

# Ohmic contacts with ultra-low optical loss on heavily doped n-type InGaAs and InGaAsP for InP-based photonic membranes

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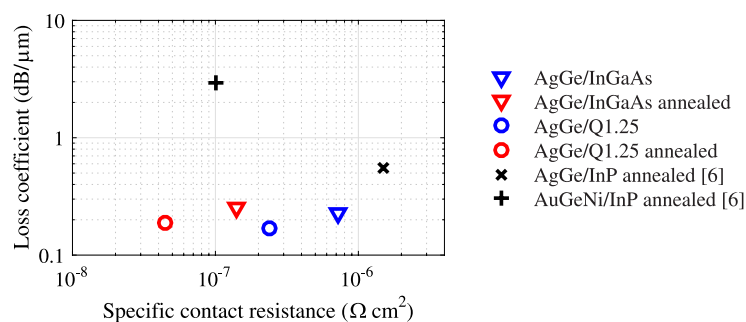
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# Ohmic Contacts With Ultra-Low Optical Loss on Heavily Doped n-Type InGaAs and InGaAsP for InP-Based Photonic Membranes

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**Abstract:** In this paper, we present significant reductions of optical losses and contact resistances in AgGe-based ohmic contacts to InP membranes. Due to the high solubility of Si in InGaAs and InGaAsP, heavily doped n-type contact layers are grown on InP wafers. This high doping concentration gives rise to annealing-free ohmic contacts and low contact resistances at the level of  $10^{-7} \Omega \text{ cm}^2$ . It also leads to strong band-filling effects in InGaAs and InGaAsP, which result in low optical absorption losses in the contact layer. Combined with the low optical loss of AgGe, a massive reduction of the propagation loss in membrane waveguides is observed compared with other existing solutions. An additional advantage is the minimal influence of thermal treatments during the processing, leading to very stable high-performing contacts.

**Index Terms:** Waveguide devices, semiconductor materials, optical and other properties, membrane photonics.

## 1. Introduction

Over the past decade, membrane photonics has emerged as a promising platform technology for hybrid integration of III-V materials with Si chips [1]–[5]. It has also brought new technological challenges for fabricating devices with good performance. For example, ohmic contacts with good electrical and optical properties become critical when they are placed on top of thin membrane devices. On the one hand, their contact resistances need to be minimized to obtain high bandwidth and low power consumption. On the other hand, low optical loss from these contacts is required for devices integrated in a membrane with sub-micron thickness. Optimizations for InP-based membrane devices are of particular importance, as this is a key material system for applications in telecommunications and optical interconnects.

Recently, we developed a new AgGe-based contact solution to InP-based membranes bonded on top of Si wafers [6]. Promising electrical and optical properties were demonstrated

by contacting AgGe to n-type doped InP. The role of Ge in forming an n-type ohmic contact was observed and its thickness was optimized to reach the minimal contact resistance. Compared with the conventional AuGeNi based n-type contacts [7], this approach shows lower optical loss in the telecommunication wavelength range due to the absence of Ni which has a high absorption coefficient and a high refractive index. Moreover, by replacing Au with Ag, the thermal stability of the metal contact is improved due to a higher eutectic temperature of the AgGe alloy compared with that of AuGe. Therefore, the well-known spiking effect in Au-based contacts during a thermal annealing process is reduced in the Ag-based solution [8]. However, the contact resistance of AgGe-based contacts remains one order of magnitude higher than that of AuGeNi-based ones. Furthermore, an increase of the optical loss after annealing is observed. Possible reasons include interface degradation due to spikes in the Ge layer and Ge diffusion into the InP layer. In order to meet the requirements of practical device applications, further optimizations in both electrical and optical properties of this new contact are in high demand.

