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SENSITIVITY OF AVAILABILITY ESTIMATES TO INPUT DATA CHARACTERIZATION

THESIS

Darren P. Durkee, Major, USAF

AFIT/GOR/ENS/97M-06

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THESIS TITLE: Sensitivity of Availability Estimates to Input Data Characterization

DEFENSE DATE: 11 February 1997

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The views expressed in this thesis are those of the author and do not reflect the official policy or position of the Department of Defense or the U. S. Government.

SENSITIVITY OF AVAILABILITY ESTIMATES TO INPUT DATA CHARACTERIZATION

THESIS

Presented to the Faculty of the Graduate School of Engineering Air Force Institute of Technology Air University In Partial Fulfillment of the Requirements for the Degree of Master of Science in Operations Research

> Darren P. Durkee, B. S., M. S. B. A. Major, USAF

February 1997

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Acknowledgments

I am indebted to my thesis committee, Dr. Mykytka, Major Pohl, and Major Murdock for their guidance and assistance in completing this thesis. My research spanned several subject areas, including an area in which I had little prior knowledge (reliability theory), and their knowledge and experience were invaluable assets. I am also very appreciative of their even-handed and no nonsense approach in the oversight of my research efforts.

I would also like to thank my AFOTEC thesis sponsor, Major Chris Swider, who provided a clear research objective, was very responsive to my queries, and proved very flexible when I was 'fine tuning' the research objectives and scope.

I am also very grateful to the Air Force for providing me the opportunity to receive a degree and conduct research in the area of Operations Research in a full-time academic environment. The knowledge and experiences I have gained here will benefit me and the Air Force as I continue to serve.

Finally, I would like to express my gratitude to my family, Karin and Caroline, for their unwavering support throughout my AFIT and thesis experience. Their patience and encouragement helped keep me going when things seemed to be a little too overwhelming.

Darren P. Durkee

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Abstract

Reliability analysts are often faced with the challenge of characterizing the behavior of system components based on limited data. Any insight into which model input data is most significant and how much data is necessary to achieve desired accuracy requirements will improve the efficiency and cost effectiveness of the data collection and data characterization processes. This thesis assesses potential significant factors in the probabilistic characterization of component failure and repair behavior with respect to the effect on system availability estimates. Potential factors were screened for significance utilizing fractional factorial and Plackett-Burman experimental designs for several system models developed using an AFOTEC simulation program entitled RAPTOR.

Two input data characterization factors were found to have a significant affect on availability estimation accuracy: the size of the structure and the number of data points used for component failure and repair distributional fitting. Estimation error was minimized when the structures analyzed were small and many data points (in this case, 25) were used for the distributional fittings. Assuming constant component failure rates and using empirical repair distributions were found to be equally effective component characterization methods (pertaining to model availability estimation error) compared to using automated software fitting tools (or 'wizards'). The results of this study also indicate that there is no apparent benefit in concentrating on 'important' components for the highest fidelity distributional fittings.

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SENSITIVITY OF AVAILABILITY ESTIMATES TO INPUT DATA CHARACTERIZATION

I. INTRODUCTION

Overview

Reliability, maintainability, and availability (RM&A) analysis plays an integral part in

the design and production of efficient, cost-effective systems. According to Kapur and

Lamberson,

"The reliability of a system is the probability that, when operating under stated environmental conditions, the system will perform its intended function adequately for a specified time." [1:1]

"Maintainability is defined as the probability that a failed system can be made operable in a specified interval of downtime." [1:225]

"Availability is defined as the probability that a system is operating satisfactorily at any point in time..." and "is a measure of the ratio of the operating time of the system to the operating time plus the downtime." [1:225]

The Department of Defense and the Air Force conduct numerous studies into the

reliability and maintainability of current and future weapons systems in an effort to control

RM&A costs of fielded systems and to verify RM&A characteristics of systems which are

still in development. One key Air Force agency which conducts such studies is

Headquarters Air Force Operational Test and Evaluation Center (HQ AFOTEC).

AFOTEC manages a large portion of the Air Force's weapons system operational

verification and validation testing.

In an effort to describe a system's RM&A characteristics, analysts frequently represent the system with an analytical and/or simulation model. Reliability analysts will base these models on observed component failure and repair data, historical performance of similar systems, contractor estimates, as well as on certain traditional theoretical assumptions which have been developed in the field of reliability. In an ideal circumstance, data from extensive testing will be available for accurate probabilistic characterization of the various system components. However, due to various constraints and limitations, the analyst is often faced with the challenge of characterizing the behavior of system components based on limited data. In this instance, the analyst will need to make judgments as to how best characterize the input data to obtain acceptable analytical results.

Background

Systems are frequently broken down into sub-structures of components for RM&A analysis. Several categories of component structures have been defined in the field of reliability. The more common classes of structures include series, parallel, series-parallel, and complex structures. A complex structure is one that cannot be defined as series, parallel, or series-parallel. The simplest example of a series system contains two components as shown in Figure 1.



Figure 1. Simple Series System

Given that p_1 and p_2 (ranging in value from 0 to 1.0) represent the reliability of

components 1 and 2, respectively, and that all components operate independently of each other, then the system reliability function, $h(\mathbf{p})$, is

$$h(\mathbf{p}) = p_1 \cdot p_2.$$

A two component parallel system is shown in Figure 2.

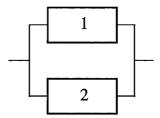


Figure 2. Simple Parallel System

In this case, the system reliability function is

$$h(\mathbf{p}) = 1 - [(1 - p_1) \cdot (1 - p_2)].$$

Series-parallel systems consist of combinations of series and parallel components in the system. An example is shown in Figure 3.

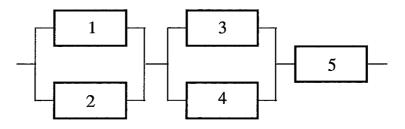


Figure 3. Series-Parallel System

The system reliability function for this series-parallel system is

$$h(\mathbf{p}) = \left[1 - (1 - p_1) \cdot (1 - p_2)\right] \cdot \left[1 - (1 - p_3) \cdot (1 - p_4)\right] \cdot p_5.$$

A typical complex structure can be illustrated by a bridge structure as shown in Figure 4.

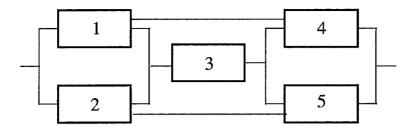


Figure 4. Bridge Structure

The system reliability function for a bridge structure is

$$h(\mathbf{p}) = 1 - [(1 - p_1 \cdot p_4) \cdot (1 - p_1 \cdot p_3 \cdot p_5) \cdot (1 - p_2 \cdot p_5) \cdot (1 - p_2 \cdot p_3 \cdot p_4)].$$

As can clearly be seen, the complexity of the system reliability function increases significantly as the size and complexity of the system structure increases.

Several analytical methods exist for determining steady-state properties of systems of components, including Markovian models, network theory, fault tree analysis, path and cut set analysis, Venn decomposition, non-homogenous Poisson processes (NHPP), and power law processes, to name a few. However, if the system under study is large and/or complicated, as is often the case, analytical methods can become cumbersome. Furthermore, most analytical methods provide insight only into the system's steady-state

properties, not it's transient properties. The task is further complicated when estimating system availability, since component repair rates must be considered. In such situations where analytical methods are inadequate or overly cumbersome, simulation provides a viable (and often times preferable) alternative [2:112].

In developing a simulation model, analysts must collect component failure and repair rate data (and/or use existing data) and then characterize this data to accurately represent the true behavior of the components of interest. More often than not, this data collection process is time consuming and expensive. Any insight into which model input data is most significant and how much data is necessary to achieve desired accuracy requirements should improve the efficiency and cost effectiveness of the data collection and data characterization processes.

Research Objectives

The general purpose of this study is to provide insight into input data characterization factors (such as volume of data utilized, data fitting methods, system size, type of system structure, and component importance) which may affect the accuracy of simulation model availability estimates. If we can identify the key factors which have a significant affect on model accuracy, the analyst can focus more attention on modeling these significant factors and less on the insignificant factors when soliciting and characterizing input data for an RM&A model.

Questions which need to be researched include:

(1) How much failure rate and repair rate data are needed for each component to obtain a desired model accuracy?

(2) Which data fitting techniques for characterizing component failure and repair probability distributions produce significant errors in model accuracy, and which do not?

(3) Do all components need the same fidelity of characterization, or can increased efficiency be realized by focusing on only the 'important' components?

(4) Are the answers to the above questions affected by system size, the underlying true component failure distributions, or other system characteristics?

Although the scope of this effort does not allow for a complete research of the above questions, much can be ascertained by conducting a controlled experiment. This research

is intended, using a design of experiment approach, to help identify the most critical pieces of data needed to ensure representative simulation results. Many efficiencies could be achieved if analysts were provided general input data characterization guidelines based on experimental results. Insights gained from this research may assist in the reduction of expensive live testing and unproductive data collection through the efficient use of simulation models.

The overall research objectives are to:

(1) Identify potential factors which affect availability model output accuracy.

(2) Screen these potential factors to determine which have a statistically significant effect (or interaction effect) on output accuracy.

(3) Assess the magnitude of the significant effects.

(4) Provide basic insight to analysts to aid in efficient input data characterization for availability models.

Scope

Although several model output measures may be of interest when analyzing a system, this study focused on the system availability output measure. A total of nine input data characterization factors (defined in Chapter 3), identified by several RM&A analysis experts and the author as factors with a potential affect on the accuracy of availability estimates, were analyzed. The probability density functions (pdf) used to define system component failure and repair rates were limited to 'common' functions encountered in reliability analysis, namely the Weibull and Lognormal pdf's. Component sparing was not considered in this research. To maintain economy of effort, the maximum size of any

analyzed system was limited to 20 total components and the structure types analyzed were series-parallel and complex.

Overview of Subsequent Chapters

Chapter 2 contains a review of existing literature covering several topics pertinent to this research. Major component importance measures, experimental designs for simulation (including screening designs), Plackett-Burman two-level experimental screening designs, and past research relating to this effort are all explored.

The research was conducted in two stages: a preliminary experiment to validate and refine the methodology, followed by a larger-scale experiment. Chapter 3 includes a description of the research methodology for the preliminary experiment which assessed five input data characterization factors. Chapter 3 also includes a discussion of the specific designed experimental screening methods used as well as specific analytical techniques used for data analysis for the preliminary experiment. The software used for availability model development, random variate generation, and data fitting are described.

Chapter 4 contains the results from the preliminary experiment. Statistical results are presented which identify the factors which proved significant in affecting availability model output accuracy.

Chapters 5 and 6 include descriptions of the methodology refinements and results of the final experiment. This experiment analyzed nine input data characterization factors.

Chapter 7 contains a summary of the thesis effort, including an overview and discussion of the impact of the results, how these results may benefit reliability analysts, and ideas for future research.

II. LITERATURE REVIEW

Overview

This chapter provides an overview of the current literature in areas pertaining to this thesis. This chapter begins by reviewing several major methods of defining component importance which are found in the literature. It then provides an overview of two-level designed experimental methods for factor screening in simulation experiments. One screening experimental technique, Plackett-Burman (P-B) experimental designs, was used in this research and is discussed in detail. Finally, past research which relate to this effort are reviewed.

Component Importance Measures

Systems are frequently broken down into sub-structures of components to aid in system design, analysis, and repair. Component importance measures provide a scientific, quantitative approach of identifying the most important components in a given structure of components. As an example of a common application, system designers can use component importance measure to identify which components are most critical in the proposed design structure. Furthermore, reliability analysts can use component important measures to determine which components are most crucial in defining the overall system reliability [3:195].

Several component importance measures have been developed in reliability theory since Birnbaum introduced the first mathematical component importance measures in 1969. Current component importance measures can be categorized into three areas: structural,

time dependent, and time independent. This section provides an outline of several of the major component importance measures which have been published in recent years and are common in use.

Terminology. All systems considered in this paper are coherent systems comprised of binary state components. A coherent system is one in which all components are relevant in maintaining a functional system. Binary state components have just two states: functioning or failed. The states are typically represented as

X(t) = 1 if the component functions at time t

= 0 if the component is failed at time *t*.

A system's (as opposed to a component's) reliability function is depicted as $h(\mathbf{p})$, where \mathbf{p} represents the component reliability vector. A component's reliability function is a function of time and is depicted as $p_{(i)}(t)$ for component *i*.

Structural Component Importance Measures. Structural importance measures are based solely upon the structural design of the system. They are used when the system structure function is known, but the individual component reliabilities are not known [4:583]. Two key structural methods have been developed by Birnbaum as well as Barlow and Proschan.

Birnbaum Structural Measure. The Birnbaum structural measure provides a measure of the criticality of a component in maintaining a system's functional state. Annotated as $I_{B,\phi}^{(i)}$ for component *i*, it represents the proportion of system state vectors which are critical for component *i* [5:456]. When the system components are independent, it can be calculated by the following equation [4:584]:

$$I_{B,\phi}^{(i)} = \frac{\partial h(\mathbf{p})}{\partial p_i} \bigg|_{p_1 = \dots = p_n = \frac{1}{2}}$$
(1)

This measure does not take into account the individual reliabilities of each system component.

Barlow-Proschan (B-P) Structural Measure. The Barlow-Proschan (B-P) structural measure assumes that component reliabilities are not known, but can be assumed to be the same for each component and assigned the value p. It is defined by the equation

$$I_{BP,\phi}^{(i)} = \int_0^1 [h(1_i, \mathbf{p}) - h(0_i, \mathbf{p})] dp$$
(2)

where $h(1_i, \mathbf{p})$ represents the system reliability function when component *i* is functioning and $h(0_i, \mathbf{p})$ represents the system reliability function when component *i* is not functioning [5:457].

Time-Dependent Component Importance Measures. While structural importance measures are only dependent upon the underlying system structure, time-dependent measures take into consideration the component reliabilities at some chosen time *t*. They are typically utilized when both the system structure and the component reliability functions are known. Two frequently used time-dependent measures include one developed by Birnbaum and another introduced by Veseley and Fussell.

Birnbaum Reliability Importance Measure. Birnbaum's reliability importance measure assesses a component's importance at time *t*. If a system is comprised of *n* components whose reliabilities at time *t* are $p_1, p_2, ..., p_n$ and $h(p_1, p_2, p_3, ..., p_n)$ represents

the system reliability at time t, then the Birnbaum reliability importance measure for component i is given by

$$I_{B}^{(i)}(t) = h(p_{1},...,p_{i-1},1,p_{i+1},...,p_{n}) - h(p_{1},...,p_{i-1},0,p_{i+1},...,p_{n})$$
$$= \frac{\partial h(\mathbf{p})}{\partial p_{i}}$$
(3)

It represents the decrease in system reliability when component *i* fails [6:266]. The Birnbaum reliability importance measure is the most frequently used time-dependent measure because of relative ease in calculation and because it provides the 'fairest' basis of comparison between components [5:458].

Veseley-Fussell (V-F) Importance Measure. Another popular time-dependent component importance measure, introduced by Veseley and Fussell in 1972, utilizes cutset theory to define component importance. The V-F importance measure, $I_{VF}^{(i)}(t)$, represents the conditional probability that a cut set containing component *i* has failed at time *t*, given that the system has failed at time *t*.

Many other time-dependent measures, most of which are variations of those discussed previously, also exist. For the sake of brevity, these additional measures, including those developed by Butler and Aven arising from network theory, will not be discussed in this paper.

Time-Independent Component Importance Measures. Both structural measures and time-dependent measures have inherent characteristics which make them inappropriate for certain analyses. Structural measures do not consider component reliabilities, and time-dependent measures are only valid for one specific instance in time. As a result, time-independent measures have been developed in an attempt to address these issues. Time-independent measures allow component importance rankings for a desired time interval. Several time-independent measures have been developed, most of which are some form of weighted average of the Birnbaum reliability measure [7:160]. Two of the most prominent time-independent measures are those developed by Barlow and Proschan and B. Natvig.

Barlow-Proschan Time-Independent Measure. The first time-independent component importance measure was introduced by Barlow and Proschan in 1975. The B-P measure represents the probability that component *i* causes system failure in the time period $(0, \tau)$. It is represented by

$$I_{BP}^{(i)} = \int_0^\tau I_B^{(i)}(t) \cdot f^{(i)}(t) dt$$
(4)

where $I_B^{(i)}(t)$ represents the Birnbaum reliability measure at time t and $f^{(i)}(t)$ is the failure probability density function for component i. $I_{BP}^{(i)}$ can also be interpreted as the probability that the system life equals the life of component i [8:158].

Natvig Importance Measure. In 1979, Natvig introduced another timeindependent component importance measure. The Natvig measure is defined by

$$I_N^{(i)} = \int_0^\tau I_B^{(i)}(t) \cdot p_{(i)}(t) \cdot (-\ln p_{(i)}(t)) dt$$
(5)

where $p_{(i)}(t)$ represents the reliability function for component *i*. The Natvig measure represents the reduction in expected remaining system lifetime (up to time τ) due to the failure of the *i*th component [9:280].

Other time-independent measures have been developed by Aven, Bergman, Narros, Boland, and Xie, most of which are extensions or advancements of the above listed measures. Furthermore, a significant amount of work has been done in the development of importance measures for multi-state and repairable components. Space does not allow discussion of these additional measures, but Boland and El-Neweihi [5] is an excellent reference providing an overview of each method and a list of applicable references.

Numerical Example of Component Importance Measures. To further demonstrate the calculation of the various importance measures, a numerical example is offered. For the given structure shown in Figure 5, the Birnbaum structural measure, Birnbaum reliability time-dependent measure, and the Barlow-Proschan and Natvig time-independent measures will be calculated.

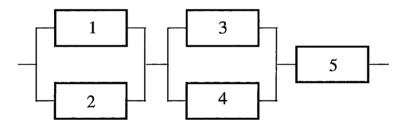


Figure 5. Example System

Table 1 defines the probability distribution and reliability functions for the various system components.

Component			
(i)	Failure Distribution	$\mathbf{f}^{(i)}(t)$	$p_{(i)}(t)$
1	Weibull: Shape = 1.1 (hrs) Scale = 3500 Location = 0	$\frac{1.1 \cdot t^{(1)}}{3500^{(1.1)}} e^{\left[-(\frac{t}{3500})^{1.1}\right]}$	$e^{\left[-(\frac{t}{3500})^{1.1}\right]}$
2	Weibull: Shape = 1.1 Scale = 3500 Location = 0	$\frac{1.1 \cdot t^{(.1)}}{3500^{(1.1)}} e^{\left[-(\frac{t}{3500})^{1.1}\right]}$	$e^{\left[-(\frac{t}{3500})^{1.1}\right]}$
3	Weibull: Shape = 1.5 Scale = 2000 Location = 0	$\frac{1.5 \cdot t^{(5)}}{2000^{(1.5)}} e^{\left[-(\frac{t}{2000})^{1.5}\right]}$	$e^{\left[-(\frac{t}{2000})^{1.5}\right]}$
4	Weibull: Shape = 1.5 Scale = 2000 Location = 0	$\frac{1.5 \cdot t^{(.5)}}{2000^{(1.5)}} e^{\left[-(\frac{t}{2000})^{1.5}\right]}$	$e^{\left[-\left(rac{t}{2000} ight)^{1.5} ight]}$
5	Weibull: Shape = 2.0 Scale = 2000 Location = 0	$\frac{2.0 \cdot t}{2000^{(2.0)}} e^{\left[-(\frac{t}{2000})^{2.0}\right]}$	$e^{\left[-(\frac{t}{2000})^{2.0}\right]}$

Table 1. Component Failure Distributions and Reliability Functions for Example System

Based on the structure function, the system reliability function is

$$h(\mathbf{p}) = \left[1 - (1 - p_1) \cdot (1 - p_2)\right] \cdot \left[1 - (1 - p_3) \cdot (1 - p_4)\right] \cdot p_5$$
(6)

Birnbaum Structural Measure Example. Since both components 1 and 2 as well as 3 and 4 are identical and in-parallel (and the structural importance measure does not consider component reliability), the structural importance measure values for components 1 through 4 will be the same.

Recall from equation (1) that

$$I_{B,\phi}^{(i)} = \frac{\partial h(\mathbf{p})}{\partial p_i} \bigg|_{p_1 = \dots = p_n = \frac{1}{2}}$$

For component 1,

$$\frac{\partial h(\mathbf{p})}{\partial p_1} = (1 - p_2) \cdot \left[1 - (1 - p_3) \cdot (1 - p_4)\right] \cdot p_5 \tag{7}$$

When $p_i = \frac{1}{2}$, from equation (7),

$$I_{B,\phi}^{(1)} = \frac{\partial h(\mathbf{p})}{\partial p_1} = .1875 = I_{B,\phi}^{(2)}$$

For component 3,

$$\frac{\partial h(\mathbf{p})}{\partial p_3} = \left[1 - (1 - p_1) \cdot (1 - p_2)\right] \cdot (1 - p_4) \cdot p_5 \tag{8}$$

•

Therefore, when $p_i = \frac{1}{2}$,

$$I_{B,\phi}^{(3)} = \frac{\partial h(\mathbf{p})}{\partial p_3} = .1875 = I_{B,\phi}^{(4)}$$

Using the same method to calculate the measure for component 5,

$$I_{B,\phi}^{(5)} = \frac{\partial h(\mathbf{p})}{\partial p_5} = .5625$$

Therefore, the Birnbaum structural measure component ranking (in descending order) is $5, \{1, 2, 3, 4\}$.

Birnbaum Reliability (Time-Dependent) Measure Example. Recall from

equation (3), $I_B^{(i)}(t) = \frac{\partial h(\mathbf{p})}{\partial p_i}$. Since this is a time-dependent measure, a specified time

value (t) must be selected. In this example, t = 1000 hours. Therefore,

for component 1,

$$I_{B}^{(1)}(t) = \frac{\partial h(\mathbf{p})}{\partial p_{1}} = (1 - p_{2}(t)) \cdot [1 - (1 - p_{3}(t)) \cdot (1 - p_{4}(t))] \cdot p_{5}(t)$$
(9)
= .158135

where $p_i(t)$ is given in Table 1. Since component 1 and 2 are identical and in-parallel, component 2's importance measure will also equal .158135.

Similarly, for components 3 and 4, $I_{B}^{(3)}(t) = \frac{\partial h(\mathbf{p})}{\partial p_{3}} = .220421 = I_{B}^{(4)}(t)$.

For component 5, $I_B^{(5)}(t) = \frac{\partial h(\mathbf{p})}{\partial p_5} = .866066$.

Therefore, the Birnbaum reliability (time-dependent) importance measure component ranking (in descending order) is 5, $\{3, 4\}$, $\{1, 2\}$.

Barlow-Proschan Time-Independent Measure Example. From equation (4),

 $I_{BP}^{(i)} = \int_{0}^{\tau} I_{B}^{(i)}(t) \cdot f^{(i)}(t) dt$. A time period of interest (for the range of integration) must be specified to calculate time-independent measures. In this example, the time period will be 0 to 50,000 hours (i.e. $\tau = 50,000$). For components 1 and 2, where $I_{B}^{(1)}(t)$ is given in equation (9) and $p_{1}(t)$ and $f^{(1)}(t)$ are provided in Table 1,

$$I_{BP}^{(1)} = \int_0^{50,000} I_B^{(1)}(t) \cdot f^{(1)}(t) dt = .056671 = I_{BP}^{(2)} .$$

Similarly, for components 3 and 4,

$$I_{BP}^{(3)} = \int_0^{50,000} I_B^{(3)}(t) \cdot f^{(3)}(t) dt = .145126 = I_{BP}^{(4)} .$$

For component 5,

$$I_{BP}^{(5)} = \int_{0}^{50,000} I_{B}^{(5)}(t) \cdot f^{(5)}(t) dt = .596417 \quad .$$

Therefore, the Birnbaum time-independent importance measure component ranking (in descending order) is 5, $\{3, 4\}$, $\{1, 2\}$.

Natvig Time-Independent Importance Measure Example. From equation (5),

 $I_N^{(i)} = \int_0^\tau I_B^{(i)}(t) \cdot p_{(i)}(t) \cdot (-\ln p_{(i)}(t)) dt$. For components 1 and 2, where $I_B^{(1)}(t)$ is given in

equation (9) and $p_1(t)$ is provided in Table 1,

$$I_N^{(1)} = \int_0^{50,000} I_B^{(1)}(t) \cdot p_{(1)}(t) \cdot (-\ln p_{(1)}(t)) dt = 66.7423 = I_N^{(2)} .$$

For components 3 and 4,

$$I_{N}^{(3)} = \int_{0}^{50,000} I_{B}^{(3)}(t) \cdot p_{(3)}(t) \cdot (-\ln p_{(3)}(t)) dt = 142.9822 = I_{N}^{(4)}$$

and for component 5,

$$I_N^{(5)} = \int_0^{50,000} I_B^{(5)}(t) \cdot p_{(5)}(t) \cdot (-\ln p_{(5)}(t)) dt = 402.3612$$

Therefore, the Natvig importance measure component ranking (in descending order) is 5, {3, 4}, {1, 2}.

In this particular example, the various demonstrated measures resulted in equivalent importance rankings for the system components (the Birnbaum structural method did not differentiate between components $\{1, 2\}$ and $\{3, 4\}$ because it considered only system structure and not component reliability) as summarized in Table 2.

Table 2. Importance Measure Rankings for Example System

Importance Measure	Ranking (highest to lowest)
Birnbaum Structural	5, {1, 2, 3, 4}
Birnbaum Reliability	5, {3, 4}, {1, 2}
Barlow-Proschan	5, {3, 4}, {1, 2}
Natvig	5, {3, 4}, {1, 2}

However, due to the different methods used in the calculation of component importance measures, there will not necessarily be agreement in component rankings between the various measures. Several instances were cited in the literature where one measure produced completely opposite ranking results from another measure. Therefore, analyst judgment is required for the selection of the most appropriate importance measure for any given situation [10:1431].

Simulation Experimental Design and Factor Screening Methods

The purpose of any experiment is to gain insight about a particular system [11:424]. Typically, changes are made to particular inputs (called *factors*), and the effects of these changes on some output parameter(s) (called *responses*) are analyzed and measured. Computer simulation models allow analysts the benefit of experimenting with a system model instead of the actual system. This usually saves time and money, and is frequently the only practical method of analyses.

Rather than randomly trying different combinations of input factor levels to ascertain their affect on the response, designed experiments provide an efficient and systematic method for conducting such analysis. Using a designed approach, the analyst can determine in advance the number of simulation runs and input configurations for each run to obtain the desired information about the system [12:657]. When more than just a few factors are under study, a logical first step is to determine or 'isolate' those factors which significantly affect the response measure. The literature commonly describes this as factor screening. Several methods of factor screening are outlined in the literature including two-level factorial designed experiments, fractional factorial experiments, and Plackett-Burman (P-B) designs. Most factor screening methods consist of two-level designed experiments [13:50]. In fact, the most popular two-level experimental designs are fractional factorials and P-B designs [14:94]. Not until recently have designed factor screening experiments been used in the field of reliability to identify important factors which affect system performance [15:206].

A P-B designed experiment was used in this effort to identify the subset of active factors which affect availability estimation accuracy. This section provides a brief discussion of two-level factorial designed experiments, fractional factorial experiments, as well as an in-depth discussion of P-B designs and their projection properties.

Two-Level (2^{*k***}) Factorial Designed Experiments**. A full two-level factorial experiment, where each factor is assigned a high and low level, will be used to estimate the effects of each of the *k* factors under study as well as their interaction effects. It requires simulation runs for each of the 2^k possible factor-level combinations (called design points) [12:660]. When a relatively small number of factors are under consideration, a full two-level factorial experiment is desirable for factor screening because it identifies all active effects without confounding. However, when *k* becomes moderate in size, which is most often the case, the amount of runs required can become unreasonably large.

Fractional Factorial Designs. To reduce the number of runs required, a fractional factorial experiment can be run using a subset $(2^{k\cdot p})$ of the 2^k full-factorial design points. This will introduce confounding, thus reducing the amount of conclusive information

gained from the experiment. However, since we commonly assume higher-order interactions are negligible in factor screening experiments [16:17], fractional factorials can serve as excellent screening designs where only the main and two-factor interactions are of interest. The main disadvantage of fractional factorials is, like full factorials, they frequently require an impractical amount of simulation runs.

Plackett-Burman (P-B) Experimental Designs. P-B designs have traditionally been used in factor screening experiments to identify significant main effects [17:137], and they require significantly fewer runs than full and fractional factorials. P-B designs are designed experiments with two levels for estimating the effects of n - 1 factors at two levels in n runs. The number of runs (n) must be a multiple of four [18:423]. P-B designs are useful for screening experiments where several factors are of interest, but only a portion of these factors are suspected as being significant. They allow analysis of the main effects with a minimal number of experimental runs. The aliasing structure of P-B designs is complex, with the main effects being aliased with other interaction effects. Therefore, P-B designs are most effective when the experimenter has good reason to believe that the interaction effects are negligible. However, if some interaction effects are significant, they may be identified when using the P-B projection techniques outlined by Lin and Draper in [19].

Projection Properties of P-B Designs. When an experimental design is projected, analysis is conducted in a smaller dimension factor space to provide more detailed information concerning certain retained factors. For example, let's say an initial full factorial experiment was conducted assessing four factors with no replicates (i.e. 16 runs)

and only two factors proved significant. By ignoring the two insignificant factors, the design could be projected into a 2^4 full factorial experiment with four replicates. In this example, the projection produces replicates which allow for the calculation of pure error and the assessment of the appropriateness of the model fit.

Because of the saturated nature of Plackett-Burman designs, their projection properties are limited, but they can still be useful. Myers and Montgomery address this limitation by describing the projection properties of Plackett-Burman (P-B) experimental designs as unattractive [20:170]. However, with augmentation of additional runs to the original P-B design, some beneficial projection properties can be obtained. As Lin and Draper show, P-B designs can be quite useful in conducting screening experiments using a limited number of runs. Additionally, interaction effects can be analyzed by utilizing Lin and Draper's P-B projection techniques to obtain a higher resolution design in the significant factor space.

Lin and Draper's P-B Projection Techniques. An overview of Lin and Draper's

P-B projection concepts can be summarized in a few concise steps:

(1) Conduct a P-B designed experiment with the appropriate number of runs (*n*) for the factors which are to be screened and analyzed.

(2) Using Yates algorithm [21:323-324], identify the k factors which exhibit significant main effects.

(3) Use the associated P-B design columns for the k significant factors as the projected design in the k factor dimension.

(4) If necessary, conduct supplemental experimental runs using specified levels for the k significant factors to achieve a desired resolution for the projected design.

P-B Projections. Table 3 delineates the projections identified for the 12-run

Plackett-Burman design.

k	Design Number	Description
2	2.1	2^2 design with 3 replicates
3	3.1	2^3 design plus 2^{3-1} design
4	4.1	Add one more run to obtain a 2^{4-1} design
		Add two more runs to obtain 3/4 replicate design
		Add five more runs to obtain a 2^4 design
5	5.1	Add two more runs to obtain a 2_{III}^{5-2} design
		Add six more runs to obtain a 2_V^{5-1} design
	5.2	Add two more runs to obtain a 2_{III}^{5-2} design
		Add eight more runs to obtain a 2_N^{5-1} design
		Add ten more runs to obtain a 2_V^{5-1} design

 Table 3. Projection of a 12-run Plackett-Burman Design into k Dimensions [19]

A brief theoretical example may be the best method to demonstrate Lin and Draper's P-B projection techniques. The following is an example where n = 12 and k = 3. After conducting the 12 P-B runs, suppose only 3 of the 11 main effects prove to be significant (i.e. k = 3). By focusing only on the 3 columns that correspond to the k significant factors (in this example A, B, and C), the smaller design can be decomposed into a full 2^3 design and a 2^{3-1} design (where I = ±ABC). Figure 6 shows a full 12-run P-B design. If, after conducting the 12 runs for the P-B design, only factors A, B, and C possess significant main effects, the design can be projected (with rows rearranged) into the arrangement shown in Figure 7.

Run	A	B	C	D	E	F	G	H	I	J	K
1	+	-	.+.		-	-	+	. +	+	-	+
2	+	+	-	+	-	_	-	+	+	+	-
3	-	+	+	-	+		_	-	+	+	+
4	+	-	+	+	-	+	-	-	_	+	+
5	+	+	-	+	+	-	+	_	-	-	+
6	+	+	+	ŀ	+	+	-	+	_	1	-
7	-	+	+	+	_	+	+	-	+	-	_
8	-	-	+	+	+	-	+	+	1	+	_
9	1	-	-	+	+	+	-	+	+	1	+
10	+	-		_	+	+	+	+	+	+	_
11	-	+	-	-	-	+	+	+	-	+	+
12	-	-	-	-	-		-		-	-	_

Figure 6. Plackett-Burman Design (n = 12)

Run	A	B	С
1	+	. +	+
2	+	+	-
3	+	-	+
4	+	-	-
5	1	+	+
6	-	+	-
7	-	-	+
8	1	_	-
9	+	_ '	+
10	+	+	-
11	-	+	+
12	-	-	-

Figure 7. P-B Design Projection for n = 12 and k = 3 (A, B, C)

As can clearly be seen, runs 1 through 8 represent a full 2^3 design, and runs 9 through 12 represent a 2^{3-1} fractional design (where I = -ABC). These 12 runs will estimate all main effects of the 3 selected factors without aliasing and will also provide information to calculate pure error needed for lack of fit testing [19].

When k = 4 and k = 5 for the 12-run P-B design, no complete projection exists for the factors of interest. However, viable projections can be achieved by conducting

supplemental runs. When k = 4, one run can be added to obtain a 2_{IV}^{4-1} design, or five runs can be added to obtain a full 2^4 factorial design. An additional option is to supplement the runs to project the design into a three-quarter replicate. The three-quarter replicate consists of fewer runs than a full factorial design but more runs than a half fraction. The three-quarter replicate allows for estimation of the main effects and 2-factor interactions without aliasing with other 2-factor interactions [22]. For k = 4, two additional runs are needed to complete a three-quarter fraction design for the 4 factors of interest. When k = 5, two possible projection opportunities occur depending on the structure of the rows of the 5 selected columns from the original P-B design. If a repeat-run pair emerges, Lin and Draper call this a 5.1 design, where two more runs can be added to obtain a 2_{III}^{5-2} design, and six more runs can be added to obtain a 2_V^{5-1} design. If a mirror image pair emerges from the selected columns of the P-B design, this is a 5.2 design, where two additional runs gives a 2_{III}^{5-2} design, eight additional runs gives a 2_{IV}^{5-1} design, and ten additional runs achieves a 2_v^{5-1} design.

Benefits of P-B Designs. Utilizing Plackett-Burman designs and Lin and Draper's projection techniques offer an efficient way to conduct screening experiments when many factors are being considered, only a few are suspected of being significant, and higher order effects are assumed to be negligible. The projection techniques outlined allow analysis of the two-factor interactions in the *k*-dimensions of the projection while requiring less additional runs than a standard foldover.

Using a P-B experimental design for factor screening in this research provided the benefit of accomplishing the required objectives with maximum efficiency. In the final experiment, nine input data characterization factors were assessed for significance. A substantial amount of effort was required to set up each experimental run. The completion of a full two-level factorial experiment would have required 512 runs, while any viable fractional factorial design would also have required a large amount of runs. This was well beyond the scope of this research. On the other hand, the selected P-B design required only 12 experimental runs, while still providing analysis of the main effects and some two-factor interactions.

Past Research

The literature was reviewed for research in the areas of input data characterization and factor screening for system availability estimation. Numerous examples of factor screening experiments were found in the current literature. A few articles reviewed were closely related to this research and many facets of the final experimental design were extracted from these specific efforts. This section will briefly discuss six articles which closely paralleled and/or helped formulate the methodology for this thesis.

Sensitivity Analysis of Availability Estimates. Wolf [23] assessed the sensitivity of space system availability estimates to the underlying component reliability estimates. He utilized an iterative response surface methodology (RSM) to identify the system components whose component reliability significantly affected average system availability estimates. Individual component reliabilities were perturbed to high and low levels, and

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fractional factorial experiments were used for factor screening. From this analysis, Wolf formulated a regression model predicting average system availability regressed against the estimated component reliabilities. Extensive regression analysis, involving several iterations, was necessary to identify the significant or 'important' components. Four of the initial one hundred components were retained in the final system availability regression model. Wolf found very little sensitivity of predicted system availability to individual component failure rate estimates. He surmised that this insensitivity may be due in part to the simplicity of the model [24:69].

Availability Analysis Using Simulation. Edgar and Bendell [24] tested the robustness of Markov models in estimating mean-time-to-failure (MTTF), mean-time-torepair (MTTR), mean-time-to-first-failure (MTTFF), and availability for coherent systems of identical repairable components (up to 10) by use of simulation. Using Weibull distributions to define component failure and repair rates, the authors analyzed steadystate simulation versus Markov analytical results for both increasing failure rate (IFR) and decreasing failure rate (DFR) component failure and repair distributions. In general, the simulation steady-state and Markov model results were found to be consistent. The authors concluded that failure distributions (as opposed to repair distributions) were more critical in defining overall system behavior, and that decreasing failure rates were more critical than increasing failure rates [24:125].

System Complexity (or Size). Hwang, Tillman, and Lee [25] performed a literature review of works which evaluate reliability calculation methods for complex systems. Their definition of a complex system was one that could not be categorized as a series-parallel

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structure. They categorized these complex systems as either small (1 - 6 components), moderate (7 - 9 components), or large (10 or more components). The article provided diagrams of the chosen example complex systems for the study with some small, some moderate, and some large. They applied various methods defined in the literature to evaluate the reliability of each example complex system. Hwang, Tillman, and Lee's definitions of complexity/size were utilized in this research effort.

Constant Failure Rate Assumption. A common practice in reliability analysis is to assume that time between failure follows an exponential distribution (i.e. a constant failure rate). Mortin, Krolewski, and Cushing [26] provided examples where this assumption produced erroneous results. They concluded that indiscriminate use of this simplifying assumption can introduce significant error in the analysis [26:54].

Repair Distributions. Kline [27], through in-depth analysis of several systems, verified that the lognormal is a good distribution for describing repair rates. He also concluded that use of the exponential distribution for repair rates resulted in negligible error when the true underlying repair distribution was lognormal [27:79].

Comparison of Screening Designs for Simulation Models. Webb and Bauer [28], using a large-scale computer simulation, compared three methods of analysis for a Plackett-Burman screening design: the Box and Meyer approach, the traditional response surface methodology (RSM) approach, and the Hamanda and Wu approach. This thesis employed the RSM and Box-Meyer analysis methods.

Box-Meyer Bayesian Method. The Box-Meyer method entails deriving the marginal posterior probability that a factor is active (i.e. statistically significant) using

Bayesian techniques. This method determines which model best fits the data by examining

all possible hypotheses and is analogous to all-subsets regression [28:307]. Box and

Meyer explain their method as follows:

"The Bayesian approach to model identification is as follows. We consider the set of all possible models labeled $M_0, ..., M_m$. Each model M_i has an associated vector of parameters θ_i , so that the sampling distribution of data y, given the model M_i , is described by the probability density $f(y|M_i, \theta_i)$. The prior probability of the model M_i , is $p(M_i)$, and the prior probability density of θ_i is $f(\theta_i | M_i)$. The predictive density of y, given model M_i , is written $f(y|M_i)$, and is given by the expression

$$f(\mathbf{y}|\mathbf{M}_i) = \int_{R_i} f(\mathbf{y}|\mathbf{M}_i, \boldsymbol{\theta}_i) d\boldsymbol{\theta}_i$$

where R_i is the set of possible values of θ_i . The posterior probability of the model M_i , given the data y, is then

$$p(M_{i}|y) = \frac{p(M_{i})f(y|M_{i})}{\sum_{h=0}^{m} p(M_{h})f(y|M_{h})}.$$

The posterior probabilities $p(M_i | y)$ provide a basis for model identification. Tentatively plausible models are identified by their large posterior probability" [14:95].

Since it considers the possibility of interactions, the Box-Meyer method increases the

likelihood of identifying active factors. This is "particularly true of Plackett-Burman

designs where the number of runs is not a power of two" [14:94].

Response Surface Methodology (RSM). The RSM approach consists of

examining the magnitude of the main effects, using analysis of variance (ANOVA), and

examining normal probability and/or Pareto plots. A Pareto plot is a bar chart where the

length of the bars is proportional to the absolute value of the estimated effects [28:309].

Summary

A key objective of this research was to ascertain whether there is utility in focusing on 'important' components when characterizing input data for availability models. This chapter provided a detailed review of current methods for computing component importance. Additionally, a general overview of two-level screening designs as well as a thorough review of Plackett-Burman (P-B) designs was provided. A P-B screening experimental design was used in this thesis to determine which selected characterization factors were significant. Finally, pertinent literature which shaped the methodology for this effort was discussed.

Many factors contribute to the accuracy of availability models. In an effort to supplement the analyst interviews, the literature review helped identify input data characterization factor candidates for analysis: component importance, underlying component failure and repair distribution characteristics (IFR versus DFR), system structure type, and system complexity level (or size). The literature review also provided insight into appropriate factor levels for the two-level screening experiments and applicable analysis methods.

III. METHODOLOGY: PRELIMINARY EXPERIMENT

General Methodology Overview

The general methodology for this research entailed a designed screening experiment to identify significant input data characterization factors affecting availability estimate accuracy. The RSM and Box-Meyer methods discussed previously were used for analysis of the experimental output data. The research was done in two steps: a simplified preliminary experiment analyzing five factors to validate and refine the methodology, and a final experiment analyzing nine factors.

Component input data characterization factors of interest were identified using reliability analyst interviews, ideas derived from the literature review, as well as personal judgment. The nine factors identified for analysis are listed in Table 4.

Input Data Characterization Factors					
True Failure probability density function (pdf) of important					
components					
True Failure probability density function (pdf) of non-important					
components					
Number of data points					
(assumed to be same for all components)					
Fitting technique for Failure pdf of important components					
Fitting technique for Repair pdf of important components					
Fitting technique for Failure pdf of					
non-important components					
Fitting technique for Repair pdf of					
non-important components					
System Complexity Level (Size)					
System Structure Type					

Table 4.	Selected	Experimental	Factors
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For the conduct of the two-level screening experiments, two levels for each factor were selected, labeled high and low for simplicity. Availability models for various generic systems of components were created using a PC-based RM&A software program developed by the Headquarters Air Force Operational Test and Evaluation Center (HQ AFOTEC). Each system of components was designed by the researcher for complete experimental control and do not represent actual existing systems. In accordance with the experimental design, factors were set to the appropriate levels for each design point. The response measure for each simulation run was system availability absolute estimation error. Following the simulation runs, the responses were analyzed to screen the active factors via traditional RSM as well as Box-Meyer statistical analysis techniques.

Preliminary Experiment

To validate the general methodology and to expose potential problem areas, an initial smaller scale screening experiment was performed on a subset of the factors listed above. A 2_v^{5-1} factorial designed experiment was conducted to determine which of 5 input data characterization factors (for a simple series-parallel structure) might significantly affect availability model accuracy.

Definitions. The system considered in the preliminary experiment was a coherent system comprised of binary state components. As defined previously, a coherent system is one in which all components are relevant in maintaining a functional system. Binary state components have just two states: functioning or failed. The states are represented as

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X(t) = 1 if the component functions at time t and

X(t) = 0 if the component is failed at time t.

A system's (as opposed to component) reliability function is depicted as $h(\mathbf{p})$, where \mathbf{p}

represents the component reliability vector. System availability (A_o) is defined as the

percentage of time the system will perform its specified function (i.e. in operational

condition) in a given period of time [29:253].

Assumptions. The following assumptions were applied to the preliminary experiment:

(1) The structure is coherent consisting of binary state components.

(2) All component failure and repair distribution means are bounded by the following limits:

(a) Weibull failure distributions: 1000 < mean < 5000 (hours)

(b) Lognormal repair distributions: 10 < mean < 200 (hours).

(3) Only these specific distributions (Weibull and Lognormal) are used to represent the true component failure and repair distributions.

(4) All parallel components are identical.

(5) No negative location parameters are allowed in distribution data fitting.

