-P. Rospars, How fast do living organisms move: Maximum speeds from bacteria to elephants and whales. *Am. J. Phys.* **83**, 719–722 (2015).
22. G. P. Sutton, M. Doroshenko, D. A. Cullen, M. Burrows, Take-off speed in jumping mantises depends on body size and a power-limited mechanism. *J. Exp. Biol.* **219**, 2127 (2016).
23. J. P. Olberding, S. M. Deban, M. V. Rosario, E. Azizi, Modeling the determinants of mechanical advantage during jumping: Consequences for spring- and muscle-driven movement. *Integr. Comp. Biol.* **59**, 1515–1524 (2019).

rather long indeed. It includes the appropriate consideration of activation and deactivation times and of variable muscle activation (61); the propagation velocity of muscle excitation (35, 62, 63); contraction history effects; nonconstant parasitic forces and gear ratios (e.g., refs. 23 and 64); muscle pennation (e.g., ref. 65); series compliance and the associated storage of strain energy in muscle and in tendons (e.g., refs. 16, 64, and 66); multisegment motion (e.g., ref. 19); and instances where muscle is lengthened, acts as a break, and does negative work (67–69)—to name but a few. I am under no illusion that the simple description of physiological similarity presented here will often be inadequate, and fail to produce a convincing account across the breathtaking diversity of tasks performed by muscle. However, it is my hope that identifying the origin of these shortcomings will push us further in our understanding of the mechanical, physiological, neurological, developmental, and phylogenetic constraints that govern the operation of muscle across the animal tree of life.

Data, Materials, and Software Availability. There are no data underlying this work.

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24. J. R. Usherwood, N. W. Gladman, Why are the fastest runners of intermediate size? Contrasting scaling of mechanical demands and muscle supply of work and power. *Biol. Lett.* **16**, 20200579 (2020).
25. W. R. Stahl, Similarity and dimensional methods in biology. *Science* **137**, 205–212 (1962).
26. A. V. Hill, The heat of shortening and the dynamic constants of muscle. *Proc. R. Soc. Lond. B: Biol. Sci.* **126**, 136–195 (1938).
27. A. M. Gordon, A. F. Huxley, F. J. Julian, The variation in isometric tension with sarcomere length in vertebrate muscle fibres. *J. Physiol.* **184**, 170–192 (1966).
28. R. K. Josephson, Mechanical power output from striated muscle during cyclic contraction. *J. Exp. Biol.* **114**, 493–512 (1985).
29. J. L. Van Leeuwen, "Muscle function in locomotion" in *Advances in Comparative and Environmental Physiology*, R. McN. Alexander, Ed. (Springer, Heidelberg, 1992), vol. 11, pp. 191–249.
30. T. L. Daniel, Invertebrate swimming: Integrating internal and external mechanics. *Symp. Soc. Exp. Biol.* **49**, 61–89 (1995).
31. R. L. Marsh, How muscles deal with real-world loads: The influence of length trajectory on muscle performance. *J. Exp. Biol.* **202**, 3377–3385 (1999).
32. M. C. Jarur, J. Dumais, S. Rica, Limiting speed for jumping. Patterns and dynamics: Homage to Pierre Couillet/Forms et dynamique: Hommage à Pierre Couillet. *C. R. Mec.* **347**, 305–317 (2019).
33. G. P. Sutton *et al.*, Why do large animals never actuate their jumps with latch-mediated springs? Because they can jump higher without them. *Integr. Comp. Biol.* **59**, 1609–1618 (2019).
34. M. Günther *et al.*, Rules of nature's formula run: Muscle mechanics during late stance is the key to explaining maximum running speed. *J. Theor. Biol.* **523**, 110714 (2021).
35. M. Günther, O. Röhrle, D. F. B. Haeufle, S. Schmitt, Spreading out muscle mass within a hill-type model: A computer simulation study. *Comput. Math. Methods Med.* **2012**, 848630 (2012).
36. M. Ilton *et al.*, The principles of cascading power limits in small, fast biological and engineered systems. *Science* **360**, ea01082 (2018).
37. R. K. Josephson, Contraction dynamics and power output of skeletal muscle. *Annu. Rev. Physiol.* **55**, 527–546 (1993).
38. A. A. Biewener, Scaling body support in mammals: Limb posture and muscle mechanics. *Science* **245**, 45–48 (1989).
39. S. Medler, Comparative trends in shortening velocity and force production in skeletal muscles. *Am. J. Physiol. Regul. Integr. Comp. Physiol.* **283**, R368–R378 (2002).
40. P. J. Bishop, M. A. Wright, S. E. Pierce, Whole-limb scaling of muscle mass and force-generating capacity in amniotes. *PeerJ* **9**, e12574 (2021).
41. R. Rockenfeller, M. Günther, S. L. Hooper, Muscle active force-length curve explained by an electrophysical model of interfilament spacing. *Biophys. J.* **121**, 1823–1855 (2022).
42. E. Otten, A myocybernetic model of the jaw system of the rat. *J. Neurosci. Methods* **21**, 287–302 (1987).
43. F. Püffel, R. Johnston, D. Labonte, A biomechanical model for the relation between bite force and mandibular opening angle in arthropods. *R. Soc. Open Sci.* **10**, 221066 (2023).
44. G. N. Askew, R. L. Marsh, The effects of length trajectory on the mechanical power output of mouse skeletal muscles. *J. Exp. Biol.* **200**, 3119–3131 (1997).

