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#### 1 Co-generation of hydroxyl and sulfate radicals via homogeneous and heterogeneous

bi-catalysis with the EO-PS-EF tri-coupling system for efficient removal of refractory 2

#### 3 organic pollutants

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14 Abstract: Advanced oxidation processes are commonly considered one of the most effective techniques to degrade refractory 15 organic pollutants, but the limitation of a single process usually makes it insufficient to achieve the desired treatment. This 16 work introduces, for the first time, a highly-efficient coupled advanced oxidation process, namely Electro-Oxidation-Persul-17 fate—Electro-Fenton (EO-PS-EF). Leveraging the EO-PS-EF tri-coupling system, diverse contaminants can be highly efficiently 18 removed with the help of reactive hydroxyl and sulfate radicals generated via homogeneous and heterogeneous bi-catalysis, 19 as certified by radical quenching and electron spin resonance. Concerning degradation of tetracycline (TC), the EO-PS-EF system 20 witnessed a fast pseudo-first-order reaction kinetic constant of 2.54 × 10<sup>-3</sup> s<sup>-1</sup>, ten times that of a single EO system and three-21 to-four times that of a binary system (EO-PS or EO-EF). In addition, critical parameters (e.g., electrolyte, pH and temperature) 22 are systematically investigated. Surprisingly, after 100 repetitive trials TC removal can still reach 100% within 30 minutes and 23 no apparent morphological changes to electrode materials were observed, demonstrating its long-term stability. Finally, its 24 universality was demonstrated with effective degradation of diverse refractory contaminants (i.e., antibiotics, dyes and pesti-25 cides).

26 Keywords: Electro-Oxidation—Persulfate—Electro-Fenton; Hydroxyl and sulfate radicals; Mechanism; Degradation pathway; 27 Application potential

#### 28 **1** Introduction

29 Environmentally-related contaminants (e.g., antibiotics, pesticides, industrial chemicals and persistent organic pollutants) 30 are emerging and ubiquitous in the environment, such as the soil, surface water and groundwater, causing devasting threats 31 to the ecological environment and human health. The environmental damage and biological toxicity of these emerging con-32 taminants have developed into a challenging multidisciplinary issue and are yet to be resolved (Johnson et al., 2020; Liu et al., 33 2021b). Hydroxyl radicals-based advanced oxidation processes (AOPs), also known as deep oxidation processes, are considered 34 one of the most effective techniques to decompose these environmental pollutants owing to their fast reaction rate and capa-35 bility of completely removing and recycling the treated wastewater (Lu et al., 2022; Zheng et al., 2022). The outstanding feature 36 37 of AOPs results from the generation of hydroxyl radicals (·OH) with a strong oxidizing ability through homogeneous or heterogeneous catalysis, which is considered the most powerful oxidant to degrade refractory organic pollutants in water.

38 Among AOPs, the Fenton method is prone to generate ·OH via the homogeneous reaction between Fe<sup>2+</sup> and H<sub>2</sub>O<sub>2</sub>, but at 39 the cost of large consumption of  $H_2O_2$  and the production of iron sludge. In addition, this method is only applicable to the 40 limited acidic water pH condition, which significantly narrows the industrial applications toward wastewater treatment. In con-41 trast, no additional H<sub>2</sub>O<sub>2</sub> needs supplemented throughout Electro-Fenton (EF) process (Lin et al., 2022). This is because H<sub>2</sub>O<sub>2</sub> 42 can be continuously produced by electroreduction of  $O_2$  at the cathode with high overpotentials, followed by a homogeneous 43 reaction with additive Fe<sup>2+</sup> to generate homogeneous ·OH, and the oxidant (Fe<sup>3+</sup>) can be reversibly reduced back to Fe<sup>2+</sup>, as 44 described in Eqs. (1-3) respectively, thus creating a catalytic loop to accelerate the removal of water contaminants (Hu et al., 45 2021; Liu et al., 2019; Liu et al., 2021a). In addition, heterogeneous OH can be generated via Electro-Oxidation (EO) of H<sub>2</sub>O on 46 the surface of a "non-active" anode, among which boron-doped diamond (BDD) exhibited the highest OH generation efficiency 47 and is considered the ideal anode material for wastewater treatment (see Eq. (4)) (Du et al., 2021). Synergistic effects of com-48 bining EO and EF were observed, and this bi-coupling system was capable of greatly enhancing the removal of refractory organic 49 pollutants, such as synthetic wastewater and real wastewater, owing to the dual catalytic treatment via homogeneous OH and 50 heterogeneous BDD(·OH) (Nidheesh et al., 2022). However, EO-EF still encountered unsatisfactory limitations such as strict pH control, loss of soluble iron catalyst due to ferric hydroxide precipitation and relatively high energy costs (He and Zhou, 2017).

51 52 53 Sulfate radicals-based AOPs have recently received widespread attention because sulfate radicals (SO4") exhibit apparent advantages over ·OH, including relatively higher generation potentials (E<sup>0</sup> = 2.5-3.1 V versus 1.9-2.7 V), stronger selectivity, and 54 longer lifespan (30-40 μs versus 20 ns) respectively. It is noted that SO<sub>4</sub><sup>--</sup> can diffuse further to react with contaminants in bulk 55 solution due to its considerably long lifetime (Yang et al., 2021). SO<sub>4</sub><sup>--</sup> is generally produced by breaking the peroxygen bond in

56 peroxymonosulfate or peroxydisulfate. The latest research demonstrated that it could be generated by persulfate (PS) via ho-57 mogeneous or heterogeneous catalysis with the help of transition metals, electricity, heat, ultrasound, ultraviolet light and 58 quinones (Wang and Wang, 2022). In terms of homogeneous catalysis, Fe<sup>2+</sup> is considered one of the best candidates for acti-59 vating PS to generate  $SO_4$  due to its environmental soundness, high abundance, low cost and high efficiency (see Eq. (5)), as 60 previously reported in the treatment of organic pollutants (Hou et al., 2021; Xiao et al., 2020). As for heterogeneous catalysis, 61  $SO_4^{-1}$  can be efficiently generated via electroreduction of PS (see Eq. (6)) and electrooxidation of  $SO_4^{-2}$  (see Eq. (7)), during which 62 PS can be regenerated via electrochemical oxidation of  $SO_4^{2-}$  (see Eq. (8)), creating a catalytic loop to greatly reduce the addition 63 of PS (Divyapriya and Nidheesh, 2021). In addition, the introduction of PS in the electrolyte can increase its conductivity and 64 thus the response current (or reduce the cell voltage), which in turn promotes the mass transport of the system and accelerates 65 the degradation efficiency.

Previous studies demonstrated that the combination of EO and PS (EO-PS) allowed the simultaneous generation of heterogeneous ·OH and SO4<sup>--</sup> during electrochemical activation of PS using BDD anode or graphite felt (GF) cathode and demonstrated the synergistic degradation efficiency toward refractory organic pollutants (Bu et al., 2019; Song et al., 2018; Zhi et al., 2020). Arellano et al. (Arellano et al., 2019) introduced the catalyst of iron-based minerals in the EO-PS system for activation of peroxymonosulfate and achieved effective degradation of 1-butyl-1-methylpyrrolidinium chloride. Until now, little research was reported regarding the co-activation of PS by the BDD anode and the GF cathode at the same time, not to mention the synergistic coupling effect in complicated wastewater environments while introducing EF in this system.