(6) Distributional fitting results obtained for identical parallel components require only one set of input data sampled from one component.

(7) Maximum Likelihood Estimation (MLE) methods are used to calculate fitted distribution parameters.

(8) The response function, defined as the absolute error of the system availability measure from each simulation run, is approximately linear with respect to the input variables.

(9) Higher order interaction effects are negligible.

(10) The component with the highest ranking Barlow-Proschan time-independent importance measure represents the most important system component.

Software. The software used to create the availability simulation model is a PC-based program entitled Rapid Availability Prototyping Tool for Testing Operational Readiness (RAPTOR), written by the Headquarters Air Force Operational Test and Evaluation Center (HQ AFOTEC). RAPTOR can be used to create availability, reliability, maintainability, and sparing models for various systems undergoing operational testing and evaluation (OT&E). The program was written in MODSIM II, an object-oriented simulation language, and requires the user to graphically define the system Reliability Block Diagram (RBD). Component failure and repair rates are simulated over time to determine overall system R & M characteristics [30]. Weibull++ Version 4.0 was the software used to generate and fit component failure and repair data sets. Weibull++ Version 4.0 is a reliability software program created by ReliaSoft, Inc. which has robust data generation and fitting routines for common reliability distributions [31].

Design of Preliminary Experiment. The structure studied was a simple seriesparallel structure consisting of five components depicted in Figure 8.

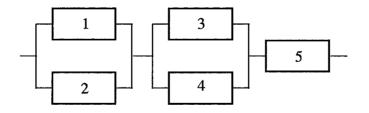


Figure 8. Experimental Structure for Preliminary Experiment

The experiment consisted of a 2_v^{5-1} factorial design (with three replicates) on the five component series-parallel system shown in Figure 8. Since this is a resolution V design, the main effects and two-factor effects can be estimated without aliasing with each other. However, two-factor

interactions are confounded with three-factor interactions [32:163]. The associated experimental

factors and levels are depicted in Table 5.

	Factors	Levels	
	Number of data points	50	+
A	(assumed to be same for all components)	10	-
	Fitting technique for Failure pdf of	Weibull++ Top MLE Ranking	+
B	important components	Weibull++ MLE: Exponential	-
	Fitting technique for Repair pdf of	Weibull++ Top MLE Ranking	+
C	important components	Empirical	-
	Fitting technique for Failure pdf of non-	Weibull++ Top MLE Ranking	+
D	important components	Weibull++ MLE: Exponential	-
	Fitting technique for Repair pdf of non-	Weibull++ Top MLE Ranking	+
E	important components	Empirical	-

Table 5. Experimental Factors and Levels for Preliminary Experiment

The Weibull++ Monte Carlo data generation module was used to generate simulated failure and repair times from the defined component distributions. The Weibull++ distribution wizard was used to fit theoretical distributions to the generated data set and to calculate distribution parameters using the maximum likelihood estimation (MLE) method. A 'forced-fit' exponential distribution was used for the low level for component failure data fitting due to the frequent use of the exponential assumption in component failure analysis. Separate data sets were generated and fitted for each of the three replications.

The defined system failure and repair distributions as well as the (replication 1) fitted distributions for each component are listed in Tables 6 and 7.

		10 Data	Points	50 Data	Points
Component	True Failure Distribution	Wizard Fit	Exponential Fit	Wizard Fit	Exponential Fit
	Weibull: (hrs)	Weibull:	Exponential:	Weibull:	Exponential:
	Shape $= 1.1$	Shape $= 1.142$	Mean = 3333	Shape = 1.304	Mean = 3333
1/2	Scale = 3500	Scale = 3677	Location = 0	Scale = 4018	Location $= 8.4$
	Location = 0	Location $= 0$		Location $= 0$	
	Weibull:	Normal:	Exponential:	Weibull:	Exponential:
	Shape $= 1.5$	Mean = 1284	Mean = 1250	Shape = 1.212	Mean = 1429
3/4	Scale = 2000	St Dev = 771	Location $= 14.2$	Scale = 1663	Location $= 136.4$
	Location = 0			Location $= 99.7$	
	Weibull:	Weibull:	Exponential:	Weibull:	Exponential:
	Shape $= 2.0$	Shape $= 1.872$	Mean = 1428	Shape $= 2.220$	Mean = 1429
5	Scale = 2000	Scale = 2014	Location $= 384.5$	Scale = 2155	Location $= 478.9$
	Location = 0	Location = 0		Location $= 0$	

 Table 6. System Failure True and Fitted Distributions (Replication 1)

Table 7. System Repair True and Fitted Distributions (Replication 1)

		10 Data P	oints	50 Data P	oints
Component	True Repair Distribution	Wizard Fit	Low Level Fit	Wizard Fit	Low Level Fit
1/2	Lognormal: Mean = 40 (hrs) St Dev = 10	Lognormal: Mean = 43.4 St Dev = 6.5	Empirical	Lognormal: Mean = 39.1 St Dev = 8.8	Empirical
3/4	Lognormal: Mean = 70 St Dev = 15	Weibull: Shape = 10.73 Scale = 65.2 Location = 0	Empirical	Lognormal: Mean = 70.6 St Dev = 16.5	Empirical
5	Lognormal: Mean = 60 St Dev = 8	Weibull: Shape = 1.582 Scale = 20.0 Location = 38.9	Empirical	Weibull: Shape = 2.744 Scale = 25.2 Location = 38.3	Empirical

Since components 1 and 2 as well as 3 and 4 were identical, the same data fit was used for each identical pair. Graphical examples of the results for failure and repair pdf data

fittings for component 5 are shown in Figures 9 and 10. The generated data sets for the preliminary experiment data fittings are available in Appendix C.

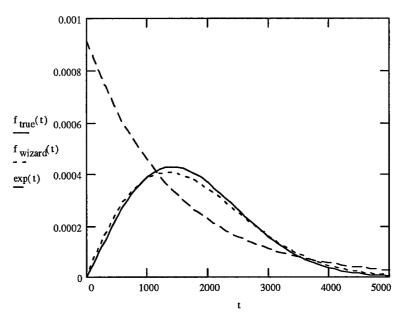


Figure 9. Component 5 True Failure pdf versus Weibull++ wizard and exponential fits (Replication 1 using 10 data points)

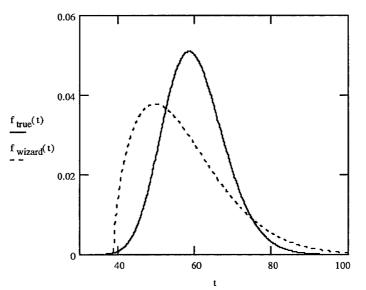


Figure 10. Component 5 True Repair pdf versus Weibull++ wizard fit (Replication 1 using 10 data points)

Simulation Runs. Run duration for each replication was 50,000 hours in simulated time. Three replications were conducted at each of the 2^4 design points, resulting in 48 total runs. The response variable was defined as the absolute error of the system availability measure from each simulation run. The value representing true availability ($A_0 = 96.6355$ %) used for calculation of absolute error was obtained by conducting 2000 runs using the defined component failure and repair distributions. Banks, Carson, and Nelson's [33:449] formula was used to calculate the initial estimate of the number of runs needed to obtain a 95% confidence limit and a ± .015% tolerance for the 'true' system availability measure:

$$R \ge \left(\frac{z_{\alpha/2}S_0}{\varepsilon}\right)^2 \tag{10}$$

where *R* is the estimated number of runs needed, S_0 is the standard deviation of the initial sample, and ε is the desired tolerance.

Since each run represents independent and identically distributed random variables, traditional statistical methods apply. One hundred initial runs of 50,000 hours duration were completed resulting in an S_0 for A_0 of .3168%. From equation (10), $R \ge 1713.56$. Therefore, 1714 or more runs were necessary to obtain a baseline availability measure which would meet the specified tolerance of \pm .015% at a 95% confidence level. A total of 2000 runs were completed which resulted in an average availability value (A_0) of 96.6355%. This point estimate of system availability for time 0 to 50,000 hours was the benchmark of comparison to calculate the absolute error of the system availability measure for each design point in the experiment. Components were rank-ordered by their Barlow-Proschan time-independent importance measure for 0 to 50,000 hours, where component 5 was deemed the most important component. Table 8 shows the calculated B-P importance measure values.

Component(s)	Calculated B-P Importance Measure
1, 2	.056671
3, 4	.145126
5	.596417

Table 8. Barlow-Proschan Time-Independent Importance Measure Values

Analysis Methods and Software. The analyzed multiple regression main-effects model can be described in the following format:

$$Y_{ij} = \beta_0 + \beta_1 X_1 + \beta_2 X_2 + \beta_3 X_3 + \beta_4 X_4 + \beta_5 X_5 + \varepsilon_{ij}$$
(11)

where

 Y_{ij} is the response value for run number *i* and replication *j*;

 β_0 represents the intercept (or response mean);

 β_k represents the regression coefficients for factors k = 1,...,5;

 X_k represents the factor level (either +1 or -1) for factor k; and

 ε_{ij} represents the residual error for run number *i* and replication *j*.

Yates algorithm [21:323-324] and least squares methods were used to calculate the main and interaction effects. The correlation coefficient (R^2), ANOVA, and lack of fit statistics were calculated to assess model adequacy. To identify significant factors, normal probability plots, Pareto plots, Box-Meyer Bayes plots, and linear regression coefficient t-test statistics were used. The primary analysis software was JMP version 3.1, a PC-based statistical analysis program developed by the SAS Institute. JMP possesses data graphing, experimental design, and statistical analysis routines [34:319-341] which proved very useful in this research.

IV. RESULTS: PRELIMINARY EXPERIMENT

Simulation Results

The 2_V^{5-1} experimental design and resulting responses for the preliminary experiment

are shown in Table 9.

	Factors				Obs	Observed Availability [*]			Absolute Error (Y)		
Design	A	B	C	D	E	Replication	Replication	Replication	Replication	Replication	Replication
Point						1	2	3	1	2	3
1	-1	-1	-1	-1	1	96.8046%	96.9903%	95.8230%	0.1691%	0.3548%	0.8125%
2	-1	-1	-1	1	-1	96.7202%	97.0266%	95.8372%	0.0847%	0.3911%	0.7983%
3	-1	-1	1	-1	-1	96.6918%	96.9858%	95.7640%	0.0563%	0.3503%	0.8715%
4	-1	-1	1	1	1	96.6324%	96.8985%	95.7639%	0.0031%	0.2630%	0.8716%
5	-1	1	-1	-1	-1	96.7904%	96.8941%	95.9042%	0.1549%	0.2586%	0.7313%
6	-1	1	-1	1	1	96.7261%	96.8518%	95.9385%	0.0906%	0.2163%	0.6970%
7	-1	1	1	-1	1	96.6137%	96.8172%	95.8354%	0.0218%	0.1817%	0.8001%
8	-1	1	1	1	-1	96.5398%	96.7937%	95.9377%	0.0957%	0.1582%	0.6978%
9	1	-1	-1	-1	-1	96.7274%	96.0124%	96.3905%	0.0919%	0.6231%	0.2450%
10	1	-1	-1	1	1	96.7276%	96.0496%	96.3695%	0.0921%	0.5859%	0.2660%
11	1	-1	1	-1	1	96.6290%	95.7957%	96.2251%	0.0065%	0.8398%	0.4104%
12	1	-1	1	1	-1	96.5982%	95.8427%	96.2454%	0.0373%	0.7928%	0.3901%
13	1	1	-1	-1	1	96.7642%	95.9374%	96.2951%	0.1287%	0.6981%	0.3404%
14	1	1	-1	1	-1	96.7929%	95.9976%	96.4092%	0.1574%	0.6379%	0.2263%
15	1	1	1	-1	-1	96.6571%	95.8386%	96.2923%	0.0216%	0.7969%	0.3432%
16	1	1	1	1	1	96.8079%	95.8528%	96.2844%	0.1724%	0.7827%	0.3511%

Table 9. Experimental Design and Responses

2000 Run 'Truth' Availability = 96.6355%

Note that all system availability estimates from each run were within \pm .88% of the defined

true system availability.

Statistical Analysis

A summary of the key model statistics is provided in Table 10.

Statistic	Value	Interpretation
		Model explains virtually
R ²	.004537	none of output variability
Whole Model F-test		Model as a whole
p-value	.9991	is not significant
Lack of Fit F-test		Linear model is appropriate
p-value	1.0	(no curvature)

Table 10. Preliminary Experiment Model Statistical Results

The model statistics show that the defined main-effects model explains very little of the response variation and that a linear model is appropriate for the experimental region. A summary of the calculated factor effects and statistics is shown in Table 11.

Factor	Effect Estimate	t-test p-value	Interpretation
Intercept	.37850%	<.0001	Significant (mean response)
. A	00386%	.9654	Not significant
В	02694%	.7624	Not significant
C	.01933%	.8282	Not significant
D	01871%	.8336	Not significant
E	.00598%	.9465	Not significant

Table 11. Estimated Effects and Statistical Analysis

The t-test for each effect estimate indicates that only the mean response (regression model intercept term) is significant. A supplemental listing of statistical analysis outputs for the preliminary experiment is provided in Appendix A.

Graphical Analysis

Figures 11, 12, and 13 show the normal probability, the Pareto, and the Box-Meyer Bayes plots.

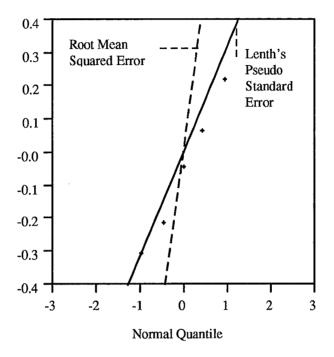


Figure 11. Normal Probability Plot

Term	Scaled Estimate	.2	2	.4	.6	.8
В	-0.0136113			\vdash		
С	0.00976686					
D	-0.0094553					$\sim \parallel$
Е	0.00302122					
A	-0.0019517					

Figure 12. Pareto Plot of Scaled Estimates

Term	Estimate	Prior	Posterior	.2	.4	.6	.8	٦
A	-0.0436317	0.2000	0.0244					
В	-0.304292	0.2000	0.0256					
С	0.21834656	0.2000	0.0250					
D	-0.2113806	0.2000	0.0250					
Е	0.06754200	0.2000	0.0245					

Figure 13. Box-Meyer Bayes Plot

The normal probability and Bayes plot results are consistent and indicate that no effects are significant. The Pareto plot indicates that factors B, C, and D explain the most variation, but since the amount of explained variation by the model is negligible this result has little significance.

Additional Analysis

Upon closer inspection of the absolute error responses shown in Table 9, it was discovered that a possible blocking effect may be present between replications. For example, notice (in Table 9) that the absolute errors in replication 1 are the smallest values in all cases. To address this, additional data analysis was conducted on models which included a blocking variable as well as other response measures: error and squared error. Table 12 contains a summary of the possible significant factors resulting from all analyses on the preliminary experimental data.

		Response					
Blocking Variable	Absolute Error	Error	Squared Error				
No	None	Possibly C	Possibly A & C				
Yes	None	None	A and possibly C				

 Table 12. Significant Factors Assessing Alternative

 Responses and a Blocking Variable

Statistical analysis showed that the blocking variable was strongly significant with all three response measures.

With the additional responses (error and squared error), factors A (number of data points) and C (fitting technique for repair pdf of important component: component 5), presented themselves as possible significant factors. However, these conclusions are not definitive and thus were addressed again in the final experiment.

Summary

The statistical analysis, using absolute error as a response measure, supports the hypothesis that there are no significant effects. With the absolute error response, no effects were shown to be significant in the t-tests, and the normal probability, Pareto, and Bayes plots revealed no clear significant factor effects. This means that using fewer data points (i.e. 10 versus 50) and less aggressive fitting techniques (i.e. exponential assumption for failure rates and use of empirical repair distributions) on important as well as non-important components did not significantly degrade model accuracy for this particular structure.

However, introducing a blocking variable in conjunction with two alternative responses, error and squared error, revealed that factors A and C *may* be significant. Therefore, the results from this experiment are inconclusive. Further analysis is required to determine conclusively if the number of data points (factor A) and the fitting technique for repair pdf of important component (factor C) are significant.

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V. METHODOLOGY: FINAL EXPERIMENT

Insights Gained from Preliminary Experiment

While the preliminary experiment assessed five input data characterization factors, the final experiment assessed nine factors listed in Table 4. Several insights were gained from the preliminary experiment which helped refine the methodology for the final experiment. After reviewing the methodology and results of the preliminary experiment, AFOTEC analysts recommended low and high levels of 5 and 25 for the 'number of data points' factor levels. They felt that levels of 10 and 50 data points were too generous based upon their experience in past operational availability analyses. They also pointed out that the mean-time-to-failure (MTTF) / mean-time-to-repair (MRT) ratios were relatively large for all five components of the experimental structure, and that a wider range of ratios may be more appropriate for future experimental designs. It was also pointed out that frequently the analyst will not have a priori knowledge of component failure behavior. This information is normally required for the calculation of component importance measures, with the exception of structural importance measures. An additional suggestion was to analyze the variability of several availability model outputs for individual runs. This was addressed in a separate study conducted using multivariate techniques on several RAPTOR model output measures. A summary of the study is provided in Appendix G. Finally, it was discovered that a significant amount of time and effort was required to setup the experimental runs, which included component failure and repair data point generation and fitting, construction of RAPTOR models, and completion of 'truth' data

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runs. Since the required effort would increase dramatically with the addition of 4 more factors, any subsequent experimental screening design would need to economize on the number of simulation runs.

Final Experiment

Assumptions. To produce diversity in the MTTF/MRT ratios for the system components, wider bounds were allowed for the means of the component failure and repair distributions. They were bounded by the following limits:

(1) Weibull failure distributions: 1000 < mean < 6500 (hours)

(2) Lognormal repair distributions: 50 < mean < 3000 (hours).

The most important components in a structure were deemed as the ones which fell in the top 20% of component importance measure rankings based upon component failure distributions. To allow for the calculation of the importance measures without knowledge of the underlying failure distributions, the Birnbaum structural importance measure was used. This measure is based solely upon system structure. All other assumptions outlined in the preliminary experiment also applied to the final experiment.

Structures. 20 components were designed which were used for the building of system structures for the RAPTOR models. Each component was designed to have true Weibull failure and lognormal repair distributions randomly set within the established bounds for the distribution means. Increasing failure rate (IFR) and decreasing failure rate (DFR) configurations were created for each component while maintaining the same distribution mean. To accomplish this, randomly selected Weibull shape and scale parameters were

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utilized to create the IFR failure distributions. Using a randomly generated DFR shape parameter for each component, the same *average* failure rate was maintained by adjusting the Weibull scale parameter to achieve an identical mean failure rate as in the IFR configuration. This procedure was used to ensure that the results were not biased by producing a different average failure rate when reconfiguring a component from IFR to DFR. The shape parameters ranged from 1.1 to 4.0 for IFR configurations and from .4 to .95 for DFR configurations. A complete listing of component failure and repair distribution parameters (for both configurations) is shown in Appendix B.

Four basic structures were created from the set of 20 components described above: a small/series-parallel structure, a small/complex structure, a large/series-parallel structure, and a large/complex structure. The small structures used components 1 through 5, while the large structures were comprised of all 20 components. Appendix B provides reliability block diagrams for each structure.

Design of Final Experiment. The factors and levels for the final experiment are shown in Table 13. Since each run demanded a large set-up effort, a design which minimized the number of runs was preferable. Replications were still desired to increase the confidence in the results and to estimate pure error for lack of fit testing. A full factorial experiment would require 1536 runs (i.e. 512 * 3 replications), and a 2_{III}^{9-5} fractional factorial design would require 48 runs (i.e. 16 * 3 replications). A Plackett-Burman (P-B) design was chosen because it required only 36 (i.e. 12 * 3 replications) total simulation runs to assess the nine factors.

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	Factors	Levels	
A	True Failure probability density function (pdf) of	Weibull IFR	+
	important components	Weibull DFR	-
В	True Failure probability density function (pdf) of	Weibull IFR	+
	non-important components	Weibull DFR	-
C	Number of data points	25	+
	(assumed to be same for all components)	5	-
D	Fitting technique for Failure pdf of important	Weibull++ Top MLE Ranking	+
	components	Weibull++ MLE: Exponential	-
E	Fitting technique for Repair pdf of important	Weibull++ Top MLE Ranking	+
	components	Empirical	-
F	Fitting technique for Failure pdf of	Weibull++ Top MLE Ranking	+
	non-important components	Weibull++ MLE: Exponential	-
G	Fitting technique for Repair pdf of	Weibull++ Top MLE Ranking	+
	non-important components	Empirical	-
H	System Complexity Level (Size)	Large (20 components)	+
		Small (5 components)	-
Ι	System Structure Type	Series-Parallel	+
		Complex	-

The 12-run 9-factor P-B design used for the final experiment is shown in Table 14.

Design					Factors				
Point	Α	B	<u> </u>	D	E	F	G	H	Ι
1	+	+	+	+	+	+	+	+	+
2	-	+	-	+	+	+	-	-	-
3	-	1	+	-	+	+	+	-	-
4	+	-	-	+	-	+	+	+	-
5	-	+	-	-	+	-	+	+	+
6	-	-	+	-	-	+	-	+	+
7	-	-	-	+	-	-	+	-	+
8	+	-	-	-	+	-	-	+	-
9	+	+	-	-	-	+	-		+
10	+	+	+	-	-	-	+	-	-
11	-	+	+	+	-	-	-	+	-
12	+	-	+	+	+	_	-	-	+

Table 14. 12-run Plackett-Burman Design for Final Experiment

Distributional Fittings. As in the preliminary experiment, Weibull++ was used to generate and fit the component failure and repair data sets for each configuration. Separate generations and fits were conducted for each replication. Components 14, 15, and 16 as well as 18, 19, and 20 were identical components, therefore only one generation and fitting was conducted for each triplicate set per replication. Final experiment fitting data is contained in Appendix D and graphical examples for the fitted distributions for some of the components are provided in Appendix E.

Important Components. A complete listing of the Birnbaum structural component importance measures calculated for each component in each of the four experimental structures is provided in Appendix F, with a summary provided in Table 15.

Structure	Top 20% Important Components
Small / Series-Parallel	Component 3
Small / Complex	Component 1
Large / Series-Parallel	Components 4, 5, 13, 17
Large / Complex	Components 1, 4, 7, 8

Table 15. Top 20% Important Components

Simulation Runs. 16 truth runs were required due to the four additional factors. For each of the four structures, 'truth' runs were done with the following configurations:

(1) All components with IFR failure distributions

(2) All components with DFR failure distributions

(3) Important components with IFR failure distributions and non-important components with DFR failure distributions

(4) Important components with DFR failure distributions and non-important components with IFR failure distributions.

As before, each simulation run duration was for 50,000 hours simulation time. Two thousand replications were run to establish 'truth' availability values for each configuration. For the P-B experimental runs, the response measure was again the absolute error of the system availability measure from each simulation run as compared to the 'truth' measure.

Analysis Methods. The analysis methods were identical to those used for the preliminary experiment. Traditional statistical measures were used to assess model adequacy, and normal probability plots, Pareto plots, Bayes plots, and linear regression coefficient t-test statistics were used to identify the significant factor effects. A response surface was formed to graphically portray the combined affect of the active factors on model availability estimation error.

VI. RESULTS: FINAL EXPERIMENT

Simulation Results

The results from the truth and Plackett-Burman experimental RAPTOR runs for the

final experiment are shown in Table 16.

Design	Structure	Component Failure PDF	Truth	Obser	ved Avail	ahility	Abso	olute Erro	or (Y)
Point	on actare	Important / Non-important	Runs			Replication 3			
1	Large / S-P	IFR / IFR	83.1373%	81.0810%	78.166%	82.5297%	2.0563%	4.9713%	0.6076%
2	Small / Complex	IFR / DFR	77.3638%	81.2591%	78.2235%	80.9242%	3.8953%	0.8597%	3.5604%
3	Small / Complex	DFR / DFR	76.4428%	77.3795%	79.5758%	74.8265%	0.9367%	3.1330%	1.6163%
4	Large / Complex	DFR / IFR	60.4257%	38.6057%	61.4589%	55.8074%	21.820%	1.0332%	4.6183%
5	Large / S-P	IFR / DFR	82.7799%	80.6977%	77.8648%	71.5604%	2.0822%	4.9151%	11.219%
6	Large / S-P	DFR / DFR	81.6366%	82.0842%	76.8906%	82.4661%	0.4476%	4.7460%	0.8295%
7	Small / S-P	DFR / DFR	64.6009%	63.2109%	65.2901%	55.2021%	1.3900%	0.6892%	9.3988%
8	Large / Complex	DFR / IFR	60.4257%	41.0340%	61.8580%	54.8932%	19.391%	1.4323%	5.5325%
9	Small / S-P	IFR / IFR	65.9448%	64.6130%	65.4925%	64.7097%	1.3318%	0.4523%	1.2351%
10	Small / Complex	IFR / IFR	78.2001%	76.4971%	80.2750%	78.4965%	1.7030%	2.0749%	0.2964%
11	Large / Complex	IFR / DFR	60.7345%	60.7147%	56.1168%	60.1398%	0.0198%	4.6177%	0.5947%
12	Small / S-P	DFR / IFR	65.0705%	63.5087%	65.8172%	65.2438%	1.5618%	0.7467%	0.1733%

Table 16. Numerical Results for Final Experimental Runs

A much larger variability in the response was observed compared to the preliminary experiment. The observed absolute errors in availability estimates ranged from .0198% to 21.82%.

Statistical Analysis

A summary of the key model statistics is provided in Table 17.

Statistic	Value	Interpretation
		Model explains one-third
R ²	.333092	of output variability
Whole Model F-test		Model as a whole
p-value	.2241	is not significant
Lack of Fit F-test		Linear model is appropriate
p-value	.9680	(no curvature)

Table 17.	Final Experiment Model Statistical Result	lts
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The model statistics show that the defined main-effects model explains approximately onethird of the response variation and that a linear model is appropriate for the experimental region. A summary of the calculated factor effects and statistics is shown in Table 18.

	Effect	t-test	
Factor	Estimate	p-value	Interpretation
Intercept	3.4997%	.0001	Significant (mean response)
A	.89372%	.5688	Not significant
В	-1.8335%	.2471	Not significant
С	-3.5403%	.0306	Significant
D	04232%	.9784	Not significant
E	.63297%	.6861	Not significant
F	53829%	.7310	Not significant
G	1.2852%	.4142	Not significant
H	3.1045%	.0555	Significant
Ι	-1.5712%	.3197	Not significant

Table 18. Estimated Effects and Statistical Analysis

The mean absolute error of availability estimates for all the P-B simulation runs is 3.4997%. The t-test for each effect estimate indicates that the mean response (regression model intercept term), factor C (number of data points) effect, and

factor H (system complexity/size) effect are significant. A supplemental listing of statistical analysis outputs for the final experiment is provided in Appendix A.

Graphical Analysis

Figures 14, 15, and 16 show the normal probability, the Pareto, and the Box-Meyer Bayes plots.

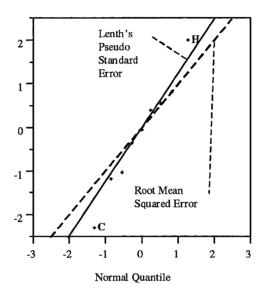


Figure 14. Normal Probability Plot

Term	Scaled Estimate	.2 .4 .6 .8
С	-1.7952429	
н	1.5742576	
В	-0.9297767	
Ι	-0.7967495	
G	0.6517153	
А	0.4531999	
Е	0.3209727	
F	-0.2729623	
D	-0.0214613	

Figure 15. Pareto Plot of Scaled Estimates

Term	Estimate	Prior	Posterior	.2 .4 .6 .8
A	0.5770951	0.2000	0.0284	
В	-1.1839578	0.2000	0.0467	
С	-2.2860239	0.2000	0.2430	
D	-0.0273283	0.2000	0.0244	
Е	0.4087198	0.2000	0.0263	
F	-0.3475843	0.2000	0.0258	
G	0.8298804	0.2000	0.0335	
н	2.0046260	0.2000	0.1524	
I	-1.0145637	0.2000	0.0393	

Figure 16. Box-Meyer Bayes Plot

The normal probability, Pareto, and Bayes plot results are consistent and suggest that factor C (number of data points) and factor H (system complexity/size) are significant, while all other factors are not significant.

Significant Effect Model

A subsequent regression model containing only factors C, H, and their interaction term was analyzed to determine if the C*H interaction term was significant. The results are shown in Table 19.

Factor	Effect Estimate	t-test p-value	Interpretation
Intercept	3.4997%	<.0001	Significant (mean response)
С	-3.5403%	.019	Significant
Н	3.1045%	.0379	Significant
C*H	-2.365766	.1086	Not significant
Statistic	Value		Interpretation
			Model explains approximately
\mathbf{R}^2	R ² .296981		one-third of output variability
Whole Model			Model as a whole
F-test p-value	F-test p-value .0095		is significant

Table 19. Estimated Effects and Statistical Analysis for C, H, C*H Model

In this case, the model explained approximately 30% of the response variability, and the model as a whole was significant. As before, the main effects for factors C and H were significant. The C*H interaction effect was not significant at a 10% level of significance.

Response Surface

A response surface was developed for the resulting C and H main-effects model:

$$Y = 3.4997 - 1.770133C + 1.5522389H$$
(12)

where Y is the estimated absolute error in the availability estimate; and

C and H represent the factor level (either +1 or -1) for each factor. The resulting response surface and contour plot are shown in Figure 17.

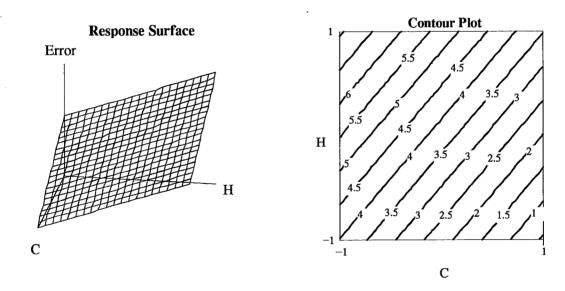


Figure 17. Two-Factor Model Response Surface and Contour Plot

As the plots in Figure 17 demonstrate, a high level for factor C (number of data points) and a low level for factor H (system size) result in the smallest availability estimation error.

Additional Analysis

As with the preliminary experiment, subsequent analysis was performed using error and squared error as response measures as well as introducing a blocking variable for the replications. In all cases, the blocking variable was insignificant. Furthermore, the results in all cases were consistent with those achieved using absolute error as the response, showing factors C and H as significant.

Summary

The statistical analysis tests and the normal probability, Pareto, and Bayes plots support the hypothesis that factors C and H are significant. Subsequent analysis indicates that the C*H interaction effect is not significant. The blocking effect between replications was insignificant, and using error and squared error as response variables resulted in identical conclusions to those achieved using the absolute error response. Analysis of the resulting two-factor model reveals that availability error is reduced when operating at a high level for factor C (number of data points) and a low level for factor H (system size).

VII. SUMMARY AND CONCLUSIONS

Research Objectives

The general purpose of this study was to provide insight into the input data

characterization factors which may affect the accuracy of availability model output. The

potential benefits of identifying the key factors would be the reduction of unproductive

data collection and more efficient RM&A modeling.

. The overall research objectives were to:

(1) Identify potential factors which affect availability model output accuracy.

(2) Screen the potential factors to determine which have a statistically significant effect (or interaction effect) on output accuracy.

(3) Assess the magnitude of the significant effects.

(4) Provide basic insights to aid in efficient component input data characterization for availability models.

Overview of Results

Component input data characterization factors thought to possibly affect system availability estimates were identified and analyzed. Using a design of experiment approach with the absolute error of system availability estimates serving as the response, a twostage experimental screening process was conducted to identify the active factors.

Preliminary Experiment. The results from the preliminary experiment were inconclusive, identifying number of data points and fitting method for the important components as possible significant factors. Using absolute error as the response, all

factors proved insignificant. The average system availability estimate absolute error was .3785%.

Final Experiment. The final experiment, analyzing four basic structures, revealed that system size (5-component versus 20-component) and the number of data points (5 versus 25) *do* affect estimate accuracy. It also showed that fitting technique, underlying component failure distribution (IFR versus DFR), and system structure type (series-parallel versus complex) *do not* have a significant effect. The interaction effect between the two active factors was not statistically significant. Using error and squared error as response variables resulted in the same conclusions achieved using the absolute error response. The average system availability estimate absolute error was 3.4997%, and the effect estimates were -3.504% for the 'number of data points' factor and 3.1045% for the 'system size' factor. The response surface from the two-factor model derived from the final experiment showed that estimation error is minimized when the number of data points is at a high level and the system size is small.

Multivariate Analysis. The supplemental multivariate analysis of RAPTOR output (Appendix G) revealed that multivariate techniques can be used to discriminate between various structures based on model outputs. It was also discovered that structures with predominantly DFR components produce higher variability in RAPTOR output measures than structures with predominantly IFR components.

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Conclusions

Several insights were gained from this research:

(1) More availability estimation error is to be expected when analyzing larger system structures;

(2) Availability estimation error can be reduced by increasing the number of failure and repair data points collected for each system component;

(3) There is no measurable significant difference in estimation error when analyzing systems with IFR component failure characteristics versus systems with DFR component failure characteristics;

(4) There is no apparent benefit in focusing on 'important' versus 'non-important' components when characterizing component failure and repair probability distributions;

(5) There is no apparent difference in estimation error when analyzing series-parallel structures versus complex structures; and

(6) No single fitting technique utilized in this research provided any distinct advantage over any other method for availability estimate error reduction.

To summarize, the availability measure appears to be robust to fitting method, component

failure characteristics, and system structure type, and sensitive to the number of data

points used in data fitting and the system size.

Comparison with Past Research Results

Sensitivity to Component Failure Rate Characterization. In analyzing a large space system, Wolf found very little sensitivity of the predicted system availability to individual component failure rate estimates [23:69]. The preliminary experimental results showed that the number of data points *may* affect availability estimation accuracy. The final experiment showed conclusively that the number of data points used in the

characterization of component failure and repair behavior *can* have a statistically significant affect on availability estimation accuracy.

Edgar and Bendell concluded that failure distributions were more critical than repair distributions in defining overall system behavior and that decreasing failure rates (DFR) were more critical than increasing failure rates (IFR) [24:125]. This study revealed that, at least when measuring system availability estimation error, the fitting fidelity of the failure and repair distributions and the underlying component failure rate (IFR versus DFR) were not significant. System availability appears to be a highly robust system characteristic and may be less sensitive than other system characteristics to changes in certain factors. The multivariate study showed that DFR component structures have higher output variability than IFR component structures.

Exponential Assumption. Mortin, Krolewski, and Cushing provided examples where the indiscriminate use of the exponential distribution for component failure characterization can produce erroneous results [26:54]. In this study, the use of the exponential distribution for component failure characterization (when the true underlying failure distribution was Weibull) did not significantly alter system availability estimation accuracy. Again, this may indicate that the availability measure is robust to component distributional assumptions.

Suggestions for Further Research

Identifying Other Factors. The final regression model (using the absolute error response) explained only a portion of the overall response measure variability with an R^2

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of .297, suggesting that other significant explanatory variables may exist. More formal methods could be conducted to identify other possible critical input data characterization factors not addressed in this study, such as a formal survey of several Air Force reliability analysts. A screening design could then be accomplished to identify other significant factors.

Mean-Time-to-Failure / Mean-Repair-Time (MTTF/MRT) Ratio. After reviewing the results of the preliminary experiment, AFOTEC analysts felt one important factor to analyze would be the component MTTF/MRT ratio. They suspected that system availability estimates might be more sensitive to some of the factors analyzed in this study when several components possessed a low MTTF/MRT ratio. Time did not allow for the inclusion of the MTTF/MRT factor in this study; in fact, it was randomized in the experimental design to mitigate ('spread around') its effect. Follow-on experiments which incorporate this factor may be insightful.

Response Surface Methodology (RSM). This research addressed qualitative as well as quantitative factors. In all cases, the qualitative factors proved insignificant. However, two quantitative factors (number of data points and system size) were significant. A simple linear response surface was developed for the resultant two-factor model for the defined experimental region. The factor levels used for the experiment (number of data points: 5 and 25; system size: 5 components and 20 components) represents a limited experimental region. Using RSM, the experimental region could be expanded and explored in more detail.

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Appendix A: Statistical Analysis Output

Preliminary Experiment: JMP Output (Without Blocking Variable)

		Screening F ABS Error Summary of	•		
	RSquare			0.004537	
	RSquare Ad	li		-0.11397	
	-	Square Error		0.30666	
	Mean of Rea			0.378498	
		s (or Sum Wg	ts)	48	
			~~)		
		Analysis of Var			
Source	DF	Sum of S		Mean Square	F Ratio
Model	5	0.0	180009	0.003600	0.0383
Error	42	3.9	496998	0.094040	Prob>F
C Total	47	3.9	677006		0.9991
		Look of Ti			
Source	D	Lack of Fi	f Squares	Mean Square	F Ratio
Lack of Fit	1).0758773	0.007588	0.0627
			3.8738225		Prob>F
Pure Error	3			0.121057	
Total Error	4	2 3	3.9496998		1.0000
Max RSq					
0.0237					
	F	Parameter Esti	mates		
Term		Estimate	Std Erro	r t Ratio	Prob>jtj
Intercer	ot	0.3784979	0.044263	3 8.55	<.0001
A		-0.001931	0.044263	3 -0.04	0.9654
В		-0.013469	0.044263	3 -0.30	0.7624
С		0.0096646	0.04426	3 0.22	0.8282
D		-0.009356			0.8336
Е		0.0029896			0.9465
0	N1	Effect Tes		F D -44-	Durk C
Source	Nparm		n of Squares	F Ratio	Prob>F
A	1	1	0.00017903	0.0019	0.9654
B	1	1	0.00870755	0.0926	0.7624
С	1	1	0.00448340	0.0477	0.8282
D	1	1	0.00420189	0.0447	0.8336
E	1	1	0.00042901	0.0046	0.9465
		Error			
		Summary of	f Fit		
	RSquare	-		0.057138	
	RSquare A	dj		-0.05511	
		Square Error		0.427632	
	Mean of Re	-		0.237094	
		ns (or Sum Wg	gts)	48	
		· · · ·			

Source Model Error C Total	An DF 5 42 47	7.68 8.14	quares N 554480 805195 459675	Mean Square 0.093090 0.182870	F Ratio 0.5090 Prob>F 0.7678
Source Lack of Fit Pure Error Total Error Max RSq 0.0614	DF 10 32 42	0 7	Squares .0345872 .6459323 .6805195	Mean Square 0.003459 0.238935	F Ratio 0.0145 Prob>F 1.0000
Term Intercep A B C D E		rameter Estin Estimate 0.2370937 0.0841313 -0.000431 0.0507771 -0.003435 0.0053354	Std Error 0.061723 0.061723 0.061723 0.061723 0.061723 0.061723	3.84 1.36 -0.01 0.82 -0.06	Prob> t 0.0004 0.1801 0.9945 0.4154 0.9559 0.9315
Source A B C D E	Nparm [1 1 1 1 1	1 1 1 1	t of Squares 0.33974723 0.00000893 0.12375899 0.00056650 0.00136640	F Ratio 1.8579 0.0000 0.6768 0.0031 0.0075	Prob>F 0.1801 0.9945 0.4154 0.9559 0.9315
Source	RSquare RSquare Adj Root Mean S Mean of Res Observations An DF	ponse	ts) iance	0.020457 -0.09616 0.274629 0.225921 48 Mean Square	
Model Error C Total	5 42 47	0.0 3.1 3.2	661547 676947 338494	0.013231 0.075421	0.1754 Prob>F 0.9703
Source Lack of Fit Pure Error Total Error Max RSq 0.0374	DF 10 32 42	() ()	t f Squares).0548711 3.1128236 3.1676947	Mean Square 0.005487 0.097276	0.0564

		Paramet	ter Estima	ates		
Term		Es	timate	Std Error	t Ratio	Prob> t
Intercep	t	0.22	259211	0.039639	5.70	<.0001
Α		-0.	.01106	0.039639	-0.28	0.7816
В		-0.0	18303	0.039639	-0.46	0.6466
С		0.02	275692	0.039639	0.70	0.4906
D		-0.0)11699	0.039639	-0.30	0.7693
Е		0.00)48954	0.039639	0.12	0.9023
		Eff	ect Test			
Source	Nparm	DF	Sum	of Squares	F Ratio	Prob>F
Α	1	1	0	.00587120	0.0778	0.7816
В	1	1	0	.01608043	0.2132	0.6466
С	1	1	0	.03648302	0.4837	0.4906
D	1	1	0	.00656969	0.0871	0.7693
Е	1	1	0	.00115031	0.0153	0.9023

Preliminary Experiment: JMP Output (With Blocking Variable)

Screening Fit ABS Error Summary of Fit

Continuary of the	
RSquare	0.526943
RSquare Adj	0.444158
Root Mean Square Error	0.216619
Mean of Response	0.378498
Observations (or Sum Wgts)	48

	An	alysis of Variance		
Source	DF	Sum of Squares	Mean Square	F Ratio
Model	7	2.0907506	0.298679	6.3652
Error	40	1.8769500	0.046924	Prob>F
C Total	47	3.9677006		<.0001

	Parameter Estima	tes		
Term	Estimate	Std Error	t Ratio	Prob> t
Intercept	0.3784979	0.031266	12.11	<.0001
Α	-0.001931	0.031266	-0.06	0.9511
В	-0.013469	0.031266	-0.43	0.6689
С	0.0096646	0.031266	0.31	0.7588
D	-0.009356	0.031266	-0.30	0.7663
E	0.0029896	0.031266	0.10	0.9243
Block[1-3]	-0.291992	0.044217	-6.60	<.0001
Block[2-3]	0.1172021	0.044217	2.65	0.0115

		Effect	Test				
Source	Nparm			Squares	F Ratio	Prob>F	
A	1	1		0001790	0.0038	0.9511	
В	1	1		0087075	0.1856	0.6689	
Ċ	1	1		0044834	0.0955	0.7588	
D	1	1		0042019	0.0895	0.7663	
E	1	1		0004290	0.0091	0.9243	
Block	2	2		0727498	22.0864	<.0001	
DIOCK	2	L	2.	0121490	22.0004	<.0001	
		Erro					
	DØ	Summar	y of Fit		0.40.4000		
	RSquare			0.434239			
	RSquare A	-			0.335231		
		n Square Eri	ror		0.339436		
	Mean of R				0.237094		
	Observatio	ons (or Sum	Wgts)		48		
		Analysis of	Varian	ce			
Source	DF		of Squ		Mean Square	F Ratio	
Model	7		3.5372		0.505328	4.3859	
Error	40)	4.6086	5707	0.115217	Prob>F	
C Total	47	1	8.1459	675		0.0011	
		_	_				
T		Parameter			. D. H		
Term		Estin		Std Err		Prob> t	
Intercep)t	0.2370		0.0489		<.0001	
A		0.0841		0.0489		0.0937	
B		-0.000		0.0489		0.9930	
С		0.0507		0.0489		0.3062	
D		-0.003		0.0489		0.9444	
E	A 7	0.0053		0.0489		0.9138	
Block[1	-	-0.30		0.0692		<.0001	
Block[2	-3]	-0.013	3144	0.0692	87 -0.19	0.8505	
		Effect	Test				
Source	Nparm	DF		Squares	F Ratio	Prob>F	
А	1	1		.3397472	2.9488	0.0937	
В	1	1	0	.0000089	0.0001	0.9930	
С	1	1	0	.1237590	1.0741	0.3062	
D	1	1	0	.0005665		0.9444	
Е	1	1	0	.0013664	0.0119	0.9138	
Block	2	2	3	.0718488	13.3307	<.0001	
		00.5	-				
		SQ E Summai					
	RSquare				0.373498		
	RSquare A	Adj			0.26386		
		n Square Er	ror		0.225056		
	Mean of F	-	_		0.225921		
		ons (or Sum	Wgts)		48		

