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Design of a freeform two-reflector system to collimate and shape a point source distribution

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Abstract: In this paper we propose a method to compute a freeform reflector system for collimating and shaping a beam from a point source. We construct these reflectors such that the radiant intensity of the source is converted into a desired target. An important generalization in our approach compared to previous research is that the output beam can be in an arbitrary direction. The design problem is approached by using a generalized Monge-Ampère equation. This equation is solved using a least-squares algorithm for non-quadratic cost functions. This algorithm calculates the optical map, from which we can then compute the surfaces. We test our algorithm on two cases. First we consider a uniform source and target distribution. Next, we use the model of a laser diode light source and a ring-shaped target distribution.

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1. Introduction

Beam shaping is an important research topic within illumination optics. Especially the shaping of a parallel beam into another parallel beam with a different distribution is well researched [1–3]. This is often linked to the shaping of laser beams. A common source for a laser is a laser diode, which can be modelled as a point source [4,5]. The diverging beam from such a diode is often collimated first with a lens, before other manipulations such as beam shaping are applied [5]. An optical system that directly shapes and collimates the output from a point source is able to skip the first collimation step. This can reduce the total number of necessary optical surfaces and increase the efficacy by avoiding Fresnel reflections. An example of a useful light distribution in a collimated beam that we will discuss is the ring shape, meaning that the projection of this beam on a plane perpendicular to it gives a ring-shaped illumination pattern. A possible benefit of such a ring-shaped target is that a subsequent focussing can be done more accurately [6]. A ring-shaped illumination pattern also has a use in welding [7].

In most research regarding collimated beams, it is assumed that the outgoing beam is in the same direction as the incoming beam. For the case of a point source, however, there is not one single direction of light emission, but often there exists a symmetry axis that plays the role of beam direction. In this paper we will drop that assumption and allow the outgoing beam to be in any arbitrary direction. This gives us the possibility to create so-called folded optics. As a result we can design more compact optical systems. As mentioned, we will look for an optical system to collimate a beam from a point source. For this we need two optical surfaces, one to shape the light to the desired target distribution and one to collimate the beam. We choose to work with two reflector surfaces as freeform optical surfaces.

Optical design for illumination can roughly be divided into two categories: forward and inverse methods. The former deals with the calculation of the output of an optical system. The result of such a forward method can then be used to iteratively refine the design, which is a slow process [8]. In this paper we will focus on inverse methods. With such methods, the goal is to compute the shape of the optical system given source and target illumination patterns.

Although the example of a laser gives an idea of the possibilities, we will not restrict ourselves to this. In our derivations we will use the approximation of geometrical optics. The goal is to find an optical map from the source to target domain. Combining this map with local energy conservation leads to a Monge-Ampère type equation with transport boundary condition [2]. This formulation can be cast in the framework of optimal transport (OT), identifying the source and target distributions with the densities in OT and the optical map with the transport plan. However, the equivalent of the total transport cost is less obvious. A rigorous formulation of our optical design problem in terms of OT is far from trivial and beyond the scope of this paper.

Several methods have been developed for solving problems similar to the point source and parallel outgoing beam. A more thorough overview of inverse methods can be found in [9]. Some of them use numerical methods such as finite differences and Newton's method to directly solve the Monge-Ampère equation [10,11]. Oliker et al. proposed the supporting quadric method [1,12]. Alternatively, the optimal mass transport problem is reduced to a linear assignment problem by Doskolovich et al. [13]. Another approach by Feng et al. uses ray mapping to calculate the shapes and positions of the surfaces [14]. A ray mapping method has been used to construct optical systems with two freeform surfaces for arbitrary input and output wavefronts [15].

To the best of our knowledge, there are only a few publications on optical system design for collimating and shaping a diverging beam from a point source. In [16], Oliker derives an explicit and detailed form of the Monge-Ampère equation, but he does not discuss a solution method. Glimm shows the equivalence, under certain conditions, of this design problem and an infinite-dimensional linear programming (LP) problem, connected to optimal transport [17]. Later, he and Henscheid proposed a numerical solution method by discretizing the LP problem [18]. Bösel and Gross proposed a method to design a system with two freeform surfaces for arbitrary given input and output wavefronts and irradiance patterns [19,20], which can be used for a point source and collimated output beam as well. Their approach involves calculating the ray mapping and substituting this into the local energy balance. They solve the resulting equations using finite differences.

In this paper we will modify a least-squares method to solve the Monge-Ampère type equation. Versions of this algorithm have been used before for multiple optical design challenges, including parallel to far-field [21], parallel to parallel [22] and point source to far-field [23].

In Section 2 we present the mathematical model linking the shapes of the surfaces to the source and target distributions. The equations in this model are used in the algorithm mentioned before. We will give a short summary of this algorithm in Section 3. For some parts of the algorithm we refer to other papers and we briefly discuss the most important parts. In Section 4 we test our algorithm on two test cases: First a uniform point source and a uniform target, second a laser diode source and a ring-shaped target. The conclusion of our findings is given in Section 5.

2. Formulation of the mathematical model

In this section we formulate the mathematical model of a reflective optical system creating a collimated beam from a point source. Given a source light distribution we want to design an optical system of two reflectors. The first reflector will be used to shape the intensity profile and the second one will collimate the beam. The collimated output beam should give a light distribution on a target plane at a distance l from the source, where the distribution is a given function of the position coordinates in the plane. A two-dimensional illustration of the system is given in Fig. 1.

2.1. Derivation of the cost function

We choose the point source to be located at the origin of a coordinate system given by the standard basis $\hat{e}_1, \hat{e}_2, \hat{e}_3$. The orientation for this coordinate system is arbitrary. Often, the \hat{e}_3 -axis

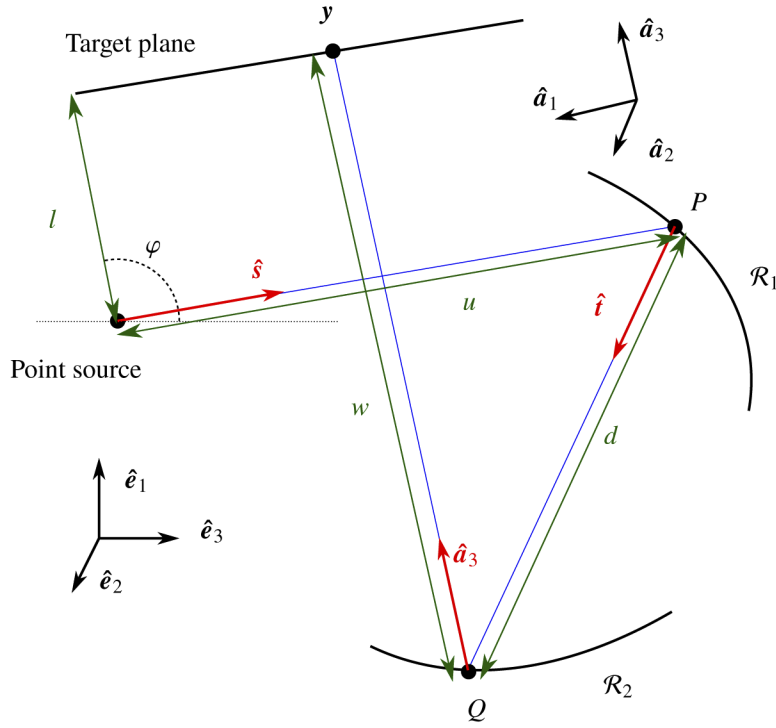


Fig. 1. A sketch of the optical system in the x, z -plane.

is chosen to coincide with the symmetry axis of the bundle of light emitted from the source. However, such a symmetry does not necessarily exist and will not be assumed for our derivations. The only restriction we have on the coordinate system is that there can be no light emitted in the negative \hat{e}_3 -direction. The reason for this will become apparent later. This source emits rays with unit direction vectors $\hat{s} = (s_1, s_2, s_3)^T$. Two reflectors, \mathcal{R}_1 and \mathcal{R}_2 , are used to collimate and shape the light emitted by the source into an output beam with the desired intensity distribution. These output rays should propagate as a parallel beam that is parallel to a given direction vector \hat{a}_3 perpendicular to the target plane. The direction of \hat{a}_3 with respect to $\hat{e}_1, \dots, \hat{e}_3$ is given by a rotation of \hat{e}_3 with a polar angle φ around the \hat{e}_2 -axis and subsequently with an azimuthal angle θ around the \hat{e}_3 -axis. The matrix associated with this composite rotation is given by

$$A = \begin{pmatrix} \cos \varphi \cos \theta & -\sin \theta & \sin \varphi \cos \theta \\ \cos \varphi \sin \theta & \cos \theta & \sin \varphi \sin \theta \\ -\sin \varphi & 0 & \cos \varphi \end{pmatrix}, \quad (1)$$

and we define $\hat{a}_i = A\hat{e}_i$, $i = 1, 2, 3$. These \hat{a}_i -vectors are the rotations of an orthogonal basis, so they are again an orthogonal basis and \hat{a}_i is equal to the i th column of A . The target plane is perpendicular to \hat{a}_3 at a distance l from the point source along \hat{a}_3 . Any point on the target plane is then given by $y_1\hat{a}_1 + y_2\hat{a}_2 + l\hat{a}_3$. The position in the target plane is denoted by $\mathbf{y} = (y_1, y_2)^T$. The first reflector, \mathcal{R}_1 , is defined by the radial distance from the source, $u = u(\hat{s})$. The second reflector, \mathcal{R}_2 , is given by the perpendicular distance from the target plane, $w = w(\mathbf{y})$. The reflectors are then mathematically described by

$$\mathcal{R}_1 : \mathbf{r}_1(\hat{s}) = u(\hat{s})\hat{s}, \quad \mathcal{R}_2 : \mathbf{r}_2(\mathbf{y}) = y_1\hat{a}_1 + y_2\hat{a}_2 + (l - w(\mathbf{y}))\hat{a}_3 = A\mathbf{r}'_2(\mathbf{y}), \quad (2)$$

where $\mathbf{r}'_2(\mathbf{y}) = (y_1, y_2, l - w(\mathbf{y}))^T$. With P and Q we denote the points where a ray hits the first and second reflector, respectively, see Fig. 1. The distance between those two points is denoted by d . In the framework of optimal mass transport we want to derive a relation between $\hat{\mathbf{s}}$ and \mathbf{y} of the form

$$u_1(\hat{\mathbf{s}}) + u_2(\mathbf{y}) = c(\hat{\mathbf{s}}, \mathbf{y}), \quad (3)$$

where u_1 and u_2 are related to the shape and location of the surfaces and c is the so-called cost function [2]. For any ray, we introduce the following notation. The 2-vectors $\mathbf{q}_s = \mathbf{0}$ and $\mathbf{q}_t = \mathbf{y}$ denote the position of the ray at the source and target, respectively. These are projections of 3-dimensional position vectors onto the plane $z = 0$ (source plane) and the target plane, respectively. Similarly, \mathbf{p}_s and $\mathbf{p}_t = \mathbf{0}$ are the projections of the direction vectors on the source and target planes. In terms of Hamiltonian characteristics, the optical path length (OPL), denoted by L , is equal to the point characteristic V [24]. We can write

$$V(\mathbf{q}_s, \mathbf{q}_t) = u(\hat{\mathbf{s}}) + d + w(\mathbf{y}). \quad (4)$$

