

A multifunctional photonic integrated circuit for diverse microwave signal generation, transmission and processing

Citation for published version (APA):

Zou, X., Zou, F., Cao, Z., Lu, B., Yan, X., Yu, G., Deng, X., Luo, B., Yan, L., Pan, W., Yao, J., & Koonen, A. M. J. (2019). A multifunctional photonic integrated circuit for diverse microwave signal generation, transmission and processing. *Laser & Photonics reviews*, 13(6), Article 1800240. <https://doi.org/10.1002/lpor.201800240>

DOI:

[10.1002/lpor.201800240](https://doi.org/10.1002/lpor.201800240)

Document status and date:

Published: 01/06/2019

Document Version:

Publisher's PDF, also known as Version of Record (includes final page, issue and volume numbers)

Please check the document version of this publication:

- A submitted manuscript is the version of the article upon submission and before peer-review. There can be important differences between the submitted version and the official published version of record. People interested in the research are advised to contact the author for the final version of the publication, or visit the DOI to the publisher's website.
- The final author version and the galley proof are versions of the publication after peer review.
- The final published version features the final layout of the paper including the volume, issue and page numbers.

[Link to publication](#)

General rights

Copyright and moral rights for the publications made accessible in the public portal are retained by the authors and/or other copyright owners and it is a condition of accessing publications that users recognise and abide by the legal requirements associated with these rights.

- Users may download and print one copy of any publication from the public portal for the purpose of private study or research.
- You may not further distribute the material or use it for any profit-making activity or commercial gain
- You may freely distribute the URL identifying the publication in the public portal.

If the publication is distributed under the terms of Article 25fa of the Dutch Copyright Act, indicated by the "Taverne" license above, please follow below link for the End User Agreement:

www.tue.nl/taverne

Take down policy

If you believe that this document breaches copyright please contact us at:

openaccess@tue.nl

providing details and we will investigate your claim.

A Multifunctional Photonic Integrated Circuit for Diverse Microwave Signal Generation, Transmission, and Processing

Xihua Zou,* Fang Zou, Zizheng Cao,* Bing Lu, Xianglei Yan, Ge Yu, Xiong Deng, Bin Luo, Lianshan Yan, Wei Pan,* Jianping Yao,* and Antonius M. J. Koonen*

Microwave photonics (MWP) studies the interaction between microwaves and optical waves for the generation, transmission, and processing of microwave signals (i.e., three key domains), taking advantage of the broad bandwidth and low loss offered by modern photonics. Integrated MWP using photonic integrated circuits (PICs) can reach a compact, reliable, and green implementation. Most PICs, however, are recently developed to perform one or more functions restricted inside a single domain. Herein, as highly desired, a multifunctional PIC is proposed to cover the three key domains. The PIC is fabricated on an InP platform by monolithically integrating four laser diodes and two modulators. Using the multifunctional PIC, seven fundamental functions across microwave signal generation, transmission, and processing are demonstrated experimentally. Outdoor field trials for electromagnetic environment surveillance along in-service high-speed railways are also performed. The success of such a PIC marks a key step forward for practical and massive MWP implementations.

1. Introduction

Microwave photonics (MWP), an emerging interdisciplinary field by bringing together microwave and optical waves,^[1–4] is capable of overcoming the current challenges and troubles in the generation, transmission, and processing of microwave signals (i.e., three key domains of MWP), thanks to the inherently broadband and low-loss features of modern photonics. Traditionally, MWP systems using discrete components are fully exploited and implemented, for instance, in arbitrary waveform generator, wireless communications, signal processing and detection, and radar.^[5–9] However, the scalability in both function and cost hinders the popularization of MWP. Hence photonic integrated circuit (PIC) leading to a compact and easy-to-handle implementation is needed

to accelerate the integrated MWP's maturity,^[10,11] as it can greatly reduce the footprint and cost and considerably enhance the stability and energy efficiency.

Recently, a large number of PICs have been developed to implement different microwave devices or systems, including signal generators,^[12–16] filters,^[17–19] true-time delay lines and beamformers,^[20–23] signal processors,^[24–30] frontends and transceivers,^[31–35] and systems for signal characterization and interference cancellation.^[36–39] Particularly, a few PICs have been developed to enable a generic, programmable processor or processor core^[25–29] in the signal processing domain. However, these PICs are currently developed to perform one or more functions covering a single domain (i.e., microwave signal generation, transmission or processing). Namely, the PIC-assisted functions are restricted inside a single domain (see the overview listed in Table 1). The weakness behind the single-domain operation leads to long development time, high foundry cost, and thus limited applications. In addition, although PICs have been widely used in MWP field, they mostly have been only conceptually demonstrated in laboratory tests with well-conditioned laboratory environments or off-line conditions.^[25–30] There exists a serious gap between laboratory demonstrations and practical applications, in which stability and robustness are two issues that must be addressed.

Therefore, we propose a multifunctional PIC capable of covering all the three key domains of MWP, the microwave signal

Prof. X. Zou, Prof. F. Zou, Prof. B. Lu, Prof. X. Yan, Prof. G. Yu, Prof. B. Luo, Prof. L. Yan, Prof. W. Pan
Center for Information Photonics and Communications
School of Information Science and Technology
Southwest Jiaotong University, and CSNMT International Cooperation
Research Center of China
Chengdu, 611756, China
E-mail: zouxihua@swjtu.edu.cn; wpan@swjtu.edu.cn

Prof. Z. Cao, Prof. X. Deng, Prof. A. M. J. Koonen
Institute for Photonic Integration (the former COBRA Research
Institute), Electro-Optics Communication Group
Eindhoven University of Technology
Eindhoven, 5600 MB, The Netherlands
E-mail: z.cao@tue.nl; a.m.j.koonen@tue.nl

Prof. J. Yao
Microwave Photonics Research Laboratory, School of Electrical
Engineering and Computer Science
University of Ottawa
Ottawa, K1N 6N5, Canada
E-mail: jpyao@eecs.uottawa.ca

 The ORCID identification number(s) for the author(s) of this article can be found under <https://doi.org/10.1002/lpor.201800240>

© 2019 The Authors. Published by WILEY-VCH Verlag GmbH & Co. KGaA, Weinheim. This is an open access article under the terms of the Creative Commons Attribution-NonCommercial License, which permits use, distribution and reproduction in any medium, provided the original work is properly cited and is not used for commercial purposes.

DOI: 10.1002/lpor.201800240

Table 1. Overview of PICs for microwave signal generation, transmission, and processing.