73 Herein, the Electro-Oxidation—Persulfate—Electro-Fenton (EO-PS-EF) triple coupling system was proposed to efficiently 74 75 degrade refractory organic pollutants via homogeneous and heterogeneous catalytic co-generation of •OH and SO4<sup>--</sup>. Taking TC as the benchmark pollutant, the performance of the single system and the coupled system were systematically compared to 76 assess the coupling effect. Effects of seven key parameters, including the concentration of PS and Fe<sup>2+</sup>, air flow rate, the species 77 and concentration of inorganic anion, solution pH and temperature, on the degradation performance are considered based on 78 TC removal rate and kinetics. Reactive species in the coupling system are identified by radical quenching and electron spin 79 resonance spectroscopy. The intermediates during TC degradation were analyzed and identified by liquid chromatography-80 mass spectrometry to determine the possible degradation pathway. In addition, degradation performance (i.e., energy con-81 sumption analysis, long-term degradation stability and degradation selectivity) toward additional organic pollutants, including 82 Orange G (OG), Reactive Blue 19 (RB-19), 2,4-Dichlorophenoxyacetic acid (2,4-D) and Atrazine (ATZ), were investigated via the 83 established EO-PS-EF system.

# 84 **2** Materials and methods

# 85 2.1 Chemicals and materials

86 Tetracycline (TC, >95%), Reactive Blue 19 (RB-19, ≥99.5%), Orange G (OG, ≥96%), Atrazine (ATZ, 97%), 2,4-Dichlorophe-87 noxyacetic acid (2,4-D, 97%), Methanol (MeOH, 99.5%), tert-Butanol (TBA, ≥98%), and 5,5-Dimethyl-1-pyrroline-N-oxide 88 (DMPO, 97%) were purchased from McLean, China. Sodium persulfate (PS, 98%), Ferrous sulfate heptahydrate (FeSO<sub>4</sub>·7H<sub>2</sub>O, 89 ≥99%), Sodium sulfate (Na<sub>2</sub>SO<sub>4</sub>, 99%), Sodium chloride (NaCl, 99.5%), Sodium phosphate (Na<sub>3</sub>PO<sub>4</sub>, 98%), Sodium carbonate 90 (Na<sub>2</sub>CO<sub>3</sub>, ≥99.8%), Sodium nitrate (NaNO<sub>3</sub>, ≥99%), Sodium hydroxide (NaOH, 96%), Sulfuric acid (H<sub>2</sub>SO<sub>4</sub>, 98%) were purchased 91 from Sinopharm, China. All chemicals were used without further purification. All solutions were prepared with ultrapure water 92 (UPT-I-10T, ACCEXP, China). Graphite felt (GF, 3 mm thickness) was purchased from Jinglong Special Carbon, China. The prepa-93 ration of flat Ti/BDD used in this work referred to the previous work (Yang et al., 2022a).

# 94 2.2 Electrochemical degradation

The electrochemical reactor consisted of a cylindrical electrolytic cell, anode, cathode, DC power supply (RD-2030, Suzhou Wanruida, China), collector-type thermostatic heating magnetic stirrer (DF-101S, Shanghai Lichen Bonsi, China) and air pump (SB-748, Zhongshan Songbao, China) (see Scheme 1). The anode was BDD or 304 stainless steel (SS) electrode, and the cathode was GF or SS electrode. The anode and cathode were placed in parallel with an equal geometric area of 4 cm<sup>2</sup> and an interspace of 1 cm. A uniformly distributed aeration device connected to the air pump was placed right below the cathode.

100 All degradation experiments were performed with a constant direct current model at the fixed value of 0.2 A and the 101 reactor was under constant stirring with a speed of 300 rpm. Before electrochemical degradation, the electrode system was 102 pre-cleaned with a constant current of 0.2 A for 30 min in 50 mM Na<sub>2</sub>SO<sub>4</sub> solution. The volume of simulated wastewater is 0.25 103 L and the initial concentration of organic pollutants is 0.1 mM. The solution pH was adjusted with the concentrated H<sub>2</sub>SO<sub>4</sub> and 104 NaOH, and a water bath maintained the reactor temperature. Prior to the degradation experiment, the solution was saturated 105 with  $O_2$  pumped by the compressed air at a flow rate of 0.25 L min<sup>-1</sup> for 15 min to ensure the electrosynthesis of  $H_2O_2$ . The 106 subsequent O<sub>2</sub> concentration was maintained by air supply at various flow rates. Samples were collected at fixed five-minute 107 intervals for analytical determinations, and the initial sample was used as the control. All experiments were repeated at least 108 three times and the averaged data are shown in the text.

# 109 2.3 Analysis methods

110TC, ATZ and 2,4-D concentrations were measured by high-performance liquid chromatography (HPLC, Agilent LC1290) with111an adjustable wavelength UV detector, equipped with an ACE, UltraCore C18 column (2.1 × 75 mm, 2.5 µm). Before analysis,112water samples were filtered using Whatman PTFE membranes (0.22 µm). Detailed analytical parameters were provided in the

supplementary materials (see Table S1). The concentrations of OG and RB-19 were measured by UV-visible spectrophotometer
 (UV-8000S, METASH, China) based on the absorbance at the maximum absorption wavelength (478 nm and 596 nm, respectively). The physicochemical information of these refractory organic pollutants is presented in Table S2.

116TC degradation intermediates were characterized by liquid chromatography-mass spectrometry (LC-MS, Agilent LC1290-117QQQ-6470) at the column temperature of 40°C and the autosampler temperature of 25°C. The sample was analyzed by elec-118trospray ionization (ESI) in a positive mode over a mass range of 30-600 amu. The supplementary materials refer to mobile119phase ratios, gradient elution parameters, and other LC-MS detection information.

120 The electron spin resonance (ESR, Bruker A300, Germany) was used to detect transient free radicals in the system. At the 121 specified reaction time intervals, 100  $\mu$ L of the solution near the anode surface was injected into 50  $\mu$ L of 100 mM DMPO trap 122 using a capillary tube. The ESR measurements were performed with a power of 6.32 mW, a central field of 3510 G, a sweep 123 width of 100 G, and microwave and modulation frequencies of 9.87 GHz and 100 GHz respectively.



Scheme 1. Schematic illustration of the electrochemical reactor.

### 126 **3** Results and discussion

124 125

# 127 **3.1 Establishment of the EO-PS-EF tri-coupling system**

# 128 **3.1.1** Synergistic effects of the EO-PS bi-coupling system

Fig. 1 gradually illustrates the establishment of the EO-PS bi-coupling system according to the degradation performance of TC, that is, the removal of TC and corresponding degradation kinetics. Note that statistical analysis of the TC removal by heat map is first introduced to clearly compare and uncover the effects of diverse parameters on the degradation performance. Three key control experiments are first presented in which almost no TC removal after 30 min was observed by GF adsorption or PS alone, or both (see the top panel in Fig. 1), indicating that GF and PS themselves cannot physicochemically remove TC and the unbiased GF cannot activate PS to generate the active radical species, in agreement with the observation from the unbiased BDD electrode (Song et al., 2018).

136 Previous works indicated that the BDD anode and the GF cathode could activate PS through different reaction mecha-137 nisms. Thus, in order to uncover this claim and clarify the contribution of PS activation at the BDD anode and GF cathode toward 138 TC degradation, control experiments were carried out with the stainless steel (SS) electrode, which is difficult to activate PS (Bu 139 et al., 2019). (i) When SS and GF were used as anode and cathode respectively, named as (+)SS|GF(-), partial degradation of TC 140 (11% at 30 min) was observed, which is mainly attributed to the direct oxidation on the SS anode. The addition of 10 mM PS, 141 (+)SS[1X PS]GF(-), increased the TC removal from 11% to 18% at 30 min, and the reaction rate constant (k) increased from 6.52 142  $\times$  10<sup>-5</sup> s<sup>-1</sup> to 1.09  $\times$  10<sup>-4</sup> s<sup>-1</sup>. The enhanced TC removal was probably attributed to the effective activation of PS at the GF cathode. 143 (ii) When BDD and SS were used as anode and cathode, (+)BDD|SS(-), the TC removal without and with adding 10 mM PS 144 increased to 23% and 33%, accounting for the 12% and 15% increase compared to the counterparts of (+)SS | GF(-), respectively. 145 The improved capability toward TC removal presumably results from the activation of PS on the BDD anode and the GF, while 146 the former exhibited a superior activation performance (10% enhancement ratio after adding 10 mM) than the latter (7% en-147 hancement ratio), indicating the difference in the electro-activation mechanism of PS on the BDD anode and the GF cathode. 148 In addition, the TC removal increased with increasing PS concentrations from 10 mM to 40 mM for both (+)BDD|SS(-) and 149 (+)SS|GF(-) systems, along with enhanced reaction rate constant at high PS concentrations.

