

Fully passive user localization for beam-steered high-capacity optical wireless communication system

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Fully Passive User Localization for Beam-Steered High-Capacity Optical Wireless Communication System

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Abstract— By means of narrow infrared beams very high capacity wireless links can be set up to users individually, while also offering high privacy and high energy efficiency. Accurate device localization for steering the beams is required. This has been achieved within the 10cm pico-cell resolution of a 2D beam-steered optical wireless communication system by applying a matrix of miniature corner-cube retro-reflectors. The localization process is self-calibrating, and does not need power-consuming elements at the receiver. In an indoor laboratory system setup, real-time transfer of multiple 10GbE high-definition video streams has been demonstrated.

Index Terms— Optical wireless communication, optical beam steering, wavelength routing, optical retro-reflector, device localization

I. INTRODUCTION

As the radio spectrum is getting seriously overcrowded due to the booming needs for wireless connectivity, new spectrum opportunities need to be found. The optical spectrum readily offers these: the visible spectrum (400-700nm, used amongst others for illumination) offers no less than 320THz of spectrum, and the infrared (IR) spectrum from 1500 to 1600 nm as used extensively in high-capacity optical fiber networks offers a respectable 12.5THz. Both the visible spectrum and the IR spectrum significantly exceed what can be reached with radio mm-wave techniques, even with sub-THz techniques.

Visible light communication (VLC) is typically using existing LED systems; these are primarily optimized for illumination, not for data transmission. Thus, their bandwidth is limited; moreover, their large footprint implies that this bandwidth is to be shared among many devices. A networked version of many small LED cells can increase the capacity per user, but at the cost of higher complexity [1].

Another option for optical wireless communication (OWC) is to use narrow infrared optical beams. These beams need to be accurately steered to the users, and give each user an unshared personal wireless channel which can readily carry multiple Gbit/s [2]. Systems have been reported which steer the beams

with MEMS mirrors [3], or with spatial light modulators [4]. In these systems, each beam needs a separate steering element which has to be controlled over a control channel. We reported the steering of narrow IR beams by means of a passive diffractive module based on a pair of crossed gratings, or on an arrayed waveguide router with 2-dimensionally arranged output fiber array [2]. Each beam is two-dimensionally steered by just changing its wavelength remotely in the associated transmitter. Thus, the beam's wavelength acts as both the carrier of the data and as the control channel, so the control channel is embedded in the data channel and no separate control channel is needed. Each beam constitutes an ultra-high capacity wireless link addressing a single device; hence, it basically has the virtues of a fiber connection to the device, but without needing a fiber. Because a beam will be directed to go only there where and when needed, it is very power-efficient (not spoiling energy to places where it is not needed) and offers high privacy (reaching only the intended device, no others receive anything so cannot listen in). As the light travels through air, not through fiber, the optical link constituted by a beam has minimum latency (3.3ns/m in air, versus 5ns/m in silica fiber). And it has intrinsically an even higher bandwidth than fiber as it is not hampered by waveguide dispersion. Moreover, IR light is 'eye-safe' beyond 1400nm, hence significantly higher power levels (up to 10mW) can be transmitted than in visible light safely according to the eye safety standards [5]. The thus attainable high link power budget enables multi-Gbit/s data rates per beam. And the narrowness of a beam enables high spatial multiplicity, hence another significant increase of attainable data throughput.

For appropriately directing the narrow IR beams the location of the user device needs to be known accurately. Various device localization techniques employing RF signals emitted or processed by the user have been reported, using triangular algorithms such as RSS (received signal strength), AoA (angle of arrival), and TDoA (time difference of arrival) [6]. Also device localization techniques employing VLC signals have been reported, using multiple luminaires and signal processing at the user device [7]. Localization by means of a camera which

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determines the position of user devices by observing active LED tags on them has been reported in [8]. High localization accuracies within a few mm have been achieved. However, in each of these techniques there is a need for active functions in the user device, which draws extra power from the mobile device and thus compromises its battery lifetime.

We propose a novel device localization concept which only requires a simple fully passive function at the user device, thus not draining the device's battery, while building on our high-capacity IR beam-steered OWC system [9][10]. We have validated this localization concept in a laboratory system experiment in which multiple high-definition video streams were carried by narrow infrared beams.