Year & Ref.	Corresponding author & affiliation	Three key domains of MWP (generation, transmission, and processing)			Integration type		Integrated element (number)	Service scenario	
		Number	Domain	Function	Passive	Active		Lab	Outdoor
2010 ^[12]	A. M. Weiner, Purdue U.	1	Generation	AWG	☺		Micro-ring (8), MZI (8)	☺	☹
2010 ^[20]	A. Meijerink, U. Twente	1	Processing	Beamforming	☺		ORR (4), splitters (3)	☺	☹
2011 ^[17]	L. A. Coldren, UCSB	1	Processing	Filter	☺	☺	SOA (21), PM (10), MMI (10)	☺	☹
2012 ^[24]	F. X. Kartner, MIT	1	Processing	ADC	☺	☺	MZM (1), ORR (2), PD (8), coupler (1)	☺	☹
2013 ^[36]	J. S. Fandiño, UPV	1	Processing	IFM	☺		RAMZI (1)	☺	☹
2014 ^[18]	S. B. Yoo, UC Davis	1	Processing	Filter	☺		PS (26), DC (18)	☺	☹
2014 ^[21]	W. Shi, McGill U.	1	Processing	TTD	☺		WBG (1)	☺	☹
2014 ^[34]	F. van Dijk, III-V Lab	1	Generation	Transmitter	☺	☺	Laser (2), SOA (8), MMI (2), PD (2)	☺	☹
2015 ^[25]	L. Zhuang, Monash U.	1	Processing	Delay line, filter, Hilbert transform	☺		Tunable M-Z couplers (array)	☺	☹
2015 ^[37]	D. Marpaung, Sydney U.	1	Processing	IFM	☺		Silicon waveguide (1)	☺	☹
2015 ^[13]	A. M. Weiner, Purdue U.	1	Generation	AWG	☺		ORR (16)	☺	☹
2016 ^[38]	J. Azaña, INRS-EMT	1	Processing	IFM	☺		WBG (1)	☺	☹
2016 ^[26]	J. Yao, U. Ottawa	1	Processing	Differentiator, Hilbert transform, integrator		☺	MMI (8), PM (12), SOA (9)	☺	☹
2017 ^[29]	B. J. Eggleton, U. Sydney	1	Processing	Filter	☺		Chalcogenide waveguide (1)	☺	☹
2017 ^[19]	J. S. Fandiño, UPV	1	Processing	Filter	☺	☺	Laser (2), MZM (1), PM (1), Coupler (4), RAMZI (1), MZI (1), PD (4)	☺	☹
2017 ^[22]	L. Zhou, SJTU	1	Processing	TTD	☺		ORR (array), MZI switch (array)	☺	☹
2017 ^[30]	J. Yao, U. Ottawa	1	Processing	Differentiator	☺		MZI (1), MMI (1)	☺	☹
2017 ^[14]	J. Hulme, UCSB	1	Generation	Signal generator	☺	☺	Laser (2), PM (2), PD (1), DC (1)	☺	☹
2017 ^[15]	K. Xu, CUHK	1	Generation	Signal generator	☺		ORR (2), MZI (1)	☺	☹
2017 ^[27]	D. Pérez, UPV	1	Processing	Multipurpose signal processor	☺		7 hexagonal MZI waveguide cells	☺	☹
2018 ^[39]	M. P. Chang, Princeton U.	1	Processing	Self-interference cancellation	☺	☺	Laser (2), SOA (3), PD (2), BPD (1)	☺	☹
2018 ^[23]	D. J. Moss, SUT	1	Processing	TTD	☺		ORR (1)	☺	☹
2018 ^[16]	M. Li, CAS	1	Generation	OEO	☺	☺	Laser (1), Delay line (1), PD (1)	☺	
	2019, this paper	3	Generation Transmission Processing	Signal generator, analog links, filters, IFM, PRR measurement		☺	Laser (4), PM (1), IM (1), MMI (7)	☺	☺

Function. ADC, analog to digital converter; AWG, arbitrary waveform generator; IFM, instantaneous frequency measurement; OEO, optoelectronic oscillator; PRR, pulse repetition rate; TTD, true time delay; **Integrated element.** BPD, balanced photodetector; DC, directional coupler; IM, intensity modulator; MMI, multimode interferometer; MZI, Mach–Zehnder interferometer; MZM, Mach–Zehnder modulator; ORR, optical ring resonator; PD, photodetector; PM, phase modulator; PS, phase shifter; RAMZI, ring-assisted Mach–Zehnder interferometer; SOA, semiconductor optical amplifier; WBG, waveguide Bragg grating; **Service scenario.** Lab, laboratory tests; Outdoor, outdoor real-world applications.

generation, transmission, and processing. The PIC is fabricated by monolithically integrating four tunable lasers, two modulators, and seven multimode interference (MMI) couplers. It is designed to enable a few multifunctional or switchable on-chip elements, modulation architectures, and optical signal-flows. Using the multifunctional PIC, seven fundamental microwave functions across the three domains have been realized. The PIC is stable and robust for direct deployment in real-world applications, including electromagnetic environment surveillance for in-service high-speed railways, broadband wireless communications, and remote high-definition (HD) video access. This work demonstrates a milestone step toward the evolution and maturity of the integrated MWP, and therefore toward the future massive applications.

2. Multifunctional Photonic Integrated Circuit (PIC)

2.1. PIC Design and Fabrication

The PIC is first designed and fabricated on the InP material platform offered by the European joint JePPiX platform (www.jeppix.eu). As shown in **Figure 1a**, it has four distributed Bragg reflection lasers (DBRLs) in parallel, one Mach–Zehnder intensity modulator (IM) and one phase modulator (PM). Each four-section DBRL (see **Figure 1b**) consists of two tunable distributed Bragg reflectors (TDBRs), one semiconductor optical amplifier (SOA), and one weak phase shift (PS). The SOA provides gain for laser emission by controlling the injection current, while the incorporation of the two TDBRs and the PS facilitates