At the GF cathode, PS activation to produce  $SO_4^{--}$  is attributed to electrochemical reduction via direct electron transfer (DET). Moreover, superoxide anion  $(O_2^{--})$ , which is converted from electrons captured by dissolved  $O_2$  (from the pumping air and oxygen evolution at the anode) at the cathode surface, is a crucial intermediate for PS activation at the GF cathode (Eq. (9) and Eq. (10)) (Bu et al., 2019). A recent study proposed that anodic discharge at the BDD anode could convert adsorbed PS molecules into a special transition state structure PS\* (Eq. (11)), which could degrade pollutants as a non-radical oxidation 155pathway (Song et al., 2018). At the same time, PS\* molecules can promote ·OH production and enhance DET reactions through156water hydrolysis at the BDD anode. Notably, SO<sub>4</sub><sup>--</sup> and PS can be generated through electrochemical activation of SO<sub>4</sub><sup>2-</sup>, HSO<sub>4</sub><sup>--</sup>157or H<sub>2</sub>SO<sub>4</sub> owing to the powerful oxidizing capacity of the BDD anode (Divyapriya and Nidheesh, 2021). Meanwhile, the decom-158position of SO<sub>4</sub><sup>--</sup> and PS will produce a large amount of SO<sub>4</sub><sup>2-</sup>, which can ensure the recycling of SO<sub>4</sub><sup>2-</sup>/PS/SO<sub>4</sub><sup>--</sup> to a certain extent.159The catalytic activation loop of SO<sub>4</sub><sup>2-</sup>, PS and SO<sub>4</sub><sup>--</sup> on the BDD anode endows its better TC degradation performance than the160GF cathode activation.

161 To investigate the activation of PS at both the BDD anode and the GF cathode, 10 mM PS was added to the (+)BDD | GF(-) 162 system, and TC removal, before and after PS addition, was observed to be 37% and 46%, respectively. The addition of PS in-163 creased the degradation rate constant from  $2.50 \times 10^{-4}$  s<sup>-1</sup> to  $2.88 \times 10^{-4}$  s<sup>-1</sup>, and a synergistic effect of activating PS at the EO-164 PS bi-coupling system was observed. Later, the effect of PS concentrations (i.e., 10, 20, 30 and 40 mM) on the (+)BDD|GF(-) 165 system was investigated. As the concentration increased from 10 mM to 20 mM, the TC removal increased from 46% to 64% 166 and the reaction rate constant was found to increase from 2.88 × 10<sup>-4</sup> s<sup>-1</sup> to 7.24 × 10<sup>-4</sup> s<sup>-1</sup> respectively, attributed to a significant 167 increase in the activation numbers of PS molecules with increasing concentrations. However, as the concentration continuously 168 increased to 30 mM and 40 mM, the TC removal did not expect to increase but in return, a slight inhibition was observed. These 169 results can be explained by the reorganization of  $SO_4^{--}$  and the consumption of  $SO_4^{--}$  (or  $\cdot OH$ ) with excess PS (Eqs. (12-14)), as 170 observed in previous works (Divyapriya and Nidheesh, 2021; Zhang et al., 2021; Zhu et al., 2018). In a nutshell, the PS can 171 greatly promote TC removal at relatively low concentrations (e.g., less than 20 mM), but excess PS (≥ 30 mM) adversely inhib-172ited its removal. Note that the (+)BDD|GF(-) system exhibits faster TC degradation efficiency than the systems of (+)BDD|SS(-) 173 and (+)SS|GF(-) under the identical addition of PS for all concentrations.

The subsequent studies will be carried out under the optimal PS concentration (i.e., 20 mM) on the (+)BDD|GF(-) system, which is named the EO-PS bi-coupling system.



176

177 Fig. 1. Establishment of the EO-PS bi-coupling system. (a) Comparative heat map showing the removal rate of TC under various 178 process parameters. 1X, 2X, 3X and 4X PS correspond to 10, 20, 30 and 40 mM PS. The symbol (+) and (-) refers to the anode 179 and cathode respectively. The solution contains 50 mM Na<sub>2</sub>SO<sub>4</sub> electrolyte, and pH and temperature are maintained at 7 and 180 20 °C, respectively. (b) Corresponding pseudo-first-order reaction rate constants.

# 181 **3.1.2** Synergistic effects of the EO-PS-EF tri-coupling system

182 In the tri-coupling system,  $Fe^{2+}$  and air are considered homogeneous and heterogeneous catalytic co-generation of  $\cdot OH$ and  $SO_4^{--}$ . Fig. 2 gradually illustrates the establishment of the EO-PS-EF tri-coupling system. In the EO-PS bi-coupling system, as the  $Fe^{2+}$  concentration increased from 0 to 0.1 mM, the TC removal in 5 min increased from 26% to 79%, and the reaction rate constant increased from 7.24 × 10<sup>-4</sup> s<sup>-1</sup> to 3.51 × 10<sup>-3</sup> s<sup>-1</sup>. It was observed that the degradation of TC by the EO-PS-Fe<sup>2+</sup> system has two-stage reaction kinetic characteristics, with an initial slump and a later decay. In the initial stage, the homogeneous catalytic reaction between  $Fe^{2+}$  and PS with a reaction rate constant of up to  $4.84 \times 10^{-4} s^{-1}$  led to the rapid generation of  $SO_4^{--}$ , 188greatly accelerating the TC removal. After that, most of  $Fe^{2+}$  was oxidized to  $Fe^{3+}$ , and the reactive oxygen species were mainly189supplied via heterogeneous electrochemical reactions with a relatively slow reaction rate, mainly including exclusive BDD ano-190dization ( $k = 2.50 \times 10^{-4} \, s^{-1}$ ) and electro-activation of PS ( $k = 4.74 \times 10^{-4} \, s^{-1}$ ). In addition, the competing intermediates during the191latter period reacted with the reactive species, partially accounting for the decay of TC removal. Thus, TC removal rates dra-192matically decreased during the heterogeneous reaction period. This phenomenon was also observed from the control experi-193ment with only 0.05 mM Fe<sup>2+</sup> and 20 mM PS, during which 37% of TC was degraded within 5 min, but only 14% of TC was194removed in the following 25 min.

195It was noted that Fe(II) and Fe(III) ions have a strong tendency to complex with TC due to the complexation sites of N-type196and O-type structures on the A-ring of the TC molecule. The complexation of Fe(II) and TC could accelerate the oxidation of197Fe(II), thus promoting the degradation of TC (Zhang et al., 2022). As shown in the control experiment, 0.05 mM Fe<sup>2+</sup> exclusively198achieved 5% TC removal within 30 min owing to the generation of reactive oxygen species (mainly ·OH) while the Fe(II)-TC199complex was oxidized to the Fe(III)-TC complex by dissolved oxygen. In addition, the Fe(III)-TC complex could spontaneously200transfer to TC oxidation intermediates and Fe(II) (Wang et al., 2016). Thus, the Fe cycle was established between the Fe(II),201Fe(III), Fe(II)-TC and Fe(III)-TC, thus promoting TC removal.