II. IR BEAM-STEERED OWC SYSTEM

Our indoor beam-steered OWC system concept is shown in Fig. 1. The (Fiber-to-the Home, FttH) access network is terminated at the entry of the house in a central communication unit, and from there the services are routed to the individual rooms by a fiber network. At the ceiling of each room, pencil beam radiating antennas (PRAs) launch the narrow IR beams to the respective mobile devices. A PRA is fully passive, and contains optical diffractive elements which two-dimensionally direct each beam into a direction determined by the signal's wavelength.

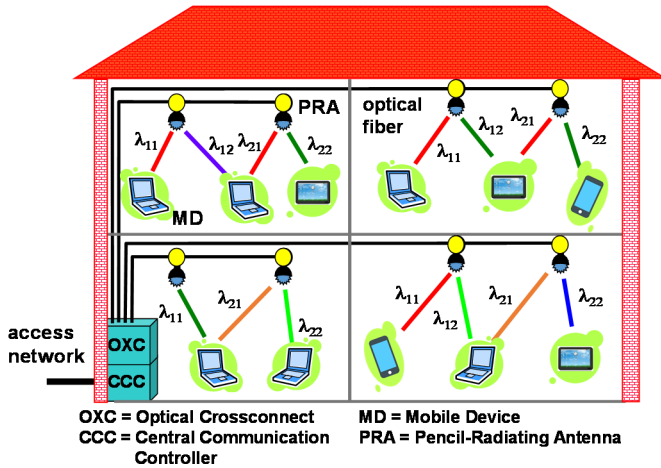


Fig. 1 Beam-steered indoor OWC system

We explored two options for implementing such a PRA [2]: by means of a pair of orthogonally-crossed diffraction gratings, and alternatively by means of an arrayed waveguide grating router (AWGR) with a high number of output fiber ports arranged in a 2D fiber array which is put in front of a lens, as shown in Fig. 2. Each incoming wavelength is by the AWGR routed to a specific fiber in this array, with its specific position with respect to the lens, and therefore after the lens is emitted as a beam into a specific direction. As shown in Fig. 3, the 2D fiber array is preferably positioned closer to the lens than the lens' focal plane, which yields slightly diverging beams [9]. This defocusing yields a more compact PRA module, and a coverage of the user plane which is less dependent on the user's distance to the lens. From the design condition that neighbouring beam spots in the image plane should touch each other for optimum coverage of the user area, and given a desired

spot diameter required for adequate received power by the detector's optical aperture, the lens' focal length f and the fiber pitch Δy in the 2D fiber array can be calculated [9].

In our previously reported system demonstrator [9], we deployed the AWGR-based PRA. Device localization was done by means of a 60GHz beam which was sent by the mobile device and was found by a scanning horn antenna positioned next to the PRA. Reading the mechanical 2D angular coordinates of this scanning antenna enabled to discover the (x,y) position of the user device, and subsequently the IR beam's wavelength was tuned such that the beam was pinpointed accurately to the device. Obviously, sending of the 60GHz beam draws power from the device's battery.

We recently reported device localization by means of a camera mounted at the ceiling which can observe the room and localize multiple user devices simultaneously [11]. Each user device has four visible LED tags surrounding its receiving optical aperture. These tags blink in a specific sequence which acts as the ID of that device, and for this operation have to draw some power from the battery of the user's device. After processing the images captured by the camera and subsequently having determined the position coordinates of the devices, these positions have to be mapped and calibrated to the specific wavelengths which direct the beams to those locations. A localization accuracy of less than 5mm over a reach of 3m was achieved.