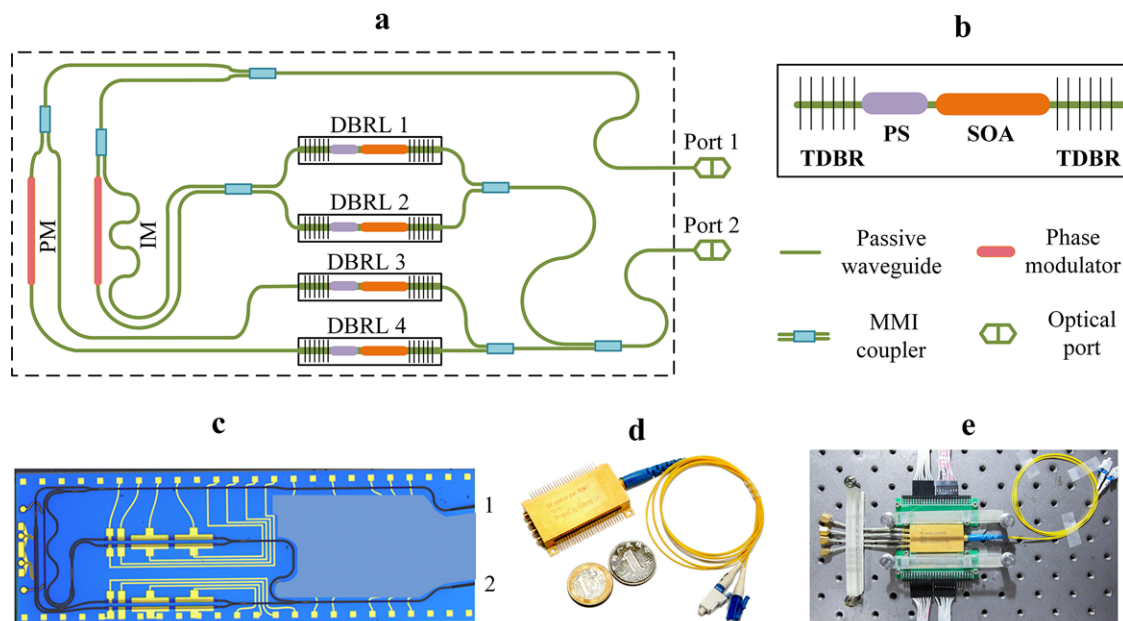


Figure 1. Layout and package of the multifunctional photonic integrated circuit. a) Layout. b) Four-section architecture of each DBRL. c) Inside view of the packaged PIC. d) External view of the packaged PIC. e) Packaged PIC assembled with a printed circuit board (PCB) peripheral interface. (DBRL, distributed Bragg reflector laser; IM, intensity modulator; MMI: multimode interference; PM, phase modulator, PS, phase shift; SOA, semiconductor optical amplifier; TDBR, tunable distributed Bragg reflector).

the wavelength tuning of each laser.^[40] Seven 3-dB MMI couplers connect the DBRLs and modulators, to provide multifunctional architectures and thus diverse applications. In addition, DBRL 1 and DBRL 2 are in parallel connected with the IM via two complementary ports of an MMI coupler, while DBRL 4 is directly connected with the PM.

As depicted in Figure 1c–e, the PIC has been delicately packaged with two optical ports (FC/APC) to obtain a switchable two-way transmission and four microwave GPPPO ports to feed the IM and PM; it is then assembled with a printed circuit board (PCB) peripheral interface. The four DBRLs are tested with linewidths of 3.3, 3.8, 4.3, and 2.5 MHz and with threshold currents of 13.2, 14.8, 15.1, and 16.1 mA. The IM and PM are characterized with an operation frequency up to 18 or 20 GHz (see Section S1, Supporting Information).

2.2. Multifunctional On-Chip Elements, Architectures, and Signal-Flows

The PIC is designed to be have multifunctional elements, modulation architectures, and switchable optical signal-flows. With the four-section body (see Figure 1b), each DBRL is playing a multifold role inside the PIC; it can operate as a single-wavelength laser for generating an optical carrier with tunable wavelength, an ultranarrow filter through optical injection locking, or a bandpass amplifier when biased slightly below the threshold current, as illustrated in Figure 2.

Four different modulation architectures are enabled in the PIC, as shown in Figure 2b. The phase modulation, intensity modulation, complementary intensity modulation, and parallel phase and intensity modulation are available, thanks to the flexible combination of the on-chip IM, PM, and MMI couplers.

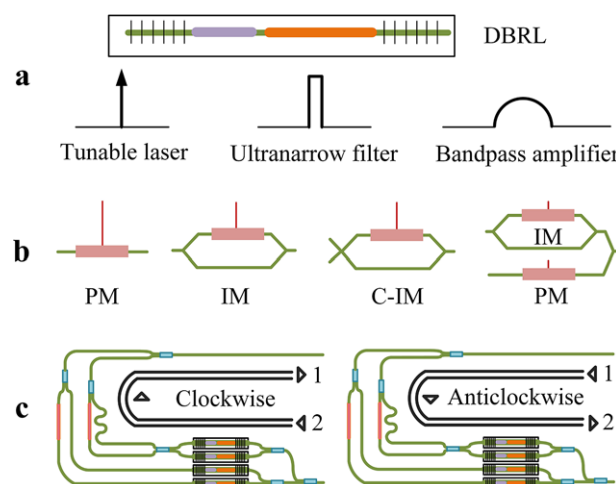


Figure 2. Multifunctional elements, architectures, and switchable signal-flows inside the photonic integrated circuit. a) The on-chip TDBR-SOA-TDBR can be configured to act as a tunable laser, an ultranarrow filter, or a bandpass amplifier. b) Four modulation architectures are available, including phase modulation, intensity modulation, complementary intensity modulation, and parallel phase and intensity modulation. c) Both clockwise and anticlockwise optical signal-flows can be switched, providing a two-way transmission.

Switchable optical signal-flows are also available in the PIC, since both optical links (without isolator or other nonreciprocal element) and microwave circuits allow a two-way transmission. Thus, the PIC can be configured to support either a clockwise optical signal-flow from Port 2 (input) to Port 1 (output) or an anticlockwise on from Port 1 (input) to Port 2 (output), as illustrated in Figure 2c. It is necessary to change the microwave input port of the on-chip IM or/and PM to retain high

electrooptic modulation efficiency for the clockwise optical signal-flow or anticlockwise one. What we have to do is only to swap the microwave input port and the 50- Ω terminal port of the IM or/and PM. These multifunctional elements, architectures, and switchable signal-flows enable the PIC to implement diverse applications across the three domains of microwave signal generation, transmission, and processing.

3. Seven Fundamental Functions across Three Key Domains

The multifunctional PIC is able to implement multiple fundamental functions across the three key domains of MWP (i.e., microwave signal generation, transmission, and processing). In detail, seven microwave photonic functions are demonstrated here, including remote signal generator, analog intensity-modulation and phase-modulation MWP links, tunable bandpass and bandstop filters, microwave frequency measurement, and pulse repetition rate measurement. The block diagrams and measured results are depicted in **Figure 3**, while more details can be found in Section S2, Supporting Information.

3.1. Signal Generation Domain: Remote Microwave Signal Generator

To implement a remote microwave signal generator, the PIC is configured with DBRL 3, DBRL 4, and the PM, as shown in Figure 3a. An optical frequency comb (OFC) with a comb spacing of 11 GHz is coupled into the PIC. One comb line from the OFC is filtered out by DBRL 4 through optical injection locking and then modulated by a designed intermediate-frequency or baseband signal, while another comb line is selected by DBRL 3 in a similar way. The two comb lines are transmitted synchronously over a long single-mode fiber for remote distribution and generation. At the remote unit, beating the two comb lines generates microwave signals with user-defined waveform and tunable carrier frequency. For example, as illustrated on the right of Figure 3b, one microwave signal with a linearly chirped frequency (LCF, from 23 to 24 GHz with a slope of 10 GHz μs^{-1}) and the other with binary frequency shift keying (2FSK, 34, or 35 GHz) are generated, when applying different intermediate-frequency signals to the on-chip PM. In addition, single-tone microwave signals with tunable carrier frequency at 22, 33, and 44 GHz have been generated (see Figure S3, Supporting Information). It should be highlighted that the PIC ensures both short-term and long-term stability on the phase and amplitude of the generated microwave signals, which are extremely difficult to achieve in conventional two-branch architectures using discrete components (see discussions in Section S3, Supporting Information).