202 The EF system mainly involves the reaction of  $Fe^{2+}$  and  $H_2O_2$  to generate  $\cdot OH$ . The formation of  $H_2O_2$  can be achieved by 203 the electrochemical reduction of  $O_2$  at the GF cathode. The EO-EF system was established by adding 0.05 mM Fe<sup>2+</sup> and the 204 pumping air at a flow rate of 0.25 L min<sup>-1</sup> to the EO system, which has slightly enhanced degradation performance than the EO-205 PS system, accounting for 5% higher TC removal. This may be related to the amount of catalysts (Fe<sup>2+</sup>, aeration and PS), the 206 complexation effect of Fe-TC and the selective oxidation of the dominant active species in different systems. Two parameters 207 of the concentration of Fe<sup>2+</sup> and the airflow rate were considered to optimize the EO-PS-EF system. Note that as the Fe<sup>2+</sup> con-208 centration doubled, only 11% of increasing TC removal rate was observed at 5 min and all those concentrations (0.05, 0.75 and 209 0.1 mM) could achieve 100% of TC removal within a considerable time (less than 30 minutes). Thus, 0.05 mM of Fe<sup>2+</sup> is chosen 210 for subsequent studies to facilitate comparison and reduce the addition of chemicals. The airflow rate itself did not exhibit the 211 apparent enhancement after addition, only with a 4% improved TC removal rate compared to the bare EO-PS system, and the 212 degradation performance remained unchanged with increasing concentrations (see the 3rd panel in Fig. 2). However, after 213 adding 0.05 mM of Fe<sup>2+</sup>, Fenton reactions can occur after aeration due to the presence of Fe<sup>2+</sup>, and the degradation perfor-214 mance of this system greatly increased, constituting a powerful EF system. Undeniably, the introduction of oxygen has a pro-215 nounced enhancement effect on the EO-PS-EF system, as observed from the comparison of EO-PS-Fe<sup>2+</sup> (0.05 mM Fe<sup>2+</sup>) and EO-216 PS-EF<sub>1</sub> (0.05 mM Fe<sup>2+</sup> + 0.25 L min<sup>-1</sup> Air), with the increment ratio of reaction kinetic constant up to 22% (from 2.08 ×  $10^{-3}$  s<sup>-1</sup> to 217  $2.54 \times 10^{-3}$  s<sup>-1</sup>). However, the effect of continuous enhancement is less significant when the oxygen flow rate further increases 218 from 0.25 L min<sup>-1</sup> to 1 L min<sup>-1</sup> (see the bottom panel in Fig. 2). The reason why the degradation of TC did not increase under a 219 high airflow rate could be attributed to the competition of oxygen reduction reaction, hydrogen evolution reaction and PS 220 activation reaction at the GF cathode. In addition, extremely high air flow rates might fill a large amount of air in the reactor, 221 which could hinder electrode/solution contact or even ion transfer. Thus, the airflow rate of 0.25 L min<sup>-1</sup> was suggested for 222 subsequent studies.

In summary, the EO-PS-EF tri-coupling system was successfully established, which could achieve homogeneous and heterogeneous catalytic co-generation of OH and SO<sub>4</sub><sup>--</sup> and exhibit powerful degradation performance for TC.



Fig. 2. Establishment of the EO-PS-EF tri-coupling system. (a) Degradation of TC by 0.05 mM Fe<sup>2+</sup>, 20 mM PS + 0.05 mM Fe<sup>2+</sup>, 20 mM PS + 0.05 mM Fe<sup>2+</sup>, EO-EF<sub>1</sub> (0.05 mM Fe<sup>2+</sup> + 0.25 L min<sup>-1</sup> Air), EO-PS-Fe<sup>2+</sup> (0.05, 0.75 and 0.1 mM Fe<sup>2+</sup>), EO-PS-Air flow rate (0.25, 0.5 and 1 L min<sup>-1</sup>), EO-PS-EF<sub>1</sub> (0.05 mM Fe<sup>2+</sup> + 0.25 L min<sup>-1</sup> Air), EO-PS-EF<sub>2</sub> (0.05 mM Fe<sup>2+</sup> + 0.5 L min<sup>-1</sup> Air) and EO-PS-EF<sub>3</sub> (0.05 mM Fe<sup>2+</sup> + 1 L min<sup>-1</sup> Air). The solution contains 50 mM Na<sub>2</sub>SO<sub>4</sub> electrolyte, and pH is fixed at 7 and temperature at 20 °C. (b) Corresponding pseudo-first-order reaction rate constants.

# 231 **3.2 Effects of inorganic anion species and concentration**

232 Inorganic anions often act as radical scavengers for the radical-based AOPs and are thus considered. Five common inor-233 ganic anion species (NO<sub>3</sub><sup>-</sup>, SO<sub>4</sub><sup>2-</sup>, PO<sub>4</sub><sup>3-</sup>, CO<sub>3</sub><sup>2-</sup> and Cl<sup>-</sup>) with various concentrations (0, 20, 50 and 100 mM) were comparatively 234 considered, as shown in Fig. 3. NO<sub>3</sub><sup>-</sup>, SO<sub>4</sub><sup>2-</sup>, PO<sub>4</sub><sup>3-</sup> and CO<sub>3</sub><sup>2-</sup> adversely inhibited the degradation performance of the EO-PS-EF 235 system, with the inhibition effect of  $NO_3^- < SO_4^{2-} < CO_3^{2-} < PO_4^{3-}$ . The inhibition phenomenon was improved with increasing ion 236 concentrations, which is more pronounced with SO<sub>4</sub><sup>2-</sup> and PO<sub>4</sub><sup>3-</sup>. In contrast, the introduction of Cl<sup>-</sup> could promote the removal 237 238 of TC molecules in the EO-PS-EF system, and the degradation performance was enhanced with increasing concentrations. Among the inhibition ions, NO<sub>3</sub><sup>-</sup> has minimal effect on TC removal, and this results from the relatively low reaction rate constant 239 for quenching active radicals (e.g., •OH and SO<sub>4</sub><sup>--</sup>). Meanwhile, a high overpotential is required for the oxidation of NO<sub>3</sub><sup>--</sup> to NO<sub>3</sub><sup>--</sup> 240 (see Eqs. (15-17)), as indicated in the previous works (Bu et al., 2018; Huang et al., 2021; Lee et al., 2020). The inhibition effect 241 of SO<sub>4</sub><sup>2-</sup> was possibly attributed to the limited active adsorption sites on the BDD surface and the competitive adsorption be-242 tween SO<sub>4</sub><sup>2-</sup> and PS partially rendered the electro-activation of PS (Cai et al., 2019a; Ding et al., 2020). Under neutral pH,  $PO_4^{3-}$ 243 exists in the forms of H<sub>2</sub>PO<sub>4</sub><sup>-</sup> and HPO<sub>4</sub><sup>2-</sup> that are not only powerful scavengers of ·OH and SO<sub>4</sub><sup>--</sup>, but also affect charge consump-244 tion (Eqs. (18-23)) (Bu et al., 2018; Wang and Wang, 2020; Xu et al., 2017). The resulting phosphate reactive species (e.g., HPO4<sup>--</sup>, 245 H<sub>2</sub>PO<sub>4</sub>) have too low activities to oxidatively degrade organic pollutants, thus leading to the slump in the degradation perfor-246 mance of the EO-PS-EF system. Similarly,  $CO_3^{2-}$  is mainly present in the form of  $HCO_3^{-}$  which is also recognized as a powerful 247 free radical scavenger, and the resulting bicarbonate radical (HCO<sub>3</sub>) has low degradation capability (k ranges between 4×10<sup>6</sup> 248 and 1×10<sup>8</sup> M<sup>-1</sup> s<sup>-1</sup>) toward organic matters. In addition to scavenging free radicals, HCO<sub>3</sub><sup>-</sup> can consume electrons to produce 249 HCO<sub>3</sub> with low oxidative capacity (Eqs. (24-26)) (Lee et al., 2020; Wang and Wang, 2020). The formation of these low reactive 250 oxygen species (ROS) may be responsible for the pronounced inhibition effect of  $PO_4^{3-}$  and  $CO_3^{2-}$ . Moreover, the competitive 251 adsorption between negatively charged anion species and PS might inhibit PS adsorption and activation.