	A	Analysis	s of Varian	ce		
Source	DF	S	um of Squ	iares l	Mean Square	F Ratio
Model	7		1.207	8352	0.172548	3.4066
Error	40		2.026	0142	0.050650	Prob>F
C Total	47		3.233	8494		0.0060
	F	arame	ter Estima	tes		
Term		E	stimate	Std Erro	or t Ratio	Prob> t
Intercept		0.2	259211	0.03248	4 6.95	<.0001
Α		-().01106	0.03248	4 -0.34	0.7353
В		-0.	018303	0.03248	4 -0.56	0.5763
С		0.0	275692	0.03248	4 0.85	0.4011
D		-0.	011699	0.03248	4 -0.36	0.7206
Е		0.0	048954	0.03248	4 0.15	0.8810
Block[1-3]	-0.	215254	0.04593	9 -4.69	<.0001
Block[2-3]	0.0	771839	0.04593	9 1.68	0.1007
		Ef	lect Test			
Source	Nparm	DF	Sum o	f Squares	F Ratio	Prob>F
Α	1	1	C).0058712	0.1159	0.7353
В	1	1	().0160804	0.3175	0.5763
С	1	1	().0364830	0.7203	0.4011
D	1	1	().0065697	0.1297	0.7206
E	$\frac{1}{2}$	1	().0011503	0.0227	0.8810
Block	2	2	1	1.1416805	11.2702	0.0001

Final Experiment - Full Main Effect Model: JMP Output (Without Blocking Variable)

		Screening Fit Abs Error summary of Fit		
	RSquare		0.333092	
	RSquare Adj		0.102239	
	Root Mean Squ	uare Error	4.645971	
	Mean of Respo		3.499722	
	Observations (or Sum Wgts)			
	Ana	lysis of Variance		
Source	DF	Sum of Squares	Mean Square	F Ratio
Model	9	280.30078	31.1445	1.4429
Error	26	561.21112	21.5850	Prob>F
C Total	35	841.51190		0.2214
		Lack of Fit		
Source	DF	Sum of Squares	Mean Square	F Ratio
Lack of Fit	2	1.51785	0.7589	0.0325
Pure Error	24	559.69327	23.3206	Prob>F
Total Error Max RSq 0.3349	26	561.21112		0.9680

		Parameter Es	timates		
Tei		Estimate		or t Ratio	Prob> t
Inte	ercept	3.499722			0.0001
Α	-	0.446861	1 0.77432	28 0.58	0.5688
В		-0.91677			0.2471
С		-1.77013	3 0.77432	-2.29	0.0306
D		-0.02116			0.9784
Е		0.316483			0.6861
F		-0.26914			0.7310
G		0.642			0.4142
Н		1.552238			0.0555
Ι		-0.78560			0.3197
		Effect Te	aet		
Source	Nparm		um of Squares	F Ratio	Prob>F
A	1	1	7.18865		0.5688
В	1	1	30.25697		0.2471
Ĉ	1	1	112.80139		0.0306
D	1	1	0.01612		0.9784
Ē	1	1	3.60582		0.6861
F	1	1	2.60779		0.7310
G	1	1	14.86565		0.4142
Н	1	1	86.74004		0.0555
Ι	1	1	22.21834		0.3197
		Error			
		Summary	of Fit		
	RSquare	,		0.36423	37
	RSquare A	Adi		0.14416	
		n Square Error	r	5.13435	
	Mean of R			2.382	
		ons (or Sum W	/gts)		36
		Analysis of V	arianco		
Source	e DF	Sum o	f Squares	Mean Square	F Ratio
Model			392.6757	43.6306	1.6551
Error	26		685.4020	26.3616	Prob>F
C Tota			078.0777		0.1515
		Lack of	Fit		
Source			of Squares	Mean Squa	re F Ratio
Lack of		2	7.62238	3.811	
Pure Err		24	677.77964	28.240	
Total Er		26	685.40201	20.210	0.8744
Max RSc					
0.3713					

	P	arameter Estin	nates		
Term	-	Estimate	Std Error	t Ratio	Prob> t
Intercep	ot	2.3826	0.855726	2.78	0.0099
Α		0.9243389	0.855726	1.08	0.2900
В		-0.987061	0.855726	-1.15	0.2592
С		-1.6128	0.855726	-1.88	0.0707
D		-0.121572	0.855726	-0.14	0.8881
Ε		-0.203883	0.855726	-0.24	0.8135
F		-0.784844	0.855726	-0.92	0.3675
G		0.8526778	0.855726		0.3282
Н		2.2535167	0.855726	2.63	0.0140
Ι		0.0108167	0.855726		0.9900
		Effect Test			
Source	Nparm		of Squares	F Ratio	Prob>F
Α	. 1	1	30.75849	1.1668	0.2900
В	1	1	35.07443	1.3305	0.2592
С	1	1	93.64046	3.5522	0.0707
D	1	1	0.53207	0.0202	0.8881
Е	1	1	1.49646	0.0568	0.8135
F	1	1	22.17531	0.8412	0.3675
G	1	1	26.17414	0.9929	0.3282
Н	1	1	182.82015	6.9351	0.0140
Ι	1	1.	0.00421	0.0002	0.9900
		SQ Error			
		Summary of	Fit		
	RSquare			0.295785	
	RSquare Ac			0.052019	
		Square Error		97.38942	
	Mean of Re			35.62339	
	Observation	ns (or Sum Wg	ts)	36)
		Analysis of Var			
Source	DF	Sum of S		Mean Square	F Ratio
Model	9		8578.18	11508.7	1.2134
Error	26		5602.20	9484.7	Prob>F
C Total	35	350)180.38		0.3290
-		Lack of Fit			
Source			f Squares	Mean Square	
Lack of Fit		2	922.26	461.1	
Pure Error			45679.94	10236.7	
Total Error Max RSq	2	6 2	46602.20		0.9560
0.2984					

	Parame	ter Estim	nates		
Term	E	stimate	Std Error	t Ratio	Prob> t
Intercept	35.	523386	16.23157	2.19	0.0373
Α	17.	173384	16.23157	1.06	0.2998
В	-22	2.02642	16.23157	-1.36	0.1864
С	-30	.17743	16.23157	-1.86	0.0744
D	1.7	020264	16.23157	0.10	0.9173
Ε	-0.	217741	16.23157	-0.01	0.9894
F	-2.	477217	16.23157	-0.15	0.8799
G	8.4	618496	16.23157	0.52	0.6066
Н	27.	486565	16.23157	1.69	0.1023
Ι	-18	8.71392	16.23157	-1.15	0.2594
	Ef	fect Test			
Source Nparm			of Squares	F Ratio	Prob>F
A 1		Oum	10617.304	1.1194	0.2998
B 1			17465.871	1.8415	0.1864
C 1			32784.393	3.4566	0.0744
D 1			104.288	0.0110	0.9173
E 1			1.707	0.0002	0.9894
F 1			220.918	0.0233	0.8799
G 1			2577.704	0.2718	0.6066
H 1			27198.406	2.8676	0.1023
I I			12607.593	1.3293	0.2594

Final Experiment - Full Main Effect Model: JMP Output (With Blocking Variable)

C Total

35

Screening Fit Abs Error Summary of Fit RSquare 0.369889 RSquare Adj 0.081088 Root Mean Square Error 4.70038 Mean of Response 3.499722 Observations (or Sum Wgts) 36 Analysis of Variance Sum of Squares DF Source Mean Square F Ratio 311.26611 28.2969 Model 11 1.2808 Error 24 530.24579 22.0936 Prob>F

841.51190

0.2931

		Parame	ter Estim	ates		
Term			stimate	Std Error	t Ratio	Prob> t
Intercep	t	3.4	997222	0.783397		0.0002
A			468611	0.783397		0.5737
В		-0.	916772	0.783397		0.2534
С		-1.	770133	0.783397		0.0332
D		-0.	021161	0.783397	-0.03	0.9787
Е		0.3	164833	0.783397	0.40	0.6898
F		-0.	269144	0.783397		0.7342
G			0.6426	0.783397	0.82	0.4201
Н		1.5	522389	0.783397	1.98	0.0591
Ι		-0.	785606	0.783397	-1.00	0.3260
Block[1	-3]	1.2	199611	1.10789	1.10	0.2817
Block[2	-3]	-1.	027106	1.10789	-0.93	0.3631
•			ect Test			
Source	Nparm	DF	Sum	of Squares	F Ratio	Prob>F
A	1	1		7.18865	0.3254	0.5737
B	1	1		30.25697	1.3695	0.2534
C	1	1		112.80139	5.1056	0.0332
D	1	1		0.01612	0.0007	0.9787
E F	1	1		3.60582	0.1632	0.6898
г G	1 1	1		2.60779	0.1180	0.7342
G H	1	1 1	•	14.86565	0.6728	0.4201
н I	1	1		86.74004 22.21834	3.9260 1.0056	0.0591
Block	1	2		30.96533		0.3260
BIOCK	Z	Z		30.90333	0.7008	0.5061
			Error			
		Sum	mary of F	=it		
	RSquare				0.415505	
	RSquare	Adj			0.147612	
	Root Me		Error		5.124008	
	Mean of I	Response	:		2.3826	
	Observat	ions (or S	Sum Wgts	s)	36	
Source	n		s of Varia		Moon Sauero	E Datia
Source Model			Sum of So	quares 1 7.9467	Mean Square 40.7224	F Ratio 1.5510
		.1				
Error C Total		4 5		0.1310 8.0777	26.2555	Prob>F
	2	0	10/6	0.0///		0.1778

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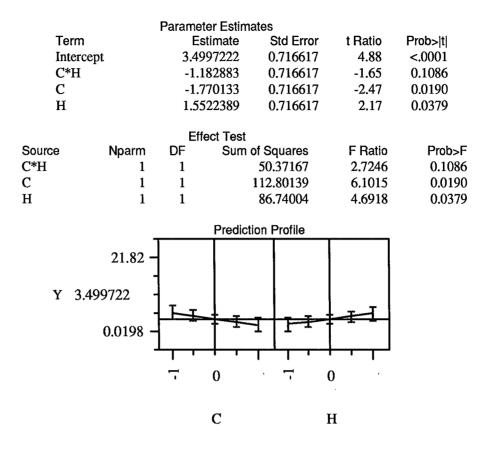
		Paramet	ter Estima	otae		
Term			stimate	Std Error	· t Ratio	Prob> t
Intercep	t		2.3826	0.854001		0.0102
A	•	0.9	243389	0.854001		0.2898
В			987061	0.854001		0.2591
Ċ			-1.6128	0.854001		0.0711
D			121572	0.854001		0.8880
Е			203883	0.854001		0.8133
F			784844	0.854001		0.3672
G			526778	0.854001		0.3280
н			535167	0.854001		0.0144
Ι			108167	0.854001		0.9900
Block[1	-31		1.45715	1.20774		0.2394
Block[2			571483	1.20774		0.2056
	- ,					
			ect Test			
Source	Nparm	DF	Sum	of Squares	F Ratio	Prob>F
Α	1	1		30.75849	1.1715	0.2898
В	1	1		35.07443	1.3359	0.2591
С	1	1		93.64046	3.5665	0.0711
D	1	1		0.53207	0.0203	0.8880
E	1	1		1.49646	0.0570	0.8133
F	1	1		22.17531	0.8446	0.3672
G	1	1		26.17414	0.9969	0.3280
H	1	1		182.82015	6.9631	0.0144
Ι	1	1		0.00421	0.0002	0.9900
Block	2	2		55.27102	1.0526	0.3646
			Q Error			
			mary of F	it		
	RSquare	Gann			0.374379	
	RSquare .	Adi			0.087636	
	Root Mea		Error		95.54236	
	Mean of I				35.62339	
	Observati			;)	36	
		•	Ũ			
			s of Varia			
Source	D		Sum of So		Mean Square	F Ratio
Model	1	-		100.15	11918.2	1.3056
Error	2)80.23	9128.3	Prob>F
C Total	3	5	3501	180.38		0.2802

		Param	eter Estin	nates		
Term		I	Estimate	Std Error	t Ratio	Prob> t
Intercep	t	35	6.623386	15.92373	2.24	0.0348
Α		17	173384	15.92373	1.08	0.2915
В		-2	2.02642	15.92373	-1.38	0.1793
С		-3	30.17743	15.92373	-1.90	0.0702
D		1.	7020264	15.92373	0.11	0.9158
E		-().217741	15.92373	-0.01	0.9892
F		-2	2.477217	15.92373	-0.16	0.8777
G		8.	4618496	15.92373	0.53	0.6000
Η		27	486565	15.92373	1.73	0.0972
I		-1	8.71392	15.92373	-1.18	0.2514
Block[1	-3]	- 38	3.210871	22.51955	1.70	0.1027
Block[2	-3]		-26.2954	22.51955	-1.17	0.2544
		E	ffect Test			
Source	Nparm	DF		of Squares	F Ratio	Prob>F
A	1	1	Oum	10617.304	1.1631	0.2915
В	1	1		17465.871	1.9134	0.1793
Ĉ	1	1		32784.393	3.5915	0.0702
D	1	1		104.288	0.0114	0.9158
E	1	1		1.707	0.0002	0.9892
F	1	1		220.918	0.0242	0.8777
G	1	1		2577.704	0.2824	0.6000
Н	1	1		27198.406	2.9796	0.0972
I	1	1		12607.593	1.3811	0.2514
Block	2	2		27521.966	1.5075	0.2417

Final Experiment - C, H, C*H Model: JMP Output

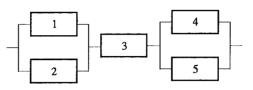
Response Variable: Absolute Error

		Screening Fit Y		
	ŝ	Summary of Fit		
	RSquare		0.296981	
	RSquare Adj		0.231073	
	Root Mean Sq	uare Error	4.299705	
	Mean of Resp	onse	3.499722	
	Observations	(or Sum Wgts)	36	
	An	alysis of Variance		
Source	DF	Sum of Squares	Mean Square	F Ratio
Model	3	249.91310	83.3044	4.5060
Error	32	591.59880	18.4875	Prob>F
C Total	35	841.51190		0.0095

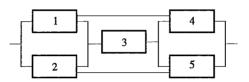


Appendix B: Final Experiment Structures and True Component Distribution Functions

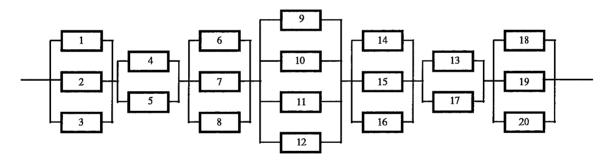
Small / Series-Parallel:



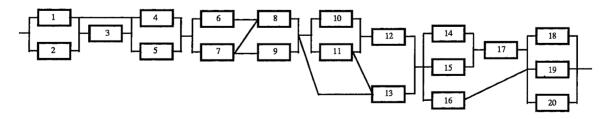
Small / Complex (Bridge Structure):



Large / Series-Parallel:



Large / Complex:



Component	IFR Failure Distribution	DFR	Repair
		Failure Distribution	Distribution
1	Weibull: Shape = 1.5 (hrs)	Weibull: Shape = .50 (hrs)	Lognormal: (hrs)
	Scale = 3000	Scale = 1354	Mean = 2800
1	Location = 0	Location = 0	S.D. = 200
	Weibull: Shape = 4.0	Weibull: Shape = $.85$	Lognormal:
2	Scale = 2500	Scale = 2082	Mean = 1500
	Location = 0	Location = 0	S.D. = 100
	Weibull: Shape = 2.5	Weibull: Shape = .95	Lognormal:
3	Scale = 4000	Scale = 3468	Mean = 1000
	Location = 0	Location = 0	S.D. = 150
_	Weibull: Shape $= 1.7$	Weibull: Shape = .60	Lognormal:
4	Scale = 1700	Scale = 1008	Mean = 150
	Location = 0	Location = 0	S.D. = 25
	Weibull: Shape $= 2.8$	Weibull: Shape $= .40$	Lognormal:
5	Scale = 3500	Scale = 938	Mean = 850
	Location = 0	Location = 0	S.D. = 90
	Weibull: Shape $= 1.9$	Weibull: Shape = .70	Lognormal:
6	Scale = 3333	Scale = 2336	Mean = 3000
	Location = 0	Location = 0	S.D. = 125
	Weibull: Shape = 1.2	Weibull: Shape = .55	Lognormal:
7	Scale = 2575	Scale = 1423	Mean = 190
	Location = 0	Location = 0	S.D. = 20
	Weibull: Shape $= 2.7$	Weibull: Shape = .78	Lognormal:
8	Scale = 1500	Scale = 1156	Mean = 1200
	Location $= 0$	Location = 0	S.D. = 75
	Weibull: Shape = 1.6	Weibull: Shape = $.91$	Lognormal:
9	Scale = 6000	Scale = 5143	Mean = 1000
	Location $= 0$	Location = 0	S.D. = 30
	Weibull: Shape = 2.3	Weibull: Shape = $.46$	Lognormal:
10	Scale = 4700	Scale = 1763	Mean = 2300
	Location = 0	Location = 0	S.D. = 133
	Weibull: Shape $= 1.4$	Weibull: Shape = .82	Lognormal:
11	Scale = 2700	Scale = 2210	Mean = 500
	Location $= 0$	Location = 0	S.D. = 60
	Weibull: Shape = 1.9	Weibull: Shape $= .67$	Lognormal:
12	Scale = 2700	Scale = 1812	Mean = 1000
	Location $= 0$	Location = 0	S.D. = 100
	Weibull: Shape = 1.3	Weibull: Shape = .86	Lognormal:
13	Scale = 4200	Scale = 3591	Mean = 90
	Location = 0	Location = 0	S.D. = 15
	Weibull: Shape = 1.5	Weibull: Shape = .62	Lognormal:
14/15/16	Scale = 2600	Scale = 1626	Mean = 2200
	Location = 0	Location = 0	S.D. = 200
	Weibull: Shape = 1.1	Weibull: Shape = .75	Lognormal:
17	Scale = 3100	Scale = 2513	Mean = 750
	Location $= 0$	Location = 0	S.D. = 60
	Weibull: Shape = 1.6	Weibull: Shape = .48	Lognormal:
18/19/20	Scale = 2000	Scale = 829	Mean = 280
	Location = 0	Location = 0	S.D. = 50

Component True Failure and Repair Distributions (Final Experiment)

Appendix C: Fitting Data (Preliminary Experiment) Components 1 and 2:

		;						:	:		(
Failure PD	F			(Top Wei	bull++ Se	ection)			(Weibull++	Exponenti	al)
0 Data Po						arameters			Low Level	Fitting Para	meters
Set1	Set2	Set3			Rep2	Rep3			Rep1		Rep3
3400.223	290.2722	189.0183	Shape	1.1424	0.8048			Lambda	0.0003		0.0004
	5161.413	and a second	fereterstanstations analysisters			2763.633		mean		3333.333	2500
		416.6079	Location	0	161.866	0		Location	0	0	145.6065
	4305.172										
	935.8477 3462.054										
*******	1673.137										
	634.8128						·····	*****	*************		
1954.587	245.1001	3211.058	•••••			•••••					
2521.536	11798.13	210.6919									
••••••											
-ailure PD					bull++ Se				(Weibull+1	- Exponenti	al)
50 Data Po						arameters			Low Level	Fitting Para	imeters
	Set2	Set3		Rep1		Rep3					Rep3
		925.3368 2083.236	Snape	1.3037	1.0481	1.2134 2914.042		Lambda	0.0003		0.0004
		2083.236 5474.835				••••••••		mean Location	3333.333 8.3745		*
	2271.222		LUCALION	<u> </u>		<u> </u>		LUCATION	0.3743	v	0,0070
		1261.039									•
		6648.759				••••••				}	
		5350.916									
	Concernation of the second	6206.759								[
*************		1753.056					******	*****			
		910.5857							RAMETERS	5	
		778.6821 5657.847						Weibull			
1802.004		1970.843						Shape Scale			
		2468.072	*****************		*******			Location		Annes an annes annes	
	A	1525.289					******	LUCATION	*************		
	8001.486										
2052.169	4769.927	298.2684					·····				*·····
		2800.817									
	المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع	2004.737									
2252.016		5362.177				ļ					
2295.502		5859.77 3807.239					••••••				
2342.247		245.7073									
	5324.474			••••••			÷				÷
**************************************	der occurrences and	1682,965									
• • • • • • • • • • • • • • • • • • • •		4229.763					••••••			·····	
3210.884	1952.818	1186.952									
3330.358		4641.868		<u>.</u>							
		242.8431									
3465.598		1407.097			ļ	.					
; <i></i>	2608.717	4102.534 8.5878		¦	<u> </u>			.			÷
		6416.082				<u>.</u>				+	
	1590.474	******									
	3452.596										
3977.555	4376	274.9632	(*************************************	******		*****			******	**********	
		1755.551	[1]					1
		202.5712	£								
		6 7054.521									
		4707.271	والمراجع والمحاصر والمحاصر والمحاصر والمحاص والمحاص والمحاص والمحاص والمحاص والمحاص والمحاص والمحاص والمحاص وال								
		3 747.6762 1450.601		<u> </u>	÷		÷				÷
		1450.601	*	•		••••••			+	÷	•
		4390,494		÷	÷		÷	••••••			•
	**************	1637.359		1	1	•			÷		•
		4152.95	An and a second second second							*****	
		3508.264		1	1	1		1	1	1	1
9717.0	7 1407.548	5992.359	1	[]	1			1		1
12809.3	5 3493.224	1 2000.326			1			1	[1
40704 0	1: 1000 000	3 2782.958	di	1	1	1		1	1	1	

		1									True Lognormal St Dev.	10
epair PD	F	[(Top Weib	ull++ Selec	tion)		(Empirical	,)		True Lognormal Variance:	100
Data P	oints			High Level	Fitting Par	ameters		Low Level	Fitting Para	meters		
et1	Set2	Set3		Rep1	Rep2	Rep3			Rep2	Rep3		
33.9979											Mean for Normal variates:	3.658567143
39.4116				0.147				(Empirical)		Var for Normal variates:	0.060624622
39.6336						1					St Dev for Normal Variates:	0.246220677
40.3567		31.9426		6.499295	8.4235	0						
43.0280					<u>.</u>							
43.6418			Weibull Shape			0.9565						
45.1152						11.9569						
46.1252						26.9208						
47.0883												
61.5145	53.8807	64.5566							.			
Janaia DD	<u>.</u>			ATTAC MARK	i Muri Calas			·····				
Repair PD 0 Data P		.		Uigh Lough	ull++ Selec	amotom		(Empirical				
	Set2	Set3		Rept	Fitting Par Rep2	Rep3		Rep1	Fitting Par Rep2	Rep3		
24.1991		18.0659	N Mean			3.6131		пері	inehs	neho	*****	
24.6871		23.8515				0.2944		(Empirical	<u>.</u>			•••••
27.6193		24.0047				38.72308		(Empirica)	<i></i>			
28.0627		24.3652		8.772902		11.65161	•••••	•••••	÷			•••••
28,9823							******				*************************************	
29,1609			Weibull Shape		3.0977							••••••
29.7943		26.7887			24.5055							
30,1743		27.0129			17.1612							
30,3590		27.1011				******	*******		*****			
30,9141	32.9141	27.8885							1			
31,3476	33.7304	29.5760);		÷				<u>.</u>			
31.6416	33.9327	29.8710)							************************	***************************************	
32.0434	34.5756	30.3222				1		•••••	1	1		
33.6861	34.654	31.8326	5			1			1	1		
34.1794						1			1			
34.2628		33.4084	l <u>i</u>									
34.2756						1			1			
34.4363		33.6211			<u>}</u>]			
36.0875												
36.1988												
36.4695						Ļ				.		
37.8517						Ļ				.		
38.0252 38.2895												
38.2895		36.5698										
38.4396				·•••••••••••••••••••••••••••••••••••••	· · · · · · · · · · · · · · · · · · ·							
38.4502		2: 36.9805		÷			******					
38.6779					•••••••••••••	÷			• • • • • • • • • • • • • • • • • • • •	÷		••••••
38,7602		9 38,7156			· <u>;</u> ·····	••••••			+	<u>.</u>		<u>.</u>
38,768		39.587		· · · · · · · · · · · · · · · · · · ·	·	<u>†</u>	1	•••••	·•••••••	<u>†</u>		<u> </u>
39.5696									1		***************************************	
40.1211					•••••••••••••••••	1	1		1	1		
40.676		4 40.308			·····	1	<u>†</u>		1	1		1
40.8159	9 41.519	2 40.362	4				1	[1	1		1
41.1818		0 41.296						[1	1		1
41.4396						1				1]
42.5334						1				1		
42.8620		7 44.0890										
43.059												
44.332	3 45.901	0 45 500	3				Į					
44.5534		6 46.413										
47.210		0 47 353										Į
47.378		4 49.997										.
48.673		3 50.080						.				↓
49.198		8 51.553					ļ					
49.492		0 54.819				. !		.				
57.248		2 55.666					÷	ļ			÷	
63,185 63,398		0 55.829										
63.398 63.408		1 61.395		•								.
	0, 37,305	5: 104.607	C 1	:	1	1	:	4	1	•	:	÷

	Componen	nts 3	and	4:
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				Co	omponen	ts 3 and 4	4:				
Componen	3 and 4	Failure Dat	a								
Failure PD	-			(Top Weibu	III++ Select	ion)			(Weibull++	Exponentia	ul)
10 Data Po				High Level						Fitting Para	
Set 1	Set2	Set3				Rep3				Rep2	Rep3
1419.354			Shape		1.842	1.701		Lambda	0.0008		0.0006
963.0771			Scale		1808.529	2257.799		Mean	1250		1666.667
14.1518			Location		317.4287	43.7521		Location	14.1518		
544.4623		5230.137	Location		017.42.07	40.7 02 1		Location	14.1010	004.0020	
382.2532		1682.83	Normal								
2046.543		1131.662	Mean	1284.115							
1318.988		2304.446	S.D.	771.0283							
2070.357											
1539.051											├─── ┨
2542.909	1025.499	459.4963								i	
	-			(T 141 1		• • • •	· · · · · · · ·		(144 - 2 11	l	
Failure PD				(Top Weib						Exponentia	
50 Data Po		0.10		High Level			1			Fitting Para	
Set1	Set2	Set3		Rep1	Rep2	Rep3		1	Rep1	Rep2	Rep3
136.4218		1696.307	Shape		2.0219	1.6765		Lambda	0.0007		0.0005
171.3912			Scale					Mean	1428.571		2000
224.7112			Location	99.6879	0	0		Location	136.4218	0	0
277.1905		1805.908								L	L
345.4204	809.518		<u> </u>								
350.7182						ļ	L				
389.1629										L	ļ]
479.4368											
500.3845		4878.578							RAMETERS	3	
527.7269								Weibull			
533.4867								Shape			
545.9969	385.2486	1467.667						Scale	2000	<u>ا</u>	
586.504	1605.537	1540.711						Location	0	1	
634.7171	3350.027	649.1847	1								
641.1439	4166.519	1783.356								1	
814.9092	2043.477	80.483									
817.0835	1839.547	4346.261									
817.7518	1992.607	2434.073	5								
1013.223		701.3264	ŀ								
1023.585	1415.027	1327.958	3				1				
1041.254	3404.917	695.0499)								
1119.601	2785.675	4072.324	L								
1162.011	1613.91	641.4696	6				1				
1323.632	1456.764	3960.691	1								
1356.765	403.8959	1580.863	3								
1452.204	2513.195	1864.181	Î								
1517.397	1049.062	2072.33	3								
1610.408	1199.236	1395.664	1								
1650.178	2189.122	1179.098	3								
1747.276	894.8619	616.6241	1								
1783.921	712.8388	2660.072	2			1					
1787.338	2992.213	2868.949	3								
1910.095	851.2721	589.046	δ								
2061.335					1	1	1	_			
2073.654			2								
2149.89				1	1	1	1				
2202.220								1		1	
2661.079					1	1	1	1	1		
2663.375				1	1	1	1	1	1	1	1
2824.27	-			1		1	1.	1	1	1	1
2938.45			-		+	1		1	1	1	1
3044.94				1	1	1	1		1	1	1
3108.324				1			1		1	1	1
3111.95							1				1
3218.4					1		1	+	+	1	1
3297.17				1	1		1	+	1		-
3818.06					+	1	+	1	+		
3881.40				-						-	+
4296.42				+		1				+	+
4296.42	_				-	+	+	1	+		+
2200.91	3 2086.617	7 465.453	9		1			1	<u> </u>		

Component and 4 Repair PS True Logermit Moort Tr	Componen	t 9 and 4	Repair Dat				·····					True Lognormal Mean:	70
Repart PDT CPC gr Wabulk - Statucon CPC and Points CPC and Points <thcpc and="" points<="" th=""> CPC and Points CP</thcpc>	Componen	to ano 4	1 (0 μαι) - Ο αί	a.									
10 Data Perints Imple Law Prime Parameters Imple Law Prime Parameters Imple Parameters Imple Parameters 60 X80 60 700 85.4810 N Mean 4280478 Poil Page Parameters Poil Page Parameters Poil Statements Auzenters	Repair PD				(Top Weib	ull++ Select	ion)		Empirical				
SA11 Sa12 Sa12 Sa12 Sa12 Mean Pep1 Pep2 Pep3 Mean for Normal variates 4.22047982 54.435 64.503 68.5271 N S.D. 0.1668 (Empirica) Variantics 4.22047982 54.435 64.501 68.101 N S.D. 0.16958 (Empirica) Variantics 4.22047982 54.545 64.501 69.146718 0.146718											meters		
55.528 50.176 58.4619 N Man 4.288			Set3									1	
54.881 64.0371 69.9191 LogN 8.D. O 1 StDev for Normal Variates 9.211985157 66.2466 70.2684 20.045 72.1974 </td <td>50.5429</td> <td></td> <td>58.4619</td> <td>N Mean</td> <td></td> <td></td> <td>· 1</td> <td></td> <td>•</td> <td></td> <td></td> <td>Mean for Normal variates:</td> <td>4.226047582</td>	50.5429		58.4619	N Mean			· 1		•			Mean for Normal variates:	4.226047582
61.5746 67.603 70.1883 LogN S.D. 0 14.7192 0 0 63.417 70.9544 83.858 Webuld Steps 10.7254 2.0011 0 0 63.8161 80.1768 85.046 91.770 Location 0 51.8268 0 0 69.8275 89.768 10.0555 0 13.801 0	54.5919	59.9039	63.5271			0.1966		(Empirical			Var for Normal variates:	0.04489532
IE22485 72245 72174 Image: constraint of the second se				LogN Mean	1	73.90835	1					St Dev for Normal Variates:	0.211885157
63.411 70.9324 63.9383 Wahudi Shape 10.7284 2.0011				LogN S.D.	0	14.67192	0						
ESSIENT ESSIENT Source Sourc			72.1974										
68.8356 82.1574 88.4354 Location 0 51.6926 72.5666 89.763 11.00655 Phopair PDF (1op Welbull++ Selector) (Emplicia) S0 101 Size Size High Lawal Filting Parameters (Emplicia) S0 1177 82.713 41.6444 N Man 70.60029 Rep2 Rep2 Rep3 S0 1177 82.717 82.711 10.6644 N Man 70.60029 Rep2 Rep3													
e9.2073 93.646 91.770 Image: solution of the solutio													
1728866 97.7683 110.0655 (Top Weibul++ Selection) (Empirica) Papar PDF Set Rep1 Rep2 Rep3 Rep1 Rep2 Rep3 Rep1 Rep3 SAt1 7871 85 731 41 6494 N Moan 42204 A2206 42206 Rep1 Rep3 Rep3 Rep1 Rep3 Rep3 443827 46.0511 432107 N Moan 42204 A2206 42206 (Empirica) Rep3 Rep3 Rep3 Rep3 443827 46.0511 432107 N Moan 42204 A2206 42206 (Empirica) Rep3 Rep3 Rep3 Rep3 Rep3 Rep3 Rep3 Rep3				Location	0		51.6926						
Paper PD (Top Webul+ Solecton) (Empirea) (Empirea) 50 Data Points High Lave Fitting Parameters Low Lovel Fitting Parameters Low Lovel Fitting Parameters 34 (177) 38.7913 41.6944 N Mean 42304 42206 Rep2 Rep3		93.0343			······								
5D Data Points High Lave Fitting Parameters Low Lovel Fitting Parameters 341 T Sti2 Str3 Rep1 Rep2 Rep2 Rep3 Rep4 Rep2 Rep3 Rep3 Rep4 Rep3	12.0300	35.1003	110.0000										
5D Data Points High Lave Fitting Parameters Low Lovel Fitting Parameters 341 T Sti2 Str3 Rep1 Rep2 Rep2 Rep3 Rep4 Rep2 Rep3 Rep3 Rep4 Rep3	Repair PD	F			(Top Weib	ult++ Selec	tion)		Empirical	L			
Sett Sett Neg1 Rep2 Rep2 Rep3 Rep3 44.3827 46.0611 42.2507 N S.D. 0.2306 42.206 (Empirical)											meters		
34.177 38.7913 41.6444 N Mean 42266 42266 (Empirical) 44.3827 45.5753 43.441 LogN Mean 70.6029 69.82744 70.5276 (Empirical) (Set3										
48.3827 46.0611 43.2507 N S.D. 0.200 0.1961 0.206 (Empirical) 49.477 55.753 43.441 1000029 69.2447 70.527.6 (Empirical) 55.3446 45.3284 55.042 47.1282 (Empirical) (Empirical) 55.444 57.0586 49.7386 (Empirical) (Empirical) (Empirical) 55.4412 57.0586 49.7386 (Empirical) (Empirical) (Empirical) 56.4412 57.0586 49.7486 (Empirical) (Empirical) (Empirical) 56.7045 55.7316 (Empirical) (Empirical) (Empirical) (Empirical) (Empirical) 56.7045 52.510 (Empirical) (Empirical) (Empirical) (Empirical) (Empirical) (Empirical) 57.375 57.5143 (Empirical) (Empi	34.1787		41.6494		4.2304	4.2268	4.2206	- 1	•				
49 9477 53 753 43.4841 LogN Maan 70.6029 69.82748 70.5276	48.3627	46.0611	43.2507	N S.D.	0.2308	0.1961	0.266	(Empirical)			
543642 55.0642 47.1625 544712 57.0686 49.748 545729 57.5047 49.7418 55729 57.6721 51.2158 56700 58.4367 52.530 56703 55.2043			43.4841	LogN Mean									
54.412 57.0986 49.7386 54.5729 57.5047 49.7416				LogN S.D.	16.51397	13.82587	19.09664						
9542729 57.5047 49.7418													
562162 57 6721 51 2158 567004 58 2534 54 6639 578385 58 4637 52 5341 578385 58 69447 54 7453 58 00539 61 3312 57 6677 51 112 62 0346 61 3115 61 1615 60 0356 61 4112 61 1615 60 0366 61 4112 62 0276 62 2415 61 1224 62 0278 62 2415 61 1224 62 0278 62 2070 61 7865 63 3113 63 0202 62 0276 63 3497 63 3424 64 3024 63 3497 63 3444 64 3024 64 3753 66 0072 65 3554 66 34097 63 3544 64 3024 67 5707 67 1334 67 4439 67 5707 67 1334 67 444 63 3410 69 3426 64 3755 66 0222 69 37515 69 3742 69 3755 69 3744 64 3753 66 35706 69 3782 69 37515 70 1056 69 3784 69 3847													
587:004 58.4367 52.5310					ļ					ļ			
56 9790 59 2594 54 6539 57 3835 59 0447 54 7453 58 0444 61 12913 56 0434 58 13425 75 167 9 61 1619 61 1619 61 1619 61 1619 61 1619 61 1619 61 5556 62 5615 61 2346 62 0807 62 39467 61 3936 62 0807 61 3936 9 63 3917 63 2020 61 26261 63 3917 63 2020 62 2647 63 3913 63 2020 62 2647 63 3913 63 2020 62 2647 63 3913 63 2947 63 2947 64 2657 63 3949 9 65 3444 63 3944 9 67 5707 67 1534 67 4949 68 3410 67 4049 9 69 2928 69 3715 9 70 1066 69 3947 9 70 2066 69 3947 9 70 2066 69 3947 9 70 2067 71 515 9 68 5706 69 37615 9<										<u> </u>			
57.3835 69.9447 54.7453 58.8944 12913 56.0434 50.0395 61.3342 57.1667 61.1619 61.15150 60.0750 61.1619 61.15150 60.0750 61.4112 62.0365 61.4124 62.0726 62.2040 61.8934 62.0887 62.2040 61.8934 62.0887 62.2040 61.8934 63.9313 63.0202 22.6219 63.4937 63.2022 22.6219 63.4937 63.2924 63.4711 64.4837 63.3924 64.3033 64.4975.31 66.072 65.3555 65.4449 67.0754 67.4449 67.5707 67.777 69.74499 68.5924 65.5944 65.5944 69.2828 69.4435 64.511 68.2928 69.4435 64.511 69.2928 69.3947 69.3947 69.3928 70.2969 70.711 70.1066 69.3942 70.296 71.11 71.117 71.117 <												-	
58.844 61 2913 56.0434													
59.0969 61.342 57.1667 61.1619 61.8150 60.0750 61.4112 62.3685 60.3466 61.8558 62.5415 61.1224 62.0867 62.9070 61.9786 62.0867 62.9070 61.9786 63.3613 63.2020 62.6218 63.3613 63.2020 62.6218 63.3633 63.2020 62.6218 63.4644 63.3633 60.072 64.4537 63.3242 64.3083 64.4537 63.3424 64.3633 64.4537 63.3554 65.4449 67.1534 67.5707 67.1534 67.5707 65.4741 68.5022 64.491 69.3706 69.7826 69.7491 69.3706 69.7826 69.7400 69.3706 69.7826 69.7400 69.3706 69.7826 69.7400 69.3706 69.7826 69.7240 70.0766 69.3984 70.2290 70.2826 70.079													
61.1619 61.8150 60.0750 61.8112 62.3686 60.3466 62.0756 62.9040 61.9786 62.0767 62.9070 61.9786 63.3937 63.0202 62.6219 63.3937 63.22976 63.3467 63.3937 63.22976 63.3046 63.3937 63.22976 63.3044 64.3753 66.6072 65.3554 64.3753 66.6072 65.3554 67.7507 67.1534 67.4849 68.3410 67.3088 67.9115 68.3620 69.4443 68.4511 69.5706 69.7515 69.7515 70.0106 69.8726 69.7515 70.0238 70.1420 70.7711 70.2328 71.1318 70.2230 71.5717 72.644 73.9264 70.5268 72.733 73.2540 70.711 70.3422 71.1318 70.2239 71.544 74.5592 75.554 72.643 73.9264 75.5547 72.644 63.7740													
61.4112 62.3685 60.3466													
62.0726 62.9070 61.8934 <td></td>													
62.0867 62.9070 61.9786	61.8558	62.5415	61.1234										
63.3931 63.0202 62.26219 63.4997 63.2976 63.4711 63.7644 63.3624 64.3033 64.2637 63.3544 64.3633 64.2637 63.3544 64.3633 65.8449 66.072 65.3554 65.8449 67.0459 65.5944 67.5707 67.1534 67.4849 67.5707 67.3584 67.4849 68.3410 67.3088 67.9115 68.3400 69.4403 68.4511 69.5706 69.8782 69.7515 700106 69.3842 70.2200 701711 70.3492 71.1318 702268 72.633 73.2540 71.6717 73.2624 1 75.8844 74.592 1 75.8845 77.8967 73.8524 75.8845 1 1 76.8853 77.8967 73.8524 76.8868 1 1 81.9052 1 1 76.8868 1 1 81.9827 78.5688 1													
63.3497 63.2776 63.4711													
63.7444 63.3544 64.3034													
64.2637 63.3544 64.3633													
64.9753 66.072 65.5944 65.8449 67.0459 65.5944 67.5707 77.1534 67.4849 68.3410 67.3008 67.9115 68.5082 69.4443 68.4511 69.228 69.4603 68.740 69.228 69.4643 68.740 69.228 69.4643 68.740 70.0106 69.9784 70.2289 70.0708 69.9784 70.2289 70.0708 70.4140 70.0711 70.3492 71.1318 71.6171 70.3492 71.1318 71.6171 70.3492 71.318 71.6171 70.3492 71.3592 75.8544 74.8592 75.8544 76.8653 77.966 73.2624 76.8653 77.8667 76.8966 81.9055 81.4962 81.9055 81.4962 81.9055 81.4962 81.9055 81.4962 81.9055 81.4962							<u> </u>						
65.8449 67.0459 65.5944													
67.5707 67.1534 67.4849						+							
68.3410 67.3088 67.9115					+								
68.5082 69.4443 68.7440 69.2928 69.4603 68.7440 69.5706 69.8782 69.7515 70.0106 69.9384 70.2290 70.0106 69.9384 70.2290													
69.5706 69.8782 69.7515	68.5082	69.444	68.4511		1	1							
70.0106 69.9384 70.2290 70.2269 70.0798 70.4140 70.771 70.3432 71.6171 72.0448 71.4524 75.8268 72.7633 73.2540 75.8544													
70.2263 70.0798 70.4140													
70.7711 70.3432 71.1318						I							
71.6171 72.0448 71.4524						<u> </u>					I		
75.8268 72.7633 73.2540 76.8544 74.5576 73.2624 76.77500 74.5592 76.8653 77.9867 76.8966 80.2664 81.3173 77.4953 81.9055 81.4992 <td< td=""><td></td><td></td><td></td><td></td><td></td><td>+</td><td>+</td><td></td><td></td><td></td><td><u> </u></td><td></td><td></td></td<>						+	+				<u> </u>		
75.8544 74.5976 73.2624 76.7763 77.2004 74.5592 76.8653 77.9867 76.8966 80.2664 81.3173 77.4953 81.9055 81.4992 78.5068					+	+	<u> </u>						
76.7763 77.2004 74.5592					+	+	1			-1	†	-	
76.8853 77.9867 76.8966					1	t	1			1	<u> </u>	1	
80.2664 81.3173 77.4953			76.8960				1				1		i
83.1295 81.5827 78.5668 84.8814 81.6052 82.8026 </td <td>80.2664</td> <td>4 81.317</td> <td>3 77.4953</td> <td>3</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	80.2664	4 81.317	3 77.4953	3									
84.8814 81.6052 82.8026 85.2087 82.0497 87.8336 85.4425 82.3824 88.8182 88.9759 82.7042 89.0255 91.0799 83.2923 102.6272			2 78.2504							1			
85.2087 82.0497 87.8336 <td></td> <td>5 81.582</td> <td>7 78.566</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1</td> <td></td> <td></td> <td></td>		5 81.582	7 78.566							1			
85.4425 82.3824 88.8162 <td></td> <td></td> <td></td> <td></td> <td></td> <td>1</td> <td>1</td> <td></td> <td></td> <td></td> <td>I</td> <td></td> <td></td>						1	1				I		
88.9759 82.7042 89.0255 91.0799 83.2923 102.6272 <td< td=""><td></td><td></td><td></td><td></td><td>1</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td> ·</td></td<>					1								·
91.0799 83.2923 102.6272 91.6729 83.6743 108.3565 94.6421 84.1560 114.8737 105.4016 91.5723 115.7703 106.3813 100.5538 122.6361						+	+				 		
91.6729 83.6743 108.3565 94.6421 84.1560 114.8737 105.4016 91.3150 115.7703 108.3813 100.5538 122.6361							+				<u> </u>		
94.6421 84.1560 114.8737 105.4016 91.3150 115.7703 108.3813 100.5538 122.6361					-	+	+			+	1		
105.4016 91.3150 115.7703 108.3813 100.5538 122.6361					-	1	1	1		+	1		
108.3813 100.5538 122.6361											1		
			8 122.636	1	-		1			1	1		

Component 5:

					Compo	nent 5:					
Componen	t 5	Failure Dat	a								
Failure PD				(Top Weibu						Exponentia	
10 Data Po	ints			High Level	Fitting Para	ameters			Low Level	Fitting Para	meters
Set1	Set2	Set3				Rep3			Rep1	Rep2	Rep3
384.4927	641.1133		Shape	1.8723	1.1411	1.8549		Lambda	0.0007	0.0006	0.0009
545.0513	836.1144	473.7554	Scale	2014.397	1492.544	1545.62		Mean	1428.571	1666.667	1111.111
1014.724	1063.66	774.6268	Location	0	530.6213	0		Location	384.4927	440.0948	244.2498
1467.796	1225.419	1200.055									
1528.46	1386.741	1259.333									
1796.037	1677.181	1431.017									
1805.159	1710.791	1463.062			· · · ·						
2685.534	2509.8										
3171.514	4063.236	2380.459									
3470.297	4405.597										
Failure PD	F			(Top Weib	ull++ Selec	tion)			(Weibull++	Exponentia	al)
50 Data Po	A 7 11 AL A A A A A A A A A A A A A A A A A			High Level						Fitting Para	
Set1	Set2	Set3			Rep2	Rep3			Rep1	Rep2	Rep3
478.862	and the second sec		Shape	2.2201	1.7751	1.8758		Lambda	0.0007	0.0007	0.0007
559.5032			Scale		1712.647	1853.406		Mean	1428.571		
606.1648		378.0646	Location	2134.500	0	0000.400		Location	478.862	139.3333	
666.5704		444.4303			0	<u> </u>		Location	-10.002	100.0000	2.77.0100
747.9887		563.182									┟────┤
874.4738		606.8696								<u> </u>	├ ───┤
898.0651	649.797	690.6264								<u> </u>	<u>├</u> ────┤
942.651		690.6264					ŀ		AMETERS	L	
956.5013		728.1186						Weibull		>	ļ'
982.7919		728.617						Shape			
1002.692		739.3244						Scale	2 2000		ļ'
		750.4836									ļ
1229.721								Location	0		 '
1271.843										I	
1296.71										l	L
1318.26										 	
1395.802										L	
1407.178									· · · · · · · · · · · · · · · · · · ·	1	
1424.359		1120.212									
1452.061		1200.526							· · · · ·		
1525.454						ļ					L
1551.733											L
1567.216											
1606.131				l						·	
1858.728										<u> </u>	
1909.199											
1927.392						ļ				ļ	
1929.022				 			<u> </u>		ļ	ļ	
1952.617		1587.083		 						 	
1967.877								I		 	l
1994.657										 	<u> </u>
2029.51		1814.845					ļ			ļ	
2038.27					L	ļ	· · · ·			1	
2122.888						1					
2235.849									1		l
2375.611			-					ļ	ļ		_
2421.885			1								
2436.823					L		L			L	
2460.293						ļ				<u> </u>	
2526.509						1			1		
2549.512											
2637.84								<u> </u>			
2680.403			-								
2842.487		1									
2864.291	2401.005	2753.988	3		1	1			T	Γ	
2932.771	2402.354	2827.33	3								
3146.245	2633.574					1					1
3370.188				1	İ	1	1	1	1	1	1
3651.116						1	1		1	1	1
3730.11						1	1	1	1		1
4825.686		1			1	1	1		1	+	+
		1.111.001	· · · · · · · · · · · · · · · · · · ·		1		4		1	<u></u>	

Component	5	Repair Data	a			Т					True Lognormal Mean:	60
		riopan bai	·								True Lognormal St Dev:	8
Repair PD				(Top Weib)	ult++ Select	ion)	(Empirical)			Desired Lognormal Variance:	64
10 Data Po					Fitting Para				Fitting Para	meters		
	Set2	Set3				Rep3				Rep3		
42.3867	47.6347	51.4372	N Mean						· ·		Mean for Normal variates:	4.085533762
43.2308	48.1388	52.2682	N S.D.				(Empirical)			Var for Normal variates:	0.017621601
48.2416	52.5022	52.7358	LogN Mean	1	1	1		/			St Dev for Normal Variates:	0.13274638
51.4218	56.1148	54.5995	LogN S.D.	0	0	0						
53.5588	57.9414	55.6594	•									
53.7508	60.2239	56.2238	WeibullShape	1.5821	2.9888	1.8122						
61.3120	65.4354	56.9997	Scale	20.0399	24.3756	7.0711						
62.2097	66.2377	59.3828	Location	38.8838	37.8505	49.9941						
70.7762	68.6597	59.7857										
81.3838	72.4364	63.5537										
Repair PD				(Top Weib	ull++ Select	ion)	(Empirical)	1			
50 Data Po	oints				Fitting Para		1	ow Level	Fitting Para	meters		
Set1	Set2	Set3		Rep1		Rep3	ŀ	7ep1	Rep2	Rep3		
43.3633	40.7621	43.0694	N Mean		4.1117	4.0748						
44.4692	48.5947	46.7846	N S.D.		0.1551	0.1146		Empirical				
45.4751	49.4850	50.4923	LogN Mean	1	61.78916							
48.6513	50.2172	51.6487	LogN S.D.	0	9.641424	6.809686						
50.0403	51.6521	51.9374										
50.2316	52.1425	52.1729	Weibull Shape	2.7445					1			
51.7557	52.2455	52.3547	Scale	25.1628								
52.2082	52.5248	52.4985	Location	38.2597								
52.3060		52.5289										
52.5053	53.1965	52.8929										
52.9333	55.0626	52.9659										
53.7309		53.8248										
53.9276												
54.3129									1			
54.9343												
55.3858		55.2281										
56.2124		55.9278										
56.7725		56.1931							1			
56.7782				<u> </u>								
57.6110		56.6643								L		
57.7294					I							
57.7883					1							
58.9255												
59.2438			· · · · · · · · · · · · · · · · · · ·									
59.5306												
60.7142									<u> </u>			
61.3204									I	<u> </u>		
61.3279				1		ļ				I	1	i
61.9357				<u> </u>	Į					l		l
62.3702	2 61.4066 6 62.7784				ł				+			
63.0976 64.0290				 					-		1	
64.2367					ł	1			+		1	
64.378 64.4379					+					I		
				+	+				1	ł		
65.6110 65.956					+						1	l
66.841										1	1	· · · · ·
67.919		63.0855								-	1	
68.079				+	+	+				+	1	
68.810										+	1	
68.854				+	+	+			1	1		
70.554				1	+							
70.554										1		l
70.930						+						
71.491						+			+			t
71.587						+			+	+	1	
75.833				1	1	+			+	1	+ · · ·	
80.949				1	1	+			-	+		t
83.300						+	I		+		+	<u> </u>
03.300	cj 0/.23/	1 79.4092	Fl	A		.l	L		1	1	- · · · · · · · · · · · · · · · · · · ·	L

Appendix D: Fitting Data (Final Experiment)

.