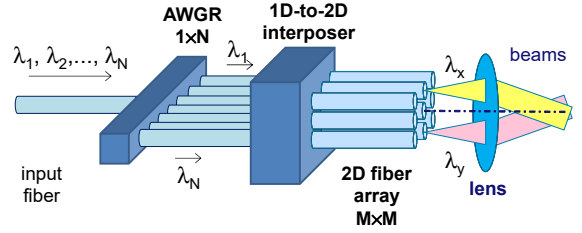


Fig. 2 2D beam steerer based on a high port count AWGR

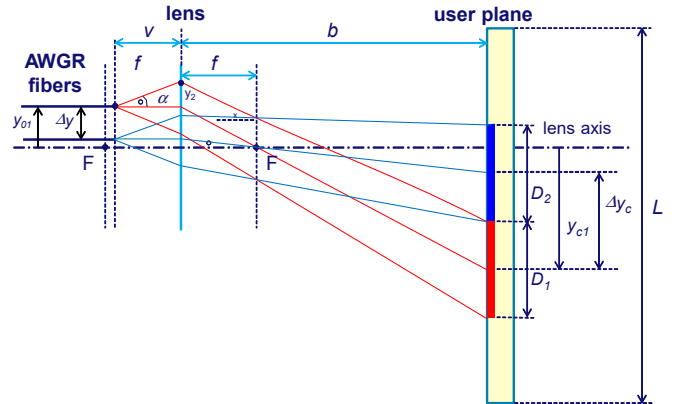


Fig. 3 Design of the AWGR-based beam steerer with defocused 2D fiber array

III. PASSIVE DEVICE LOCALIZATION

To enable localization of the user's device without drawing power from it, we explored how to equip the device with passive means for that, in particular a passive retroreflector based on an optical corner cube (CC) [10]. A CC reflects light rays in the same direction as they came from, but there is a displacement between incoming and reflected rays, as is

analysed in Fig. 4. The magnitude of this displacement Δ is dependent on the entry point of the incoming ray into the CC, and on the incident angle α with respect to the main axis of the CC. The maximum displacement Δ_{\max} is proportional to the entry aperture D of the CC; for the 2D case shown in Fig. 4, it follows that

$$\Delta = 2h = 2L \cdot \sin(\pi/4 - \alpha) \leq D \sqrt{2} \sin(\pi/4 - \alpha) = \Delta_{\max}$$

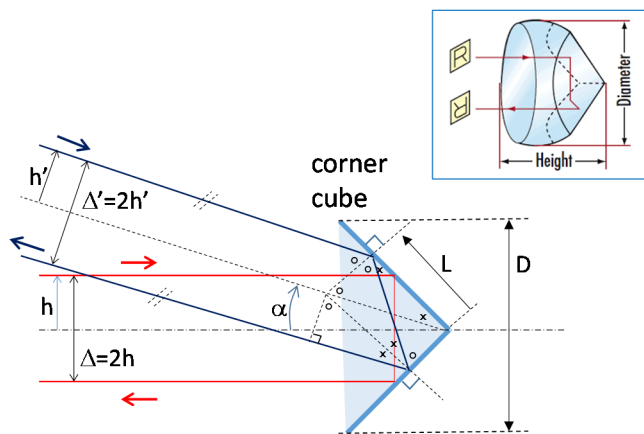


Fig. 4 Ray paths in optical corner cube reflector (inset: 3D view)

As illustrated in Fig. 5, a retro-reflecting CC mounted on the user device's OWC receiver will direct part of the incoming narrow IR beam back to the PRA, into the AWGR output port it came from. From the AWGR's input port, the reflected signal is subsequently returned to the central site, where via an optical circulator it is monitored in the localization processor. This processor is controlling the wavelength of the tunable laser diode. The device localization process begins by a command from the localization processor to the tunable laser diode to start scanning the room with an IR beam by sweeping its wavelength. As soon as the processor detects a returning reflected signal, it halts and stores the actual wavelength of the tunable laser, and thus has found and stored the location of the user device. The laser is then set to this wavelength, and by the correspondingly steered IR beam the system has established a high-speed wireless communication link to the user. In this way, the localization is self-calibrating: the device position is directly mapped to the wavelength needed for directing the beam, and no separate calibration is needed.

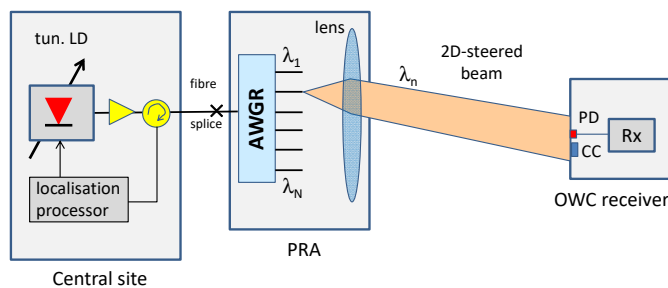


Fig. 5 Localising the user's OWC receiver by means of a retro-reflecting corner cube (CC)