1 Interestingly that the presence of Cl<sup>-</sup> promoted the degradation of TC in the EO-PS-EF system, and the promotion effect increased with increasing concentrations. This corresponds to the production of highly reactive and strongly selective reactive chlorine species (RCS), which are highly susceptible to addiction, substitution or oxidation reactions with organic compounds with unsaturated bonds and electron-rich groups. It has been demonstrated that RCS reacts faster with certain phenolic compounds (e.g., benzoic acid, bisphenol A) than ·OH and/or SO<sub>4</sub><sup>--</sup> (Chen et al., 2022). Cl<sup>-</sup> can react with SO<sub>4</sub><sup>--</sup> to form chlorine radicals (Cl·) and then dichlorine radical (Cl<sub>2</sub><sup>--</sup>), and the chlorine products (e.g., Cl· and Cl<sub>2</sub><sup>--</sup>) can promote the production of ·OH through the reaction, thus accelerating TC removal (see Eq. (27-33)) (Farhat et al., 2017; Oyekunle et al., 2021).

In addition, the influence of the introduction of  $NO_3^-$ ,  $PO_4^{3-}$ ,  $CO_3^{2-}$  and Cl<sup>-</sup> with the same molar concentration on the performance of the system was also studied with 50 mM  $Na_2SO_4$  as the background electrolyte. Its TC removal rate resulted from the mixed effect of the two salts, which was similar to a compromise effect. In general, almost all inorganic anions are capable of consuming electrons and scavenging free radicals with different reaction rates and producing reactive species with varying redox capabilities. The difference in oxidation capacity of these reactive species with respect to the target contaminants determines their impact on water treatment performance.



265 266

Fig. 3. Effects of inorganic anion species and concentration on the degradation performance of the EO-PS-EF tri-coupling

**system**. (a) Effects of five individual inorganic anions  $(NO_3^-, SO_4^{2-}, PO_4^{3-}, CO_3^{2-} \text{ and } Cl^-)$  at various concentrations (0, 20, 50 and 100 mM) on TC removal. The control experiment (EO-PS-EF<sub>1</sub> without 50 mM Na<sub>2</sub>SO<sub>4</sub>) was shown on the top panel. (b) Corresponding pseudo-first-order reaction rate constants.

### Table 1 Elementary reactions during the EO-PS-EF system.

No.	Reaction equation	E <sup>0</sup> or k	Ref.
1	$0_2 + 2H^+ + 2e^- \rightarrow H_2O_2$	<i>E</i> <sup>0</sup> = 0.67 V vs. RHE	(Hu et al., 2021)
2	$Fe^{2+} + H_2O_2 \rightarrow Fe^{3+} + OH + OH^-$	k = 40-80 M <sup>-1</sup> s <sup>-1</sup>	(Liu et al., 2021a)
3	$Fe^{3+} + e^- \rightarrow Fe^{2+}$	<i>E</i> <sup>0</sup> = 0.77 V vs. RHE	(Liu et al., 2019)
4	$BDD + H_2O \rightarrow BDD(\cdot OH) + H^+ + e^-$	<i>E</i> <sup>0</sup> = 1.9-2.7 V vs. RHE	(Du et al., 2021)
5	$Fe^{2+} + S_2O_8^{2-} \rightarrow Fe^{3+} + SO_4^{2-} + SO_4^{2-}$	k = 20-30 M <sup>-1</sup> s <sup>-1</sup>	(Xiao et al., 2020)
6	$S_2 O_8^{2-} + e^- \rightarrow SO_4^{} + SO_4^{2-}$	-	(Divyapriya and Nidheesh, 2021)
7	$SO_4^{2-} \rightarrow SO_4^{} + e^-$	<i>E</i> <sup>0</sup> = 2.5-3.1 V vs. RHE	(Divyapriya and Nidheesh, 2021)
8	$2SO_4^{2-} \rightarrow S_2O_8^{2-} + 2e^-$	E <sup>0</sup> = 2.01 V vs. RHE	(Divyapriya and Nidheesh, 2021)
9	$O_2 + e^- \rightarrow O_2^{\cdot-}$	-	(Bu et al., 2019)
10	$0_2^{-} + S_2 0_8^{2-} \rightarrow 0_2 + S0_4^{-} + S0_4^{2-}$	-	(Bu et al., 2019)
11	$BDD + PS \rightarrow BDD(PS^*)$	-	(Song et al., 2018)
12	$2SO_4^{-} \rightarrow S_2O_8^{2-}$	k = 7.6 × 10 <sup>8</sup> M <sup>-1</sup> s <sup>-1</sup>	(Divyapriya and Nidheesh, 2021)
13	$S_2O_8^{2-} + SO_4^{} \rightarrow S_2O_8^{} + SO_4^{2-}$	k = 6.3 × 10 <sup>5</sup> M <sup>-1</sup> s <sup>-1</sup>	(Zhu et al., 2018)
14	$S_2 O_8^{2-} + \cdot OH \rightarrow S_2 O_8^{} + OH^{}$	k = 1.4 × 10 <sup>7</sup> M <sup>-1</sup> s <sup>-1</sup>	(Zhu et al., 2018)
15	$NO_3^- + OH \rightarrow NO_3^- + OH^-$	<i>k</i> < 5.0 × 10 <sup>5</sup> M <sup>-1</sup> s <sup>-1</sup>	(Huang et al., 2021)
16	$NO_3^- + SO_4^- \rightarrow NO_3^- + SO_4^2^-$	k = 5.5 × 10 <sup>5</sup> M <sup>-1</sup> s <sup>-1</sup>	(Huang et al., 2021)
17	$NO_3^- \rightarrow NO_3^- + e^-$	<i>E</i> <sup>0</sup> = 2.3-2.5 V vs. RHE	(Bu et al., 2018)
18	$H_2PO_4^- + OH \rightarrow H_2PO_4^+ + OH^-$	k = 2.2 × 10 <sup>6</sup> M <sup>-1</sup> s <sup>-1</sup>	(Wang and Wang, 2020)
19	$H_2PO_4^- + SO_4^- \rightarrow H_2PO_4^- + SO_4^{2-}$	<i>k</i> < 7 × 10 <sup>4</sup> M <sup>-1</sup> s <sup>-1</sup>	(Wang and Wang, 2020)
20	$HPO_4^{2-} + \cdot OH \rightarrow HPO_4^{\cdot-} + OH^-$	k = 8.0 × 10 <sup>5</sup> M <sup>-1</sup> s <sup>-1</sup>	(Wang and Wang, 2020)
21	$\mathrm{HPO}_4^{2-} + \mathrm{SO}_4^{} \rightarrow \mathrm{HPO}_4^{} + \mathrm{SO}_4^{2}$	k = 1.2 × 10 <sup>6</sup> M <sup>-1</sup> s <sup>-1</sup>	(Wang and Wang, 2020)
22	$H_2PO_4^- \rightarrow H_2PO_4^\cdot + e^-$	-	(Bu et al., 2018)
23	$HPO_4^{2-} \rightarrow HPO_4^{} + e^-$	-	(Bu et al., 2018)
24	$HCO_3^- + OH \rightarrow HCO_3^- + OH^-$	k = 8.5 × 10 <sup>6</sup> M <sup>-1</sup> s <sup>-1</sup>	(Lee et al., 2020)
25	$HCO_3^- + SO_4^- \rightarrow HCO_3^- + SO_4^{2-}$	k = 9.1 × 10 <sup>6</sup> M <sup>-1</sup> s <sup>-1</sup>	(Wang and Wang, 2020)
26	$HCO_3^- \rightarrow HCO_3^\cdot + e^-$	<i>E</i> <sup>0</sup> = 1.7 V vs. RHE	(Wang and Wang, 2020)
27	$Cl^- \rightarrow Cl^+ + e^-$	<i>E</i> <sup>0</sup> = 2.41 V vs. RHE	(Farhat et al., 2017)
28	$2Cl^- \rightarrow Cl_2^- + e^-$	E <sup>0</sup> = 2.09 V vs. RHE	(Farhat et al., 2017)
29	$\text{Cl}^- + \text{SO}_4^- \rightarrow \text{Cl}^+ + \text{SO}_4^{2-}$	k = 3.2 × 10 <sup>8</sup> M <sup>-1</sup> s <sup>-1</sup>	(Farhat et al., 2017)
30	$Cl^{\cdot} + Cl^{-} \rightarrow Cl_{2}^{\cdot-}$	k = 6.5 × 10 <sup>9</sup> M <sup>-1</sup> s <sup>-1</sup>	(Farhat et al., 2017)
31	$Cl^{-} + OH^{-} \rightarrow HOCl^{-}$	k = 1.8 × 10 <sup>10</sup> M <sup>-1</sup> s <sup>-1</sup>	(Farhat et al., 2017)
32	$Cl_2^{-} + OH^- \rightarrow HOCl^{-} + Cl^-$	k = 4.5 × 10 <sup>7</sup> M <sup>-1</sup> s <sup>-1</sup>	(Farhat et al., 2017)
33	$HOCI^{-} \rightarrow OH + CI^{-}$	k = 6.1 × 10 <sup>9</sup> M <sup>-1</sup> s <sup>-1</sup>	(Farhat et al., 2017)
34	$SO_4^{-} + H_2O \rightarrow SO_4^{2-} + OH + H^+$	<i>k</i> < 2.0 × 10 <sup>3</sup> M <sup>-1</sup> s <sup>-1</sup>	(Gao et al., 2020)
35	$SO_4^{\cdot-} + OH^- \rightarrow SO_4^{2-} + OH$	k = 6.5 × 10 <sup>7</sup> M <sup>-1</sup> s <sup>-1</sup>	(Gao et al., 2020)
36	$S_2 O_8^{2-}$ + Heat $\rightarrow 2SO_4^{}$	-	(Tian et al., 2022)