In this paper, we present a significant improvement to reduce both the contact resistance and the optical loss. InGaAs and InGaAsP are used as contact layers between the AgGe contact and the InP waveguide (WG) layers. They are grown with Metal-Organic Chemical Vapor Deposition (MOCVD) at 650 °C using disilane as the doping gas source. The solubility of Si in the ternary and quaternary alloys is known to be much higher than that in InP [9]. Also, disilane has a higher decomposition reaction efficiency at 650 °C than silane, which was used previously [10]. Consequently, these contact layers can be doped with electron concentrations of higher than  $10^{19} \text{ cm}^{-3}$ , which is expected to result in very low contact resistance [8]. It will be shown in the next section that ohmic contacts between AgGe and these heavily doped contact layers can be formed without any annealing process, and their specific contact resistances can be minimized to the same level of those in conventional AuGeNi contacts. Furthermore, the thickness of the Ge layer, which was suggested to be the origin of the increase of the WG propagation loss after annealing [6], can be dramatically reduced while maintaining a low contact resistance. The major focus of this paper will be on the investigation of the optical properties of this new contact structure. The material absorption of InGaAs and InGaAsP has not been fully studied in literatures for such high doping levels. This is critical for devices requiring low optical loss and will be studied in Section 3, showing low absorption losses due to a strong band-filling effect in these heavily n-type doped materials. In Section 4, optical propagation losses from these contacts are measured with membrane WGs before and after annealing, showing clear reductions compared to existing solutions. These results are expected to lead to immediate improvements in a number of advanced photonic devices. For instance, high metal loss and high contact resistance are currently the major performance limitations of electrically-pumped nano-lasers with a metallic cavity [11], [12]. A membrane photodetector is another example in which the responsivity and the electrical bandwidth are highly dependent on the contact qualities [13]. With the new contact technology proposed in this paper, we expect strongly enhanced performance of these devices.

## 2. Specific Contact Resistance

For the measurement of the specific contact resistances, two samples are prepared containing an n-InGaAs contact layer and an n-InGaAsP contact layer, respectively. The InGaAsP quaternary alloy has a bandgap wavelength of  $1.25 \mu\text{m}$  (hereafter referred to as Q1.25). These contact layers are 100 nm thick and are grown on top of Fe-doped semi-insulating InP (100) substrates using MOCVD. The doping concentrations are characterized using an electrochemical C-V profiler, yielding  $2 \times 10^{19} \text{ cm}^{-3}$  and  $5 \times 10^{19} \text{ cm}^{-3}$  for n-InGaAs and n-Q1.25, respectively. It should be taken into account however that the relative error in the C-V measurement can be up to 50%. The circular transfer length method (CTLTM) is used to characterize the specific contact resistance [14]. Metal patterns are defined using optical lithography and a lift-off process. Before metal deposition, the samples are cleaned in an oxygen plasma (50 W, 5 minutes), followed by dipping in a  $\text{H}_3\text{PO}_4:\text{H}_2\text{O}$  (1:10) solution for 2 minutes. After these surface treatments, a layer of Ge is deposited on top of the contact layer using electron beam evaporation, followed by

TABLE 1

Specific contact resistances

Metals	Contact material and doping level ( $\text{cm}^{-3}$ )	Thickness Ge (nm)	Specific contact resistance ( $\Omega \text{ cm}^2$ )	
			Before annealing	After annealing
AgGe	InGaAs: $2 \times 10^{19}$	2	$7.2 \times 10^{-7}$	$1.4 \times 10^{-7}$
		15	Non-Ohmic	$1.9 \times 10^{-7}$
AgGe	Q1.25: $5 \times 10^{19}$	2	$2.4 \times 10^{-7}$	$4.4 \times 10^{-8}$
		15	Non-Ohmic	$4.2 \times 10^{-8}$
AgGe	InP: $2 \times 10^{18}$	2	$5.6 \times 10^{-4}$	$2.6 \times 10^{-5}$
		30	Non-Ohmic	$1.5 \times 10^{-6}$
AuGeNi	InP: $2 \times 10^{18}$	50	Non-Ohmic	$1.0 \times 10^{-7}$

[6]

[7]

deposition of 300 nm of Ag. Samples are measured both before and after annealing, for which a rapid thermal process at 400 °C is performed for 15 seconds.

