

# Multimode optical fiber beam-by-beam cleanup

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**Abstract**—We introduce and experimentally demonstrate the concept of all-optical beam switching in graded-index multimode optical fibers. Nonlinear coupling between orthogonally polarized seed and signal beams permits to control the spatial beam quality at the fiber output. Remarkably, we show that even a few-mode control beam whose power is about ten times lower than that of the total beam may substantially enhance the quality of an intense, highly multimode signal beam. We propose a simple geometrical representation of the beam switching operation, whose validity is quantitatively confirmed by the experimental mode decomposition of the output beam. All-optical switching of multimode beams may find important applications in high-power beam delivery and fiber lasers.

**Index Terms**—Optical switch, Multimode fibers, Spatial beam self-cleaning, Optical transistor.

## I. INTRODUCTION

THE future of optical communications relies on the capacity to deliver and process complex ultrafast optical signals. In the realm of optical beam delivery, multimode fibers (MMFs) are well suited for the transmission of high-power, structured optical laser beams. As a matter of fact, MMFs support the propagation of optical beams with complex temporal and spatial properties [1], [2]. In addition, opening up the spatial degree of freedom is the key for upgrading the capacity of optical communication systems via the space-division-multiplexing technique [3]. Another noteworthy ad-

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vantage of MMFs with respect to their singlemode counterparts is their capability to support the propagation of both high-energy optical pulses and high-power beams. In this framework, MMFs naturally find applications for the power or energy up-scaling of fiber-based light sources, ranging from mode-locked ultrafast lasers [4] to supercontinuum generators [5]–[8]. In addition, high peak power beam propagation in MMF allows for exploring intriguing fundamental effects and nonlinear phenomena, such as multimode solitons [9]–[12].

Material nonlinearity plays a key role in all-optical signal processing devices: beyond birefringence, exploiting nonlinearity is the only way that two optical beams can interact. As a matter of fact, two beams propagating in a linear medium can only produce interference, but one can never change the properties of a beam by acting on another beam of light. Hence, nonlinear beam propagation has paved the way for signal processing based on all-optical technologies. This basic concept has been largely explored in the recent past [13]. Many studies of nonlinear all-optical signal processing devices have been reported in the literature, including, e.g., logic gates, switches, amplifiers and transistors [14]–[16]. All-optical signal processing has been proposed in several platforms, ranging from gases [17], [18] to semiconductors [19], [20], glasses [21], [22], quantum dot cavities [23] and integrated optical circuits [24].

In this work, we introduce a new optical platform for optical signal processing in the form of multimode guided beams. At variance with MMF-based switching devices that exploit linear beam propagation for the multiplexing of optical signals [25]–[29], here we make use of the nonlinear evolution of light. Specifically, we demonstrate the all-optical switching of a multimode light beam, controlled by a different, co-propagating multimode beam. The physical mechanism for switching is the intensity-dependent refractive index, or Kerr effect, in a standard graded-index (GRIN) MMF. When considering the propagation of a single multimode light beam in such a fiber, the same Kerr effect may self-induce a significant improvement of its spatial quality at the fiber output. Such a nonlinear phenomenon has been firstly observed in 2016 by Krupa et al. [30], and it is known as spatial beam self-cleaning [31], [32].

A sketch of the beam-by-beam switching principle is shown in Fig. 1a. We consider two orthogonally polarized laser beams, simultaneously injected into the core of a few meters long GRIN MMF. Orthogonal polarizations are chosen for the two beams, in order to avoid any spatial interference between the two beams. One of the two beams is launched with a tilt angle ( $\alpha_{sign} \simeq 2^\circ$ ) with respect to the fiber axis. This leads to exciting a relatively large number of modes in the

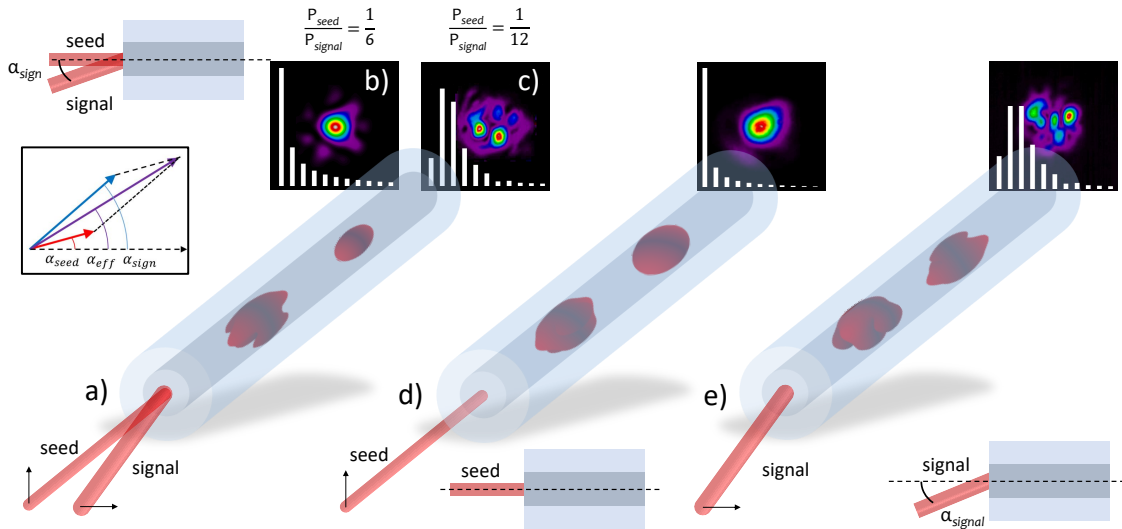


Fig. 1. (a) Sketch of the MMF-based optical beam-by-beam switching geometry. (b) Switch-on and (c) switch-off configurations: seed and signal beams are simultaneously injected into the fiber, as shown in (d) and (e), respectively: at the fiber output, the beam emerges with either high (b) or low (c) spatial quality, depending on the seed and signal injection conditions; in each case, the output mode distribution is illustrated by white histograms. (d) Injection of the sole seed beam, straight onto the fiber axis. If its input power is high enough, the output beam self-organizes into a bell shape: its mode distribution is similar to that in (b) (the fundamental mode is most populated); (e) Injection of the sole signal beam with nonzero tilt angle  $\alpha_{\text{sign}}$ . The output beam is speckled, similarly to (c), and the fundamental mode is generally not highly populated. The black arrows represent the polarization vector of the input beams.

fiber. We will refer to such a beam as signal. Whereas, a weaker beam, which we dub seed, is injected straight onto the fiber axis. Correspondingly, only fewer modes are excited. Now, by progressively increasing the seed power relative to the signal, one observes a cleanup of the total output beam, or a substantial increase in its brightness and quality. When this is achieved, that we will refer to as switch-on output state, a bell-shaped beam is obtained (see Fig. 1b). In this case, the fundamental fiber mode is the most populated in the output beam: the corresponding mode occupancy is sketched by a white histogram in Fig. 1b. To the contrary, in the switch-off configuration, a low spatial quality, speckled beam is observed at the fiber output. Correspondingly, the fundamental mode occupancy is equal or lower than for high-order modes (HOMs). This is shown in Fig. 1c.

