

1 ***In situ* groundwater remediation with bioelectrochemical systems (BES): a critical review and**  
2 **future perspectives**

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13 **Abstract:** *Groundwater contamination is an ever-growing environmental issue that has attracted much*  
14 *and undiminished attention for the past half century. Groundwater contamination may originate from*  
15 *both anthropogenic (e.g., hydrocarbons) and natural compounds (e.g., nitrate and arsenic); to tackle the*  
16 *removal of these contaminants, different technologies have been developed and implemented. Recently,*  
17 *bioelectrochemical systems (BES) have emerged as a potential treatment for groundwater*  
18 *contamination, with reported in situ applications that showed promising results. Nitrate and*  
19 *hydrocarbons (toluene, phenanthrene, benzene, BTEX and light PAHs) have been successfully removed,*  
20 *due to the interaction of microbial metabolism with poised electrodes, in addition to physical migration*  
21 *due to the electric field generated in a BES. The selection of proper BESs relies on several factors and*  
22 *problems, such as the complexity of groundwater and subsoil environment, scale-up issues, and energy*  
23 *requirements that need to be accounted for. Modeling efforts could help predict case scenarios and select*  
24 *a proper design and approach, while BES-based biosensing could help monitoring remediation*  
25 *processes. In this review, we critically analyze in situ BES applications for groundwater remediation,*  
26 *focusing in particular on different proposed setups, and we identify and discuss the existing research*  
27 *gaps in the field.*

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29

30 **Keywords:** bioelectrochemical systems, *in situ* treatment, groundwater remediation,  
31 bioelectroremediation, denitrification, microbial electrochemical technologies

## 32        **1. Introduction**

33        Groundwater (GW) is highly susceptible to many pollutants, and contamination may render it unsafe or  
34        unfit for human or other uses. Contamination might be linked to natural causes, for example, arsenic (As)  
35        or nitrate (NO<sub>3</sub><sup>-</sup>)-containing rocks (Menció et al., 2016; Tabelin et al., 2018) or, more frequently, to direct  
36        or indirect anthropic influence (Burri et al., 2019).

37                Different treatment technologies have been applied to GW remediation: physical, chemical, and  
38        biological, with a variable rate of success (Callegari et al., 2018; Dong et al., 2019; O'Connor et al.,  
39        2018; Sarkar and Paul, 2016). Application of Pump & Treat (P&T) schemes are among the most diffused  
40        strategies. In this treatment, GW is extracted and subsequently treated outside of the aquifer; this type of  
41        solution allows for better process control (i.e., directly observable by the operator); however, it may be  
42        highly energy-intensive when the treated, extracted GW does not require immediate use (Favara and  
43        Gamlin, 2017). Therefore, much research is focusing on the development of *in situ* treatments, which are  
44        generally considered to be more sustainable for the protection of this resource. Compared to P&T, *in situ*  
45        treatment requires a more detailed study of the characteristics of the aquifer and its surroundings, since  
46        no one-fits-all or standardized solution can be applied with the same success and effectiveness in sites  
47        with different characteristics. Therefore, the application of *in situ* GW treatment should be implemented  
48        with customized and knowledge-intensive approaches, with a focus on the underlying processes,  
49        involving detailed field trials to ensure appropriateness and robustness of the design (Kuppusamy et al.,  
50        2016; Majone et al., 2015). Despite the intensive investigation effort required, the application of *in situ*  
51        treatments as an alternative to P&T is constantly growing. The latest U.S. EPA Superfund Report showed  
52        in fact that *in situ* treatment was chosen as a treatment strategy for GW remediation in 51% of cases,  
53        compared to 23% where P&T was selected. A complete reversal of the situation was observed in the year  
54        2000 (EPA, 2017).

55        A large variety of contaminants and their combinations have been found in GW. As shown in Table 1,  
56        these compounds include metals, organic, and inorganic compounds. Pharmaceutically active

57 compounds (PhACs) and contaminants of emerging concern (CECs) have also been identified in GW  
 58 recently (Bexfield et al., 2019).

59

60 **Table 1.** Common contaminants detected in groundwater.

Contaminants	References	
<b>Metals</b>	<i>Metals</i>	Mahato et al. (2016); Trezzi et al. (2016)
	<i>Metalloids</i>	Kozyatnyk et al. (2016); Luu et al. (2009)
	<i>Explosive metals</i>	Chatterjee et al. (2017); Fuller et al., (2019)
	<i>Radioactive metals</i>	Caridi et al. (2017); Waseem et al. (2015)
	<i>Organometallic pesticides and herbicides</i>	Hakoun et al. (2017); Munira et al. (2018)
<b>VOCs</b>	<i>Halogenated VOCs</i>	Plummer et al. (2008); Squillace et al. (2004)
	<i>BTEX</i>	Powers et al. (2001); Rama et al. (2019)
	<i>other non-halogenated VOCs</i>	Plummer et al. (2008); Squillace et al. (2004)
<b>SVOCs</b>	<i>PCBs</i>	Coxon et al. (2019); Samia et al. (2018)
	<i>PHAs</i>	Coxon et al. (2019); Samia et al. (2018)
	<i>Organic pesticides and herbicides</i>	Hakoun et al. (2017); Munira et al. (2018)
	<i>Phenols</i>	Han et al. (2016); Rudel et al. (1998)
	<i>Most fuels and distillates</i>	McMahon et al. (2019); Rama et al. (2019)
	<i>Most explosives</i>	Best et al. (1999); Degnan et al. (2016)
	<i>Dioxins and furans</i>	Hofmann and Wendelborn (2007); Thuan et al. (2011)
	<i>Other halogenated and non-halogenated SVOCs</i>	Plummer et al. (2008); Squillace et al. (2004)
<b>Other</b>	Non-metallic inorganics	Cecconet et al. (2018c); Knoll et al. (2019)
	PhACs	Bexfield et al. (2019); Lopez et al. (2015)
	Asbestos	Apollaro et al. (2018); Oskierski et al. (2016)

61

62 Bioelectrochemical systems (BESs) have steadily emerged in the last 15 years as a versatile and  
 63 promising technology. BESs have been employed in different ways for a variety of tasks: 1) microbial  
 64 fuel cells (MFC), degrading organic matter and producing electrical energy (Capodaglio et al., 2013), 2)  
 65 microbial electrolysis cells (MEC), producing valuable hydrogen gas at the cathode (Miller et al., 2019),  
 66 3) microbial desalination cells (MDC), providing desalinated water from seawater or brackish water  
 67 (Brastad and He, 2013), and 4) microbial electrosynthesis systems (MES), synthesizing value-added  
 68 chemicals and commodities using a poised biocathode (Wang and Ren, 2013). Additionally, BESs have  
 69 been integrated with other technologies such as membrane bioreactors, algal photobioreactors, and

70 capacitive deionization, in hybrid system configurations to increase overall performance, both in terms  
71 of energy consumption/production and contaminant removal (Xiao et al., 2012; Yuan et al., 2012).

72 Among different applications of BESs, *in situ* GW bioelectroremediation, i.e., remediation using  
73 bioelectrochemical systems, showed to be a promising niche, due to its peculiar characteristics. These  
74 include: the option to exploit different redox environments both at anode and cathode, the possibilities  
75 to work at different set potentials and to operate as a flexible technology (Modin and Aulenta, 2017). In  
76 addition, the combination of anodic and cathodic redox environments with microbial metabolism paves  
77 the way for the development of a variety of intriguing and beneficial removal pathways.

78 Modin and Aulenta (2017) reviewed challenges and opportunities of *in situ*  
79 bioelectroremediation, mainly focusing on the general process and the biological mechanisms of  
80 electron-electrode transfer; however, the focus of this review will concentrate on different aspects of *in*  
81 *situ* bioelectroremediation. The first in-depth assessment is on different *in situ* applications of  
82 bioelectrochemical systems for GW remediation, then critical bioelectroremediation challenges and  
83 current research gaps and potential future research directions, including energy consumption and scaling-  
84 up will be identified and discussed.

