

# Temperature-programmed reduction of Al2O3-, SiO2-, and carbon-supported Re2O7 catalysts

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## Temperature-Programmed Reduction of Al<sub>2</sub>O<sub>3</sub>-, SiO<sub>2</sub>-, and Carbon-Supported Re<sub>2</sub>O<sub>7</sub> Catalysts

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Temperature-Programmed Reduction (TPR) has been applied to characterize the reducibility of  $Al_2O_3$ -,  $SiO_2$ -, and carbon-supported  $Re_2O_7$  catalysts, over a wide range of transition metal content. Dried catalysts are found to contain a so-called monolayer-type  $Re^{7+}$  surface phase as well as crystalline  $NH_4ReO_4$ . Calcination at 575 or 825 K resulted in decomposition of  $NH_4ReO_4$ , formation of the  $Re^{7+}$  surface phase and  $Re_2O_7$  clusters, and Re loss via sublimation of  $Re_2O_7$ . Differences in reducibility of the various catalyst samples are ascribed to variations in the strength and the heterogeneity of the  $Re^{7+}$ -support interaction. The strength of the interaction was found to depend on the support material applied and decreased in the order:  $Al_2O_3 > SiO_2 >$  carbon. The heterogeneity was essentially the same for all three supports. The largely varying literature data on the reducibility of  $Re_2O_7/Al_2O_3$  catalysts is supposedly related with the presence of additives, such as chlorides, which may increase the  $Re^{7+}$ -support interaction. © 1985 Academic Press, Inc.

### INTRODUCTION

Rhenium catalysts have several interesting properties. They show high activity for metathesis (1, 2), hydrodesulfurization (HDS) (3-6), and hydrodenitrogenation (7), in comparison with Mo and W catalysts. Re also increases the stability of Pt reforming catalysts (8-11) and, for a large range of organic syntheses, Re appears to be a selective hydrogenation catalyst (12).

The present study describes the reducibility, as measured by Temperature-Programmed Reduction (TPR), of Al<sub>2</sub>O<sub>3</sub>-, SiO<sub>2</sub>-, and carbon-supported Re<sub>2</sub>O<sub>7</sub> catalysts as a function of Re content and calcination conditions. The TPR technique was chosen for two reasons. First, TPR provides information on the reducibility, as such, over a wide range of temperatures. Second, TPR patterns give indications on the structure of catalysts, e.g., on the pres-

ence of crystallites and on the metal-oxygen bond strength.

Detailed information on the reducibility, as such, is important, because catalytically active Re sites are only created by reduction of the Re<sup>7+</sup> ions, generally present in freshly prepared catalysts, to lower valencies, as occurs in the formation of Re carbenes (metathesis) (13),  $ReS_2$  (HDS) (3), or Re metal (hydrogenation, reforming). Studies carried out on the reduction of Re<sup>7+</sup> by H<sub>2</sub> mainly deal with reforming catalysts. Initially, reduction has been studied isothermally (14, 15). Subsequently, the TPR method (16) has been used frequently (4, 17-22). It is well established now that reduction results in conversion of Re<sup>7+</sup> to Re metal in a narrow temperature range. However, as will be shown in the present study, the reported reduction temperatures vary to a large extent. It was thought that a more systematic study of the reduction of supported Re<sub>2</sub>O<sub>7</sub> catalysts might reveal the origin of the inconsistencies in the literature data.

The present TPR study is also part of a

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larger investigation which has the objective to correlate the HDS activity of sulfided Re catalysts with the structure of the oxidic precursor systems (5). The latter project focuses on the influence of type of support, by analogy with recent work on the reducibility and HDS activity of Al<sub>2</sub>O<sub>3</sub>-, SiO<sub>2</sub>-, and carbon-supported Mo and W catalysts (4, 23, 24).

#### **EXPERIMENTAL**

### a. Materials

NH<sub>4</sub>ReO<sub>4</sub> (Drijfhout, "for analysis") and ReO<sub>3</sub> (ICN), being XRD-pure, were used as received. Re<sub>2</sub>O<sub>7</sub> was prepared in situ by oxidation of ReO<sub>3</sub> in dry air followed by purification via sublimation. The following support materials were applied: High-purity  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> (Ketjen 000-1. 5E (CK 300), specific surface area 195 m<sup>2</sup>/g, pore volume  $0.50 \text{ cm}^3/\text{g}$ , particle size  $100-150 \mu\text{m}$ , chlorine content 0.04 wt%); SiO<sub>2</sub> (Grace 62, specific surface area 350 m<sup>2</sup>/g, pore volume 1.05 cm<sup>3</sup>/g, particle size 160–210  $\mu$ m); and activated carbon (Norit RO-3, specific surface area 1000 m<sup>2</sup>/g, pore volume 0.8 cm<sup>3</sup>/g, particle size 175-300  $\mu$ m). The activatedcarbon support was purified by a treatment with boiling HCl (1 h), followed by washing with boiling H<sub>2</sub>O and drying in air (16 h, 380 K). The remaining impurity level was low; X-ray fluorescence showed presence of chlorine, sulfur, and silicon.

### b. Catalyst Preparation

The supported Re catalysts were prepared by pore volume impregnation of dried supports with solutions of NH<sub>4</sub>ReO<sub>4</sub> in demineralized H<sub>2</sub>O. The samples so obtained were dried, in air at 1 bar, by heating to 380 K at a rate of 20 K/h, followed by a 16-h isothermal period at 380 K. In some cases a 0.5-h calcination was applied, at 575 or 825 K. The medium used was air for Al<sub>2</sub>O<sub>3</sub>and SiO<sub>2</sub>-supported systems, whereas it was air (at 575 K) or Ar (at 575 or 825 K) for carbon-supported systems. The gases were purified in order to prevent carbon deposition on the catalysts. The Re content was varied drastically. High-loading catalysts were prepared by repeated pore volume impregnation and drying. Table 1 gives the Re content of the dried catalysts and also shows for which samples the presence of crystalline NH<sub>4</sub>ReO<sub>4</sub> was established by means of XRD and TPR analysis. The catalysts are denoted as Re(x)/y, with x representing the theoretical Re content, expressed as the number of Re atoms per square nanometer support surface area (at./nm<sup>2</sup>), and y representing the support material using the abbreviations Al, Si, and C for the  $Al_2O_3$ ,  $SiO_2$ , and carbon supports, respectively. Atomic absorption spectrometry (Perkin-Elmer 300 AAS) was applied to check the theoretical Re content of dried catalysts (see Table 1) and to measure the Re loss due to calcination (see Table 2).

