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Supporting Information

# Integrated Cascade Process for the Catalytic Conversion of 5-Hydroxymethylfurfural to Furanic and TetrahydrofuranicDiethers as Potential Biofuels

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# **Supporting Information**

Integrated cascade process for the catalytic conversion of 5hydroxymethylfurfural (HMF) to furanic and tetrahydrofuranic diethers as potential bio-fuels

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Test	[HMF] (wt%)	Catalyst	T (°C)	t (h)	HMF <sup>[a]</sup> Conversion (mol%)	EMF <sup>[b]</sup> Yield (mol%)	EL <sup>[c]</sup> Yield (mol%)	Ref.
<b>S</b> 1	7.4	$H_2SO_4$	100	12	100	54	n.a. <sup>[d]</sup>	1
S2	7.4	<i>p</i> -toluene sulfonic acid	100	12	100	61	n.a. <sup>[d]</sup>	1
<b>S</b> 3	7.4	Graphene oxide	100	12	96	92	n.a. <sup>[d]</sup>	1
<b>S</b> 4	3.1	<i>p</i> -toluene sulfonic acid	110	0.5	100	83	17	2
<b>S</b> 5	3.1	Amberlyst-15	110	0.5	85	71	7	2
<b>S</b> 6	3.1	PDVTA-SO <sub>3</sub> H <sup>[e]</sup>	110	0.5	100	88	12	2
<b>S</b> 7	10.5	$H_2SO_4$	140	5	100	3	96	3
<b>S</b> 8	10.5	Amberlyst-15	140	5	100	0	99	3
<b>S</b> 9	10.5	Z-SBA-15 <sup>[f]</sup>	140	5	100	76	23	3
S10	1.3	ZSM-5	140	6	84	56	n.a. <sup>[d]</sup>	4
S11	1.3	AT(0.50)-OT <sup>[g]</sup>	140	6	97	90	n.a. <sup>[d]</sup>	4
S12	3.3	Nafion NR50	180	3	96	52	27	5
S13	3.3	Ni <sub>2</sub> P/SiO <sub>2</sub>	180	3	97	65	18	5
S14	2.5	Amberlyst-15	160	2.5	84	64	20	6
S15	2.5	β-zeolite (BEA-25)	160	2.5	66	63	3	6

Table S1. Overview of the literature on the pure HMF etherification to EMF carried out in ethanol compared under the same reaction conditions with different catalytic systems.

[a] HMF = 5-hydroxymethylfurfural; [b] EMF = 5-ethoxymethylfurfural; [c] EL = ethyl levulinate; [d] n.a. = not available; [e] Sulfonated copolymer divenylbenzene-triallylamine; [f]  $ZrO_2$  dispersed on the SBA-15 support; [g] ZSM-5 subjected to an alkaline treatment (AT) with NaOH at 0.50 M followed by an oxalic acid treatment (OT)



Scheme S1. Different pathways in the hydrogenation of HMF in ethanol



Figure S1. Mass spectrum of 5-methylfurfural (MF), identified by the comparison with library pattern (Wiley Registry 10<sup>th</sup> Edition).



with library pattern (Wiley Registry 10<sup>th</sup> Edition).



Figure S3. Mass spectrum of 5-methyltetrahydrofurfurylalcohol (MTHFA) identified by the comparison with library pattern (Wiley Registry 10<sup>th</sup> Edition).



Figure S4. Mass spectrum of 1,2,6-hexanetriol (1,2,6-HT) identified by the comparison with

library pattern (Wiley Registry 10<sup>th</sup> Edition).



comparison with library pattern (Wiley Registry 10<sup>th</sup> Edition).