85

## 86 **2. Practical obstacles in GW remediation suggesting BESs application**

87 An aquifer is undisputedly a challenging environment, and therefore, due to its intrinsic nature, GW  
88 remediation will face several practical issues. Biological water/wastewater treatment requires electron  
89 donors (in case of reductive processes) and acceptors (in case of oxidation). In a hydrocarbon-  
90 contaminated aquifer scenario, for instance, the limited presence of electron acceptors ( $\text{NO}_3^-$ , oxygen,  
91 sulfate) could limit contaminant oxidation. In addition, insufficient intra-aquifer mixing allows  
92 replenishment of electron acceptors only at a contaminated plume's physical boundary, where diffusion  
93 and dispersion are the predominant mixing factors (Li and Yu, 2015). Due to ordinarily low concentration  
94 of organic matter in GW, similar behavior can be observed for reduction reactions, such as denitrification,  
95 where the limiting electron donor may limit potential reaction rates (Shen et al., 2015). Besides,

96 metabolism and growth rates of microorganisms may be slowed down in such circumstances, since the  
 97 majority of biota is attached to soil particles in the sediment, where diffusion of electron acceptors/donors  
 98 might be particularly difficult (Li and Yu, 2015).

99 According to these premises, *in situ* bioremediation may become particularly challenging. In  
 100 addition, a few technologies developed so far often contemplate the addition of (expensive) chemicals,  
 101 nutrients, and oxygen or introduction/augmentation of microbial communities adapted to the selective  
 102 degradation of target contaminants. Some of these processes require post-treatments or are efficient only  
 103 on a limited range of contaminants. These drawbacks may render an *in situ* remediation process quite  
 104 complex. Some of these issues are summarized in Table 2.

105

106 **Table 2.** Advantages and drawbacks of some commonly applied technology for *in situ* GW remediation.

Technology	Advantages	Drawbacks	References
<i>Heating</i>	Increases performance of the technology used in post-treatment	Necessarily followed by another remediation technology	(Baker et al., 2016)
<i>Permeable reactive barriers</i>	Intercepts GW flow, long-lasting, variety of setups and solutions	Strongly dependent on the site characteristics, necessary addition of chemicals/nutrients	(Obiri-Nyarko et al., 2014)
<i>Air Sparging</i>	Simple, rapid and economical	Not applicable to nonvolatile contaminants; not suited for confined aquifers	(Bass et al., 2000)
<i>Natural Attenuation</i>	Uses naturally-occurring processes	Long remediation time, needs appropriate conditions	(Weatherill et al., 2018)
<i>Bioaugmentation</i>	Pre-adapted bacteria are able to remove target contaminants, mimics natural process	Long remediation time, not suitable for large-scale sites, may need addition of nutrients, oxygen	(Lyon et al., 2013)
<i>Biostimulation</i>	use of naturally-present bacteria	Not suited for highly-polluted sites addition of nutrients, oxygen supply may be costly in the long period	(Prasad and Prasad, 2012)
<i>Nanoremediation</i>	Reactive materials catalyze and reduce contaminants, nanoparticles diffuse well in aquifer	May be linked to ecotoxicological effects on flora and fauna	(Ingle et al., 2014)
<i>Chemical oxidation/reduction</i>	Highly effective	High cost	(Borden et al., 2011)
<i>Bioelectroremediation</i>	No chemicals addition, electrodes acting as electron donor/acceptor, use of indigenous microbial consortia, low	Still at lab or pilot scale	(Pous et al., 2018)

energy demand can be supplied by  
renewable sources

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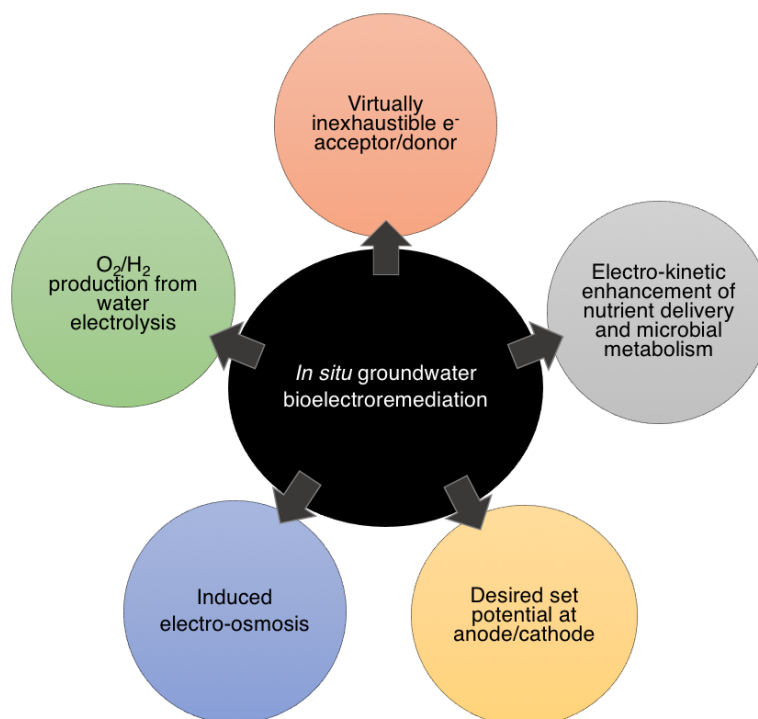
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108 BES application may become a solution to the challenges mentioned above or at least a large part  
109 of them. The lack of natural onsite electron acceptors and donors required by bioremediation can be  
110 substituted electrodes inserted in the soil matrix, acting as “virtually” inexhaustible electron acceptors  
111 (anode) or donors (cathode) and supporting microbial metabolism (Aulenta et al., 2011). In other  
112 solutions, chemicals acting as electron donors/acceptors are added instead (e.g., reactive barriers),  
113 requiring periodic replacement of spent agents. In addition, when reduction reactions are involved, BESs  
114 allow setting the desired cathodic electrode potential at reductive levels that cannot be reached by the  
115 mere addition of chemical reagents (Li and Yu, 2015; Williams et al., 2010).

116 Concomitant phenomena may amplify the effectiveness of BES applications. Water electrolysis  
117 (occurring at the electrodes’ surface) may generate oxygen and hydrogen, which could serve as an  
118 additional electron acceptor and donor, respectively. Such electrokinetic enhancement was reported to  
119 enhance mixing and mass transport due to the electric field generated in electrodes’ proximity (Gill et  
120 al., 2014). Electro-osmosis effects may induce water displacement with subsequent resuspension of  
121 immobilized bacteria and contaminants, leading to enhanced contact between substrate and bacteria,  
122 independently of hydraulic conductivity of the porous medium (Gill et al., 2014; Jones et al., 2011; Li  
123 and Yu, 2015; Lohner et al., 2008; Xu et al., 2010). Li and Yu (2015) reported other advantages of BESs  
124 application for GW *in situ* remediation, namely: electrokinetic enhancement of nutrient delivery and  
125 microbial metabolism connected to higher bioavailability, higher bacterial enrichment, and adsorption  
126 due to large electrodes’ surface.

127 As shown in Figure 1, an additional advantage of BES application for *in situ* remediation is their  
128 higher environmental sustainability; this is mainly due to the general lack of chemicals addition. This  
129 aspect becomes especially relevant when BESs are compared to other technologies where a  
130 constant/intermittent supply of electron donors/acceptors and chemicals is an operational condition.

131 Combination of electrochemical and biological mechanisms, limited amount of energy requirements that  
 132 are sufficient to induce otherwise non-spontaneous reactions, make these systems more convenient than  
 133 those requiring the full energy input for equivalent reactions. Given the peculiarity of each site's  
 134 condition, a broader analysis, taking into consideration all the possible effects of bioelectroremediation  
 135 on the surrounding environment, should always be conducted.



