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# Deformation produced by a simple tensile load in an isotropic elastic body

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#### ABSTRACT

It is shown that a simple tensile load produces a simple extension provided the empirical inequalities (Truesdell and Noll [1], eqn. 51.27) hold.

One form of the general constitutive equation for an unconstrained isotropic homogeneous elastic material (Cf. § 47 of [1]) is

$$T = f_0 \mathbf{1} + f_1 \mathbf{B} + f_{-1} \mathbf{B}^{-1}, \tag{1}$$

where T is the Cauchy stress tensor, B is the left Cauchy-Green tensor with respect to an undistorted configuration, and the response coefficients  $f_{\alpha}$  ( $\alpha = -1, 0, 1$ ) are functions of the principal invariants of B. In order that equation (1) describe a response that is physically reasonable. Truesdell and Noll ([1], eqn. 51.27) proposed that  $f_{\alpha}$ satisfy the following inequalities.

$$f_0 \leqslant 0, \ f_1 > 0, \ f_1 \leqslant 0.$$
 (2)

The Cauchy–Stress tensor for a simple tensile load along the  $x_3$ -axis of a rectangular Cartesian set of axes is

$$\begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & T \end{bmatrix}$$
(3)

where T is a positive constant. The constitutive relation (1) requires that TB=BT. This together with (3) gives that

$$B_{13} = B_{23} = 0 \; .$$

Thus

$$\boldsymbol{B} = \begin{bmatrix} B_{11} & B_{12} & 0 \\ B_{12} & B_{22} & 0 \\ 0 & 0 & B_{33} \end{bmatrix}.$$
 (4)

Since **B** is positive definite,

$$B_{33} > 0, \quad C \equiv B_{11} B_{22} - B_{12}^2 > 0. \tag{5}$$

Substituting from (3) and (4) into (1), we conclude that

$$0 = \left(f_{1} - \frac{1}{C}f_{-1}\right)B_{12},$$

$$0 = f_{0} + f_{1}B_{11} + \frac{1}{C}f_{-1}B_{22},$$

$$0 = f_{0} + f_{1}B_{22} + \frac{1}{C}f_{-1}B_{11},$$

$$T = f_{0} + f_{1}B_{33} + \frac{1}{B_{33}}f_{1}.$$
(6)

Substraction of  $(6)_3$  from  $(6)_2$  yields

$$0 = \left(f_1 - \frac{1}{C} f_{-1}\right) (B_{11} - B_{22}).$$
<sup>(7)</sup>

When inequalities (2) hold, it follows from  $(6)_1$  and (7) that

$$B_{12} = 0, \quad B_{11} = B_{22}. \tag{8}$$

Thus B has the form

$$\boldsymbol{B} = \operatorname{diag}(\alpha^2 v^2, \, \alpha^2 v^2, \, v^2) \,, \tag{9}$$

where

$$v^2 = B_{33}$$
,  
 $\alpha^2 = B_{11}/B_{33}$ . (10)

In (10)<sub>2</sub> the positive definiteness of **B** has been used. **B** given by (9) corresponds to simple tension (*Cf.* [2], eqn. 44.1). That  $\alpha < 1$  follows from (9), (2) and the equation obtained by subtracting (6)<sub>2</sub> from (6)<sub>4</sub>.

The constitutive relation for an incompressible isotropic elastic material is

$$T = -p\mathbf{1} + f_1 \mathbf{B} + f_{-1} \mathbf{B}^{-1}, \tag{11}$$

where p is an arbitrary hydrostatic pressure and  $f_1$  and  $f_{-1}$  are functions of the first and second invariant of **B**; the third invariant of **B** equals 1. The E inequalities, suggested as plausible by Truesdell (Eqn. (41.14) of [3]) in 1952, are

$$f_1 > 0, \ f_{-1} \leqslant 0.$$
 (12)

Proceeding as we did before, we obtain (4), (6)<sub>1</sub> and (7) and, in view of (12), we conclude that for incompressible isotropic elastic materials **B** should have the form given by (9) except that  $\alpha$  now equals  $v^{-\frac{3}{2}}$  since the determinant of **B** must be 1.

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