We introduce an simple, and yet useful, representation of the beam-by-beam switching effect, which relies on a purely geometrical approach. Specifically, we describe the configuration where both seed and signal beams are injected together into the fiber in terms of a sum of two vectors in the plane. Each vector has a modulus equal to the power of the corresponding beam, whereas the orientation of the vector is measured by the injection angle ( $\alpha$ ) of the beam with respect to the fiber axis. We sketch the geometry of such representation in the inset of Fig. 1a. It is important to underline that, since seed and signal have orthogonal states of polarization, when both beams are simultaneously coupled into the fiber core, the total peak power in the fiber is

$$P_{\text{eff}} = P_{\text{seed}} + P_{\text{sign}}. \quad (1)$$

Moreover, since we are dealing with small injection angles (smaller than  $2^\circ$ ), we may use the approximations  $\cos \alpha \simeq 1$ ,  $\sin \alpha \simeq \tan \alpha \simeq \alpha$ . Thus, by following the sketch in the inset

of Fig. 1, we may write

$$\alpha_{\text{eff}} = \frac{P_{\text{seed}} \cdot \alpha_{\text{seed}} + P_{\text{sign}} \cdot \alpha_{\text{sign}}}{P_{\text{seed}} + P_{\text{sign}}}. \quad (2)$$

We underline that the sums in Eqs.(1-2) do not correspond to a vectorial sum of the electric fields associated with seed and signal beams, which are orthogonally polarized. Indeed, here we are simply performing a sum of two vectors, whose modulus is given by the beam power instead of the field amplitude [33]. In particular, in our case, we have  $\alpha_{\text{seed}} = 0$ .

The validity of such a geometric representation is strengthened by the following argument. It has been shown that, at a given propagation distance, the threshold power for self-enhancing the spatial quality of laser beam propagating into a MMF (or spatial beam self-cleaning) depends on  $\alpha$ . Specifically, the threshold power for self-cleaning increases when  $\alpha$  grows larger, as reported in Ref. [34]. Therefore, it is reasonable to associate an effective angle to the seed + signal input configuration: this angle is obtained as the weighted average of the injection angle of seed and signal beams, respectively. Here the weights are proportional to the power of each beam. As a matter of fact, this is in agreement with Eq.(2), where the weights for obtaining the average or effective angle are exactly provided by the powers of each beam.

In this regard, it is worth mentioning that the cleaning effect reported in this work requires powers of tens of kW, since only a few meter long fiber spans are used. However, experiments have shown that the power threshold for achieving spatial beam cleaning can be significantly reduced by three orders of magnitude, when using km long fiber spans [35], which are of common use for telecommunications.

In order to better appreciate the difference between the switch-on and switch-off situations, it is useful to consider

the limit cases where the power of either the signal or the seed is set to zero. These cases are shown in Figs. 1d and 1e, respectively. When a single powerful laser beam is injected straight on-axis into the GRIN MMF core, it mostly excites the fundamental mode and a few HOMs. This is a favorable condition for obtaining beam self-cleaning, whereby a bell-like shaped beam is formed at the fiber output (see Fig.1d). Being based on the Kerr effect, beam self-cleaning requires an input peak power which is above a certain threshold value ( $P_{thr}$ ). Specifically, for a few meters of a standard GRIN MMF,  $P_{thr}$  is of the order of a few kW [30], [36]. Now, the value of  $P_{thr}$  increases as the injection angle ( $\alpha$ ) grows larger, because a higher number of modes is excited in this case [34]. This significantly limits the possibility of self-cleaning for tilted beams: we found that, for  $\alpha \simeq 2^\circ$ , the value of  $P_{thr}$  at  $L = 2$  m is so high, that it overcomes of the threshold for fiber damaging. Therefore, in the absence of a seed beam, the tilted beam generates a speckled spatial intensity pattern at the fiber output (see Fig. 1e), which is similar to that of Fig. 1c.

Remarkably, injecting a seed beam alongside with the highly multimode signal beam permits to all-optically switch the output beam from a low to a high-quality state. This occurs even if the seed beam power carries down to only 10% of the signal power. In other words, one may all-optically (i.e., instantaneously) control the spatial quality of a high-power multimode beam with a relatively weak seed beam. This paves the way for efficient all-optical complex beam processing based on the MMF platform. Fiber lasers stand out among the domains of applications of beam-by-beam switching, given that controlling the spatial quality of their emission still remains a key challenge. Indeed, the switch-on configuration can be seen as a synchronized beam-combining mechanism that permits the amplification of the seed beam by a multimode signal, which is extremely useful property when building up a laser cavity.

Still, appropriate conditions must be matched for triggering the beam-by-beam switching effect. This will be the main topic of the next Sections. Specifically, we will show that specific constraints must be imposed on the power of both the signal and the seed beam, as well as on the tilting angle  $\alpha$ . By determining such constraints, we will define the working conditions for the all-optical switch. Importantly, these conditions turn out to be compatible with the operating regime of the state-of-the-art fiber devices. Our results point to the potential of our all-optical switching approach, which could be easily combined within MMF-based technologies, such as high-power fiber lasers [37], and high-resolution nonlinear imaging [38], [39].

This Article is organized as follows: in Section II, we numerically provide a proof-of-concept of the all-optical switching effect. In Section III we describe the experimental setup used for light beam characterization at the MMF output. In Section IV we discuss experimental demonstrations of the switch, including a quantitative assessment of the spatial beam quality. Moreover, we propose a simple and yet extremely useful representation of the experimental results. Specifically, we introduce a geometrical approach-based phase diagram, which allows for discriminating the working regimes (on and off) of the switch. In Section V we directly test the validity

of this representation, by carrying out an experimental mode decomposition of the beam at the switch output. Finally, in Section VI we draw our final conclusions.

## II. NUMERICAL STUDY OF THE SWITCHING EFFECT

In order to simulate the nonlinear spatial dynamics of a laser beam into a GRIN MMF, we numerically solved the vectorial two-dimensional nonlinear Schrödinger equation (2D-NLSE) as in Ref. [32]. In the numerical model, each polarization is associated with a scalar equation. Whereas, polarization coupling occurs via cross-phase modulation. The spatial window is a square of  $100 \mu\text{m} \times 100 \mu\text{m}$  with  $128 \times 128$  sampling points, with metallic boundaries and suppression of the highest spatial frequencies by a filter. In all simulations, the field remains confined within the core, which is smaller than the computational window. For sufficiently long optical pulses, and in the normal dispersion regime, nonlinear beam reshaping at the output of a MMF is essentially a spatial effect [40]. Therefore, here we do not consider temporal dynamics, i.e., we model our switching principle in the continuous wave (CW) regime. However, as we will see in the following, beam-by-beam switching can also be implemented with short pulsed sources. These are needed in experiments, in order to reach the necessary high peak power values.