136  
 137 **Figure 1:** Main advantages of *in situ* bioelectroremediation.  
 138

### 139 **3. *In situ* bioelectroremediation: the quest for an ideal setup**

140 Due to the multidisciplinary and faceted nature of BESs, different setups based on this technology have  
 141 been proposed or developed in the last decade. Most applications have focused on GW denitrification  
 142 and removal of petroleum hydrocarbons (as seen in Table 1). Petroleum hydrocarbons are usually  
 143 removed in BESs by anodic oxidation;  $\text{NO}_3^-$  is reduced to nitrogen gas via autotrophic denitrification or  
 144 autohydrogenotrophic denitrification (at the cathode) or via heterotrophic denitrification (at the anode);  
 145 the presence of organic matter is necessary in the latter case.

146

147 **Table 3:** Specifications of BES performing *in situ* GW treatment. All experiments performed in batch.

Target	Name	Removal pathway(s)	Volume (mL)	Applied potential/voltage/driving force	Initial conc.	Rem. rate	$\eta$	Inoculum	Prevalent microbial species	Ref.
Nitrate	BES	Anodic heterotrophic denitrification	90 <sup>A</sup> , 160 <sup>C</sup>	0.8 V (between electrodes)	25 mg NO <sub>3</sub> <sup>-</sup> -N L <sup>-1</sup>	208.2 ± 13.3 gNO <sub>3</sub> <sup>-</sup> -N m <sup>-3</sup> d <sup>-1</sup>	90.50%	Digested sludge	-	Tong and He (2013)
Nitrate	SMD DC	Cathodic autotrophic denitrification	18	Voltage generated by OM oxidation at the anode	20 mg NO <sub>3</sub> <sup>-</sup> -N L <sup>-1</sup>	0.483 kgN O <sub>3</sub> <sup>-</sup> -N m <sup>-3</sup> TCV d <sup>-1</sup>	90.5% in 12 hrs	Electrodes precolonized in a MFC performing denitrification at the cathode	<i>Gammaproteobacteria</i> ( <i>Shewanella</i> ) (anode); <i>Alphaproteobacteria</i> and <i>Sphingobacteria</i> (cathode)	Zhang and Angelidaki (2013)
Nitrate	BES	Physical migration in a concentrating chamber & successive anodic heterotrophic denitrification	500 <sup>A</sup>	0.8 V (between electrodes)	21.4 mgNO <sub>3</sub> <sup>-</sup> -N L <sup>-1</sup>	-	55% in 17 hrs	Anaerobic sludge	-	Tong and He (2014)
Nitrate	Biocathode buried in simulated aquifer	Cathodic autotrophic denitrification	350 <sup>C</sup>	-0.7 V vs SHE	50 mg NO <sub>3</sub> <sup>-</sup> -N L <sup>-1</sup>	322.6 mg m <sup>-2</sup> d <sup>-1</sup>	-	Anaerobic sludge	<i>Thiobacillus</i> , <i>Paracoccus</i>	Nguyen et al. (2016a)
Nitrate	Biocathode buried	Cathodic autotrophic	110 <sup>C</sup>	-0.303 V vs SHE	30 mg NO <sub>3</sub> <sup>-</sup> -N L <sup>-1</sup>	35.35 mgN O <sub>3</sub> <sup>-</sup> -N	97%	Parent biocathode	-	Cecconet et al.



	in sand or gravel	phic denitrification				$m^{-2} d^{-1}$				(2019a)
			110 <sup>C</sup>	1.0 V (between anode and cathode)	30 mg $NO_3^-$ -N $L^{-1}$	36.23 mgN $O_3^-$ -N $m^{-2} d^{-1}$	100%	Parent biocathode	-	
Nitrate	SMFC-CBER	Cathodic autotrophic denitrification	250 (BER)	0.27 mA, powered by a SMFC	30 mg $NO_3^-$ -N $L^{-1}$	3.87 mgN $L^{-1} h^{-1}$	-	Ground water	-	<i>Hyphomicrobium</i> , <i>Terrimicrobium</i> , <i>Teridiphaera</i> , <i>Prostheco bacter</i> Liu et al. (2019)
Phenanthrene and benzene	MFC	Anodic oxidation	500 <sup>A</sup> , 300 <sup>C</sup>	MFC setup	100 ppm (phenanthrene), 2000 ppm (benzene)	-	>80% (phenanthrene), >90% (benzene)	Parent MFC	-	Adelaja et al. (2017)
Phenol	Bioelectric well	Anodic phenol oxidation	250	+0.2 V vs SHE (anode potential)	25 mg $L^{-1}$	59 ± 3 mg $L^{-1} d^{-1}$	99.5 ± 0.4%	Refinery wastewater	<i>Geobacter</i>	Palm et al. (2018a)
Toluene	Bioelectric well	Anodic toluene oxidation	250	+0.2 V vs SHE (anode potential)	25 mg $L^{-1}$	67.2 ± 5.7 mg $L^{-1} d^{-1}$	100%	Refinery wastewater	<i>Geobacter</i>	Palm et al. (2018b)
Benzene, toluene, ethylbenzene, xylene	Bioelectric well	Anodic oxidation	250	+0.2 V vs SHE (anode potential)	5 mg $L^{-1}$ (benzene), 14 mg $L^{-1}$ (toluene), 2 mg $L^{-1}$ (ethylbenzene), 4 mg $L^{-1}$ (xylene)	31.3 ± 1.5 mg $L^{-1} d^{-1}$ (toluene), 6.1 ± 0.3 mg $L^{-1} d^{-1}$ (benzene), 3.3 ± 0.1 mg $L^{-1} d^{-1}$ (ethylbenzene), 4.5 ± 0	-	Refinery wastewater	<i>Geobacter</i>	Palm et al. (2019)

										.2 mg L <sup>-1</sup> d <sup>-1</sup> (xylene)
Benzene	t-MFC	Anodic oxidation	3300 <sup>A</sup>	MFC setup	60 mg L <sup>-1</sup>	-	100% in 12 d	Selectively enriched mixed microflora	-	Liu et al. (2018)
Light PAHs	GAC-BES	Anodic oxidation and adsorption on GAC	80.46	MFC setup	1546 mg L <sup>-1</sup>	-	99%	Contaminated ground water	<i>Beta-proteobacteria</i> (in particular <i>Pseudomonadaceae</i> )	Kirmizakis et al. (2019)

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<sup>A</sup>: net volume anodic chamber; <sup>C</sup>: net volume cathodic chamber

149 Tong and He (2013) developed an *in situ* laboratory BES, placed in aquifer medium, that attracted  
150  $\text{NO}_3^-$  into the anode chamber, removing it by heterotrophic denitrification (Figure 2A). This system was  
151 tested with both synthetic and real GW. Anode and cathode chambers consisted of separated porous tubes  
152 wrapped by anionic (AEM) and cationic (CEM) exchange membranes, respectively. The anode was fed  
153 with GW medium while the cathode with buffer solution. The system was operated in both MFC and  
154 MEC modes; application of 0.8 V potential between anode and cathode in MEC mode led to the best  
155 results, obtaining  $\text{NO}_3^-$  removal rates up to  $208.2 \pm 13.3 \text{ gNO}_3\text{-N m}^{-3} \text{ d}^{-1}$ . Competition between ion  
156 exchange and electricity-driven ion migration was observed; an open circuit  $\text{NO}_3^-$  removal rate of  $158.2 \pm$   
157  $4.2 \text{ gNO}_3\text{-N m}^{-3} \text{ d}^{-1}$  was reported, caused by the sole ion exchange. In closed circuit conditions, electricity  
158 generation prevented undesired ions migration into the GW by inhibition of ion exchange. Higher current  
159 densities were generated when the system was operated with real GW due to the natural presence of ions  
160 that would enhance charged particles' general movement and favor electricity generation (Tong and He,  
161 2013). This phenomenon should encourage the experimental application of BER in field-scale  
162 applications. In a follow-up study by the same researchers (Tong and He, 2014), the current generated  
163 by a tubular BES induced  $\text{NO}_3^-$  migration out of groundwater, with accumulation in a concentration  
164 chamber. This BES setup was similar to a tubular MDC (Figure 2C): electrons generated by organic  
165 matter oxidation at the anode flowed to the cathode, while cations migrated to the concentration chamber  
166 from the anode. Simultaneously, anions, including the target pollutant  $\text{NO}_3^-$ , reached the concentration  
167 chamber through the AEM, where they were retained by the CEM, preventing their intrusion into the  
168 anode chamber. In this case, rather than biological denitrification,  $\text{NO}_3^-$  removal from GW was due  
169 mainly to physical migration induced by electric current (Tong and He, 2014).. Subsequent denitrifying  
170 treatment of the concentrated solution (brine) would then be necessary to achieve final removal of nitrate.