3.2. Signal Transmission Domain: Analog Intensity-Modulation and Phase-Modulation MWP Links

The PIC can be installed in analog intensity-modulation and phase-modulation MWP links, providing remote transmission of microwave signal. In the analog intensity-modulation MWP link, one laser (DBRL 1 or DBRL 2) is activated, and inside the

on-chip IM the microwave signal to be transmitted is modulated on the optical carrier from the laser. For instance, an 8-GHz analog microwave signal carrying 500-Mbaud OOK (on-off keying) or QPSK (quadrature phase shift keying) baseband signal is applied, which is then transmitted over a 10-km single-mode fiber with the assistance of the PIC. In the central unit, the baseband signal is recovered via optical envelope detection and electronic down-conversion. The bit error rate (BER) curves and corresponding eye diagrams are recorded and shown in Figure 3b.

Likewise, in the phase-modulation link, the same microwave signal is applied to the PM inside the PIC, when DBRL 4 is switched on. As well known, linear phase demodulation is the critical step in the phase-modulation MWP link. Here, in the central unit the microwave signal is generated via phase-modulation to intensity-modulation conversion using an optical bandstop filter (actually a fiber Bragg grating with a 3-dB notch bandwidth of 0.08 nm) for phase demodulation. The BER curves and eye diagrams are recorded and shown in Figure 3c. It is clear that a BER of 10^{-4} is achieved at an optical power level around -10 dBm in both analog intensity-modulation and phase-modulation links when the microwave signal is carrying an OOK (500 Mbit s^{-1}) or QPSK (1 Gbit s^{-1}) signal.

3.3. Signal Processing Domain: Tunable Bandpass and Bandstop Filters, Microwave Frequency Measurement, and Pulse Repetition Rate Measurement

The PIC can also be employed for performing multiple functions in the microwave signal processing domain. In this section, tunable bandpass and bandstop filters, and systems for microwave frequency measurement and pulse repetition rate measurement will be demonstrated.

Both tunable bandpass and bandstop filters can be implemented by using the PIC. In the tunable bandpass filter, the PIC is configured to operate at an anticlockwise signal-flow mode and DBRL 4 is biased slightly below its threshold to act as a bandpass amplifier. The optical carrier of an external laser is phase-modulated inside the on-chip PM, and then the bandpass amplifier provides a gain response to perform phase-modulation to intensity-modulation conversion. Tunable bandpass responses can be achieved only inside the gain response, when tuning the wavelength difference between the optical carrier and gain response. The measured passbands (see Figure 3d) indicate a tunable frequency range from 10.8 to 12.4 GHz, as the wavelength of the external laser is configured as 1550.845, 1550.849, 1550.853, and 1550.857 nm, respectively. Also, a tunable bandstop or notch filter can be configured inside the PIC as a two-tap transverse microwave filter, when introducing a 5-km fiber as a delay element. The center frequency of the tunable stopband or notch is determined by the wavelength spacing between DBRL 1 and DBRL 2. Thus, by tuning this wavelength spacing as 4.0, 5.0, 5.7, and 8.0 nm, a tunable range from 9.3 to 12.3 GHz has been observed for the stopband or notch (see Figure 3e).

Microwave frequency measurement^[36–38] is of significance for civil and military applications, and the PIC enables us to implement such a measurement system. A dispersion-induced microwave power fading response from the PM branch of the PIC is incorporated with the periodic response of the two-tap