The measured specific contact resistances are summarized in Table 1. For comparison, the optimal values obtained from AgGe/InP contacts and from conventional AuGeNi/InP contacts are also shown. Before annealing, samples with a 2 nm Ge layer show ohmic behavior. After annealing, the contact resistances reduce to a level comparable to or even lower than the values from the conventional low-resistance AuGeNi/InP contact. As these values of the contact resistance are sufficiently low for most device applications, no further optimizations on the annealing conditions are performed in this work. Samples with a Q1.25 contact layer provide lower contact resistances compared to the ones with InGaAs, which can be attributed to the higher doping level in Q1.25. The dependence of the contact resistance on the Ge thickness observed in previous works is not obvious in these highly doped contacts, suggesting that the contribution of Ge to the doping at the contact surface is not important in a contact layer with such a high doping level. The remaining 2 nm Ge mainly serves as a nucleation layer to improve the adhesion and the surface quality of the Ag layer [15], [16]. The reduction of the Ge thickness will benefit the optical properties, as will be discussed in Section 4.

The ohmic behavior observed before annealing is assumed to result from the tunneling current through the thin barrier of the 2 nm Ge layer. The current flow in heavily doped semiconductor contacts is governed by the field emission mechanism, for which the specific contact resistance depends strongly on the doping concentration [8]. Consequently, the high doping concentration in the contact layer of Q1.25 leads to a very low specific contact resistance ( $2.4 \times 10^{-7} \Omega \text{ cm}^2$ ), which is almost one order of magnitude lower than the minimal value from the annealed AgGe/InP contact [6]. This annealing-free low-resistance contact is highly desirable in membrane photonic devices, as it fundamentally avoids any high temperature related degradation of the optical properties.

### 3. Optical Properties of Highly Doped InGaAs and Q1.25

In this section, the effects that will influence the optical absorption and the refractive index of InGaAs and Q1.25 with high doping concentrations will be described, supplemented by experimental results on material absorption.

#### 3.1. Carrier-Induced Change in Material Absorption

In order to evaluate the optical performance of the newly developed contacts, the optical loss introduced by the InGaAs and Q1.25 contact layers need to be studied first. This is particularly important for InGaAs, which has a bandgap energy of 0.74 eV, which is smaller than the photon energy in the telecommunication wavelength range. Therefore intrinsic InGaAs is usually used as the absorption material in 1.55  $\mu\text{m}$  photodetectors. In n-type heavily doped semiconductors, however, a reduction of absorption near the bandgap is a well-known phenomenon, which has been explained by the band-filling effect [17]. That is, the energy states at the bottom of the conduction band are filled by the high concentration of free electrons so that photons need energies higher than the bandgap energy to excite an electron from the valence band to the

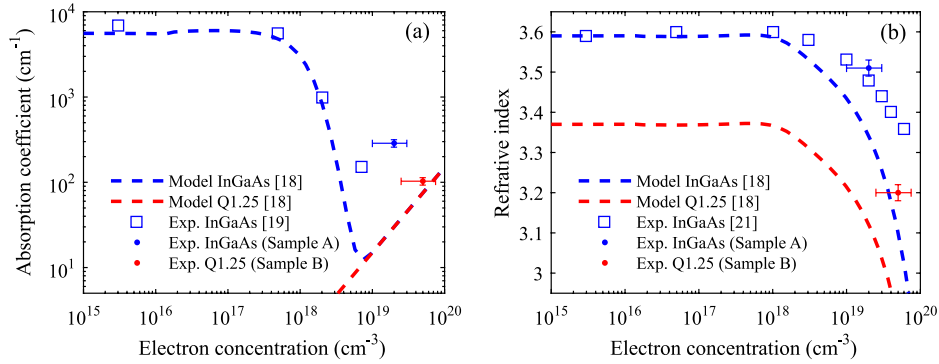


Fig. 1. (a) Absorption coefficient and (b) refractive index of InGaAs and Q1.25 at 1.55  $\mu\text{m}$  as a function of electron concentration. Both modeling and experimental data are included.