Figure S6. Mass spectrum of 5-(hydroxymethyl)-furfural diethyl acetal (HMFDA) identified by the comparison with literature (main m/z values: 109, 127, 155, 200).<sup>[7]</sup>



Figure S7. Mass spectrum of 5-(ethoxymethyl)furfuryl alcohol (EMFA) identified by the comparison with literature (main m/z values: 29, 41, 55, 83, 97, 111, 125, 165).<sup>[7]</sup>



comparison with literature (main m/z values: 29, 55, 83, 97, 111, 125, 139, 155, 184).<sup>[7]</sup>



identified by the comparison with literature (main m/z values: 29, 43, 57, 83, 101, 129).<sup>[8]</sup>

			Carbon Balance (mol%) <sup>[a]</sup>								
_	Т	P H <sub>2</sub>									
Run			Time (min)								
	(°C)	(bar)	15	20	60	00	120	190	240	200	
			15	30	00	90	120	100	240	300	
1	100	50	93.2	97.6	93.0	85.6	86.7	90.4	89.7	86.5	
2	80	50	83.1	81.8	82.2	86.5	89.4	92.1	87.0	89.4	
3	50	50	96.5	97.3	89.6	93.9	89.1	84.8	86.6	88.6	
4	100	60	89.1	92.0	90.5	88.0	87.0	86.3	85.5	85.3	
5	100	20	74.6	81.3	93.5	92.4	84.0	80.3	78.4	76.8	
6	80	60	83.9	85.9	82.1	88.2	88.7	89.1	89.1	87.2	
7	80	20	75.9	75.0	78.4	82.2	83.9	89.4	90.7	85.1	
8	100	10	75.9	71.6	72.1	73.4	78.0	74.0	73.2	68.8	
9	100	70	92.5	93.9	93.1	90.6	89.2	88.3	88.2	85.3	

Table S2. Carbon balance values of the reactions reported in Figures 1–3. Reaction conditions:  $[HMF] = 30 \text{ g L}^{-1}$ ; Ru/HMF = 1 wt%.

[a] Carbon Balance =  $[(mol_{unconverted HMF} + mol_{BHMF} + mol_{BHMTHF})/mol_{starting HMF}] \times 100$ 

## Calculations of internal diffusion limitations through the Weisz-Prater criterion

The Weisz-Prater parameter was calculated using the equation 1 (Eq.S1) and the internal diffusion can be considered negligible when  $N_{W-P}$  is lower than 0.3:

$$N_{W-P} = \frac{-R_{exp} \cdot r_{\rho}^2}{C_s \cdot D_{eff}}$$
 Eq.S1

In the Eq. S1:

•  $R_{exp}$  is the experimentally observed reaction rate (mol m<sup>-3</sup><sub>cat</sub> s<sup>-1</sup>): it was determined by the ratio between the rate of HMF conversion at the beginning of the reaction and the volume of the employed catalyst, estimated by using the amount of catalyst (0.3 g) and its bulk density,

provided by the supplier and equal to  $750 \text{ kg m}^{-3}$ ;

• r<sub>p</sub> is the radius of catalyst particle (m): according to the supplier information, the particle size distribution is the following one:

 $d_{10} = 5 \ \mu m$  (10% of all particles are characterized by a diameter smaller than 5  $\mu m$ )  $d_{50} = 25 \ \mu m$  (50% of all particles are characterized by a diameter smaller than 25  $\mu m$ )  $d_{90} = 75 \ \mu m$  (90% of all particles are characterized by a diameter smaller than 75  $\mu m$ ) We can suppose the mean value for the particle diameter between 75 and 25  $\mu m$ , thus an average radius of  $2.5 \times 10^{-5}$  m was considered.

- $C_s$  is the concentration of the component at the catalyst surface (mol m<sup>-3</sup>): we supposed that the concentration of HMF on the particle surface was equal to that in the bulk of the solution;
- D<sub>eff</sub> is the effective diffusion coefficient of the component (m<sup>2</sup> s<sup>-1</sup>): the diffusion coefficient of HMF in water was estimated trough the Wilke-Chang equation (Eq.S2):<sup>[10,11]</sup>

$$D_{AB} = \frac{7.4 \, (10^{-8} \, T \, (f_B \, M_B)^{0.5})}{V_{bA}^{0.6} \, m}$$
Eq.S2

Where the symbols with subscript A are referred to the solute (HMF), whereas those with subscript B to the solvent (ethanol):