In our simulations, we considered a standard parabolic GRIN MMF with a core diameter of  $50 \mu\text{m}$ , a maximum value for the core refractive index  $n_{co} = 1.47$ , and a cladding refractive index  $n_{cl} = 1.457$ . We took into account the presence of fiber disorder, that leads to power exchanges between orthogonally polarized beams, and it has been shown to facilitate the occurrence of the nonlinear spatial beam cleaning [41]. In order to mimic an effect similar to that of fiber stress or bending, we applied a coarse step beam propagation method. This approach is based on introducing a sequence of random local deformations to the refractive index profile. The coarse step is applied every 5 mm. At each step, the electric field is first rotated by a random angle taken from a uniform distribution. Then, the fiber core is made slightly elliptical along the segment of propagation; the values of the fiber diameter are selected by random variables with uniform distribution and a maximum deviation of  $0.1 \mu\text{m}$  from the reference value  $R = 25 \mu\text{m}$  on each axis; the procedure is repeated for both polarization components. The ellipse describing the local deformation of the fiber core is also randomly oriented. Moreover, the ellipse orientation as well as the maximum and minimum values of the fiber diameter assume different values for the two polarization components. In this way, at each coarse step the waveguide contribution to the linear polarization is calculated with slightly different refractive index profiles for the two polarization components. We considered a nondispersive Kerr nonlinear index  $n_2 = 2.7 \times 10^{-20} \text{ m}^2/\text{W}^{-1}$ . We used an input beam diameter (full-width-half-maximum of intensity) of  $40 \mu\text{m}$  at a laser wavelength of 1064 nm.

The results of our numerical simulations are shown in Fig.2. In particular, in Figs. 2a and 2b, we illustrate the propagation of the sole seed beam (like in Fig. 1d). As it can be seen, in

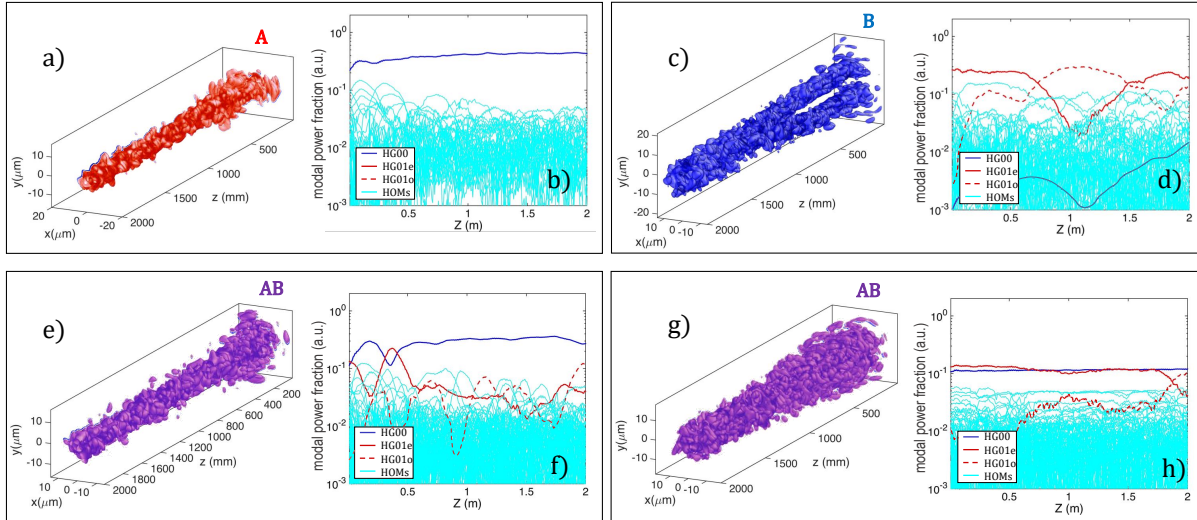


Fig. 2. Numerical simulations illustrating the beam-by-beam switching principle. a,b) Beam evolution in the presence of the sole input seed beam, with intensity of  $5 \text{ GW/cm}^2$  (a); corresponding output mode occupancy (b). c,d) Same as (a,b), with the sole input signal beam, with intensity of  $5 \text{ GW/cm}^2$ . e,f) Same as (a,b), with both seed and signal beams at the fiber input, each with intensity of  $5 \text{ GW/cm}^2$ . g,h) Same as (e,f), for low power seed and signal beams (with intensity of  $0.5 \text{ kW/cm}^2$ , quasi-linear propagation regime).

the nonlinear regime, the beam progressively shrinks its size: the diameter in the  $xy$  plane reduces upon propagation in the  $z$  direction (see Fig. 2a). This corresponds to an increase of the fundamental mode population, whose fractional occupation is shown by a dark blue line in Fig. 2b. Whereas the occupancy of HOMs reduces by more than one order of magnitude after 2 m of propagation (light blue curves in Fig. 2b). For the mode representation, we consider the Hermite-Gaussian base (from mode HG00 to HG1010), so that the fundamental mode is dubbed HG00, and the first HOM is HG01. The latter is then distinguished into ordinary HG01o and extraordinary HG01e, since in our vector model we took into account fiber birefringence. Specifically, the ordinary index corresponds to the horizontal polarization, i.e., that of the seed, and the extraordinary index corresponds to vertical polarization, i.e., that of the signal.

In Fig. 2c,d, we present a case that mimics the injection of the mere signal beam. Specifically, we show the nonlinear evolution of a vertically polarized laser beam, which is not injected straight onto the fiber axis. To the contrary, we consider an input beam configuration with a dual-lobe profile (see Fig. 2c). This corresponds to a mode composition at the fiber input where the fundamental mode is poorly populated (see the dark blue line in Fig. 2d). Whereas the most populated mode is the HG01e mode (as shown as a red solid line in Fig. 2d). The relative occupation of HG01e and HG01o modes periodically oscillates during their propagation. Note that the fundamental mode occupancy progressively grows up (dark blue curve in Fig. 2d). However, after 2 m of propagation, its occupancy is still relatively weak, so that the output beam remains speckled, as it occurs in the presence of the sole signal beam.

Under these conditions, we may reproduce the optical

switching effect which occurs whenever both seed and signal beams are simultaneously injected into the fiber core. This is shown in Figs. 2e and 2f, where the seed and the signal beams have the same intensity. As it can be seen, the combined beam evolution qualitatively resembles that of Fig. 2a with the seed beam only. Indeed, the beam progressively shrinks during its propagation (cfr. Fig. 2d), and the fundamental mode is again the most populated at the fiber output (dark blue line in Fig. 2e). As a result, the output beam acquires a bell-like shape, similar to the case reported in the inset of Fig. 1b. Finally, we underline that the optical switching process is actually driven by the MMF nonlinearity.

As a matter of fact, when considering the seed + signal configuration in the linear propagation regime, the combined beam only slightly reduces its size after two meters of propagation, simply due to the linear guiding properties of the MMF (see Fig. 2g). Moreover, at variance with the nonlinear regime, the occupancy of the fundamental mode remains constant during beam propagation, and there is only a random mode coupling induced exchange of mode occupancy between degenerate modes, as illustrated in Fig. 2h.

### III. EXPERIMENTAL SETUP

Our experiments were carried out by means of two separate experimental setups, involving two different laser sources. Specifically, the source that we used in the first setup was a Nd:Yag laser (Spark Laser, Sirius-type) emitting pulses of 65 ps with 100 kHz repetition rate at 1064 nm. Whereas, in the second setup we used a Yb-based laser (Light Conversion PHAROS-SP-HP), generating pulses with tunable duration, ranging between 174 fs to 7.8 ps with 100 kHz repetition rate, at 1030 nm.