Component 1:

Commonsat	1: IFR Failur		r	r	T	r		1	· · ·	1	F	rr	
Component	I. IFN FARUN										ļ	TRUE IFR PARA	METERS
Failure PDF					ull++ Selec					Exponenti		Weibull	
5 Data Point					Fitting Par					Fitting Para		Shape	1.5
Set1	Set2	Set3		Rep1	Rep2	Rep3			Rep1	Rep2	Rep3	Scale	3000
181.1979 982.1146		287.5772 937.6879	Shape Scale		0.6094			Lambda mean	0.0004	0.0008		Location	0
2226.3576	2383,1759		Location		2218.289			Location		1547.451	2300		
2388.7594	2472.4279	2778.1681	Loodinoit		2210.200	10.7020		Location	<u> </u>	1017.107			
5399.2774	4496.5138		Exp. Lambda	0.0004									
			mean	2500									
			Location	0					L				
Failure PDF				(Top Woih	l ull++ Selec	tion\			Molbullu	Exponenti	al)		
25 Data Poin					Fitting Par					Fitting Para			
Set1	Set2	Set3		Rep1	Rep2	Rep3			Rep1	Rep2	Rep3		
68.4728		319.593	Shape					Lambda	0.0005				
331.6175	852.5509	651.7494		2430,633		2918.504		mean	2000				
416.3119	872.1424	712.6503	Location	0	76.2918	126.3392		Location	68.4728	0	319.593		
765.5116 985.3227	885.9164 1339.2671	756.6507 945.8708											
1091.8591	1384.6532	956.1866		· · ·									
1209.8468	1873.6413	1104.1897											
1442.4947	2102.4384	1498.2734				i							
1595.0677	2249,4598	1754.579			<u> </u>								
1651.5536 1712.5829	2297.4357 2419.0937	1915.9636 1961.8824								<u> </u>			
1712,5829	2419,0937 2440.497	2283.4476											
1970.983	2480.1319	2561.7131											
2395.9298	2690.5506	2579.4042											
2535.9024	2764.3675	2604.1896											·
2590.8444	2930.4622	3034.4819 3627.4104				ļ							
2856.3818 2939.8024	2971.7748 2976.9494	3627.4104											
2977.372	3598.5336	4224.4737			· · · · · · · · · · · · · · · · · · ·								
3046.7539	3959.8607	4353.1658											
3702.9801	4424.5982	4731.5963											
3778.5931	4635.2492	4792.5074							L		L		
3787.6137 3996.1117	5039.1509 7344.0245	4808.6287 5785.7093											
5170.1898	8029.4939	7695.7031											··
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	4.050 5-14.				r	/		L	· · · · · · · · ·	r	[]		
Com po ne nt	1: DFR Failu	rə					· · · · · ·		· · · · · · · · · · · · · · · · · · ·				AMETERS
Com po ne nt Failure PDF	1: DFR Failu	70		(Top Weib	ull++ Selec	tion)	·····		(Weibull++	Exponenti	al)	TRUE DFR PAR Welbull	AMETERS
Failure PDF 5 Data Points	3			High Level	ull++ Selec Fitting Para	ameters			Low Level	Exponenti Fitting Para	meters	Weibull Shape	0.5
Failure PDF 5 Data Points Set1	3 Set2	Set3		High Level Rep1		ameters Rep3			Low Level Rep1	Fitting Para Rep2	Rep3	Welbull Shape Scale	0.5 1354
Failure PDF 5 Data Points Set1 139.4629	3 Set2 0.0637	Set3 0.6333	Shape	High Level Rep1 0.5196	Fitting Par	ameters Rep3 0.2708		Lambda	Low Level Rep1 0.0002	Fitting Para Rep2 0.0004	meters Rep3 0.0004	Weibull Shape	0.5
Failure PDF 5 Data Points Set1 139.4629 469.7426	3 Set2 0.0637 1038.2233	Set3 0.6333 3.8248	Shape Scale	High Level Rep1 0.5196 2709.083	Fitting Par	ameters Rep3 0.2708 509.9078		mean	Low Level Rep1 0.0002 5000	Fitting Para Rep2 0.0004 2500	meters Rep3 0.0004 2500	Welbull Shape Scale	0.5 1354
Failure PDF 5 Data Points Set1 139.4629 469.7426 836.6793	3 Set2 0.0637 1038 2233 1703 1888	Set3 0.6333 3.8248 425.0307	Shape Scale	High Level Rep1 0.5196	Fitting Par	ameters Rep3 0.2708			Low Level Rep1 0.0002	Fitting Para Rep2 0.0004	meters Rep3 0.0004	Welbull Shape Scale	0.5 1354
Failure PDF 5 Data Points Set1 139.4629 469.7426	3 Set2 0.0637 1038.2233	Set3 0.6333 3.8248 425.0307 3214.1432	Shape Scale Location Exp. Lambda	High Level Rep1 0.5196 2709.083	Fitting Par Rep2 0.0004	ameters Rep3 0.2708 509.9078		mean	Low Level Rep1 0.0002 5000	Fitting Para Rep2 0.0004 2500	meters Rep3 0.0004 2500	Welbull Shape Scale	0.5 1354
Failure PDF 5 Data Points Set1 139.4629 469.7426 836.6793 7502.4567	3 Set2 0.0637 1038.2233 1703.1888 2524.7519	Set3 0.6333 3.8248 425.0307 3214.1432	Shape Scale Location Exp. Lambda mean	High Level Rep1 0.5196 2709.083	Fitting Par Rep2 0.0004 2500	ameters Rep3 0.2708 509.9078		mean	Low Level Rep1 0.0002 5000	Fitting Para Rep2 0.0004 2500	meters Rep3 0.0004 2500	Welbull Shape Scale	0.5 1354
Failure PDF 5 Data Points Set1 139.4629 469.7426 836.6793 7502.4567	3 Set2 0.0637 1038.2233 1703.1888 2524.7519	Set3 0.6333 3.8248 425.0307 3214.1432	Shape Scale Location Exp. Lambda	High Level Rep1 0.5196 2709.083	Fitting Par Rep2 0.0004	ameters Rep3 0.2708 509.9078		mean	Low Level Rep1 0.0002 5000	Fitting Para Rep2 0.0004 2500	meters Rep3 0.0004 2500	Welbull Shape Scale	0.5 1354
Failure PDF 5 Data Point Set1 139.4629 469.7426 836.6793 7502.4567 14660.2643	3 Set2 0.0637 1038.2233 1703.1888 2524.7519	Set3 0.6333 3.8248 425.0307 3214.1432	Shape Scale Location Exp. Lambda mean	High Level Rep1 0.5196 2709.083 120.3868	Fitting Par Rep2 0.0004 2500 0	ameters Rep3 0.2708 509.9078 0.6248		mean	Low Level Rep1 0.0002 5000 0	Fitting Para Rep2 0.0004 2500 0	meters Rep3 0.0004 2500 0	Welbull Shape Scale	0.5 1354
Failure PDF 5 Data Points Set1 139.4629 469.7426 836.6793 7502.4567 14660.2643 Failure PDF	3 Set2 1038,2233 1703,1888 2524,7519 6112,2116	Set3 0.6333 3.8248 425.0307 3214.1432	Shape Scale Location Exp. Lambda mean	High Level Rep1 0.5196 2709.083 120.3868	Fitting Par Rep2 0.0004 2500 0 ull++ Select	ameters Rep3 0.2708 509.9078 0.6248		mean	Low Level Rep1 0.0002 5000 0 (Weibull++	Fitting Para Rep2 0.0004 2500 0	ameters Rep3 0.0004 2500 0 0	Welbull Shape Scale	0.5 1354
Failure PDF 5 Data Points Set1 139.4629 469.7426 836.6793 7502.4567 14660.2643 Failure PDF Z5 Data Poin Set1	3 Set2 0.0637 1036.2233 1703.1888 2524.7519 6112.2116 6112.2116	Set3 0.6333 3.8248 425.0307 3214.1432 7872.6754 Set3	Shape Scale Location Exp. Lambda mean Location	High Level Rep1 0.5196 2709.083 120.3868 (Top Weibh High Level Rep1	Fitting Para Rep2 0.0004 2500 0 Ull++ Select Fitting Para Rep2	ameters Rep3 0.2708 509.9078 0.6248 		mean Location	Low Level Rep1 0.0002 5000 0 (Weibull++ Low Level Rep1	Fitting Para Rep2 0.0004 2500 0 0 Exponenti Fitting Para Rep2	meters Rep3 0.0004 2500 0 0 al) meters Rep3	Welbull Shape Scale	0.5 1354
Failure PDF 5 Data Points 5 Data Points 5 Data Points 5 Data Points 7502.4567 14660.2643 Failure PDF 25 Data Poin Set1 8.5763	3 Set2 0.0637 1038,2233 1703,1888 2524,7519 6112,2116 6112,2116 13 Set2 0.001	Set3 0.6333 3.8248 425.0307 3214.1432 7872.6754 Set3 0.23	Shape Scale Location Exp. Lambda mean Location Shape	High Level Rep1 0.5196 2709.083 120.3868 120.3868 (Top Weib) High Level Rep1 0.5068	Fitting Para Rep2 0.0004 2500 0 ull++ Select Fitting Para Fitting Para Rep2 0.4887	ameters Rep3 0.2708 509.9078 0.6248 		mean Location Lambda	Low Level Rep1 0.0002 5000 0 0 (Weibull++ Low Level Rep1 0.0003	Fitting Para Rep2 0.0004 2500 0 0 Exponentii Fitting Para Rep2 0.0004	meters Rep3 0.0004 2500 0 	Welbull Shape Scale	0.5 1354
Failure PDF 5 Data Points Set1 139.4629 469.7426 836.6793 7502.4567 14660.2643 Failure PDF 25 Data Poin Set1 8.5763 12.033	3 Set2 0.0637 1038.2233 1703.1888 2524.7519 6112.2116 6112.2116 13 Set2 0.001 0.1838	Set3 0.6333 3.8248 425.0307 3214.1432 7872.6754 Set3 0.23 3.3597	Shape Scale Location Exp. Lambda mean Location Shape Scale	High Level Rep1 0.5196 2709.083 120.3868 120.3868 (Top Weib High Level Rep1 0.5068 1517.284	Fitting Par Rep2 0.0004 2500 0 ull++ Select Fitting Par Rep2 0.4887 1589.497	ameters Rep3 0.2708 509.9078 0.6248 0.6248 1000		mean Location Lambda mean	Low Level Rep1 0.0002 5000 0 (Weibull++ Low Level Rep1 0.0003 3333.333	Fitting Para Rep2 0.0004 2500 0 Exponenti Fitting Para Rep2 0.0004 2500	ameters Rep3 0.0004 2500 0 0 al) Rep3 0.0006 1666.667	Welbull Shape Scale	0.5 1354
Failure PDF 5 Data Points Set1 139.4629 469.7426 836.6793 7502.4567 14660.2643 14660.2643 Failure PDF 5 Failure PDF 25 Data Poin Set1 8.5763 12.033 35.734	3 Set2 0.0637 1038.2233 1703.1888 2524.7519 6112.2116 112.2116 set2 0.001 0.1838 6.1297	Set3 0.6333 3.8248 425.0307 3214.1432 7872.6754 Set3 0.23 3.3597 8.0134	Shape Scale Location Exp. Lambda mean Location Shape	High Level Rep1 0.5196 2709.083 120.3868 120.3868 (Top Weib) High Level Rep1 0.5068	Fitting Para Rep2 0.0004 2500 0 ull++ Select Fitting Para Fitting Para Rep2 0.4887	ameters Rep3 0.2708 509.9078 0.6248 		mean Location Lambda	Low Level Rep1 0.0002 5000 0 0 (Weibull++ Low Level Rep1 0.0003	Fitting Para Rep2 0.0004 2500 0 0 Exponentii Fitting Para Rep2 0.0004	meters Rep3 0.0004 2500 0 	Welbull Shape Scale	0.5 1354
Failure PDF 5 Data Points Set1 139.4629 469.7426 836.6793 7502.4567 14660.2643 Failure PDF 25 Data Poin Set1 8.5763 12.033 35.734 38.9043	3 Set2 0.0637 1038.2233 1703.1888 2524.7519 6112.2116 15 Set2 0.001 0.1838 6.1297 13.0001	Set3 0.6333 3.8248 425.0307 3214.1432 7872.6754 Set3 0.23 3.3597 8.0134 9.1801	Shape Scale Location Exp. Lambda mean Location Shape Scale Location	High Level Rep1 0.5196 2709.083 120.3868 120.3868 (Top Weib High Level Rep1 0.5068 1517.284	Fitting Par Rep2 0.0004 2500 0 ull++ Select Fitting Par Rep2 0.4887 1589.497	ameters Rep3 0.2708 509.9078 0.6248 0.6248 1000		mean Location Lambda mean	Low Level Rep1 0.0002 5000 0 (Weibull++ Low Level Rep1 0.0003 3333.333	Fitting Para Rep2 0.0004 2500 0 Exponenti Fitting Para Rep2 0.0004 2500	ameters Rep3 0.0004 2500 0 0 al) Rep3 0.0006 1666.667	Welbull Shape Scale	0.5 1354
Failure PDF 5 Data Points Set1 139.4629 469.7426 836.6793 7502.4567 14660.2643 14660.2643 Failure PDF 5 Failure PDF 25 Data Poin Set1 8.5763 12.033 35.734	3 Set2 0.0637 1038.2233 1703.1888 2524.7519 6112.2116 112.2116 set2 0.001 0.1838 6.1297	Set3 0.6333 3.8248 425.0307 3214.1432 7872.6754 Set3 0.23 3.3597 8.0134	Shape Scale Location Exp. Lambda mean Location Shape Scale Location	High Level Rep1 0.5196 2709.083 120.3868 120.3868 (Top Weib High Level Rep1 0.5068 1517.284	Fitting Par Rep2 0.0004 2500 0 ull++ Select Fitting Par Rep2 0.4887 1589.497	ameters Rep3 0.2708 509.9078 0.6248 0.6248 1000		mean Location Lambda mean	Low Level Rep1 0.0002 5000 0 (Weibull++ Low Level Rep1 0.0003 3333.333	Fitting Para Rep2 0.0004 2500 0 Exponenti Fitting Para Rep2 0.0004 2500	ameters Rep3 0.0004 2500 0 0 al) meters Rep3 0.0006 1666.667	Welbull Shape Scale	0.5 1354
Failure PDF 5 Data Points Set1 139.4629 469.7426 836.6793 7502.4567 14660.2643 Failure PDF 25 Data Poin Set1 8.5763 12.033 35.734 38.9043 43.0139 73.9562 117.0724	3 Set2 0.0637 1038.2233 1703.1888 2524.7519 6112.2116 5012 0.001 0.1838 6.1297 13.0001 80.2815 156.3244 199.4423	Set3 0.6333 3.8248 425.0307 3214.1432 7872.6754 Set3 0.23 3.3597 8.0134 9.1801 14.0094 9.1801 14.0094 3.8833 3.8.816	Shape Scale Location Exp. Lambda mean Location Shape Scale Location	High Level Rep1 0.5196 2709.083 120.3868 120.3868 (Top Weib High Level Rep1 0.5068 1517.284	Fitting Par Rep2 0.0004 2500 0 ull++ Select Fitting Par Rep2 0.4887 1589.497	ameters Rep3 0.2708 509.9078 0.6248 0.6248 1000		mean Location Lambda mean	Low Level Rep1 0.0002 5000 0 (Weibull++ Low Level Rep1 0.0003 3333.333	Fitting Para Rep2 0.0004 2500 0 Exponenti Fitting Para Rep2 0.0004 2500	ameters Rep3 0.0004 2500 0 0 al) meters Rep3 0.0006 1666.667	Welbull Shape Scale	0.5 1354
Failure PDF 5 Data Points Set1 139.4629 469.7426 836.6793 7502.4567 14660.2643 Failure PDF 25 Data Poin Set1 8.5763 12.033 35.734 43.0139 73.9562 117.0724 233.2414	3 Set2 0.0637 1038.2233 1703.1888 2524.7519 6112.2116 58et2 0.001 0.1838 6.1297 13.0001 80.2815 156.3244 199.4423 265.532	Set3 0.6333 3.8248 425.0307 3214.1432 7872.6754 Set3 0.23 3.3597 8.0134 9.1801 14.0094 22.8633 38.816 65.5375	Shape Scale Location Exp. Lambda mean Location Shape Scale Location	High Level Rep1 0.5196 2709.083 120.3868 120.3868 (Top Weib High Level Rep1 0.5068 1517.284	Fitting Par Rep2 0.0004 2500 0 ull++ Select Fitting Par Rep2 0.4887 1589.497	ameters Rep3 0.2708 509.9078 0.6248 0.6248 1000		mean Location Lambda mean	Low Level Rep1 0.0002 5000 0 (Weibull++ Low Level Rep1 0.0003 3333.333	Fitting Para Rep2 0.0004 2500 0 Exponenti Fitting Para Rep2 0.0004 2500	ameters Rep3 0.0004 2500 0 0 al) meters Rep3 0.0006 1666.667	Welbull Shape Scale	0.5 1354
Failure PDF 5 Data Points Set1 139.4629 469.7426 836.6793 7502.4567 14660.2643 14660.2643 525 Data Poin Set1 8.5763 12.033 35.734 38.9043 43.0139 73.9562 117.0724 233.2414 238.2957	3 Set2 0.0637 1038.2233 1703.1888 2524.7519 6112.2116 112.2116 8612 0.001 0.1838 6.1297 13.0001 80.2815 156.3244 199.4423 285.532 285.532 326.6303	Set3 0.6333 3.6248 425,0307 3214,1432 7872.6754 Set3 0.23 3.3597 8.0134 9.1801 14.0094 22.8833 38.816 65.5375 90.886	Shape Scale Location Exp. Lambda mean Location Shape Scale Location	High Level Rep1 0.5196 2709.083 120.3868 120.3868 (Top Weib High Level Rep1 0.5068 1517.284	Fitting Par Rep2 0.0004 2500 0 ull++ Select Fitting Par Rep2 0.4887 1589.497	ameters Rep3 0.2708 509.9078 0.6248 0.6248 1000		mean Location Lambda mean	Low Level Rep1 0.0002 5000 0 (Weibull++ Low Level Rep1 0.0003 3333.333	Fitting Para Rep2 0.0004 2500 0 Exponenti Fitting Para Rep2 0.0004 2500	ameters Rep3 0.0004 2500 0 0 al) meters Rep3 0.0006 1666.667	Welbull Shape Scale	0.5 1354
Failure PDF 5 Data Points Set1 139.4629 469.7426 836.6793 7502.4567 14660.2643 	3 Set2 0.0637 1038.2233 1703.1888 2524.7519 6112.2116 5612.2116 5612.2116 0.001 0.16338 6.1297 13.0001 80.2815 156.3244 199.4423 285.532 285.5564	Set3 0.6333 3.8248 425.0307 3214.1432 7872.6754 Set3 0.23 3.3597 8.0134 9.1801 14.0094 22.8833 38.816 65.5375 90.886 129.6294	Shape Scale Location Exp. Lambda mean Location Shape Scale Location	High Level Rep1 0.5196 2709.083 120.3868 120.3868 (Top Weib High Level Rep1 0.5068 1517.284	Fitting Par Rep2 0.0004 2500 0 ull++ Select Fitting Par Rep2 0.4887 1589.497	ameters Rep3 0.2708 509.9078 0.6248 0.6248 1000		mean Location Lambda mean	Low Level Rep1 0.0002 5000 0 (Weibull++ Low Level Rep1 0.0003 3333.333	Fitting Para Rep2 0.0004 2500 0 Exponenti Fitting Para Rep2 0.0004 2500	ameters Rep3 0.0004 2500 0 0 al) meters Rep3 0.0006 1666.667	Welbull Shape Scale	0.5 1354
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Failure PDF 5 Data Points Set1 139.4629 469.7426 836.6793 7502.4567 14660.2643 	3 Set2 0.0637 1038.2233 1703.1888 2524.7519 6112.2116 5612.2116 0.001 0.1838 6.1297 13.0001 80.2815 156.3244 199.4423 285.532 326.8303 765.5564 865.7244	Set3 0.6333 3.8248 425.0307 3214.1432 7872.6754 Set3 0.23 3.3597 8.0134 9.1801 14.0094 22.8833 3.8.816 65.5375 90.886 129.6294 169.409	Shape Scale Location Exp. Lambda mean Location Shape Scale Location	High Level Rep1 0.5196 2709.083 120.3868 120.3868 (Top Weib High Level Rep1 0.5068 1517.284	Fitting Par Rep2 0.0004 2500 0 ull++ Select Fitting Par Rep2 0.4887 1589.497	ameters Rep3 0.2708 509.9078 0.6248 0.6248 1000		mean Location Lambda mean	Low Level Rep1 0.0002 5000 0 (Weibull++ Low Level Rep1 0.0003 3333.333	Fitting Para Rep2 0.0004 2500 0 Exponenti Fitting Para Rep2 0.0004 2500	ameters Rep3 0.0004 2500 0 0 al) meters Rep3 0.0006 1666.667	Welbull Shape Scale	0.5 1354
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Failure PDF 5 Data Points Set1 139.4629 469.7426 836.6793 7502.4567 14660.2843 5731 525 Data Poin Set1 8.5763 12.033 35.734 38.9043 43.0139 73.9562 117.0724 238.2414 298.2957 359.7071 543.8688 545.6467 920.3555 973.9422 1081.318 1525.3416	3 Set2 0.0637 1038.2233 1703.1888 2524.7519 6112.2116 524.7519 6112.2116 0.001 0.1838 6.1297 13.0001 80.2815 156.3244 199.4423 285.532 326.8303 765.5564 865.7244 1064.9274 1061.9274 1061.9274 1065.1005 2491.2659 2491.2659 2455.2228	Set3 0.6333 3.8248 425,0307 3214.1432 7872.6754 Set3 0.23 3.3597 8.0134 9.1801 14.0094 22.8833 38.816 65.5375 90.886 129.6294 169.409 199.2903 283.987 346.233 379.0188 466.5133	Shape Scale Location Exp. Lambda mean Location Shape Scale Location	High Level Rep1 0.5196 2709.083 120.3868 120.3868 (Top Weib High Level Rep1 0.5068 1517.284	Fitting Par Rep2 0.0004 2500 0 ull++ Select Fitting Par Rep2 0.4887 1589.497	ameters Rep3 0.2708 509.9078 0.6248 0.6248 1000		mean Location Lambda mean	Low Level Rep1 0.0002 5000 0 (Weibull++ Low Level Rep1 0.0003 3333.333	Fitting Para Rep2 0.0004 2500 0 Exponenti Fitting Para Rep2 0.0004 2500	ameters Rep3 0.0004 2500 0 0 al) meters Rep3 0.0006 1666.667	Welbull Shape Scale	0.5 1354
Failure PDF 5 Data Points Set1 139.4629 469.7426 836.6793 7502.4567 14660.2643 Failure PDF 25 Data Poin Set1 8.5763 12.033 35.734 35.734 33.0438 43.0139 73.9562 117.0724 233.2414 298.2957 920.3555 973.9422 1081.318 1525.3416 1646.0548	3 Set2 0.0637 1038.2233 1703.1888 2524.7519 6112.2116 5612 0.001 0.1838 6.1297 13.0001 80.2815 156.3244 199.4423 285.532 326.8303 765.5564 865.7244 1061.9274 1665.1605 2491.2869 2855.2928 2916.4294	Set3 0.6333 3.8248 425.0307 3214.1432 7872.6754 Set3 0.23 3.3597 8.0134 9.1801 14.0094 22.8833 38.816 65.5375 90.886 65.5375 90.886 129.6294 169.409 199.2903 283.987 346.233 379.0188 466.5133 575.8503	Shape Scale Location Exp. Lambda mean Location Shape Scale Location	High Level Rep1 0.5196 2709.083 120.3868 120.3868 (Top Weib High Level Rep1 0.5068 1517.284	Fitting Par Rep2 0.0004 2500 0 ull++ Select Fitting Par Rep2 0.4887 1589.497	ameters Rep3 0.2708 509.9078 0.6248 0.6248 1000		mean Location Lambda mean	Low Level Rep1 0.0002 5000 0 (Weibull++ Low Level Rep1 0.0003 3333.333	Fitting Para Rep2 0.0004 2500 0 Exponenti Fitting Para Rep2 0.0004 2500	ameters Rep3 0.0004 2500 0 0 al) meters Rep3 0.0006 1666.667	Welbull Shape Scale	0.5 1354
Failure PDF 5 Data Points Set1 139.4629 469.7426 836.6793 7502.4567 14660.2843 5731 525 Data Poin Set1 8.5763 12.033 35.734 38.9043 43.0139 73.9562 117.0724 238.2414 298.2957 359.7071 543.8688 545.6467 920.3555 973.9422 1081.318 1525.3416	3 Set2 0.0637 1038.2233 1703.1888 2524.7519 6112.2116 524.7519 6112.2116 0.001 0.1838 6.1297 13.0001 80.2815 156.3244 199.4423 285.532 326.8303 765.5564 865.7244 1064.9274 1061.9274 1061.9274 1065.1005 2491.2659 2491.2659 2455.2228	Set3 0.6333 3.8248 425,0307 3214.1432 7872.6754 Set3 0.23 3.3597 8.0134 9.1801 14.0094 22.8833 38.816 65.5375 90.886 129.6294 169.409 199.2903 283.987 346.233 379.0188 466.5133	Shape Scale Location Exp. Lambda mean Location Shape Scale Location	High Level Rep1 0.5196 2709.083 120.3868 120.3868 (Top Weib High Level Rep1 0.5068 1517.284	Fitting Par Rep2 0.0004 2500 0 ull++ Select Fitting Par Rep2 0.4887 1589.497	ameters Rep3 0.2708 509.9078 0.6248 0.6248 1000		mean Location Lambda mean	Low Level Rep1 0.0002 5000 0 (Weibull++ Low Level Rep1 0.0003 3333.333	Fitting Para Rep2 0.0004 2500 0 Exponenti Fitting Para Rep2 0.0004 2500	ameters Rep3 0.0004 2500 0 0 al) meters Rep3 0.0006 1666.667	Welbull Shape Scale	0.5 1354
Failure PDF 5 Data Points Set1 139.4629 469.7426 836.6793 7502.4567 14660.2643 Failure PDF 25 Data Poin Set1 8.5763 12.033 35.734 35.734 35.734 33.0439 73.9562 117.0724 233.2414 298.2957 920.3555 973.9422 1081.318 1525.3416 1646.0548 2183.3176 2858.4604 2183.3176 2858.4604	3 Set2 0.0637 1038.2233 1703.1888 2524.7519 6112.2116 5612 0.001 0.1838 6.1297 13.0001 80.2815 156.3244 199.4423 285.532 326.8303 765.5564 865.7244 1061.9274 1665.1605 2491.2869 2855.2928 2916.4294 2917.5233 3149.028	Set3 0.6333 3.8248 425.0307 3214.1432 7872.6754 Set3 0.23 3.3597 8.0134 9.1801 14.0094 22.8833 38.816 65.5375 90.886 90.886 90.886 90.886 90.886 91.99.2903 33.8977 346.233 379.0188 466.5133 575.8503 675.9627 1191.9816 1654.3719	Shape Scale Location Exp. Lambda mean Location Shape Scale Location	High Level Rep1 0.5196 2709.083 120.3868 120.3868 (Top Weib High Level Rep1 0.5068 1517.284	Fitting Par Rep2 0.0004 2500 0 ull++ Select Fitting Par Rep2 0.4887 1589.497	ameters Rep3 0.2708 509.9078 0.6248 0.6248 1000		mean Location Lambda mean	Low Level Rep1 0.0002 5000 0 (Weibull++ Low Level Rep1 0.0003 3333.333	Fitting Para Rep2 0.0004 2500 0 Exponenti Fitting Para Rep2 0.0004 2500	ameters Rep3 0.0004 2500 0 0 al) meters Rep3 0.0006 1666.667	Welbull Shape Scale	0.5 1354
Failure PDF 5 Data Points Set1 139.4629 469.7426 836.6793 7502.4567 14660.2643 14660.2643 55 Data Poin 8.5763 12.033 35.734 38.9043 43.0139 43.0139 73.9562 117.0724 233.2414 233.2414 233.2414 233.2414 233.2414 233.2414 233.2414 233.2414 233.2414 233.2414 233.2414 243.2457 359.7071 543.8686 545.6467 920.3555 973.9422 1081.318 1525.3416 1646.0548 2183.3176 2858.4604 3234.4206	3 Set2 0.0637 1038.2233 1703.1888 2524.7519 6112.2116 12.21	Set3 0.6333 3.6248 425,0307 3214,1432 7872,6754 Set3 0.23 3.3597 8.0134 9.1801 14.0094 12.8633 38.816 65.5375 90.886 129.6294 169.409 199.2903 283.987 9.92903 283.987 199.2905 283.987 199.2905 283.987 199.2905 283.987 199.2905 297.8503 197.56503 195.56505 195.5505 19	Shape Scale Location Exp. Lambda mean Location Shape Scale Location	High Level Rep1 0.5196 2709.083 120.3868 120.3868 (Top Weib High Level Rep1 0.5068 1517.284	Fitting Par Rep2 0.0004 2500 0 ull++ Select Fitting Par Rep2 0.4887 1589.497	ameters Rep3 0.2708 509.9078 0.6248 0.6248 1000		mean Location Lambda mean	Low Level Rep1 0.0002 5000 0 (Weibull++ Low Level Rep1 0.0003 3333.333	Fitting Para Rep2 0.0004 2500 0 Exponenti Fitting Para Rep2 0.0004 2500	ameters Rep3 0.0004 2500 0 0 al) meters Rep3 0.0006 1666.667	Welbull Shape Scale	0.5 1354
Failure PDF 5 Data Points Set1 139.4629 469.7426 836.6793 7502.4567 14660.2643 5733 12033 12.033 35.734 8.5763 12.033 35.734 38.9043 43.0139 73.9562 117.0724 233.2414 298.2957 359.7071 543.8688 545.6467 920.3555 973.9422 1081.318 1525.3416 1646.0548 2183.3176 2185.3416 2185.3416 2183.3176	3 Set2 0.0637 1038.2233 1703.1888 2524.7519 6112.2116 0.112.2116 0.112.2116 0.1838 6.1297 13.0001 80.2815 156.3244 199.4423 285.532 2326.8303 765.5564 865.7244 1064.201 1061.9274 1665.1605 2491.26599 2491.26599 2491.26599 2491.26599 2491.2659959245959 245	Set3 0.6333 3.8248 425,0307 3214.1432 7872.6754 Set3 0.23 3.3597 8.0134 9.1801 14.0094 2.8833 38.816 65.5375 90.886 129.6294 169.409 199.2903 348.233 379.0188 466.5133 575.8503 375.8503 3587.6506 4577.0942	Shape Scale Location Exp. Lambda mean Location Shape Scale Location	High Level Rep1 0.5196 2709.083 120.3868 120.3868 (Top Weib High Level Rep1 0.5068 1517.284	Fitting Par Rep2 0.0004 2500 0 ull++ Select Fitting Par Rep2 0.4887 1589.497	ameters Rep3 0.2708 509.9078 0.6248 0.6248 1000		mean Location Lambda mean	Low Level Rep1 0.0002 5000 0 (Weibull++ Low Level Rep1 0.0003 3333.333	Fitting Para Rep2 0.0004 2500 0 Exponenti Fitting Para Rep2 0.0004 2500	ameters Rep3 0.0004 2500 0 0 al) meters Rep3 0.0006 1666.667	Welbull Shape Scale	0.5 1354
Failure PDF 5 Data Points Set1 139.4629 469.7426 836.6793 7502.4567 14660.2643 Failure PDF 25 Data Poin Set1 8.5763 12.033 35.734 38.9043 43.0139 73.9562 117.0724 233.2414 293.2414 293.2414 293.2414 293.2414 293.2414 293.2414 293.2414 293.2414 293.2414 293.2414 293.2414 293.2414 294.2355 973.9422 1081.318 1525.3416 1548.0548 2183.3176 2858.4604 3234.4206 4179.5228 4360.3714 10713.9065	3 Set2 0.0637 1038.2233 1703.1888 2524.7519 6112.2116 5612 0.001 0.1838 6.1297 13.0001 80.2815 156.3244 199.4423 285.532 326.8303 765.5564 865.7244 1061.9274 1665.1605 2491.2669 2855.2928 2916.4294 2916.4294 2917.5233 3149.028 3167.2536 5480.5496 5517.3566 6790.4468	Set3 0.6333 3.8248 425.0307 3214.1432 7872.6754 Set3 0.23 3.3597 8.0134 9.1801 14.0094 9.1801 14.0094 9.8803 38.816 65.5375 90.886 129.6294 169.409 199.2903 38.817 346.233 379.0188 466.5133 575.8503 675.9627 1191.9816 1654.3719 3587.6506 4577.0942 5097.7195	Shape Scale Location Exp. Lambda mean Location Shape Scale Location	High Level Rep1 0.5196 2709.083 120.3868 120.3868 (Top Weib High Level Rep1 0.5068 1517.284	Fitting Par Rep2 0.0004 2500 0 ull++ Select Fitting Par Rep2 0.4887 1589.497	ameters Rep3 0.2708 509.9078 0.6248 0.6248 1000		mean Location Lambda mean	Low Level Rep1 0.0002 5000 0 (Weibull++ Low Level Rep1 0.0003 3333.333	Fitting Para Rep2 0.0004 2500 0 Exponenti Fitting Para Rep2 0.0004 2500	ameters Rep3 0.0004 2500 0 0 al) meters Rep3 0.0006 1666.667	Welbull Shape Scale	0.5 1354
Failure PDF 5 Data Points 5 Eata Points 5 Eata Points 5 Eata Points 5 Eata Points 7 502 4567 14660.2843 14660.2843 Failure PDF 25 Data Point 8 5763 12.033 35.734 38.9043 43.0139 73.9562 117.0724 238.2414 238.2957 359.7071 543.8688 545.6467 920.3555 973.9422 1081.318 1525.3416 1646.0548 2183.3176 24858.4604 3234.4206 4179.5228	3 Set2 0.0637 1038.2233 1703.1888 2524.7519 6112.2116 0.112.2116 0.112.2116 0.1838 6.1297 13.0001 80.2815 156.3244 199.4423 285.532 2326.8303 765.5564 865.7244 1064.201 1061.9274 1665.1605 2491.26599 2491.26599 2491.26599 2491.26599 2491.2659959245959 245	Set3 0.6333 3.8248 425,0307 3214.1432 7872.6754 Set3 0.23 3.3597 8.0134 9.1801 14.0094 2.8833 38.816 65.5375 90.886 129.6294 169.409 199.2903 348.233 379.0188 466.5133 575.8503 375.8503 3587.6506 4577.0942	Shape Scale Location Exp. Lambda mean Location Shape Scale Location	High Level Rep1 0.5196 2709.083 120.3868 120.3868 (Top Weib High Level Rep1 0.5068 1517.284	Fitting Par Rep2 0.0004 2500 0 ull++ Select Fitting Par Rep2 0.4887 1589.497	ameters Rep3 0.2708 509.9078 0.6248 0.6248 1000		mean Location Lambda mean	Low Level Rep1 0.0002 5000 0 (Weibull++ Low Level Rep1 0.0003 3333.333	Fitting Para Rep2 0.0004 2500 0 Exponenti Fitting Para Rep2 0.0004 2500	ameters Rep3 0.0004 2500 0 0 al) meters Rep3 0.0006 1666.667	Welbull Shape Scale	0.5 1354

Component	1: Repair			<u> </u>					True Logno	rmal Mean:	2800
Repair PDF	•			(Top Weib	ull++ Selec	tion)		Т	rue Lognorr	nal St Dev:	200
5 Data Points	S			High Level	Fitting Par	ameters	 (Empirical)	Tru	e Lognorma	I Variance:	40000
Set1	Set2	Set3		Rep1	Rep2	Rep3	 Low Level	Fitting Para	ameters		
2601.5784	2612.9115	2601.2429	N Mean				 Rep1	Rep2	Rep3		
2624.7145	2771.1435	2735.2400						Mea	an for Norm	al variates:	7.934830161
2866.0380			LogN Mean	1	1	1	(Empirical)	·V	ar for Norm	al variates:	0.00508907
2909.4363	2887.8300	2910.3966	LogN S.D.	0	0	0		St De	ev for Norma	al Variates:	0.071337714
2917.5533	3024.6103	3032.1756									
		l l	Veibull Shape	26.0652	4.3832	3.5523					
			Scale	2848.267	574.006						
			Location	0	2299.462	2341.219					
Repair PDF				(Top Weib	ull++ Selec	tion)	 (Empirical)				
25 Data Poin	ts			High Level	Fitting Par	ameters	Low Level	Fitting Para	ameters		
	Set2	Set3		Rep1	Rep2	Rep3	Rep1	Rep2	Rep3		
2439.4242	2096.6104	2531.1515	N Mean								
2481.7399	2381.0876	2552.3793	N S.D.				(Empirical)				
2513.2920	2593.7256	2577.2550	LogN Mean	1	1	1	 				
2517.1491	2614.5585	2607.0592	LogN S.D.	0	0	0					
2534.7232	2614.9443	2615.0955		A							
2577.0690	2707.7951	2635.5129	Veibull Shape	2.1543		3.1876					
2631.8083	2730.1049		Scale	413.0219	2853.353	556.6646					
2631.9734	2739.8425		Location	2372.44	0	2322.432					
2644.6329	2763.4976		_								
2691.8745	2814.7469										
2707.8326	2828.4549										
2708.698	2828.6183						 				
2710.402	2833.0496										
2724.2737	2849.2983										
2738.4129	2849.4621	2853.2614									
2778.041	2868.1963										
2797.5505	2885.1118										
2806.1783	2892.7576										
2843.8775	2912.0356	2953.696									
2917.4224	2912.6882	2986.0419					 				
2925.327	2933.7764	3031.5726									
2952.5002	2939.0819	3040.0791									
2969.4237	2945.88										
3099.2115	2962.0594	3079.2475									
3102.8011	2970.7126	3148.6606									