### c. X-Ray Diffraction (XRD)

XRD has been carried out in a Philips diffractometer PW 1050/25 using  $CuK\alpha$  radiation. A Ni filter was applied to remove  $CuK\beta$  radiation. Crystallite sizes have been calculated using the Scherrer equation with correction for natural line broadening and assuming that the crystallite-shape factor K equals 1 (25).

### d. Temperature-Programmed Reduction (TPR)

The TPR equipment has been described in detail elsewhere (26). A high-purity mixture of 67% H<sub>2</sub>/Ar (flow rate 12  $\mu$ mol/s; 1.0 bar) was used. In some cases this mixture was saturated with H<sub>2</sub>O at room temperature, resulting in 2.6% H<sub>2</sub>O in the reducing mixture. In a typical TPR experiment the heating rate was 10 K/min and the catalyst sample contained 2–5  $\mu$ mol Re. The sample size was varied reciprocally with heating rate. H<sub>2</sub>O, NH<sub>3</sub>, CO<sub>2</sub>, and organics (except CH<sub>4</sub>), which evolved during reduction, were trapped in 3A and 5A molecular sieve columns. H<sub>2</sub> consumption as well as CH<sub>4</sub>, CO, and O<sub>2</sub> production were measured as a positive peak by means of a thermal con-

TABLE 1
Dried Catalysts

Catalyst notation <sup>a</sup>	Theoretical Re content (wt% Re) <sup>b</sup>	Number of impregnation steps	Re content (AAS) <sup>c</sup> (at./nm <sup>2</sup> )	Crystalline NH <sub>4</sub> ReO <sub>4</sub> <sup>d</sup>		Crystallite size <sup>c,e</sup> of NH <sub>4</sub> ReO <sub>4</sub>
				(TPR)	(XRD)	(nm)
Re(0.0097)/A1	0.058	1	n.m.	-	_	n.m.
Re(0.025)/Al	0.147	1	n.m.	_	_	n.m.
Re(0.049)/Al	0.29	1	n.m.	_	_	n.m.
Re(0.097)/AI	0.58	1	n.m.	_	_	n.m.
Re(0.24)/Al	1.44	1	0.19	_		n.m.
Re(0.49)/Al	2.8	2	0.41	_	_	n.m.
Re(0.97)/Al	5.4	4	0.91	+	+	130
Re(2.43)/Al	12.1	10	2.61	+	+	260
Re(0.010)/Si	0.108	1	n.m.	_	_	n.m.
Re(0.025)/Si	0.27	1	n.m.	_	-	n.m.
Re(0.050)/Si	0.54	1	n.m.	_	_	n.m.
Re(0.10)/Si	1.07	1	n.m.	_	+	70
Re(0.25)/Si	2.6	1	0.24	+	+	110
Re(0.50)/Si	5.0	2	0.49	+	+	170
Re(1.00)/Si	9.4	3	0.97	+	+	170
Re(2.50)/Si	19.5	7	2.85	+	+	200
Re(0.0080)/C	0.25	1	n.m.	_	_	n.m.
Re(0.040)/C	1.22	1	n.m.	_	_	n.m.
Re(0.20)/C	5.7	1	n.m.	+	_	n.m.
Re(0.38)/C	10.7	2	0.36	+	_	n.m.
Re(0.80)/C	18.2	4	0.73	+	+	n.m.

<sup>&</sup>lt;sup>a</sup> Theoretical Re content (at./nm²) is given in parentheses; Al, Si and C refer to Al<sub>2</sub>O<sub>3</sub>, SiO<sub>2</sub>, and carbon, respectively.

TABLE 2
Effect of Calcination in Air on the Re Content

Catalyst notation <sup>a</sup>	Re content <sup>b</sup> after drying (380 K) (at./nm <sup>2</sup> )	Re content <sup>b</sup> after calcination (575 K) (at./nm <sup>2</sup> )	Re content <sup>b,c</sup> after calcination (825 K) (at./nm <sup>2</sup> )
Re(0.49)/Al	0.42	0.39	n.m.
Re(0.97)/Al	0.91	0.81	n.m.
Re(2.43)/Al	2.61	2.45	n.m.
Re(0.50)/Si	0.49	0.49	0.46
Re(1.00)/Si	0.97	0.94	0.93
Re(2.50)/Si	2.85	2.46	1.63
Re(0.38)/C	0.36	0.36	n.m.
Re(0.80)/C	0.73	1.20	n.m.

<sup>&</sup>lt;sup>a</sup> For catalyst notation see footnote of Table 1.

<sup>&</sup>lt;sup>b</sup> Re is assumed to be present in the stoichiometry NH<sub>4</sub>ReO<sub>4</sub>.

 $<sup>^{</sup>c}$  n.m. = not measured.

<sup>&</sup>lt;sup>d</sup> The presence or absence of crystalline NH<sub>4</sub>ReO<sub>4</sub>, derived from TPR and XRD data, is indicated by a plus and a minus sign, respectively.

<sup>&</sup>lt;sup>e</sup> Calculated from XRD results.

<sup>&</sup>lt;sup>b</sup> Measured by AAS.

c n.m. = not measured.

ductivity detector (TCD). A flame ionization detector (FID) was used for CH<sub>4</sub> detection only. CH<sub>4</sub> and CO were retarded by the 5A molecular sieves, to an extent which depended on the H<sub>2</sub>O content of the zeolite surface. The retardation times for CH4 and CO were 2.5 and 4.2 min, respectively (for TPR measurements on reference compounds and Al<sub>2</sub>O<sub>3</sub>- or SiO<sub>2</sub>-supported catalysts), or 4.5 and 18 min, respectively (for TPR measurements on carbon-supported catalysts). Since the TPR patterns shown in Figs. 1–9 have not been corrected for these retardations, the CH<sub>4</sub> production peak is situated at a somewhat too high temperature (with a heating rate of 10 K/min and a retardation time of 2.5 min the peak shift is about 25 K).