### 271

Note: E<sup>0</sup>: Standard reduction potential, k: reaction rate constant

# 272 **3.3 Effect of pH and temperature**

Fig. 4 shows the TC removal of the EO-PS-EF system with respect to pH (top panel) and temperature (bottom panel). The degradation efficiency of TC improves with increasing acidity but decreases with alkalinity. TC removal was observed to be highly efficient in neutral and acidic conditions, and the TC removal reached 96%, 99% and 100% after 20 min at pH of 7, 5 and 3, respectively. However, the TC removal decreased to 69% and 59% at pH of 9 and 11, respectively.

TC molecules have three types of pH-relevant functional groups with different protonation and deprotonation constants ( $pK_a = 3.3, 7.7 \text{ and } 9.7$ ), and their forms vary with changing pH, as shown in Fig. S1 (Gao et al., 2022b; Lalliansanga et al., 2022). At pH = 3, most TC molecules were protonated and existed in the cationic form of TCH<sup>+</sup>, while at pH = 5 it remained unchanged. At the neutral condition (pH = 7), some TC molecules were transformed into a monovalent anion (TC<sup>-</sup>). In contrast, as pH increased to 9, the TC mainly existed in the form of TC<sup>-</sup>, while the form of a divalent anion (TC<sup>2-</sup>) dominated at a pH of 11. When TC species are positively charged, the negative charge on the GF cathode surface facilitates TC adsorption. Also, the lower pH favors the adsorption of PS anions on the cathode, which in turn promotes the generation of SO<sub>4</sub><sup>--</sup> (Liu et al., 2018).

284 The iron species present in the EO-PS-EF tri-coupling system is closely related to solution pH (Dihingia and Tiwari, 2022; 285 Gabriel et al., 2021). On the one hand, iron species are present under alkaline environments in the form of hydroxide complexes 286 such as FeOH<sup>+</sup>, Fe(OH)<sub>2</sub><sup>+</sup>, Fe(OH)<sub>3</sub> and Fe(OH)<sub>4</sub><sup>-</sup>, leading to a decrease in the concentration of active Fe<sup>2+</sup>. The stronger alkaline, 287 the lower the concentration of Fe<sup>2+</sup>, as shown in Fig. S2. However, Fe<sup>2+</sup> participated in the generation of SO<sub>4</sub><sup> $\cdot\cdot$ </sup> from PS and  $\cdot$ OH 288 from H<sub>2</sub>O<sub>2</sub>. Thus, the degradation performance of the EO-PS-EF tri-coupling system toward TC would be severely inhibited due 289 to the loss of Fe<sup>2+</sup> in alkaline environments. On the other hand, SO<sub>4</sub><sup>--</sup> dominated in acidic conditions while SO<sub>4</sub><sup>--</sup> could be con-290 verted to ·OH in neutral and alkaline conditions, and ·OH would dominate in relatively concentrated alkaline conditions (see 291 Eq. (34) and Eq. (35)) (Gao et al., 2020). However, the generation potential of •OH decreased and the oxygen evolution reaction 292 increased under alkaline environments, leading to a decrease in the degradation performance of the EO-PS-EF tri-coupling 293 system. In general, low pH contributes to the removal of TC in EO-PS-EF systems as a result of a comprehensive evaluation of 294 multiple factors.

Later, the critical factor, temperature, was considered under the solution pH of 7. As expected, the degradation performance of the EO-PS-EF system increased with increasing temperatures from 20 °C to 60 °C, and the TC removal within 5 min increased from 72% to 96%, and the reaction rate constant was increased from  $2.54 \times 10^{-3}$  s<sup>-1</sup> to  $1.07 \times 10^{-2}$  s<sup>-1</sup>, respectively. The increase in temperature increased the average kinetic energy of molecules and thus the collision frequency between reactant molecules, increasing the mass transfer and accelerating the activation of PS through the heat to generate more SO<sub>4</sub><sup>--</sup> (see Eq. (36)) (Tian et al., 2022). Nevertheless, high temperatures would reduce the solubility of oxygen in the water and adversely 301 reduce the yield of H<sub>2</sub>O<sub>2</sub>, unavoidably increasing energy consumption. A balance between removal efficiency and energy con-

302 sumption should be addressed concerning industrial applications.



Fig. 4. Effects of pH and temperature on the degradation performance of the EO-PS-EF tri-coupling system. (a) The effect of
 pH (3, 5, 7, 9 and 11) and temperature (20, 30, 40, 50 and 60 °C) on TC removal in the EO-PS-EF<sub>1</sub> system. The solution pH and
 temperature were leveled off throughout the degradation period. (b) Corresponding pseudo-first-order reaction rate constants.

# **307 3.4 Identification of the major reactive species**

# 308 3.4.1 Free radicals quenching

309 MeOH has equivalently high reaction rates to ·OH and SO<sub>4</sub><sup>--</sup> ( $k_{\cdot OH} = 9.7 \times 10^8 \text{ M}^{-1} \text{ s}^{-1}$ ,  $k_{SO_4^{--}} = 1.0 \times 10^7 \text{ M}^{-1} \text{ s}^{-1}$ ) and was widely 310 used as a scavenger for hydroxyl and sulfate radicals. The reaction rate constant between TBA and  $\cdot$ OH ( $k_{\text{OH}}$  = 3.8-7.6 × 10<sup>8</sup> M<sup>-</sup> 311 <sup>1</sup> s<sup>-1</sup>) is three orders of magnitude higher than that between TBA and SO<sub>4</sub><sup>--</sup> = 4.0-9.1 × 10<sup>5</sup> M<sup>-1</sup> s<sup>-1</sup>). Thus, TBA was chosen 312 as a ·OH scavenger (Cai et al., 2019b). The electro-generated active radical species usually exist in the vicinity of the electrode 313 surface, which is different from those homogeneous radical species existed in the bulk solution. Thus, quenching equal concen-314 trations of heterogeneous radical species required higher concentrations of a scavenger than quenching homogeneous radical 315 species, as previously reported (Song et al., 2018). The EO-PS-EF system involves homogeneous catalytic and electrochemical 316 reactions, producing homogeneous and heterogenous radical species. Therefore, the contribution of free radicals evaluated by 317 free radical scavenging studies is of great significance for understanding the reaction mechanism of the EO-PS-EF system. Fig. 318 5 shows the effects of radical scavenger concentrations (0.1, 1, 2, 4 and 6 M) on the TC degradation performance of the EO-PS-319 EF system. As the scavenger concentrations increased from 0.1 M to 6 M, the effect of inhibiting TC removal increased. When 320 the concentration of MeOH and TBA was greater than 1 M, the inhibition did not change significantly with further increasing 321 quenchers. Furthermore, we found comparable quenching effects for high-concentration MeOH and TBA, which conflicts with 322 the basic assumption that the added high-concentration quenchers only remove their target active species. This may be related 323 to the confounding effects of high-concentration quenchers that interfere with reactive species production and quench non-324 target reactive species as reported in the literature (Gao et al., 2022a). For the case of 0.1 M MeOH and 0.1 M TBA, the remain-325 ing TC accounts for 44% and 24%, respectively. According to the previous study, it can be distinguished that the respective 326 contributions of  $\cdot$ OH and SO<sub>4</sub><sup>--</sup> were 61.6% and 19.3% respectively (Cai et al., 2019b).