Because the variables $\hat{\mathbf{s}}$ and \mathbf{y} denote a direction at the source and a position on the target, we work with the second mixed characteristic $W^* = W^*(\mathbf{p}_s, \mathbf{q}_t)$, given by

$$W^*(\mathbf{p}_s, \mathbf{q}_t) = V(\mathbf{q}_s, \mathbf{q}_t) + \mathbf{q}_s \cdot \mathbf{p}_s. \quad (5)$$

However, since $\mathbf{q}_s = \mathbf{0}$ we can dismiss the second term and the mixed characteristic is equal to the optical path length. The following relations can be derived for the mixed characteristic [24]

$$\frac{\partial W^*}{\partial \mathbf{p}_s} = \mathbf{q}_s = \mathbf{0}, \quad \frac{\partial W^*}{\partial \mathbf{q}_t} = \mathbf{p}_t = \mathbf{0}. \quad (6)$$

This proves that W^* is independent of the direction from the source and the position on the target plane. As a result, the optical path length $L = V = W^*$ is a constant.

We will eliminate d from Eq. (4) by using the fact that d is the distance between P and Q . We denote by $\mathbf{r}_P = \mathbf{r}_1(\hat{\mathbf{s}})$ and $\mathbf{r}_Q = \mathbf{r}_2(\mathbf{y})$ the position vectors of P and Q , respectively. Furthermore, we use $\mathbf{r}'_Q = \mathbf{r}'_2(\mathbf{y})$, so we can write

$$\begin{aligned} d^2 &= |\mathbf{r}_Q - \mathbf{r}_P|^2 \\ &= |\mathbf{A}\mathbf{r}'_Q - \mathbf{r}_P|^2 \\ &= |\mathbf{A}\mathbf{r}'_Q|^2 + |\mathbf{r}_P|^2 - 2(\mathbf{A}\mathbf{r}'_Q) \cdot \mathbf{r}_P. \end{aligned} \quad (7)$$

Because \mathbf{A} is a rotation matrix, we have $|\mathbf{A}\mathbf{r}'_Q| = |\mathbf{r}'_Q|$. We also have $\mathbf{r}_P = u\hat{\mathbf{s}}$ and $\mathbf{A} = (\hat{\mathbf{a}}_1, \hat{\mathbf{a}}_2, \hat{\mathbf{a}}_3)$. This can be used to write

$$\begin{aligned} d^2 &= |\mathbf{r}'_Q|^2 + u^2 - 2u(\mathbf{A}\mathbf{r}'_Q) \cdot \hat{\mathbf{s}} \\ &= u^2 + |\mathbf{y}|^2 + (l - w)^2 - 2u(y_1\hat{\mathbf{a}}_1 + y_2\hat{\mathbf{a}}_2 + (l - w)\hat{\mathbf{a}}_3) \cdot \hat{\mathbf{s}} \\ &= u^2 + |\mathbf{y}|^2 + l^2 - 2lw + w^2 - 2u\hat{\mathbf{s}} \cdot (\mathbf{A}_2\mathbf{y}) - 2ul\hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3 + 2uw\hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3, \end{aligned} \quad (8)$$

where $\mathbf{A}_2 = (\hat{\mathbf{a}}_1, \hat{\mathbf{a}}_2) \in \mathbb{R}^{3 \times 2}$ and we omit the dependence of u and w on $\hat{\mathbf{s}}$ and \mathbf{y} for now. We combine Eq. (4) and Eq. (8) to obtain

$$|\mathbf{y}|^2 + l^2 - 2lw - 2u\hat{\mathbf{s}} \cdot (\mathbf{A}_2\mathbf{y}) - 2ul\hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3 + 2uw\hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3 - L^2 + 2Lu + 2Lw - 2uw = 0. \quad (9)$$

We want to separate u and w to get an equation of the form of Eq. (3). For that, we first divide Eq. (9) by u . It is reasonable to assume $u > 0$, since otherwise the reflector coincides with the

source at some point. Introducing $\tilde{u} = 1/u$, Eq. (9) reads

$$|\mathbf{y}|^2\tilde{u} + l^2\tilde{u} - 2l\tilde{u}w - 2\hat{\mathbf{s}} \cdot (\mathbf{A}_2\mathbf{y}) - 2l\hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3 + 2w\hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3 - L^2\tilde{u} + 2L + 2L\tilde{u}w - 2w = 0. \quad (10)$$

The parameter $\beta = L - l$ is introduced, which is called the reduced optical path length. This is used to rewrite the equation above as

$$\tilde{u}w + \tilde{u}\frac{1}{2}\left(\frac{1}{\beta}|\mathbf{y}|^2 - (L + l)\right) - w\frac{1}{\beta}(1 - \hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3) = \frac{\hat{\mathbf{s}} \cdot (\mathbf{A}_2\mathbf{y}) + l\hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3 - L}{\beta}. \quad (11)$$

To obtain an equation of the desired form, we will factorize the equation above and then apply logarithms to both sides of the equation. The factorization leads to

$$\kappa_1(\hat{\mathbf{s}})\kappa_2(\mathbf{y}) = T(\hat{\mathbf{s}}, \mathbf{y}), \quad (12a)$$

$$\kappa_1(\hat{\mathbf{s}}) = \tilde{u} - \frac{1}{\beta}(1 - \hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3), \quad \kappa_2(\mathbf{y}) = w + \frac{1}{2}\left(\frac{|\mathbf{y}|^2}{\beta} - (L + l)\right), \quad (12b)$$

$$T(\hat{\mathbf{s}}, \mathbf{y}) = \frac{1}{\beta}\hat{\mathbf{s}} \cdot \mathbf{A}_2\mathbf{y} - \frac{1 - \hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3}{2\beta^2}|\mathbf{y}|^2 - \frac{1}{2}(\hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3 + 1). \quad (12c)$$

As mentioned, we would like to take the logarithm of both sides of the equation to get to the form of Eq. (3). However, we need to make sure that both sides are positive. We use $L = u + d + w$ and we can write

$$l = u\hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3 + d\hat{\mathbf{t}} \cdot \hat{\mathbf{a}}_3 + w, \quad (13)$$

where $\hat{\mathbf{t}}$ is the (unit) direction vector after the first reflection. Combining both relations, we obtain $\beta = (1 - \hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3)u + (1 - \hat{\mathbf{t}} \cdot \hat{\mathbf{a}}_3)d$. Since $\hat{\mathbf{t}}$ is a unit direction vector, we know that $\beta \geq (1 - \hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3)u \geq 0$, with the first equality only if $\hat{\mathbf{t}} \cdot \hat{\mathbf{a}}_3 = 1$. In that case $\hat{\mathbf{t}}$ is parallel to $\hat{\mathbf{a}}_3$, so there would be no second reflection. We can disregard this case and therefore write

$$\kappa_1 = \frac{1}{u} - \frac{1 - \hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3}{\beta} > \frac{1}{u} - \frac{1 - \hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3}{(1 - \hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3)u} = 0. \quad (14)$$

The vector \mathbf{y} is the displacement along the plane spanned by $\hat{\mathbf{a}}_1$ and $\hat{\mathbf{a}}_2$. We have $y_1\hat{\mathbf{a}}_1 + y_2\hat{\mathbf{a}}_2 = \mathbf{A}_2\mathbf{y}$. This displacement is determined completely by the first two ray segments; from the source to the first reflector, and from the first to the second reflector. Using this, we write

$$y_1 = u\hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_1 + d\hat{\mathbf{t}} \cdot \hat{\mathbf{a}}_1, \quad y_2 = u\hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_2 + d\hat{\mathbf{t}} \cdot \hat{\mathbf{a}}_2. \quad (15)$$

Substituting this into the expression for κ_2 and using Eq. (4) and Eq. (13) gives us

$$2\beta\kappa_2 = 2\beta w + (u\hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_1 + d\hat{\mathbf{t}} \cdot \hat{\mathbf{a}}_1)^2 + (u\hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_2 + d\hat{\mathbf{t}} \cdot \hat{\mathbf{a}}_2)^2 - \beta((1 + \hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3)u + (1 + \hat{\mathbf{t}} \cdot \hat{\mathbf{a}}_3)d + 2w). \quad (16)$$

We now use again that $\beta = (1 - \hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3)u + (1 - \hat{\mathbf{t}} \cdot \hat{\mathbf{a}}_3)d$ to obtain

$$\begin{aligned} 2\beta\kappa_2 &= (u\hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_1 + d\hat{\mathbf{t}} \cdot \hat{\mathbf{a}}_1)^2 + (u\hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_2 + d\hat{\mathbf{t}} \cdot \hat{\mathbf{a}}_2)^2 \\ &\quad - ((1 - \hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3)u + (1 - \hat{\mathbf{t}} \cdot \hat{\mathbf{a}}_3)d)((1 + \hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3)u + (1 + \hat{\mathbf{t}} \cdot \hat{\mathbf{a}}_3)d) \\ &= u^2\left(-1 + \sum_{i=1}^3(\hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_i)^2\right) + d^2\left(-1 + \sum_{i=1}^3(\hat{\mathbf{t}} \cdot \hat{\mathbf{a}}_i)^2\right) - ud\left(2 - 2\sum_{i=1}^3(\hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_i)(\hat{\mathbf{t}} \cdot \hat{\mathbf{a}}_i)\right). \end{aligned} \quad (17)$$