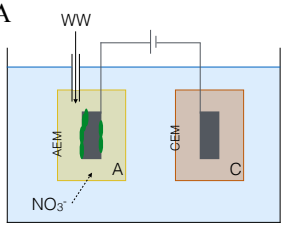
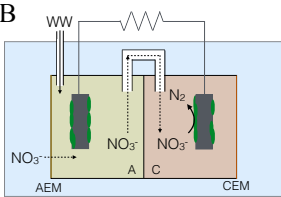
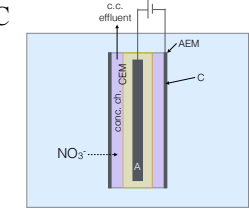
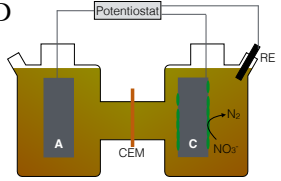
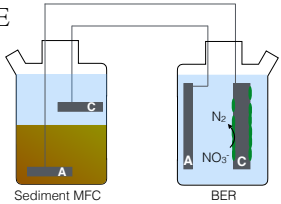
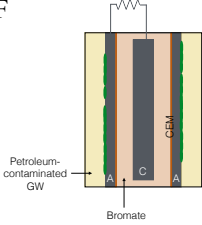
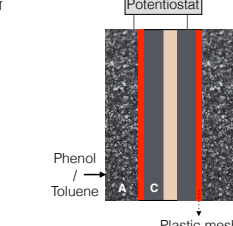
171 Zhang and Angelidaki (2013) proposed a modification of the MDC setup: bioelectricity was used  
172 to attract  $\text{NO}_3^-$  into the anodic chamber through an AEM, then it was transferred to the cathode chamber,  
173 where it was reduced *via* autotrophic denitrification (Figure 2B).  $\text{NO}_3^-$  removal efficiency of 90.5% was  
174 obtained with 12 hours HRT, the ionic strength of GW being a limiting factor for  $\text{NO}_3^-$  removal. Addition

175 of a nitrification step in the anode to cathode  $\text{NO}_3^-$  transferring loop was beneficial to both bioelectricity  
176 production and  $\text{NO}_3^-$  attraction, removing ammonia ( $\text{NH}_3/\text{NH}_4^+$ ) that appeared in the anode chamber due  
177 to anoxic conditions. This setup proved to be versatile and capable, with minor modifications, to remove  
178  $\text{NH}_3$  from anaerobic reactors, at the same time balancing  $\text{NH}_3$  inhibition (Zhang and Angelidaki, 2015a,  
179 2015b). For bioelectricity generation, Tong and He (2013, 2014) and Zhang and Angelidaki (2014) used  
180 synthetic or real wastewater as anode feed in their systems. While this increased the energy sustainability  
181 of treatment, the use of wastewater as anolyte was not always be practically feasible and represented  
182 additional concerns due to possible leakages contaminating GW both in terms of organic matter and  
183 microbial contamination.

184 Denitrification processes using biocathodes buried in simulated aquifers have been investigated  
185 by Nguyen et al. (2016a). Electrodes were immersed in sand at a variable submersion percentage (10,  
186 50, and 100%, plus a control without sand), showing that  $\text{NO}_3^-$  removal rates depend on the sand/medium  
187 ratio. 30% decrease in  $\text{NO}_3^-$  removal rates were observed when liquid recirculation was reduced by the  
188 addition of sand at the bottom of the cathode chamber (Nguyen et al., 2016a) (Figure 2D).

189 The influence of local recirculation was discussed by Jain and He (2018), where, in order to  
190 achieve better BES performances, proper liquid recirculation was indicated as essential to promote  
191 contact between substrate and biomass and decrease overpotentials. This required, however, stirring, and  
192 its energy contribution in small reactors (possibly pumping in the bigger ones) cannot be neglected, and  
193 may massively affect the overall energy balance of an application (Jacobson et al., 2015; Zou and He,  
194 2018). Recently, Cecconet et al. (2019a) confirmed the decrease in  $\text{NO}_3^-$  removal rates previously  
195 reported by Nguyen et al. (2016a) by operating buried biocathodes completely immersed in sand and  
196 gravel, assisted by potentiostat or power supply. Biocathodes operated in gravel achieved better results  
197 due to a greater degree of water movement, compared to those in sand. In addition, higher accumulation  
198 of intermediate nitrogen species was found in biocathodes operated by potentiostat, compared with those  
199 operated by power supply. Increased accumulation of intermediate nitrogen species, e.g., nitrous oxide  
200 ( $\text{N}_2\text{O}$ ), has been shown in other studies to be a potential route of nitrogen loss in bioelectroremediation

201 systems (Srinivasan et al., 2016; Van Doan et al., 2013; Vilar-Sanz et al., 2013). This is likely due to the  
202 intrinsic behavior of biofilms and their microbial stratification and interaction, substrate gradients, ~~and~~  
203 ~~cross-influences~~ that allow biotic and abiotic formation of N<sub>2</sub>O (Sabba et al., 2018). The results of  
204 Cecconet et al. (2019a) and Nguyen et al. (2016a) suggest that the insertion of electrodes in a porous  
205 medium, even though feasible and simple, presents severe limitations that should be eliminated with a  
206 dedicated design (Figure 2D). Both studies were performed in lab-scale H-cells; in a field application  
207 contribution of GW advective flow should be properly assessed, as it would favor contact between  
208 substrate and biomass, and may reduce the drawbacks mentioned above.

Target	Setup	Advantages	Drawbacks	Ref.
$\text{NO}_3^-$		Heterotrophic denitrification (higher kinetics compared to autotrophic)	Necessity of power supply despite OM oxidation; wastewater as anolyte may contaminate the aquifer	Tong and He (2013)
$\text{NO}_3^-$		Versatile	Use of wastewater as anolyte may contaminate the aquifer	Zhang and Angelidaki (2013)
$\text{NO}_3^-$		Tubular, adapt to be used in wells	N physically concentrated, and not biologically removed	Tong and He (2014)
$\text{NO}_3^-$		Simulation of an aquifer remediation	Membrane use not feasible, low performances	Nguyen et al. (2016a); Ceconet et al. (2019a)
$\text{NO}_3^-$		Synergic remediation of sediment and groundwater	No need of wastewater or power supply to fuel the system	Liu et al. (2019)
Phenanthrene and benzene		High performances in PAH removal	Use of bromate as catholyte is not sustainable	Adelaja et al. (2017)
Phenol, toluene, BTEX		High performances, internal recirculation, absence of expensive membrane	Granular graphite may possess non-scalable properties	Palma et al. (2018a, 2018b, 2019)

209

210 **Figure 2:** Advantages and disadvantages of different BES setups for *in situ* GW denitrification. OM:

211 organic matter; WW: wastewater; CEM: cation exchange membrane; AEM: anion exchange membrane;

212 BTEX: benzene, toluene, ethylbenzene, xylene; PAH: polycyclic aromatic hydrocarbons; MFC:  
213 microbial fuel cell; BER: bioelectrochemical reactor.