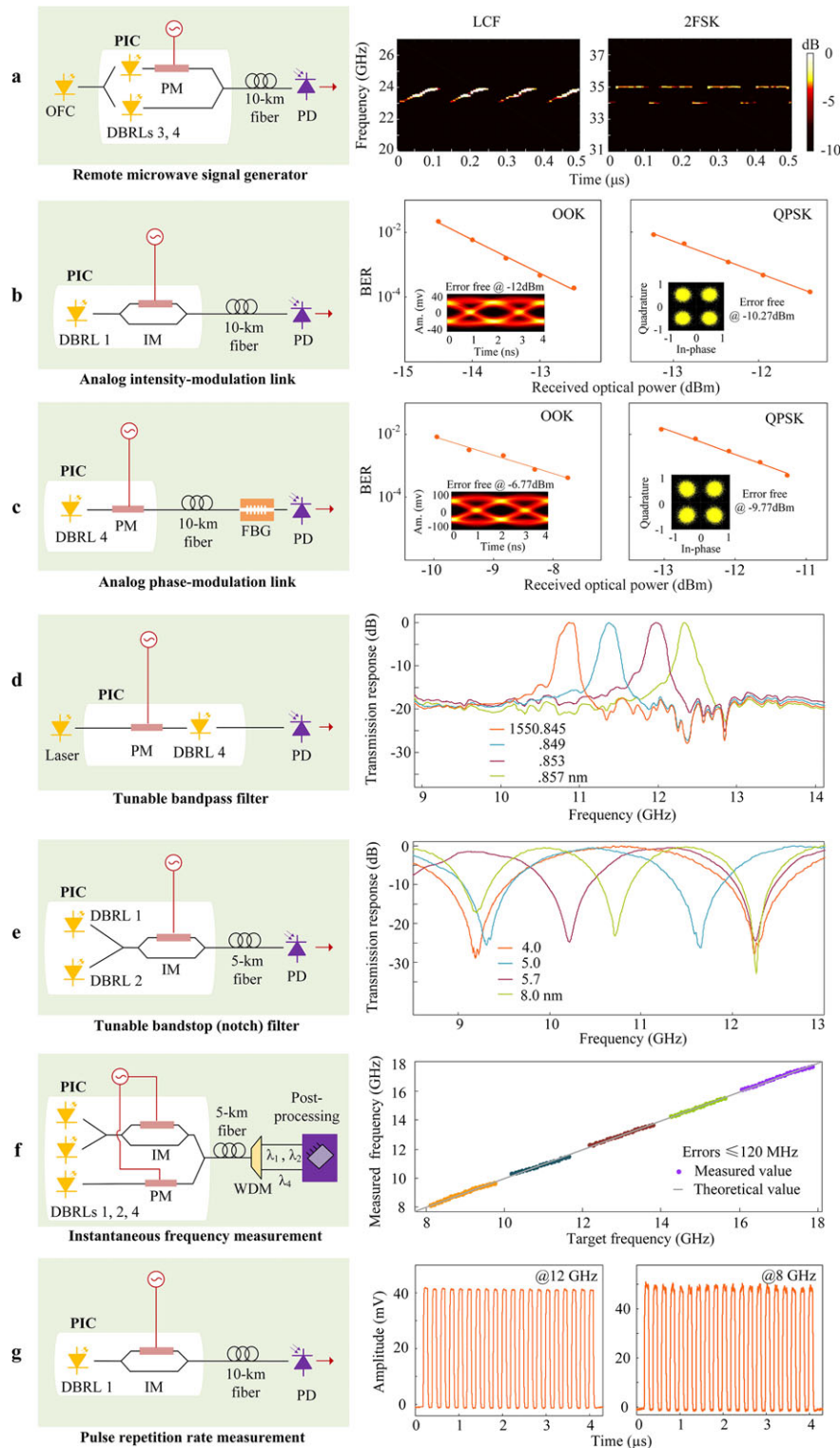


Figure 3. Seven fundamental microwave photonic functions enabled by the multifunctional PIC. a) Remote microwave signal generator and the time-frequency distributions of the microwave signals generated with LCF and 2FSK. The LCF ranges from 23 to 24 GHz, while the 2FSK switches between 34 and 35 GHz. b) Analog intensity-modulation link and c) analog phase-modulation link; the BER curves, eye, and constellation diagrams for the transmitted OOK and QPSK signals were presented. d–g) Signal processing: d) bandpass filter and its tunable passbands from 10.8 to 12.4 GHz; e) bandstop (notch) filter and its tunable stopbands (notches) from 9.3 to 12.3 GHz; f) instantaneous frequency measurement system and measured microwave frequencies within the range of 8.1–17.9 GHz; g) pulse repetition rate measurement system and measured pulse repetition rates for microwaves signals at 8 and 12 GHz. (FBG, fiber Bragg grating; OFC, optical frequency comb; PD, photodetector; PIC, photonic integrated circuit; WDM, wavelength division multiplexer).

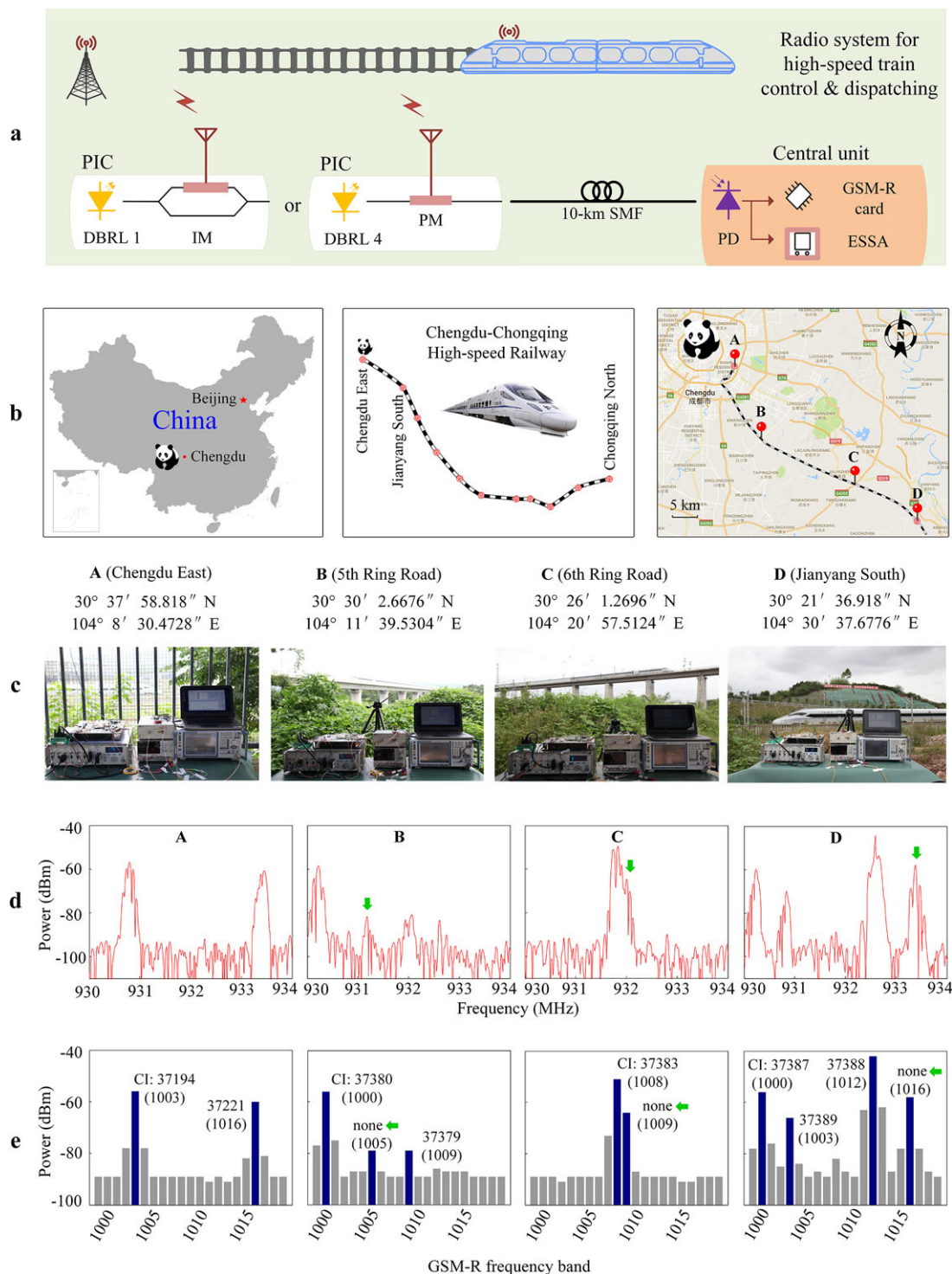


Figure 4. Field trials for electromagnetic environment surveillance along an in-service high-speed railway. a) PIC-assisted photonic system for implementing remote signal acquisition and transmission. b) Four test points distributed along the Chengdu–Chongqing High-speed Railway at a speed level of $\approx 300 \text{ km h}^{-1}$ in Southwest China. c) Locations and pictures of the field trials at the four test points. d) Real-time radio spectra acquired from the four test points. e) Cell identification (CI) and suspected electromagnetic interferences. The “green arrows” indicate suspected adjacent-channel or out-of-band interferences, as no licensed CI (“none”) is recognized. The definitions of the CI (e.g., 37 194) and frequency band (e.g., 1003) are described in Section S10, Supporting Information. (ESSA, electrical signal, and spectrum analyzer; PIC, photonic integrated circuit).