327

Fig. 5. Free radicals quenching reactions. (a) Effects of MeOH and TBA concentrations on TC removal in EO-PS-EF system. (b)
 Corresponding pseudo-first-order reaction rate constants.

# 330 3.4.2 Electron Spin Resonance

331 The reactive radicals involved in the EO-PS-EF system were directly determined by the ESR spectroscopy (see Fig. 6). Typical 332 DMPO-OH and DMPO-SO<sub>4</sub> adduct signals were observed based on their hyperfine coupling constants (DMPO-OH:  $a_H = a_N = 14.9$ 333 G; DMPO-SO<sub>4</sub>: a<sub>N</sub> = 13.2 G, a<sub>H</sub> = 9.6 G, a<sub>H</sub> = 1.48 G, a<sub>H</sub> = 0.78 G) (Gao et al., 2020). The signal of the DMPO-SO<sub>4</sub> adduct was lower 334 than that of the DMPO-OH adduct in ESR spectrum. This might result from that SO<sub>4</sub><sup>--</sup> could be converted into •OH under neutral 335 and alkaline pH. Besides, the DMPO-SO<sub>4</sub> adduct could also undergo a rapid nucleophilic substitution reaction with H<sub>2</sub>O/OH<sup>-</sup> 336 forming the DMPO-OH adduct (Gao et al., 2020). According to the relative intensities of the adduct signals, it can be seen that 337 the concentration of free radicals increases with the prolongation of the reaction time, resulting from the accumulation of free 338 radicals. The free radical concentration decreased to a certain extent when the reaction time was further prolonged due to the 339 quenching reaction. In conclusion,  $\cdot OH$  and  $SO_4$  are the dominant reactive species in the EO-PS-EF system.



340 341

Fig. 6. ESR spectrum recorded at different reaction times of the EO-PS-EF system.

# **342 3.5 Degradation mechanism and the pathways**

# 343 3.5.1 Analysis of the plausible mechanism

Scheme 2 schematically shows the possible degradation mechanism of the EO-PS-EF system. As an ideal anode material, BDD has more substantial oxidation capability and longer service life than other anode materials (e.g., PbO<sub>2</sub>, SnO<sub>2</sub>, mixed-metal oxides and Ti<sub>4</sub>O<sub>7</sub>) and can generate heterogeneous  $\cdot$ OH and SO<sub>4</sub><sup>--</sup> by anodizing H<sub>2</sub>O, PS and SO<sub>4</sub><sup>-2</sup>. GF is a commercial EF cathode material with low cost, large specific surface area, and stable production yield of H<sub>2</sub>O<sub>2</sub>, and also allows for cathodic electroactivation of PS. When Fe<sup>3+</sup> was reduced to Fe<sup>2+</sup> on the GF surface, the reduced Fe<sup>2+</sup> would react with PS to generate homogeneous SO<sub>4</sub><sup>--</sup>. The spontaneous aqueous chemical reactions of Fe<sup>2+</sup>, H<sub>2</sub>O<sub>2</sub> and PS in the bulk solution can generate homogeneous  $\cdot$ OH and SO<sub>4</sub><sup>--</sup>, respectively. In summary, it is obvious that the homogeneous and heterogeneous catalytic co-generation of  $\cdot$ OH and  $SO_4^{--}$  is a reasonable mechanism to efficiently remove refractory organic pollutants. Notably, Fe cycling and PS cycling in the EO-PS-EF system might expand its application potential.



#### 353 354

Scheme 2. Schematic illustration of the plausible degradation mechanism of the EO-PS-EF system.

# 355

3.5.2 Possible degradation intermediates and pathways

356 The degradation intermediates of TC were analyzed and identified by LC-MS, which provided a theoretical basis for the 357 degradation pathways and mechanism of TC in the EO-PS-EF system. Various oxidation by-products were detected during TC 358 degradation due to the complexity of TC molecules. 36 intermediates were identified by total ion flow chromatograms and 359 mass spectra with different residence times (Fig. S3 and Table S4). Intermediates were classified into five types such as tetra-360 cyclic, tricyclic, bicyclic, monocyclic and short-chain carboxylic acids, according to their structures. Combined with the mecha-361 nism of the major reactive species ( $\cdot$ OH, SO<sub>4</sub><sup>--</sup> and electrons) reacting with organics, a possible degradation pathway of TC in 362 the EO-PS-EF system was proposed (Scheme. 3). Four functional groups can be identified based on the chemical structural 363 formula of TC, including the amide group (-(C=O)-NH<sub>2</sub>) and dimethylamine group (-N(CH<sub>3</sub>)<sub>2</sub>) at the C2 position and C4 position 364 of the A ring, the phenolic hydroxyl group (-OH) at the D ring (C10 position) and two conjugated double bond systems of ketone 365 group (R1-(C=O)-R2) and enol group (-C=C-OH) across the ABC ring (Yang et al., 2022b). The electron clouds at these functional 366 group positions were denser and more easily attacked by reactive species to undergo reactions such as electron transfer, dou-367 ble bond addition or hydrogen extraction.

368 The reaction of TC and reactive species will produce three primary intermediates with m/z = 460, m/z = 416 and m/z = 100369 401. The m/z = 460 primary intermediate was produced by cycloaddition of the double bond (C11a-C12 position) in the TC 370 molecule (Barhoumi et al., 2017; Liang et al., 2018). The m/z = 416 primary intermediate was produced by the demethylation 371 of dimethylamino  $(-N(CH_3)_2)$  (C4 position). The m/z = 401 primary intermediate was produced by dedimethylamidation (C2 372 position). The double bond (C2-C3 position) of the m/z = 460 primary intermediate can generate the m/z = 476 intermediate 373 by cycloaddition, further removing the dimethylamino group (C4 position) to produce m/z = 447 intermediate. In addition, the 374 dimethylamino group  $(-N(CH_3)_2)$  (C4 position) of the m/z = 460 primary intermediate can also undergo an aldehyde conversion 375 reaction to generate the m/z = 474 intermediate, followed by the oxidation of dimethylamino to generate m/z = 432 interme-376 diate. The m/z = 432 intermediate can also be generated from the m/z = 416 primary intermediate by deamination (C4 position) 377 and cycloaddition (C11a-C12 position). The m/z = 432 intermediate can be produced by cycloaddition (double bond at C2-C3 378 position) and deamidation reaction (C2 position) to produce m/z = 447 and m/z = 407 intermediates. The m/z = 401 primary 379 intermediate then underwent a cycloaddition reaction (C2 position) and removal of the dimethylamino group (C4 position) to 380 generate the m/z = 391 intermediate, which was further subjected to a cycloaddition reaction (C11a-C12 position) can produce 381 m/z = 407 intermediate. Overall, TC molecules formed 9 tetracyclic intermediates in the EO-PS-EF system through cycloaddi-382 tion, demethylation, deamidation, and deamination reactions. The above tetracyclic intermediates generated 9 tricyclic inter-383 mediates (m/z = 451, m/z = 413, m/z = 365, m/z = 349, m/z = 347, m/z = 332, m/z = 317, m/z = 306 and m/z = 274). The ring-384 opening positions are located at C7-C8, C1-C2, C3-C4 and C1-C12a. Some tricyclic intermediates can be generated by cycload-385 dition, dehydroxylation, carbonylation or decarboxylation of other tricyclic intermediates. For example, the m/z = 349 interme-386 diate can be produced by oxidation of the m/z = 451, m/z = 413, m/z = 332, m/z = 317 and m/z = 306 intermediates. Further 387 ring opening of these tricyclic intermediates will yield bicyclic (m/z = 250, m/z = 242, m/z = 218) and monocyclic intermediates 388 (m/z = 245, m/z = 230, m/z = 213, m/z = 203, m/z = 201 and m/z = 185). Among them, some intermediates can be produced by 389 the oxidation of other intermediates. For instance, m/z = 230 intermediates can be generated from m/z = 250, m/z = 242, m/z390 = 203 and m/z = 185 intermediates. Nine short-chain carboxylic acids were identified (m/z = 239, m/z = 223, m/z = 178, m/z = 188, m/ 391 149, m/z = 118, m/z = 101, m/z = 90, m/z = 71, m/z = 45). m/z = 239 can yield m/z = 223 and m/z = 178 intermediates by 392 sequential oxidation. m/z = 149 can be oxidized to produce m/z = 71. m/z = 118 can be further oxidized to produce m/z = 101. 393 m/z = 90 can be oxidized to produce m/z = 45. Finally, all intermediates might be gradually mineralized into CO<sub>2</sub>, H<sub>2</sub>O and 394 inorganic ions (Li et al., 2019).