214

215 A BES setup, known as “bioelectric well”, was proposed for *in situ* remediation of hydrocarbon  
216 contaminated GW (Palma et al., 2018b) (Figure 2G). The setup consisted of a granular graphite anode  
217 and a stainless steel mesh cathode, physically separated by a polyethylene mesh, which maintained  
218 hydraulic continuity. The system, operated at a set anode potential of +0.2 V vs. Standard Hydrogen  
219 Electrode (SHE), obtained nearly complete (99.5%) phenol removal. This BES showed an average  
220 degradation rate of  $59 \pm 3 \text{ mg L}^{-1} \text{ d}^{-1}$  when inoculated with refinery wastewater; lower performances, i.e.,  
221  $23 \pm 1 \text{ mg L}^{-1} \text{ d}^{-1}$ , were recorded when municipal activated sludge was used for inoculum. In both cases,  
222 *Geobacter* species were predominant in mature biofilm on the surface of the graphite granules at the  
223 anode.

224 In a follow-up study, Palma et al. (2018a) using the same, previously applied anode potential for  
225 phenol removal, tested the bioelectric well during long term operation to remove toluene, achieving the  
226 highest toluene removal rate reported so far for anaerobic toluene oxidation ( $67.2 \pm 5.7 \text{ mg L}^{-1} \text{ d}^{-1}$ )  
227 (Figure 2G). *Geobacter* species acted as a catalyzer for the oxidation, initiated by fumarate addition, a  
228 common removal pathway for hydrocarbon-degrading anaerobic microorganisms (Palma et al., 2018a).

229 Recently, a bioelectric well showed to successfully remove mixtures of benzene, toluene, ethyl-  
230 benzene, and xylenes (BTEX) from GW (Palma et al., 2019). Compared to previous applications, the  
231 bioelectric well, due to its vertical design, has the advantage of being easily adaptable for placement in  
232 existing groundwater wells. In addition, the setup may be easily scaled-up and configured to include  
233 internal recirculation; the lack of membranes increases its economic sustainability. However, the use of  
234 granular graphite as electrode material might require some special attention due to its non-scalable  
235 properties (Rozendal et al., 2008; Zhou et al., 2011) and the tendency to internally form dead volumes  
236 with resulting performance loss (Cecconet et al., 2018b). Therefore, the application of other 3-D, scalable  
237 electrode materials (e.g., carbon or graphite foam) should be further investigated. At the moment, the

238 bioelectric well is the most advanced BES for *in situ* bioelectroremediation, showing potential to remove  
239 different contaminants with excellent rates. However, its ability to reduce oxidized contaminants has yet  
240 to be tested, as well as the ability of biomass to exert anocathophilic abilities.

241 Kirmizakis et al. (2019) proposed a BES designed with a graphite electrode chamber (in place of  
242 conventional non-conductive material) coupled with granular activated carbon (GAC) to increase  
243 available anode surface area, for gasworks GW *in situ* remediation. A latex membrane was used to divide  
244 anode from the cathode chamber. This GAC-BES showed 99% removal of aliphatic and aromatic  
245 compounds with rapid bacterial colonization. The main class of bacteria found in the system was  
246 betaproteobacteria with specific PAH-degrading *Pseudomonadaceaea*, commonly detected in gasworks-  
247 contaminated GW (Kirmizakis et al., 2019).

248 *In situ* treatment of phenanthrene and benzene contaminated GW with MFC was reported by  
249 Adelaja et al. (2017), where a tubular MFC with carbon felt anode was exposed to contaminated GW and  
250 tested for long term operation (155 days) (Figure 2F). This system removed up to 90% petroleum  
251 hydrocarbons at the anode and up to 79% bromate ( $\text{BrO}_3^-$ ) at the cathode (added as catholyte). The MFC  
252 was tested under copiotrophic (high concentration) organic C ( $\approx 1500$  ppm benzene and 100 ppm  
253 phenanthrene) and oligotrophic (low concentration) organic C ( $\approx 50$  ppb for both considered  
254 contaminants) conditions. The highest ( $0.76 \text{ mW m}^{-2}$ ) and lowest ( $0.01 \text{ mW m}^{-2}$ ) power densities were  
255 achieved in copiotrophic and oligotrophic conditions, respectively, while contaminants removal  
256 remained consistently high (higher than 80% for benzene and phenanthrene in copiotrophic conditions).  
257 Despite these interesting results, due to the toxicity of  $\text{BrO}_3^-$ , a known carcinogen (Hutchinson et al.  
258 1997), and the possibility of leaks, the use of  $\text{BrO}_3^-$  as catholyte in *in situ* applications should be avoided  
259 and should be strictly restricted to *ex situ* treatment. The presence of  $\text{BrO}_3^-$  in GW was reported (Butler  
260 et al., 2005), mainly as a byproduct of potabilization processes (Butler et al., 2006). *Ex situ* treatments  
261 would allow a combined treatment of both contaminants, maintaining separate streams.

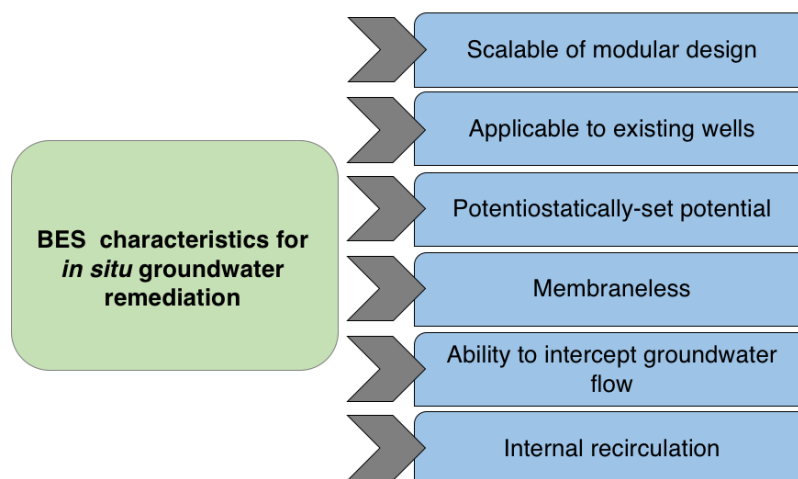
262 A small scale tubular BES composed of three air-cathode MFC connected in series was proposed  
263 for GW benzene removal. The tubular shape allows displacement in wells, and air was insufflated to



264 ensure the presence of oxygen at the cathode (Liu et al., 2018). Effects of the necessary insufflation of  
265 air should be further investigated, as this might induce air sparging, with additional sideway stripping of  
266 volatile compounds.

267 Recently, a 3-chamber BES was proposed by Liu et al. (2019), where a sediment MFC was used  
268 to drive  $\text{NO}_3^-$  reduction in a bioelectrochemical reactor, whose electrodes were connected to the sediment  
269 MFC's electrodes (Figure 2E). The connection of the two systems enhanced both performances, allowing  
270 a 66% decrease of organic matter content in the sediment and observed denitrification rate of  $3.7 \text{ mg N}$   
271  $\text{L}^{-1} \text{ h}^{-1}$ . These results were achieved in both simulated GW and, at higher levels, in real GW. The presence  
272 of microcurrent positively influenced the establishment of naturally occurring GW denitrifying  
273 microorganisms (Liu et al., 2019). From a sustainability point of view, the approach followed by Liu et  
274 al. (2019) is of particular interest due to the use of sediment as a source of organic matter for GW  
275 denitrification. This setup needs further testing at a larger scale to demonstrate operational feasibility in  
276 practical GW remediation cases.