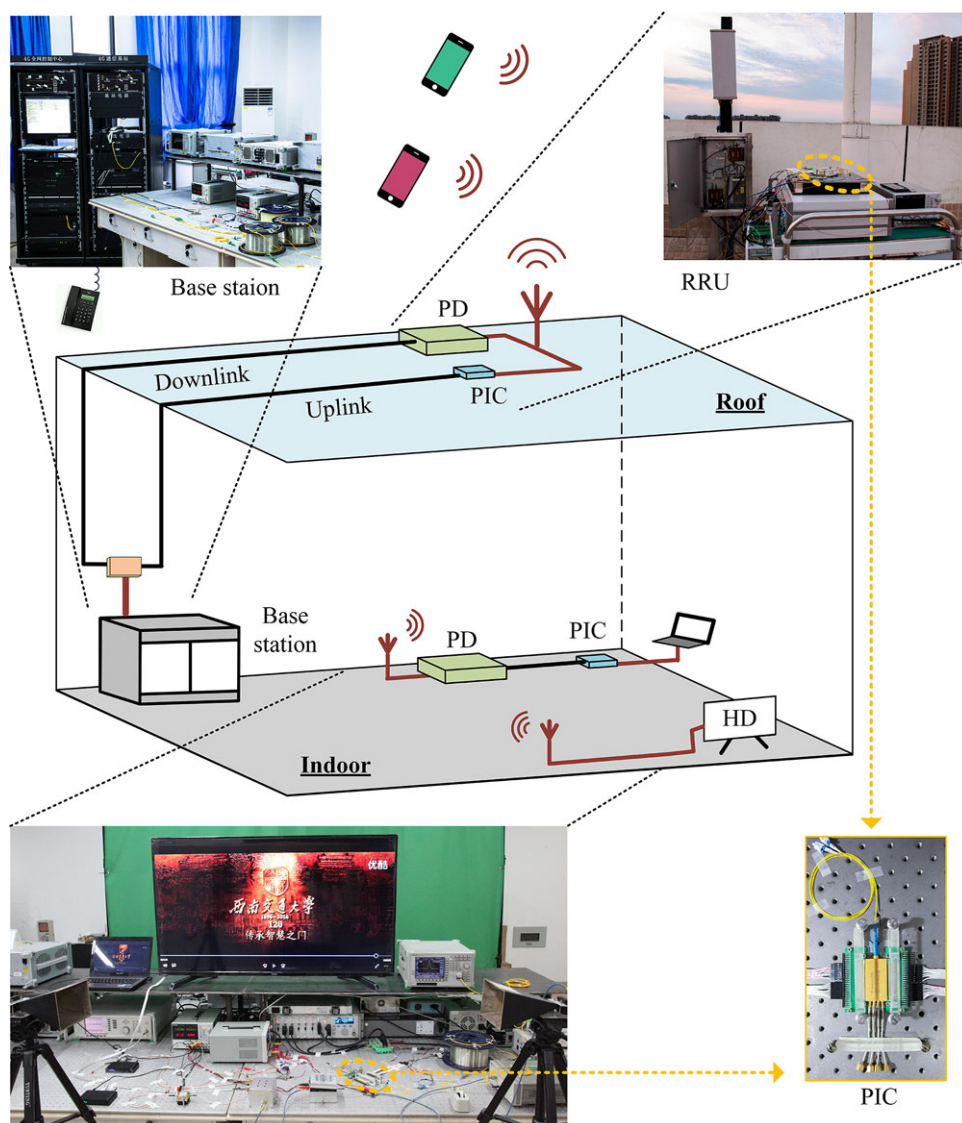


Figure 5. Field trials for broadband wireless communications (top) and remote HD video access (bottom), with the PIC-enabled microwave signal transmission. Videos about the two field trials can be found in Movies S2 and S3, Supporting Information. Inset: PIC installed in the two real-world application systems. (HD, high-definition video; PIC, photonic integrated circuit; RRU, remote radio unit).

microwave filter in the IM branch. As shown in Figure 3f, microwave frequency measurement has been realized within the range of 8.1–17.9 GHz without ambiguity, while frequency errors are estimated to be less than 120 MHz (see details in Section S8, Supporting Information).

For the measurement of the pulse repetition rate (PRR) or time-of-arrival (TOA) of a microwave signal,^[41] a system is designed by configuring the PIC with the IM and DBRL 1. The target microwave signal is remotely received by the PIC and transmitted to the central unit through a 10-km fiber. By incorporating a photodetector (PD) and a low-pass filter (or equivalently using a low-speed PD), the PRR can be measured in the central unit, totally independent of the carrier frequency. As shown in Figure 3g, the PRR at 10 MHz is successfully obtained from the target microwave signal without any prior information about the carrier frequency (8 or 12 GHz). Furthermore, the measurement

to other PRRs (e.g., 50 and 100 MHz) of microwave signals at 8 and 12 GHz has also been demonstrated in Figure S6, Supporting Information, while the carrier frequencies are unknown during the measurement.

More details about the seven functions referring to the three key domains of MWP can be found in Sections S3–S9, Supporting Information.

4. Real-World Applications in the Microwave Signal Transmission Domain

Besides the experiments demonstrated in laboratory above, the PIC is fully packaged and assembled to support a host of real-world applications for microwave signal generation, transmission, and processing in both indoor and outdoor scenarios for the

Table 2. Summary of the multifunctional PIC for the seven MWP functions.

MWP domain	Available function	Multifunctional elements and configurations	Laboratory tests	Real-world applications
Generation	Remote microwave signal generator	Ultrathin filter (DBRL); Phase modulation; Clockwise signal-flow.	☺	
Transmission	Analog intensity-modulation link	Tunable laser (DBRL); Intensity modulation; Clockwise signal-flow.	☺	☺ ^{a,b,c}
	Analog phase-modulation link	Tunable laser (DBRL); Phase modulation; Clockwise signal-flow.	☺	☺ ^a
Processing	Tunable bandpass filter	Bandpass amplifier (DBRL); Phase modulation; Anticlockwise signal-flow.	☺	
	Tunable bandstop filter	Tunable laser (DBRL); Intensity modulation; Clockwise signal-flow.	☺	
	Microwave frequency measurement system	Tunable laser (DBRL); Parallel modulation; Clockwise signal-flow.	☺	
	Pulse repetition rate measurement system	Tunable laser (DBRL); Intensity modulation; Clockwise signal-flow.	☺	

^a) High-speed railways; ^b) broadband wireless communications; ^c) remote HD video access.

first time. Concerning the microwave signal transmission using the PIC, in particular, the remote electromagnetic environment surveillance, broadband wireless communications, and remote HD video access have been demonstrated here.