Note that we can combine the $\hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_i$ terms into a vector written as

$$\begin{pmatrix} \hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_1 \\ \hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_2 \\ \hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3 \end{pmatrix} = \mathbf{A}^T \hat{\mathbf{s}}. \quad (18)$$

This vector can be used to eliminate the u^2 term, since

$$\sum_{i=1}^3 (\hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_i)^2 = |\mathbf{A}^T \hat{\mathbf{s}}|^2 = |\hat{\mathbf{s}}|^2 = 1, \quad (19)$$

as \mathbf{A} is a rotation matrix and therefore $\mathbf{A}\mathbf{A}^T = \mathbf{I}$. Similarly, swapping $\hat{\mathbf{t}}$ for $\hat{\mathbf{s}}$ gives us $\sum_{i=1}^3 (\hat{\mathbf{t}} \cdot \hat{\mathbf{a}}_i)^2 = 1$. We use this to rewrite

$$\begin{aligned} 2\beta\kappa_2 &= -2ud \left(1 - \sum_{i=1}^3 (\hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_i)(\hat{\mathbf{t}} \cdot \hat{\mathbf{a}}_i) \right) \\ &= -2ud \left(1 - (\mathbf{A}^T \hat{\mathbf{s}}) \cdot (\mathbf{A}^T \hat{\mathbf{t}}) \right) \\ &= -2ud (1 - \hat{\mathbf{s}} \cdot \hat{\mathbf{t}}) \\ &\leq 0, \end{aligned} \quad (20)$$

with equality if and only if $\hat{\mathbf{t}} = \hat{\mathbf{s}}$. This will not occur, since there would be no reflection at the first surface in that case. We deduced that $\kappa_1 > 0$ and $\kappa_2 < 0$. Consequently, T must be negative as well. Both sides of Eq. (12a) are therefore multiplied by -1 to obtain

$$\kappa_1(\hat{\mathbf{s}})(-\kappa_2(\mathbf{y})) = -T(\hat{\mathbf{s}}, \mathbf{y}). \quad (21)$$

Before we apply the logarithm to this equation, we scale all the lengths by a factor β . Note that $\hat{\mathbf{s}}$ is already dimensionless. We introduce the variable z such that $\mathbf{y} = \beta z$. We substitute this into the function $-T(\hat{\mathbf{s}}, \mathbf{y}) = \hat{T}(\hat{\mathbf{s}}, z)$ and obtain

$$\hat{T}(\hat{\mathbf{s}}, z) = -\hat{\mathbf{s}} \cdot \mathbf{A}_2 z + \frac{1}{2} (1 - \hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3) |z|^2 + \frac{1}{2} (\hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3 + 1). \quad (22)$$

Next, we scale all the other lengths, viz. $w(\mathbf{y}) = \beta \hat{w}(z)$, $L = \beta \hat{L}$ and $l = \beta \hat{l}$. Furthermore, \tilde{u} has the dimension of length inverse, so we scale this by $1/\beta$ to $\tilde{u}(\hat{\mathbf{s}}) = (1/\beta)\hat{u}(\mathbf{x})$. Substituting this in the expressions for κ_1 and κ_2 gives

$$\kappa_1(\hat{\mathbf{s}}) = \frac{1}{\beta} (\hat{u}(\mathbf{x}) + \hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3 - 1), \quad (23a)$$

$$\kappa_2(\mathbf{y}) = \beta \left(\hat{w}(z) + \frac{1}{2} (|z|^2 - (\hat{L} + \hat{l})) \right). \quad (23b)$$

So we can now define the new functions $\hat{\kappa}_1$ and $\hat{\kappa}_2$ by

$$\hat{\kappa}_1(\hat{\mathbf{s}}) = \hat{u}(\hat{\mathbf{s}}) + \hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3 - 1, \quad (24a)$$

$$\hat{\kappa}_2(z) = \hat{w}(z) + \frac{1}{2} (|z|^2 - (\hat{L} + \hat{l})), \quad (24b)$$

and $\kappa_1 \kappa_2 = \hat{\kappa}_1 \hat{\kappa}_2$. Now Eq. (21) becomes

$$\hat{\kappa}_1(\hat{\mathbf{s}}) (-\hat{\kappa}_2(z)) = \hat{T}(\hat{\mathbf{s}}, z). \quad (25)$$

For the algorithm that will be introduced in Section 3., we want to change the source coordinates into two independent variables instead of three variables on the unit sphere. For that we choose

the stereographic projection from the south pole $(0, 0, -1)$ onto the equator plane $z = 0$, written as \mathbf{x} . These coordinates are given by

$$\mathbf{x} = \begin{pmatrix} x_1 \\ x_2 \end{pmatrix} = \frac{1}{1 + s_3} \begin{pmatrix} s_1 \\ s_2 \end{pmatrix}, \quad \hat{\mathbf{s}} = \begin{pmatrix} s_1 \\ s_2 \\ s_3 \end{pmatrix} = \frac{1}{|\mathbf{x}|^2 + 1} \begin{pmatrix} 2x_1 \\ 2x_2 \\ 1 - |\mathbf{x}|^2 \end{pmatrix}. \quad (26)$$

Furthermore, we introduce

$$u_1(\mathbf{x}) = \log(\hat{\kappa}_1(\hat{\mathbf{s}}(\mathbf{x}))), \quad (27a)$$

$$u_2(\mathbf{z}) = \log(-\hat{\kappa}_2(\mathbf{z})). \quad (27b)$$

When we take the logarithm of both sides of Eq. (25), taking into account the functions we just introduced, we get the desired form of Eq. (3), given by

$$u_1(\mathbf{x}) + u_2(\mathbf{z}) = c(\mathbf{x}, \mathbf{z}), \quad (28)$$

where the function c is called the cost function and is defined as

$$\begin{aligned} c(\mathbf{x}, \mathbf{z}) &= \log(\hat{T}(\hat{\mathbf{s}}(\mathbf{x}), \mathbf{z})) \\ &= \log\left[-\hat{\mathbf{s}}(\mathbf{x}) \cdot \mathbf{A}_2 \mathbf{z} + \frac{1}{2}(1 - \hat{\mathbf{s}}(\mathbf{x}) \cdot \hat{\mathbf{a}}_3)|z|^2 + \frac{1}{2}(\hat{\mathbf{s}}(\mathbf{x}) \cdot \hat{\mathbf{a}}_3 + 1)\right]. \end{aligned} \quad (29)$$

2.2. Energy conservation

We have deduced an equation that implicitly links \mathbf{x} and \mathbf{z} . We assume that there exists an explicit relation given by $\mathbf{z} = \mathbf{m}(\mathbf{x})$. A constraint for this function is that the energy of the source should be conserved through the optical system. By $\mathcal{S} \subset S^2$, with S^2 the unit sphere, we denote the set of direction vectors $\hat{\mathbf{s}}$ from the source. For the stereographic projection \mathbf{x} of this set we use $\mathcal{X} \subset \mathbb{R}^2$. The energy density of the source is given by $f = f(\hat{\mathbf{s}})$. We write $\mathcal{T} \subset \mathbb{R}^2$ for the set of target positions \mathbf{y} and $\mathcal{Z} \subset \mathbb{R}^2$ for the set of scaled target variables \mathbf{z} . The desired illuminance on the target plane is then given by $g = g(\mathbf{y})$ for $\mathbf{y} \in \mathcal{T}$. The energy of any subset of the source domain should be conserved through the optical system. For any subset $\tilde{\mathcal{A}} \subset \mathcal{S}$ there is a corresponding set \mathcal{A} of stereographic coordinates. Energy conservation is given by the equation

$$\iint_{\tilde{\mathcal{A}}} f(\hat{\mathbf{s}}) dS(\hat{\mathbf{s}}) = \iint_{\beta\mathbf{m}(\mathcal{A})} g(\mathbf{y}) dA(\mathbf{y}), \quad (30)$$

where $\mathbf{y} = \beta\mathbf{z}$. The first integral is over a surface element on the unit sphere, while the second one is over an area element in \mathbb{R}^2 . When $\mathcal{A} = \mathcal{S}$ we have the special case of global energy conservation. This means that the total energy in the source and target should be equal. We assume that f and g are constructed such that this is true. First, we want to transform the left-hand side integral to an integral over \mathbf{x} instead of $\hat{\mathbf{s}}$. From integration by substitution we have

$$\iint_{\tilde{\mathcal{A}}} f(\hat{\mathbf{s}}) dS(\hat{\mathbf{s}}) = \iint_{\mathcal{A}} f(\hat{\mathbf{s}}(\mathbf{x})) \left| \frac{\partial \hat{\mathbf{s}}}{\partial x_1} \times \frac{\partial \hat{\mathbf{s}}}{\partial x_2} \right| dA(\mathbf{x}) = \iint_{\mathcal{A}} f(\hat{\mathbf{s}}(\mathbf{x})) \frac{4}{(|\mathbf{x}|^2 + 1)^2} dA(\mathbf{x}). \quad (31)$$

Now, for the right-hand side of Eq. (30) we also want to transform the integration variable to \mathbf{x} . For that we first have to change from \mathbf{y} to \mathbf{z} , since we know $\mathbf{z} = \mathbf{m}(\mathbf{x})$. We had defined $\mathbf{y} = \beta\mathbf{z}$, so the Jacobi matrix of this transformation is given by β^2 . Substituting this and Eq. (31) into Eq. (30) gives

$$\iint_{\mathcal{A}} f(\hat{\mathbf{s}}(\mathbf{x})) \frac{4}{(|\mathbf{x}|^2 + 1)^2} dA(\mathbf{x}) = \iint_{\mathcal{A}} g(\beta \mathbf{m}(\mathbf{x})) \beta^2 |\det(\mathbf{D}\mathbf{m})| dA(\mathbf{x}). \quad (32)$$

We use $\mathbf{D}\mathbf{m}$ to denote the Jacobi matrix of \mathbf{m} . This equation should hold for any \mathcal{A} corresponding to an $\tilde{\mathcal{A}} \subset \mathcal{S}$. Therefore the integrands should be equal almost everywhere. Then for any $\mathbf{x}(\hat{\mathbf{s}})$ with $\hat{\mathbf{s}} \in \mathcal{S}$ we have the generalized Monge-Ampère equation

$$|\det(\mathbf{D}\mathbf{m})| = \frac{4}{\beta^2(|\mathbf{x}|^2 + 1)^2} \frac{f(\hat{\mathbf{s}}(\mathbf{x}))}{g(\beta \mathbf{m}(\mathbf{x}))} =: F(\mathbf{x}, \mathbf{m}(\mathbf{x}); \beta). \quad (33a)$$

The boundary condition of the problem is a transport boundary condition given by

$$\partial \mathcal{Z} = \mathbf{m}(\partial \mathcal{X}). \quad (33b)$$

It states that the boundary of the source domain should be mapped to the boundary of the target domain, which is a result of the edge-ray principle [25]. This holds under the assumption that our reflector surfaces are smooth. For the remainder of this article we will assume that $\det(\mathbf{D}\mathbf{m}) > 0$, so we can ignore the absolute value in Eq. (33a).