277 Based on existing literature analysis, the main characteristics of an optimal BES for *in situ* GW  
278 treatment can be identified, as shown in Figure 3. These include the possibility to be positioned in existing  
279 wells or trenches, avoiding additional expensive excavations, ability to passively intercept GW flow, lack  
280 of membranes to reduce costs and maintenance, internal recirculation to allow proper intensive contact  
281 between biomass and substrate, large electrodes' surface to allow ample biofilm growth, use of  
282 sustainable-source power supply or potentiostat to set the desired work potential and avoid limitations  
283 linked to anodic organic matter oxidation rate, ease of scalability, modular design setup or both.



284

285

**Figure 3:** Optimal BES characteristics for *in situ* bioelectroremediation

286

#### 287 **4. Discussion**

288 Based on sections 2 and 3, different issues involving *in situ* GW BES have been identified; their current  
 289 status and present gaps are discussed in the following subsections.

290

##### 291 **4.1. Evolution of permeable reactive barriers: a future for BES development?**

292 Among the options for remediation of contaminated GW plumes, the use of permeable reactive barriers  
 293 (PRBs), and in particular of their biological declination, has been advocated and applied widely. A PRB  
 294 consists of a trench or a series of injection wells through which a reactive medium is introduced in the  
 295 soil matrix orthogonally to the flowpath of a contaminated GW plume. The latter, driven by the natural  
 296 hydraulic gradient, passively migrates through the barrier, allowing the contact of solute contaminants  
 297 with the reactive material, leading to their fixation, transformation, or precipitation to a neutral or less  
 298 environmentally harmful form (Obiri-Nyarko et al., 2014).

299 Combination of PRBs with microbial metabolism will constitute so-called “biobarriers”, or bio-  
 300 PRBs. These are built with the same technologies used for conventional PRBs, but consist of materials  
 301 that enhance, support and stimulate microbial metabolism, allowing *in situ* bioremediation of  
 302 contaminated GW (Obiri-Nyarko et al., 2014). Microbial populations, necessary for the degradation of

303 target compounds, are usually already present in a contaminated area (Careghini et al., 2013) and, to  
304 maximize their growth and metabolic action, they may need supplemental nutrients or oxygen –supplied  
305 through the barrier filling material-. In the absence of strains not adapted to the specific contaminants,  
306 the barrier can be initially used to introduce properly enriched, pre-adapted bacterial species to speed up  
307 and promote efficacy of the remediation process (Sarkar et al., 2017).

308 Several examples of contaminants removed through biobarriers are reported in recent literature:  
309 reduced compounds, such as petroleum hydrocarbons, were removed by direct oxygen (terminal electron  
310 acceptor) addition via air sparging, or indirectly by addition of oxygen-releasing compounds, such as  
311  $\text{CaO}_2$ ,  $\text{MgO}_2$ ,  $\text{H}_2\text{O}_2$ , in the barrier filling (Careghini et al., 2013). Oxidized compounds instead, were  
312 removed by the addition of low-cost, recycled organic matter of plant or anthropic origin, such as wood  
313 chips, alfalfa waste, leaves, sawdust, mulch, composted municipal sewage sludge, acting as an electron  
314 donor (Zhang et al., 2018).

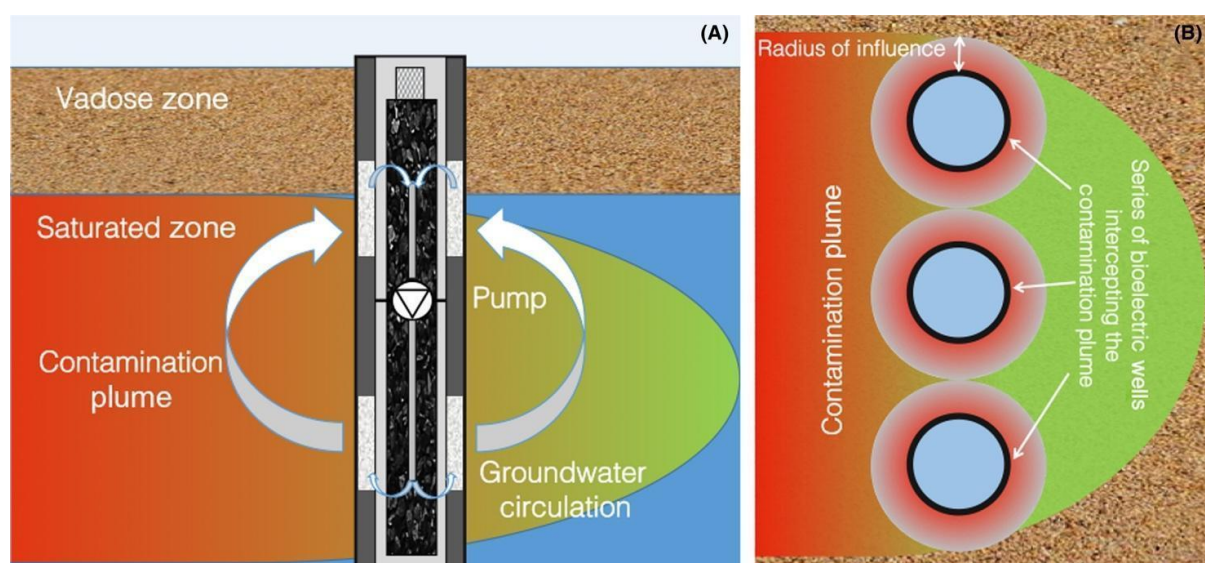
315 Advantages of using PRBs and bio-PRBs are many and include the passive nature of the  
316 technology, which does not require constant energy input, the possibility of combining multiple selective  
317 barriers to sequentially remove a series of contaminants in a plume, the avoidance of GW extraction and  
318 high related energy consumption, the possibility of using the above-ground areas in the remediation site  
319 for other purposes (Obiri-Nyarco et al., 2014; Careghini et al., 2013). Conversely, one disadvantage,  
320 maybe the need for periodical removal/replacement of reactive materials for continuous, long-time  
321 operation.

322 Integration of BESs with PRBs has been proposed by Palma et al. (2018b) as a possible practical  
323 application of their bioelectric well (Figure 4A). Such setup could provide efficient GW treatment and  
324 save pumping energy by using natural flow to achieve contact between substrate and bioelectrodes.  
325 Aquifer natural flow may also (completely or partially) substitute internal recirculation needs, with an  
326 additional decrease in the overall system energy demand.

327 3-D electrodes assembled with innovative materials, such as carbon foam or granular graphite,  
328 could constitute a good candidate for these applications, as they have a porous medium structure that

329 allows water to flow through freely, while still offering a large surface area for biofilm growth, combined  
 330 with excellent electrical conductivity. Microbial populations able to perform direct or indirect electron-  
 331 electrode transfer, necessary for BES establishment, have been already reported to naturally occur in  
 332 GW. These were used as indigenous inocula, meaning that the addition of exogenous bacteria may not  
 333 be necessary (Kirmizakis et al., 2019; Liu et al., 2019; Yang et al., 2015).

334



335

336 **Figure 4:** Scheme of the bioelectrochemical barriers proposed by Palma et al. (2018b).

337

338 One advantage of BES/PRB integration stems from both anode and cathode acting as virtually  
 339 inexhaustible electron sink and donor. Contrary to conventional PRBs, therefore, no replacement of  
 340 reactive materials or chemicals is needed. The build-up of thick biofilms could, however, modify the  
 341 original conductivity of the electrodes, and this may create the necessity of their periodical flushing or  
 342 replacement. On the other hand, Czurda and Haus (2002) reported that integration of electrochemical  
 343 processes in bio-PRBs might in fact reduce fouling induced by excessive microbial growth and remove  
 344 undesired biomolecules and precipitates. Based on this idea, existing permeable barriers may be  
 345 retrofitted and offer new possibilities of enhanced removal by oxidation/reduction of a variety of  
 346 contaminants.