As reported before [9], to achieve a compact design of the PRA it is required to position the 2D fiber array of the AWGR outputs not in the focal plane of the lens, but a bit closer to it;

i.e. to introduce an amount of defocusing $p=1 - v/f > 0$ (see Fig. 3). Next to a reduction of the PRA's size, this defocusing yields a slight divergence of the beams, which improves the coverage of the user plane and makes the coverage less dependent on the actual distance to the lens; this relaxes the device mobility requirements. But the defocusing makes that the displaced beam returning from the CC may not end in the same fiber port as where it came from; see Fig. 6. At the fiber plane, this lateral offset δ of the returning beam is

$$\delta = \frac{f - v}{f} \cdot \frac{\Delta}{\cos \alpha} \leq p \cdot D_{CC} \cdot (1 - \tan|\alpha|)$$

To minimize this offset issue, it is preferred that the displacement Δ is minimized, and therefore the aperture D_{CC} of the CC is minimized. But this implies that only a very small fraction of the beam is retro-reflected, which compromises the detection process. We therefore opted to apply not a single small CC, but a matrix of many miniature CC-s. Such CC arrays are readily available in retro-reflecting foils; these are commercially available and are widely used already, e.g. for road signage. We acquired such a foil containing a fine pattern of miniature molded CC-s (from Orafol [12]); Fig. 7 shows a microscopic view of its structure; the diameter of a CC in it is about 100 μ m.

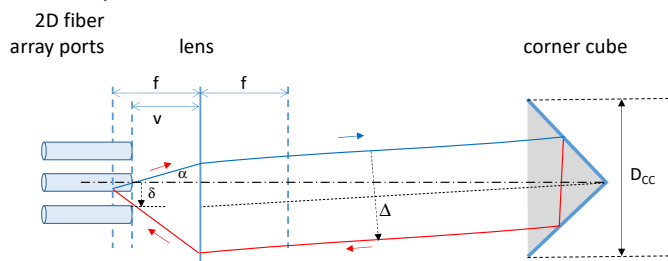


Fig. 6 Operating the retro-reflecting CC in a defocused PRA

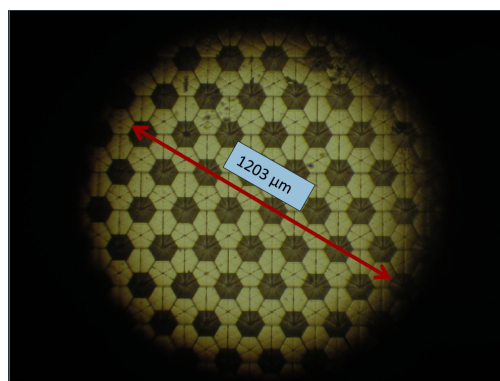
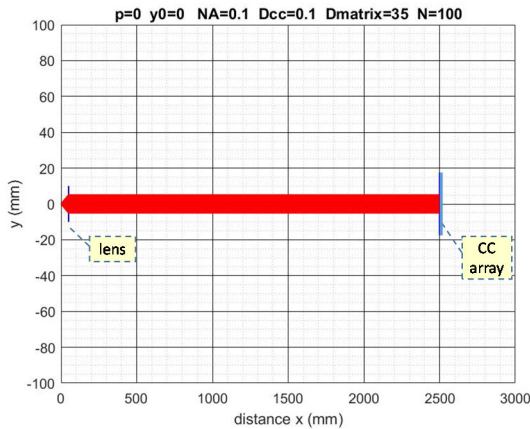


Fig. 7 Foil with many miniature corner cubes, each with a diameter of 100 μ m (from Orafol)

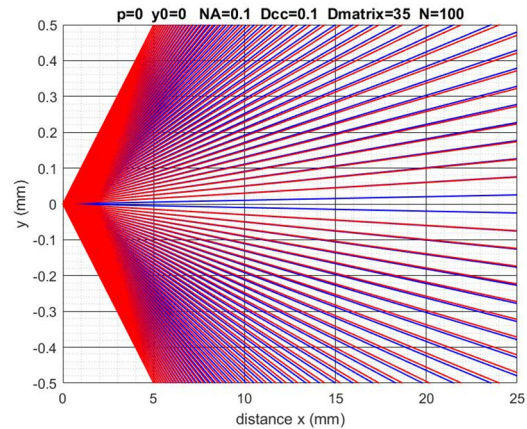
With 2D ray tracing, the impact of defocusing on the lateral offset δ when applying a matrix of CC-s has been assessed. A lens with focal length $f=50$ mm and negligible aberrations was assumed, and a CC matrix foil with diameter of 35mm. In the system design for indoor application, a distance lens-CC matrix $b=2.5$ m was assumed. With a fiber NA=0.1, the beam diameter at the CC matrix was about 10mm when the 2D fiber array is in focus (so $p=0$), and 108mm when the 2D fiber array is 20% defocused ($p=0.2$). Fig. 8 shows the ray tracing results; the blue rays are running towards the CC matrix, and the red rays