2.3. Polar coordinates

In general, the rays will be emitted by the source in a conical bundle symmetric around the z -axis. In that case, the source domain in stereographic coordinates, \mathcal{X} , will be a circle. So, it makes sense to switch to the polar coordinate system. The polar stereographic coordinates are written as $\omega = (\rho, \zeta)$ and the transformation $\mathbf{x} = \mathbf{x}(\omega)$ is given by

$$x_1 = \rho \cos \zeta, \quad x_2 = \rho \sin \zeta. \quad (34)$$

We define Ω to be the source domain in polar stereographic coordinates, so $\Omega = \omega(\mathcal{X})$. Furthermore we define $u_1^*(\omega) = u_1(\mathbf{x}(\omega))$ and $c^*(\omega, \mathbf{z}) = c(\mathbf{x}(\omega), \mathbf{z})$, so Eq. (28) changes to

$$u_1^*(\omega) + u_2(\mathbf{z}) = c^*(\omega, \mathbf{z}). \quad (35)$$

We also need to transform the energy conservation equation to polar coordinates. With integration by substitution, we change Eq. (32) to

$$\iint_{\omega(\mathcal{A})} f(\hat{\mathbf{s}}(\omega)) \frac{4}{(\rho^2 + 1)^2} \rho d\omega = \iint_{\omega(\mathcal{A})} g(\beta \mathbf{m}^*(\omega)) \beta^2 \det(\mathbf{D}\mathbf{m}^*) \rho d\omega, \quad (36)$$

where $d\omega = \rho d\rho d\zeta$. We introduce the notation $\mathbf{m}^*(\omega) = \mathbf{m}(\mathbf{x}(\omega))$, implying $\mathbf{z} = \mathbf{m}^*(\omega)$. Note that Eq. (36) should hold for \mathcal{A} corresponding to any arbitrary part of the source domain, so for any $\omega \in \Omega$ we have

$$\det(\mathbf{D}\mathbf{m}^*) = \frac{4}{\beta^2(\rho^2 + 1)^2} \frac{f(\hat{\mathbf{s}}(\omega))}{g(\beta \mathbf{m}^*(\omega))} := F^*(\omega, \mathbf{m}^*(\omega)). \quad (37a)$$

The matrix $\mathbf{D}\mathbf{m}^*$ is the Jacobian of \mathbf{m} expressed in polar coordinates and is given by

$$\mathbf{D}\mathbf{m}^* = \begin{pmatrix} \frac{\partial m_1}{\partial \rho} & \frac{1}{\rho} \frac{\partial m_1}{\partial \zeta} \\ \frac{\partial m_2}{\partial \rho} & \frac{1}{\rho} \frac{\partial m_2}{\partial \zeta} \end{pmatrix}. \quad (37b)$$

This follows from a coordinate transformation of the Jacobian with Cartesian coordinates in Section 2.2. The boundary condition (33b) changes to

$$\partial \mathcal{Z} = \mathbf{m}^*(\omega)(\partial \mathcal{X}). \quad (37c)$$

Note that we have $\Omega = \omega(\mathcal{X})$, but $\partial \Omega \neq \omega(\partial \mathcal{X})$. For example, the relation $\rho = 0$ would give a point in the interior of \mathcal{X} , but a line on the boundary of Ω . In the remainder of this article we will omit the asterisks, because we will only work with functions of ω .

2.4. Mapping

We want to find an (implicit) expression for the optical mapping $\mathbf{z} = \mathbf{m}(\omega)$. This can be done using Eq. (35). There are many solutions to solve this equation for \mathbf{m} , so we make a special choice [2]. It is possible to find a c -convex pair of functions u_1, u_2 such that

$$u_1(\omega) = \max_{\mathbf{z} \in \mathcal{Z}} (c(\omega, \mathbf{z}) - u_2(\mathbf{z})), \quad u_2(\mathbf{z}) = \max_{\omega \in \Omega} (c(\omega, \mathbf{z}) - u_1(\omega)). \quad (38)$$

Conversely it is possible to find a c -concave pair defined by

$$u_1(\omega) = \min_{\mathbf{z} \in \mathcal{Z}} (c(\omega, \mathbf{z}) - u_2(\mathbf{z})), \quad u_2(\mathbf{z}) = \min_{\omega \in \Omega} (c(\omega, \mathbf{z}) - u_1(\omega)). \quad (39)$$

In either case, the solution for u_2 has an argument $\hat{\omega}$ that is a stationary point. This leads to the requirement that

$$\nabla_{\omega} c(\hat{\omega}, \mathbf{z}) - \nabla_{\omega} u_1(\hat{\omega}) = \mathbf{0}. \quad (40)$$

The gradient with respect to ω is given by

$$\nabla_{\omega} = \mathbf{e}_{\rho} \frac{\partial}{\partial \rho} + \frac{1}{\rho} \mathbf{e}_{\zeta} \frac{\partial}{\partial \zeta}. \quad (41)$$

To ensure that the solution is a maximum we need the Hessian w.r.t. ω of $c(\omega, \mathbf{z}) - u_1(\omega)$ to be symmetric negative definite (SND). Similarly, to ensure a minimum we require the Hessian to be symmetric positive definite (SPD). The Hessian matrix of any function v in polar coordinates is given by [26]

$$H[v] = \begin{pmatrix} \frac{\partial^2 v}{\partial \rho^2} & \frac{1}{\rho} \frac{\partial^2 v}{\partial \rho \partial \zeta} - \frac{1}{\rho^2} \frac{\partial v}{\partial \zeta} \\ \frac{1}{\rho} \frac{\partial^2 v}{\partial \rho \partial \zeta} - \frac{1}{\rho^2} \frac{\partial v}{\partial \zeta} & \frac{1}{\rho^2} \frac{\partial^2 v}{\partial \zeta^2} + \frac{1}{\rho} \frac{\partial v}{\partial \rho} \end{pmatrix}. \quad (42)$$

In the Hessian of the function $c(\omega, \mathbf{z}) - u_1(\omega)$ the first derivative terms cancel because of Eq. (40), so this Hessian is given by

$$H [c(\omega, \mathbf{z}) - u_1(\omega)] = D_{\omega\omega} c(\omega, \mathbf{z}) - D_{\omega\omega} u_1(\omega), \quad (43)$$

with

$$D_{\omega\omega} = \begin{pmatrix} \frac{\partial^2}{\partial \rho^2} & \frac{1}{\rho} \frac{\partial^2}{\partial \rho \partial \zeta} \\ \frac{1}{\rho} \frac{\partial^2}{\partial \zeta \partial \rho} & \frac{1}{\rho^2} \frac{\partial^2}{\partial \zeta^2} \end{pmatrix}. \quad (44)$$

Note that $D_{\omega\omega} v$ is not equal to the Hessian matrix of v . We assume that a mapping $\mathbf{z} = \mathbf{m}(\omega)$ exists, and substitute this into Eq. (40). We then take the derivative with respect to ω and apply the chain rule to obtain

$$D_{\omega\omega} c + \mathbf{C} D\mathbf{m} = D^2 u_1, \quad (45a)$$

where

$$\mathbf{C} = D_{\omega\mathbf{z}} c = \begin{pmatrix} \frac{\partial^2 c}{\partial \rho \partial z_1} & \frac{\partial^2 c}{\partial \rho \partial z_2} \\ \frac{1}{\rho} \frac{\partial^2 c}{\partial \zeta \partial z_1} & \frac{1}{\rho} \frac{\partial^2 c}{\partial \zeta \partial z_2} \end{pmatrix}. \quad (45b)$$

Note that the first term in Eq. (45a) means differentiating $c(\omega, \mathbf{z})$ w.r.t. ω twice and then substituting $\mathbf{z} = \mathbf{m}(\omega)$. We can rewrite Eq. (45a) to

$$\mathbf{C} D\mathbf{m} = D_{\omega\omega} u_1 - D_{\omega\omega} c =: \mathbf{P}. \quad (46)$$

Note that $-\mathbf{P}$ is the Hessian matrix in Eq. (43). Therefore, for a c -convex or c -concave pair of functions u_1, u_2 , we have the condition that \mathbf{P} should be SPD or SND, respectively. We assumed

that a mapping \mathbf{m} is defined (implicitly) by Eq. (40). By the implicit function theorem such a mapping is guaranteed to exist if the Jacobian matrix of the left-hand side of the equation with respect to \mathbf{z} is invertible [27, Sec. 12.8].

To summarize, we need to find a mapping \mathbf{m} satisfying Eq. (37c) and Eq. (46) for a matrix \mathbf{P} that is SPD or SND, with $\det(\mathbf{P}) = F \det(\mathbf{C})$. The exact mapping is determined by the parameters l and β (or L) and the direction of the outgoing beam, given by φ and θ .