347 Palma et al. (2018a, 2018b) proposed the combined use of multiple units of tubular-designed  
348 bioelectric well. An evolution of this proposed system could be a setup similar to the common funnel-  
349 and-gate or open channel PRB design, able to intercept natural GW flow. (Fig. 4B). Addition of graphene  
350 oxide to enhance treatment performance of these systems was proposed by Camedda et al. (2019).

351

#### 352 **4.2. Complex, multi-contaminant groundwater matrix**

353 Concomitant anthropic activities of different nature (i.e., agriculture, industry) may induce GW  
354 contamination with various pollutants (Bartzas et al., 2015; Han et al., 2016; Venkatramanan et al., 2016).  
355 Therefore, while focusing on single contaminants is useful to assess basic removal pathways and related  
356 kinetics for each solute, results achieved might not be of immediate use for real applications. This is  
357 mainly due to complex interactions that may occur between different contaminants, including conflicting  
358 redox conditions, which may require different remediation techniques. Earlier attempts of using BESs  
359 for the removal of multiple GW contaminants have been reported: Butler et al. (2010) first studied the  
360 interaction and competition of  $\text{NO}_3^-$  and perchlorate as terminal electron acceptors (often associated in  
361 groundwater) in a BES biocathode; Xie et al. (2014) showed inhibition of perchlorate reduction in the  
362 presence of 2.1 mM of  $\text{NO}_3^-$  and its slowed reduction at lower nitrate concentrations. Nguyen et al.  
363 (2016b) studied As oxidation at the anode and denitrification at the cathode of a BES, maintaining strict  
364 streams separation (i.e., anodic and cathodic influents). Competition between vanadium and chromium  
365 in BES cathodes was also investigated (Zhang et al., 2012), while Lai et al. (2015) performed reductive  
366 BES dechlorination of cis-dichloroethylene (cis-DCE) in  $\text{NO}_3^-$  and  $\text{SO}_4^{2-}$  contaminated real GW with  
367 simultaneous reduction of all three compounds. Chromium presence was reported to partially hinder  
368  $\text{NO}_3^-$  removal in an MFC treating synthetic GW at the cathode and remediating sediment at the anode  
369 (Han et al., 2018). Interaction of chromium with other heavy metals during BER was recently reviewed  
370 by Beretta et al. (2019).

371 In order to enhance GW treatment sustainability, multi-contaminant approaches could be of  
372 advantage, exploiting industry-originated organic carbon or organic contaminants sources that are

373 commonly detected in GW (e.g., petroleum hydrocarbons); Liu et al. (2019) reported that anodic  
374 remediation of contaminated sediments, could be another feasible option as anodic electron source.  
375 Potential inhibition effects due to interaction of different contaminants should be assessed: application  
376 of BESs with separated chambers should be evaluated, as separation of reduced and oxidized  
377 contaminants in real conditions is not always feasible as in lab experiments. Flow-through systems,  
378 similar to the one described by Pous et al. (2017), may represent a valid option. The contaminated stream  
379 would first be exposed to the anode, performing oxidation, then to the cathode, where reduction would  
380 occur. Another option is the use anocathophilic bacteria-based systems, employing electrodes as both  
381 electron acceptors and donors based on redox conditions. Examples in this direction have been reported  
382 for biofilms capable of catalyzing organic matter oxidation and  $\text{NO}_3^-$  or chromium reduction (Beretta et  
383 al., 2018; Molognoni et al., 2017; Pous et al., 2016).

384

### 385 **4.3. Contaminants of emerging concern**

386 CECs are a class of substances used for a variety of purposes: personal care, food production, human and  
387 animal health (pharmaceuticals), industrial manufacturing, and fire suppression (Richardson and Kimura,  
388 2017). CECs have been detected in GW worldwide: their presence was reported in Europe (Stuart et al.,  
389 2012), the Americas (Montes-Grajales et al., 2017), Asia (Lapworth et al., 2018), Africa (Arukwe et al.,  
390 2012) and Oceania (Sui et al., 2015), in developed and developing countries alike. Their occurrence in  
391 groundwater is to be ascribed to anthropic activities (Lapworth et al., 2012); therefore, CECs can be used  
392 as tracers to identify GW contamination due to wastewater infiltration and discharges (McCance et al.,  
393 2018). Most of the world population relies on GW use for drinking water supply, and given that CECs'  
394 regulations have not been officially issued at the present time in most countries, much debate on this  
395 sensitive issue is still ongoing (Lapworth et al., 2019).

396 BESs proved the capability to remove some CECs with high efficiency and in some cases higher  
397 than conventional water and wastewater treatments (e.g., biological process). Interesting results were  
398 obtained, particularly in the removal of recalcitrant contaminants with a combination of microbial

399 metabolisms at different redox conditions offered by anode and cathode (Cecconet et al., 2017).  
400 Investigation on CECs removal considering aquifer environment particularities and influence (general  
401 low conductivity, and low concentration of nutrients and organic matter is quite active. Removal of  
402 multiple contaminants in solution, especially when concentrations differ by orders of magnitude, as  
403 discussed in section 4.2., is still an issue that needs great attention.

404

#### 405 **4.4. Energy consumption: the stone guest**

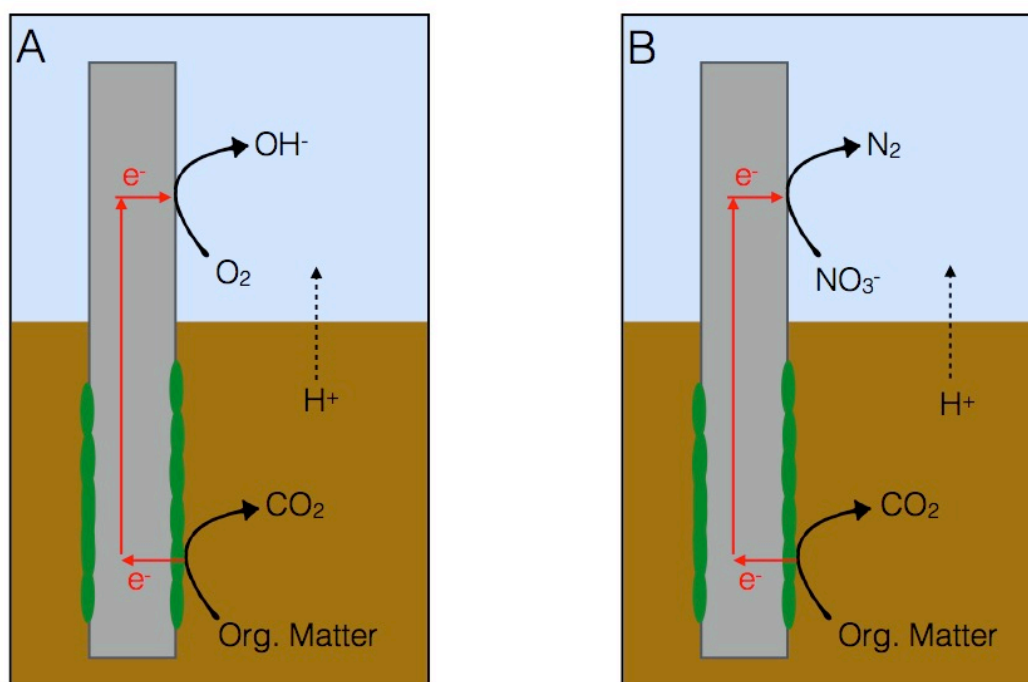
406 Zou and He (2018) recently analyzed the energy sustainability of bioelectrochemical systems for  
407 different applications (desalination, wastewater treatment, hydrogen production) considering additional  
408 energy costs due to recirculation and feeding/extraction of influents/effluents. A similar analysis of *in*  
409 and *ex situ* treatment with MFC and power supply-assisted biocathodes was conducted by Cecconet et  
410 al. (2018d), showing that *in situ* denitrification using MFC can be energy-positive. Performances of  
411 poised biocathodes were far higher than MFC's in terms of nitrogen removal rates (by approx. 30%).  
412 Based on that estimate, it is possible to consider the use of MFC for long-term GW denitrification  
413 applications (or biocathodic reduction of other chemicals). Electrons produced by anodic organic matter  
414 oxidation could be used for cathodic reduction, and the limitation of achievable removal rates would be  
415 acceptable for *in situ* treatment, where the spatial dimensions of contamination are large. One issue to be  
416 addressed is the use of organic matter as anolyte and the need to avoid additional contamination. On the  
417 other hand, in *ex situ* configurations, the use of a poised biocathode would benefit from higher removal  
418 rates, ensuring higher flow rates. A more precise assessment of the real energy consumption of BESs,  
419 taking into account all different aspects, such as recirculation, pumping, etc., could be achieved through  
420 a specific life cycle assessment (LCA) of this technology.