conduction band. This effect is particularly strong in n-type materials owing to the smaller effective mass of electrons and the lower density of states. In this paper, a model proposed by Weber is used [18], including mainly three free-carrier induced effects: bandfilling (BF), bandgap shrinkage (BS), and free carrier absorption (FCA). This model is originally used to study carrier-injection related effects. It should also be applicable to doped materials by calculating the Fermi level shift due to free electrons, instead of calculating the quasi-Fermi levels for the conduction band and the valence band under injection. In this model, the interband absorption coefficient from an undoped direct-bandgap semiconductor is given by

$$\alpha(E) = \begin{cases} CE^{-1}(E - E_g)^{\frac{1}{2}}, & E > E_g \\ 0, & E < E_g \end{cases} \quad (1)$$

where  $E$  and  $E_g$  are the photon energy and the bandgap energy, respectively. The constant  $C$  is a material constant determined from measurement data. It should be noted that parabolic bands are assumed and that the Urbach tail is neglected in this equation. In this model, the bandfilling effect is considered based on a narrowed bandgap. To be more specific, free carriers are first modeled as a cause for bandgap shrinkage, followed by their filling of the new band structure:

$$\alpha_{BF,BS} = \alpha(E - \Delta E_g)[f(E_v) - f(E_c)] \quad (2)$$

where  $\Delta E_g$  is the shrank bandgap energy.  $E_v$  and  $E_c$  are the energies in the valence band and the conduction band, respectively, between which the interband transition takes place. They can be calculated by applying energy and momentum conservations. Heavy holes and light holes are both considered in the calculation.  $f$  indicates the probability of an energy state being occupied by an electron, which is described by the Fermi-Dirac distribution function

$$f(E_{v,c}) = \left[ 1 + \exp\left(\frac{E_{v,c} - E_F}{k_B T}\right) \right]^{-1} \quad (3)$$

where  $k_B$  is Boltzmann's constant, and  $T$  is absolute temperature.  $E_F$  is the carrier dependent Fermi level in doped semiconductors which can be calculated by the Nilsson approximation [17]. For highly doped (degenerate) n-type semiconductors, the Fermi level is usually a few  $k_B T$  into the conduction band. In this case,  $f(E_v)$  is almost equal to 1 for photon energies in the telecommunication window.  $f(E_c)$  increases with an increasing electron concentration and approaches to 1, indicating a reduction of the absorption coefficient. Details about the calculation can be found in [18].

By applying this model to InGaAs at a wavelength of 1.55  $\mu\text{m}$ , it predicts a steep drop of the absorption coefficient for electron concentrations higher than  $10^{18} \text{ cm}^{-3}$  [see Fig. 1(a)], as a

result from the dominant bandfilling effect. Experimental data from [19] show a reasonable agreement with this model. Comparisons with measurement results from our samples will be discussed in Section 3.3.

Apart from the interband absorption, free carrier absorption is also taken into account. In n-type InP related materials, the free electron absorption is usually very low in the telecommunication wavelength range. However, it is assumed to be proportional to the electron concentration, implying a stronger effect in very heavily doped materials. A linear relation between the electron concentration and the resulting absorption coefficient at 1.55  $\mu\text{m}$  is proposed in [20]:

$$\alpha_{FCA} = A \times 10^{-18} N_e \quad (4)$$

where  $N_e$  indicates the electron concentration in  $\text{cm}^{-3}$ . The value of the constant  $A$  is estimated to be between 1 and 2  $\text{cm}^2$ , based on measured data from different InGaAsP alloys with a bandgap wavelength from 1  $\mu\text{m}$  to 1.3  $\mu\text{m}$ . This bandgap range covers Q1.25 but not InGaAs. Nevertheless we use the mean value of 1.5  $\text{cm}^2$  as an approximation of the constant  $A$  in our model for both InGaAs and Q1.25. The contribution from the free carrier absorption is shown in Fig. 1(a) as the rise of the InGaAs absorption coefficient beyond  $10^{19} \text{cm}^{-3}$ .

In terms of Q1.25, the absorption changes due to bandfilling and bandgap shrinkage are not visible till a electron concentration of  $10^{20} \text{cm}^{-3}$ , owing to its much larger initial bandgap energy compared with the photon energy at 1.55  $\mu\text{m}$ . Instead of interband absorption, the free carrier absorption is the dominant loss source in n-Q1.25.