Component 2:

IFR Failure			···		1	[1	1	Г		1		
								-			1	TRUE IFF	PARAME
Failure PDF				(Top Weib	ull++ Selec	tion)			(Weibull++	Exponenti	ial)	Weibull	
5 Data Point	s			High Level	Fitting Par	ameters			LowLevel	Fitting Para	ameters	Shape	4
Set1	Set2	Set3				Rep3		1	Rep1	Rep2	Rep3	Scale	2500
1612.093	1188.4488	1529.0469	Shape	3.6567				Lambda	0.0023	0.001	0.0013	Location	0
1960.6681	1290.1264	2175.3435	Scale	1065.07			[mean	434.7826	1000	769.2308		
1984.2974	2068.7919	2253.8368	Location	1092.293				Location	1612.093	1045.345	1529.047		
2194.6551	2641.2489	2700.0165						1			1		
2503.2496	3009.1271	2855.9128	Ex	p. Lambda	0.001	2302.831	Norma!		1		100000		
				mean	1000	464.9841	s.d.						
				Location	1045.345								
Failure PDF				(Top Weib	ull++ Selec	tion)			(Weibull++	Exponenti	al)		
25 Data Poir	nts			High Level	Fitting Par	ameters		-	Low Level	Fitting Para	ameters		
Set1		Set3				Rep3				Rep2	Rep3		
1217.1241	870.7077	1216.433	Shape					Lambda	0.0009				
1642.9021	1074.6883		Scale		2625.438			mean			1111.111		
1680.602			Location	800.3591	0	1021.904		Location	1217.124	870.7077	1216.433		
1769.1628													
1834.9983	1758.271	1605.873						_					
1871.1207	1763.2181												
1899.1965		1757.8406											
2004.5769		1872.5433											
2015.2816													
2087.2999		2049.4764											
2092.0926		2054.6868											
2117.5404													
2230.4854		2229.1075											
2384.9624	2560.0652												
2583.2324	2641.315												
2610.2233													
2619.4521	2687.7639												
2648.8951	2863.5512	2638.066											
2663.6457	2941.8754												
2749.9839	2947.5725												
2904.3552	2964.1242												
3138.4561	2974.0513	3128.5016											
3234.2694													
3271.5803	3487.88	3426.7407											
3936.8724	3637.9667	3504.4876											

DFR Failure						1		[1	· · · ·			
												TRUE DFF	PARAME
Failure PDF				(Top Weib	ull++ Selec	tion)			(Weibull++	Exponenti	al)	Weibull	
5 Data Point	S			High Level	Fitting Par	ameters			LowLevel	Fitting Para	meters	Shape	0.85
Set1	Set2	Set3				Rep3			Rep1	Rep2	Rep3	Scale	2082
674.0396	263.9219	305.1914	Shape	0.9576	0.4635	0.7888		Lambda	0.0003	0.0004	0.0005	Location	0
1182.5319	333,1048	700.7444	Scale	3132.762	1321.79	1698.197		mean	3333.333	2500	2000		
3294.7512	1151.8919	1065.9406	Location	492.1489	261.3827	226.7046		Location	66.0606	0	0		
5069.5254		2255.4658											
8181.8846	6547.0311	6553.1903											
Failure PDF				(Top Weib						Exponentia			
25 Data Poir				High Level			_		Low Level	Fitting Para			
Set1	Set2	Set3				Rep3					Rep3		
2.98		11.2664	Shape					Lambda	0.0007	0.0004			
35.3013			Scale	1300.736	2575.825	1948.33		mean	1428.571	2500	2500		
54.894	78.5878		Location	0	0	0		Location	0	0	0		
123.6012													
192.524	584.1955												
210.4099													
260.8614	690.6734												
362.1208													
459.2924													
554.3346													
593.4356		921.3175											
903.4713		930.201											
960.4571													
985.9974		1230.0908											
1104.6616													
1235.0752	2953.0618												
1271.5847		2464.6736											
1282.2785													
1769.534													
2395.5922		3266.1679											
2886.6052		4024.5976											
3184.4881	5343.4851												
3624.5633		6764.8413											
4284.256		8281.6728											
8885.7876	9886.4638	12787.509											

Repair	ł		[<u> </u>	r			1		True Logno	mal Mean	1500
Repair PDF				(Top Weih	ull++ Select	tion)				rue Lognorr		100
5 Data Point	s				Fitting Par			(Empirical)		le Lognorma		10000
Set1	Set2	Set3				Rep3		Low Level			Tanandor	10000
1367.8815		1460.5701	N Mean					Rep1	Rep2	Rep3		
1371.0849		1543.4742	NS.D.							an for Norm	al variates:	7.31 1003
1396.5115			LogN Mean	1	1	1		(Empirical)		ar for Norm		0.004435
1544.1540		1628.3525		0	Ó	0		<u></u>		ev for Norm		0.066593
1753.2314		1637.7601					Normal			T		
		v	eibull Shape	0.619	17.4996	1564.779	Mean					
			Scale	85.9718	1530.836	64.5028	S.D.					-
			Location	1364.562	0							
Repair PDF				(Top Weib	ull++ Select	tion)		(Empirical)				
25 Data Poir	nts			High Level	Fitting Para	ameters		Low Level	Fitting Par	ameters		
Set1	Set2	Set3		Rep1		Rep3			Rep2	Rep3		
1280.1149	1272.3984	1289.9730	N Mean					1		1		
1357.4532	1361.6546	1313.6635	NS.D.					(Empirical))			
1362.4470	1405.7792	1373.7726	LogN Mean	1	1	1						
1363.4113	1415.0487	1374.1309	LogN S.D.	0	0	0						
1373.1505	1433.5246	1381.1836										
1385.1089	1461.6078	1409.4947	eibull Shape	17.499	17.5	2.9224						
1423.8314		1415.6678	Scale	1533.556	1584.373	357.4828						
1463.0150			Location	0	0	1196.55						
1471.5777		1460.7675										
1489.5132		1462.5032										
1494.1853		1469.2258										
1507.5896	1546.8919	1510.4431										
1508.8267	1547.176	1511.885										
1514.6871	1549.4138											
1520.1 19	1569.7016	1526.01										
1539.861	1588.6071	1541.3123										
1544.7079	1588.8253	1573.9059										
1545.5162	1592.5024											
1556.2519	1604.8355	and the second second										
1574.2129	1617.0122	1631.1695										
1582.1842	1626.4206											
1595.5558	1630.7171	1678.8727										
1596.281	1670.211	1679.022										
1622.4525	1691.6267	1689.7559										
1660.6851	1723.4756	1736.7218										

Component 3:

IFR Failure		[· · · · ·			l		[1	[
											TRUE IFR	PARAME
Failure PDF				(Top Weib	ull++ Selec	tion)		(Weibull++	Exponenti	al)	Weibull	
5 Data Point	s			High Level	Fitting Par	ameters			Fitting Para		Shape	2.5
Set1	Set2	Set3		Rep1	Rep2	Rep3	 	Rep1	Rep2	Rep3	Scale	4000
2883.5319	2998.5673	2434.8346	Shape	1.0003		3.4133	 Lambda	0.0009	0.0011	0.0006	Location	0
3060.1663	3038.2884	2947.7713	Scale	925.7452		4586.741	mean	1111.111	909.0909	1666.667		
3514.6735	3636.2092	4363.5149	Location	2811.544		0	Location	2634.388	2788.847	2313.926		
3998.5685	3832.8183	4588.3683					 					
5228.9477	4806.3682	6214.0369	Exp. Lambda		0.0011							
			mean		909.0909							
			Location		2788.847		1					
Failure PDF				(Top Weib	ull++ Selec	tion)	 	(Weibull++	Exponenti	al)		
25 Data Poir	its			High Level	Fitting Para	ameters		Low Level	Fitting Para	meters		
Set1	Set2	Set3		Rep1	Rep2	Rep3		Rep1	Rep2	Rep3		
1711.4399	1278.0886	1557.278	Shape	1.2574			 Lambda	0.0006				
1794.8646	1808.9081	1611.9093		1927.631	4258.217	4263.149	mean	1666.667	2500	2500		
2052.9023	2465.6908	1982.5562	Location	1617.411	166.2515	0	Location	1711.44	1278.089	1557.278		
2058.9274	2494.8888	2069.6192										
2073.6771	2546.2591	2151.6954										
2098.9349	2767.6346	2251.1667										
2404.9142	3152.5575	2314.9334										
2624.2049	3162.102	2443.4072							· · · · · · · · · · · · · · · · · · ·			
2772.2025		2877.3355										
2833.8453	3592.8889	3028.6866										
2915.2481		3596.0093										
2985.502		3917.9257										
2987.2932		4019.9073										
31 09.4728		4087.4007										
31 31 .6845		41 46.7606										
31 98 .8659		41 92 7926										
3283.6123		4734.3948										
3796.4672		4745.9303										
3801.7873												
4162.7148							 L					
4228.3248	5574.046											
5341.9776		5028.4013										
6312.7596												
6389.2901		6387.1472										
7126.3486	7081.6374	6617.8441										

DFR Failure									T				
												TRUE DF	R PARAMI
Failure PDF				(Top Weib	ull++ Selec	tion)			(Weibull++	Exponenti	al)	Weibull	
5 Data Point	s			High Level	Fitting Par	ameters			Low Level	Fitting Para	meters	Shape	0.95
Set1	Set2	Set3		Rep1	Rep2	Rep3			Rep1	Rep2	Rep3	Scale	3468
868.5596	698.6931	169.6434	Shape	2.3023	0.6745	0.8935		Lambda	0.0007	0.0003	0.0004	Location	0
1516.3796	1366.5098	401.407	Scale	2553.192	2135.705	2627.934		mean	1428.571	3333.333	2500		
2218.6249	1700.3733	2722.0258	Location	0	658.6182	0		Location	852.0483	0	0		
2697.295	2792.1665	3234.4815									· · · ·		
3966.098	10702.2462	7299.204											
							·····						
Failure PDF				(Top Weib	ull++ Selec	tion)			(Weibull++	Exponenti	al)		
25 Data Poir	its			High Level	Fitting Par	ameters				Fitting Para			
Set1	Set2	Set3		Rep1	Rep2	Rep3			Rep1	Rep2	Rep3		
207.8036	42.6759	26.6541	Shape	0.9439	0.7877	0.8449		Lambda	0.0003	0.0003	0.0003		
266.2007	110.6362	73.5251	Scale	3714.093	2702.41	3310.37		mean	3333.333	3333.333	3333.333		
564.8699	125.2635	202.0481	Location	126.86	21.438	0		Location	0	0	0		
571.728	367.1112	481.4955											
575.5735	412.2275	578.7774											
956.9291	417.0253	911.8075		······									
1372.7997	514.4869	958.3334											
1458.9632	646.2646	1024.3937											
1807.3052	905.7708												
2216.5446	937.2157	1340.3025											
2250.8431		1446.7933											
2279.4159		1703.5091											
2631.9957	1660.6554	1726.7708											
3200.9254		2022.7823											
3607.7149	2070.6515												
3808.4165	2174.3106												
41 35.81 81	2720.8299												
4219.2527	3012.5395	5004.063											
4349.9903	4941.1598	5040.78											
4892.6842		6443.4536											
5591.2831	6328.194												
6274.9309	8346.4754	10469.55					•						
9276.5345	8829.5878	10626.242											
15164.2679	10020.3126	11879.798											
16880 6085	13523.2832	13441.007											

Repair								1		True Logno	rmal Mean:	1000
Repair PDF				(Top Weib	ull++ Selec	tion)			1	rue Lognorr		150
5 Data Point	S				Fitting Para			(Empirical)	Tru	e Lognorma	Variance:	22500
Set1	Set2	Set3		Rep1	Rep2	Rep3		LowLevel	Fitting Par	ameters		
953.3588	833.6803	902.1094	N Mean					Rep1	Rep2	Rep3		
967.4331	1032.5035	979.9325	NS.D.						Me	an for Norm	al variates:	6.89663
1086.5469	1233.167	997.9914	LogN Mean	1	1	1		(Empirical)	١	/ar for Norm	al variates:	0.022251
1088.9893	1274.3727	1123.6429	LogN S.D.	0	0	0			St D	ev for Norm	al Variates:	0.149166
1149.2014	1390.9536	1136.5109				,	Expon.					
		V	Veibull Shape	16.4584	7.3676	0.0078	lambda					
			Scale	1084.1	1234.108	128.2051	mean					
			Location	0	0	900.1852	location					
Repair PDF				(Top Weib	ull++ Select	tion)		(Empirical)				
25 Data Poin	nts			High Level	Fitting Para	ameters		LowLevel	Fitting Par	ameters		
Set1	Set2	Set3		Rep1	Rep2	Rep3		Rep1	Rep2	Rep3		
71 6.0199	844.7964	785.3390	N Mean		6.9252			1				
763.9341	863.4181	831.6782	NS.D.		0.115			(Empirical)				
809.2789	878.9243	836.1035	LogN Mean	1	1024.349	1		1				
838.1591	881.2346	861.4089	LogN S.D.	0	118.1907	0						
851.0674	882.3148	890.2926										
852.7825	906.7347	902.7939	Veibull Shape	2.4568			Normal					
853.2847	917.9051	905.3131	Scale	426.864		1017.332	mean					
855.4755	959.7401	945.2810	Location	623.04		124.465	SD					
916.6027	968.1007	974.6158										
936.9255		979.8526										
978.7269		1032.3233										
989.9185												
1003.1626	1004.4521	1039.3221										
1023.0763	1007.1396	1039.5993										
1027.2774	1036.1979											
1027.7069												
1071.4796		1067.1107										
1082.6045												
1093.7505	1096.0161						L	-l				
1123.4648												
1154.6627	1161.7262											
1155.8881	1178.4055									ļ		
1165.0033	1203.5632											
1353.3809		1224.9552										
1381.8487	1247.8068	1281.3968						1				

Component 4:

IFR Failure	3											
											TRUE IFR	PARAME
Failure PD				(Top Weib	ull++ Selec	tion)		(Weibull++	Exponentia	al)	Weibull	
5 Data Poir	nts			High Level	Fitting Par	ameters		Low Level	Fitting Para	ameters	Shape	1.7
	Set2	Set3			Rep2	Rep3		Rep1	Rep2	Rep3	Scale	1700
	814.5934		Shape	1.3709			Lambda	0.0012		0.0024	Location	0
1321.429	1365.19			995.1192			mean		1428.571			
1895.723	1475.554		Location	971.24	0		Location	1040.31	0	458.4051		
2216.109	1517.455											
2873.409	1664.4	Ex	p. Lambda			0.0024						
			mean			416.6667						
			Location			458.4051						
Failure PD	F			(Top Weib	ull++ Selec	tion)		(Weibullu	Exponentia	 al)		
25 Data Po					Fitting Par		 		Fitting Para			
		Set3				Rep3	 			Rep3		
530.2771	200,3715		Shape	1.298			 Lambda	0.0008				·····
540.401	248.5755	835.6282	Scale	1501.29			mean		1428.571			
726.1561	359.6599	848.035	Location	440.23		483.3504	Location	530.2771	200.3715			
760.3249	426.0651	866.1735			<u>~</u>							
840.5436	434,9741											
944.0206	554,9306	1048,103										
979.1587	579.127	1054,785										
1069.765	688.181	1079.655										
1075.722	959.4233	1129.904										
1153.189	996.8733	1156.848										
1153.868	1140.553	1350.402										
1375.649	1432.618	1367.315										
1501.503	1493.902	1469.085										
1627.924	1678.524	1596.448										
1919.104	1869.419											
2285.03	1912.531	1842.271										
2482.025	2045.89	1905.994										
2566.556	2082.82	2044.315										
2708.679	2267.416											
2774.881	2288.218											
2938.419	2367.334	2530.151										
2953.365	2973.474	2671.39										
3212.516	3181.629	3003.419										
3238.114	3333.269	3034.194										
4378.909	3692.152	3810.435										

DFR Failu	re								r					
												TRUE DF	PARAME	TERS
Failure PD	F			(Top Weib	ull++ Select	tion)			(Weibull++	Exponentia	al)	Weibull		
5 Data Poi	nts			High Level	Fitting Par	ameters			Low Level	Fitting Para	meters	Shape	0,6	
Set1	Set2	Set3		Rep1	Rep2	Rep3			Rep1	Rep2	Rep3	Scale	1008	
11.0497	480.894	70.1082	Shape	0.4993		0,9992	La	ımbda	0.0002	0.0017	0.0026	Location	0	
242.6425	559.0181	150.3176	Scale	2642.701		337.1318	m	ean	5000	588.2353	384.6154			
1947.525	728.0175	232.7354	Location	0		43.9176	Lo	cation	0	349.5782	0			
3472.224	1285.811	569.4263												
18283.15	1555.789	883.2029	p. Lambda		0.0017									
			mean		588.2353									
			Location		349.5782									
Failure PD	F			(Top Weib	ull++ Select	tion)			(Weibull++	Exponentia	al)			
25 Data Po					Fitting Par					Fitting Para				
Set1	Set2	Set3		Rep1	Rep2	Rep3			Rep1	Rep2	Rep3			
5.5541	16.9831	1.5864	Shape	0.6606	0.4855	0.6164	La	ımbda	0.0008	0.0009	0.0005			
19.0226	22.131	5.3811	Scale	1006.345	540.1314	1474.721	m	ean	1250	1111.111	2000			
54.6918	22.4463	11.718	Location	3.3075	16.7859	0	La	cation	0	0	0			
60.0507	23.8545	44.7068												
61.9173	27.0709	111.0731												
68.6155	29.8473	117.8029												
82.5532	37.277	184.8074												
114.3219														
131.4785														
216.6277														
439.2135														
	312.0662													
851.5921		902.3072												
859.8882		990.0742												
1061.002														
1417.39														
1651.562														
1744.063		1785.762												
1967.511		2833.623												
2031.855														
	1366.809													
3238.654		4453.8												
3680.447														
3779.719														
6110.383	11335.71	9351.056							L					

Repair		(1		[<u>г</u>	1	T		True Lognor	mal Mean:	150
Repair PD				(Ton Weih	ull++ Selec	tion)				rue Lognorn		25
5 Data Poi					Fitting Par			(Empirical)		e Lognorma		625
	Set2	Set3		Rep1		Rep3			Fitting Para		runanoo.	
107.9361	112.7261	110.8108	N Mean	4.9334		nopo			Rep2	Rep3		
		148.5015		0.16				1.001		an for Norm	al variates:	4.996936
			ogN Mean	140.6395	1	1		(Empirical)		ar for Norm		0.027399
		158.4165		22.64711	Ö			(,		v for Norma		0.165526
166,6536		179.0876								I		
			ibull Shape		3.7243	8.6173						
			Scale		56.8317							
			Location		83.5173							
		· · · · · · · · · · · · · · · · · · ·										
Repair PD	-			(Top Weib	ull++ Selec	tion)		(Empirical)				
25 Data Po	oints			High Level	Fitting Para	ameters		Low Level	Fitting Para	itting Parameters Rep2 Rep3		
Set1	Set2	Set3		Rep1	Rep2	Rep3		Rep1	Rep2	Rep3		
112.1810	109.6944	123.0544	N Mean			- I		1				
115.7299	113.2002	128.6623	N S.D.					(Empirical)	· · · · · · · · · · · · · · · · · · ·			
116.9827	119.7126	130.3761	.ogN Mean	1	1	1						
122.1091	120.6516	132.2960	LogN S.D.	0	0	0						
	120.9405											
135.6326			bull Shape	3.6758	6.7394	1.8917						
	134.9671	141.9222		82.7082		43.151						
			Location	76.3831	0	116.0788	1					
	139.9656											
147.6691	142.7575											
151.1929	151.9322	146.617										
151.7625												
	155.0988											
158.1261	159.2667	151.3792										
158.4126	159.6028	154.678										
158.8591	162.5519	158.9568										
	165.5747	160.7683										
170.0568		164.3028										
171.5999	167.1319	165.501										
172.6964	169.7564	167.8884										
173.419	175.133	173.1062										
175.2563		180.6055										
183.8417	198.3452	200.29										
201.9854	198.8682	218.1923										

Component 5:

IFR Failur	•							1	1		l		
in the real day	ř					·····						TRUE IFR	
Failure PD	F			(Top Weib	ull++ Selec	tion)			(Weibull++	Exponentia	/aù	Weibull	CARAMG
5 Data Poi				High Level						Fitting Para		Shape	2.8
		Set3				Rep3					Rep3	Scale	
	2113.463		Shape		3.3664			Lambda	0.0006				0000
	2682.808					3631.724		mean	1666.667			Loonion	- V
	3010.518				919.46			Location		2113.463			
	3646.33				010110			Loodinon	LOLIOTT	2110.100	1001.000		
			Exp. Lambda	0.0006	Normal								
			mean		s.d.								
			Location										
Failure PD	F			(Top Weib	II++ Select	tion)			(Weibull++	Exponentia	al)		
25 Data Po	oints			High Level						Fitting Para			
Set 1	Set2	Set3				Rep3					Rep3		
900.3416	1123.459	1418.0763	Shape		2.4586	3.8567		Lambda	0.0005				
1428.436	1170.309	1520.0759	Scale		2852.708	3717.19		mean	2000	2000	2000		
1455.073	1770.679	2050.2135	Location		452.2922	0		Location	900.3416	1123.459	1418.076		
	1829.859	2147.0789											
1710.945	1835.78	221 1.8287	Normal										
	1859.992			2954.431									
	2241.777		SD	1083.48									
	2250.085												
	2434.664												
	2599.351						÷						
	2735.001												
	2854.768												
	2888.969												
	3017.953												
	3076.167												
	3108.421												
	3270.869												
3547.358		4054.2415											
	3510.003												
	3867.605												
	4291.402												
	4704.565												
	4760.473												
	4794.134												
5272.08	5119.947	5530.892											

						l	[TRUE DF	PARAME
Failure PDF	-			(Top Weib	ull++ Selec	tion)		(Weibull++	Exponentia	al)	Weibull	
5 Data Poir	nts			High Level	Fitting Par	ameters		Low Level	Fitting Para	ameters	Shape	0.4
Set1	Set2	Set3		Rep1	Rep2	Rep3	 	Rep1		Rep3	Scale	938
0.3887	237.7436	102.8577	Shape	0.3551	0.4961	0.3509	 Lambda	0.0005	9.55E-05	0.0018	Location	0
	1030.879		Scale	455.3751			mean	2000	10471.27	555.5556		
	1372.084		Location	0	207.53	102.7	Location	0	0	0		
		308.7439										
9511.298	32699.48	2043.3231	Exp. Lambda									
			mean		#DIV/0!							
			Location									
Failure PDF				(Top Weibi					- Exponentia			
25 Data Po				High Level	Fitting Par	ameters	 		Fitting Para			
		Set3				Rep3				Rep3		
0.0044	0.0011	0.0001	Shape				Lambda	0.0006		0.0003		
0.1409	0.153	2.1644		889.8248			mean	1666.667		3333.333		
0.2395	2.0381	2.5861	Location	0	0	0	Location	0	0	0		
2.3157	2.8481	2.5863										
3.4037	3.3508	8.3013					 					
15.5762	9.2546	12.2399					 					
41.4359	69.4667	14.4416					 					
66.006	72.4795	21.25					 L					
169.6024	98.3835	23.2016					 					
	188.9514	25.7567					 					
	228.1191	57.6914					 					
747.3958	472.309	161.199										
	542.8395	213.563										
		1 145.2239					 					
		1530.8733					 					
		1631.1368					 					
		1795.8049					 					
		2049.4273					 					
		2686.2033					 					
		2855.1948										
3469.24		3805.9691					 					
	9999.785						 					
	10923.76	12312.46					 					
		16991.308					 					
10400.45	15384.06	24172.201										

Repair							T	T		True Logno	rmal Mean:	850
Repair PDI	F			(Top Weib	uli++ Selec	tion)				rue Lognom		90
5 Data Poi	nts				Fitting Par			(Empirical		e Lognorma		8100
Set1	Set2	Set3			Rep2	Rep3			Fitting Par			
747.1571	850.0651	772.8667	N Mean		•			Rep1	Rep2	Rep3		
828.7058	935.5551	827.0410	N S.D.							an for Norm	al variates:	6.739662
830.6967	957.0606	937.0020	LogN Mean	1	1	1		(Empirical		ar for Norm		0.011149
833.6765		978.3519		0	0	0		-p		ev for Norma		0.105587
902.3605	988.9605	1027.9719										
		1	Veibull Shape	8.4598	27.9086		Normal					
			Scale	384.543	963.8849	908.6467	Mean					
			Location	465.21	0	94.8652	SD					
Repair PD	-			(Top Weib	uli++ Selec	tion)		(Empirical)				
25 Data Po	ints			High Level	Fitting Par	ameters		Low Level	Fitting Par	ameters		
Set1	Set2	Set3		Rep1	Rep2	Rep3		Rep1	Rep2	Rep3		
642.7415	691.2975	674.5797	N Mean	6.7196		6.7245		1				
696.8263	723.6644	683.9227	N S.D.	0.1017	0.09473	0.1036		(Empirical)				
728.8017	735.9082	711.2389	LogN Mean	832.7816	838.8122	837.0355						
745.0789	738.2158	752.3358	LogN S.D.	84.91336	79.63928	86.95008						
773.4927	739.9673	779.8016										
774.3035	763.4049	786.2454	Veibull Shape									
792.5570	771.2505	787.2781	Scale									
792.6556	817.6816	795.3255	Location									
811.2078	822.2252	798.9932										
811.2933	823.0084	802.8723										
814.0875	827.8375	805.9737						1				
815.4539	831.2502	817.539										
830.9855	834.2116	838.9178										
834.2839	843.8531	843.2974				-						
858.9568	851.4224	843.6612										
862.9996		844.3625										
867.1553	862.0037	870.6218					_					
872.307	862.5475	878.4302										
873.9636		885.2466										
883.4647	936.0016	886.0297										
884.7831	941.7188	917.3511										
906.1892	943.284	940.4368										
940.6469		958.6495										
943.1421		1000.5771										
1061.907	964.0956	1022.3195						1				

Component 6:

IFR Failure					l	1	I	T	r			
n n n andre											TRUE IFR	
Failure PDF	<u>-</u>			(Top Weib	ull++ Selec	tion)		(Weibull++	Exponenti	al)	Weibull	
5 Data Poin				High Level					Fitting Para		Shape	1.9
Set1	Set2	Set3		Rep1	Rep2	Rep3	 	Rep1	Rep2	Rep3	Scale	3333
943.0678	1272.6057	1373,1654	Shape				 Lambda	0.0005				(
2219.2323	1816.7934	2175.7739	Scale			2673.545	 mean		3333.333			
2853.3978	2781.1238	2552.2985	Location	0	1065.907	0	 Location	864.6482	519.5057			
3069.4	4368.796	2779.7657					 	1			1	
5680.3975	7831.8613	3285.1362										
							 <u> </u>					
Failure PDF				(Top Weib					Exponenti			
25 Data Poi				High Level					Fitting Para			
		Set3				Rep3				Rep3		
556.924	478.1575		Shape				Lambda	0.0004				
888.1491			Scale		3112.881	3793.36	mean	2500				
980.9987	835.3915		Location	151.86	0	0	Location	556.924	478.1575	338.3958		
	1028.4228											
	1252.9216											
1554.7179								L				
	1326.7294							L				
	1403.6103											
2333.6979		2704.5543										
2639.6742		3017.2549										
	1971.7594	3194.8691										
	3073.1181	3298.5318										
		3363.2244										
2911.8353		3371.6199										
	3451.9756	3503.761										
	3453.6347	3767.7098										
	3474.3802	3811.3404										
		3829.0021										
4454.7244	3609.0219	3895.2994										
	3828.5382	4917.9287										
	3974.7389	5125.8579										
	4201.9076	5385.3977										
6572.5149	4593.8342	5832.9327										
	5073.4553	5849.498										
7321.4379	6986.9939	8078.036										

DFR Failur	e												
												TRUE DF	R PARAME
Failure PDF				(Top Weib	ull++ Selec	tion)			(Weibull++	Exponenti	al)	Weibull	
5 Data Poin	its			High Level	Fitting Par	ameters			LowLevel	Fitting Para	meters	Shape	0.7
Set1	Set2	Set3		Rep1	Rep2	Rep3			Rep1	Rep2	Rep3	Scale	2336
126.6007	132.5105		Shape	0.8337	0.7236			Lamoda	0.0001	0.0003	0.0012	Location	0
3871.6142	151.9939	542.8767	Scale	7308.818	2441.373			mean	10000	3333.333	833.3333		
4941.3851	1810.4893	1450.5999	Location	0	Ō			Location	0	0	347.763		
8492.4261	5181.3916	1450.9201											
22172.966	7327.3941	1977.9812					Normal	1					
						1178.198	Mean						
						582.3018	SD						
Failure PDF				(Top Weib	ull++ Selec	tion)				Exponenti			
25 Data Poi				High Level		ameters			LowLevel	Fitting Para	meters		
Set1		Set3				Rep3			Rep1	Rep2	Rep3		
3.9292	50.9178	2.0586	Shape					Lambda	0.0003		0.0003		
49.8137	62.3909	4.4384	Scale	2679.482	2139.152	2139.572		mean	3333,333	2500	3333.333		
61.4687	116.6026	62.1906	Location	0	44.271	0		Location	0	0	0		
302.8609		170.9058											
318.0808		173.6596											
448.9909		174.1197											
	541.5138	348.7671											
609.2363		638.6683											
754.8118		641.4655											
	1030.7575	697.9511											
	1209.2986	1150.9406											
	1575.5976	1324.3103											
	1681.0466	1527.1351											
	1915.0946	1677.1838											
	1927.3436	1803.4187											
	1932.9038	1816.459	-										
	2428.3783												
	2650.1936	2704.6759											
	2672.4901	3679.97											
	2715.7387	4895.6748											
	2867.5279								L				
	3093.7406												
	8740.5562	6360.7816											
	12507.125	6552.6711											
12761.655	19032.824	21372.6813								L			

Repair										True Logno	mal Mean:	3000
Repair PDF				(Top Weib	ull++ Selec	tion)				rue Lognorr		125
5 Data Poin					Fitting Par			(Empirical)		e Lognorma		15625
Set1	Set2	Set3		Rep1	Rep2	Rep3		Low Level				
2928.2077	2937.2639	2727.4405	N Mean						Rep2	Rep3		
2955.5721	3008.5301	2758.0500	NS.D.							an for Norm	al variates:	8.0055
3118.5662	3023.0372	3009.5544	LogN Mean	1	1	1		(Empirical)	V	ar for Norm	al variates:	0.001735
3192.1467	3067.5622	3059.0098	LogN S.D.	0	0	0		1	St De	v for Norm	al Variates:	0.041649
3339.1724	3123.3886	3116.5662										
		V	Veibull Shape	2.9516			Normal					
			Scale	456.2813	3031.956	2934.124	Mean					
			Location	2701.37	66.0042	160.18	SD					
Repair PDF				(Top Weib	ull++ Selec	tion)		(Empirical)				
25 Data Poi	nts			High Level	Fitting Para	ameters		Low Level	Fitting Para	meters		
Set1	Set2	Set3		Rep1	Rep2	Rep3		Rep1	Rep2	Rep3		
2725.9674	2758.7299	2741.9086	N Mean									
2729.9413		2747.9049						(Empirical)	I			
	2780.2585	2794.2454		1	1	1						
2801.4099		2891.3966	LogN S.D.	0	0	0						
2833.9725		2930.3131										
	2896.7268		Veibull Shape	5.9116			Normal					
2920.6486		2965.6203	Scale	856.388	630.048	3032.937						
2930.9072	2934.3030	2976.0747	Location	2214.95	2420.89	145.72	SD					
2935.5857	2944.4503	2985.9873										
2941.8176	2948.8804	2997.5822										
2970.6641	2960.577	3001.2277										
3004.238		3011.5071										
3022.9127	2980.7188	3024.4465										
3034.4321	3026.4141	3044.4719										
3089.3571	3030.2903	3059.7489										
	3035.5214	3071.8224										
3107.0562		3080.8281										
3110.1218	3089.8191	31 19.0444										
31 16.66 1	3089.8886	3122.4055										
3122.7704	3097.7068	3165.1266										
3135.9401	31 17.2651	3171.3008										
3170.1508	31 26.96 59	3187.1087										
3201.7674	31 53.7086	3197.7748										
3202.9599	31 79.33 16	3213.9189										
3321.2597	3345.2504	3374.7772										

Component 7:

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IFR Failur	re		ļ										DADAME
E-11-00				The late the	0.1.	1			1141-11-11			TRUE IFR Weibull	PARAME
Failure PD					ull++ Selec					Exponenti		Shape	1.2
5 Data Po Set1	Set2	Set3		Rept	Fitting Par	Rep3				Fitting Para Rep2	Rep3	Scale	2575
	755.0101		Shape					Lambda	0.0011	0.0002		Location	2010
	1517.403					1953.159		mean	909.0909	50002			
	3151.586					212.1063	··· ····	Location	960.43		27.5108		
	3215.274		Looditon					Loodinori			27.0100		
	11455.09								-				
Failure PD)F				ull++ Selec				(Weibull++				
25 Data Po	oints				Fitting Par				Low Level		meters		
Set1	Set2	Set3			Rep2	Rep3					Rep3		
75.305		28.3818						Lambda	0.0004				
163.5098		351.9838		2989.621				mean	2500	2500			
234.3425			Location	0	0	0		Location	75.305	11.1745	28.3818		
273.5559													
703.7099		780.3233											
862.866													
999.166													
1593.052		1250.599	ļ	ļ		L							
1876.896						ļ							
2199.876				L					ļ				
2224.738		1971.803							ļ			ļ	
2360.094		2005.742										<u> </u>	
2548.09		2273.373			I								
	2409.684				 						<u> </u>		
	2631.809												
	2892.163				·								
3737.317		2640.37									·		
4502.703													
	3224.334												
4518.089													
	3975.867 5169.694												
		5547.4											
	5926.245 6115.789												
	0110.705	0000.202											
6102 1/6	70/2 011	6864 031											
	7042.011	6864.931											
6192.146 DFR Failu		6864.931											
DFR Failu	re	6864.931		(Top Weib	ull++ Selec	tion)			(Weibull++	Exponenti		TRUE DFF Weibull	R PARAME
DFR Failu Failure PD	re 	6864.931			ull++ Selec					Exponentia Fitting Para	al)	Weibull	
DFR Failu Failure PD 5 Data Poi	re F nts			High Level	Fitting Par	ameters			Low Level	Fitting Para	al)		R PARAME 0.55 1423
DFR Failu Failure PD 5 Data Poi	re F nts Set2	Set3	Shape	High Level	Fitting Par Rep2	ameters Rep3		Lambda	Low Level	Fitting Para Rep2	al) meters Rep3	Weibull Shape	0.55
DFR Failu Failure PD 5 Data Poi Set1	re F nts Set2 6.0805	Set3		High Level Rep1	Fitting Par Rep2 0.3562	ameters Rep3 0.5816		Lambda mean	Low Level Rep1 0.0002	Fitting Para Rep2	al) meters Rep3 0.0007	Weibull Shape Scale	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924	re IF Set2 6.0805 16.1423 37.7049	Set3 33.8777 340.1097		High Level Rep1 0.3744	Fitting Par Rep2 0.3562 181.6411	ameters Rep3 0.5816			Low Level Rep1 0.0002	Fitting Para Rep2 0.0014	al) meters Rep3 0.0007	Weibull Shape Scale	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097	re If Set2 6.0805 16.1423 37.7049 385.8074	Set3 33.8777 340.1097 370.6554 897.4695	Scale	High Level Rep1 0.3744 1592.354	Fitting Par Rep2 0.3562 181.6411	ameters Rep3 0.5816 928.9105		mean	Low Level Rep1 0.0002 5000	Fitting Para Rep2 0.0014 714.2857	al) meters Rep3 0.0007	Weibull Shape Scale	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924	re If Set2 6.0805 16.1423 37.7049 385.8074	Set3 33.8777 340.1097 370.6554	Scale	High Level Rep1 0.3744 1592.354	Fitting Par Rep2 0.3562 181.6411	ameters Rep3 0.5816 928.9105		mean	Low Level Rep1 0.0002 5000	Fitting Para Rep2 0.0014 714.2857	al) meters Rep3 0.0007	Weibull Shape Scale	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097	re If Set2 6.0805 16.1423 37.7049 385.8074	Set3 33.8777 340.1097 370.6554 897.4695	Scale	High Level Rep1 0.3744 1592.354	Fitting Par Rep2 0.3562 181.6411	ameters Rep3 0.5816 928.9105		mean	Low Level Rep1 0.0002 5000	Fitting Para Rep2 0.0014 714.2857	al) meters Rep3 0.0007	Weibull Shape Scale	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097	re If Set2 6.0805 16.1423 37.7049 385.8074	Set3 33.8777 340.1097 370.6554 897.4695	Scale	High Level Rep1 0.3744 1592.354	Fitting Par Rep2 0.3562 181.6411	ameters Rep3 0.5816 928.9105		mean	Low Level Rep1 0.0002 5000	Fitting Para Rep2 0.0014 714.2857	al) meters Rep3 0.0007	Weibull Shape Scale	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097 11366.33	re F Set2 6.0805 16.1423 37.7049 385.8074 3016.537	Set3 33.8777 340.1097 370.6554 897.4695	Scale	High Level Rep1 0.3744 1592.354 491.84	Fitting Par Rep2 0.3562 181.6411 5.91	ameters Rep3 0.5816 928.9105 24.41		mean	Low Level Rep1 0.0002 5000 0	Fitting Para Rep2 0.0014 714.2857 0	al) meters Rep3 0.0007 1428.571	Weibull Shape Scale	0.55
DFR Failu Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097 11366.33 Failure PD	re F set2 6.0805 16.1423 37.7049 385.8074 3016.537 F	Set3 33.8777 340.1097 370.6554 897.4695	Scale Location	High Level Rep1 0.3744 1592.354 491.84 (Top Weibt	Fitting Par Rep2 0.3562 181.6411 5.91	ameters Rep3 0.5816 928.9105 24.41		mean	Low Level Rep1 0.0002 5000 0 	Fitting Pare Rep2 0.0014 714.2857 0 Exponentia	al) meters Rep3 0.0007 1428.571	Weibull Shape Scale	0.55
DFR Failure PD 5 Data Poi 5 Data Poi 526.3141 1281.924 9009.097 11366.33 Failure PD 25 Data Pc	re F nts Set2 6.0805 16.1423 37.7049 385.8074 3016.537 5 F pints	Set3 33.8777 340.1097 370.6554 897.4695 5712.437	Scale Location	High Level Rep1 0.3744 1592.354 491.84 (Top Weibh High Level	Fitting Par Rep2 0.3562 181.6411 5.91 Ull++ Selec Fitting Par	ameters Rep3 0.5816 928.9105 24.41 		mean Location	Low Level Rep1 0.0002 5000 0 0 (Weibull++ Low Level	Fitting Pare Rep2 0.0014 714.2857 0 Exponentia Fitting Pare	al) meters Rep3 0.0007 1428.571	Weibull Shape Scale	0.55
DFR Failure PD 5 Data Poi 5 Set1 492.9745 526.3141 1281.924 9009.097 11366.33 Failure PD 25 Data Pc Set1	re F nts Set2 6.0805 16.1423 37.7049 385.8074 3016.537 Set2 Set2	Set3 33.8777 340.1097 370.6554 897.4695 5712.437 Set3	Scale Location	High Level Rep1 0.3744 1592.354 491.84 (Top Weib High Level Rep1	Fitting Par Rep2 0.3562 181.6411 5.91 Ull++ Select Fitting Par Rep2	ameters Rep3 0.5816 928.9105 24.41 24.41 (in) ameters Rep3		mean Location	Low Level Rep 1 0.0002 5000 0 (Weibull++ Low Level Rep 1	Fitting Para Rep2 0.0014 714.2857 0 Exponentia Fitting Para Rep2	al) meters Rep3 0.0007 1428.571 1428.571 1428.571 al) meters Rep3	Weibull Shape Scale Location	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097 11366.33 Failure PD 25 Data Pc Set1 0.2394	re F nts Set2 6.0805 16.1423 37.7049 385.8074 3016.537 F Dints Set2 1.6826	Set3 33.8777 340.1097 370.6554 897.4695 5712.437 5712.437 Set3 1.4205	Scale Location	High Level Rep1 0.3744 1592.354 491.84 (Top Weib High Level Rep1 0.5956	Fitting Par Rep2 0.3562 181.6411 5.91 Ull++ Select Fitting Par Rep2 0.5474	ameters Rep3 0.5816 928.9105 24.41 24.41 (in) ameters Rep3 0.6307		mean Location Lambda	Low Level Rep 1 0.0002 5000 0 0 (Weibull++ Low Level Rep 1 0.0004	Fitting Para Rep2 0.0014 714.2857 0 Exponentia Fitting Para Rep2 0.0004	al) meters Rep3 0.0007 1428.571 1428.57	Weibull Shape Scale Location	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097 11366.33 Failure PD 25 Data PC Set1 0.2394 34.385	re F nts Set2 6.0805 16.1423 37.7049 385.8074 3016.537 F F Set2 1.6826 2.2468	Set3 33.8777 370.6554 597.4695 5712.437 Set3 1.4205 4.2473	Scale Location Shape Scale	High Level Rep1 0.3744 1592.354 491.84 (Top Weib High Level Rep1 0.5956 1671.235	Fitting Par Rep2 0.3562 181.6411 5.91 UIL++ Selec Fitting Par Rep2 0.5474 1783.465	ameters Rep3 0.5816 928.9105 24.41 		mean Location Lambda mean	Low Level Rep 1 0.0002 5000 0 0 (Weibull++ Low Level Rep 1 0.0004 2500	Fitting Para Rep2 0.0014 714.2857 0 Exponentia Fitting Para Rep2 0.0004 2500	al) meters Rep3 0.0007 1428.571 1428.571 1428.571 al) neters Rep3 0.0006 1666.667	Weibull Shape Scale Location	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097 11366.33 Failure PD 25 Data PC Set1 0.2394 34.385 49.2658	re rF nts Set2 6.0805 16.1423 37.7049 385.8074 3016.537 Set2 1.6826 2.2468 8.1568	Set3 33.8777 340.1097 370.6554 897.4695 5712.437 Set3 1.4205 4.2473 23.3267	Scale Location Shape Scale	High Level Rep1 0.3744 1592.354 491.84 (Top Weib High Level Rep1 0.5956	Fitting Par Rep2 0.3562 181.6411 5.91 UIL++ Selec Fitting Par Rep2 0.5474 1783.465	ameters Rep3 0.5816 928.9105 24.41 		mean Location Lambda	Low Level Rep 1 0.0002 5000 0 0 (Weibull++ Low Level Rep 1 0.0004	Fitting Para Rep2 0.0014 714.2857 0 Exponentia Fitting Para Rep2 0.0004	al) meters Rep3 0.0007 1428.571 1428.571 1428.571 al) neters Rep3 0.0006 1666.667	Weibull Shape Scale Location	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097 11366.33 Failure PD 25 Data Pc Set1 0.2394 49.2658 55.1196	re re set2 6.0805 16.1423 37.7049 385.8074 3016.537 Set2 1.6826 2.2468 8.1568 9.7845	Set3 33.8777 340.1097 370.6554 897.4695 5712.437 5712.437 5712.437 1.4205 4.2473 23.3267 59.4448	Scale Location Shape Scale	High Level Rep1 0.3744 1592.354 491.84 (Top Weib High Level Rep1 0.5956 1671.235	Fitting Par Rep2 0.3562 181.6411 5.91 UIL++ Selec Fitting Par Rep2 0.5474 1783.465	ameters Rep3 0.5816 928.9105 24.41 		mean Location Lambda mean	Low Level Rep 1 0.0002 5000 0 0 (Weibull++ Low Level Rep 1 0.0004 2500	Fitting Para Rep2 0.0014 714.2857 0 Exponentia Fitting Para Rep2 0.0004 2500	al) meters Rep3 0.0007 1428.571 1428.571 1428.571 al) neters Rep3 0.0006 1666.667	Weibull Shape Scale Location	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097 11366.33 Failure PD 25 Data Pc Set1 0.2394 34.385 49.2658 55.1196 147.6313	re F nts Set2 6.0805 16.1423 37.7049 385.8074 3016.537 Set2 1.6826 2.2468 8.1568 9.7845 57.1513	Set3 33.8777 340.1097 370.6554 897.4695 5712.437 55712.437 597.488 1.4205 4.2473 23.3267 59.4488 105.133	Scale Location Shape Scale	High Level Rep1 0.3744 1592.354 491.84 (Top Weib High Level Rep1 0.5956 1671.235	Fitting Par Rep2 0.3562 181.6411 5.91 UIL++ Selec Fitting Par Rep2 0.5474 1783.465	ameters Rep3 0.5816 928.9105 24.41 		mean Location Lambda mean	Low Level Rep 1 0.0002 5000 0 0 (Weibull++ Low Level Rep 1 0.0004 2500	Fitting Para Rep2 0.0014 714.2857 0 Exponentia Fitting Para Rep2 0.0004 2500	al) meters Rep3 0.0007 1428.571 1428.571 1428.571 al) neters Rep3 0.0006 1666.667	Weibull Shape Scale Location	0.55
DFR Failure PD 5 Data PO Set1 492.9745 526.3141 1281.924 9009.097 11366.33 Failure PD 25 Data PC Set1 0.2394 34.385 49.2658 55.1196 147.6313 215.7498	re F nts Set2 6.0805 16.1423 37.7049 385.8074 3016.537 Set2 1.6826 2.2468 8.1568 9.7845 57.1513 92.2753	Set3 33.8777 340.1097 370.6554 5712.437 5712.437 Set3 1.4205 4.2473 23.3267 59.4488 105.133 180.356	Scale Location Shape Scale	High Level Rep1 0.3744 1592.354 491.84 (Top Weib High Level Rep1 0.5956 1671.235	Fitting Par Rep2 0.3562 181.6411 5.91 UIL++ Selec Fitting Par Rep2 0.5474 1783.465	ameters Rep3 0.5816 928.9105 24.41 		mean Location Lambda mean	Low Level Rep 1 0.0002 5000 0 0 (Weibull++ Low Level Rep 1 0.0004 2500	Fitting Para Rep2 0.0014 714.2857 0 Exponentia Fitting Para Rep2 0.0004 2500	al) meters Rep3 0.0007 1428.571 1428.571 1428.571 al) neters Rep3 0.0006 1666.667	Weibull Shape Scale Location	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097 11366.33 Failure PD 25 Data Pc Set1 0.2394 34.385 49.2658 55.1196 147.6313	re F nts Set2 6.0805 16.1423 37.7049 385.8074 3016.537 3016.537 Set2 1.6826 2.2468 8.1568 9.7845 57.1513 92.2753 188.8081	Set3 33.8777 340.1097 370.6554 997.4695 5712.437 597.4495 5712.437 597.4495 14.2473 23.3267 59.4488 105.133 180.356 202.0613	Scale Location Shape Scale	High Level Rep1 0.3744 1592.354 491.84 (Top Weib High Level Rep1 0.5956 1671.235	Fitting Par Rep2 0.3562 181.6411 5.91 UIL++ Selec Fitting Par Rep2 0.5474 1783.465	ameters Rep3 0.5816 928.9105 24.41 		mean Location Lambda mean	Low Level Rep 1 0.0002 5000 0 0 (Weibull++ Low Level Rep 1 0.0004 2500	Fitting Para Rep2 0.0014 714.2857 0 Exponentia Fitting Para Rep2 0.0004 2500	al) meters Rep3 0.0007 1428.571 1428.571 1428.571 al) neters Rep3 0.0006 1666.667	Weibull Shape Scale Location	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097 11366.33 Failure PD 25 Data Pc Set1 0.2394 34.385 49.2658 55.1196 147.6313 215.7498	re F ris Set2 6.0805 16.1423 37.7049 385.8074 3016.537 3016.537 Set2 1.6826 2.2468 8.1568 9.7845 57.1513 92.2753 188.8081 457.0314	Set3 33.8777 340.1097 370.6554 997.4695 5712.437 597.4495 5712.437 597.4495 14.2473 23.3267 59.4488 105.133 180.356 202.0613	Scale Location Shape Scale	High Level Rep1 0.3744 1592.354 491.84 (Top Weib High Level Rep1 0.5956 1671.235	Fitting Par Rep2 0.3562 181.6411 5.91 UIL++ Selec Fitting Par Rep2 0.5474 1783.465	ameters Rep3 0.5816 928.9105 24.41 		mean Location Lambda mean	Low Level Rep 1 0.0002 5000 0 0 (Weibull++ Low Level Rep 1 0.0004 2500	Fitting Para Rep2 0.0014 714.2857 0 Exponentia Fitting Para Rep2 0.0004 2500	al) meters Rep3 0.0007 1428.571 1428.571 1428.571 al) neters Rep3 0.0006 1666.667	Weibull Shape Scale Location	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097 11366.33 711366.33 711366.33 711366.33 711366.33 711366.33 711366.33 711366.33 711561 715	re F nts Set2 6.0805 16.1423 37.7049 385.8074 3016.537 9385.8074 3016.537 5.8074 3.8074 3.8076 3.8074 3.8076 3	Set3 33.8777 340.1097 370.6554 897.4695 5712.437 5712.437 1.4205 4.2473 23.3267 59.4488 105.133 180.356 202.0613 202.0613	Scale Location Shape Scale	High Level Rep1 0.3744 1592.354 491.84 (Top Weib High Level Rep1 0.5956 1671.235	Fitting Par Rep2 0.3562 181.6411 5.91 UIL++ Selec Fitting Par Rep2 0.5474 1783.465	ameters Rep3 0.5816 928.9105 24.41 		mean Location Lambda mean	Low Level Rep 1 0.0002 5000 0 0 (Weibull++ Low Level Rep 1 0.0004 2500	Fitting Para Rep2 0.0014 714.2857 0 Exponentia Fitting Para Rep2 0.0004 2500	al) meters Rep3 0.0007 1428.571 1428.571 1428.571 al) neters Rep3 0.0006 1666.667	Weibull Shape Scale Location	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097 11366.33 71366.33 71366.33 71366.33 71366.33 71366.33 71366.33 71366.33 71366.33 71366.33 715.7498 717.501 717.7498 727.1501 7301.8768 352.9605	re F nts Set2 6.0805 16.1423 37.7049 385.8074 3016.537 Set2 1.6826 2.2468 8.1568 9.7845 57.1513 92.2753 188.8081 457.0314 483.8325 655.3901	Set3 33.8777 340.1097 370.6554 897.4695 5712.437 25712.437 23.3267 59.4488 105.133 180.356 202.0613 205.8487 205.8487 205.8487	Scale Location Shape Scale	High Level Rep1 0.3744 1592.354 491.84 (Top Weib High Level Rep1 0.5956 1671.235	Fitting Par Rep2 0.3562 181.6411 5.91 UIL++ Selec Fitting Par Rep2 0.5474 1783.465	ameters Rep3 0.5816 928.9105 24.41 		mean Location Lambda mean	Low Level Rep 1 0.0002 5000 0 0 (Weibull++ Low Level Rep 1 0.0004 2500	Fitting Para Rep2 0.0014 714.2857 0 Exponentia Fitting Para Rep2 0.0004 2500	al) meters Rep3 0.0007 1428.571 1428.571 1428.571 al) neters Rep3 0.0006 1666.667	Weibull Shape Scale Location	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097 11366.33 711567.35 71157.35 71157.55 715	re F IF IS Set2 6.0805 16.1423 37.7049 385.8074 3016.537 Set2 1.6826 2.2468 8.1568 9.7845 57.1513 92.2753 188.8081 457.0314 483.8325 655.3901	Set3 33.8777 340.1097 370.6554 897.4685 5712.437 5712.437 23.267 4.2473 23.3267 59.4488 105.133 180.356 202.0613 205.8487 260.4402 310.1456	Scale Location Shape Scale	High Level Rep1 0.3744 1592.354 491.84 (Top Weib High Level Rep1 0.5956 1671.235	Fitting Par Rep2 0.3562 181.6411 5.91 UIL++ Selec Fitting Par Rep2 0.5474 1783.465	ameters Rep3 0.5816 928.9105 24.41 		mean Location Lambda mean	Low Level Rep 1 0.0002 5000 0 0 (Weibull++ Low Level Rep 1 0.0004 2500	Fitting Para Rep2 0.0014 714.2857 0 Exponentia Fitting Para Rep2 0.0004 2500	al) meters Rep3 0.0007 1428.571 1428.571 1428.571 al) neters Rep3 0.0006 1666.667	Weibull Shape Scale Location	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097 11366.33 711366.33 711366.33 711366.33 725 Data PC Set1 0.2394 3.435 55.1196 147.6313 215.7498 352.9605 359.6454 359.06454 359.06454 359.06454	re re Set2 6.0805 16.1423 37.7049 385.8074 3016.537 3016.537 5612 1.6826 2.2468 8.1568 9.7845 57.1513 92.2753 188.8081 457.0314 483.8325 655.3901 888.7466	Set3 33.8777 340.1097 370.6554 997.4695 5712.437 597.4695 5712.437 2012 4.2473 23.3267 59.4488 105.133 180.356 202.0613 205.8487 260.4402 310.1456 440.4745	Scale Location Shape Scale	High Level Rep1 0.3744 1592.354 491.84 (Top Weib High Level Rep1 0.5956 1671.235	Fitting Par Rep2 0.3562 181.6411 5.91 UIL++ Selec Fitting Par Rep2 0.5474 1783.465	ameters Rep3 0.5816 928.9105 24.41 		mean Location Lambda mean	Low Level Rep 1 0.0002 5000 0 0 (Weibull++ Low Level Rep 1 0.0004 2500	Fitting Para Rep2 0.0014 714.2857 0 Exponentia Fitting Para Rep2 0.0004 2500	al) meters Rep3 0.0007 1428.571 1428.571 1428.571 al) neters Rep3 0.0006 1666.667	Weibull Shape Scale Location	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097 11366.33 71366.33 71366.33 71366.33 71366.33 71366.33 71366.33 71366.33 71366.33 715.7498 721.5501 301.8768 352.9605 359.6454 399.631 507.7724 756.2171	re re set2 6.0805 16.1423 37.7049 385.8074 3016.537 3016.537 5et2 1.6826 2.2468 8.1568 9.7845 57.1513 92.2753 188.8081 457.0314 483.8325 665.3901 888.7466 1068.396	Set3 33.8777 340.1097 370.6554 897.4695 5712.437 5712.437 1.4205 4.2473 23.3267 59.4488 105.133 180.356 202.0613 202.6437 260.4402 310.1456 440.4745 553.3837	Scale Location Shape Scale	High Level Rep1 0.3744 1592.354 491.84 (Top Weib High Level Rep1 0.5956 1671.235	Fitting Par Rep2 0.3562 181.6411 5.91 UIL++ Selec Fitting Par Rep2 0.5474 1783.465	ameters Rep3 0.5816 928.9105 24.41 		mean Location Lambda mean	Low Level Rep 1 0.0002 5000 0 0 (Weibull++ Low Level Rep 1 0.0004 2500	Fitting Para Rep2 0.0014 714.2857 0 Exponentia Fitting Para Rep2 0.0004 2500	al) meters Rep3 0.0007 1428.571 1428.571 1428.571 al) neters Rep3 0.0006 1666.667	Weibull Shape Scale Location	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097 11366.33 Failure PD 25 Data Pc Set1 0.2394 34.385 49.2658 55.1196 147.6313 215.7498 271.5501 301.8768 352.9605 359.6454 399.0531 507.724 756.2171 1014.603	re F f nts Set2 6.0805 16.1423 37.7049 385.8074 3016.537 3016.537 5612 1.6826 2.2468 8.1568 9.7845 57.1513 92.2753 188.8081 457.0314 483.8325 655.3901 888.7466 1068.396 1217.062	Set3 33.8777 340.1097 370.6554 897.4695 5712.437 5712.437 23.3267 59.4488 105.133 180.356 202.0613 205.8487 205.8487 205.8487 205.8487 205.8487 265.4402 310.1456 440.4745 553.3837 698.8552	Scale Location Shape Scale	High Level Rep1 0.3744 1592.354 491.84 (Top Weib High Level Rep1 0.5956 1671.235	Fitting Par Rep2 0.3562 181.6411 5.91 UIL++ Selec Fitting Par Rep2 0.5474 1783.465	ameters Rep3 0.5816 928.9105 24.41 		mean Location Lambda mean	Low Level Rep 1 0.0002 5000 0 0 (Weibull++ Low Level Rep 1 0.0004 2500	Fitting Para Rep2 0.0014 714.2857 0 Exponentia Fitting Para Rep2 0.0004 2500	al) meters Rep3 0.0007 1428.571 1428.571 1428.571 al) neters Rep3 0.0006 1666.667	Weibull Shape Scale Location	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097 11366.33 Failure PD 25 Data Pc Set1 0.2394 34.385 49.2658 55.1196 147.6313 215.7498 271.5501 301.8768 352.9605 359.6454 399.0531 507.724 756.2171 1014.603	re re Set2 6.0805 16.1423 37.7049 385.8074 3016.537 3016.537 5612 1.6826 2.2468 8.1568 9.7845 57.1513 92.2753 188.8081 457.0314 483.8325 555.3901 888.7466 1068.396 1217.062 1854.382 1965.781	Set3 33.8777 340.1097 370.6554 897.4695 5712.437 Set3 1.4205 4.2473 23.3267 59.4488 105.133 180.356 202.0613 205.8487 260.4402 553.3837 698.8552 782.0061	Scale Location Shape Scale	High Level Rep1 0.3744 1592.354 491.84 (Top Weib High Level Rep1 0.5956 1671.235	Fitting Par Rep2 0.3562 181.6411 5.91 UIL++ Selec Fitting Par Rep2 0.5474 1783.465	ameters Rep3 0.5816 928.9105 24.41 		mean Location Lambda mean	Low Level Rep 1 0.0002 5000 0 0 (Weibull++ Low Level Rep 1 0.0004 2500	Fitting Para Rep2 0.0014 714.2857 0 Exponentia Fitting Para Rep2 0.0004 2500	al) meters Rep3 0.0007 1428.571 1428.571 1428.571 al) neters Rep3 0.0006 1666.667	Weibull Shape Scale Location	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 11281.924 9009.097 11366.33 711366.33 711366.33 711366.33 711366.33 711366.33 711366.33 711366.33 711366.33 725 Data PO 25 Data PO 26 Data PO 26 Data PO 27 Data PO 26 Data	re re set2 6.0805 16.1423 37.7049 385.8074 3016.537 3016.537 5et2 1.6826 2.2468 8.1568 9.7845 57.1513 92.2753 188.8081 457.0314 483.8325 655.3901 888.7466 1068.396 1217.062 1865.781 2178.458	Set3 33.8777 340.1097 370.6554 997.4695 5712.437 597.4695 5712.437 23.267 4.2473 23.3267 59.4488 105.133 180.356 202.0613 205.8487 260.4402 310.1456 310.1455 553.3837 698.8552 782.0061 845.8762	Scale Location Shape Scale	High Level Rep1 0.3744 1592.354 491.84 (Top Weib High Level Rep1 0.5956 1671.235	Fitting Par Rep2 0.3562 181.6411 5.91 UIL++ Selec Fitting Par Rep2 0.5474 1783.465	ameters Rep3 0.5816 928.9105 24.41 		mean Location Lambda mean	Low Level Rep 1 0.0002 5000 0 0 (Weibull++ Low Level Rep 1 0.0004 2500	Fitting Para Rep2 0.0014 714.2857 0 Exponentia Fitting Para Rep2 0.0004 2500	al) meters Rep3 0.0007 1428.571 1428.571 1428.571 al) neters Rep3 0.0006 1666.667	Weibull Shape Scale Location	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097 11366.33 711366.33 711366.33 711366.33 725 Data PC Set1 0.2394 9.2658 55.1196 147.6313 215.7498 352.9605 359.6454 352.9605 359.6454 359.9655 359.6454 359.9655 359.6454 359.6556 359.6454 359.6556 359.6454 359.6556 359.6556 359.6556 359.6556 359.6556 359.6556 359.6556 359.6556 359.6556 359.65666 359.65666 359.65666 359.656666666666666666666666666666666666	re F f nts Set2 6.0805 16.1423 37.7049 385.8074 3016.537 3016.537 5 5 5 5 5 5 5 5 5 5 5 5 5	Set3 33.8777 340.1097 370.6554 897.4695 5712.437 5712.437 1.4205 4.2473 23.3267 59.4488 105.133 180.356 202.0613 202.6402 310.1456 440.4745 553.3837 698.8552 782.0061 845.8762 1603.001	Scale Location Shape Scale	High Level Rep1 0.3744 1592.354 491.84 (Top Weib High Level Rep1 0.5956 1671.235	Fitting Par Rep2 0.3562 181.6411 5.91 UIL++ Selec Fitting Par Rep2 0.5474 1783.465	ameters Rep3 0.5816 928.9105 24.41 		mean Location Lambda mean	Low Level Rep 1 0.0002 5000 0 0 (Weibull++ Low Level Rep 1 0.0004 2500	Fitting Para Rep2 0.0014 714.2857 0 Exponentia Fitting Para Rep2 0.0004 2500	al) meters Rep3 0.0007 1428.571 1428.571 1428.571 al) neters Rep3 0.0006 1666.667	Weibull Shape Scale Location	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097 11366.33 711567.72 71157.72 7	re F f nts Set2 6.0805 16.1423 37.7049 385.8074 3016.537 3016.537 5.8074 3016.537 5.8074 3016.537 5.8074 3016.537 5.812 1.6826 2.2468 8.1568 8.1568 8.1568 8.1568 8.1568 8.1563 9.7845 57.1513 92.2753 188.8081 483.8325 655.3901 888.7466 1068.396 1217.062 1854.382 1965.781 2178.458 2284.18	Set3 33.8777 340.1097 370.6554 897.4695 5712.437 5712.437 1.4205 4.2473 23.3267 59.4488 105.133 180.356 202.0613 205.8437 260.4402 310.1456 440.4745 553.3837 698.8552 782.0061 845.8762 1603.001 1717.026	Scale Location Shape Scale	High Level Rep1 0.3744 1592.354 491.84 (Top Weib High Level Rep1 0.5956 1671.235	Fitting Par Rep2 0.3562 181.6411 5.91 UIL++ Selec Fitting Par Rep2 0.5474 1783.465	ameters Rep3 0.5816 928.9105 24.41 		mean Location Lambda mean	Low Level Rep 1 0.0002 5000 0 0 (Weibull++ Low Level Rep 1 0.0004 2500	Fitting Para Rep2 0.0014 714.2857 0 Exponentia Fitting Para Rep2 0.0004 2500	al) meters Rep3 0.0007 1428.571 1428.571 1428.571 al) neters Rep3 0.0006 1666.667	Weibull Shape Scale Location	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097 11366.33 711366.33 711366.33 711366.33 711366.33 711366.33 711366.33 711366.33 725 Data PC 25 Data PC 271.5501 301.8768 359.6454 359.6454 359.6454 359.6454 359.6454 369.0531 1014.6033 1450.057 1476.586 2169.176 2169.1	re F nts Set2 6.0805 16.1423 37.7049 385.8074 3016.537 Set2 1.6826 2.2468 8.1568 9.7845 67.1513 92.2753 188.8081 457.0314 483.8325 655.3901 888.7466 1068.396 1217.062 1854.382 1965.781 2178.458 2284.18 2074.79	Set3 33.8777 340.1097 370.6554 897.4695 5712.437 Set3 1.4205 4.2473 23.3267 59.4488 105.133 180.356 202.0613 205.8487 260.4402 310.1456 440.4745 553.3837 698.8552 131.1456 440.4745 553.3837 698.8552 1776.2061	Scale Location Shape Scale	High Level Rep1 0.3744 1592.354 491.84 (Top Weib High Level Rep1 0.5956 1671.235	Fitting Par Rep2 0.3562 181.6411 5.91 UIL++ Selec Fitting Par Rep2 0.5474 1783.465	ameters Rep3 0.5816 928.9105 24.41 		mean Location Lambda mean	Low Level Rep 1 0.0002 5000 0 0 (Weibull++ Low Level Rep 1 0.0004 2500	Fitting Para Rep2 0.0014 714.2857 0 Exponentia Fitting Para Rep2 0.0004 2500	al) meters Rep3 0.0007 1428.571 1428.571 1428.571 al) neters Rep3 0.0006 1666.667	Weibull Shape Scale Location	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097 11366.33 711366.33 711366.33 725 Data PC Set1 0.2394 34.385 55.1196 147.6313 215.7498 55.1196 147.6313 301.8768 359.9605 359.6454 359.9605 359.6454 359.9655 359.6454 359.6556 369.6556 369.6556 369.6556 369.6556 369.6556 369.6556 369.655656 369.655656 369.6556565656565656565656565656565656565	re re Set2 6.0805 16.1423 37.7049 385.8074 3016.537 3016.537 5612 1.6826 2.2468 8.1568 9.7845 57.1513 92.2753 188.8081 457.0314 483.8325 555.3901 888.7466 1068.396 1217.062 1854.382 1965.781 2178.458 2284.18 2674.79 2723.829	Set3 33.8777 340.1097 370.6554 997.4695 5712.437 597.4695 5712.437 23.267 4.2473 23.3267 59.4488 105.133 180.356 202.0613 205.8487 260.4402 310.1456 553.3837 698.8552 782.0061 845.8762 1603.001 1717.025 1776.987 1810.474	Scale Location Shape Scale	High Level Rep1 0.3744 1592.354 491.84 (Top Weib High Level Rep1 0.5956 1671.235	Fitting Par Rep2 0.3562 181.6411 5.91 UIL++ Selec Fitting Par Rep2 0.5474 1783.465	ameters Rep3 0.5816 928.9105 24.41 		mean Location Lambda mean	Low Level Rep 1 0.0002 5000 0 0 (Weibull++ Low Level Rep 1 0.0004 2500	Fitting Para Rep2 0.0014 714.2857 0 Exponentia Fitting Para Rep2 0.0004 2500	al) meters Rep3 0.0007 1428.571 1428.571 1428.571 al) neters Rep3 0.0006 1666.667	Weibull Shape Scale Location	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097 11366.33 711367.35 711367.55 711367.55 711367.55 711367.55 711367.55 711367.55 711367.55	re re set2 6.0805 16.1423 37.7049 385.8074 3016.537 3016.537 5et2 1.6826 2.2468 8.1568 9.7845 57.1513 92.2753 188.8081 457.0314 483.8325 655.3901 888.7466 1068.396 1217.062 1854.382 1965.781 2178.458 2284.18 2674.79 4181.331	Set3 33.8777 340.1097 370.6554 897.4695 5712.437 5712.437 23.3267 59.4488 105.133 180.356 202.0613 202.0613 205.8487 260.4402 310.1456 440.4745 553.3837 698.8552 782.0061 845.8762 1603.001 1717.026 1776.987 1810.474 1898.635 2164.609	Scale Location Shape Scale	High Level Rep1 0.3744 1592.354 491.84 (Top Weib High Level Rep1 0.5956 1671.235	Fitting Par Rep2 0.3562 181.6411 5.91 UIL++ Selec Fitting Par Rep2 0.5474 1783.465	ameters Rep3 0.5816 928.9105 24.41 		mean Location Lambda mean	Low Level Rep 1 0.0002 5000 0 0 (Weibull++ Low Level Rep 1 0.0004 2500	Fitting Para Rep2 0.0014 714.2857 0 Exponentia Fitting Para Rep2 0.0004 2500	al) meters Rep3 0.0007 1428.571 1428.571 1428.571 al) neters Rep3 0.0006 1666.667	Weibull Shape Scale Location	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097 11366.33 711366.33 711366.33 711366.33 711366.33 711366.33 711366.33 711366.33 711366.33 711366.33 711366.33 711366.33 711366.33 711367.724 711367.724 711367.724 711367.724 711367.724 711367.724 71281.768	re F F nts Set2 6.0805 16.1423 37.7049 385.8074 3016.537 37.7049 385.8074 3016.537 5.802 1.6826 2.2468 8.1588 8.15888 8.1588 8.1588	Set3 33.8777 340.1097 370.6554 897.4695 5712.437 597.4695 5712.437 2012.437 2012.437 2012.437 2012.437 2012.4402 202.0613 205.4487 202.0613 205.4487 202.0613 202.0614 202.0613 202.0614 202.0613 202.0614 202.061	Scale Location Shape Scale	High Level Rep1 0.3744 1592.354 491.84 (Top Weib High Level Rep1 0.5956 1671.235	Fitting Par Rep2 0.3562 181.6411 5.91 UIL++ Selec Fitting Par Rep2 0.5474 1783.465	ameters Rep3 0.5816 928.9105 24.41 		mean Location Lambda mean	Low Level Rep 1 0.0002 5000 0 0 (Weibull++ Low Level Rep 1 0.0004 2500	Fitting Para Rep2 0.0014 714.2857 0 Exponentia Fitting Para Rep2 0.0004 2500	al) meters Rep3 0.0007 1428.571 1428.571 1428.571 al) neters Rep3 0.0006 1666.667	Weibull Shape Scale Location	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097 11366.33 711366.33 711366.33 711366.33 711366.33 711366.33 711366.33 711366.33 711366.33 711366.33 711366.33 711366.33 711366.33 711367.7498 711367.7498 711367.7498 711367.7498 71146.037 71476.586 7150.085 7169.7724 756.2171 1014.603 71476.586 7169.7724 756.2171 1014.603 71476.586 7169.7724 7281.768 8678.168 8678.168	re F f f nts Set2 6.0805 16.1423 37.7049 385.8074 3016.537 Set2 1.6826 2.2468 8.1568 9.7845 57.1513 92.2753 188.8081 457.0314 483.8325 655.3901 888.7466 1068.396 1217.062 1854.382 1965.781 2178.458 2284.18 2273.829 4181.331 6027.841 36027.841	Set3 33.8777 340.1097 370.6554 897.4695 5712.437 5712.437 2012.437 2012.437 23.2267 59.4488 105.133 180.356 202.0613 202.077,774 203.077,7744	Scale Location Shape Scale	High Level Rep1 0.3744 1592.354 491.84 (Top Weib High Level Rep1 0.5956 1671.235	Fitting Par Rep2 0.3562 181.6411 5.91 UIL++ Selec Fitting Par Rep2 0.5474 1783.465	ameters Rep3 0.5816 928.9105 24.41 		mean Location Lambda mean	Low Level Rep 1 0.0002 5000 0 0 (Weibull++ Low Level Rep 1 0.0004 2500	Fitting Para Rep2 0.0014 714.2857 0 Exponentia Fitting Para Rep2 0.0004 2500	al) meters Rep3 0.0007 1428.571 1428.571 1428.571 al) neters Rep3 0.0006 1666.667	Weibull Shape Scale Location	0.55
DFR Failure PD 5 Data Poi Set1 492.9745 526.3141 1281.924 9009.097 11366.33 711366.33 711366.33 711366.33 7250.24 250.250.24 250.250.240.240.240.240.240.240.240.240.240.24	re re set2 6.0805 16.1423 37.7049 385.8074 3016.537 37.7049 385.8074 3016.537 5.802 1.6826 2.2468 8.1568 9.7845 57.1513 92.2753 188.8081 457.0314 483.8325 655.3901 888.7466 1068.396 1217.062 1854.382 1854.382 1854.382 1855.781 2178.458 2284.18 2674.79 2723.829 4181.331 4659.631 26027.841 7419.469	Set3 33.8777 340.1097 370.6554 897.4695 5712.437 5712.437 23.3267 23.3267 23.3267 23.3267 23.3267 23.3267 20.0613 202.613 202.613 202.6487 260.4402 310.1456 440.4745 553.3837 698.8552 782.0061 845.8762 163.001 1717.025 1810.474 1810.474 1810.474 1810.474 1810.474 1810.474 1810.474	Scale Location Shape Scale	High Level Rep1 0.3744 1592.354 491.84 (Top Weib High Level Rep1 0.5956 1671.235	Fitting Par Rep2 0.3562 181.6411 5.91 UIL++ Selec Fitting Par Rep2 0.5474 1783.465	ameters Rep3 0.5816 928.9105 24.41 		mean Location Lambda mean	Low Level Rep 1 0.0002 5000 0 0 (Weibull++ Low Level Rep 1 0.0004 2500	Fitting Para Rep2 0.0014 714.2857 0 Exponentia Fitting Para Rep2 0.0004 2500	al) meters Rep3 0.0007 1428.571 1428.571 1428.571 al) neters Rep3 0.0006 1666.667	Weibull Shape Scale Location	0.55

Repair							. · · · · · · · · · · · · · · · · · · ·			True Lognoi	rmal Mean:	190
Repair PD	-			(Top Weib	uli++ Selec	tion)				rue Lognorn		20
5 Data Poi				High Level	Fitting Para	ameters		(Empirical)	Tru	e Lognorma	Variance:	400
Set1	Set2	Set3			Rep2	Rep3		Low Level	Fitting Para	meters		
185.8123	176.8805	161.1705	N Mean					Rep1		Rep3		
199.7590	182.3526	180.6640	N S.D.					1		n for Norm	al variates;	5.241514
216.3888	193.4207	189.0722	ogN Mean	1	1	1		(Empirical)	V	ar for Norm	al variates:	0.011019
220.6105	219.0957	200.6946	LogN S.D.	Ō	0	0		p	St De	v for Norma	al Variates:	0.104973
221.3073	255.7414	206.9923										
		We	bull Shape	20.7942	0.902	14.647						
			Scale	214.8776	28.8798	194.8546						
			Location	0	175.21	0						
Repair PDI	-			(Top Weib	ull++ Select	tion)		(Empirical)				
25 Data Po				High Level	Fitting Para	ameters		Low Level	Fitting Para	meters		
Set1	Set2	Set3		Rep1	Rep2	Rep3		Rep1	Rep2	Rep3		
151.6819	148.6942	160.2890	N Mean									
153.2431	159.6656	165.3794	N S.D.					(Empirical)				
165.8580	160.8646	165.6153	ogN Mean	1	1	1		r				
167.9612	160.8802	169.2260	LogN S.D.	0	0	0						
171.7100	164.4242	169.8451				**************************************						
	165.3973		buil Shape	3.1127	2.9685	1.5717						
172.8264			Scale	63.9041	63.9722	33.6968						
178.2464	168.8557	172.9980	Location	133.2	130.5792	157.98						
180.0406	178.5186	177.9281										
180.6566		177.9786										
185.031		179.4088										
185.5818		181.4112										
186.8724												
193.4076	190.6778											
193.7151	195.9077	184.081										
200.0819												
202.1416		195.4155										
203.9582	198.6056	197.4176										
207.5767	199.5267	208.3743										
207.8584	204.4908											
216.2846												
217.6444		215.905										
219.7088		218.6615										
219.8784		222.0428										
222.1331	226.4753	222.46										

Component 8:

IFR Failure							l		1				
												TRUE IFR PAR	AMETER
Failure PDF				(Top Weib				1	(Weibull++	Exponenti	al)	Weibull	
5 Data Points				High Level				1		Fitting Para		Shape	2.7
		Set3		Rept	Rep2	Rep3			Rep1	Rep2	Rep3	Scale	1500
715.6579		396.932	Shape					Lambda	0.0016			Location	0
	1052.8389		Scale					mean	625	1428.571			
	1749.2671		Location					Location	602.7056	0	396.932		
	1829.2196												
1981.4671	2063.0686	1727.8931	xp. Lambda		1454.782		Normal						
			mean	625	552.1929	464.9773	s.d.		1				
			Location	602.7056									
Failure PDF				(Top Weib		tion)			Woibullu	- Exponenti	al)		
25 Data Poin	ts.			High Level						Fitting Para			
		Set3				Rep3					Rep3		
386,4647	460.3561	321,6691	Shape	2.2265	3.32			Lambda	0.001	0,0015			
390,4854		861.4311	Scale	1502.22				mean		666.6667			
502.7313		880.9627	Location	59.04	0			Location	386.4647			-	
508.1095	690.7912	960.5415											
661.7125		1045.6098				1374.37	Normal						
886.7261	749.5275	1053.1594				409,1649			1				
906.5238	883.7888	1066.5678						1	1				
944.8981	928,9266	1089.5723											
949.4023	980.7257	1099.6847						-					
975.2178	1038.1204	1185.9197											
1025.5719	1055.5777	1276.0984											
1209.4939	1071.9417	1333.207											
1370.8123	1140.857	1397.2204			·								
1618.6314		1415.0802			· _ · · · · · · · · · · · · · · · · · ·								
	1223.9014								1				
1840.8863	1251.3599	1540.3965											
	1257.6638	1627.901											
	1351.7852							-					······
	1374.6089												
2000.4766	1459.8623	1762.6073											
2046.725	1565.2797	1791.0901											
20942647	1600.459	1869.8137						1					
2145.1233	1631.8315	1893.3337	···									l l	
2231.8448	1685.4786	1915.3189											
2438.5156	1891.9785	2001.1393											

DFR Failure								1	ſ			
							 				TRUE DFR PA	BAMETEP
Failure PDF				(Top Weib	ull++ Selec	tion)		(Weibull++	Exponenti		Weibull	
5 Data Point	s			High Level	Fitting Par	ameters		Low Level	Fitting Para	meters	Shape	0.78
Set1	Set2	Set3		Rep1	Rep2	Rep3		Rep1	Rep2	Rep3	Scale	1156
118.6141	198.6125	60.58	Shape	0.6114	2.0641	0.6051	Lambda	0.0008		0.001	Location	0
194.014	720.2697	187.8718	Scale	790.3363	903.1276	674.4438	 mean	1250	588.2353	1000		
577.863	730.3799	237.5621	Location	109.52	0	51.29	Location	0	198.6125	0		
2314.9153	897.7414	1671.916										
2729.5595	1460.2987	2889.6972										
Failure PDF				(Top Weib	ull++ Selec	tion)		(Weibull++	Exponenti	al)		· · · · · ·
25 Data Poir	nts			High Level	Fitting Par	ameters		Low Level	Fitting Para	meters		
		Set3				Rep3		Rep1	Rep2	Rep3		
3.408	1.0488	0.3558	Shape				 Lambda	0.0009				
14.7588	13.4405	39.3497	Scale	841.598	688.7619	1280.568	mean	1111.111	909.0909	1666.667		
29.1609		100.0813	Location	0	0	0	Location	0	0	0		
36.31 46		191.2237										
40.3934		193.1598										
50.2688	99.5667	218.2887										
91.3994		237.5243										
155.1646	125.5608	329.7486										
225.2397	155.9482	361.0288										
265.9484	185.5911	382.4978										
333.1285	230.0614	437.0379										
386.2892		614.6348										
408.6879		644.8552										
629.3238	345.492	749.0729										
703.2736	507.993	839.4346										
1169.0581	686.1628	978.339										
1248.8722					-							
1445.3937												
1513.3078												
	1640.0109											
	1765.7716											
	2216.9765						 					
	2403.9948											
7113.8146	4681.3171	10811.838										

Repair	1				r	[1	True Lognoi	mal Mean	1200
Repair PDF				(Top Weib	ull++ Selec	tion)		1		rue Lognorn		75
5 Data Point	s	~~~~		High Level				(Empirical		e Lognorma		5625
Set1	Set2	Set3			Rep2	Rep3		Low Level				
1131,1176			N Mean	· · · · E ·		1.000		Rep1	Rep2	Rep3		
	1247.7035		N S.D.							an for Norm	al variates:	7.088127516
	1261.8463		LogN Mean	1	1	1		(Empirical		ar for Norm		0.00389864
	1293.5526		LogN S.D.	0						ev for Norma	al Variates:	0.062439094
1253.5318	1366.3922	1288.2809								1		
		W	eibull Shape	2.3119	1.3987	0.7407						
			Scale	98.3282	75.4893	45.4674						
			Location	1100.11	1209.59	1104.75						
Repair PDF					uli++ Selec			(Empirical)				
25 Data Poin				High Level					Fitting Par			
Set1	Set2	Set3		Rep1	Rep2	Rep3		Rep1	Rep2	Rep3		
1066.9783			N Mean									
	1086.7744		N S.D.					(Empirical)				
		1157.4686		1	1	1						
	1127.3754		LogN S.D.	0	0	0						
	1129.1260											
1122.0693			eibull Shape	2.035								
	1153.3699		Scale									
1133.9859			Location	1037.74	1001.39	1108.629						
1134.2086	1164.572	1189.92										
1162.8855					,					ļ		
1184.7496	1198.9882							1				
1185.8258	1205.5373									ļ		
1201.6919	1211.736											
1201.9551	1214.0789	1228.067										
1209.1298	1230.3851	1237.6677										
1217.8168	1233.3579	1237.788										
1220.1794	1234.021	1243.0786				L		ļ				
1224.1166	1252.4657	1255.4936				L						
1224.2382	1266.4462	1268.1241								ļ		
1239.0689	1271.6447	1279.6191						L				
1277.6708	1301.5777	1306.2891						ļ				
1318.4832	1309.9897	1309.9517										
1335.9845	1313.2514											
1417.6112	1330.7274	1378.1332			. .			I		L		

Conmponent 9:

LED E							10111 7.	r	,				
IFR Failure													L
												TRUE IFR	PARAME
Failure PDF					ull++ Selec					Exponentia		Weibull	
5 Data Poin		-			Fitting Par					Fitting Para		Shape	1.6
		Set3				Rep3					Rep3	Scale	6000
	1654.2175		Shape					Lambda	0.0006			Lo cation	0
	2271.7078			1849.276				mean		1428.571	5000		
	3279.2189		Location	0	0	0		Location	0	1654.218	0		
	3331.5225				_								
3320.8389	4547.5771	16070.173											
Failure PDF			-		ull++ Select					Exponentia			
25 Data Poi					Fitting Par				Low Level	Fitting Para			
		Set3				Rep3					Rep3		
710.1353		677.8381	Shape	1.5749				Lambda	0.0002				
1404.275				5451.465				mean		3333.333			
	865,1356		Location	136.8	0	188.2		Location	710.1353	315.042	677.8381		
1712.0311		1269.5125											
	1555.3756			i									
	1768.3454												
	2018.1662												
	2216.0917												
	2299.0348												
	2308.5815												
	2723.8316												
	2833.595												
	2897.0913												
	3439.8605												
4687.6538	3915.9635	5293.0437											
	4195,1227												
	4859.5895												
	4934.6351												
	5281.6802												
	5447.2768						-						
	7422.3666												
	7939.4749												
	9350.079												
	9705.5429												
15570.734	12771.24	13027.447											

DFR Failur	9				Γ	r		[1				
								··				TRUE DF	R PARAM
Failure PDF				(Top Weib	ull++ Selec	tion)			(Weibull++	Exponenti	al)	Weibull	
5 Data Poin	ts				Fitting Par					Fitting Para		Shape	0.91
Set1	Set2	Set3		Rep1		Rep3			Rep1		Rep3	Scale	
681.5702	596.0467	119.6449	Shape		•	0.8243		Lambda	0.0001	0.0002		Location	C
2458.446	712.2351	936.5725	Scale			5389.666		mean	10000				
5510.2312	3365.8145	6880.5072	Location			0		Location	0	0	Ö		
10184.901	6731.4725	9813.6578			1								
24128.051	8823.3123	11431.131	Exp. Lambda	0.0001	0.0002	·····							
			mean	10000	5000								
			Location	0	0								
Failure PDF				(Top Weib	ull++ Select	tion)			(Weibull++	Exponenti	al)		
25 Data Poi	nts			High Level	Fitting Par	ameters				Fitting Para			
Set1	Set2	Set3		Rep1	Rep2	Rep3			Rep1	Rep2	Rep3		
288.5507	242.1327	41.8282	Shape	0.886	1.0473	0.8983		Lambda	0.0002		0.0002		
454.0527	494.4891	167.0204	Scale	4238.59	5726.453	4840.68		mean	5000	5000	5000		
700.2991	677.5071	403.0769	Location	235.27	62.45	0		Location	0	0	0		
701.9181	1235.1553	619.0767											·
1006.5467	1267.3978	879.9276											
1021.5041	1763.3643	930.1831											
1249.7236	2731.0845	1029.6775											
1519.4028	3326.5544	1328.8312											
1523.0142	3337.5112	1474.8382											
1751.3391	3365.3735	1684.7109											
2166.3748	3429.2985	2502.2854											
2540,1512	3515.0382	2693.31											
3018.4221	3761.8152	2807.075											
3857.1797	3920.6132	3551.0629											
4542.7513	4452.365	4450.4991											
4934.3277	4718.1228	5411.8571											
5396.2548	4722.0321	5604.2964					• • • • • • • •						
5451.2574	4969.9776	6749.6905											
	5292.6751												
6602,0741	8146.6918	9127.3135											
6605,3121	8953.005	9613.4038											
7288.3094	9086.6108	13044.791											
	15407.676												
	17600.539												
	25513.732												

Repair							[1		True Lognor	mal Mean:	1000
Repair PDF				(Top Weib	ull++ Selec	tion)				rue Lognom		30
5 Data Poin				High Level				(Empirical)		e Lognorma		900
Set1	Set2	Set3			Rep2	Rep3			Fitting Para			
957.3293	976,9499	980.0563	N Mean			6.9174		Rep1	Rep2	Rep3		
1004.1691	986.0260	993.8689	N S.D.			0.0225		1 '	Mea	an for Norm	al variates:	6.907305
1019.7928	1008.2677	1005.0293	LogN Mean	1	1	1009.947		(Empirical)	V	ar for Norm	al variates:	0.0009
1021.4267	1009.6679	1027.3645		0	0	22.72668		1	St De	v for Norma	al Variates:	0.029993
1063.3764	1033.7083	1043.4408										
		v	Veibull Shape	1013.219	1002.924		Normal					
			Scale	34.1523			SD					
			Location									
Repair PDF				(Top Weib	ull++ Selec	tion)		(Empirical)				
25 Data Poi	nts			High Level	Fitting Par	ameters		Low Level	I Fitting Parameters Rep2 Rep3			
Set1	Set2	Set3		Rep1	Rep2	Rep3		Rep1	Rep2	Rep3		
969.4499	929,7908	906.8867	N Mean	6.9207								
987.9844	943.7861	965.8418	N S.D.	0.0214				(Empirical)				
988.6763	960.9697	978.3340	LogN Mean	1013.261	1	1		1 · · ·				
991.4813	979.3975	979.6999	LogN S.D.	21.68627	0	0		1				
991.5687	983,9974	981.6159						1				
992.9107	990,1479	984.8527	Veibull Shape		1005.308	1002.698	Normal					
1001.3602	990.5475	986.9105	Scale		29.702	30.7377	SD	1				
1002.5114	995,3010	987.5617	Location					1				
1003.7589	1001.762	988.0836										
1005.574		995.0697										
1008.0845	1002.689	1003.6294										
1008.701	1004.0883	1004.238										
	1008.1903						_					
	1008.6868											
	1009.8558											
1015.6193								1				
1019.8246								1				
1021.0363	1020.745											
	1021.1124											
1028.7856		1021.9361								L		
1030.7385		1030.1 529										
1044.5651	1037.4256											
	1041.2503											
	1049.9777							1				
1060.5552	1056.0762	1067.1425			l	l	l		l	l		

Component 10:

IFR Failure	1				-	r		1		r	г — т	
										TRUE	PARAMETERS	
Failure PDF				(Ton Weih	ull++ Selec	tion)	 	(Weibull++	Exponenti		Weibull	
5 Data Point	s			High Level					Fitting Para		Shape	2.3
Set1	Set2	Set3		Rep1		Rep3				Rep3	Scale	4700
2460,3635	1391,2082	3104,3889	Shape				 Lambda	0.0004			Location	0
2985.2778	3824.9763	3239.3708	Scale	1682.075			 mean	2500				
3428.4506	4646.9928	4151.6844	Location	2349.75			 Location	1454.85	939.0042	2888.68		
3829.4519	5099.4023	5067.2464										
7899.659	10868.3625	5136.9909	Exp. Lambda		0.0002	0.0008						
			mean		5000	1250						
			Location		939.0042	2888.68						
										<u> </u>		
Failure PDF				(Top Weib				(Weibull++				
25 Data Poin				High Level					Fitting Para			
		Set3		Rep1		Rep3		Rept		Rep3		
894.4406		2131.6465	Shape				Lambda	0.0003	0.0002			
1023.1727		2340.2868	Scale		4955.363		mean	3333.333	5000			
1310.8676		2502.6929	Location	38.11	0	1897.27	Location	894.4406	331.2133	2131.647		
2000.8766		2821.5088										
2112.3535		2917.4431										
2350.6133		3105.3902										
2447.3256		3417.3013										
2531.0481		3425,1682										
2756.9077	3162.4144											
2899.8222		3778.0157					 					
2938.7555		3824.1597										
3549.4744		3860.8158										
3725.4581		4335.5436										
3818.6762	4515.6644											
4007.7806		5010.0428					 _	ļ				
4367.2804	4715.7704						 					
4622.0827		5377.7319					 					
5262.9528		5787.9227										
5510.4431	4983.704											
5649.2894	5094.7207	6666.7204									L	
6078.4149		6890.9982					 					
6198.2355												
6370.6497		7089.9942					 					
6873.8549		7181.9843										
8151.8431	9904.6635	10476.828			I		 					

DFR Failure													
											TRUE DF	R PARAMETERS	5
Failure PDF				(Top Weib	ull++ Select	lion)			(Weibull++	Exponenti	al)	Weibull	
5 Data Points	s			High Level	Fitting Para	ameters			Low Level	Fitting Para	meters	Shape	0.46
Set1	Set2	Set3		Rep1	Rep2	Rep3			Rep1	Rep2	Rep3	Scale	1763
381.118	44.4075	152.6667	Shape	0.5506	0.4267	0.5068		Lambda	0.0004	0.0006	0.0003	Location	
617.0898	70.8841	321.0095	Scale	1454.575	695.0183	1963.222		mean	2500	1666.667	3333.333		
720,741	817,1918	983,4334	Location	368.83	43.18	138.65		Location	0	0	0		
4788.7914	890.296	3473.1754											
6703.657	6248.1205	13650.636											
Failure PDF				(Top Weib	uli++ Select	ion)			(Weibull++	Exponentia	al)		
25 Data Poin	ts			High Level	Fitting Para	ameters			Low Level	Fitting Para	meters		
Set1	Set2	Set3		Rep1	Rep2	Rep3			Rep1	Rep2	Rep3		
0.6963	0.1052	0.9617	Shape	0.3712	0.4054	0.4449		Lambda	0.0002	0.0004	0.0002		
0.7089	0.2974	13.3046	Scale	1373.869	835.7398	2318.451		mean	5000	2500	5000		
4.3471	3.9251	14.061	Location	0.57	0.0365	0.566		Location	0	0	0		
6.2738	16.0122	14.1847											
7.6485	28.5815	52.6527											
8.8736	34.0162	64.047											
42.1304	42.8644	98.1549											
62.9165	60.1729	105.1859											
99.5838	94.3021	377.3271											
143.9298	161.3008	426.0947											
308,4204	168.157	436.5944											
445.9509	176.267	677.0956											
528,1258	210.9908	830.3045											
673.2927	335.5744	924.6434											
1225.3759		2801.9214											
1893.414		2950.2222											
2204.4939													
2916.5381		3479.9136											
3221.0717	1287.1444	5239.1908											
7677.4195	1903.4808	6528.7926					1						
10511.7004	2861.968	9335.2173											
10960.5403	4074.9577	11385.745											
11707.1679	8267.2338	21325.116											
	16146.7854												
43477.963	26798.4491	38939.663											

Repair									[]	True Logno	rmal Mean:	2300
Repair PDF				(Top Weib	ull++ Selec	tion)				rue Lognorr		133
5 Data Points	3			High Level	Fitting Par	ameters		(Empirical)		e Lognorma		17689
Set1	Set2	Set3				Rep3		Low Level	Fitting Para	ameters	1	
2244.4884	2141.4443	2276.3188	N Mean		7.7629			Rep1	Rep2	Rep3		
2260.0039	2328.3686	2482.6217	N S.D.		0.0551				Me	an for Norm	al v ariates:	7.738995263
2354.3167	2335.8325	2514.6316	LogN Mean	1	2355.287	1		(Empirical)	i v	ar for Norm	al v ariates:	0.003338278
2362.9009	2463.2166	2525.4142	LogN S.D.	0	129.8749	0			St De	ev for Norm	al Variates:	0.057777834
2414.3795	2507.9680	2627.1859										
			Normal				Weibull Shape					
			SD	64.7559		2535.908	Scale					
						0	Location					
										I		
Repair PDF					ull++ Selec			(Empirical)				
25 Data Poin					Fitting Par	ameters			Fitting Para			
	Set2	Set3		Rep1	Rep2	Rep3		Rep1	Rep2	Rep3		
2041.8124			N Mean									
2077.4957	2142,4601		N S.D.					(Empirical)				
2129.4412		2169.5474		1	1							
2135.9223		2169.6936		0	0	0						
2177.7875		2197.0539										
2201.6623			Veibull Shape				Normal			<u> </u>		
2227.5785	2265.4355			141.1561		337.9804	SD					
2247.9478		2234.5096	Location		1138.31	2024.68						
2278.6822	2269.1553											
2285.9912	2277.6492											
2288.4621	2287.4753											
2291.1901	2303.3847	2276.2228										
2325.2501	2303.3995				~							
2348.7154	2304.2275	2325.19										
2348.8709	2304.6355											
2351.348	2318.4564								L			
2372.4001	2332.3781							•				
2374.8429												
2383.5781	2368.9782											
2445.5536	2372.1516											
2453.2725	2375.4344											
2453.3264	2404.7957	2475.733										
2473.8595												
2503.4369	2483,9576											
2664.3045	2511.8641	2558.3395										

Component 11:

IFR Failur	e					A			[
												TRUE IFR	PARAME
Failure PD	F			(Top Weib	ull++ Select	tion)			(Weibull++	Exponenti	al)	Weibult	
5 Data Poi	nts				Fitting Para					Fitting Para		Shape	1.4
Set1	Set2	Set3				Rep3					Rep3	Scale	2700
399.3785	348.758	1171.1815	Shape	1.717	1.5995			Lambda	0.0008			Location	0
830.8968	1017.428	1221.9844			2057.368			mean	1250		2500		
1580.886	1719.111	3127.0986	Location	0	0			Location	321.4348	0	657.75		
1953.553	2494.546	4832.3086											
3139.557	3653.888	5037.1987				0.0004	Ex. lambda						
						2500	mean						
						657.75	location						
Failure PD)F			(Top Weib	ull++ Selec	tion)			(Weibull++	Exponenti	al)		
25 Data P	oints			High Level	Fitting Par	ameters			Low Level	Fitting Para	meters		
Set1	Set2	Set3		Rep1	Rep2	Rep3			Rep1	Rep2	Rep3		
135.1654	205.6775	125.7678	Shape	1.4844				Lambda	0.0005	0.0004	0.0005		
611.4846	394.5768	252.0802	Scale	2507.105	2599.055	2230.025		mean	2000	2500	2000		
651.0371	509.5215	291.4994	Location	0	45.86	49.46		Location	135.1654	0	125.7678		
	737.8067												
	752.9524												
	840.2453												
1263.096					1								
	1356.857											1	
		924.6418											
		1208.1672											
1385.471		1245.9077							<u> </u>				
		1306.397											
		1530.4185											
		1958.8213											
		2204.4944										1	
		2349.3161					L	ļ					
		2484.0128											
		2976.4458											
		3206.0688					1					ļ	
		3282.3602		L					L	L			
3995.412	4339.191	3711.8226											
		4345.3492		L	L					ļ			
		5114.9785		ļ									
		5357.2256		ļ		l	I	I	I	L	L	ļ	I
6151.23	1 5482.621	6614.3085	l	I	I	L		1			1	I	<u> </u>

DFR Failu	re											
											TRUE DF	R PARAME
Failure PD	F			(Top Weib	JII++ Select	tion)	 	(Weibull++	Exponentia	ai)	Weibull	
5 Data Poi	nts			High Level					Fitting Para		Shape	0.82
Set1	Set2	Set3				Rep3				Rep3	Scale	2210
8.6383	257.351	652,8088	Shape	0.3717	0.8764		Lambda	0.0016			Location	0
25.3535	674.1752	871.4467	Scale	216.4645	1894.652	1694.464	 mean	625	2000	3333.333		
		1860.3552	Location	8.48	140.36	625.16	Location	0	0	0		
1408.127	2304.159	2150.5854										
1577.924	6288.88	10252.167										
Failure PD					ull++ Selec				Exponenti			
25 Data Po					Fitting Par				Fitting Para			
Set1	Set2	Set3		Rep1		Rep3				Rep3		
62.2017			Shape				Lambda	0.0005				
83.1745		120.7591	Scale		1885.069	2157.154	mean	2000	2000	2500		
98.2315			Location	59.81	0	0	Location	0	0	0		
	118.1574											
132.6368							 	L				
141.8487												
	428.7619											
	463.5295											
	527.5761											
402.0495												
	1148.423											
	1270.221	1101.879										
		1577.8085										
		1969.9017										
1360.007		2016.8713										
		2172.5559										
		2262.6457										
		2444.5492										
		2861.5444										
3542.853		2865.5286										
3571.851		3978.9659										
		4345.9862										
7229.554	4981.317	5207.9364										
		8198.7492										
10447.32	7468.848	9183,7914										

Repair								1		True Lognor	mal Mean	500
Repair PDF	-			(Top Weib	JII++ Selec	tion)				rue Lognom		60
5 Data Poir				High Level				(Empirical)		e Lognorma		3600
Set1	Set2	Set3				Rep3			Fitting Para			
408.5751	382.8029	434.3379	N Mean		6.158			Rep1		Rep3		
505.4561	456.0501	487.9058	N S.D.		0.125					an for Norm	al variates:	6.207459
517.8744	469.2272	519.6217	LogN Mean	1	476.1879	1		(Empirical)		ar for Norm		0.014297
541.2839	527.4465	520.6206	LogN S.D.	0	59.75676	0				v for Norma		0.119571
549.1956	545.1056	521.6798										
		V	Veibull Shape	17.501		496.8332	Normal		-			
			Scale	526.3015		33.7279	SD					
			Location	0								
Repair PDF	=			(Top Weib	ull++ Selec	tion)		(Empirical				
25 Data Po	oints			High Level	Fitting Par	ameters		Low Level	Fitting Para	meters		
Set1	Set2	Set3		Rep1	Rep2	Rep3		Rep1	Rep2	Rep3		
379.2242	376.3529	360.0695	N Mean		6.1715							
384.8839	399.4062	396.3990	N S.D.		0.1185			(Empirical)			
397.9237	413.9606	423.6617	LogN Mean	1	482.2782	1						
402.2933	419.7963		LogN S.D.	0	57.35118	0						
415.7437	420.9450	428.3661										
418.8344	445.0704	437.9965	Veibull Shape	1.9775		9.1918						
	449.3883		Scale	119.471		524.4168						
435.1145	450.3172	453.0509	Location	360.36		0						
	452.9297	462.2056										
447.9557	454.7003	484.4993										
452.1994	456.0182	498.8031										
459.6537	456.1584	504.6379										
461.5911	469.0703	517.1915										
462.7588										1		
465.9207										1		
467.9612		523.6307										
468.4529												
470.0837												
489.2458												
493.1113												
525.0043												
	546.9055											
	557.0174											
	584.6395											
601.0891	603.7306	624.3891				1			1			

Component 12:

IFR Failure											1		[
												TRUE IFF	PARAME
Failure PDF				(Top Weib					(Weibull++			Weibull	
5 Data Poin				High Level	Fitting Par	ameters			LowLevel	Fitting Para	ameters	Shape	1.9
	Set2	Set3		Rep1		Rep3			Rep1	Rep2	Rep3	Scale	2700
1261.7666	1257.1554	594.7325	Shape	0.5878				Lambda	0.0005	0,0007	0.0004	Location	0
1412.4101		1682.0797	Scale	894.3969	3023.592			mean	2000	1428.571	2500		1
1515.381		2224.6969	Location	1252.4	0			Location	494.34	1257.155	403.5007		
4174.5672		4679.6372										- The second second second	
4349.6919	3691.6301	4807.4154				0.0004	xp. Lamioda						
						2500	mean						
						403.5007	Location						
E-11				<i>(</i>	l					L			
Failure PDF					ull++ Selec				(Weibull++				
25 Data Poi	nts Set2	0.10			Fitting Par					Fitting Para			
Set1 473.7039		Set3 660.4892	Chara a			Rep3 1.524		1		Rep2	Rep3		
609.1241	469.3594		Shape Scale			1.524		Lambda	0.0007	0.0004		· · · · · · · · · · · · · · · · · · ·	<u></u>
670.3734	765.0322							mean	1428.571				
714,7449		837.6972 1114.6858	Location	0	0	535.1		Location	473.7039	261.6811	660.4892		ļ
		1142.0944											L
799.4156 821.8652		1249.2308											<u> </u>
1026,1816													
1026.1816					h						I	ļ	l
1113.5933									ł		ļ		
1280.8095		1467.4095							 				
1280.8095		1508.0267											
1752.6716		1508.0267									· · · ·		
						ļ		i .					L
1775.5144 2202.4022		1648.2241											
2202.4022					I								
		1849.1673			1				I				1
2304.0152 2453.8687		1978.8131				ļ			<u> </u>		ļ		
		2673.5422											
2731.204 2904.4548		2681.0014 2798.3986							<u> </u>				
2904.4548						ļ					-		
3017.5133		3016.9451					·						Į
3274.07		3237.0632											<u> </u>
3560.5859		3403.7783			I							L	I
3581.0894		3759.0765			L				ļ				
4126.65	5439.7757	4214.8319			1	1	l		L	L	1		1

DFR Failure	- 1										rT	
							 				TRUE DFF	
Failure PDF				(Top Weib	ull++ Select	ion)		(Weibull++	Exponentia	al)	Weibull	
5 Data Point	ts			High Level			 		Fitting Para		Shape	0.67
Set1	Set2	Set3				Rep3				Rep3	Scale	1812
7.6546	96.0899	21.1995	Shape	0.7685		0.6072	 Lambda	0.0019			Location	0
197.1153	113.9879	755.0449		471.1644	1448.012	2426.685	mean	526.3158	2000	3333.333		
325.2801	1001.18	781.0092	Location	0	0	0	Location	0	0	0		
513.3453	1377.4546	4275.7639					 					
1654.598	7131.7167	11255.07										
Failure PDF				(Top Weib	ull++ Select	tion)		(Weibull++	Exponentia	al)		
25 Data Poi	nts			High Level	Fitting Para	ameters	1	LowLevel	Fitting Para	uneters		
Set1	Set2	Set3		Rep1	Rep2	Rep3		Rep1	Rep2	Rep3		
10.9449	3.7484	87.0939	Shape	0.7077	0.7423		Lambda	0.0005	0.0005	0.0004		
11.1556	45.4783	90.6331	Scale	1630.637	1816.511	2203.728	 mean	2000	2000	2500		
11.6602	76.0758	124.7874	Location	0	0	62.81	Location	0	0	0		
49,9084	175.6294	149.4903										
153.5405	188.8683											
176.5265	272.3074	196.7246										
468.0817	378.9127	411.433										
576.0046	526.0171	476.6189	-					1				
642.2621	853.6597	740.2461						1				
648.6122												
692.8479		1142.9903						1				
788.1248	976.4346	1361.5264										
797.9105		1742.5392										
1019.872		1782.2856										
1162.9292		2169.7709										
1711.7281		2414.2543										
2346.9917		2528.401										
2932.8064		2761.1596										
3121.6927		3271.3115					 1					
3265.6842		4597.1368					 					
3767.835		5929.2883										
5175.5476		6308.3627										
5842.0775		8273.6667						1				
6673.5799												
7470.7063	9901.7573	11152.869									1	

Repair										True Lognor	mal Mean:	1000
Repair PDF				(Top Weib	ull++ Select	tion)				rue Lognorn		100
5 Data Poin	ts				Fitting Para			(Empirical)		e Lognorma		10000
Set1	Set2	Set3		Rep1		Rep3		Low Level				
921.2770	820.7662	1047.2591	N Mean						Rep2	Rep3		
1026.9795	1007.9188	1086.8297	NS.D.						Me	an for Norm	al variates:	6.90278
1030.6159	1161.9647	1105.9727	LogN Mean	1	1	1		(Empirical)	V	ar for Norm	al variates:	0.00995
1081.1291	1213.9549	1108.9158	LogN S.D.	0	0	0			St De	ev for Norma	al Variates:	0.099751
1179.9064	1230.9343	1149.3595										
		W	eibull Shape	3.5735	9.636	1099.667	Normal					
			Scale	299.5936	1150.825	33.1844	SD					
			Location	778.58	0							
Repair PDF					ull++ Selec			(Empirical)				
25 Data Po					Fitting Par			Low Level		ameters		
Set1	Set2	Set3		Rep1	Rep2	Rep3		Rep1	Rep2	Rep3		
863.4720	816.3019	836.3563	N Mean		6.9115							
870.4745	836.0325	857.4328	NS.D.		0.111			(Empirical))			
878.7886	888.8314				1009.954							
881.4143	889.2766		LogN S.D.	0	112.4511	0						
883.4105	898.2122											
891.1241	915.6568		eibull Shape			1.8793						
892.3451	927.0283		Scale		t i	227.2435						
930.7104		930.0624	Location	813.92		807.18						
935.6024					<u> </u>							
947.4867	967.8106											
951.459												
966.2918												
986.5928												
989.2622	1029.7179											
994.1616					<u> </u>							
1008.1781		1031.0253										
1008.6267		1051.3581										
1011.5922			ļ									
1030.4598									L			
1037.8319		1107.9219					ļ					L
1056.746		11 14.7 159			1							I
1058.7383		1146.3594							I			L
1068.7242		1160.0313							L			
1137.1276			*				l		1			
1142.8991	1368.8295	1284.396	<u>i </u>									

Component 13:

										T			
IFR Failure													L
											TRUE IFR		ERS
Failure PDF					ull++ Select					Exponentia		Weibuli	I
5 Data Poin					Fitting Para					Fitting Para		Shape	
		Set3				Rep3			Rep1		Rep3	Scale	
1534.7392	896.028		Shape	1.0452	0.9373	1.4478		Lambda	0.0002		0.0004	Location	0
2953.8106	1543.0735				3617.809			mean	5000	5000	2500		
4334.0274	3307.1905	3895.0499	Location	1089.76	669.88	1841.89		Location	0	0	2058.92		
5885.3096	5861.0583	5460.114											
14192.729	10349.6589	7561.16	Exp. Lambda		Normal								
			mean	#DIV/01	s.d.								
			Location										
Failure PDF				(Top Weib	ull++ Select	tion)			(Weibull++	Exponentia	al)		
25 Data Poi				High Level	Fitting Par	ameters				Fitting Para	imeters		
Set1	Set2	Set3		Rept	Rep2	Rep3			Rep1	Rep2	Rep3		
303.173	364.9067	52.2914	Shape	1.099	1.5637	1.3457		Lambda	0.0003	0.0003	0.0003		
426.5639	471.2389	517.6315	Scale	3738.021	4208.958	3298.907	-	mean	3333.333	3333.333	3333.333		
716.8078	534.2293	536.4013	Location	185.79	0	0		Location	203.05	364.9067	52.29		
876.5694	692.8011	676.0851											
972.2855	835.1185	743.9198											
1083.6165	1157.1796	1353.7882							1			······	
1800.6851	1813.9937	1552.2205											
1888.3481	2007.6607	1642.183					**********						
1970.5479	2590.7362	1664.7736											
2143.4951	3074.3267	2000.7745											1
2294.3538	3756.3237	2496.9661											
2343.1229	3858.5608	2515.8117											
2403.8472	4232.3753	2581.3519								1			
2907.9941		2815.3824			1	T			1	1			
2996.2714	4630,4668	2816.2662											1
3180.0696	4673.2074	3561.1123	1										
4185.0583	5054.6401						·····	1	1	1	ĺ		1
4862.0909	5222.681								1				
5179.9238	5749.319	3843.1136			1				1			1	1
5292.771	5893.3512	3992.5466									1	1	1
6423.234	6030.9471	5862.6757						1		1	1	1	1
8207.1477	6260.7526	5985.4605		1		1			1	1			1
9439.1723	6386.9334	6126.255	1						1	1			1
9843.7147	7641.1074	7591.0921		1	1	1		1	1			i	1
13060.971	8022.6307	7761.8746				1		1				1	1

DFR Failure													
											TRUE DE		TERS
Failure PDF				(Top Weib	Ill++ Select	tion)		-	(Weibull++	Exponentia		Weibull	
5 Data Point				High Level						Fitting Para		Shape	0.86
		Set3				Rep3		t			Rep3	Scale	3591
821.429	1923.5228	505.3313	Shape	0.7792	0.4406			Lambda	0.0003	0.0002			0
1765.5065	2224,9034	1174.8287	Scale	2059.37	1153.917	2315.178		mean	3333.333	5000	2500		
1978,1663	2262.4041	1524.5589	Location		1918.814	333.62		Location	0	0000			
2189.6663	2516.0291	3041.0487									-		
8948.9675	16093,1049	7387.8961											
					· · · ·			1					
									1				-
								· · · · · · · · · · · · · · · · · · ·					
Failure PDF				(Top Weib	uli++ Selec	tion)			(Weibull++	Exponenti	al)		
25 Data Poi	nts			High Level						Fitting Para			-
Set1	Set2	Set3				Rep3					Rep3		
36.3236	21.5841	49.1341	Shape	0.7608	0.855			Lambda	0.0002	0.0002			
188.6881	102.3341	118.9211	Scale	4714.48	5917.635	3668.353		mean	5000	5000			
199,9364	498.039	274.2967	Location	11.09	0			Location	0	0	0		
222.5115	614.9749	393.2561							-	-		1 1	
266.6395	831.7648	485.8735											
567.3778	1468.5343	521.5053						<u> </u>				1 1	
944.2548	1831.2292	545.8457					•						
1038.0092	2044,4742	566.8894											
1948.6666	2640.3637	1212.735											
2286.6888	2906.0534	1218.5584						1					· · · · ·
2759.1723	3043.1824	1545.1322											
2961.0126	3600.0084	1764.2993											
3450.8804	4234.745	1880.0662											
3551.7663	4412.2526	2024.5855											
3829.7049	5383.6358	2314.5517						1					
4366.7506	5846.0498	2387.5884					·	1					
5261.639	5928.3691	3156.058						1		1	1		
6222.2804	6579.8596	3413.1687							1				
6379.6793	8293.0474	3588.0676				<u> </u>		1	1		1		
6982.4762	8534.6481	4226.6113				T					1		
8316.9783	10004.7272												
13430.928		5564.6401				1		1					
19695.835									1			1	
20668.013	19319.2679	8800.8698		1	l	1							
22262.107	31005.7548							1			1		

Repair										True Lognor	mal Mean:	90
Repair PDF				(Top Weib	ull++ Selec	tion)				rue Lognom		15
5 Data Poin	ts				Fitting Par			(Empirical)		e Lognorma		225
Set1	Set2	Set3				Rep3			Fitting Para			
81.0415	90.2785	80.5283	N Mean					Rep1	Rep2	Rep3		
88.5546	90.3328	81.1774	N S.D.						Mea	an for Norma	al variates:	4.48611
95.8472	92.9108	82.0838	LogN Mean	1	1	1		(Empirical)	v	ar for Norm	al variates:	0.027399
100.2568				Ó	0	Ō				ev for Norma		0.165526
116.9931	101.0421	119.3345										
			Weibull Shape	2.1677	0.1872	0.0476	Exp. lambda	3				
			Scale	27,7927	5.34188	21.0084	mean					
			Location	72.02	88.7781	72.2	location					
Repair PDF				(Top Weib	ull++ Selec	tion)		(Empirical)				
25 Data Pol	Ints			High Level	Fitting Par	ameters		Low Level	Fitting Para	ameters		
Set1	Set2	Set3		Rep1	Rep2	Rep3		Rep1	Rep2	Rep3		
73.2955	57.2922	58.9802	N Mean			4.4783						
73.6014	58.4706	71.5267	N S.D.			0.1567		(Empirical	Ì			
79.8333	63.5220	75.1428	LogN Mean	1	1	89.17292	2					
80.8700	64.6013	75.5645	LogN S.D.	0	0	14.05962		1				
81.6838	70.2260	77.7277										
83.8330	73.0534		Weibull Shape	7.8912	88.9987	Normal						
84.8072	73.7476	78.4352	Scale	103.3727	18.6082	SD	T					
86.3784	76.5441	80.4052		0								
88.3803												
90.2415												
92.4393		87.5769										
96.4936	91.0671	87.8593										
96.8319		89.5182										
97.3717		89.5254										
98.1219										1		
107.6175												
107.9168				I								
108.8023									1			
108.9241	100.4516					ļ		1		L		
111.1314										ļ		
114.572												
115.0058									L		l	
115.7103							-l			<u> </u>		
116.1526										ļ		
119.8311	125.2759	122.622	!			L	I		L	<u> </u>		

Components14, 15, 16 (Identical):

IFR Failure												
											TRUE IFR	PARAME
Failure PDF				(Top Weibu					Exponentia		Weibull	
5 Data Point				High Level					Fitting Para		Shape	1.5
	Set2	Set3			Rep2	Rep3				Вер 3	Scale	2600
821.4516		1102.2931	Shape	0.7578			 Lambda	0.0006	0.001	0.0004	Location	0
	1103.9043			1147.527			 mean	1666.667	1000	2500		
	1667.3854		Location	786.64			Location	313.35	623.85	0		
	2454.4122											
4565.1962	2486.4593	4846.733	Ex	p. Lambda	0.001	0.0004						
				mean	1000	2500						
				Location	623.85	0						
				A 141 1					L	l		
Failure PDF				(Top Weib					Exponenti			
25 Data Poir		0.10		High Level					Fitting Para			
Set1 246.3968	Set2	Set3				Rep3	 			Rep3		
	188.0413	476.4257	Shape	1.3582	1.3692	1.8777	Lambda	0.0006				
301.6394		502.2544	Scale		2086.813		 mean		1666.667			
373.9172 459.5992		739.9818	Location	0	0	71.56	Location	246.3968	188.0413	476.4257		
		1028.7516										
460.1965												
653.3902		1209.3161 1437.0933					 					
726.7555		1437.0933					 					
803.0814							 					
882.3804		1572.3952					 	L				
987.415		1634.8171										
1171.1423		1883.5857										
1498.7366		1885.5797										
1781.2094		1895.3852								L		
1825.0894							 ·	L				
	1964.0803							L				
	2534.5844							ļ	L			
		2716.3803					 			L		
		2736.2439										
2721.5915		3602.3901										
		3651.0592					 					
	3096.9098											
3375.3331		3917.4935										
		3969.5992			L							
		4061.0864										
5672.4301	5232.4088	4927.1196										

DFR Failure							 · · · · · · · · · · · · · · · · · · ·					
	·										TRUE DF	PARAME
Failure PDF				(Top Weib	JII++ Select	tion)	 	(Weibull++	Exponentia	al)	Weibull	
5 Data Points	3			High Level	Fitting Para	ameters		Low Level	Fitting Para	meters	Shape	0.62
Set1	Set2	Set3		Rep1	Rep2	Rep3		Rep1	Rep2	Rep3	Scale	1626
68.4451	294.4203	766.6737	Shape	0.761	0.713	0.5346	Lambda	0.0017	0.0003	0.0003	Location	0
186.4102	356.9395	862.8837	Scale	461.4434	22.81.88	1331.235	 mean	588.2353	3333.333	3333.333		
	1463.7002		Location	51.78	154.67	757.19	Location	0	0	0		
	3642.0894											
1675.0516	9153.306	7681.8881										
								1				
Failure PDF					ull++ Selec				Exponentia			
25 Data Poir					Fitting Par				Fitting Para			
	Set2	Set3				Rep3				Rep3		
16.2601	1.3678	21.873	Shape	0.667			Lambda	0.0004				
53.0656		22.5653	Scale		1547.771	1646.667	mean	2500	2000	2000		
56.5048		27.6429	Location	10.47	0	0	Location	0	0	0		
75.7388		47.1459										
167.0309		89.8158										
305.4133		212.3958										
363.3778		539.9818										
398.2837		622.2503										
453.2609		672.6159										
533.8485		902.2155					 					
573.2808		922.8244										
828.9389		925.753										
1142.1472	838.1515	1075.3										
1168.4655		1229.0825										
1667.4281		1310.0152										
	1787.7082											
	1977.4734											
	2248.1439										l	
	2500.3208					ļ						
4050.3354		3035.7101		L						L	L	
	2734.3145											
	3052.4287					L	 					
	4481.6833			,			 ļ					L
	5679.4627		I				 					
12985.957	12446.341	7724.7371				1						

Repair								1		True Lognor	mal Mean:	2200
Repair PDF				(Top Weib	JII++ Select	tion)				rue Lognorn		200
5 Data Points	5			High Level				(Empirical)		e Lognorma		40000
Set1	Set2	Set3		Rep1	Rep2	Rep3		Low Level				
1949.6625	1886.9895	1872.2611	N Mean					Rep1	Rep2	Rep3		
2100.3616	1967.0133	1955.0769	N S.D.		#*************************************	*		1	Mea	an for Norm	al variates:	7.692097
2166.0339	1995.4006	2187.3587	LogN Mean	1	1	1	_	(Empirical)	v	ar for Norm	al variates:	0.00823
2211.5068	2135.2229	2274.0560	LogN S.D.	0	0	0				ev for Norma	al Variates:	0.090722
2217.2812	2277.0469	2636.5608										
			Weibull Shape	31.399	0.0055	1.2609	Ex. lambd	a				
			Scale	2171.618				1				
			Location	0	1869.98	1825.55	location			1		
Repair PDF				(Top Weib	ull++ Selec	tion)		(Empirical)				
25 Data Poin					Fitting Par	ameters		Low Level	Fitting Para	ameters		
Set1	Set2	Set3		Rep1	Rep2	Rep3		Rep1	Rep2	Rep3		
1968.6689			N Mean									
	1988.0872		NS.D.		1.0 1.0			(Empirical				
	1994.3224		LogN Mean		1	1						
	1999.3083		LogN S.D.	194.9885	0	0						
	2010.2552											
	2011.2372		Weibull Shape		2.2168	2.4171						
	2023.9646		Scale		518.9681	375.512						
	2084.5795		Location		1774.82	1877.01		1				
	2121.9681											
	2128.7886											
	2156.8377											
	2192.9171											
	2223.1086											
	2232.0927											
2237.4657												
2258.3989												
2275.9476												
2276.3111												
2307.7167												
2326.8208												
2378.565	2408.2664	2356.1085						1		1		
2407.8434	2478.9498	2381.4711						1				
2477.8152	2545.9917	2449.3159				T						
2609.5416	2692.0111	2469.2448										
2755.4595	2726.8006	2570.2291						1		1	1	

Component 17:

IFR Failure						<u></u>							
in n i andie										·····		TRUE IFF	PARAME
Failure PDF				(Top Weib)	JII++ Select	ion)			(Weibull++	Exponentia	al)	Weibull	
5 Data Points	3				Fitting Para					Fitting Para		Shape	1.1
		Set3				Rep3					Rep3	Scale	3100
	18.1282	1342,6858	Shape			0.5709		Lambda	0.0004				C
		2023.619		2283.543		2591.26		mean		3333,333			
1837.1238	3433.2333	2130,4663	Location	416.94		1315.93		Location	0	18.13	0		
2624.7316	4400.4372	4532.2146											
6958.4368	6291.3935	17067.397	Ex	p. Lambda	0.0003				-				
					3333.333								
				Location	18.13								
Failure PDF				(Top Weib	ull++ Selec	tion)			(Weibull++	Exponenti	al)		
25 Data Poir				High Level	Fitting Par	ameters			LowLevel	Fitting Para			
	Set2	Set3		Rep1	Rep2	Rep3			Rep1		Rep3		
		243.6169	Shape					Lambda	0.0003		0.0003		
		280.0406	Scale	4161.14	4131.261	4075.564		mean	3333.333	3333.333	3333,333		
	1176.0653		Location	0	0	112.77		Location	407.9259	161.6904	243.6169		
		687.6845											
		980.0645											
		1318.0745											
		1840.1952											
		1848.0641											
		1872.9607											
		1912.3393										L	
	2714.4592											L	
		2535.8871											
		2578.4347											
		2825.9499									-		
		3064.6348							ļ				
		4203.3075											
		4662.8708											
		6309.9644		L		L							──
		6627.4906		———		<u> </u>		•		L			───
		7723.7112		ļ		I	·	I		L	l	↓	<u> </u>
		8116.545		ļ		ļ		I		<u> </u>		<u> </u>	<u> </u>
		8335.255		ļ						ļ		<u> </u>	<u> </u>
		8715.5821		ļ		ļ		L				L	
		9680.6486		ļ		ļ				└── ─		 	<u> </u>
11462.4756	12305.858	12644.521		[.1	I	1	I	1

DFR Failure												
DTITI MILLIO							 		~ ~		TRUE DF	
Failure PDF			-	(Top Weibt	ull++ Select	tion)		(Weibull++	Exponentia	al)	Weibull	
5 Data Points	3			High Level			 		Fitting Para		Shape	0.75
Set1	Set2	Set3				Rep3	 			Rep3	Scale	2513
59.5865	100.8272	16.3306	Shape	0.5047	0.5698	0.6788	 Lambda	0.0008	0.0004	0.0008	Location	0
107.9897	254.9411	155.4217	Scale	649.5001	1728.702	1012.114	mean	1250	2500	1250		
335.4129			Location	55.81	82.27	0	 Location	0	0	0		
1597.24	3186.4542	1255.9734										
3875.1825	8918.2656	3990.7473										
Failure PDF	-			(f)W. 1	uli++ Selec	()		(16/-:	Exponenti	-0		
25 Data Poin					Fitting Par		 		Fitting Para			
	Set2	Set3				Rep3	 			Rep3		
0.5437	7.0806	28.9356	Shape				 Lambda	0.0003				
8.6153			Scale				 mean	3333.333	2500			
65.457			Location				 Location	0000.000	0			
164.9746			Loodion		- · ·		Location		v	<u> </u>		
231.0014		390.2366					 					
379.0323							 ·	1				
631.9394							 ·	- ·				
737.8507							 	· · · ·	······································			
901.6432							 	-				
1019.4881							 					
1207.4124		1511.2874			1		 	1	<u> </u>			
1363,3861			······································									
1662.5712	1631.9059	1578.4342										
1837.826		1734.3744	· · ·							1		
1899.0532	2392.6403	1954,1419										
2045.8198	3086.4352	2278.26										
2924.5257		2790.8143					 					
3373.4443	3221.2884	2814.2229										
3523.4982								1				
6008,3335												
6643.9093		5383.2228										
6991.3563	6352.5353	7049.654										
7986.5179	7558.4107	7307.1499								1		
8894.9477	8582.6366	9437.1436										
17469.7751	8876.2789	10066.398										

Repair								-	Frue Lognor	mal Mean:	750
Repair PDF			·	(Top Weib	ull++ Select	ion)			ue Lognorn		60
5 Data Points	5				Fitting Para		 (Empirical)		e Lognorma		3600
Set1	Set2	Set3				Rep3		Fitting Para			
703.4492	703.7980	679.0828	N Mean	6.6232				Rep2	Rep3		
738.2612	712.6273	741.9910	NS.D.	0.0442				Mea	n for Norma	al variates:	6.616883
754.8842	838.4393	748.2545	LogN Mean	753.084	1	1	 (Empirical)	V	ar for Norma	al variates:	0.00638
763.2433	854.3706	757.6201	LogN S.D.	33.30258	0	0	 <u></u>		v for Norma	al Variates:	0.079872
805.4866	971.8440	781.9900									
		v	Veibull Shape		2.9491	29.4958					
			Scale		298.658	756.6656					
1			Location		550.82	0					
Repair PDF				(Top Weib	ull++ Select	tion)	(Empirical)				
25 Data Poin	its		-	High Level	Fitting Para	ameters	 Low Level	Fitting Para	meters		
Set1	Set2	Set3		Rep1	Rep2	Rep3	Rep1	Rep2	Rep3		
655.1149	603.5467	612.7326	N Mean		6.6108						
667.5307	657.4044	690.7836	NS.D.		0.0803		(Empirical)	•			
672.4019	680.2897	696.1823	LogN Mean	1	745.4768	1	r				
690.0443	688.6749	710.6512	LogN S.D.	0	59.95842	0	 				
706.7640	693.7778	715.0063									
715.2020	698.8124	718.9385	Veibull Shape	3.3904		17.4999	 				
719.0928	707.1852	735.5823	Scale	158.0607		786.4869					
719.6680	714.0726	737.1192	Location	602.81		0					
722.7592	716.6129	750.8118									
723.5153											
726.2934											
731.1426											
746.4191	740.4143										
750.8742											
755.3336											
755.3454											
761.3573								1			
766.6826											
779.6974											
784.3381	783.1043						 				
797.9828						L					
801.5392											
816.6847											
820.8974				L							
826.7362	843.1758	855.3795	L								

Components 18, 19, 20 (Identical):

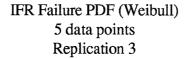
IFR Failure	e				<u> </u>							
							 				TRUE IFA	PARAME
Failure PDF	F			(Top Weib	ull++ Select	ion)		(Weibull++	Exponentia	al)	Weibull	
5 Data Poir	nts				Fitting Para		 		Fitting Para		Shape	1.6
Set1	Set2	Set3				Rep3				Rep3	Scale	
1502.388	1191.844	875.9743	Shape			0.965	 Lambda	0.0008			Location	0
2241.608	1611.518	975,103	Scale	1434.795	1769.724	489.0612	mean	1250	476.1905			
2294.656	1786.227	1294.217	Location	1292.15	0	841.0353	Location		1191.844			
2571.865	1812.564	1312.462										
4379.824	1931.782	2231.183										
Failure PDF	F			(Top Weib	ull++ Selec	tion)		(Weibull++	Exponenti	al)		
25 Data Po				High Level	Fitting Par	ameters		LowLevel	Fitting Para	umeters		
		Set3		Rep1	Rep2	Rep3		Rep1	Rep2	Rep3		
	210.9166					1.9818	Lambda	0.0007				
		568.2492		1786.976	1352.796	2071.292	 mean	1428.571	1250	2000		
		643.8168	Location	187.47	148.27	0	Location	314.9132	210.9166	0		
	432.1534											
	501.6268						 					
	666.8802						 					
	704.2608											
1000.785	728.4266	1300.138										
	779.4753											
		1370.584										
	829.2261											
	1015.429											
		1689.858					 					
	1449.675											
		2001.905										
		2041.049										
	1640.227											
		2186.686										
		2200.286										
		2424.663								[
		2814.613								I		
		3143.374										
		3409.666					 1					
		3651.85									1	-
4357.785	4504.255	3834.279										i

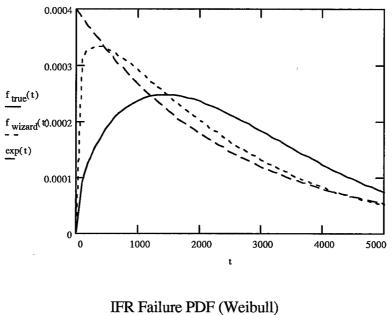
DFR Failu	re												
												TRUE DF	R PARAME
Failure PD	F			(Top Weib	ull++ Select	ion)			(Weibull++	Exponentia	al)	Weibull	
5 Data Poi					Fitting Para				Low Level	Fitting Para	meters	Shape	0.48
		Set3			Rep2	Rep3			Rep1	Rep2	Rep3	Scale	829
19.2842			Shape	0.3007		0.3947		Lambda	0.0003	0.0028		Location	0
45.759			Scale		160.2191	310,1298		mean	3333.333	357.1429	909.0909		
		103.7989	Location	19.14	23.48	0		Location	0	0	0		
	219.2888												
14259.96	1387.394	3958.93	p. Lambda										
			mean		#DIV/01								
			Location										
Failure PD					ull++ Selec					Exponenti			
25 Data Po					Fitting Par					Fitting Para			
	Set2	Set3				Rep3					Rep3		
0.0133			Shape			0.5169		Lambda	0.0006				
8.8798		23.4149	Scale	753.4989	1087.99			mean	1666.667	3333.333	2500		
19.6567	11.611	24.6482	Location	0	0	8.45		Location	0	0	0		
20.7896		33.4034											
45.0159												l	
88.2708		75.9579											
93.5473													
107.3531		324.5026										-	
125.3961													
	251.8883												
		372.9556											
317.6282													
404.9284													
	345.1927								1				
	659.6077										L		
	783.5122												
564.3061												ļ	
		1164.115							ļ	·			
		2691.308							ļ			ļ	[
		3127.158								ļ	ļ		
2198.133											I	 	
	3877.281						L	ļ	ļ	<u> </u>			
		11599.86						Į	l		L	l	
	9381.876							 				I	
1/009.16	59438.62	13556.88					L						

Repair										True Lognor	mal Mean:	280
Repair PDF				(Top Weib	ull++ Selec	ion)				rue Lognorn		50
5 Data Poir	nts			High Level				(Empirical)		e Lognorma		2500
Set1	Set2	Set3			Rep2	Rep3			Fitting Para			
160.9515	263.4569	205.7862	N Mean						Rep2	Rep3		
207.5786	268.0693	261.3554	N S.D.							an for Norm	al variates:	5.619095
249.9895	268.5295	293.0248	ogN Mean	1	1	1		(Empirical)	V	ar for Norm	al variates:	0.03139
259.1388	306.5290	324.6998	LogN S.D.	0	0	0		<u> </u>		v for Norma	al Variates:	0.177172
288.9591	354.9991	334.4042										
		We	ibull Shape	6.497	0.6542	283.8541	Normal					
			Scale	251.3703	22.0338	46.7088	SD					
			Location	0	262.9							
Repair PDI	=			(Top Weib	ull++ Selec	tion)		(Empirical)				
25 Data Po				High Level	Fitting Par			Low Level	Fitting Para	ameters		
Set1	Set2	Set3		Rep1	Rep2	Rep3		Rep1	Rep2	Rep3		
226.1870		162,4683	N Mean			5.5349						
226.2906		192.8644				0.1931		(Empirical)				
233.5470		198.9839		1	1	258.1508						
234.2416		204.5344	LogN S.D.	0	0	50.31723				1		
237.7709												
238.4575			bull Shape		3.1754							
242.8845	244.4475		Scale	74.3501	174.918							
250.1624		232.3286	Location	210.45	132.27							
260.8614												
267.3973												
271.7493	284.9472	237.1974										
271.9375	293.7138											
272.2074												
276.2545												
280.349		261.3496										
281.0325												
289.3342	321.275											
294.0659												
295.8926	325.7814											
300.4485	328.0474											
301.0505	329.8898											
326.5971	334.6501	313.1513								1		
327.3225	350.851	317.2415					1					
329.0394	377.8968	321.3988										
371.0237	408.8771	374.819						1			1	

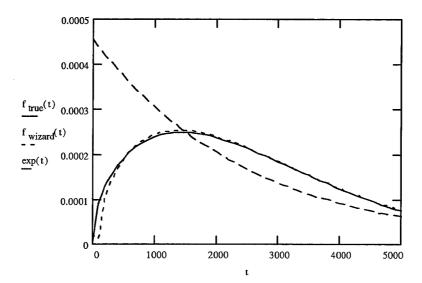
Appendix E: Data Fitting Graphs

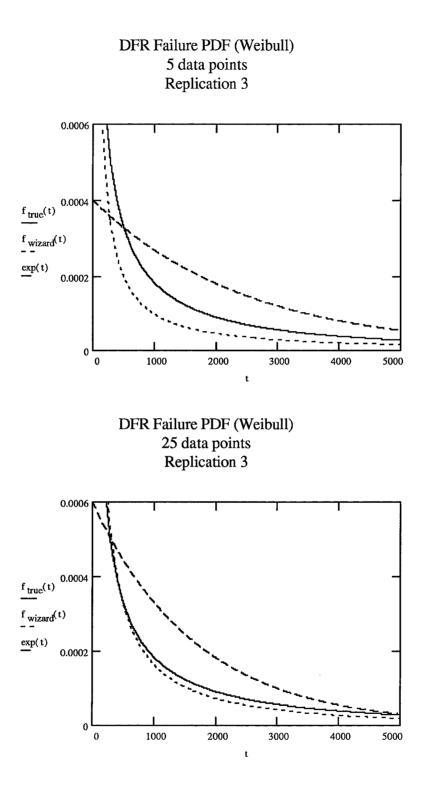
Examples of True versus Weibull++ Wizard and Exponential Fitted Distributions for Component 1 (Final Experiment):

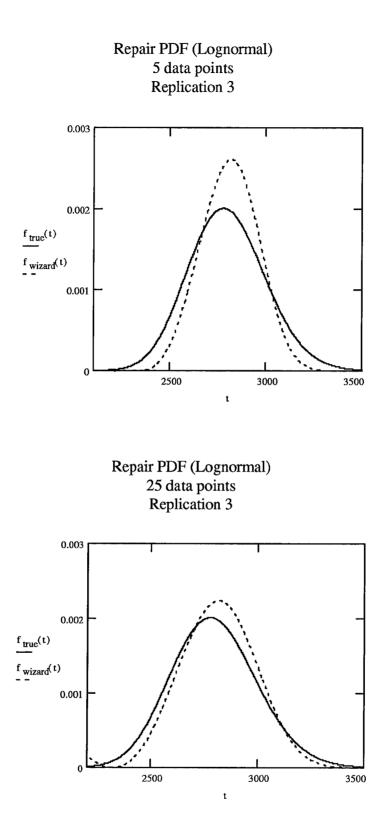




25 data points Replication 3







Appendix F:

Birnbaum Structural Component Importance Measure Results for Final Experiment

Small / Series-Parallel Structure:

Component	Birnbaum Structural Importance Measure	Тор 20 <i>%</i>
1	.1875	
2	.1875	
3	.5625	\checkmark
4	1875	
5	.1875	

Small / Complex Structure:

Component	Birnbaum Structural Importance Measure	Тор 20%
1*	.410156	\checkmark
2	.410156	
3	.246094	
4	.410156	
5	.410156	
* Sm	allect MTTE/M	DT ratio

Smallest MTTF/MRT ratio

Large / Complex Structure:

Component	Birnbaum Structural Importance	Тор 20 <i>%</i>
	Measure	
1	.090469	√
2	.038773	
3	.064621	
4	.090469	\checkmark
5	.038773	
6	.042004	
7	.084007	\checkmark
8	.084007	1
9	.042004	
10	.015274	
11	.015274	
12	.045822	
13	.07637	
14	.015274	
15	015274	
16	.07627	
17	.045822	
18	.024002	
19	.024002	
20	.024002	

Large / Series-Parallel Structure:

	Birnbaum Structural	Тор
Component	Importance	20%
Component	Measure	2070
1	.08832	
2	.08832	
3	.08832	
4	.206079	$\overline{\mathbf{A}}$
5	.206079	\checkmark
6	.08832	
7	.08832	
8	.08832	
9	.041216	
10	.041216	
11	.041216	
12	.041216	
13	.206079	V
14	.08832	
15	.08832	
16	.08832	
17	.206079	1
18	.08832	
19	.08832	
20	.08832	

Appendix G: Multivariate Analysis of RAPTOR Output

I. ANALYSIS TECHNIQUES

Overview

A main objective of this study was to provide insight for the reliability community in assessing differences in various systems of components through multivariate analysis of simulation output. Several multivariate techniques were applied, including discriminant analysis (DA), neural networks, logistic regression, principal component analysis (PCA), and factor analysis (FA).