3. Numerical method

We explain the least-squares algorithm which we use to solve the problem derived in the previous section. This algorithm has been explained thoroughly for a source with Cartesian [2,21] and polar [9] coordinates. In this section we give a brief overview. We first compute the mapping, followed by a calculation of the surfaces. We restrict ourselves to the c -convex solution of Eq. (35). As shown in the previous section, we need to solve

$$\mathbf{C}(\omega, \mathbf{m}(\omega)) \mathbf{D}\mathbf{m}(\omega) = \mathbf{P}(\omega), \quad (47)$$

where $\mathbf{C} = \mathbf{D}_{\omega\mathbf{z}}\mathbf{c}$ and \mathbf{P} satisfies $\det(\mathbf{P}) = F \det(\mathbf{C})$, see Eq. (37a). To get the c -convex solution, \mathbf{P} needs to be SPD. We enforce the equality in Eq. (47) by minimizing the functional J_1 defined by

$$J_1[\mathbf{m}, \mathbf{P}] = \frac{1}{2} \iint_{\Omega} \|\mathbf{C}\mathbf{D}\mathbf{m} - \mathbf{P}\|_{\mathbb{F}}^2 d\omega. \quad (48)$$

The norm $\|\cdot\|_{\mathbb{F}}$ is the Frobenius norm. To enforce the boundary condition we minimize the difference between the (given) boundary of \mathcal{T} and the mapping of the boundary of the source:

$$J_B[\mathbf{m}, \mathbf{b}] = \frac{1}{2} \int_{\omega(\partial\mathcal{X})} |\mathbf{m} - \mathbf{b}|^2 ds, \quad (49)$$

where $\mathbf{b} \in \partial\mathcal{Z}$. We combine these two functionals into a weighted average with parameter $\alpha \in [0, 1]$ given by

$$J[\mathbf{m}, \mathbf{P}, \mathbf{b}] = \alpha J_1[\mathbf{m}, \mathbf{P}] + (1 - \alpha) J_B[\mathbf{m}, \mathbf{b}]. \quad (50)$$

All of these functionals are defined on the following spaces

$$\mathcal{P}(\mathbf{m}) = \{\mathbf{P} \in [C^1(\Omega)]^{2 \times 2} \mid \det(\mathbf{P}) = F \det(\mathbf{C}), \mathbf{P} \text{ SPD}\}, \quad (51a)$$

$$\mathcal{B} = \{\mathbf{b} \in [C^1(\omega(\partial\mathcal{X}))]^2 \mid \mathbf{b}(\omega) \in \partial\mathcal{Z}\}, \quad (51b)$$

$$\mathcal{M} = [C^2(\Omega)]^2. \quad (51c)$$

We cover the domain Ω by a grid with gridpoints ω_{ij} . The algorithm to find \mathbf{m} is initialized by a guess \mathbf{m}^0 for the mapping. With this mapping we compute the matrix \mathbf{C}^0 . Then, we iteratively perform the next steps either for a fixed number of iterations or until a stopping criterion is met,

$$\mathbf{b}^{n+1} = \operatorname{argmin}_{\mathbf{b} \in \mathcal{B}} J_B[\mathbf{m}^n, \mathbf{b}], \quad (52a)$$

$$\mathbf{P}^{n+1} = \operatorname{argmin}_{\mathbf{P} \in \mathcal{P}(\mathbf{m}^n)} J_1[\mathbf{m}^n, \mathbf{P}], \quad (52b)$$

$$\mathbf{m}^{n+1} = \operatorname{argmin}_{\mathbf{m} \in \mathcal{M}} J[\mathbf{m}, \mathbf{P}^{n+1}, \mathbf{b}^{n+1}], \quad (52c)$$

$$\mathbf{C}^{n+1} = \mathbf{C}(\omega, \mathbf{m}^{n+1}). \quad (52d)$$

The minimization procedures for \mathbf{b} and \mathbf{P} do not contain derivatives of their respective variables, so these can be minimized pointwise.

A method for solving step (52a) is given by Romijn et al. [23]. We will explain step (52b) in a bit more detail. The matrix \mathbf{P} needs to be SPD. The symmetry of \mathbf{P} is enforced by defining

$$\mathbf{P} = \begin{pmatrix} p_{11} & p_{12} \\ p_{12} & p_{22} \end{pmatrix}. \tag{53}$$

We approximate \mathbf{Dm} using central differences and define $\mathbf{Q} = \mathbf{CDm}$. Instead of minimizing $\|\mathbf{Q} - \mathbf{P}\|_F$ we solve an equivalent problem with the same minimizers [21]. We introduce the symmetric matrix $\mathbf{Q}_S = \frac{1}{2}(\mathbf{Q} + \mathbf{Q}^T)$, with off-diagonal entries $q_S = \frac{1}{2}(q_{12} + q_{21})$. The optimization problem that needs to be solved is then

$$\begin{aligned} \text{minimize} \quad & H_S(p_{11}, p_{22}, p_{12}) = \frac{1}{2} \|\mathbf{Q}_S - \mathbf{P}\|_F^2, \\ \text{subject to} \quad & \det(\mathbf{P}) = F \det(\mathbf{C}). \end{aligned} \tag{54}$$

It turns out that we can always select at least one solution of this problem that satisfies the constraint that \mathbf{P} is SPD [2]. To solve problem (54) we use the Lagrange multiplier method. We introduce the Lagrangian function

$$\Lambda(p_{11}, p_{22}, p_{12}, \lambda) = H_S(p_{11}, p_{22}, p_{12}) + \lambda (p_{11}p_{22} - p_{12}^2 - F \det(\mathbf{C})). \tag{55}$$

To find stationary points we take the derivatives w.r.t. each variable and set them equal to zero. Elementary calculation lead us then to the system of equations

$$p_{11} + \lambda p_{22} = q_{11}, \tag{56a}$$

$$\lambda p_{11} + p_{22} = q_{22}, \tag{56b}$$

$$(1 - \lambda)p_{12} = q_S, \tag{56c}$$

$$p_{11}p_{22} - p_{12}^2 = F \det(\mathbf{C}). \tag{56d}$$

Solutions of this system can be calculated analytically and explicitly [2]. In the case that we find multiple solutions, we have to choose the one that gives the lowest value for H_S .

3.1. Computing the mapping

In the functional J there are derivatives of \mathbf{m} , so we can no longer optimize pointwise. To be able to minimize this functional, we apply calculus of variations. The first variation of \mathbf{m} in the direction of an arbitrary function $\boldsymbol{\eta} = (\eta_1, \eta_2)^T \in \mathcal{M}$ is given by

$$\begin{aligned} \delta J[\mathbf{m}, \mathbf{P}, \mathbf{b}](\boldsymbol{\eta}) &= \lim_{\varepsilon \rightarrow 0} \frac{1}{\varepsilon} \left(J[\mathbf{m} + \varepsilon \boldsymbol{\eta}, \mathbf{P}, \mathbf{b}] - J[\mathbf{m}, \mathbf{P}, \mathbf{b}] \right) \\ &= \lim_{\varepsilon \rightarrow 0} \frac{1}{\varepsilon} \left(\frac{\alpha}{2} \iint_{\Omega} \|\mathbf{CDm} + \varepsilon \mathbf{CD}\boldsymbol{\eta} - \mathbf{P}\|_F^2 \rho \, d\omega + \frac{1-\alpha}{2} \int_{\omega(\partial\mathcal{X})} |\mathbf{m} + \varepsilon \boldsymbol{\eta} - \mathbf{b}|^2 \, ds \right. \\ &\quad \left. - \frac{\alpha}{2} \iint_{\Omega} \|\mathbf{CDm} - \mathbf{P}\|_F^2 \rho \, d\omega - \frac{1-\alpha}{2} \int_{\omega(\partial\mathcal{X})} |\mathbf{m} - \mathbf{b}|^2 \, ds \right) \\ &= \lim_{\varepsilon \rightarrow 0} \frac{1}{\varepsilon} \left(\alpha \iint_{\Omega} \varepsilon \rho (\mathbf{CDm} - \mathbf{P}) : \mathbf{CD}\boldsymbol{\eta} + \frac{\varepsilon^2}{2} \rho \|\mathbf{CD}\boldsymbol{\eta}\|_F^2 \, d\omega \right. \\ &\quad \left. + (1-\alpha) \int_{\omega(\partial\mathcal{X})} \varepsilon (\mathbf{m} - \mathbf{b}) \cdot \boldsymbol{\eta} + \frac{\varepsilon^2}{2} |\boldsymbol{\eta}|^2 \, ds \right) \\ &= \alpha \iint_{\Omega} (\mathbf{CDm} - \mathbf{P}) : \mathbf{CD}\boldsymbol{\eta} \rho \, d\omega + (1-\alpha) \int_{\omega(\partial\mathcal{X})} (\mathbf{m} - \mathbf{b}) \cdot \boldsymbol{\eta} \, ds, \end{aligned} \tag{57}$$

where $:$ denotes the Frobenius inner product associated with the Frobenius norm $\|\cdot\|_F$. Like before, $\mathbf{D}\boldsymbol{\eta}$ denotes the Jacobian of $\boldsymbol{\eta}$ w.r.t. ω . We can rewrite the inner product in the first

integral to obtain

$$(\mathbf{CDm} - \mathbf{P}) : \mathbf{CD}\eta = \mathbf{w}_1 \cdot \nabla\eta_1 + \mathbf{w}_2 \cdot \nabla\eta_2, \quad (58)$$

where \mathbf{w}_1 and \mathbf{w}_2 are defined by

$$\begin{bmatrix} \mathbf{w}_1^T \\ \mathbf{w}_2^T \end{bmatrix} = \mathbf{C}^T(\mathbf{CDm} - \mathbf{P}). \quad (59)$$

We use this and Gauss's divergence theorem to rewrite the integral over Ω as

$$\begin{aligned} \iint_{\Omega} (\mathbf{CDm} - \mathbf{P}) : \mathbf{CD}\eta \rho \, d\omega &= \sum_{k=1}^2 \iint_{\Omega} \mathbf{w}_k \cdot \nabla\eta_k \rho \, d\omega \\ &= \sum_{k=1}^2 \left[\oint_{\omega(\partial\mathcal{X})} \eta_k \mathbf{w}_k \cdot \hat{\mathbf{n}} \, ds - \iint_{\Omega} \eta_k \operatorname{div}(\mathbf{w}_k) \rho \, d\omega \right], \end{aligned} \quad (60)$$

where $\hat{\mathbf{n}}$ is the outward unit normal of \mathcal{X} . We substitute this into Eq. (57) and set the first variation equal to zero to obtain

$$\sum_{k=1}^2 \left[\oint_{\omega(\partial\mathcal{X})} \eta_k (\alpha \mathbf{w}_k \cdot \hat{\mathbf{n}} + (1 - \alpha)(m_k - b_k)) \, ds - \iint_{\Omega} \alpha \eta_k \operatorname{div}(\mathbf{w}_k) \rho \, d\omega \right] = 0. \quad (61)$$

At a minimum of J , the first variation should be equal to zero for any vector η . We can split this in two cases. First we choose $\eta_2 = 0$ and set the first variation equal to zero for any $\eta_1 \in C^2(\Omega)$. Similarly, we have the case where $\eta_1 = 0$. With the use of the fundamental lemma of calculus of variations [28] we get the boundary value problem

$$\operatorname{div}(\mathbf{C}^T \mathbf{CDm}) = \operatorname{div}(\mathbf{C}^T \mathbf{P}), \quad \text{for } \omega \in \Omega, \quad (62a)$$

$$\alpha \mathbf{C}^T \mathbf{C}(\mathbf{Dm})\hat{\mathbf{n}} + (1 - \alpha)\mathbf{m} = \alpha \mathbf{C}^T \mathbf{P}\hat{\mathbf{n}} + (1 - \alpha)\mathbf{b}, \quad \text{for } \omega \in \omega(\partial\mathcal{X}), \quad (62b)$$

where div is defined in the following way. Let $\mathbf{B} = (b_{ij}) \in \mathbb{R}^{2 \times 2}$, then

$$\operatorname{div}(\mathbf{B}) = \frac{1}{\rho} \left(\frac{\partial}{\partial \rho} (\rho b_{11}) + \frac{\partial b_{12}}{\partial \zeta} \right) \mathbf{e}_1 + \frac{1}{\rho} \left(\frac{\partial}{\partial \rho} (\rho b_{21}) + \frac{\partial b_{22}}{\partial \zeta} \right) \mathbf{e}_2. \quad (63)$$

This boundary value problem is then solved using the finite volume method [9, Appendix A].