4.1. Remote Electromagnetic Environment Surveillance along In-Service High-Speed Railways

With the rapid growth of in-service high-speed railways all over the world (e.g., 31 043 km in-service high-speed lines in China and totally 46 483 km in the world by March 19, 2019^[42]), real-time electromagnetic environment surveillance is of great significance to ensure the safety and high operation efficiency of the high-speed railway network (see discussions in Section S10, Supporting Information). Using the PIC, a photonic system is designed to monitor the electromagnetic environment and interferences in the global system for mobile communications-railway (GSM-R, a radio system widely used to support high-speed train control & dispatching function). As shown in Figure 4a–c, the multifunctional PIC is installed for implementing remote signal acquisition and transmission in either analog intensity-modulation or phase-modulation link, along the Chengdu-Chongqing High-speed Railway at a speed level of $\approx 300 \text{ km h}^{-1}$ in Southwest China. At each test point, the remotely acquired radio signal is transmitted over a 10-km single-mode fiber to a central unit (e.g., railway station) where it is identified and analyzed both in the frequency domain and the temporal domain with high resolution. The spectra of the acquired radio signals and the cell identification (CI) of the frequency bands are then obtained, as illustrated in Figure 4d,e. If no licensed CI is recognized (marked by “none” or “green arrows”), the radio components will be discriminated and alarmed as suspected adjacent-channel or out-of-band electromagnetic interferences (EMIs) from inter-modulation or foreign sources. Besides, the in-band or adjacent-channel interferences can also be effectively monitored from the eye and constellation diagrams, as the PIC is used for implementing remote microwave signal (GSM-R signal) acquisition and transmission. More results are shown in Figure S8, Supporting Information.

Consequently, based on the PIC-enabled function in the microwave signal transmission domain, a low-cost and real-time photonic system to electromagnetic environment surveillance

has been established for promoting the safety and efficiency of the high-speed railway network. This photonic system can also be seamlessly compatible with next-generation wireless communication system, for example, long-term evolution for railway (LTE-R). More details can be found in Section S10, Supporting Information and Movie S1, Supporting Information.

4.2. Broadband Wireless Communications and Remote HD Video Access

For the implementation of broadband wireless communications, the multifunctional PIC is embedded into a commercial time-division LTE (TD-LTE) system operating at 2.35 GHz, as shown on the top of Figure 5. It is installed in the remote radio unit (RRU) located on the roof of the college building, to transmit microwave signal in analog intensity-modulation link. Voice service between a cellular phone on the roof and a wired telephone connected to the base station, and video traffic between two cellular phones on the roof have been successfully demonstrated. (see Section S11, Supporting Information and Movie S2, Supporting Information)

To provide remote HD video access, the multifunctional PIC is installed to transmit microwave signal in analog intensity-modulation link, as shown on the bottom of Figure 5. At first, real-time HD video signal (source) is converted into an HD-SDI (high-definition serial digital interface) signal at a data rate of $1.485 \text{ Gbit s}^{-1}$ and then upconverted to 9.1 GHz. The upconverted microwave signal carrying the HD video is applied to the on-chip IM to modulate the optical carrier from DBRL 1, and then remotely dispatched to user terminal over a 5-km fiber and 1.5-m free space. At the user terminal, the received microwave signal is down-converted and demodulated to recover the HD video signal, offering a remote high-fidelity video access. (see Section S12, Supporting Information and Movie S3, Supporting Information).

5. Conclusion

We have proposed and demonstrated a multifunctional PIC for MWP. As listed in Table 2, the PIC has been designed to provide multiple fundamental microwave functions across the three key domains of MWP (i.e., microwave signal generation, transmission, and processing), not a single function as in

previous reports. They are compelling for a wide range of applications, including the remote microwave signal generator, analog intensity-modulation and phase-modulation MWP links, tunable microwave bandpass and bandstop filters, microwave frequency measurement, and pulse repetition rate measurement.

Then the PIC has been directly deployed for remote signal transmission in real-world MWP applications, such as electromagnetic environment surveillance for an in-service high-speed railway, broadband wireless communications, and remote HD video access. To the best of our knowledge (see the overview in Table 1), this work can be considered as the first demonstration to a multifunctional PIC for diverse applications across the microwave signal generation, transmission, and processing, as well as real-world applications integrated MWP in both indoor and outdoor scenarios.

Supporting Information

Supporting Information is available from the Wiley Online Library or from the author.

Acknowledgements

X.Z., F.Z., and Z.C. contributed equally to this work. This work was supported in part by European Research Council in Advanced Grant project BROWSE and Proof-of-Concept project BROWSE+, the Sichuan Science and Technology Program (2019JDJQ0022, 2018HH0002), the National Natural Science Foundation of China (61775185), the "111" Plan (B18045), and the National High Technology Research and Development Program of China (2015AA016903). X.Z. was supported by the Research Fellowship of the Alexander von Humboldt Foundation, Germany.

Conflict of Interest

The authors declare no conflict of interest.

Keywords

broadband wireless communications, electromagnetic environment surveillance, integrated microwave photonics, microwave signal generation/transmission/processing, photonic integrated circuits

Received: September 17, 2018

Revised: December 11, 2018

Published online: May 10, 2019

[1] A. J. Seeds, K. J. Williams, *J. Lightwave Technol.* **2006**, *24*, 4628.

[2] R. Minasian, *IEEE Trans. Microwave Theory Tech.* **2006**, *54*, 832.

[3] J. Capmany, D. Novak, *Nat. Photonics* **2007**, *1*, 319.

[4] T. Berceli, P. R. Herczfeld, *IEEE Trans. Microwave Theory Tech.* **2010**, *58*, 2992.

[5] Z. Jia, J. Yu, G. Ellinas, G. K. Chang, *J. Lightwave Technol.* **2007**, *25*, 3452.

[6] S. Koenig, D. Lopez-Diaz, J. Antes, F. Boes, R. Henneberger, A. Leuther, A. Tessmann, R. Schmogrow, D. Hillerkuss, R. Palmer, T. Zwick, *Nat. Photonics* **2013**, *7*, 977.

[7] P. Ghelfi, F. Laghezza, F. Scotti, G. Serafino, A. Capria, S. Pinna, D. Onori, C. Porzi, M. Scaffardi, A. Malacarne, V. Vercesi, *Nature* **2014**, *507*, 341.

[8] T. Nagatsuma, G. Ducournau, C. C. Renaud, *Nat. Photonics* **2016**, *10*, 371.

[9] X. Zou, B. Lu, W. Pan, L. Yan, A. Stöhr, J. Yao, *Laser Photonics Rev.* **2016**, *10*, 711.

[10] D. Marpaung, J. Yao, J. Capmany, *Nat. Photonics* **2019**, *13*, 80.