The two setups were rather similar, at least, as far as the optical components placed before the fiber input (as sketched in Fig. 3) are concerned. We split the laser source into two temporally overlapping laser beams with orthogonal linear polarization, in order to inject them into a 2 m long off-shelf Alcatel GRIN MMF with 50  $\mu\text{m}$  core diameter, according to the geometry of Fig. 1a, and with  $\alpha_{\text{sign}} = 1.83^\circ$ . The splitting of the laser source beam into two arms (seed and signal), as well as the control of their state of polarization, was obtained by means of a polarizing beam splitter (PBS). Specifically, we used a configuration that resembles that of a Michelson interferometer. However, at variance with the latter, the presence of a PBS, on the one side, produces two beams with orthogonal linear polarization and, on the other side, requires the insertion of quarter-waveplates ( $\lambda/4$ ) in both the seed and the signal arms. In fact, in the absence of such  $\lambda/4$  retarders, both seed and signal beams would be reflected back towards the laser source by the PBS, since they would maintain their polarization state. To the contrary, the combined action of the PBS, the  $\lambda/4$  and the mirrors (M) allows for light to reach the fiber input. In particular, the mirror of the signal arm was slightly tilted, in order to introduce a nonzero injection tilt angle  $\alpha_{\text{sign}}$  as in Fig. 1. Note that, by acting on the orientation angle of each  $\lambda/4$ , we could vary the power of each arm, without varying that of the other (see results in Fig. 4a). Whereas, by acting on the half-waveplate ( $\lambda/2$ ), we could vary the value of the power fraction  $R = P_{\text{seed}}/P_{\text{sign}}$ , while keeping constant that of  $P_{\text{seed}} + P_{\text{sign}}$  (as it occurs for the results shown in Fig. 4b and in Fig. 6, respectively). The latter, instead, was varied by means of a variable attenuator (VA), as in Fig. 4c.

Finally, as we were working with short pulses, in order to verify the synchronization of the seed and signal beams, we interposed a flipping mirror (FM) between the PBS and the injection lens (L1) which focuses both beams into the fiber core. A CCD camera was placed after an optical path, which was equivalent to that travelled by the light in order to reach the fiber input. We inserted a  $45^\circ$  oriented polarizer (LP1) in order to image interference fringes on the camera. In this way, the temporal synchronization of the two beams could be verified by the occurrence of an interference pattern. To this purpose, the mirror of the seed beam was placed on a micrometric slit, as it is conventionally done for standard Michelson interferometers.

The main difference between the two setups consists of the methods for beam analysis at the fiber output. In the setup involving the Nd:Yag laser, we only measured the intensity profile of the output beam by means of a silicon CCD camera (Gentec Beamage), along with the fiber power transmission. Whereas, the setup that involves the Yb-based laser system also included an apparatus for performing the mode decomposition (MD) of the output beam. A sketch of the optical components that we used for the MD study is illustrated in the right side of Fig. 3.

At the fiber output, the beam is collected by means of a microlens ( $\mu\text{L}$ ). A second lens (L2) is used for imaging the near-field at the fiber output onto a spatial light modulator (SLM) (Hamamatsu LCOS- X15213). In order to image the

field that reaches the SLM, we inserted a flipping mirror (FM2), so that the focus of the L2 lens coincides with the screen of a CCD camera (Gentec Beamage-4M-IR), dubbed as near-field (NF) camera. Finally, a third lens (L3) projects the Fourier transform of the beam reflected at the SLM surface onto a CCD camera (Gentec Beamage-4M-IR), dubbed as far-field (FF) camera. Note that, since the SLM only works with a linearly polarized beam, we placed a linear polarizer (LP2) right before L2. In order to maximize the power that reaches the SLM, we also added a  $\lambda/2$  waveplate right before LP2. We underline that the orientation angle of the  $\lambda/2$  waveplate was different for the three configurations shown in Fig. 1, since the output polarization depends on the input state of polarization. Moreover, a bandpass filter (BPF) was used in order to avoid a possible loss of temporal coherence due to significant self-phase-modulation induced spectral broadening in the MMF. This would be disturbing for the MD analysis, since the SLM requires to operate under nearly monochromatic excitation.

The MD analysis relies on the association to each intensity pattern on the NF camera to a set of images on the FF camera, which are obtained by varying the phase mask that is encoded by the SLM. Such phase masks are chosen in order to separate information coming from each of the modes that compose the output beam. Thus, by means of a numerical algorithm, it is possible to retrieve the value of amplitude and phase associated to each mode for a given output beam. In this way, we could reconstruct the beam patterns shown in Figs. 6b-d. Here, we do not provide details about our MD algorithm, whose full description can be found in Ref. [42].

As a final note, it is important to underline that the presence of the linear polarizer LP2 allows for properly measuring the mode content of a beam which has a linear polarization state. This idea applies well to the cases of either sole seed or sole signal injection, where the output state of polarization remains approximately linear even at the MMF output. Specifically, besides the occurrence of some depolarization effects, the circular component of the output beam polarization was negligible with respect to the linear one. To the contrary, one may wonder what is the polarization state at the fiber output, in the case of simultaneous injection of both seed and signal. However, we verified that, in the experimental conditions of Fig. 6, the degree of linear polarization at the fiber output still remained quite higher than that of circular polarization. Moreover, the direction of the linear polarization vector, i.e., the angle of the  $\lambda/2$  that maximized the power transmitted through LP2, was the same as that corresponding to the injection of the sole seed beam. Therefore, for all of the experiments reported in this work, the MD performed along one polarization direction can be identified, within a reasonable approximation, with that corresponding to the entire output beam.

#### IV. EXPERIMENTAL RESULTS WITH THE ND:YAG LASER

Fig. 4 illustrates the experimental demonstration of MMF-based beam-by-beam cleanup. Here we report three different experiments, each with a different set of initial conditions. Specifically, we fixed: (a) the ratio  $R$  between the seed and

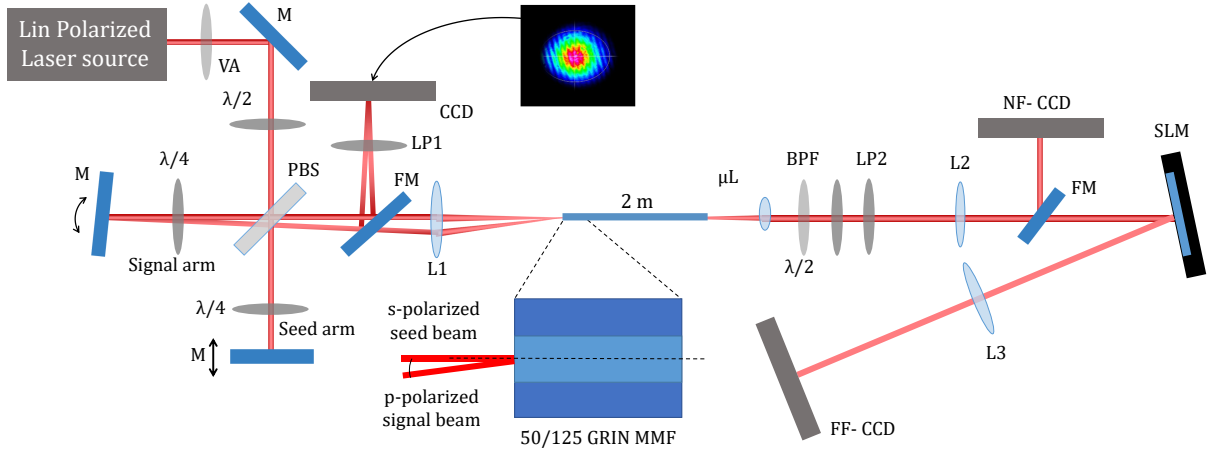


Fig. 3. Sketch of the experimental setup. VA: Variable Attenuator;  $\lambda/2$ : Half waveplate;  $\lambda/4$ : Quarter waveplate; M: Mirror; FM: Flipping Mirror; PBS: Polarizing Beam Splitter; FM: Flipping Mirror; LP: Linear Polarizer; L1: Injection Lens;  $\mu L$ : Microlens; BPF: Band Pass Filter; L2, L3: Mode decomposition lenses; SLM: Spatial Light Modulator.