3.2. Computation of the reflector surfaces

The algorithm (52) computes a mapping \mathbf{m} . From this mapping we can compute the shape of the surfaces, given by u and w . To find u we first compute u_1 from Eq. (40). We introduce the functional I to quantify how close a function ϕ is to the exact solution of that equation. Our solution u_1 is then given by

$$u_1 = \arg \min_{\phi} I[\phi], \quad (64)$$

where

$$I[\phi] = \frac{1}{2} \iint_{\Omega} |\nabla\phi - \nabla_{\omega} c(\cdot, \mathbf{m})|^2 \rho \, d\omega. \quad (65)$$

To solve this optimization problem we use calculus of variations. The first variation of (65) is

$$\delta I[u_1](v) = \frac{1}{2} \iint_{\Omega} (\nabla u_1 - \nabla_{\omega} c) \cdot \nabla v \rho \, d\omega, \quad (66)$$

analogous to Eq. (57). Similar to the calculation of the mapping, we use Gauss’s divergence theorem and the fundamental lemma of calculus of variations to get the boundary value problem

$$\Delta u_1 = \text{div}(\nabla_{\omega} c), \quad \omega \in \Omega \tag{67a}$$

$$\frac{\partial u_1}{\partial \rho} = \frac{\partial c(\cdot, \mathbf{z})}{\partial \rho} \Big|_{z=m(\omega)}, \quad \omega \in \omega(\partial \mathcal{X}). \tag{67b}$$

Here, Δ denotes the Laplace operator, which in polar coordinates is given by

$$\Delta u_1 = \text{div}(\nabla u_1) = \frac{1}{\rho} \frac{\partial}{\partial \rho} \left(\rho \frac{\partial u_1}{\partial \rho} \right) + \frac{1}{\rho^2} \frac{\partial^2 u_1}{\partial \zeta^2}. \tag{68}$$

Let u_1 be a solution to this boundary value problem. To calculate the shapes of the reflector surfaces, u and w , we combine Eq. (24) and Eq. (27) to obtain

$$u(\hat{\mathbf{s}}) = \frac{\beta}{1 - \hat{\mathbf{s}} \cdot \hat{\mathbf{a}}_3 + e^{u_1}}, \quad w(\mathbf{z}) = l + \frac{1}{2} \beta (1 - |\mathbf{z}|^2) - \beta e^{u_2}, \tag{69}$$

where $u_2 = c - u_1$, using Eq. (28).

The solution to the boundary value problem (67) is unique up to an additive constant [9]. This means that choosing the value of u_1 in one point gives us a unique solution. We use this degree of freedom to choose the position of one of the reflectors along the central ray given by $\hat{\mathbf{s}} = \hat{\mathbf{s}}_0 := (0, 0, 1)^T$. For example, we can choose $u(\hat{\mathbf{s}}_0) = u_0$ for some $u_0 > 0$. With Eq. (69), this then gives

$$u_1(\omega_0) = \log \left(\frac{\beta}{u_0} - (1 - \hat{\mathbf{s}}_0 \cdot \hat{\mathbf{a}}_3) \right) = \log \left(\frac{\beta}{u_0} - (1 - \cos \varphi) \right), \tag{70}$$

where $\omega_0 = \omega(\hat{\mathbf{s}}_0)$ and φ is the polar angle of the output rays. This expression, together with the boundary value problem (67), gives a unique solution for u_1 and therefore also for u and w . In this case we cannot freely choose the position of the second reflector along the central ray. Alternatively, we could give $w(\mathbf{m}(\omega_0)) = w_0$ as input instead of u_0 . This would also fix u_1 , u and w .

4. Results

We will apply the method from the previous section to examples with two distinct combinations of source and target distributions. We create several optical systems with different layouts to show the possibilities of the algorithm.

4.1. Uniform to uniform

The example we will look at first consists of a uniform conical source and a uniform circular target distribution. We will test several layouts of optical systems, so different angles for the outgoing beam. Because our source is rotationally symmetric, our choice of θ does not matter and we can choose $\theta = 0$. We will discuss optical systems with $\varphi = 0$, $\varphi = \pi/2$ and $\varphi = \pi$. The first and last one have outgoing beams parallel to the $\hat{\mathbf{e}}_3$ -axis in the positive and negative direction, respectively. For $\varphi = \pi/2$ the output beam is parallel to the $\hat{\mathbf{e}}_1$ -axis. We shift the target domain along the target plane to avoid mirrors obstructing rays. Otherwise, for example, the first reflector could be in the way of the rays from the second reflector to the target. For the point source, we use a uniform distribution in the direction vector $\hat{\mathbf{s}}$ rather than the stereographic coordinates \mathbf{x} . This means that the intensity distribution given by $f = f(\hat{\mathbf{s}})$ is constant. The source domain is given by $\rho \leq 0.1$ and we choose the value of f such that the total flux is 1. The target domain is a circle with radius 2. The target distribution g is constant over this domain, with a flux of 1.

There are some parameter choices that will affect the optimization procedure or the resulting optical system. For example, the functional in Eq. (50) contains the parameter α . The smaller α , the more important the boundary is in the optimization, relative to the interior. The choice of α will have an impact on the convergence speed of the algorithm [2]. Other parameters have an influence on the layout of the optical system. These are the distance to the target plane, l , the reduced optical path length, β (or L), and either u_0 or w_0 .

For our first test case we use $\alpha = 0.1$. From numerical experiments we found that this value works well. We discretize the polar source domain with a 200×200 grid. The results of our test case were obtained by running the least-squares algorithm for 200 iterations. First, we did this for a case where $\varphi = 0$. We use a target plane at a distance $l = 20$ and we choose to shift the target domain by a distance -10 along the \hat{a}_1 -direction. Furthermore, we put $u_0 = 10$ and $\beta = 15$.

The full algorithm ran for 167 seconds, with each iteration taking approximately 0.6 seconds on average. The calculations were done on a laptop with Intel Core i7-8750H CPU 2.20 GHz with 32.0 GB of RAM. After iterating, the error functionals reached the values $J_1 = 6.641 \cdot 10^{-10}$ and $J_B = 6.785 \cdot 10^{-12}$. The resulting optical system is visualized using a ray trace procedure. For this, we triangulate the reflector surfaces and use the normals on these triangles to calculate the reflected ray directions. The result can be seen in Fig. 2. In the figure we show 100 random rays that are obtained from this ray trace. On the target plane we show the illumination pattern in a bounding box of the target domain. We divide this box in 100 by 100 bins and use a quasi-Monte Carlo method tracing ten million rays to get an illumination pattern. A better view of the illumination pattern is given in Fig. 3. As we can see, the illuminated part of the bounding box forms a circle. The flux per bin, and thus the illumination, on this circle is nicely uniform. The exact flux in a bin within the circle should be $1.572 \cdot 10^{-4}$. We take a square of 50×50 bins to ensure that they are all fully inside the circle. The average calculated flux in these bins was $1.569 \cdot 10^{-4}$. We calculated the rms of the difference between expected and calculated values of the flux in a bin and found the value $6.87 \cdot 10^{-6}$. This is 4.4% of the mean flux. This variation is caused by the numerical errors of our algorithm and the Monte Carlo method, but we cannot separate the two contributions.

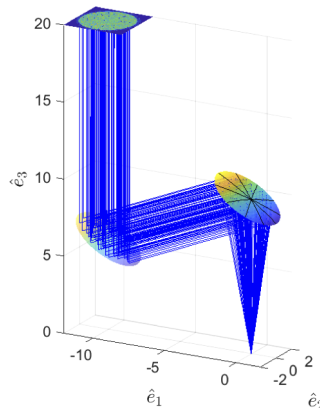


Fig. 2. The resulting optical system for the first test case with $\varphi = 0$, $u_0 = 10$ and $\beta = 15$.

As mentioned before, an important benefit of our algorithm is the ability to construct a wide variety of optical systems. Some examples of possible layouts are shown in Fig. 4. The first two figures both have $\varphi = \pi/2$, $\theta = 0$ and $\beta = 22$. The target plane is located at a distance $l = 5$ and the center of the target domain is shifted by -5 along \hat{a}_1 . With $\varphi = \pi/2$ and $\theta = 0$ we have $\hat{a}_1 = -\hat{e}_3$. The difference between the two optical systems is that in Fig. 4(a) we have $u_0 = 10$ and in Fig. 4(b) we have $u_0 = 1$. Note that these two have the exact same mapping, since the

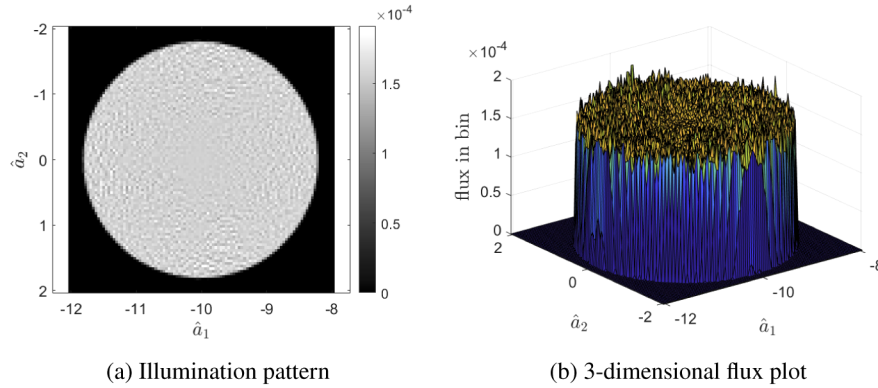


Fig. 3. The ray traced light flux per bin on the target domain visualized in two ways.

parameter u_0 only plays a role in the calculation of the surfaces (see Sec. 3). Therefore, we only need to calculate the mapping once, and we are able to construct both of these optical systems from this mapping by varying u_0 . For Fig. 4(c) we change the angle of the outgoing beam to $\varphi = \pi$ and we use $w_0 = 6$. We choose $l = 0$, so the target plane is equal to the source plane. We shift the target domain by 10 along the \hat{e}_1 -axis and we again use $\beta = 22$. In each of the previously mentioned optical systems, there is a plane of symmetry. However, this is not necessary for our algorithm. In Fig. 4(d), we shift the target domain by -5 along \hat{a}_1 and 5 along \hat{a}_2 . This breaks the symmetry of the optical system. Furthermore, we set $\beta = 15$ and $w_0 = 5$.