# **397 3.6 Application potential of EO-PS-EF system**

# **398 3.6.1 Energy consumption**

399 The electric energy efficiency of these AOPs (i.e., EO, EO-PS, EO-EF and EO-PS-EF) was evaluated based on the energy 400 consumption per cubic meter of contaminant removal (EC, kWh m<sup>-3</sup>) according to reference (Wei et al., 2020). Under the power 401 consumption of 1.65 kWh m<sup>-3</sup>, the TC removal of the EO, EO-PS, EO-EF and EO-PS-EF systems was 21%, 60%, 55%, and 100%, 402 respectively (Fig. 7). For the fixed TC removal of 37%, the power consumption of EO, EO-PS, EO-EF and EO-PS-EF systems were 403 calculated to be 3.04, 0.62, 0.75 and 0.17 kWh m<sup>-3</sup>, respectively. This result indicated that the EO-PS-EF coupling process pro-404 vided significant advantages over other processes in terms of pollutant removal and energy consumption. Moreover, Table S5 405 listed a comparison of the EO-PS-EF method with the reported AOPs for the degradation of TC, indicating that the proposed 406 EO-PS-EF method exhibits significantly faster pollutant removal and lower energy consumption than other methods.



407 C<sub>t</sub>/C<sub>o</sub>
 408 Fig. 7. Comparison of energy consumption related to TC removal rate collected from the EO, EO-PS, EO-EF and EO-PS-EF systems
 409 individually.

# 410 3.6.2 Long-term stability

The long-term stability of the EO-PS-EF system was considered via repetitive measurements up to 100 times to assess its possible practical applications. Fig. S4 shows repetitive TC removal results taken at the 1<sup>st</sup>, 25<sup>th</sup>, 50<sup>th</sup>, 75<sup>th</sup> and 100<sup>th</sup> run. With one-hundred repetitive measurements, the TC degradation performance of the EO-PS-EF tri-coupling system was almost kept unchangeable with only a 5% difference between all runs. In addition, no apparent changes were found in the surface morphologies, phase composition and potential windows of the BDD anode and GF cathode before and after the 100<sup>th</sup> degradation experiment (Fig. S5 and S6). The degradation tests and experimental observations demonstrated that the EO-PS-EF tri-coupling system had considerably long-term repetitive stability and could run for a quite long lifetime.

# 418 3.6.3 Selective degradation of RB-19, OG, ATZ and 2,4-D

419 Different structural refractory organic pollutants, including Azo dyes (RB-19 and OG) and organochlorine pesticides (ATZ 420 and 2,4-D), were selected as target pollutants to assess the degradation performance of the EO-PS-EF system (see Fig. 8). Other 421 single and bi-coupling systems were also compared including PS, EO, EO-EF and EO-PS. The degradation performance for Azo 422 dyes (RB-19 and OG) are EO-PS-EF > EO-PS > EO-EF > EO > PS, while for organochlorine pesticides (ATZ and 2,4-D) it follows 423 with EO-PS-EF > EO-EF > EO-PS > EO > PS. The comparative results indicate that the bi-coupling system exhibited higher degra-424 dation performance than the single system for all Azo dyes and organochlorine pesticides, while the EO-PS-EF significantly 425 improved degradation performance than other single and bi-coupling systems, especially for OG and 2,4-D. The tri-coupling 426 system exhibited exceptional selectivity for 2,4-D that was degraded entirely at around 15 min, with over five times the degra-427 dation performance of the other systems. The selectivity preference results from the pollutant structures. The degradation rate 428 is 2,4-D > TC > OG > RB-19 > ATZ for the EO-PS-EF tri-coupling system. This provides an experimental database for the application 429 of the EO-PS-EF system to treat various organic pollutants.



430 431

Fig. 8. Comparison of degradation performance of organic pollutants with the PS, EO, EO-PS, EO-EF and EO-PS-EF systems
 individually, including (a) RB-19, (b) OG, (c) ATZ and (d) 2,4-D. (e) Corresponding pseudo-first-order reaction rate constants.

# 433 4 Conclusions

434 In summary, the EO-PS-EF tri-coupling system based on BDD anode and GF cathode was established for the first time, 435 which efficiently removed pollutants by homogeneous and heterogeneous catalytic co-generation of  $\cdot$ OH and SO<sub>4</sub><sup>--</sup>. Compared 436 with PS, EO, EO-PS and EO-EF systems, the EO-PS-EF system can significantly improve pollutant removal efficiency and reduce

437 energy consumption. Adjustment of PS concentration, Fe<sup>2+</sup> concentration and air flow rate can optimize EO-PS-EF system per-

438 formance. NO<sub>3</sub><sup>-</sup>, SO<sub>4</sub><sup>2-</sup>, PO<sub>4</sub><sup>3-</sup> and CO<sub>3</sub><sup>2-</sup> had different degrees of inhibition on pollutant removal through radicals quenching and

electron consumption. However, Cl<sup>-</sup> showed a significant promotion effect by generating highly reactive and selective RCS.
 Besides, low pH and high temperature can facilitate the removal of contaminants. The possible coupling mechanisms and TC

Besides, low pH and high temperature can facilitate the removal of contaminants. The possible coupling mechanisms and TC degradation pathways of the EO-PS-EF system were revealed based on TC degradation rate constants, radical quenching, ESR

and LC-MS data. The high pollution removal efficiency, low energy consumption, long-term cycle stability, and efficient degra-

443 dation of various pollutants of the EO-PS-EF system demonstrated its potential for practical applications. This study developed

an economic, efficient and stable coupling process for removing various emerging pollutants and provided a theoretical basisand experimental foundation for understanding the synergistic mechanism and designing new coupling processes.

# 446 Author Contributions

W. Yang: Investigation, Conceptualization, Writing - original draft, Writing - review & editing; Z. Deng: Conceptualization, Validation, Data Curation, Writing - original draft, Writing - review & editing; L. Liu: Resources, Supervision; K. Zhou: Analysis, Suggestion, Resources; S. P. E: Suggestion, Resources; L. Meng: Suggestion, Resources; L. Ma: Resources, Supervision; Q. Wei:
Conceptualization, Resources, Funding acquisition, Supervision, Project administration.

# 451 Notes

452 The authors declare no competing financial interest.

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