the signal power (cfr., Fig. 4a); (b) the power of the signal beam (cfr., Fig. 4b); (c) or the sum of the seed and the signal power (cfr. Fig. 4c). In each subfigure, we show the beam profile in the presence of: (i) the sole seed beam (“seed” column); (ii) the sole signal beam (“sign” column); (iii,iv) both seed and signal beams synchronized and out-of-sync (“seed+seed” and “linear” column, respectively), as the power of the seed grows larger. The out-of-sync configuration was achieved by displacing the mirror at the bottom of Fig. 3 to

make disappearing the interference fringes shown in the inset of the same figure. In this regard, we underline that the last column coincides with the incoherent linear average of the first two columns weighted by their corresponding power. For this reason, we name this column as “linear”. The peak power value at the fiber input associated with the near-field beam profile is reported under each image in Fig. 4a-c and it was calculated as

$$P = \frac{\langle P \rangle}{\tau \cdot RR}, \quad (3)$$

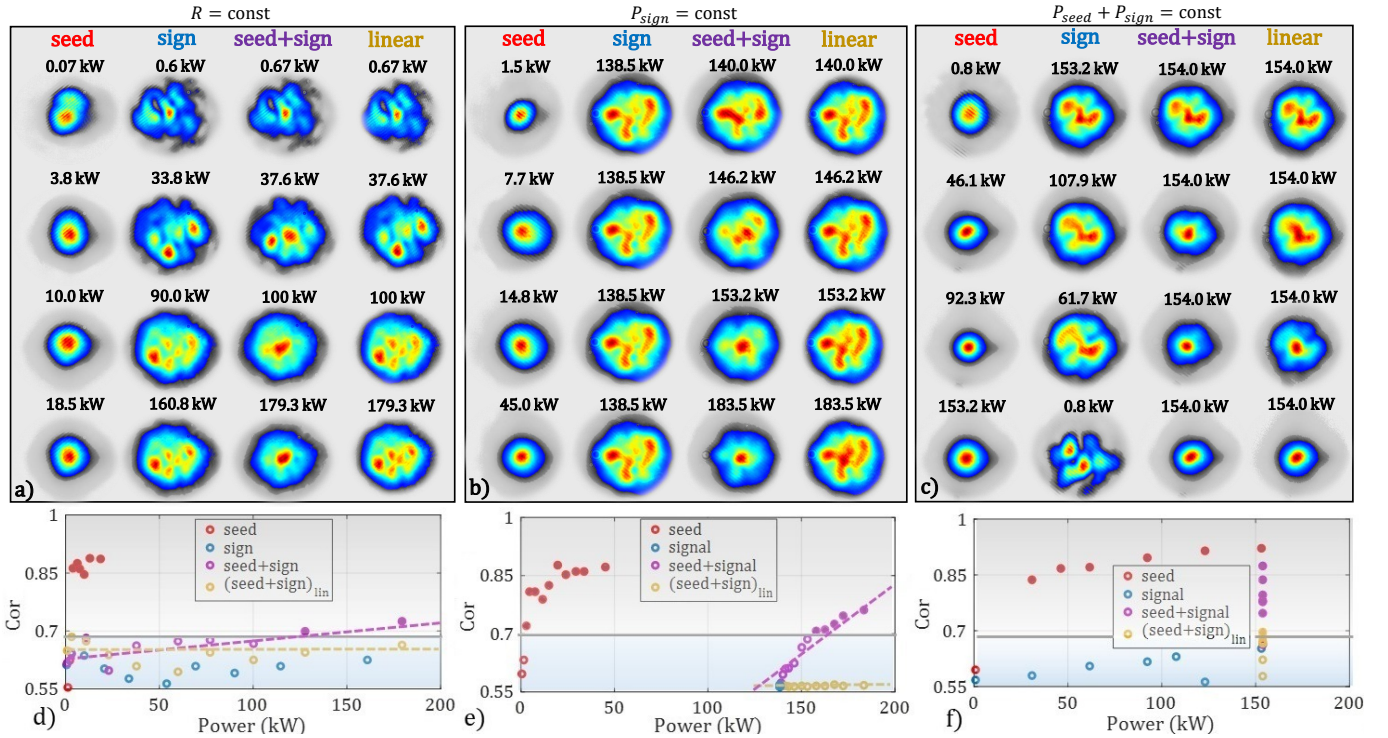


Fig. 4. Beam images at the fiber output for three separate beam switching experiments. Here we fix either: the ratio between the power of the seed and the signal beam  $R \simeq 1 : 9$  (a), the power of the signal beam (b), and the sum of the latter (c). In each panel, the first (second) column shows the case when the sole seed (signal) is injected; for the third (fourth) column, both beams are injected in-sync (out-of-sync). d-f) Evaluation of the correlation parameter  $Cor$ , calculated by Eq. (4), for the experimental data in (a-c). The dashed lines are guides for the eye.

where  $\langle P \rangle$  is the measured average beam power at the fiber output, RR is the laser repetition rate, and  $\tau$  is the pulse duration.

As it can be seen in Fig. 4a, whenever the power ratio ( $R$ ) between seed and signal is fixed (e.g.,  $R = 1 : 9$ ), the seed beam must be powerful enough in order to clean-up the overall output beam. Note that here the seed power threshold value ( $P_{seed} = 10.0$  kW) is one order of magnitude higher than the power threshold for self-cleaning of the seed beam alone (which is about 1 kW). Moreover, in Fig. 4b we show that when the signal beam power is fixed, there is again a threshold value of  $P_{seed}$  for obtaining cleanup of the signal beam: here this threshold turns out to be equal to 14.8 kW. As a matter of fact, the same panel also shows that signal cleanup (switch-on condition) occurs for values of  $R$  as low as 1 : 9 (i.e., 14.7 kW : 138 kW). The results in Figs. 4a and 4b demonstrate that one must control both  $P_{seed}$  and  $R$ , in order to properly operate the beam-by-beam switching. Finally, in Fig. 4c, we show that results obtained when the sum of the seed and signal power is kept at a constant value are consistent with the observations in Figs. 4a,b. In this regard, we also underline that in all panels of Fig. 4 the power values in the third and fourth columns are equal to the sum of the powers appearing in the first two columns, in agreement with Eq. (1).