- $D_{AB}$  is the diffusivity of HMF in ethanol solution,  $cm^2 s^{-1}$ ;
- $M_B$  is the molecular weight of ethanol, g mol<sup>-1</sup>;
- T is the temperature, K;
- $\mu$  is the viscosity of ethanol at 100 °C, cP;

-  $V_{bA}$  is the HMF molar volume at its normal boiling point, cm<sup>3</sup> mol<sup>1</sup>. It was calculated according to the generalized correlation proposed by Maloka regarding the liquid molar volume at the normal boiling point;<sup>[12]</sup>

-  $\phi_B$  is the association factor of ethanol;<sup>[10]</sup>

The effective diffusion coefficient (Deff) was considered as 10% of the diffusion coefficient,

according to the Wilke-Chang equation.<sup>[10,11]</sup>

In Table S3 are reported the parameters adopted for the calculation of the Weisz-Prater criterion:

Table S3. Parameters for calculating the Weisz-Prater criterion for the reaction carried out at 100 °C and 50 bar.

Parameter	rameter Description			
		2 1		
R <sub>exp</sub>	experimentally observed reaction rate	24.7 mol $m^{-3} s^{-1}$		
r <sub>p</sub>	radius of catalyst particle	$2.5 \times 10^{-5} \text{ m}$		
Cs	concentration of the component at the catalyst surface	238 mol $m^{-3}$		
Т	temperature	373 K		
$\phi_{\mathrm{B}}$	association factor of ethanol	1.5		
M <sub>B</sub>	molecular weight of ethanol	46.07 g mol <sup>-1</sup>		
V <sub>bA</sub>	HMF molar volume at its normal boiling point	$119.7 \text{ cm}^3 \text{ mol}^1$		
μ	viscosity of ethanol at 100 °C	0.01104 cP		

From the calculation  $N_{W-P}$  was equal to 0.005, which was strongly lower than 0.3, thus we can infer that the internal mass transfer limitation is negligible in the investigated reaction.

#### Calculations of external diffusion limitations through the Mears criterion

The Mears parameter was calculated using the equation S3 (Eq.S3) and the external diffusion can be considered negligible when  $C_M$  is lower than 0.15:

$$C_{M} = \frac{-R_{exp} (r_{p}) n}{k_{c} (C_{AS})}$$
Eq.S3

In the Eq.S3:

• R<sub>exp</sub> is the experimentally observed reaction rate (mol m<sup>-3</sup><sub>cat</sub> s<sup>-1</sup>): it was determined as reported previously;

- $r_p$  is the radius of catalyst particle (m): it was  $2.5 \times 10^{-5}$  m, as previously reported;
- n is the reaction order of HMF;
- $C_{AS}$  is the concentration of HMF in the solution (mol m<sup>-3</sup>);
- k<sub>c</sub> is the mass transfer coefficient for HMF-ethanol (m s<sup>-1</sup>): it was calculated according to Eq.S4:

$$k_c = \frac{Sh \cdot D_{AB}}{d_p}$$
 Eq.S4

where  $D_{AB}$  is the diffusion coefficient of HMF in ethanol at 373 K (1.185 × 10<sup>-7</sup> m<sup>2</sup> s<sup>-1</sup>), d<sub>p</sub> is the catalyst particle diameter (5 × 10<sup>-5</sup> m) and Sh is the Sherwood number, which is calculated according to Eq.S5:<sup>[13]</sup>

$$Sh = 2 + 0.6 \ \hat{R}e^{0.5} \ \hat{S}e^{1/3}$$
 Eq. S5

where Re is the Reynolds number and Sc is the Schmidt number, which are defined according to Eq. S6 and S7, respectively:

$$Re = \frac{N \cdot D^2 \cdot r}{m}$$
 Eq.S6

where N is the rotational speed of the stirrer (1000 rpm/60 s = 16.67 s<sup>-1</sup>), D is the stirrer diameter ( $3.5 \times 10^{-2}$  m),  $\rho$  is the density of ethanol at 373 K (713 kg m<sup>-3</sup>),  $\mu$  is the dynamic viscosity of ethanol at 373 K ( $11.04 \times 10^{-6}$  kg m<sup>-1</sup> s<sup>-1</sup>).

$$\mathfrak{S} = \frac{V}{D_{AB}}$$
 Eq.S7

where V is the kinetic viscosity of ethanol at 373 K (7.27  $\times 10^{-6}$  m<sup>2</sup> s<sup>-1</sup>) and D<sub>AB</sub> is the diffusion coefficient of HMF in ethanol at 373 K (1.185  $\times 10^{-7}$  m<sup>2</sup> s<sup>-1</sup>).