### 3.2. Carrier-Induced Change in Refractive Index

The change in the refractive index is related to the absorption change induced by bandfilling and bandgap shrinkage, which is described by the Kramers-Kronig integral

$$\Delta n(E)_{BF,BS} = 2chP \int_0^{\infty} \frac{\Delta\alpha(E')_{BF,BS}}{E'^2 - E^2} dE' \quad (5)$$

where  $c$ ,  $\hbar$ , and  $P$  indicate the speed of light, the reduced Plank constant, and the principal value of the integral, respectively.  $\Delta\alpha(E)_{BF,BS}$  is calculated by subtracting (2) by (1). The refractive index change due to the free carrier absorption (also known as the plasma effect) is calculated separately [17], [18]. For n-type materials

$$\Delta n_{FCA} = -\frac{6.893 \times 10^{-28}}{n_0 E^2 m_e^*} N_e \quad (6)$$

where  $n_0$  is the index of the undoped material, and  $m_e^*$  is electron effective mass. The total index change is the sum of these two effects, and the resultant refractive index is therefore

$$n = n_0 + \Delta n_{BF,BS} + \Delta n_{FCA}. \quad (7)$$

The calculated refractive indices of InGaAs and Q1.25 are plotted in Fig. 1(b). Both of them reduce at the high doping range. Experimental data on n-InGaAs can be found in [21]. Our samples are characterized using spectroscopic ellipsometry [22], giving refractive indices of 3.51 and 3.20 for n-InGaAs (Sample A) and n-Q1.25 (Sample B), respectively. The error of these measured results are estimated to be  $\pm 0.02$  as indicated by the vertical error bar. It originates from the surface roughness and oxidation of the samples. Even though the decreasing trend in all these experimental data is evident, its magnitude deviates from the model. According to [21], the overestimation of the index reduction in the model is assumed to be a result of the neglected conduction band nonparabolicity and the Urbach tail near the bandgap. It seems to be impractical to precisely quantify these two missing effects in the model due to the lack of accurate experimental data. The reduced refractive index in the contact layer will also help to reduce the optical loss as the mode will be more confined in the WG layer and will have less overlap with

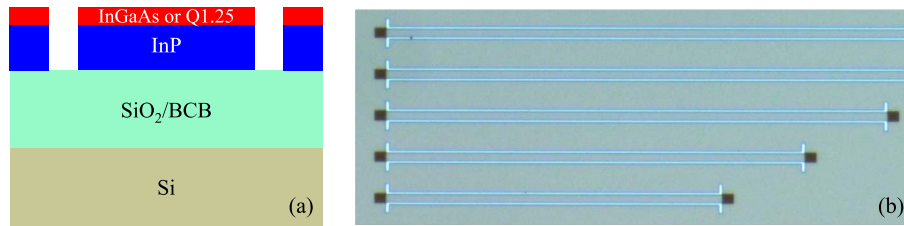


Fig. 2. (a) Schematic cross-section of a membrane WG with a contact layer (50 nm) on top. (b) Microscope image of an array of the fabricated WGs of various length. The dark parts at both ends of each WG are the grating couplers.

the metal contact on top. This effect is, however, very limited due to the relatively small reduction of the index.

### 3.3. Waveguide Measurements of Absorption From InGaAs and Q1.25

Although the model introduced in Section 3.1 predicts low optical absorption from both highly doped n-InGaAs and n-Q1.25, existing experimental data are very limited in the high doping range. To our knowledge, the only data for n-InGaAs [19] is measured using transmission spectroscopy from Liquid Phase Epitaxy grown layers with thickness inhomogeneities. The minimal absorption coefficient that could be measured is  $300 \text{ cm}^{-1}$ . As lower optical absorption in the contact layer is essential, our MOCVD grown contact layers need to be characterized to give an accurate value of the absorption coefficient.