### **RESULTS**

### a. X-Ray Diffraction

The Al<sub>2</sub>O<sub>3</sub>- and SiO<sub>2</sub>-supported catalysts show very broad XRD lines of  $\gamma$ - or  $\eta$ -Al<sub>2</sub>O<sub>3</sub> and  $\alpha$ -crystobalite, respectively. The carbon-supported catalysts show very broad XRD lines at d values around 210 and 370 pm, which are typical for activated carbon; moreover, sharper lines are observed at d values of 335 (graphite impurities) and 405 pm (origin unknown). Depending on the type of support and the Re content some dried catalysts show NH<sub>4</sub>ReO<sub>4</sub> lines, superimposed on the support pattern (see Table 1). Dried Re(0.0097-0.49)/Al samples do not show any NH<sub>4</sub>ReO<sub>4</sub> lines; for dried Re(0.97)/Al, sharp NH<sub>4</sub>ReO<sub>4</sub> lines of low intensity are observed (crystallite size 130 nm), while for dried Re(2.43)/Al these lines are of much higher intensity (crystallite size 260 nm). Dried Re(0.10-2.50)/Si catalysts show sharp NH<sub>4</sub>ReO<sub>4</sub> lines, the intensity of which increases regularly with increasing Re content, whereas the crystallite size increases from 70 to 200 nm. For carbon-supported catalysts NH<sub>4</sub>ReO<sub>4</sub> lines, of very low intensity, are observed only for the dried Re(0.80)/C sample. Calcination of Al<sub>2</sub>O<sub>3</sub>-, SiO<sub>2</sub>-, and carbon-supported catalysts at 575 or 825 K leads to disappearance of the NH<sub>4</sub>ReO<sub>4</sub> lines, with the exception of Re(2.50)/Si. In the latter case, after calcination at 575 K, NH<sub>4</sub>ReO<sub>4</sub> lines are still present, although they are reduced sharply in intensity. Besides NH<sub>4</sub>ReO<sub>4</sub>- and support-lines, both dried and calcined Re(0.25–2.50)/Si catalysts show additional lines of low intensity with d values of 318 and 486 pm. These lines could not be assigned to Re<sub>2</sub>O<sub>7</sub> (27), Re<sub>2</sub>O<sub>7</sub> · 2H<sub>2</sub>O (28), nor to any Re compound included in the ASTM system, but for obvious candidates, namely Re silicates, no ASTM data are available.

### b. Colors

All Al<sub>2</sub>O<sub>3</sub>-supported catalysts are white, independent of calcination temperature. SiO<sub>2</sub>-supported catalysts are white after drying. Calcination at 575 K changes the color to light grey-blue (Re(0.25)/Si), dark grey-blue (Re(0.50)/Si),and (Re(1.00-2.50)/Si). Calcination at 825 K leads to recovery of the white color. In separate experiments, in which the Re(2.50)/Si sample was calcined in air at various temperatures, it is observed that coloring starts around 500 K. The color disappears around 600 K, while simultaneously Re<sub>2</sub>O<sub>7</sub> sublimation takes place.

### c. Temperature-Programmed Reduction

Figures 1–9 show the TPR data. In all TPR patterns the Re reduction peaks are sharp, while quantitative analysis of TPR results generally indicates a single-step reduction from Re<sup>7+</sup> (Re<sup>6+</sup> in the case of ReO<sub>3</sub>) to Re<sup>0</sup>. Once Re<sup>0</sup> is formed, considerable CH<sub>4</sub> production is found in most cases, due to reduction of organic impurities, adsorbed on Re catalysts and on the quartz wool plugs around the samples. About 1.2 mol H<sub>2</sub> per CH<sub>4</sub> is consumed, in agreement with the conclusion drawn previously that these organics consist of (polymerized) acetone (26).

Figure 1 shows the TPR patterns of crystalline reference compounds. The reducibility increases in the order: NH<sub>4</sub>ReO<sub>4</sub> <

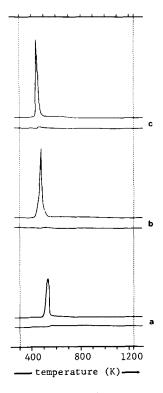


FIG. 1. TPR patterns (1 K/min) of reference compounds: (a) NH<sub>4</sub>ReO<sub>4</sub>, (b) Re<sub>2</sub>O<sub>7</sub>, (c) ReO<sub>3</sub>. The upper and lower part of each pattern represent the TCD and FID signals, respectively.

 $Re_2O_7 < ReO_3$ . For TPR analysis of NH<sub>4</sub>ReO<sub>4</sub> and ReO<sub>3</sub> exceptionally small samples have been used (ca. 5  $\mu$ -mol Re at a heating rate of 1 K/min); larger samples (especially in the case of NH<sub>4</sub>ReO<sub>4</sub>) showed TPR peak broadening toward higher temperatures due to inhibition of reduction by NH<sub>3</sub> or H<sub>2</sub>O. For Re<sub>2</sub>O<sub>7</sub> the influence of sample size on TPR has not been checked because of its time-consuming in situ preparation procedure. In order to limit Re<sub>2</sub>O<sub>7</sub> sublimation (29) during TPR analysis, the crystalline compounds were heated at a rate of 1 K/min. TPR of Re<sub>2</sub>O<sub>7</sub> at 10 K/min shows the reduction maximum at higher temperature (565 K) and a significant sublimation of Re<sub>2</sub>O<sub>7</sub>, in agreement with literature (17).

Figure 2 gives a survey of the position of the TPR peak maxima  $(T_{max})$ , due to reduc-

tion of Re ions in supported Re catalysts.  $T_{\rm max}$  values are given as a function of support, calcination, and Re content. The corresponding TPR patterns (10 K/min) are shown in the Figs. 3 and 5–9. For all three supports two lines can be drawn:

- (i) Most peaks observed in the range 540–560 K for dried catalysts with high Re contents are assigned to reduction of NH<sub>4</sub>ReO<sub>4</sub> crystallites (see also Table 1).
- (ii) All other peaks, found over the temperature range 510–730 K, are assigned to reduction of Re<sup>7+</sup> surface ions which interact with the support.

The NH<sub>4</sub>ReO<sub>4</sub> reduction peak has its  $T_{\rm max}$  value at slightly lower temperatures in the case of carbon-supported catalysts (540 K) than in the case of Al<sub>2</sub>O<sub>3</sub>- or SiO<sub>2</sub>-supported catalysts (560 K), probably due to the different crystallite sizes involved. NH<sub>4</sub>ReO<sub>4</sub>

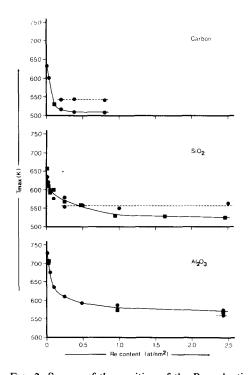


FIG. 2. Survey of the position of the Re reduction peak maxima ( $T_{\text{max}}$ ), at 10 K/min, as a function of Re content of catalysts supported on Al<sub>2</sub>O<sub>3</sub>, SiO<sub>2</sub>, or carbon, which are dried at 380 K (circles) or calcined at 575 or 825 K (squares). The dotted lines represent reduction of NH<sub>4</sub>ReO<sub>4</sub> crystallites; the full lines represent reduction of Re<sup>7+</sup> surface species.