45. G. S. Sawicki, P. Sheppard, T. J. Roberts, Power amplification in an isolated muscle-tendon unit is load dependent. *J. Exp. Biol.* **218**, 3700–3709 (2015).
46. J. M. Gabriel, The effect of animal design on jumping performance. *J. Zool.* **204**, 533–539 (1984).
47. P. Aerts, S. Nauwelaerts, Environmentally induced mechanical feedback in locomotion: Frog performance as a model. *J. Theor. Biol.* **261**, 372–378 (2009).
48. C. T. Richards, Building a robotic link between muscle dynamics and hydrodynamics. *J. Exp. Biol.* **214**, 2381–2389 (2011).
49. C. T. Richards, G. S. Sawicki, Elastic recoil can either amplify or attenuate muscle-tendon power, depending on inertial vs. fluid dynamic loading. *J. Theor. Biol.* **313**, 68–78 (2012).
50. C. T. Richards, C. J. Clemente, Built for rowing: Frog muscle is tuned to limb morphology to power swimming. *J. R. Soc. Interface.* **10**, 20130236 (2013).
51. C. J. Clemente, C. Richards, Muscle function and hydrodynamics limit power and speed in swimming frogs. *Nat. Commun.* **4**, 2737 (2013).
52. C. R. Taylor, S. L. Caldwell, V. J. Rowntree, Running up and down hills: Some consequences of size. *Science* **178**, 1096–1097 (1972).
53. A. V. Birn-Jeffery, T. E. Higham, The scaling of uphill and downhill locomotion in legged animals. *Integr. Comp. Biol.* **54**, 1159–11572 (2014).
54. L. G. Halsey, C. R. White, A different angle: Comparative analyses of whole-animal transport costs when running uphill. *J. Exp. Biol.* **220**, 161–166 (2017).
55. T. Wöhrli, L. Reinhardt, R. Blickhan, Propulsion in hexapod locomotion: How do desert ants traverse slopes? *J. Exp. Biol.* **220**, 1618–1625 (2017).
56. R. M. Alexander, The maximum forces exerted by animals. *J. Exp. Biol.* **115**, 231–238 (1985).
57. M. J. McHenry, There is no trade-off between speed and force in a dynamic lever system. *Biol. Lett.* **7**, 384–386 (2011).
58. A. S. Arnold, C. T. Richards, I. G. Ros, A. A. Biewener, There is always a trade-off between speed and force in a lever system: Comment on McHenry (2010). *Biol. Lett.* **7**, 878–879 (2011).
59. A. C. Osgood, G. P. Sutton, S. M. Cox, Simple muscle-lever systems are not so simple: The need for dynamic analyses to predict lever mechanics that maximize speed. bioRxiv [Preprint] (2021). <https://doi.org/10.1101/2020.10.14.339390> (Accessed 20 May 2023).
60. K. Schmidt-Nielsen, *Scaling: Why is Animal Size so Important?* (Cambridge University Press, 1984).
61. N. C. Holt, J. M. Wakeling, A. A. Biewener, The effect of fast and slow motor unit activation on whole-muscle mechanical performance: The size principle may not pose a mechanical paradox. *Proc. R. Soc. Lond. B: Biol. Sci.* **281**, 20140002 (2014).
62. F. Mörl, T. Siebert, S. Schmitt, R. Blickhan, M. Günther, Electro-mechanical delay in hill-type muscle models. *J. Mech. Med. Biol.* **12**, 1250085 (2012).
63. R. Rockenfeller, M. Günther, Extracting low-velocity concentric and eccentric dynamic muscle properties from isometric contraction experiments. *Math. Biosci.* **278**, 77–93 (2016).
64. T. J. Roberts, R. L. Marsh, Probing the limits to muscle-powered accelerations: Lessons from jumping bullfrogs. *J. Exp. Biol.* **206**, 2567–2580 (2003).
65. E. Azizi, E. L. Brainerd, T. J. Roberts, Variable gearing in pennate muscles. *Proc. Natl. Acad. Sci. U.S.A.* **105**, 1745–1750 (2008).
66. A. Wilson, G. Lichtwark, The anatomical arrangement of muscle and tendon enhances limb versatility and locomotor performance. *Philos. Trans. R. Soc. B: Biol. Sci.* **366**, 1540–1553 (2011).
67. B. Katz, The relation between force and speed in muscular contraction. *J. Physiol.* **96**, 45 (1939).
68. B. C. Abbott, X. M. Aubert, The force exerted by active striated muscle during and after change of length. *J. Physiol.* **117**, 77 (1952).
69. R. K. Josephson, D. R. Stokes, The force-velocity properties of a crustacean muscle during lengthening. *J. Exp. Biol.* **202**, 593–607 (1999).