Standard optical loss measurements using membrane WGs fabricated in our platform (InP Membranes on Silicon, IMOS [3]) have been demonstrated with very high accuracy and resolution for the determination of the optical loss coefficient. Details of the fabrication process and the measurement setup can be found in [23], [24]. Fig. 2(a) shows the schematic cross-section of the WG structure used in this work. The WG contains a 250 nm undoped InP layer and a 50 nm contact layer on top. Two samples (Sample A and Sample B) are fabricated with n-InGaAs and n-Q1.25, respectively, as the contact layer. Their doping concentrations are the same as mentioned in Section 2. The WG array used in the loss measurements [see Fig. 2(b)] consists of WGs with a fixed width ( $10 \mu\text{m}$ ) and various lengths (ranging from  $400 \mu\text{m}$  to  $1300 \mu\text{m}$ ). Grating couplers on both sides of the WG are fabricated to couple the fundamental TE polarized WG mode with single-mode fibers placed at an angle of  $9^\circ$  off vertical. A commercial laser with a tunable wavelength ranging from  $1.52 \mu\text{m}$  to  $1.63 \mu\text{m}$  is used in this measurement.

Insertion loss (including both propagation loss from WGs and coupling loss from gratings) from WGs of different lengths is measured, followed by a linear fitting. The normalized data at a input wavelength of  $1.55 \mu\text{m}$  are plotted in Fig. 3(a), showing the propagation loss from the WGs in Sample A and B as a function of the WG length. Clearly the WGs with n-Q1.25 as the contact layer produce lower loss compared to the ones with n-InGaAs. From the linear fitting the propagation loss coefficients from the WGs in the two samples can be extracted. With these modal absorption coefficients, simulations based on a vectorial mode solver can be performed to calculate the material absorption coefficient of the contact layer. The refractive indices measured in Section 3.2 are used in the simulations. Given the uncertainties in the measured indices and in the thickness of the grown layers, an error of up to 10% is estimated in the results. The calculated material absorption coefficients from measurements at different wavelengths are plotted in Fig. 3(b). At  $1.55 \mu\text{m}$  the absorption coefficients of n-InGaAs and n-Q1.25 are  $287 \text{ cm}^{-1}$  and  $103 \text{ cm}^{-1}$ , respectively. While the absorption of n-Q1.25 is close to the modeling result in Fig. 1(a), the value of n-InGaAs is almost one order of magnitude higher compared to the modeling result. This could indicate an overestimation of the bandfilling effect in the model we used. It can also be seen from Fig. 3(b) that the absorption of n-InGaAs drops with increasing wavelength, which is a signature of interband absorption. This remaining interband absorption could be related to the unfilled energy states in the conduction band, for which the amount is



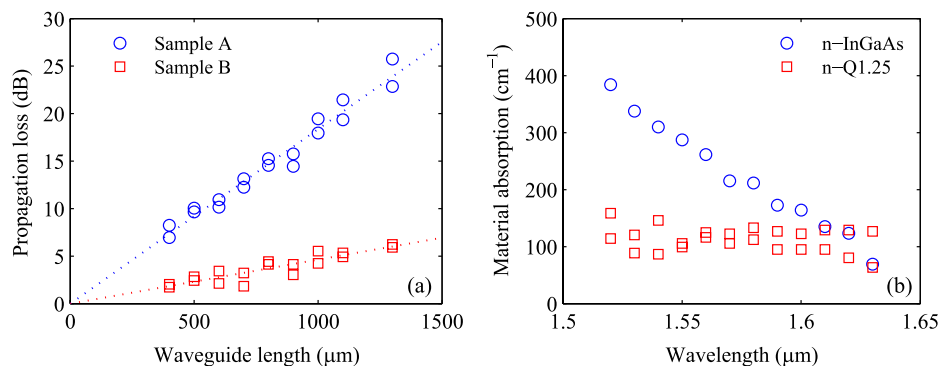


Fig. 3. (a) Propagation loss (at  $1.55 \mu\text{m}$ ) of membrane WGs in Sample A and B as a function of WG length. Dotted lines represent linear fits. (b) Material absorption coefficient of n-InGaAs and n-Q1.25 as a function of wavelength, obtained from Sample A and B, respectively.