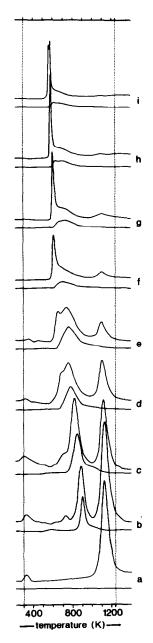


Fig. 3. TPR patterns (10 K/min) of dried  $Re_2O_7/Al_2O_3$  catalysts having the following Re contents (at./nm²): (a) 0, (b) 0.0097, (c) 0.025, (d) 0.049, (e) 0.097, (f) 0.24, (g) 0.49, (h) 0.97, (i) 2.43. The upper and lower part of each pattern represent the TCD and FID signals, respectively.

crystallites are observed at much lower Re content for SiO<sub>2</sub>- and carbon-supported than for Al<sub>2</sub>O<sub>3</sub>-supported catalysts. Calcination results in decomposition of

NH<sub>4</sub>ReO<sub>4</sub> and formation of more Re<sup>7+</sup> surface species, but does not significantly change the reduction temperature of the surface species. The  $T_{\rm max}$  values for reduction of Re<sup>7+</sup> surface species decrease with increasing Re content for all supports, but are higher for Al<sub>2</sub>O<sub>3</sub>-supported than for SiO<sub>2</sub>- or carbon-supported catalysts over the entire Re loading range studied. The shape of the curves shown in Fig. 2 for the latter reduction is different for each support, whereas the total shift of  $T_{\rm max}$  is only slightly larger for Al<sub>2</sub>O<sub>3</sub>-supported than for SiO<sub>2</sub>- or carbon-supported catalysts, namely ca. 155 and 125 K, respectively.

Besides Re<sup>7+</sup> reduction, the TPR patterns of supported catalysts show also other common features:

- (i) Just above room temperature, a peak is found which is probably caused by O<sub>2</sub> desorption from the support surface.
- (ii) Production of CH<sub>4</sub> (FID) and H<sub>2</sub> (negative TCD signal) in the range 400-650 K indicates that some cracking of organic impurities occurs at temperatures where Re<sup>0</sup> is not yet formed (see Figs. 3b-e and 6b-c).
- (iii) CH<sub>4</sub> production peaks, due to reduction of organic impurities, are found in the range 580-870 K and shift to lower temperature with increasing Re content, apparently due to the concomitant shift of the Re<sup>7+</sup> reduction peaks to lower temperature which results in Re<sup>0</sup> formation.
- (iv) In the high-temperature part of the TPR patterns, each support is found to have a characteristic TPR pattern.

Figure 3 shows the TPR patterns of dried Al<sub>2</sub>O<sub>3</sub>-supported catalysts as a function of Re content. At low Re contents the TPR patterns are dominated by peaks which are not related to reduction of Re ions. Besides CH<sub>4</sub> production, a peak near 1100 K is found, assigned to reduction of Al<sub>2</sub>O<sub>3</sub> impurities, such as iron, sulfite, and sulfate (26). The latter shifts ca. 50 K to lower temperatures with increasing Re content, suggesting that this reduction is catalyzed by Re.

Figure 4 shows the TCD part of the TPR patterns obtained for dried Al<sub>2</sub>O<sub>3</sub>-supported

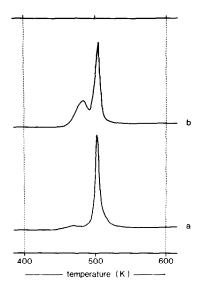


FIG. 4. TPR patterns (0.2 K/min) of dried  $Re_2O_7/Al_2O_3$  catalysts having the following Re contents (at./nm²): (a) 0.97, (b) 2.43. Only the TCD part of the patterns is shown.

catalysts having the two highest Re contents. Note that, in this case, the heating rate was 0.2 instead of 10 K/min. Clearly two peaks are present, one around 505 K due to reduction of Re7+ surface ions and another at about 475 K caused by reduction of NH<sub>4</sub>ReO<sub>4</sub> crystallites. At the lower heating rate (0.2 K/min) these peaks are better resolved and the distribution of Re7+ over the two phases can be calculated easily. Approximately 9 and 40% of the Re ions is present as NH<sub>4</sub>ReO<sub>4</sub> crystallites, corresponding to a concentration of Re<sup>7+</sup> surface phase of about 0.88 and 1.46 at./nm<sup>2</sup> in the dried Re(0.97)/Al and Re(2.43)/Al catalyst, respectively. Separate TPR experiments showed that the NH<sub>4</sub>ReO<sub>4</sub> TPR peak intensity decreases slightly with increasing heating rate, due to some decomposition of NH<sub>4</sub>ReO<sub>4</sub> during TPR.

Figure 5 shows the TPR patterns of Re(2.43)/Al as a function of calcination temperature. Calcination leads to disappearance of the NH<sub>4</sub>ReO<sub>4</sub> reduction peak and to a 10 K shift of the peak due to reduction of the remaining Re<sup>7+</sup> surface phase to lower temperature. The latter effect has

also been found for the other Re/Al samples. In order to check the possible influence of  $H_2O$  on the reducibility, some TPR analyses of dried Re(0.97)/Al have been executed using  $H_2O$ -saturated  $H_2/Ar$  as reducing mixture. The addition of  $H_2O$  causes a shift of ca. 10 K to higher temperature for the peak due to reduction of  $Re^{7+}$  surface ions.

For the  $Al_2O_3$ -supported catalysts no  $Re_2O_7$  deposition has been observed in colder parts of the calcination reactor, showing that no Re loss takes place during calcination. AAS- and quantitative TPR-results are in agreement with this.

Figure 6 shows the TPR patterns of dried SiO<sub>2</sub>-supported catalysts as a function of Re content. Besides Re<sup>7+</sup> reduction and CH<sub>4</sub> production, a reduction pattern is observed between 800 and 1200 K, which is

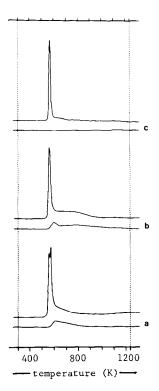


Fig. 5. TPR patterns (10 K/min) of the Re(2.43)/Al catalyst as a function of calcination temperature: (a) 380 K (drying), (b) 575 K, (c) 825 K. The upper and lower part of each pattern represent the TCD and FID signals, respectively.