When only looking at the first three columns in Fig. 4b,c, one may argue that a tight Gaussian seed beam added to a large size speckled signal beam with comparable powers could produce a clean output intensity profile, even in the absence of a nonlinear clean-up mechanism, because the tight seed beam could dominate the color scale. This possibility is clearly disproved by looking at the fourth column (linear), which shows the sum of the output beam intensities that are obtained when injecting each beam at a time. Indeed, one can appreciate that a clean “seed+sign” column is not associated with a clean “linear” column, unless the seed power is higher than the signal power (two bottom columns of Fig.4c. This demonstrates the true nonlinear nature of the beam-by-beam clean-up effect.

### Quantitative evaluation of the spatial quality

So far, when discussing the experimental results in Fig. 4a-c, we only qualitatively distinguished the shape and quality of the output beam profiles. Namely, we did not yet quantify the spatial quality of the output beams. Here, we provide a quantitative analysis of the images reported in Fig. 4a-c. Specifically, we evaluate the correlation of the intensity of the output beam ( $I$ ) with that of the fundamental mode of the GRIN MMF that we used in the experiments ( $I_0$ ). According to the specifications provided by the manufacturer, the fundamental mode intensity profile can be represented in terms of a 2D Gaussian beam shape with a waist  $w = 6.33$   $\mu\text{m}$ . Hence, the image correlation with the fundamental mode is evaluated as [34]

$$Cor = \frac{\int I(x, y)I_0(x, y)dxdy}{\sqrt{\int I(x, y)^2dxdy \int I_0(x, y)^2dxdy}}, \quad (4)$$

where  $I_0 \propto \exp\{-2(x^2 + y^2)/w^2\}$ . Note that both  $I$  and  $I_0$  are normalized in a way that their integral over the CCD camera area is equal to 1. The values of  $Cor$  which correspond to the same experimental conditions as in Figs. 4a-c are reported in Figs. 4d-f. For sake of completeness, we calculate  $Cor$  for all of the four configurations that we have considered in Fig. 4a-c, i.e., injection of the sole seed, of the sole signal, and of both seed and signal, either in-sync and out-of-sync. The corresponding results are collected in Fig. 4d-f, and marked by red, blue, violet and yellow dots, respectively. Therein, we plot as void circles data that correspond to low spatial quality output beams in Fig. 4a-c. Whereas, beams that we dubbed as highly spatial quality or clean beams are represented here by full circles. As it can be seen in all of the graphs of Fig. 4d-f, there is a threshold value of the correlation ( $Cor = 0.68$ ), which permits to split apart void and full circles. As a consequence, we can associate to an output beam the label of either “high” or “low” spatial quality, by computing its correlation  $Cor$  with the fundamental from Eq. (4). If  $Cor > (<)$  0.68, then we consider the corresponding beam to be of high or low quality, respectively. In this regard, we underline that the existence of a threshold of the  $Cor$  value in determining the beam cleanliness at the fiber output must be seen in analogy with the gate contrast parameter of optical switches. The latter is defined as the ratio between the total power which passes through an output aperture, either in the presence or in the absence of the seed beam [43]. In particular, we found that  $Cor = 0.68$  corresponds to a gate contrast equal to 2. In addition, analogously to what discussed in the previous Section, one can appreciate how the beam-by-beam clean-up is indeed due to the nonlinear interaction between the signal and the seed beams. As a matter of fact, for all input powers, the yellow dots in Fig. 4d-f are always associated with smaller values of  $Cor$  with respect to violet dots. In particular, in Fig. 4d,e, it can be seen how the growth of  $Cor$  vs. input power for the in-sync seed+sign configuration turns out to be steeper than that of the out-of-sync configuration (the corresponding trends are highlighted by dashed lines).

As a final note, we stress the reason behind the evaluation of the spatial beam quality by means of  $Cor$  instead of the more conventional  $M^2$  parameter. Since in the next Section, we will compare the evaluation of the beam quality with MD experiments, the evaluation of  $Cor$  is more appropriate than that of  $M^2$ . In fact, the main difference between  $Cor$  and  $M^2$  is that the former is somewhat related to the occupancy of the fundamental mode, i.e., it is bound to the fiber size, whereas the latter does not depend on the beam diameter (at least as long as collimated beams are considered) as it accounts for the divergence of laser beams that propagate in the free-space.

### Geometrical approach-based representation

Before presenting the MD results, here we display the experimental data of Fig. 4 in terms of  $(\alpha_{eff}, P_{eff})$  phase plane diagrams, following the geometrical representation introduced in Section I. The result is shown in Figs. 5a-c. As it can be seen, for each couple of points (seed, signal) which is depicted by either red or blue circles, respectively, we may associate