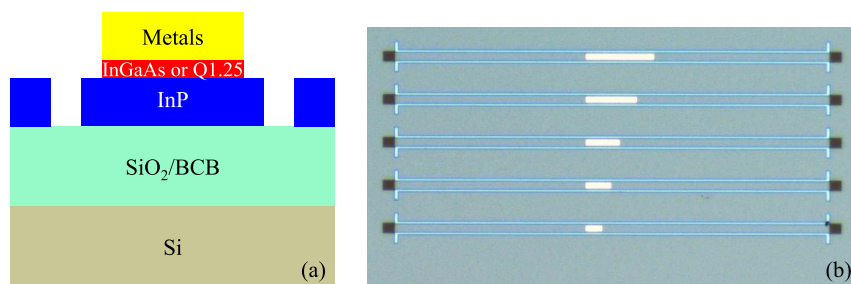


Fig. 4. (a) Schematic cross-section of a membrane WG with metal contact on top. (b) Microscope image of an array of the fabricated WGs with metal contacts of various length.

underestimated in the model. In contrast, the absorption coefficient of n-Q1.25 does not show a clear wavelength dependence, which is a typical free carrier absorption dominant behavior in n-type III-V materials in this wavelength range [25]. Considering the lower value of both the material absorption and the refractive index, n-Q1.25 should be the better choice as the contact layer material.

#### 4. Propagation Loss From Metal Contacts

After the characterization of the material loss of the contact layer with membrane WGs, the propagation loss from metal contacts is measured using the same WGs. Based on the electrical measurement results in Section 2, metal contacts with 2 nm Ge and 300 nm Ag are chosen, since they provide annealing-free ohmic contacts with sufficiently low contact resistance. They are patterned on top of the WGs using electron beam lithography and a lift-off process. Afterwards, the contact layer of InGaAs (in Sample A) and Q1.25 (in Sample B) are removed with a selective etching solution of H<sub>2</sub>SO<sub>4</sub>:H<sub>2</sub>O<sub>2</sub>:H<sub>2</sub>O (1:1:10) using the metal contacts as mask. The schematic cross-section of the resulting structure can be seen in Fig. 4(a). The width of metal contacts is designed as  $7 \mu\text{m}$ , which is slightly smaller than the WG width ( $10 \mu\text{m}$ ), to avoid metal covering of the side-walls of the WGs. Metal contacts with varying lengths deposited on top of WGs with a fixed length are measured [see Fig. 4(b)]. The same measurement approach from Section 3.3 is used here to obtain the propagation loss from the metal contacts together with the contact layers. The results are plotted in Fig. 5 for a wavelength of  $1.55 \mu\text{m}$ . The corresponding propagation loss coefficients extracted from the linear fitting are plotted versus the specific contact resistances obtained from these contacts in Fig. 6. In addition, we also compare the results from AgGe/InP and AuGeNi/InP contacts after thermal annealing (which is essential for forming ohmic

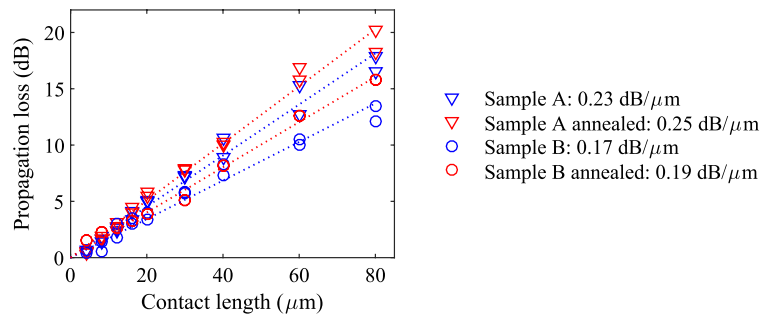


Fig. 5. Propagation loss (at  $1.55 \mu\text{m}$ ) of membrane WGs in Sample A and B as a function of the length of metal contact. Results obtained both before and after annealing are shown. The loss coefficients are obtained from the linear fits (dotted lines) and are listed in the legend.