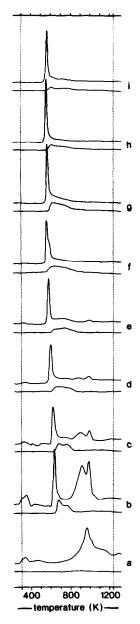


FIG. 6. TPR patterns (10 K/min) of dried  $Re_2O_7/SiO_2$  catalysts having the following Re contents (at./nm²): (a) 0, (b) 0.010, (c) 0.025, (d) 0.050, (e) 0.10, (f) 0.25, (g) 0.50, (h) 1.00, (i) 2.50. The upper and lower part of each pattern represent the TCD and FID signals, respectively.

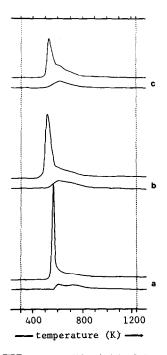
typical for the  $SiO_2$  support. As in the  $Al_2O_3$  case, it is assigned to reduction of impurities. Again, one concludes that Re catalyzes this reduction, since its presence causes the appearance of a second distinct

maximum in the SiO<sub>2</sub> reduction pattern as well as a shift to lower reduction temperatures.

Figure 7 shows the TPR patterns of Re(2.50)/Si as a function of calcination temperature. AAS and quantitative TPR analysis show that Re loss takes place, especially upon calcination at 825 K. Calcination results in some TPR peak broadening; this is also observed for Re(0.50–1.00)/Si. At lower Re contents no significant calcination effects are observed.

Figure 8 shows the TPR patterns of dried carbon-supported catalysts as a function of Re content. The Re reduction peaks are small compared with those caused by gasification of the support. Three different gasification regions can be discerned, in the broad temperature range of 500-1240 K:

1. The first region (500-900 K) represents pyrolysis of the activated carbon. At low Re content this is observed as production of



Ftg. 7. TPR patterns (10 K/min) of the Re(2.50)/Si catalyst as a function of calcination temperature: (a) 380 K (drying), (b) 575 K, (c) 825 K. The upper and lower part of each pattern represent the TCD and FID signals, respectively.

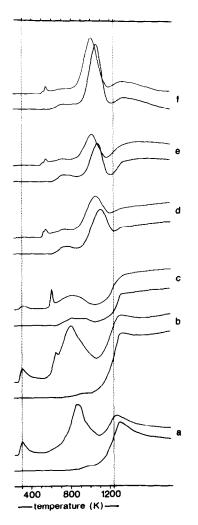


FIG. 8. TPR patterns (10 K/min) of dried Re<sub>2</sub>O<sub>7</sub>/carbon catalysts having the following Re contents (at./nm<sup>2</sup>): (a) 0, (b) 0.0080, (c) 0.040, (d) 0.20, (e) 0.38, (f) 0.80. The upper and lower part of each pattern represent the TCD and FID signals, respectively.

CO and consumption of H<sub>2</sub> (CO<sub>2</sub> and H<sub>2</sub>O production cannot be detected in the TPR apparatus). At higher Re contents CH<sub>4</sub> production dominates; this CH<sub>4</sub> probably is formed from the primary pyrolysis products CO and CO<sub>2</sub>, since it was shown in separate experiments that CO and CO<sub>2</sub> are converted quantitatively to CH<sub>4</sub> over Re<sup>0</sup> centers, under the TPR conditions applied.

2. The second region (900-1100 K) can only be distinguished in the TPR patterns recorded for the Re(0.20-0.80)/C catalysts

as a relatively sharp peak which is associated with strongly catalyzed gasification. Apparently this type of gasification is deactivated fast at temperatures around 1100 K.

3. The third region (above 1100 K) represents weakly catalyzed gasification. During the isothermal reduction stage some activation of this type of catalysis occurs at low Re contents, whereas at higher Re contents an activity decrease is observed, probably due to carbon shortage at high burn-off.

Re-catalyzed gasification has hardly been studied (30). More work has been done on the Ni-catalyzed gasification (31-33). Re and Ni seem to act similarly in catalytic gasification. Accordingly, it is proposed that gasification in the second region is catalyzed by Re<sup>0</sup> crystallites. The deactivation observed at the high-temperature side of this region might be caused by carbon deposition on the Re<sup>0</sup> phase, by Re carbide formation or by loss of dispersion because of Re<sup>0</sup> crystallite growth. The remaining gasification activity observed in the third region is then associated with (partially) covered Re<sup>0</sup> crystallites or with Re carbide. Redispersion of these Re phases assumedly accounts for the reactivation of gasification in the isothermal reduction stage.

Figure 9 shows the TPR patterns of Re(0.20)/C as a function of calcination temperature and medium. Calcination at 575 and 825 K leads to decomposition of NH<sub>4</sub>ReO<sub>4</sub> followed by significant Re<sub>2</sub>O<sub>7</sub> sublimation (40 and 55% Re loss, respectively), but does not affect gasification in region two and three. This can be explained assuming that NH<sub>4</sub>ReO<sub>4</sub> crystallites are precursors of relatively large Re<sup>0</sup> crystallites having a low gasification activity. The increase of Re content upon calcination, especially for the Re(0.80)/C catalyst (see Table 2), shows that also carbon loss takes place, obviously via catalytic oxidation. Moreover, the oxygen content of the carbon is influenced by the calcination medium, since calcination in air and Ar lead to an increase and decrease of pyrolysis activity, respectively. The small peak at 475 K,

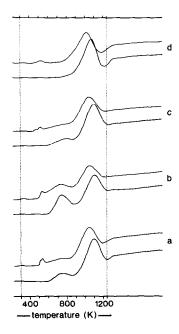


FIG. 9. TPR patterns (10 K/min) of the Re(0.20)/C catalyst as a function of temperature treatment and medium: (a) 380 K, air (drying), (b) 575 K, air, (c) 575 K, Ar, (d) 825 K, Ar. The upper and lower part of each pattern represent the TCD and FID signals, respectively.

observed only after heating at 575 K in Ar, is assigned to reduction of some partly reduced Re phase, e.g., ReO<sub>3</sub> crystallites.