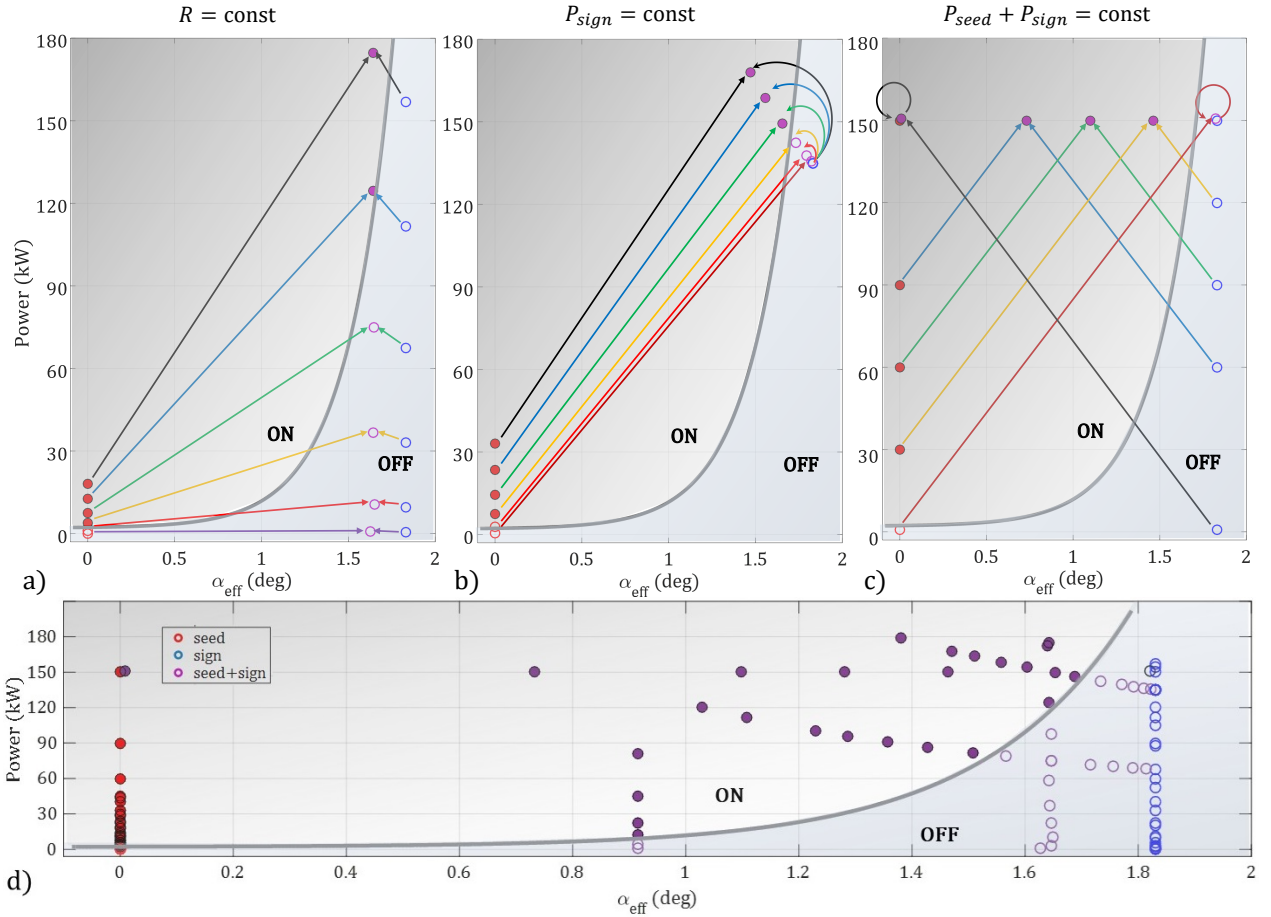


Fig. 5. a-c) Geometrical-based representation of the data in Figs. 4a-c, as depicted in the inset of panel (a). The values of power in the vertical axis are calculated by Eq. (1), whereas the values of  $\alpha$  in the horizontal axis are calculated by Eq. (2). d) Plot of the data obtained in the experiment with the Nd:Yag laser within the  $(\alpha_{\text{eff}}, P_{\text{eff}})$  diagram.

a violet dot, whose coordinates ( $\alpha$  and  $P$ ) are calculated by means of Eqs. (2) and (1), respectively. Each association is marked by two colored arrows. Analogously to Fig. 5a-c, again we assigned full and empty circles to high or low spatial quality beams, respectively. Note that here we are not considering the out-of-sync data in the “linear” columns of Figs. 4a-c since these do not provide the beam-by-beam clean-up effect.

As it can be seen, all the graphs in Figs. 5a-c can be split into two separate phase plane domains. A first zone, in the bottom-right side of all graphs, collects all of the void circles, and it can be associated with the switch-off regime of Fig. 1c. Whereas, a second region, in the top-left side of the panels in Figs. 5a-c, corresponds to the switch-on condition of Fig. 1b, since it incorporates all of the full circles.

The switch-on and switch-off regions are separated by a threshold condition, that links the input peak power to the injection angle. Such a threshold is depicted by a gray solid line in Figs. 5a-c. To the best of our knowledge, no studies of the shape of such curve have been reported in the literature so far. Here we used an empirical curve, which appears to properly describe the separation between the switch-on and switch-off conditions. In this regard, however, we underline

that the separatrix must be considered as a mere guide for the eye; as a matter of fact, we used an arbitrary exponential curve which, among the elementary functions, turned out to be the best one to fit the experimental data. The validity of the fit can be appreciated in Fig. 5d, where we report in the same diagram all available data related to the experiments carried out with the Nd:Yag laser.

It is worth underlining that, although the quantitative evaluation of the beam quality turns out to be effective for representing the cross-cleaning process, upon which the optical switching effect is based, the exact value of  $Cor$  which provides the partition of the  $(\alpha_{\text{eff}}, P_{\text{eff}})$  plane is somehow arbitrary. As a matter of fact, the threshold value  $Cor = 0.68$  is chosen by starting from a qualitative distinction between low- and high-quality beams in Fig. 4. Hence, the gray separatrix in Fig. 5a-d does not describe for a sort of phase-transition from low to high-quality beams. Indeed, cross-cleaning relies on the same physical mechanism (Kerr effect) as beam self-cleaning does. The latter only occurs when the input coupling conditions are favorable enough (in terms of peak power and injection angle, respectively).

However, the occurrence of beam self-cleaning does not have a precise power threshold, so that it suddenly ap-



appears when a certain input power and coupling condition is reached. To the contrary, self-cleaning is based on a mechanism whereby a multimode beam approaches its state of equilibrium (bell-shaped beam on a background), which is gradually reached upon its propagation. In this regard, it has been recently shown that such an equilibrium is reached whenever the distribution of the mode power fraction follows a Rayleigh-Jeans (RJ) law [44]. Therefore, one can theoretically establish whether or not a beam is clean, i.e., whether or not the mode distribution of a clean beam obeys the RJ law. Experimentally, this requires to resolve the mode content of a beam, which is the topic of the next Section. As far as the results reported so far are concerned, we underline that the existence of a theoretical condition for beam self-cleaning validates the tracing of the separatrix in Fig. 5d, as well as the existence of a threshold value of  $Cor$  (as illustrated in Fig. 4d-f). As a matter of fact, the parameter  $Cor$  can be associated with the occupancy of the fundamental mode, whose value at thermal equilibrium is fixed, once that the laser-fiber coupling conditions are given [44]. In this regard, it is worth mentioning that, generally speaking, the occurrence of the spatial beam self-cleaning effect does not imply that all the optical power is transferred to the fundamental mode (see, for instance Ref. [36]). As a consequence, clean beams intrinsically own a multimode nature which derives from a process of classical wave thermalization towards the RJ distribution.

## V. EXPERIMENTAL RESULTS WITH THE YB-LASER

In this Section, we report experiments carried out with the Yb-laser source at 1030 nm; we have set the pulse duration to 2 ps, and varied the values of the signal injection angle  $\alpha_{sign}$ . With this setup, we have also carried out an experimental MD analysis of the output beam, for all the beam configurations that we have described in the previous Section, i.e., with the injection of either the sole seed, the sole signal, or both.

### Experimental results with different values of $\alpha_{sign}$

At first, we repeated our experiments with input beam conditions similar to the experiments with the Nd:Yag laser. Here we used a length  $L = 3$  m of the same GRIN MMF; we set  $R = 1:2$ , and considered two different values of  $\alpha_{sign}$ , i.e.,  $\alpha_{sign} = 1.5^\circ$  and  $\alpha_{sign} = 1.6^\circ$ , respectively. The overall results are summarized in the phase plane portrait of Fig. 6a, as we did in Figs. 5. As it can be seen, even when varying the injection angle of the signal, we always obtain an exponential dependence of the threshold power on angle  $\alpha_{sign}$ , which separates the switch-on and the switch-off regions.