4.2. Laser diode to ring-shaped target

The second test case for our algorithm is the case of a laser diode [5] to a ring-shaped target pattern. In this case we choose $\varphi = \pi/2$ and $\theta = 0$, so that the outgoing beam is parallel to the \hat{e}_1 -axis. Note that the angle θ only matters when the source distribution is not rotationally symmetric. The intensity distribution of a laser diode can be modeled by an elliptical Gaussian on a plane perpendicular to the \hat{e}_3 -axis [4]. The emitted light has a $1/e^2$ intensity angle of θ_x in the \hat{e}_1, \hat{e}_3 -plane, and θ_y in the \hat{e}_2, \hat{e}_3 -plane. From this we can derive a density in terms of the x -variables, see Appendix A. The following density function is obtained:

$$f(\mathbf{x}) = B_x \frac{1 + |\mathbf{x}|^2}{(1 - |\mathbf{x}|^2)^3} \left(\exp \left[\frac{-8}{(1 - |\mathbf{x}|^2)^2} \left(\frac{x_1^2}{\sigma_x^2} + \frac{x_2^2}{\sigma_y^2} \right) \right] + \delta \right), \quad (71)$$

with $\sigma_x = \tan(\theta_x/2)$ and $\sigma_y = \tan(\theta_y/2)$. The scalar B_x is a scaling parameter such that the flux of f over \mathcal{X} is 1. The parameter δ is used to ensure a minimal value for the source density. The source domain \mathcal{X} is given by

$$\mathcal{X} = \{\mathbf{x} \in \mathbb{R}^2 \mid \rho \leq \tan(\Theta/2)\}, \quad (72)$$

where $\Theta = \max(\theta_x, \theta_y)/2$.

We want to have a target which consists of a ring on a target plane with an outer radius r_o and an inner radius r_i . For this we will construct a density as a function of the unscaled target variables \mathbf{y} . We want this density to be uniform on a ring Ω_r . With our algorithm we need a simply connected domain. So, instead of a ring, the domain we use will be a disk $\Omega_T = \Omega_r \cup \Omega_i$, where Ω_i is the circular domain enclosed by Ω_r . The ring will have a higher density than the inner disk. Our model assumes that the density is smooth, so we will need to approximate this discontinuous change in density between the ring and the inner circle. From the derivation in

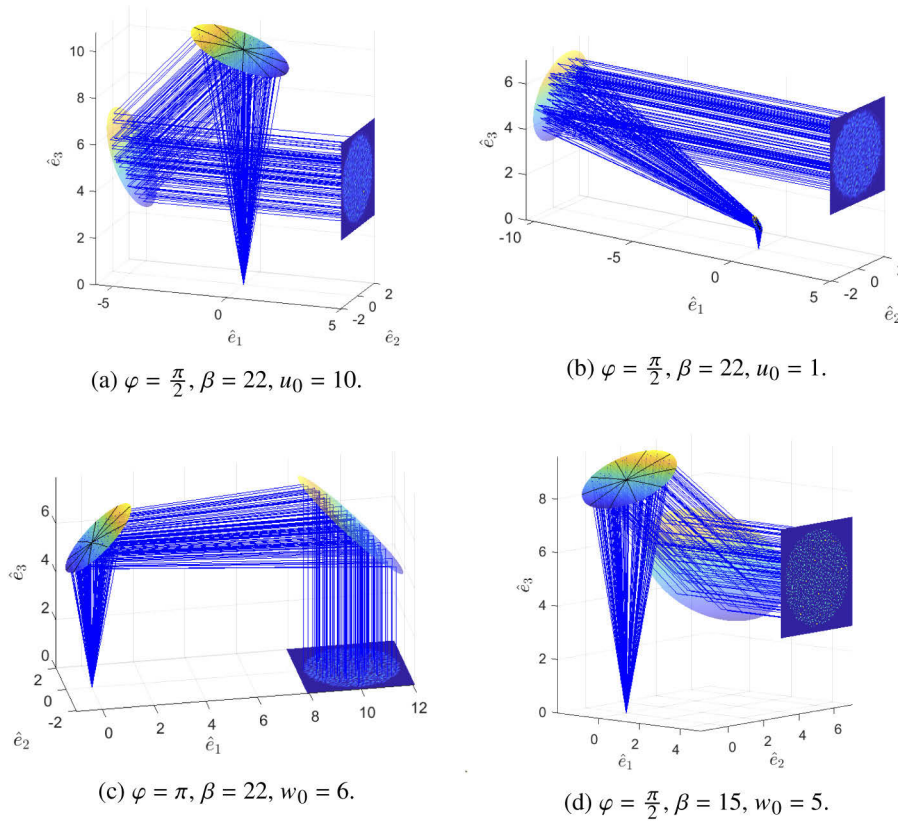


Fig. 4. Some examples of layouts constructed with our algorithm

Appendix B. we obtain the target intensity distribution

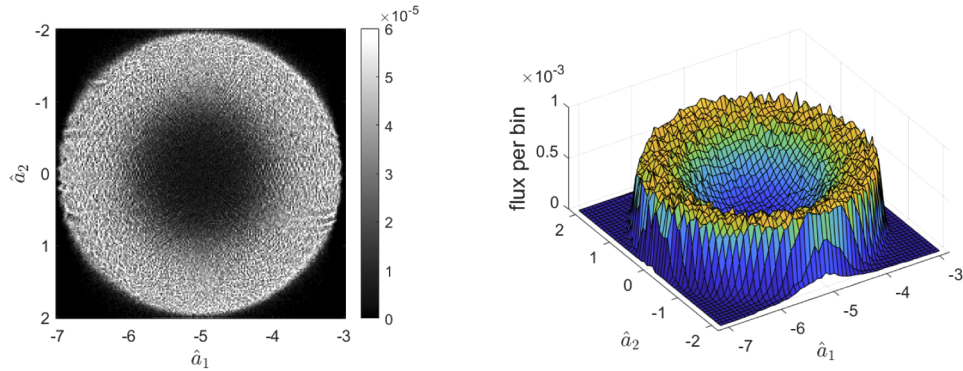
$$g(\mathbf{y}) = \frac{c}{1 + e^{-2k(|\mathbf{y}| - r_i)}} + \varepsilon. \quad (73)$$

We choose c so that the total flux over the target domain is equal to 1. The parameters k and ε determine how close this density is to the ideal density, uniform on Ω_r and zero on Ω_i . They also influence the convergence of the algorithm. Generally a smaller k or larger ε will give better convergence, but a less pronounced difference in density between the inner region and the outer ring.

For the source density, we choose to work with $1/e^2$ intensity angles $\theta_x = 45^\circ$ and $\theta_y = 13^\circ$. These are typical values for a laser diode [5]. To avoid a too large difference in intensity in the source, we choose $\delta = 10^{-3}$ in the density function from Eq. (71). The target domain consists of an outer radius $r_o = 2$ and an inner radius $r_i = 1$. This is shifted by -5 along the $\hat{\mathbf{a}}_1$ -axis in the target plane at a distance $l = 5$ from the point source. We choose ε such that the density in the inner circle is at least 10% of the density in the ring. Furthermore, we used $k = 100$ in the target density. We set $\beta = 30$ and $u_0 = 20$. Because the intensity on the boundary of the source is much lower than at the center, it is more difficult for the algorithm to find a good mapping for the boundary compared to our previous test case. To counter this problem we decrease α . We now choose $\alpha = 0.01$ to put more emphasis on J_B relative to J_I . Compared to the previous cases, we also increase the number of grid points and apply a 400×400 grid to the source domain.

This time, we ran the algorithm for 1000 iterations. This took 3010 seconds, with approximately 2.65 seconds per iteration, converging to the values $J_I = 6.792 \cdot 10^{-7}$ and $J_B = 2.590 \cdot 10^{-9}$.

Tracing one million rays through the system that results from our algorithm gives us the illumination pattern and optical system in Fig. 5 and Fig. 6.



(a) illumination pattern, using 200×200 bins.

(b) 3-dimensional density plot, using 50×50 bins.

Fig. 5. The ray traced light intensity on the target plane for a laser diode source and ring-shaped target intensity.

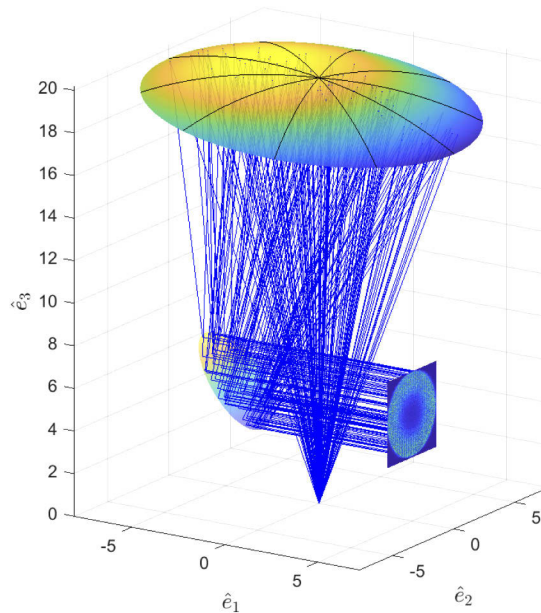


Fig. 6. The optical system of our solution to the laser diode to ring-target problem.

