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Prediction of Acoustical Behavior of Granular Material Stacks as Measured in a Standing Wave Tube by using a Biot Theory-based Model

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PREDICTION OF ACOUSTICAL BEHAVIOR OF GRANULAR MATERIAL STACKS AS MEASURED IN A STANDING WAVE TUBE BY USING A BIOT THEORY-BASED MODEL

Zhuang Mo, Guochenhao Song, Tongyang Shi, J. Stuart Bolton



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Content

- Introduction
- Testing Procedure
- Model Predictions Compared with Measurements
- Summary





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Introduction



Granular activated carbon



Glass bubbles https://www.3m.com/3M/ en_US/p/d/b40064606/



20 mm glass bubble







Glass bubbles are sensitive to sample preparation





Exposure to strong signal improves consistency



No treatment



Exposed to 5min of 1000 m Vrms 0-6400 Hz signal

Softening with increasing input level





Softening with increasing input level



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Finite Difference Approach



Finite Difference Approach

Jassen's model – Force deflection in cylindrical container and friction on container wall (Duran, 2000, Springer)

	p'_0		$A\Delta\sigma + J\mu_W C_L p_v dh = \rho g A dh$
	p_v		
Jμ _W C _L σdh		dh	$\sigma = \frac{\rho g}{\beta} \left(1 - e^{-\beta x} \right) + p_0' e^{-\beta x}$
	ρgAdh		Ρ
σ	$+ \Delta p_v$		
			β is the Jassen factor:
			$\beta = 4J\mu_W/d$

Hertzian contact – effective stiffness increases with the contact surface area (Fischer-Cripps, 1999)

$$E = E_0 \sigma^{1/3}$$

With Jassen's model and Hertzian contact theory, the stiffness of particle stack can be expressed as a function of depth, which has been applied in previous studies, e.g., Matchett and Yanagida, 2003; Tsuruha et al., 2020

$$E = E_0 \left[\frac{\rho g}{\beta} (1 - e^{-\beta x}) + p'_0 e^{-\beta x} \right]^{1/3}$$
1. [og]^{-2/3}

$$\frac{\partial E}{\partial x} = \frac{1}{3} E_0 \left[\frac{\rho g}{\beta} \left(1 - e^{-\beta x} \right) + p_0' e^{-\beta x} \right]^{-2/3} \left(\rho g - \beta p_0' \right) e^{-\beta x}$$



Finite Difference Approach

See (Venegas and Umnova, 2016) for details

For glass bubbles, only the interstitial pores need to be considered:

For granular activated carbon, triple porosity model is applied:

$$k_{p} = -j\delta_{\nu}^{2}(1 - 3C/x^{2})^{-1}$$

$$B = \left(\frac{1}{B_{p}} + \frac{1 - \phi_{p}}{B_{u}}F_{d}\right)^{-1}$$

$$k_{p}' = -j\delta_{t}^{2}\left(1 - \zeta^{3} + \frac{3\zeta}{x_{t}^{2}}\left(\zeta x_{t}\frac{1 + x_{t} + \tanh(x_{t}(\zeta - 1))}{x_{t} + \tanh(x_{t}(\zeta - 1))}\right) - 1\right)$$

$$B_{u} = \left(\frac{1}{B_{m}} + \frac{1 - \phi_{m}}{B_{n}}F_{nm}\right)^{-1}$$

where $\zeta = (1 - \phi)^{1/3}$, and all other parameters follow the definitions in the references.





Model Predictions Compared with Measurements





Model Predictions Compared with Measurements

The finite difference model provides predictions that match different thicknesses:





Conclusions

The measurement and model description of granular materials are introduced

- Testing procedure is developed for acoustic measurement of granular materials
- A numerical implementation of Biot theory is introduced
- The model prediction match very well with the measurement
- Future work
 - Improve the testing procedure, pursuing better consistency
 - Establish more complete model for forward prediction of material properties



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