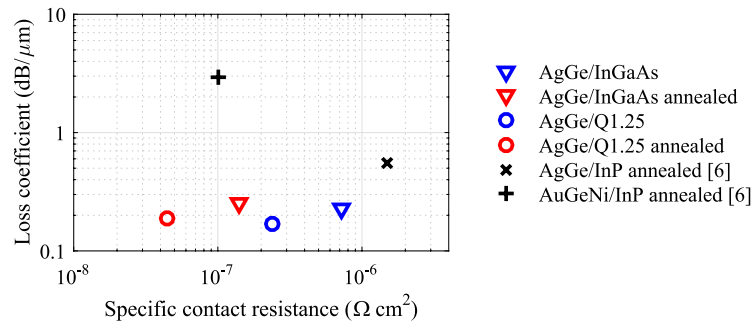


Fig. 6. Propagation loss coefficients (at  $1.55 \mu\text{m}$ ) of various contact schemes versus their specific contact resistances. For comparison, the results obtained from [6] are also included.

contacts there) [6]. It can be clearly seen that reductions not only in the contact resistance but in the optical loss are obtained in this work as well.

Without annealing, both ohmic contacts in Sample A and B show very low propagation loss, which can be expected from the low-loss AgGe metal contacts. Sample B with Q1.25 as the contact layer gives a lower loss coefficient, which is reasonable considering the lower material absorption measured from n-Q1.25 compared with that from n-InGaAs. Simulations using the material coefficients of the contact layer (obtained in Section 3.3) and of the metals (obtained in [6]) give 0.18 and 0.14 dB/ $\mu\text{m}$  for the non-annealed Sample A and B, respectively. A reasonable match with the measurement results can be seen. The residual difference can be related to the limited reproducibility of the metal deposition process, which can be overcome with better equipment and process control. Compared to the values measured from AgGe/InP and AuGeNi/InP (ohmic contacts, with annealing), the loss coefficient from the AgGe/Q1.25 annealing-free ohmic contact is lower by a factor of 3 and 17, respectively. The comparison is reasonable as all of the WG structures used in the measurements are fabricated in one membrane platform with the same thickness of the semiconductor membrane (300 nm).

Furthermore, the samples measured in this work show only a slight increase (about 10%) of the propagation loss even after the standard thermal annealing process (400 °C, 15 seconds), which is in strong contrast to previous samples. This may be related to the reduction of the Ge thickness in the new samples. According to our previous work [6], metal spikes were observed in the Ge layer after annealing, which could contribute to the propagation loss. Also, the diffusion of Ge could be another source of the increasing loss in the annealed contacts. However, the amount of Ge cannot be significantly reduced in ohmic contacts to n-InP in order to maintain a low contact resistance. In the present work, the Ge thickness can be reduced to only 2 nm thanks to the use of highly doped contact layers. Therefore, a better thermal stability and a larger thermal process window is obtained.

## 5. Conclusion

We have developed novel n-type ohmic contacts based on AgGe on InGaAs and Q1.25 contact layers. These layers can be heavily doped in MOCVD to a level which is one order of magnitude higher than the maximum doping in InP, thanks to the higher solubility of Si. This high doping concentration, from the electrical point of view, provides annealing-free ohmic contacts with low contact resistances at the level of  $10^{-7} \Omega \text{ cm}^2$ . The optical properties of the highly doped contact materials are studied. Strong bandfilling effects are observed to result in low optical absorption loss in the contact layer. The annealing-free contacts have been tested with optical loss measurements using membrane WGs. Compared to previously demonstrated AgGe/InP ohmic contacts and conventional AuGeNi/InP ones, the new solution based on AgGe/Q1.25 shows reductions in the propagation loss of a factor of 3 and 17, respectively. Furthermore, the Ge thickness in this new solution can be reduced to only 2 nm, which results in better thermal stability of the contacts. These optimized ohmic contacts with ultra-low contact resistance and optical loss are expected to enable more advanced devices fabricated in membrane photonic platforms.

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