are returning from the CC matrix. The impact of the CC diameter has been analysed by considering CC-s with diameter $D_{CC}=100\mu\text{m}$ and $=1\text{mm}$. No lateral offset occurs when the 2D fiber array is in focus ($p=0$); Fig. 8.a shows the collimated beam for the whole lens-to-CC matrix link, and Fig. 8.b the situation at the endface of a fiber in the 2D array. But when defocusing is introduced, e.g. $p=0.2$, a lateral offset δ occurs which is about

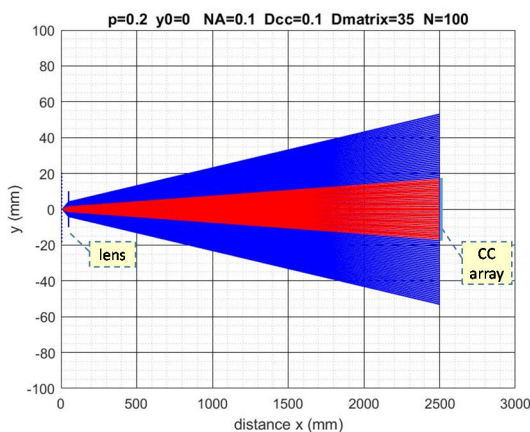
20% of the CC's diameter. Fig. 8.c shows the diverging beam for the lens-to-CC matrix link for $D_{CC}=100\mu\text{m}$. Only a part of the beam falls onto the CC matrix (with diameter 35mm) and is returned (red rays); the remainder of the beam is not returned. Fig. 8.d shows the lateral offset of the returning rays at the fiber endface in a zoomed-in view. Fig. 8.e and Fig. 8.f show similar ray tracings, but for $D_{CC}=1\text{mm}$. These show the clear increase



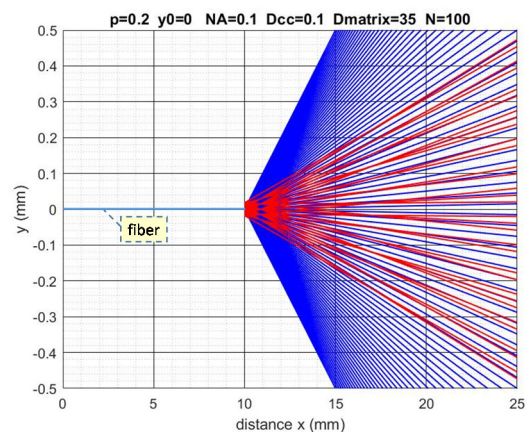
a) Focused ($p=0$), CC aperture $D_{CC}=100\mu\text{m}$



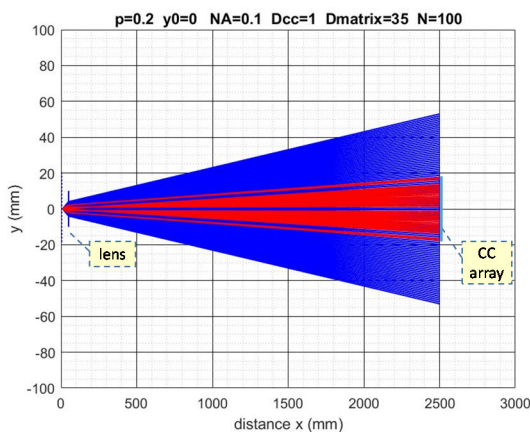
b) Focused ($p=0$), $D_{CC}=100\mu\text{m}$; zoomed-in at fiber in array