### DISCUSSION

### a. Preparation and Structure of Oxidic Re Catalysts

All TPR patterns reported here show sharp peaks connected with a one-step reduction of high-valent Re ions with formation of mainly Re<sup>0</sup>. The sharpness of the peaks suggests strongly that autocatalysis plays an important role in the reduction mechanism (34). In agreement with this, it has been reported that reduction of Re<sup>7+</sup> can be accelerated by the presence of Re<sup>0</sup> and Pt<sup>0</sup> (17, 20). In addition, if autocatalysis is indeed an important factor, it can be easily understood why the observed reduction peaks are sharper than one would expect on the grounds of peak width calculations, carried out assuming that the

reducibility of a Re catalyst is the sum of intrinsic reducibilities of all Re ions present (for this calculation the curves of Fig. 2 can be used). Finally, for Al<sub>2</sub>O<sub>3</sub>-supported catalysts the activation energy value for reduction of Re<sup>7+</sup> surface species is only slightly higher than the value for reduction of NH<sub>4</sub>ReO<sub>4</sub> crystallites (111 versus 95 kJ/mol), again suggesting autocatalysis (35).

Dried catalysts. TPR shows the presence of NH<sub>4</sub>ReO<sub>4</sub> crystallites in dried catalysts. Generally the TPR data agree well with the XRD data with respect to the presence of NH<sub>4</sub>ReO<sub>4</sub> (see Table 1). Except for Re(0.10)/Si, which contains a very small fraction of crystalline NH<sub>4</sub>ReO<sub>4</sub>, TPR is more sensitive than XRD; TPR has the advantage of enabling both detection of small crystallites, such as are present in Re(0.20–0.80)/C samples, and quantification of the fraction of crystalline material formed.

By means of quantitative TPR analysis, the capacity of the supports to bond ReO<sub>4</sub> ions during impregnation and drying, with formation of Re<sup>7+</sup> surface species, is determined to be 0.05, 0.05, and 0.8 at./nm<sup>2</sup> for carbon, SiO<sub>2</sub>, and Al<sub>2</sub>O<sub>3</sub>, respectively. The SiO<sub>2</sub> and carbon values are very small. However, even in the Re/Al case, the capacity is small in comparison with the monolayer capacity of 3.3 at./nm<sup>2</sup> obtained for calcined catalysts (36). The strength of the interaction of ReO<sub>4</sub> ions with the Al<sub>2</sub>O<sub>3</sub> (and the NH<sub>4</sub>ReO<sub>4</sub>) lattice might be similar, leading to competition between formation of Re7+ surface species and NH<sub>4</sub>ReO<sub>4</sub> crystallites. The formation of the Re<sup>7+</sup> surface phase during impregnation and drying can probably be favored by adjustment of the pH of the impregnation solution to lower values, in order to increase the positive charge density at the support surface (37, 38).

The fact that the carbon-supported NH<sub>4</sub>ReO<sub>4</sub> crystallites could not be detected by XRD implies that their size is small (<3 nm). For the Al<sub>2</sub>O<sub>3</sub>- and SiO<sub>2</sub>-supported catalysts, however, very large NH<sub>4</sub>ReO<sub>4</sub> crystallites have been found (ca. 100 nm).

This striking difference between carbon, on the one hand, and Al<sub>2</sub>O<sub>3</sub> and SiO<sub>2</sub>, on the other hand, is explained tentatively considering the construction of their pore systems. In the case of Al<sub>2</sub>O<sub>3</sub> and SiO<sub>2</sub> mesoand macropores are usually interconnected, resulting in easy formation of NH<sub>4</sub>ReO<sub>4</sub> crystallites in the macropores, by transport of ReO<sub>4</sub> ions from nearby mesopores. In the case of activated carbon, the abundantly present micropores as well as the mesopores are longer and generally not directly connected with the macropores (39). As a result, ReO<sub>4</sub> ions cannot migrate from the narrow pores during drying and only small crystallites can be formed. Therefore, it is concluded that activated carbon is an excellent support to create small crystallites.

Calcined catalysts. Calcination at 575 or 825 K leads to decomposition of NH<sub>4</sub>ReO<sub>4</sub> crystallites with formation of Re<sub>2</sub>O<sub>7</sub> which sublimes under the calcination conditions applied (29) when no interaction with the support takes place. Calcination of Al<sub>2</sub>O<sub>3</sub>supported catalysts leads, without Re loss, to formation of a Re<sup>7+</sup> surface phase of the so-called monolayer-type (36). Apparently, the Re ions originating from large NH<sub>4</sub>ReO<sub>4</sub> crystallites present in the macropores have moved into the mesopores. In order to explain this Re<sup>7+</sup> mobility two possibilities suggest themselves. Surface migration cannot be excluded, but is not very likely to occur in view of the high charge of the Re ions and the important Re<sup>7+</sup>-Al<sub>2</sub>O<sub>3</sub> interaction. Probably Re ions are transported as gas-phase Re<sub>2</sub>O<sub>7</sub>, which rapidly transforms into monolayer Re<sup>7+</sup> species upon collision with the Al<sub>2</sub>O<sub>3</sub> surface. In this way Re loss via the gas phase is efficiently blocked.

SiO<sub>2</sub>-supported catalysts show a more complicated behavior upon calcination. Again decomposition of NH<sub>4</sub>ReO<sub>4</sub> crystallites causes an increase in Re dispersion, but now also Re loss takes place via gasphase Re<sub>2</sub>O<sub>7</sub>, especially during calcination of the Re(2.50)/Si sample at 825 K (see Table 2). The dark colors observed after calci-

nation at 500-600 K are reminiscent of the deep green-blue color observed for solid Re<sub>2</sub>O<sub>7</sub>, which is slightly reduced by H<sub>2</sub>Oassisted oxygen loss, suggesting the presence of small Re<sub>2</sub>O<sub>7</sub> clusters on SiO<sub>2</sub>-supported catalysts with high Re content. Considering the small Re loss due to calcination at 575 K, the clusters are probably stabilized by the support, which is only compatible with the presence of very smallsized clusters. They are probably formed at ca. 500-600 K from large NH<sub>4</sub>ReO<sub>4</sub> crystallites, via gas-phase Re<sub>2</sub>O<sub>7</sub>, and decompose above ca. 600 K with formation of gasphase Re<sub>2</sub>O<sub>7</sub> once more. It is concluded that SiO<sub>2</sub>-supported catalysts can obtain two kinds of Re<sup>7+</sup> surface species, namely small Re2O7 clusters as well as monolayertype Re<sup>7+</sup> surface species. For the Re(2.50)/ Si sample a surface coverage of 1.6 at./nm<sup>2</sup> results after calcination at 825 K, which value is postulated as the monolayer capacity of calcined SiO<sub>2</sub>-supported Re catalysts.