Discriminant Analysis (DA)

A primary analysis objective was to discriminate between large versus small, complex versus series-parallel, and increasing failure rate (IFR) versus decreasing failure rate (DFR) component structures. Discriminant analysis was the key method to achieve this objective. Due to the relatively small size of the data set, the discriminant function was formed from the entire data set. Therefore, true validation cannot occur until the discriminant function is tested against future observations. As will be discussed later, the formatting of the data was a major difficulty in conducting discriminant analysis. Because of this, and as a learning exercise, DA was attempted on different forms of the data set, namely standardized data and transformed data (using a Box-Cox transformation). Furthermore, since the variance-covariance matrices were only statistically equal for the IFR versus DFR case, discriminant functions were calculated using the within-class covariance matrices in addition to using the pooled matrices (for the large versus small and complex versus series-parallel cases). This was done mostly as a learning exercise to see what would happen and if any differences would occur in the discriminant results. In general, as detailed in the results section of this paper, significant success was achieved in discriminating between classes in all 3 cases.

Neural Networks

Since a quadratic discriminant function was the most effective for the complex versus series-parallel case, a neural network was also employed to assess it's ability to discriminate between complex and series-parallel component structures. The neural net was trained on standardized data using back-propagation and sigmoidal processing with one hidden layer containing 20 nodes. A 'full' neural net was run using all the variables as well as a 'reduced' net containing only the 3 most salient variables. Good discriminant success was achieved (consistent with the DA results) for the training and validation sets for both the full and reduced models.

Logistic Regression

As an additional exercise, logistic regression was also tried in an attempt to discriminate between complex and series-parallel component structures. The models included a full model logistic regression of raw, standardized, and transformed data, without success. The software used in the logistic regression analysis (SAS and

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JMP) could only produce a viable regression model on a reduced set of variables (the 3 most salient variables identified in the neural net analysis were used). Logistic regression proved to be the least powerful method for discriminating between complex and series-parallel component structures.

Principal Component Analysis (PCA)

Another analysis objective was to see if the majority of output variance could be adequately explained in smaller dimensions. To achieve this objective, principal component analysis (PCA) based on the correlation matrix was conducted. Although the loading structure was not completely clear-cut, by using Kaiser's criterion a reduction in the dimensionality of the data set to 3 components was achieved which explained a majority (82%) of the output data variance. Some success in discriminating between large versus small and IFR versus DFR structures using component score rankings was also achieved.

Factor Analysis (FA)

Our final analysis objective was to identify possible common underlying factors with common variance. Using factor analysis with varimax data rotation, 3 underlying factors were identified. The rotation produced much more clearly defined factor loadings. As with PCA, some success was achieved in discriminating between large versus small and IFR versus DFR structures using factor score rankings.

II. DATABASE

General Description

Multivariate analysis was conducted on output data produced by system component reliability models developed and run on the Rapid Availability Prototyping for Testing Operational Readiness (RAPTOR) software. RAPTOR, created by HQ AFOTEC/SAL, creates reliability, maintainability, availability (RM&A) and sparing models for various systems undergoing operational test and evaluation (OT&E).

Specific Output Measures

The specific output measures analyzed are defined below:

Availability: The ratio of the time the system is up (operational) versus total simulation time.

Mean Time Between Downing Events (MTBDE): The average time between events which bring the entire system down.

Mean Down Time (MDT): The average amount of time the entire system is down.

Mean Time Between Maintenance (MTBM): The average amount of time between any maintenance actions performed on any components of the system.

Mean Repair Time (MRT): The average amount of time it takes to repair any component in the system.

Analysis on the *standard deviations* of all of the above simulation output measures was also conducted.

Thirty-eight different system models with various characteristics were created and run on RAPTOR for a duration of 50,000 simulation time units per run. The three characteristics which define each system of components are structure type, failure probability density function (pdf) type, and system size. The breakdown for each category is as follows:

- Structure Type: Complex (non series-parallel) or Series-Parallel network

- Overall Component Failure pdf Type: Increasing Failure Rate (IFR) or

Decreasing Failure Rate (DFR)

- Size: Large (20 components) or Small (5 components)

Two examples of structure types used in the study are shown in Figures F-1 and F-2.

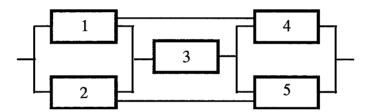


Figure F-1. Small / Complex Structure Type

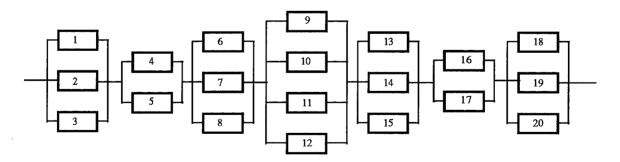


Figure F-2. Large / Series-Parallel Structure Type

Twelve basic structures/systems were developed: 3 large complex systems, 3 large seriesparallel systems, 3 small complex systems, and 3 small series-parallel systems. The parameters of the Weibull distributed failure rates for specific components in each system were varied, and 10 runs for each configuration measuring the outputs described above (averaged over the 10 simulation runs) were conducted. When re-configuring a component failure rate from IFR to DFR, the same *average* failure rate was maintained by adjusting the Weibull scale parameter. Therefore, when a component is altered from IFR to DFR (or vice versa), the only thing that changes is the fact that it's failure distribution is changed from Weibull IFR to Weibull DFR. Some runs were conducted with all component failure pdf's either exclusively IFR or DFR, and some were run where 20% of the component failure distributions were altered to the opposite type. To simplify the analysis, any system which had a predominant (80% or more) component failure distributions of IFR or DFR, was labeled as IFR or DFR, respectively. The final result was 38 total configurations. An entire overview of the structure types and simulation outputs is provided in Table F-1.

	Failure					Simulation	Output	Parameters				···· ·
Structure	PDF	Size	Ao	Ao S.D.	MTBDE	MTBDE S.D.	MDT	MDT S.D.	MTBM	MTBM S.D.	MRT	MRT S.D.
Complex	IFR	Large	0.62195	0.0317	831.36136	75.576532	506.489	69.955175	153.7701	6.125785	972.288	36.924329
Complex	DFR	Large	0.58173	0.0483	699.71808	96.007519	507.801	103.79795	139.7672	9.816596	990.091	76.259607
Complex	IFR	Large	0.63395	0.0373	880.95237	158.622887	505.67	87.795161	154.7226	9.789738	965.661	45.291379
Complex	DFR	Large	0.59402	0.0503	728.2015	125.372449	490.995	51.204153	139.7718	10.318022	990.298	90.250027
S-P	IFR	Large	0.84397	0.0239	1859.4221	185.712002	343.404	58.046129	160.8931	5.027334	934.313	19.928222
S-P	DFR	Large	0.82293	0.0515	1900.4104	682.441413	373.829	85.693138	151.0831	12.875395	924.663	71.292258
S-P	IFR	Large	0.8545	0.0273	2012.4874	488.187184	331.872	48.445802	162.9239	9.168588	927.149	42.11069
S-P	DFR	Large	0.83093	0.0649	1813.4586	468.103509	340.372	73.421084	152.8934	12.891715	935.142	51.081099
Complex	IFR	Small	0.79723	0.0411	2517.4118	600.101875	613.235	62.90322	607.9589	52.450363	962.774	40.528591
Complex	DFR	Small	0.77137	0.0709	2330.3009	1113.381932	603.902	153.02025	622.7378	176.694094	1050.93	96.956241
Complex	IFR	Small	0.79269	0.0727	2265.9171	623.983857	557.461	176.63768	591.8588	56.288879	972.672	102.08752
Complex	DFR	Small	0.78156	0.0535	2124.4053	546.198341	583.181	166.19736	567.2333	46.76866	964.838	111.4952
S-P	IFR	Small	0.64951	0.0356	1608.0276	186.849893	863.769	97.571768	594.1459	47.864929	1016.68	43.676779
S-P	DFR	Small	0.6214	0.0592	1336.2383	391.090585	788.749	128.67521	530.1731	83.196167	1097.2	140.45746
S-P	IFR	Small	0.64273	0.0302	1535.4473	265.502618	844.903	99.479778	580.5185	33.05382	1018.08	64.554289
S-P	DFR	Small	0.66742	0.0562	1658.0624	336.932573	812.166	150.83298	580.4298	117.845115	994.381	128.14823
Complex	IFR	Large	0.65005	0.0436	978.83652	182.752826	521.406	84.959954	152.2207	7.777956	987.486	33.613689
Complex	DFR	Large	0.65614	0.0592	993.56181	194.133449	511.751	85.010133	150.2238	16.701989	984.548	58.906297
S-P	IFR	Large	0.8629	0.0308	2562.1308	460.556013	396.451	66,725463	165.5002	6.53677	940.918	26.54521
S-P	DFR	Large	0.85516	0.0434	2318.5127	727.267637	377.627	130.5672	156.2256	12.517785	940.307	48.952462
S-P	IFR	Large	0.87645	0.0416	2751.387	1254.914262	341.681	124.08618	160.7838	12.007663	935.579	46.547722
S-P	DFR	Large	0.86522	0.0399	2793.5271	855.937428	417.518	121.19979	160.3137	10.684756	954.882	43.011271
Complex	IFR	Small	0.73506	0.0199	1771.9746	242.296206	636.269	81.977295	599.5027	26.616841	1001.37	62.470026
Complex	DFR	Small	0.74472	0.0884	1971.814	1053.069465	591.845	145.91455	568.734	87.423621	972.397	149.6474
Complex	IFR	Small	0.71677	0.051	1645.915	359.040565	633.405	89.892948	576.4315	38.333944	1039.75	99.237831
Complex	DFR	Small	0.74244	0.0324	1730.6547	489.090361	581.963	90.847932	558.1052	95.639121	973.869	84.669393
S-P	IFR	Small		0.0218	3428.6584	502.256878	912.667	69.040485	601.2296	29.823233	931.045	42.499865
S-P	DFR	Small	0.77451	0.0418	2949.9511	514.004513	838.49	111.39209	578.9948	77.061728	993.46	116.64769
S-P	IFR	Small	0.76007	0.0584	3148.3652	987.897623	922.938	43.752593	607.5508	33.812394	968.5	60.030239
S-P	DFR	Small	0.78267	0.0314	3549.7397	741.920113	958.127	63.235759	571.3842	77.493459	978.117	113.25613
S-P	IFR	Small	0.65559	0.0172	1573.4532	157.864481	822.169	31.769495	599.1858	27.791716	980.591	27.843022
S-P	DFR	Small		0.0772	1225.7376	388.082703	819.015	78.426313	539.2185	89.841237	944.66	111.6787
Complex	IFR	Small	0.65806	0.0219	1345.2839	117.197318	697.664	57.717031	572.4634	21.554528	980.978	60.770088
Complex	DFR	Small	0.67109	0.0622	1435.7829	365.305281	678.578	110.01039	589.7982	75.434413	1011.1	96.192313
S-P	IFR	Large	0.94244	0.0175	8397.0178	3438.66978	470.046	132.21821	163.135	5.218078	922.436	25.571554
S-P	DFR	Large	0.95354	0.0211	10122.331	6056.891589	389.935	111.03885	156.0759	11.852342	911.461	40.316235
Complex	IFR	Large	0.93384	0.0122	4155.5733	1040.334833	285.465	43.771342	162.8321	4.4553	912.337	27.591806
Complex	DFR	Large	0.9245	0.0354	3976.5947	3138.595902	225.842	64.706545	156.56	17.740922	933.373	39.069533

Table F-1. RAPTOR Output Database

III. ANALYSIS OBJECTIVES

Purpose of Investigation

The purpose of the investigation was to:

1) Ascertain whether one can distinguish between the complex versus seriesparallel structures, IFR versus DFR configurations, and large versus small system sizes based on the simulation outputs;

2) Identify which output measures provide the most discriminant power;

3) See if one can adequately explain a majority of the output variance in smaller dimensions; and

4) Identify possible common underlying factors with common variance.

Variables Used

All 10 RAPTOR output variables were used in the analysis. In some cases, nearly equivalent results could be obtained by only using the most salient variables (this will be discussed in more detail in the results section of this report). Since there is a large disparity in magnitudes of the output variables, the variance-covariance matrix was sparse (contained many zeros). To alleviate computational problems resulting from this, standardized data was used for most analyses. The standardized data set is depicted in Table F-2.

When checking for multivariate normality for discriminant analysis, several of the variables did not pass the Shapiro-Wilk test for normality (at a 10% level of significance). In an attempt to achieve multivariate normality, a Box-Cox transformation was conducted

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on all variables. The affects of the Box-Cox transformation on the passage of the Shapiro-

	Failure					Simulatio	n Output Pa	arameters				
Structure	PDF	Size	Ao	Ao S.D.	MTBDE	MTBDE S.D.	MDT	MDT S.D.	MTBM	MTBM S.D.	MRT	MRT.S.D.
Complex	IFR	Large	-1.23508	-0.60383	-0.84725	-0.63232609	-0.377552	-0.65269	-1.05905	-0.85128284	0.020338	-0.88381
Complex	DFR	Large	-1.61179	0.30777	-0.91868	-0.6139671	-0.370949	0.286585	-1.12462	-0.75528568	0.469788	0.242433
Complex	IFR	Large	-1.12264	-0.29764	-0.82035	-0.55770183	-0.381668	-0.15756	-1.05459	-0.75598425	-0.14697	-0.64425
Complex	DFR	Large	-1.49669	0.418498	-0.90323	-0.5875802	-0.455488	-1.1731	-1.1246	-0.74224371	0.47501	0.643005
S-P	IFR	Large	0.844632	-1.03029	-0.28944	-0.53335994	-1.197926	-0.98321	-1.0257	-0.8798533	-0.93838	-1.37044
S-P	DFR	Large	0.647505	0.483103	-0.2672	-0.08700604	-1.044875	-0.2159	-1.07163	-0.67572702	-1.18199	0.100208
S-P	IFR	Large	0.943237	-0.84711	-0.20639	-0.2615601	-1.255933	-1.24966	-1.01619	-0.77214022	-1.11923	-0.73532
S-P	DFR	Large	0.722469	1.214216	-0.31438	-0.279607	-1.213178	-0.55649	-1.06316	-0.67530254	-0.91744	-0.47848
Complex	IFR	Large	-0.97185	0.049844	-0.76724	-0.53601902	-0.302513	-0.23624	-1.06631	-0.80831024	0.404019	-0.9786
Complex	DFR	Large	-0.91481	0.904462	-0.75925	-0.52579255	-0.351082	-0.23485	-1.07566	-0.57619818	0.329852	-0.25443
S-P	IFR	Large	1.021919	-0.65423	0.091846	-0.28638907	-0.931079	-0.74232	-1.00412	-0.84059321	-0.77163	-1.18099
S-P	DFR	Large	0.949401	0.039314	-0.04034	-0.04672584	-1.025772	1.029537	-1.04755	-0.68502837	-0.78705	-0.53942
S-P	IFR	Large	1.148794	-0.06083	0.194534	0.42740982	-1.206594	0.849663	-1.02621	-0.69829653	-0.90642	-0.60828
S-P	DFR	Large	1.043613	-0.15406	0.217399	0.06889498	-0.825104	0.769555	-1.02841	-0.73270504	-0.41908	-0.70953
S-P	IFR	Large	1.766935	-1.38288	3.257803	2.38970111	-0.560873	1.075359	-1.0152	-0.87489209	-1.23822	-1.20886
S-P	DFR	Large	1.870899	-1.185	4.193942	4.74239756	-0.96386	0.487548	-1.04825	-0.70233639	-1.51529	-0.78669
Complex	IFR	Large	1.686361	-1.67371	0.956433	0.23459184	-1,48938	-1.37939	-1.01662	-0.89473177	-1.49317	-1.15102
Complex	DFR	Large	1.598865	-0.40272	0.859321	2.12005904	-1.789305	-0.79836	-1.04599	-0.54917577	-0.96212	-0.82239
Complex	IFR	Small	0.406776	-0.08683	0.067581	-0.16099517	0.1594215	-0.84841	1.067802	0.35360887	-0.21986	-0.78061
Complex	DFR	Small	0.164557	1.545412	-0.03394	0.30023091	0.11247	1.652698	1.137008	3.58515997	2.005838	0.835017
Complex	IFR	Small	0.364287	1.646762	-0.06888	-0.13953516	-0.121144	2.308175	0.992409	0.4534478	0.030039	0.981935
Complex	DFR	Small	0.260034	0.593831	-0.14566	-0.20943211	0.0082353	2.018415	0.877094	0.20582907	-0.16774	1.251295
S-P	IFR	Small	-0.97687	-0.39093	-0.42584	-0.53233745	1.4196953	0.113784	1.003119	0.23434278	1.141103	-0.69048
S-P	DFR	Small	-1.24016	0.904078	-0.57331	-0.3488097	1.0423186	0.977027	0.70355	1.15330022	3.173793	2.08054
S-P	IFR	Small	-1.04043	-0.68653	-0.46522	-0.46166124	1.3247934	0.166739	0.939305	-0.15089079	1.176339	-0.09271
S-P	DFR	Small	-0.80916	0.739385	-0.39869	-0.39747531	1.1601118	1.591992	0.93889	2.05451145	0.578095	1.728104
Complex	IFR	Smail	-0.17557	-1.24933	-0.33689	-0.48251419	0.2752868	-0.31902	1.028203	-0.31831514	0.754506	-0.15239
Complex	DFR	Small	-0.08506	2.50533	-0.22846	0.24603499	0.0518184	1.455487	0.884121	1.26325533	0.023086	2.343666
Complex	IFR	Small	-0.34686	0.45623	-0.40528	-0.37760939	0.260883	-0.09933	0.920167	-0.01355597	1.723533	0.900343
Complex	DFR	Small	-0.10642	-0.56577	-0.35931	-0.26074851	0.0021111	-0.07283	0.834349	1.47693861	0.060263	0.483221
S-P	IFR	Small	0.316085	-1.14524	0.562016	-0.24891727	1.6656677	-0.67807	1.03629	-0.23491762	-1.02088	-0.72417
S-P	DFR	Small	0.194006	-0.04854	0.302273	-0.23836102	1.2925298	0.497352	0.93217	0.99374486	0.554858	1.398821
S-P	IFR	Small	0.058729	0.861685	0.409931	0.18747251	1.717337	-1.37991	1.065891	-0.13116045	-0.07528	-0.22224
S-P	DFR	Small	0.270356	-0.62149	0.627713	-0.03355934	1.8943498	-0.83918	0.896531	1.00497408	0.167492	1.301714
S-P	IFR	Small	-0.91996	-1.39872	-0.4446	-0.55838332	1.2104309	-1.71249	1.026719	-0.28775691	0.229945	-1.14383
S-P	DFR	Small	-1.55452	1.891527	-0.63327	-0.35151254	1.1945657	-0.41758	0.745908	1.32613697	-0.67716	1.256549
Complex	IFR	Small	-0.89678	-1.14206	-0.5684	-0.59492625	0.5841287	-0.99234	0.901585	-0.44998475	0.239736	-0.20106
Complex	DFR	Small	-0.77479	1.066304	-0.5193	-0.37198001	0.4881198	0.459005	0.98276	0.95141877	1.000255	0.813144

Wilk test for each variable are shown in Table F-3.

Table F-2. Standardized Data Set

	Lar	ge	Sma	ıll	Com	olex	S-F	>	IFF	2	DF	R
Variable	Before	After										
Ao	Fail	Fail	Fail	Fail	Pass	Pass	Pass	Pass	Fail	Fail	Pass	Pass
Ao S.D.	Pass	Pass										
MTBDE	Fail	Pass										
MTBDE S.D.	Fail	Pass										
MDT	Pass	Pass	Fail	Fail	Fail	Pass	Fail	Fail	Pass	Pass	Pass	Pass
MDT S.D.	Pass	Pass	Pass	Pass	Fail	Pass	Pass	Pass	Pass	Pass	Pass	Pass
MTBM	Fail	Pass	Pass	Pass	Fail	Fail	Fail	Fail	Fail	Fail	Fail	Fail
MTBM S.D.	Pass	Pass	Fail	Pass	Fail	Pass	Fail	Pass	Fail	Fail	Fail	Fail
MRT	Fail	Fail	Pass	Pass	Pass	Pass	Fail	Fail	Pass	Pass	Pass	Pass
MRT S.D.	Pass	Pass	Pass	Pass	Pass	Pass	Fail	Pass	Fail	Pass	Pass	Pass

* Boldface cells note where improvement was achieved

Table F-3. Effects of Box-Cox Transformation on Shapiro-Wilk Normality Test for Each Variable

From Table F-3, it is apparent that an improvement in the overall normality of the data was achieved. Although not all variables passed the Shapiro-Wilk test after the transformation, the majority of the variables did pass. Therefore, the assumption of multivariate normality was reasonably justified for use in discriminant analysis.

IV. ANALYSIS RESULTS

Special Problems Encountered

The most difficult problem encountered was the formatting of the data. As discussed previously, the large scale differences in the data caused numerical problems, but this was overcome via standardization. Another problem was the lack of multivariate normality, which was addressed by the use of Box-Cox transformations. In the end, several different data formats were tried (raw, standardized, and transformed) in the discriminant analysis to see what type of results would be achieved with each format.

When conducting logistic regression, SAS and JMP could not produce a viable regression model using all variables. This was true using the raw simulation output data, standardized data, as well as transformed data. However, a viable model was produced when the set of variables was reduced (down to 3) to those that were identified as most salient in the neural network analysis.

Another problem was the difficulty in interpreting the principal components. A 'clean' separation in the principal component loadings was not apparent, making the analysis challenging. Although principal components were defined from this analysis, the interpretation may be subject to debate due to the ambiguity in component loadings. However, after varimax rotation of the data, a much clearer loading structure was revealed in the subsequent factor analysis.

Discrimination Between Categories of Component Structures

Several multivariate techniques were used in an attempt to discriminate between large versus small, complex versus series-parallel, and increasing failure rate (IFR) versus

decreasing failure rate (DFR) component structures: DA, neural nets, logistic regression, as well as score rankings resulting from PCA and FA. The overall discriminant results for all methods are shown in Table F-4 for direct comparison.

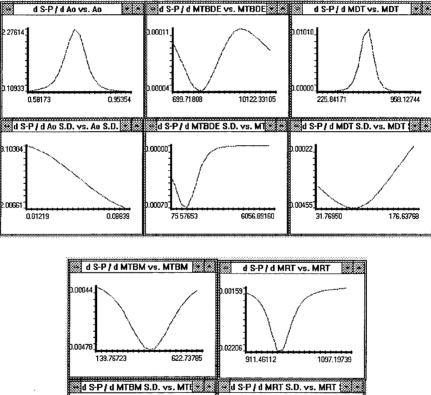
	Discrimin (percentages show cl	ant Results	2011)	· · · · · ·
Data	Method	Large/Small	Complex/S-P	IFR/DFR
Standardized	SAS Pooled	100% / 100%	94% / 85%	95% / 95%
	SAS Pooled	100% / 100%	94% / 90%	89% / 95%
Transformed	SAS Unpooled	100% / 100%	100 % / 100%	
	JMP	100% / 100%	94% / 90%	89% / 95%
	Full Neural Net: Training		93% / 100 %	
	Full Neural Net: Validation		100% / 100%	
Standardized	Reduced Neural Net: Training		98% / 100 %	
	Reduced Neural Net: Validation		100% / 100%	
	Reduced Logistic Regression		67% / 85%	
Raw	Component Score Ranking	89% / 90%		84% / 74%
	Factor Score Ranking	100% / 100%		84% / 95%
	Best Discriminant Function	Linear	Quadratic	Linear
			MTBDE	MRT SD
		MTBM	Ao	Ao SD
	Best Discriminant Variable(s)		MRT	MTBM SD
			MDT	MDT SD

Table F-4. Classification Accuracy for all Methods Used for Discrimination

For the most part, the results were consistent across methods with excellent discriminant success. There was strong agreement between methods on which variables served as the best discriminants (e.g. discriminant loadings, neural net salient variables, and components/factors which best discriminated for each category showed strong agreement). This general consistency across methods provided greater confidence in the overall analysis. The classification accuracy percentages for DA may be inflated because the entire data set was used. Logistic regression proved to be the weakest discriminant tool in the complex versus series-parallel case.

Neural Net Results

To help identify the variables which contributed most in discriminating between classes in the neural net, several graphical outputs produced by the Statistical Neural Network Analysis Package (SNNAP) software were reviewed. As an example, the following derivative graphs help show which variables had the greatest discriminant power. Looking at Figure F-3, the graphs with the more 'pointed' curves identify the more salient variables (A₀, MDT, and MRT).



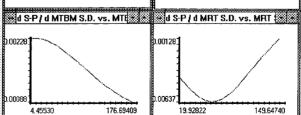


Figure F-3. Neural Net Derivative Saliency Graphs

Reduction in Dimensionality (PCA)

The objectives of performing a PCA on the database were to reduce the dimensionality of the data and to further attempt to discriminate between structure (by type, failure pdf, and size). Due to the difference in the units of the data, the PCA was performed using the data's correlation matrix (see Table F-5).

Variable	Ao	Ao S.D.	MTBDE	MTBDE S.D.	MDT	MDT S.D.	МТВМ	MTBM S.D.	MRT	MRT S.D.
Ao	1	-0.318	0.7206	0.6327	-0.5495	0.0577	-0.332	-0.2459	-0.658	-0.3873
Ao S.D.	-0.3177	1	-0.371	-0.2081	0.1285	0.4976	0.2352	0.5285	0.344	0.692
MTBDE	0.7206	-0.371	1	0.9219	-0.1915	0.1148	-0.173	-0.1442	-0.472	-0.2649
MTBDE S.D.	0.6327	-0.208	0.9219	1	-0.3184	0.169	-0.255	-0.1122	-0.41	-0.1986
MDT	-0.5495	0.1285	-0.192	-0.3184	1	0.0143	0.8225	0.5198	0.544	0.4617
MDT S.D.	0.0577	0.4976	0.1148	0.169	0.0143	1	0.1952	0.455	0.268	0.5232
MTBM	-0.3315	0.2352	-0.173	-0.2554	0.8225	0.1952	1	0.7034	0.547	0.5575
MTBM S.D.	-0.2459	0.5285	-0.144	-0.1122	0.5198	0.455	0.7034	1	0.549	0.7272
MRT	-0.6576	0.3435	-0.472	-0.4099	0.5439	0.2676	0.5474	0.5487	1	0.5559
MRT S.D.	-0.3873	0.692	-0.265	-0.1986	0.4617	0.5232	0.5575	0.7272	0.556	1

Table F-5. Data Correlation Matrix

JMP software calculated the principle components. Three components were retained based on Kaiser's criterion. As Table F-6 indicates, these components accounted for

81.85% of the data set variation.

EigenValue:	4.6365	2.19	1.363	0.5431	0.4333	0.3292	0.2094	0.1776	0.101	0.0219
Percent:	46.3649	21.859	13.626	5.4311	4.3333	3.2919	2.0938	1.7758	1.006	0.2187
Cum Percent	46.3649	68.224	81.85	87.2808	91.614	94.906	96.9998	98.7756	99.78	100

Table F-6. Component Eigenvalues and Percentages

Using the eigenvalues and eigenvectors (eigenvector multiplied by the square root of the corresponding eigenvalue), JMP calculated the loadings matrix. As shown in Table F-7,

only the first three loadings were analyzed.

	Component 1	Component 2	Component 3
Availability	-0.7264	0.49766	0.01967
Ao S.D.	0.615163	0.28342	-0.59
MTBDE	-0.607411	0.6781	0.35319
MTBDE S.D.	-0.572701	0.7072	0.16203
MDT	0.71309	-0.01032	0.6206
MDT S.D.	0.33791	0.6865	-0.3972
МТВМ	0.74412	0.21079	0.52521
MTBM S.D.	0.75028	0.47291	0.0949
MRT	0.81152	-0.05729	0.067
MRT S.D.	0.79726	0.39407	-0.1759

Table F-7. PCA Loadings Matrix

After careful examination of the above loading matrix, in conjunction with knowledge of

the database, each component was labeled based on the bold numbers in the respective

column of the matrix.

- Component 1 \rightarrow Maintenance Index
- Component 2 \rightarrow Deviation Down Time Index
- Component 3 → Down Time Average Index

After successfully reducing the dimensionality of the database from ten to three,

component scores were calculated to see if they were effective at discriminating a given

structure into the following attributes:

- Type: Complex or Series-Parallel
- Failure pdf: Increase Failure Rate (IFR) or Decreasing Failure Rate (DFR)
- Size: Large or Small

Each vector of component scores was sorted in descending order to look for a pattern. The noticeable patterns appear in Table F-8.

Com	ponent 1	Componen	Component 2					
Size	Score	Failure pdf Type	Score					
Small	3.9875798	DFR	4.2453607					
Small	3.27563	IFR	2.7344832					
Small	3.1916125	DFR	2.6642524					
Small	2.5766016	DFR	2.2635533					
Small	2.5624751	IFR	1.9337528					
Small	2.3625727	DFR	1.4825866					
Small	1.8048802	DFR	1.4374841					
Small	1.7765076	DFR	1.0900088					
Small	1,5808509	DFR	0.9908706					
Small	1.5494862	DFR	0.6643567					
Small	1.5341994	DFR	0.622185					
Small	1.256253	IFR	0.5673482					
Small	1.2471147	DFR	0.354911					
Small	1.0250701	DFR	0.2859006					
Small	0.6167541	DFR	0.2601498					
Large	0.5833746	DFR	0.2469027					
Small	0.4965454	DFR	0.0693093					
Large	0.4641742	IFR	-0.134626					
Small	0.4333046	IFR	-0.141776					
Small	0.2313683	DFR	-0.239745					
Large	0.2225142	IFR	-0.251629					
Small	-0.096977	IFR	-0.376745					
Large	-0.292476	DFR	-0.504691					
Large	-0.394207	IFR	-0.505771					
Small	-0.451488	IFR	-0.810156					
Large	-0.550943	IFR	-0.821429					
Large	-1.330643	IFR	-0.847647					
Large	-1.357726	IFR	-0.899332					
Large	-1.53975	IFR	-1.165003					
Large	-1.637563	DFR	-1.242413					
Large	-1.977937	DFR	-1.399575					
Large	-2.244068	IFR	-1.485876					
Large	-2.327493	IFR	-1.587855					
Large	-2.39671	IFR	-1.683993					
Large	-3.35344	IFR	-1.697677					
Large	-3.691377	DFR	-1.879922					
Large	-4.077877	IFR	-2.083892					
Large	-5.058193	IFR	-2.153662					

Table F-8. Component Scores

Even though the component scores do not discriminate completely, there appears to be some usefulness in these scores in determining the attributes of a given structure using the following formulas:

- If Component 1 Score $\geq 0 \rightarrow$ Classify the Structure as Small
- If Component 1 Score $< 0 \Rightarrow$ Classify the Structure as Large
- If Component 2 Score $\geq 0 \Rightarrow$ Classify the Structure as DFR
- If Component 2 Score $< 0 \rightarrow$ Classify the Structure as IFR

The component score 3 did not appear to have any discriminating power.

Identification of Underlying Factors (FA)

Factor analysis was performed on the database for two reasons: to identify any possible underlying factors and to use these factors to discriminate between the attributes of a given structure. Using SAS and varimax rotation, a rotated factor pattern was obtained. As can be seen in Table F-9, the underlying factors fell out very well.

	Factor 1	Factor 2	Factor 3
Avail	0.79513	-0.37048	-0.07841
Ao S.D.	-0.30561	0.02208	0.84431
MTBDE	0.9701	-0.01508	-0.11017
MTBDE S.D.	0.91457	-0.12722	0.04128
MDT	-0.21567	0.92026	-0.01965
MDT S.D.	0.21902	0.05537	0.832
МТВМ	-0.09176	0.91097	0.18895
MTBM S.D.	-0.02499	0.64731	0.61313
MRT	-0.47654	0.57019	0.33782
MRT S.D.	-0.19501	0.46513	0.75333

Table F-9. Rotated Factor Pattern (from SAS with Varimax Rotation)

- Factor 1 → Functionality
- Factor 2 -> Repair
- Factor 3 → Variance

The common variance contributions for each factor can be seen in Figure F-4.

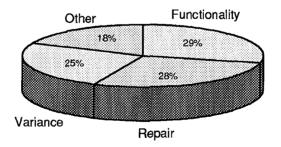


Figure F-4. Common Variance Contributions by Factor

Using standardized data, the factor scores were obtained for each of the three factors.

As with PCA, an attempt was made to discriminate a given structure by one of its three

attributes by sorting each factor score in descending order. As seen in Table F-10, factor scores 2 and 3 were very good at discriminating respectively between structure size and its failure rate pdf.

Size	Factor 2	Failure pdf Type	Factor 3
Small	1.754919849	DFR	2.375509734
Small	1.262692335	DFR	2.108713858
Small	1.257212778	IFR	1.879361215
Small	1.248601501	DFR	1.412724627
Small	1.198436102	DFR	1.338927349
Small	1.171639447	DFR	1.319662935
Small	1.160513013	DFR	0.809561313
Small	1.148780849	DFR	0.752946945
Small	1.070286433	DFR	0.476564177
Small	1.041964654	IFR	0.402846391
Small	0.803497969	DFR	0.39528509
Small	0.781802256	DFR	0.351588765
Small	0.708731145	DFR	0.312586852
Small	0.645365044	IFR	0.298188266
Small	0.636668185	DFR	0.287840003
Small	0.616611494	DFR	0.235440949
Small	0.581937118	DFR	0.217068964
Small	0.058035318	DFR	0.0410742
Small	0.045624986	DFR	-0.116572823
Small	-0.135169869	DFR	-0.154178944
Large	-0.157786373	DFR	-0.209412144
Large	-0.304504477	IFR	-0.331720076
Large	-0.712301993	IFR	-0.357517609
Large	-0.754459578	IFR	-0.382424315
Large	-0.796558728	DFR	-0.52311732
Large	-0.818000077	IFR	-0.624436134
Large	-0.874071803	IFR	-0.652270592
Large	-0.917883041	IFR	-0.658484054
Large	-0.925917777	IFR	-0.728537638
Large	-0.975227776	IFR	-0.751696689
Large	-1.066756545	IFR	-0.788207166
Large	-1.081593052	IFR	-0.84117866
Large	-1.104270837	IFR	-0.871777043
Large	-1.109476158	IFR	-1.021398497
Large	-1.301022087	IFR	-1.239891531
Large	-1.306582726	IFR	-1.303301235
Large	-1.327933971	IFR	-1.459488901
Large	-1.523803607	IFR	-2.00028026

Table F-10. Factor Scores

• If Factor Score $2 \ge -0.15$	→	Classify the Structure as Small
• If Factor Score 2 < -0.15	→	Classify the Structure as Large
• If Factor Score $3 \ge -0.30$	→	Classify the Structure as DFR
• If Factor Score 3 < -0.30	→	Classify the Structure as IFR

Factor score 1 did not appear to have any discriminating power.

Insights

Several useful conclusions can be drawn from this study. First, it was demonstrated (using a moderately small sample size) that successful discrimination can occur between large versus small, complex versus series-parallel, and IFR versus DFR component structures based on RAPTOR simulation output. All multivariate techniques demonstrated were moderately-to-highly successful in discriminating between the defined classes. Through the discrimination analysis, it was discovered that predominantly DFR structures display a relatively higher simulation output variability. Therefore, RAPTOR availability model output variability serves as a good discriminant for IFR versus DFR structures. Furthermore, Mean Time Between Maintenance (MTBM) is an excellent discriminant variable for the large versus small structure classification case. This conclusion makes intuitive sense, since one would expect a decrease in the average time between maintenance actions on components as the number of components in the structure increases. The analysis provides empirical support to this intuitive assessment. Additionally, it was discovered that neural nets can be used to effectively discriminate when the discriminant function may be of a higher order.

Additionally, the analysis revealed that the RAPTOR simulation output variance can be explained via 3 principal components: a maintenance index, a deviation down time index, and a down time average index. A majority of the output variance (82%) is explained by these three components. By using a rank order of the maintenance index

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(component 1) scores and deviation down time index (component 2) scores, reasonable discrimination between large and small structures, and IFR and DFR structures respectively, can be achieved.

Finally, three underlying factors were identified by use of factor analysis. The first factor, functionality, relates to the structure's ability to get the job done in an efficient manner. The second factor, repair, reflects the maintenance and down time which is inherent in the structure. The third factor, variance, refers to the inherent variability of the output variables measured for each structure. Some success was also achieved in discrimination between large versus small structures and IFR versus DFR structures by using a rank order of the repair factor (factor 2) scores and variance factor (factor 3) scores respectively.

Throughout the discrimination analysis, consistency in the results was observed for each of the various methods used: similar classification accuracy and similar best discriminant variable selections. This consistency was further highlighted when component/factor score rankings were used as a discriminant. For example, based on the DA observations one would expect the factor which represents maintenance/repair (factor 2) to be the best in large versus small discrimination. This in fact was the case, with the factor 2 scores being the best large/small discriminant among all factor scores. The same proved true for factor 3 (variability) and IFR versus DFR discrimination. This consistency in results provided increased confidence in the conclusions.

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Vita

Major Darren P. Durkee **Academy**. Upon graduation, he attended Undergraduate Navigation States Air Force Academy. Upon graduation, he attended Undergraduate Navigation Training (UNT) and Electronic Warfare Training at Mather AFB, CA. He subsequently served in several flying assignments compiling over 4000 hours as a navigator and electronic warfare officer (EWO), including tours flying the RC-135 Rivet Joint at Offutt AFB, NE, the EC-130H Compass Call at Sembach AB, Germany, and the E-3 Airborne Warning and Control System (AWACS) at Tinker AFB, OK. During his flying tours, he served in several staff positions at the Wing and Air Division level in the areas of training, standardization and evaluation, requirements, and weapons and tactics. Major Durkee was selected to attend the AFIT Graduate Program in Operations Research in 1995. Upon graduation from AFIT in March 1997, he was assigned to the Air Staff as an operations analyst in the Air Force Studies and Analysis Agency, Pentagon,

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1. AGENCY USE ONLY (Leave blank)	2. REPORT DATE February 1997	3. REPORT TYPE ANI Master	o dates cov 's Thesis			
 4. TITLE AND SUBTITLE SENSITIVITY OF AVAILAE TO INPUT DATA CHARAC 6. AUTHOR(S) Darren P. Durkee, Major, USA 	TERIZATION		5. FUNDING	I NUMBERS		
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) Air Force Institute of Technology/ENS 2750 P Street Wright-Patterson AFB, Ohio 45433-7765			REPORT	NING ORGANIZATION NUMBER GOR/ENS/97-06		
9. SPONSORING/MONITORING AGENCY HQ AFOTEC/SAL 8500 Gibson Blvd. SE Kirtland AFB, NM 87117	NAME(S) AND ADDRESS(ES)			RING/MONITORING REPORT NUMBER		
11. SUPPLEMENTARY NOTES						
12a. DISTRIBUTION / AVAILABILITY STAT Approved for Public Release;		d	12b. DISTRIE	BUTION CODE		
13. ABSTRACT (Maximum 200 words)		Need taken procedure that the first and the first standard and the standard and the standard and the standard	a data mandarat separata dan meneri di 2002 ad 400	5 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -		
Reliability analysts are often faced with the challenge of characterizing the behavior of system components based on limited data. Any insight into which model input data is most significant and how much data is necessary to achieve desired accuracy requirements will improve the efficiency and cost effectiveness of the data collection and data characterization processes. This thesis assesses potential significant factors in the probabilistic characterization of component failure and repair behavior with respect to the effect on system availability estimates. Potential factors were screened for significance utilizing fractional factorial and Plackett-Burman experimental designs for several system models developed using an AFOTEC simulation program entitled RAPTOR. Two input data characterization factors were found to have a significant affect on availability estimation accuracy: the size of the structure and the number of data points used for component failure and repair distributional fitting. Estimation error was minimized when the structures analyzed were small and many data points (in this case, 25) were used for the distributional fittings. Assuming constant component failure rates and using empirical repair distributions were found to be equally effective component characterization methods (pertaining to model availability estimation error) compared to using automated software fitting tools (or 'wizards'). The results of this study also indicate that there is no apparent benefit in concentrating on 'important' components for the highest fidelity distributional fittings.						
14. SUBJECT TERMS Availability Estimation, Fractiona Component Reliability, Distribution				. NUMBER OF PAGES 134 . PRICE CODE		
17. SECURITY CLASSIFICATION 18. OF REPORT	SECURITY CLASSIFICATION OF THIS PAGE Unclassified	19. SECURITY CLASSIFIE OF ABSTRACT Unclassified		UL Join 298 (Rev. 2-89)		