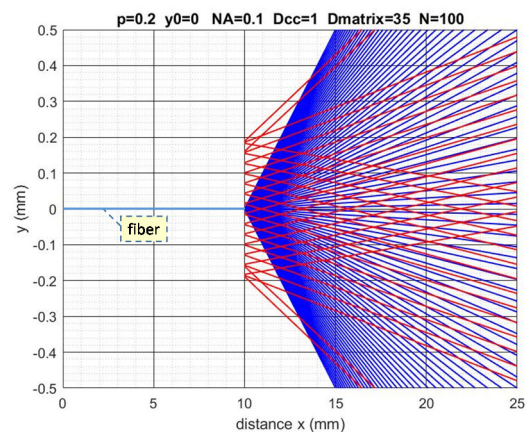
c) Defocused ($p=0.2$), CC aperture $D_{CC}=100\mu\text{m}$



d) Defocused ($p=0.2$), $D_{CC}=100\mu\text{m}$; zoomed-in at fiber in array



e) Defocused ($p=0.2$), CC aperture $D_{CC}=1\text{mm}$



f) Defocused ($p=0.2$), $D_{CC}=1\text{mm}$; zoomed-in at fiber in array

Fig. 8 Ray tracing with $N=100$ rays when the 2D fiber array: in a) and b) is in focus; in c) and d) is 20% defocused w.r.t. lens and CC diameter $D_{CC}=100\mu\text{m}$; in e) and f) is 20% defocused w.r.t. lens and $D_{CC}=1\text{mm}$. Blue rays are running towards the corner cube array; red rays are returning from the CC array; lens $f=50\text{mm}$, CC matrix diameter $D_{matrix}=35\text{mm}$, distance lens-to-user area $b=2.5\text{m}$.

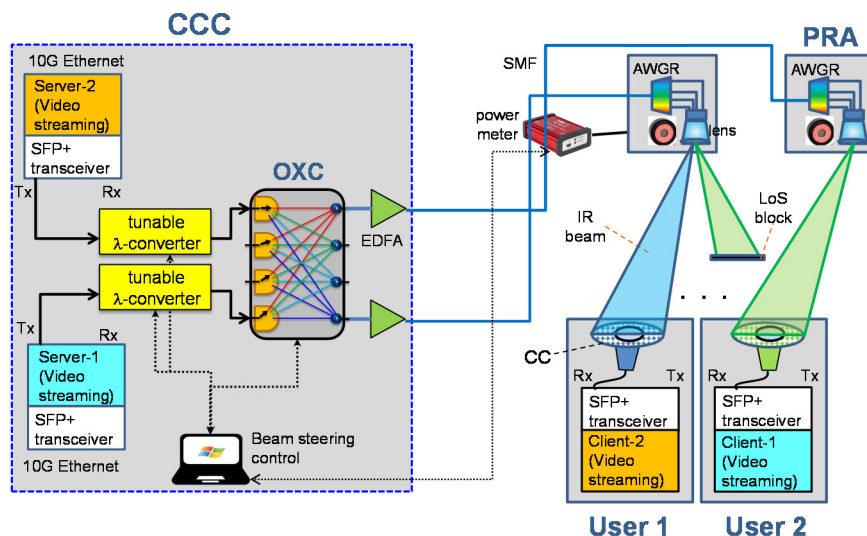


Fig. 9 Laboratory system demonstrator

in the lateral offset of the returning rays when the diameter of a CC is increased, and thus underline the need for a matrix array of miniature CC-s.

IV. SYSTEM EXPERIMENTS

Our laboratory demonstrator setup is shown in Fig. 9. In order to extend the area of coverage, and also in order to circumvent possible line-of-sight blockings, it features two PRA-s which can be selected by the optical cross-connect (OXC) in the central site (CCC). Equipped with a C+L band AWGR with channels spaced at 50GHz and -3dB bandwidths of 35GHz and 24GHz in the C-band and L-band, respectively, a PRA can launch up to 129 beams, each with diameter $\varnothing 10\text{cm}$, and cover a user area of about $\varnothing 1.3\text{m}$ at a reach of 2.5m. The OXC is composed of a 4x4 MEMS switch, with insertion losses of 7.0dB. In the demonstrator two user terminals are included, each equipped with a lens-based free-space optical receiver with $\varnothing 3\text{cm}$ aperture. A $\varnothing 4\text{cm}$ CC foil with a central hole of $\varnothing 3\text{cm}$ is mounted around this aperture. The physical details of the setup are shown by the photo in Fig. 10.