The unknown XRD lines at d values of 318 and 486 pm, observed in the diffractograms of both dried and calcined SiO<sub>2</sub>supported catalysts, may well be due to crystallites of a mixed Re-Si oxide (Re-silicate). The formation of these crystallites might be related to the hygroscopic nature of Re compounds such as Re<sub>2</sub>O<sub>7</sub>. Adsorption of H<sub>2</sub>O is supposed to result in a liquid H<sub>2</sub>O film in which Re<sup>7+</sup> monolayer species and Re<sub>2</sub>O<sub>7</sub> clusters dissolve, resulting in a low-pH solution. Subsequently, proton-catalyzed hydrolysis of the SiO<sub>2</sub> surface can take place, followed by crystallization of a Re-silicate from the solution. A separate scanning electron microscopic study supported this picture. The Re fraction present as large Re-silicate-type crystallites is estimated to be small, because a significant shift of  $T_{\text{max}}$  as a function of Re content is found (see Fig. 2) consistent with dominance of surface species. Moreover, no separate TPR peak has been observed for reduction of Re-silicate-type crystallites.

As for SiO<sub>2</sub>-supported catalysts, Re loss is observed due to calcination of carbonsupported catalysts. An increase of calcination temperature from 575 to 825 K leads to an increase of Re loss for the Re(0.20)/C sample, suggesting that, on carbon as on SiO<sub>2</sub>, Re<sub>2</sub>O<sub>7</sub> clusters are present after calcination at 575 K. Heating at 575 K in Ar might lead to partial reduction of these clusters, while during heating at 825 K in Ar the Re loss as Re<sub>2</sub>O<sub>7</sub> is supposed to be much faster than partial reduction. On the basis of the Re content of the Re(0.20)/C sample heated at 825 K in Ar, the monolayer capacity of heat-treated carbon-supported Re catalysts is estimated to be 0.1 at./nm<sup>2</sup>. The much higher Re content of the Re(0.80)/C sample after calcination at 575 K in air is supposedly related to the presence of a large fraction of Re<sub>2</sub>O<sub>7</sub> clusters, while also the oxygen content of the activated carbon can affect the monolayer capacity.

For all three supports studied the effect of calcination on catalyst structure is limited almost completely to decomposition of NH<sub>4</sub>ReO<sub>4</sub> crystallites. No significant influence of calcination is found on the reducibility of Re<sup>7+</sup> surface species which are already present on dried samples, showing that the same monolayer-type Re<sup>7+</sup> surface species are present on both dried and calcined catalysts. No significant solid-state diffusion processes, leading to stronger Re<sup>7+</sup>-support interaction, have taken place at elevated temperatures.

The small shift of  $T_{\rm max}$  of the Re<sup>7+</sup> surface phase reduction peak, due to calcination of Al<sub>2</sub>O<sub>3</sub>-supported catalysts, may arise from adsorbed H<sub>2</sub>O (22, 36), which blocks some vacancies which are necessary for the initiation of reduction. The surprisingly small effect of the H<sub>2</sub>O content on the  $T_{\rm max}$  value has been reported before (21) and is confirmed in this study by the finding that intentional saturation of the H<sub>2</sub>/Ar reducing mixture with H<sub>2</sub>O leads to an upward  $T_{\rm max}$  shift of only about 10 K.

The  $T_{\text{max}}$  value determined for the reduction of Re<sup>7+</sup> surface species is considerably

influenced by the Re content and the support choice (see Fig. 2). Differences in reducibility between Al<sub>2</sub>O<sub>3</sub>- and SiO<sub>2</sub>-supported Re catalysts have been reported before (15, 40). The results of the present study are explained both by differences in interaction forces between Re7+ ions and the various supports and by heterogeneity of the interaction. The strength of the Re<sup>7+</sup>-support interaction becomes noticeable in several ways: (i) the capacity of the supports for the uptake of ReO<sub>4</sub> ions during impregnation and drying; (ii) the capacity of the supports for the formation of stable Re<sup>7+</sup> surface species during calcination at 825 K (the monolayer capacity); and (iii) the  $T_{\text{max}}$  value of the Re<sup>7+</sup> surface phase reduction peak for various supports at comparable Re content (at./nm<sup>2</sup>).

Everything points to Al<sub>2</sub>O<sub>3</sub> being the support which interacts strongest with Re<sup>7+</sup> ions. SiO<sub>2</sub> exhibits stronger interaction than carbon, as can be easily seen from the differences in monolayer capacity.

Heterogeneity of the Re<sup>7+</sup>-support interaction becomes evident from the shape of the curves shown in Fig. 2. Clearly a distribution of Re<sup>7+</sup> ions over "stronger" and "weaker" sites has taken place. Remarkably, this is the case for all three supports to a comparable extent. It is shown elsewhere that, besides bond-energy factors, also entropy factors affect the observed heterogeneity (35).

### b. Comparison with Literature Data for Re<sub>2</sub>O<sub>7</sub>/Al<sub>2</sub>O<sub>3</sub> Reduction

A sharp Re reduction peak has also been found in all other studies on TPR of Re catalysts. Occasionally, a high-temperature contribution in the range 650-950 K is also reported (4, 18, 22). However, its assignment to Re reduction is questionable, because it may be present due to reduction of organic impurities.

The literature values of  $T_{\rm max}$  for the Re<sup>7+</sup> reduction peak vary over a wide range (550–880 K). As shown in Fig. 9, the  $T_{\rm max}$  value is obviously dependent on Re con-

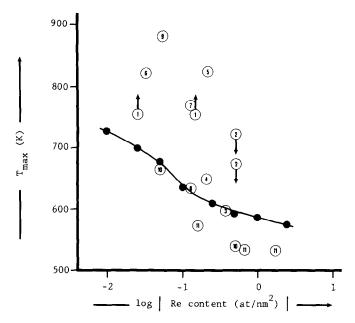


Fig. 10. Comparison of  $Re_2O_7/Al_2O_3$  reducibility data ( $T_{max}$  of  $Re^{7+}$  surface phase); data for the dried catalysts from this study (closed circles plus full line) and various literature data (open circles with numbers included), as a function of Re content. The studies used are: 1 and 2, Refs. (14, 15), respectively (isothermal studies; the open circles indicate the reduction temperature chosen, while the arrows show where  $T_{max}$  is expected in case the experiments had been performed in the TPR mode); 3, Ref. (17); 4, Ref. (18); 5, Ref. (18), TPR after  $N_2$  treatment at 775 K for 16 h; 6, Ref. (19); 7, Ref. (20); 8, Ref. (20), TPR after reduction-reoxidation; 9, Ref. (21); 10, Ref. (4); 11, Ref. (22).