In Table S4 are reported the parameters adopted for the calculation of the Mears criterion:

Table S4. Parameters for calculating the Mears criterion for the reaction carried out at 100 °C and 50 bar.

Parameter	Description	Value
R <sub>exp</sub>	experimentally observed reaction rate	24.7 mol m <sup>-3</sup> s <sup>-1</sup>
r <sub>p</sub>	radius of catalyst particle	$2.5 \times 10^{-5} \mathrm{m}$
n	reaction order of HMF	1
C <sub>AS</sub>	concentration of HMF in the solution	$238 \text{ mol m}^{-3}$
D <sub>AB</sub>	diffusion coefficient of HMF in ethanol at 373K	$1.185 \times 10^{-7} \text{ m}^2 \text{ s}^{-1}$
N	rotational speed of the stirrer	16.67 s <sup>-1</sup>
D	diameter of the stirrer	$3.5 \times 10^{-2} \text{ m}$
ρ	density of ethanol at 373K	713 kg m <sup>-3</sup>
μ	dynamic viscosity of ethanol at 373 K	$11.04 \times 10^{-6} \text{ kg m}^{-1} \text{ s}^{-1}$
V	kinetic viscosity of ethanol at 373 K	$7.27 \times 10^{-6} \text{ m}^2 \text{ s}^{-1}$

From the calculation  $C_M$  was equal to  $4.02 \times 10^{-7}$ , which was strongly lower than 0.15, thus we can infer that the external mass transfer limitation is negligible in the investigated reaction.



Figure S10. Hydrogen reaction order in the hydrogenation of HMF carried out at 100°C.



Figure S11. DRIFTS spectra recorded at increasing temperature after pyridine adsorption over HZSM-5 Si/Al=15 (top) and Si/Al=25 (bottom) at 50 °C.



Scheme S2. Possible patwhays of by-products formation in the etherification of pure BHMF.



(DHEMMF) identified by the comparison with literature (adapted from the fragmentation of the respective methanol ether).<sup>[9]</sup>



comparison with literature (main m/z values: 43, 55, 73, 113).<sup>[7]</sup>





Figure S15. Proposed fragmentation of 2,5-bis(ethoxymethyl)tetrahydrofuran (BEMTHF) in the mass spectrometer



comparison with library pattern (Wiley Registry 10<sup>th</sup> Edition).



Figure S17. Recyclability tests of: A) 5 wt% Ru/C employed in the optimised hydrogenation of HMF to BHMF (Ru/HMF ratio = 1 wt%, [HMF] = 3.7 wt% 100 °C, 20 bar, 60 min); B) HZSM-5 (Si/Al = 25) employed in the optimised etherification of BHMF to BEMF ( $mol_{BHMF}/mol_{total acid sites} = 8.3$ , [BHMF] = 3.0 wt%, 80 °C, 2h).



Figure S18. TGA of fresh 5 wt% Ru/C and spent 5 wt% Ru/C recovered at the end of the fifth recycle run (Reaction conditions: Ru/HMF ratio = 1 wt%, [HMF] = 3.7 wt% 100 °C, 20 bar, 60 min).



Figure S19. TGA of fresh zeolite HZSM-5 (Si/Al = 25) and spent zeolite HZSM-5 (Si/Al = 25) recovered at the end of the fifth recycle run (Reaction conditions:  $mol_{BHMF}/mol_{total acidity} = 8.3$ , [BHMF] = 3.0 wt%, 80 °C, 2h).

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