Two high-definition video streams are transmitted from the CCC, each embedded in a 10 Gbit/s Ethernet stream. The video servers are equipped with SFP+ transceivers which are operated at a fixed wavelength. The tunable wavelength converters translate these video streams to the wavelengths appropriate for the 2D beam steering to the respective user terminals by the PRAs. Each user terminal is connected to a client for receiving the video stream, and displaying it on a monitor. Good real-time transmission of both video streams was achieved, with $\text{BER} < 3 \cdot 10^{-12}$ at transmitted beam power of 6.0dBm and received power levels of -19 to -23dBm.

We included the passive localization function by attaching a circular piece of Orafol foil containing the miniature CC-s on an OWC receiver, as depicted in Fig. 9. Due to internal optical reflections in the PRA (we used a commercial 50mm F/0.9 camera lens which was not anti-reflection coated for the $\lambda = 1.5\mu\text{m}$ window, and connector joints between the 2D fiber array and the AWGR output fibers), we had to catch the

returning rays by a small $\varnothing 1\text{cm}$ power detector next to the lens. The optical power launched into the wireless channel was 6dBm in all the measurements. When the beam is scanning the user plane by tuning its wavelength, Fig. 11 shows the reflected power received by the localization detector for the case of two users, one equipped with a CC sheet with a diameter of 4cm and the other of 5cm. There is a 1-to-1 relation between the beam's wavelength and the device's position; hence the power peaks in Fig. 11 indicate the pico-cells where the devices are located. The height of the power peaks is related to the size of the CC sheet, as shown in Fig. 12. An adequate $\text{SNR} > 5\text{dB}$ for the

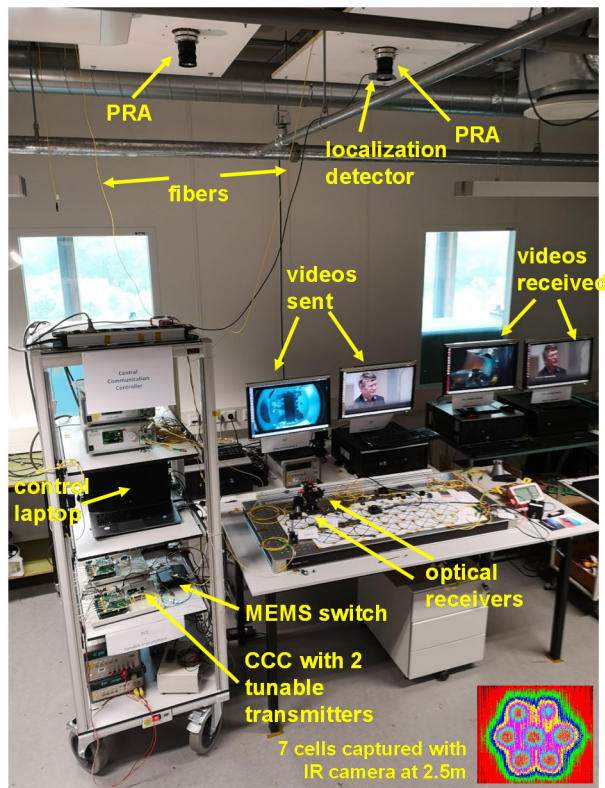


Fig. 10 Photo of laboratory demonstrator setup

localization requires a CC foil diameter $>4\text{cm}$. Background noise contributions are coming from the room illumination and from spurious reflections of the demonstrator table's surface. SNR values up to 15dB have been achieved, which enabled localization clearly within the required resolution of a single pico-cell (diameter 10cm). Scanning the whole user area takes about 15 s; the scan time is limited by the communication links between the power meter and the LABVIEW program running in the laptop which acts as localization processor and performs the beam steering control. The localization time is intrinsically constrained by the time needed to tune the wavelength of a laser diode over the full range for scanning the PRA's whole area, which can be done within a few milliseconds. However, the scanning process involves additional steps: the stepwise tuning to each cell consecutively, deciding whether there is retro-reflected power from that cell exceeding the background noise level, and subsequently moving to the next cell. Per cell 115ms is needed for all this, of which only a few ms is needed for the actual laser tuning, and the majority is taken by the Labview software running in the laptop controller, by the Arduino board which controls the laser tuning, and by the readout time of the localization power meter. Scanning the 129 cells in the area covered by the PRA thus takes about 15 seconds; this time may be reduced considerably by deploying more efficient algorithms implemented in embedded software.