tent. Therefore in Fig. 10 a survey of  $T_{\text{max}}$ values, taken from the present as well as from already published studies, is given as a function of Re content. Data taken from two isothermal reduction studies are also included. Slightly different experimental conditions have been applied in the assembled temperature-programmed studies. The spreading in  $H_2$  pressure (0.05–1 bar) has to be accounted for, because it has been shown that  $T_{\text{max}}$  shifts more than 220 K to higher temperatures when the H<sub>2</sub> pressure is decreased by a factor of 1000 (17). The diversity in heating rates (4-10 K/min) is of minor importance, because it has been established that an increase of the heating rate by a factor of 10 leads to a 55 K upward shift of  $T_{\text{max}}$  (35). The results of the present study agree well with most literature data, taking into account the variations in H<sub>2</sub> pressure and heating rate as well as the use of different Al<sub>2</sub>O<sub>3</sub> batches. However, in five

references (14, 18-21) describing the reduction of catalysts with low Re content,  $T_{\text{max}}$  values have been reported which lie up to 200 K above the generally found values.

The following explanations will be considered:

First, it has been reported that pretreatment of Re<sub>2</sub>O<sub>7</sub>/Al<sub>2</sub>O<sub>3</sub> catalysts with low Re content at high temperature in inert gas or under vacuum leads to prereduction of Re<sup>7+</sup> to Re<sup>4+</sup> (18). The resulting supported Re<sup>4+</sup> ions reduce at much higher temperature than the original Re<sup>7+</sup> ions, suggesting the formation of a rather stable compound between Re<sup>4+</sup> oxides and Al<sub>2</sub>O<sub>3</sub>, via diffusion of Re<sup>4+</sup> ions. This does not explain, however, why in references (14, 19–21), dealing with reduction of calcined Re<sup>7+</sup> catalysts, also very high T<sub>max</sub> values are reported.

A second possibility is that upon calcination very stable compound formation between  $Re^{7+}$  oxides and  $Al_2O_3$  occurs, leading to structures having very high  $T_{max}$  values (15, 16, 21). The present study shows that calcination does not cause such an effect.

Also the  $H_2O$  concentration at the catalyst surface might influence the reducibility of  $Re^{7+}$  (15, 19, 41). Although the presence of  $H_2O$  has a tremendous effect on alloy formation and reducibility of  $Re^{7+}$  in Pt-Re/Al<sub>2</sub>O<sub>3</sub> catalysts, it does not appear to be a critical factor in the monometallic Re catalysts (21). This is supported by our finding that TPR measurements using  $H_2O$ -saturated  $H_2/Ar$  did not result in a significant  $T_{max}$  shift.

A more suitable explanation might be found in the role of additives present on the  $Al_2O_3$  support. Interestingly, in some references (20, 21) the presence of chloride is reported, whereas in others (14, 19) no attention is paid to possible additives such as chloride. Although it is shown that a decrease in chloride content by a factor of 10 does not influence the  $T_{\text{max}}$  value (21), the CI/Re ratio after removal of chloride was still 1.3, which is high enough to allow the presence of a stoichiometric Re-Cl complex. Moreover, the catalyst applied contained also Pt leaving open the possibility of a Pt-catalyzed Re reduction camouflaging the influence of chloride. In another study (20) it is found that  $T_{\text{max}}$  for reduction of Re<sup>7+</sup> is decreased after a reduction-reoxidation cycle, which might be due to loss of chloride (e.g., as HCl) during reduction. Also in the present study the Al<sub>2</sub>O<sub>3</sub> support contains some chloride (0.04 wt%), leading to Cl/Re ratios above 1 for the Re(0.0097-0.025)/Al samples, which can explain part of the heterogeneity observed.

We therefore propose that additives such as chloride might modify the support locally, in such a way that very polar, strong Re<sup>7+</sup> chemisorption sites are created resulting in very low Re<sup>7+</sup> reducibility.

### CONCLUSIONS

1. Under the TPR conditions applied, Re<sup>7+</sup> ions reduce in a very narrow tempera-

ture range leading to sharp TPR peaks, most probably as a result of autocatalysis by instantly formed Re<sup>0</sup>. Ultimately, Re<sup>7+</sup> reduces to mainly Re<sup>0</sup>. Reduction of organic impurities (probably polymerized acetone) is catalyzed by Re<sup>0</sup> and leads to CH<sub>4</sub> formation.

- 2. For dried catalysts TPR indicates the presence of both a Re<sup>7+</sup> surface phase (of monolayer type) and NH<sub>4</sub>ReO<sub>4</sub> crystallites. With respect to the detection of NH<sub>4</sub>ReO<sub>4</sub> crystallites TPR has advantages over XRD: TPR can be used for quantitative analysis and for detection of very small crystallites.
- 3. Under the preparation conditions applied, the ReO<sub>4</sub> adsorption capacity of Al<sub>2</sub>O<sub>3</sub>, SiO<sub>2</sub>, and carbon during impregnation and drying is small.
- 4. Calcination at 575 or 825 K leads to decomposition of NH<sub>4</sub>ReO<sub>4</sub> crystallites with formation of Re<sub>2</sub>O<sub>7</sub>. Depending on calcination temperatures, type of support, and transition metal content Re is redistributed over the surface or disappears from the catalyst sample. In both cases Re transport supposedly takes place via gas-phase Re<sub>2</sub>O<sub>7</sub>. Redistributed Re ions take part in monolayer formation or, in the case of limited monolayer capacity (SiO<sub>2</sub>, carbon), form small Re<sub>2</sub>O<sub>7</sub> clusters.
- 5. The reducibility mainly depends on Re content and support properties. The calcination temperature has only a small effect. The differences in reducibility are caused both by the strength of the  $Re^{7+}$ -support interaction, which decreases in the order  $Al_2O_3 > SiO_2 > carbon$ , and by heterogeneity of this interaction, which is similar for the three supports.
- 6. TPR of carbon-supported Re catalysts shows three types of gasification. At 500–900 K pyrolysis of oxygen-containing groups takes place with production of CO and CO<sub>2</sub>, which are converted easily to CH<sub>4</sub> over Re<sup>0</sup> under the TPR conditions applied. At 900–1100 K gasification is strongly catalyzed, probably by Re<sup>0</sup> crystallites. Above ca. 1100 K gasification is supposed to be only weakly catalyzed.
  - 7. For Re<sub>2</sub>O<sub>7</sub>/Al<sub>2</sub>O<sub>3</sub> catalysts containing

small amounts of Re, literature reduction data are inconsistent. Differences in the concentration of additives such as chloride might explain these variations.

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