One may notice that the exponential separatrices in Fig. 6a and in Figs. 5d do not exactly overlap. This might be due to differences in the experimental conditions, i.e., the different bending of the MMF, as well as its length (in the Nd:Yag laser experiments we used  $L = 2$  m, and here  $L = 3$  m). However, one may appreciate that, in the spite of the different wavelengths and pulse durations of the two laser sources, the threshold input peak powers remain relatively similar (i.e., of the same order of magnitude) in both experiments. For instance, at  $\alpha_{eff} = 1^\circ$  the separatrix provides a peak power

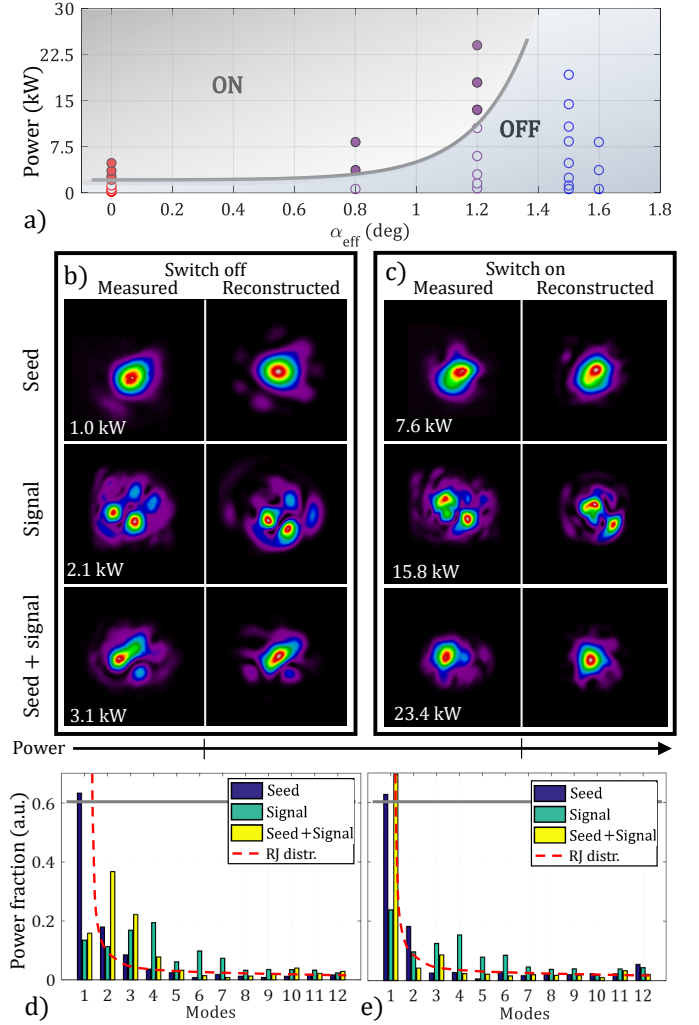


Fig. 6. Experimental results with the Yb-laser. a) Phase plane diagram of the switch operation, as in Fig. 5. Two set of data, corresponding to  $\alpha_{seed} = 1.5^\circ$  or  $\alpha_{seed} = 1.6^\circ$ , respectively, are plotted on the same graph, in order to highlight the general validity of the separatrix (gray solid line) between the switch-on and the switch-off regions. b,c) Measured output beam profile (left column) and its reconstruction by means of the MD analysis (right column). In these experiments, the ratio between the seed and the signal power is equal to  $R = 1:2$ ; the power of the seed beam was varied from 1.0 kW (b) up to 7.6 kW (c). d,e) MD results corresponding to the output beams in (b,c).

of 11.5 kW in Fig. 5d, and of 5 kW in Fig. Va. This is consistent with previous observations that beam self-cleaning is a purely spatial effect while group velocity dispersion remains negligible [44].

### Mode decomposition

In order to complement the measurements of the correlation between the output intensity and that of the fundamental mode with more comprehensive information about the modal content of the output field, we carried out the MD of beam at the fiber output. We considered the case with  $\alpha_{sign} = 1.6^\circ$  (cfr. Fig. 6a). In our MD, we computed the power fraction in the fundamental mode, i.e., the HG00 mode, along with that of the first 77 HOMs. Such relatively large number of modes was found to provide a good compromise between the time convergence of the MD algorithm, and the quality of the near-

field reconstruction of the output intensity profiles. Indeed, in Figs. 6b,c, one may appreciate the similarity between the measured output beam profile (left column) and its reconstruction by means of the MD technique (right column). Specifically, in the subpanels, we compare the images obtained with: (i) injection of the sole seed (top row); (ii) injection of the sole signal (mid row); (iii) injection of both signal and seed (bottom row). In addition, in Figs. 6b,c, we compare the results for two values of  $P_{seed}$ , i.e., 1.0 kW and 7.6 kW, which correspond to the switch-off and switch-on cases, respectively.

The MD results for the cases in Figs. 6b,c are shown in Fig. 6d,e. In order to improve the readability of the figures, here we report the measured relative mode occupancy of the first 12 modes only. In this regard, it is worth underlying that the mode occupancy quickly decreases as the mode number grows larger. The most evident feature of Fig. 6d,e is that, whenever the output beam has a bell shape, i.e., for the seed alone and for the total field with  $P_{eff} = 23.4$  kW, the fundamental is the most populated mode. Conversely, whenever the fundamental mode has an occupancy close to that of some HOMs, a speckled output beam intensity profile is obtained.

From the MD analysis, we may empirically define a threshold value of the relative fundamental mode occupancy, which permits for distinguishing between high and low quality beams. Such a value turns out to be equal to 0.6, and it is indicated by a horizontal line in Figs. 6d,e. This result further supports the validity of the geometrical representation that we have introduced in Section IV. In fact, it turns out that evaluating the correlation of a beam with the fundamental mode by means of Eq. (4) also provides a good tool for distinguishing between high and low quality beams. This is because, as mentioned in Sec. IV, crossing the threshold for  $Cor$  also corresponds to crossing the fundamental mode occupancy threshold. Finally, we would like to underline that, in the cleaning configuration, the mode distribution associated with the simultaneous injection of the seed and the signal beams can be well approximated by a RJ law (red curve in Fig. 6e), in agreement with the predictions of a thermodynamic description.

## VI. CONCLUSION

In conclusion, we introduced and experimentally demonstrated the all-optical control of multimode beams in optical fibers. Specifically, a relatively weak seed beam may control the spatial quality of an intense, orthogonally polarized signal beam at the fiber output. The seed beam can lead to a substantial enhancement of the spatial quality of signal beams with up to tenfold higher power, thanks to a proper adjustment of their injection conditions at the fiber input. The operating mechanism of the switch relies on the nonlinear properties of GRIN MMFs, and, in particular, on the Kerr beam cleaning effect in GRIN fibers. Numerical simulations, based on the vector 2D-NLSE, predict that the propagation of two orthogonally polarized laser beams with different multimode content in a GRIN MMF may lead to the enhancement of the overall beam quality at the fiber output, leading to the generation of a bell-shaped profile with a waist close to that of the

fundamental mode of the fiber. This concept was experimentally verified, and the beam injection configurations leading to the beam-by-beam cleanup effect, i.e., the switch-on and switch-off conditions, could be determined. A simple empirical geometrical representation was proposed, and experimentally validated across an extensive range of different input beam conditions, laser wavelengths and pulse durations. The output beam quality was quantitatively assessed by computing the intensity correlation of the output images with the intensity profile of the fundamental mode. Finally, we confirmed our findings by carrying out a mode decomposition analysis of beams emerging from the fiber output. This confirmed that, indeed, cleaned beams have a dominant fundamental mode contribution.

Because of its all-in-fiber nature, beam-by-beam cleaning can be naturally incorporated in state-of-the-art MMF-based technologies, such as space division multiplexed networks and high-power fiber lasers. Finally, since the beam self-cleaning effect has been described as result of wave thermalization [44], [45], our results may pave the way for new developments in the physics of multimode wave systems.

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