The CC foil preferably surrounds the detector of the lens-based OWC receiver, which has an aperture of $\varnothing 3\text{cm}$. Hence we also measured the returned localization power for a $\varnothing 4\text{cm}$ CC foil with a central hole of $\varnothing 3\text{cm}$ hosting the receiver's detector, and a $\varnothing 4\text{cm}$ foil without hole. As shown in Fig. 13, the central hole caused a reduction of returned power of about 3.2dB (theoretically 3.6dB when uniformly illuminated).

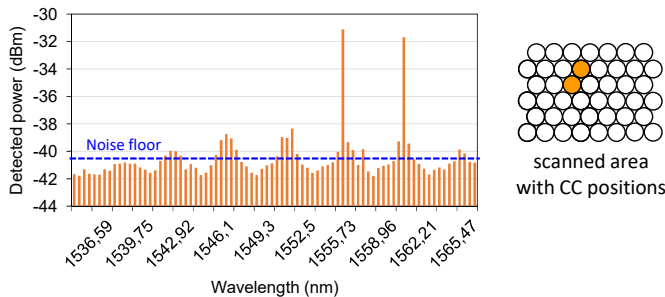


Fig. 11 Power received by localization detector when scanning across the system's pico-cells (for CC sheet diameter $\varnothing 4\text{cm}$)

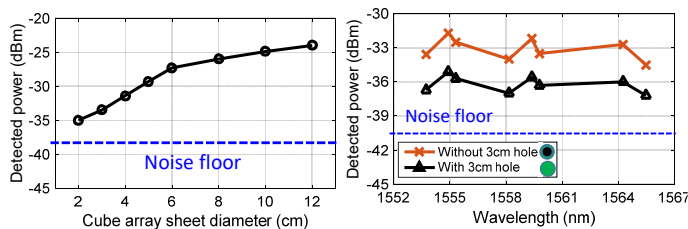


Fig. 12 Detected peak localization power vs. diameter of circular CC sheet

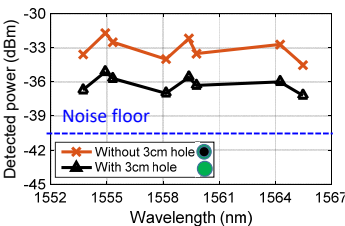


Fig. 13 Detected peak power vs. wavelength, for $\varnothing 4\text{cm}$ CC foil with $\varnothing 3\text{cm}$ hole, and $\varnothing 4\text{cm}$ CC foil without hole

V. CONCLUDING REMARKS

By means of narrow infrared optical beams on-demand, wireless links to individual users offering high capacity, high energy efficiency as well as strongly protected privacy can be established. This technology may enable highly-demanding broadband applications such as 8K ultra-high definition wireless video streaming, real-time virtual reality gaming or training without being hampered by wires, tele-presence meetings, Distinct advantages can be obtained in environments such as exhibition halls with frequently changing constellations of independent booths (which do not like capacity sharing), conference halls (where delegates want to download the proceedings instantly), electromagnetic radiation-sensitive areas (such as intensive care and surgery rooms in hospitals, inside airplanes, ...), airport waiting areas near the gate (where people want to do fast downloading or other voluminous internet things before getting on board), inside data centers between racks (where it provides minimum latency, as light travels 50% faster in air than in silica fiber), business meeting rooms requiring high privacy, etc., etc.

Efficient device localization is required in order to direct the beams on-demand and instantly to the user. Applying passive retro-reflection by means of a foil containing many miniature corner cubes has enabled device localization within the pico-cell resolution of our 2D beam-steered high-capacity optical wireless system setup. Real-time 10GbE video streaming to mobile devices has been demonstrated.

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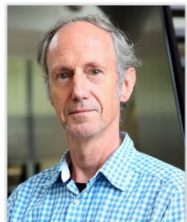
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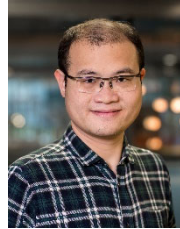
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