5. Conclusion

In this paper we introduced a method for computing the shapes of two reflectors to collimate a beam from a point source, for given source and target light distributions. A specific point of interest is the fact that the outgoing beam can be in any arbitrary direction. First we have derived a relation between the surface shapes and locations, and the optical mapping. Then we derived a Monge-Ampère type equation for this problem. We proposed an algorithm based on the least-squares method to solve this equation.

We tested our algorithm on two test cases. A uniform source and target, and a model of a laser diode to a ring-shaped target. The former was used to test the algorithm and the different layouts that it could attain. The latter consisted of more complicated source and target distributions instead. The second test case showed us that we might need to put some restrictions on our model to improve the convergence of the algorithm. For example, the variation of the intensity in the source cannot be too large. This was solved by imposing a minimal value of the source distribution.

We have chosen to present these two test cases, but the algorithm can be used for other source and target distributions. We have shown some limitations, e.g., the value of g cannot be 0, but the method can still be used broadly. For example, it has been shown by Romijn et al. in [23] that with a slightly different cost function, this algorithm can also be used to create complicated grayscale images as a target.

For further research there are several points of interest. In this paper we have skipped over some practical constraints. There is nothing in the algorithm yet preventing the rays from crossing a reflector. For example, the first reflector might (partially) be in the way of the outgoing beam. We managed to work around this by varying parameters to get a feasible solution. However, for the future it might be interesting to research if it could be possible to incorporate physical constraints like this into our algorithm. Furthermore we want to extend our algorithm to include more physical phenomena. Examples of this are Fresnel reflection (for lenses) and scattering.

Appendix A. Laser diode model

The intensity distribution of a laser diode can be modeled by an elliptical Gaussian on a plane perpendicular to the \hat{e}_3 -axis [4]. We choose the plane $z = z_p$. The intersection of a ray with this plane is given by the position vector $\mathbf{p} = (p_1, p_2)^\top$ on this plane. The p_1 - and p_2 -axes are parallel to the \hat{e}_1 - and \hat{e}_2 -axes, respectively. The intensity on the plane is then given by

$$I(\mathbf{p}) = B \exp \left[-2 \left(\frac{p_1^2}{w_1^2} + \frac{p_2^2}{w_2^2} \right) \right], \quad (74)$$

where w_1 and w_2 are the $1/e^2$ intensity radii. These are the values along the p_1 - and p_2 -axes where the intensity has decreased to a factor $1/e^2$ of the maximum. The factor B will be used to scale the function such that the total flux of the source is equal to 1.

We denote by Ω_p the source domain in \mathbf{p} -coordinates, so $\Omega_p = \{\mathbf{p} = \mathbf{p}(\mathbf{x}) \mid \mathbf{x} \in \mathcal{X}\}$. We need to have a finite support for the intensity, so we choose the domain Ω_p given by $|\mathbf{p}| \leq \max(w_1, w_2)$. The difference between w_1 and w_2 can often be quite large. This could create a ratio of many orders of magnitude between the minimal and maximal value of I in the domain. This causes problems with grid lines getting too close to each other on the target. Therefore we add a constant $\delta > 0$ to the intensity to assure a minimal value. This gives the new intensity

$$\tilde{I}(\mathbf{p}) = \tilde{B} \left(\exp \left[-2 \left(\frac{p_1^2}{w_1^2} + \frac{p_2^2}{w_2^2} \right) \right] + \delta \right). \quad (75)$$

Again, the factor \tilde{B} is used to scale the total flux to 1. Now we have a formula for the source intensity on the plane $z = z_p$, but we want to convert this into an intensity f in stereographic coordinates. For this, we first convert \mathbf{p} to a directional vector $\hat{\mathbf{s}}$ and then to stereographic coordinates \mathbf{x} to obtain

$$\mathbf{p} = \frac{z_p}{s_3} \begin{pmatrix} s_1 \\ s_2 \end{pmatrix} = \frac{2z_p \mathbf{x}}{1 - |\mathbf{x}|^2}. \quad (76)$$

We already used \mathcal{X} for the source domain in stereographic coordinates. For any subset $\mathcal{A} \subset \mathcal{X}$ we have a corresponding set $\mathcal{A}_p = \mathbf{p}(\mathcal{A}) \subset \Omega_p$. The total flux in those two sets should be equal,

so

$$\iint_{\mathcal{A}} f(\mathbf{x}) dA(\mathbf{x}) = \iint_{\mathcal{A}_p} \tilde{I}(\mathbf{p}) dA(\mathbf{p}). \quad (77)$$

We write the right-hand side as an integral over \mathcal{A} by using integration by substitution. Because this holds for any subset \mathcal{A} , this gives a source density function f , with

$$\begin{aligned} f(\mathbf{x}) &= \det(\mathbf{D}\mathbf{p}(\mathbf{x})) \tilde{I}(\mathbf{p}(\mathbf{x})) \\ &= 4\tilde{B}z_p^2 \frac{1 + |\mathbf{x}|^2}{(1 - |\mathbf{x}|^2)^3} \left(\exp \left[\frac{-8z_p^2}{(1 - |\mathbf{x}|^2)^2} \left(\frac{x_1^2}{w_1^2} + \frac{x_2^2}{w_1^2} \right) \right] + \delta \right). \end{aligned} \quad (78)$$

This density seems to be dependent on z_p , while the intensity of the point source should of course not depend on the plane of projection. We will show that we can in fact write f as a function independent of z_p . In general, the increase of w_1 and w_2 for increasing z_p is given by the full angles at the source point, θ_x and θ_y . So these radii of a laser diode increase linearly in z_p . We then have

$$w_1 = z_p \tan(\theta_x/2), \quad w_2 = z_p \tan(\theta_y/2), \quad (79)$$

so that

$$f(\mathbf{x}) = B_x \frac{1 + |\mathbf{x}|^2}{(1 - |\mathbf{x}|^2)^3} \left(\exp \left[\frac{-8}{(1 - |\mathbf{x}|^2)^2} \left(\frac{x_1^2}{\sigma_x^2} + \frac{x_2^2}{\sigma_y^2} \right) \right] + \delta \right), \quad (80)$$

with $\sigma_x = \tan(\theta_x/2)$, $\sigma_y = \tan(\theta_y/2)$ and $B_x = 4\tilde{B}z_p^2$. With Eq. (75) and integration by substitution, B_x can be written as

$$B_x = \left(\iint_{\mathcal{X}} \frac{1 + |\mathbf{x}|^2}{(1 - |\mathbf{x}|^2)^3} \left(\exp \left[\frac{-8}{(1 - |\mathbf{x}|^2)^2} \left(\frac{x_1^2}{\sigma_x^2} + \frac{x_2^2}{\sigma_y^2} \right) \right] + \delta \right) dA \right)^{-1}. \quad (81)$$

This shows that B_x is independent of z_p and indeed also our source density f is independent of z_p . The only part left for our source density is to define the boundary of the domain in stereographic coordinates. We mentioned before that the boundary of the domain in \mathbf{p} -coordinates on the plane $z = z_p$ is given by $|\mathbf{p}| = \max(w_1, w_2)$, which is written as $|\mathbf{p}| = \max(z_p \tan(\theta_x/2), z_p \tan(\theta_y/2)) = z_p \tan(\Theta/2)$, with $\Theta = \max(\theta_x, \theta_y)/2$. From Eq. (76) we obtain

$$|\mathbf{x}| = \frac{\sqrt{z_p^2 + |\mathbf{p}|^2} - z_p}{|\mathbf{p}|}. \quad (82)$$

On the boundary this gives

$$|\mathbf{x}| = \frac{\sqrt{z_p^2 + z_p^2 \tan^2(\Theta)} - z_p}{z_p \tan(\Theta)} = \frac{1 - \cos(\Theta)}{\sin(\Theta)} = \tan(\Theta/2). \quad (83)$$

Again, this result is independent of the choice of z_p . We have now modeled the laser diode by the intensity distribution in Eq. (80), defined on the domain

$$\mathcal{X} = \{\mathbf{x} \in \mathbb{R}^2 \mid |\mathbf{x}| \leq \tan(\Theta/2)\}. \quad (84)$$

Appendix B. Ring-target density

We define our circular domain Ω_T by an angle $\xi \in [0, 2\pi)$ and a radius $r \in [0, r_o]$. The outer ring is denoted by Ω_r and given by $r \in [r_i, r_o]$. The inner disk Ω_i is then given by $r \in [0, r_i]$ such that

we have $\Omega_T = \Omega_r \cup \Omega_i$. We denote the area of the ring by A and we have

$$A = \pi(r_o^2 - r_i^2). \quad (85)$$

Ideally, we would have a density function \tilde{h} defined on Ω_T with values

$$\tilde{h}(\mathbf{y}) = \begin{cases} 1/A, & \text{for } |\mathbf{y}| \geq r_i, \\ 0, & \text{for } |\mathbf{y}| < r_i. \end{cases} \quad (86)$$

This density has similarities to the Heaviside stepfunction H . We use this to write $\tilde{h}(\mathbf{y}) = (1/A)H(|\mathbf{y}| - r_i)$. As can be seen in Eq. (37a), we cannot have a target intensity equal to 0 at any point in the target domain. To avoid this, we construct a density which has value ε on Ω_i . We define the function h by

$$h(\mathbf{y}) = cH(|\mathbf{y}| - r_i) + \varepsilon = \begin{cases} c + \varepsilon, & \text{for } |\mathbf{y}| \geq r_i, \\ \varepsilon, & \text{for } |\mathbf{y}| < r_i. \end{cases} \quad (87)$$

The problem with the density function that we have proposed now is that it is discontinuous across the circle $|\mathbf{y}| = r_i$. Experiments have shown that our algorithms will not work with discontinuities. To avoid this problem, we have to approximate the discontinuous density by a smooth function. The Heaviside stepfunction that was mentioned before can be approximated by

$$H(y) \approx \frac{1}{2}(1 + \tanh(ky)) = \frac{1}{1 + e^{-2ky}}, \quad (88)$$

where $k > 0$. The approximation converges pointwise to H for $k \rightarrow \infty$ [29, Ch. 9]. We use this in combination with Eq. (87) to construct a density that approximates the ring target. This density is given by

$$g(\mathbf{y}) = \frac{c}{1 + e^{-2k(|\mathbf{y}| - r_i)}} + \varepsilon. \quad (89)$$

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Data availability. Data underlying the results presented in this paper are not publicly available at this time but may be obtained from the authors upon reasonable request.

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