[11] L. R. Chen, *J. Lightwave Technol.* **2017**, *35*, 824.

[12] M. H. Khan, H. Shen, Y. Xuan, L. Zhao, S. Xiao, D. E. Leaird, A. M. Weiner, M. Qi, *Nat. Photonics* **2010**, *4*, 117.

[13] J. Wang, H. Shen, L. Fan, R. Wu, B. Niu, L. T. Varghese, Y. Xuan, D. E. Leaird, X. Wang, F. Gan, A. M. Weiner, *Nat. Commun.* **2015**, *6*, 5957.

[14] J. Hulme, M. J. Kennedy, R. L. Chao, L. Liang, T. Komljenovic, J. W. Shi, B. Szafraniec, D. Baney, J. E. Bowers, *Opt. Express* **2017**, *25*, 2422.

[15] X. Wu, K. Xu, W. Zhou, C. W. Chow, H. K. Tsang, *IEEE Photonics Technol. Lett.* **2017**, *29*, 1896.

[16] J. Tang, T. Hao, W. Li, D. Domenech, R. Baños, P. Muñoz, N. Zhu, J. Capmany, M. Li, *Opt. Express* **2018**, *26*, 12257.

[17] E. J. Norberg, R. S. Guzzon, J. S. Parker, L. A. Johansson, L. A. Coldren, *J. Lightwave Technol.* **2011**, *29*, 1611.

[18] B. Guan, S. S. Djordjevic, N. K. Fontaine, L. Zhou, S. Ibrahim, R. P. Scott, D. J. Geisler, Z. Ding, S. B. Yoo, *IEEE J. Sel. Top. Quantum Electron.* **2014**, *20*, 359.

[19] J. S. Fandiño, P. Muñoz, D. Doménech, J. Capmany, *Nat. Photonics* **2017**, *11*, 124.

[20] A. Meijerink, C. G. Roeloffzen, R. Meijerink, L. Zhuang, D. A. Marpaung, M. J. Bentum, M. Burla, J. Verpoorte, P. Jorna, A. Hulzinga, W. van Etten, *J. Lightwave Technol.* **2010**, *28*, 3.

[21] W. Shi, V. Veerasubramanian, D. Patel, D. Plant, *Opt. Lett.* **2014**, *39*, 701.

[22] X. Wang, L. Zhou, R. Li, J. Xie, L. Lu, K. Wu, J. Chen, *Optica* **2017**, *4*, 506.

[23] X. Xu, J. Wu, T. G. Nguyen, T. Moein, S. T. Chu, B. E. Little, R. Morandotti, A. Mitchell, D. J. Moss, *Photonics Res.* **2018**, *6*, B30.

[24] A. Khilo, S. J. Spector, M. E. Grein, A. H. Nejadmalayeri, C. W. Holzwarth, M. Y. Sander, M. S. Dahlem, M. Y. Peng, M. W. Geis, N. A. DiLello, J. U. Yoon, A. Motamedi, J. S. Orcutt, J. P. Wang, C. M. Sorace-Agaskar, M. A. Popovic, J. Sun, G. Zhou, H. Byun, J. Chen, J. L. Hoyt, H. I. Smith, R. J. Ram, M. Perrott, T. M. Lyszczarz, E. P. Ippen, F. X. Kartner, *Opt. Express* **2012**, *20*, 4454.

[25] L. Zhuang, C. G. Roeloffzen, M. Hoekman, K. J. Boller, A. J. Lowery, *Optica* **2015**, *2*, 854.

[26] W. Liu, M. Li, R. S. Guzzon, E. J. Norberg, J. S. Parker, M. Lu, L. A. Coldren, J. Yao, *Nat. Photonics* **2016**, *10*, 190.

[27] D. Pérez, I. Gasulla, L. Crudgington, D. J. Thomson, A. Z. Khokhar, K. Li, W. Cao, G. Z. Mashanovich, J. Capmany, *Nat. Commun.* **2017**, *8*, 636.

[28] D. A. B. Miller, *Photonics Res.* **2013**, *1*, 1.

[29] A. Choudhary, B. Morrison, I. Aryanfar, S. Shahnia, M. Pagani, Y. Liu, K. Vu, S. Madden, D. Marpaung, B. J. Eggleton, *J. Lightwave Technol.* **2017**, *35*, 846.

[30] W. Liu, W. Zhang, J. Yao, *J. Lightwave Technol.* **2017**, *35*, 2487.

[31] R. C. Hsu, A. Ayazi, B. Houshmand, B. Jalali, *Nat. Photonics* **2007**, *1*, 535.

[32] V. S. Ilchenko, A. B. Matsko, I. Solomatine, A. A. Savchenkov, D. Seidel, L. Maleki, *IEEE Photonics Technol. Lett.* **2008**, *20*, 1600.

[33] T. R. Clark, R. Waterhouse, *IEEE Microwave Mag.* **2011**, *12*, 87.

[34] F. van Dijk, G. Kervella, M. Lamponi, M. Chtioui, F. Lelarge, E. Vinet, Y. Robert, M. J. Fice, C. C. Renaud, A. Jimenez, G. Carpintero, *IEEE Photonics Technol. Lett.* **2014**, *26*, 965.

- [35] X. Zou, W. Bai, W. Chen, P. Li, B. Lu, G. Yu, W. Pan, B. Luo, L. Yan, L. Shao, *J. Lightwave Technol.* **2018**, 36, 4337.
- [36] J. S. Fandiño, P. Muñoz, *Opt. Lett.* **2013**, 38, 4316.
- [37] M. Pagani, B. Morrison, Y. Zhang, A. Casas-Bedoya, T. Aalto, M. Harjanne, M. Kapulainen, B. J. Eggleton, D. Marpaung, *Optica* **2015**, 2, 751.
- [38] M. Burla, X. Wang, M. Li, L. Chrostowski, J. Azaña, *Nat. Commun.* **2016**, 7, 13004.
- [39] M. P. Chang, E. C. Blow, M. Z. Lu, J. J. Sun, P. R. Prucnal, *IEEE Trans. Microwave Theory Tech.* **2018**, 66, 596.
- [40] A. J. Ward, D. J. Robbins, G. Busico, E. Barton, L. Ponnampalam, J. P. Duck, N. D. Whitbread, P. J. Williams, D. C. Reid, A. C. Carter, M. J. Wale, *IEEE J. Sel. Top. Quantum Electron.* **2005**, 11, 149.
- [41] J. B. Tsui, *Microwave Receivers with Electronic Warfare Applications*, Wiley, New York **1986**, Ch. 3.
- [42] International Union of Railways (UIC), *High speed lines in the world (summary)*. Available at https://uic.org/IMG/pdf/20190319_high_speed_lines_in_the_world.pdf (March 19, **2019**). Accessed: March 31, **2019**.