421 Recently, microbial electrochemical snorkel emerged as a novel BES type (Figure 5). A snorkel  
422 is basically a short-circuited MFC, where a microbial anode is directly coupled with a biotic or abiotic  
423 cathode. The snorkel does not produce (or require) power but works continuously at the maximum  
424 current sustainable by the system, and at the same time, performs at maximum electrochemical reaction



425 rate (Hoareau et al., 2019). These systems are characterized by extreme constructive simplicity, as they  
 426 may consist of a single rod of graphite, steel, or carbon, exposed to two different redox environments  
 427 (Viggi et al., 2017, 2015). Snorkels have been used to degrade organic matter in wastewater (Aguirre-  
 428 Sierra et al., 2016) and remove  $\text{NO}_3^-$  from low-organic wastewater, in addition to remediating  
 429 hydrocarbon-contaminated sediments (Yang et al., 2015); promising results have been reported, showing  
 430 removal up to 91% of COD removal and 98% of  $\text{NO}_3^-$  removal, respectively in Aguirre-Sierra et al.  
 431 (2016) and Yang et al. (2015).

432 Snorkels application for GW remediation would allow treatment where no external energy is  
 433 available or provided, and where simplicity could be the primary reason to suggest its use *in situ*. A  
 434 snorkel is a relatively new type of BESs, and some of its operational challenges are still unsolved, such  
 435 as the inability of fully controlling electrode potential, the lack of accurate delimitation of anodic and  
 436 cathodic zones, and the possible presence of oxygen in the anodic zone. Some solutions, contemplating  
 437 system's numerical and mathematical modeling and the use of anocathophilic biofilms, have been  
 438 proposed (Hoareau et al., 2019).



439

440 **Figure 5:** Microbial electrochemical snorkel. (A) Oxygen and (B) nitrate as electron acceptor.



441

#### 442 **4.5. Process modeling**

443 Modeling is an advantageous approach to assess and help understand the behavior of complex systems  
444 in variable conditions. MFC operation and understanding have advanced extensively with the possibility  
445 of predicting organic matter removal and energy production interactions (Capodaglio et al., 2017;  
446 Gadkari et al., 2018; Pinto et al., 2010). MEC and MDC processes have also been successfully modeled  
447 (Ping et al., 2014; Pinto et al., 2011). Latter models evaluated the effects of the integration of BESs with  
448 membrane bioreactors and algal photobioreactors (Li and He, 2016; Luo et al., 2017). Statistical methods  
449 have been applied to BES technology to improve operational knowledge (Ceconet et al., 2018a; Luo et  
450 al., 2016).

451 To date, only limited modeling efforts were reported for BES-based GW remediation. Srinivasan  
452 et al. (2016) developed a model for GW denitrification based on the one proposed by Pan et al. (2013),  
453 which showed competition between  $\text{NO}_3^-$  and  $\text{NO}_2^-$  for electrons in an MFC biocathode. Based on existing  
454 models (Srinivasan et al., 2016; Pan et al., 2013), removal of target GW contaminants could be simulated,  
455 taking into account competition effects between different electron acceptors.

456

#### 457 **4.6. Scaling-up issues**

458 BES applications at full scale for wastewater treatment have been reported (Table 4), but no data are  
459 available for full-scale applications for GW treatment, yet, as most results for such applications are still  
460 at laboratory scale only. Recently, Wang and He (2019) discussed the required dimension BES systems  
461 should reach in order to be considered “pilot scale”, concluding that most examples of pilot scale reactors  
462 cited in literature should not be considered as such, based on practical flow or hydraulic capacity. A pilot  
463 reactor should, in fact, operate at between 0.1 and 5% of the related full scale application flow rate. This  
464 concept is, however, difficult to apply for *in situ* GW bioelectroremediation since the estimation of a  
465 proper reactor flow-rate is not feasible.

466           Conversely, a range of flow rate values can be easily determined for *ex situ*, on-site applications.  
467   In drinking water treatment plants built to serve small or medium communities (with a flow rate in the  
468   500-5000 m<sup>3</sup> d<sup>-1</sup> range), no reported BES study was able to meet the 0.5-250 m<sup>3</sup> d<sup>-1</sup> flow-rate required  
469   for pilot-scale classification. Different considerations emerge in case of decentralized applications:  
470   considering isolated dwellings housing four people, a daily water consumption of 400 L d<sup>-1</sup> can be  
471   estimated based on World Health Organization (WHO) requirements of 100 L d<sup>-1</sup> per capita as daily  
472   minimum water intake (Howard and Bartram, 2003). Therefore, a pilot scale BES reactor for such  
473   decentralized application should guarantee flow rates in the range of 0.4-20 L d<sup>-1</sup>. This condition was  
474   met by BES performing GW denitrification treatment, with flow values exceeding 12 L d<sup>-1</sup> described by  
475   Pous and co-workers (2017). It is possible, therefore, to state that BESs for GW treatment have reached  
476   pilot scale (limited to decentralized applications) and are no longer confined to laboratory settings.

477           Recently, the application of small scale BESs in series has been proposed as an alternative to  
478   sheer size increase for upscaling (Greenman and Ieropoulos, 2017). Serial application of multiple small-  
479   scale BESs may be a feasible option to both remove different contaminants, as in biocathodes poised at  
480   different potentials, each focusing on a specific contaminant, similar to what reported by Huang et al.  
481   (2015) and increase energy production. A comparable sequential approach was tested by Cecconet et al.  
482   (2019b) for GW denitrification. Sequential coupling of two denitrifying biocathodes showed to be  
483   particularly promising in terms of energy sustainability: the specific energy consumption (SEC) of the  
484   system decreased at the increase of the NO<sub>3</sub><sup>-</sup> load, showing that such a system was more energy-efficient  
485   when operated at low HRTs, a highly advantageous aspect in full-scale facilities.

486           Electrical connection of two or more BES units, in series or parallel depending on the final goal,  
487   represents another aspect of the flexibility potential of this technology. Applications of stacked MFCs  
488   have been reported (Kim et al., 2017; Liu et al., 2018), as well as their application to supply sufficient  
489   voltage to MEC processes (Choi et al., 2014; Liu et al., 2016).

490  
491   **Table 4:** Notable examples of full and pilot scale BES. WW: wastewater

BES type	Size (L)	Influent	Modular	N° of modules	Reference
MFC	1000	Brewery WW	Yes	12	Logan (2010)
MFC	90	Brewery WW	Yes	5	Dong et al. (2015)
MFC	200	Municipal WW	Yes	96	Ge and He, (2016)
MFC	250	Municipal WW	No	-	Feng et al. (2014)
MEC	130	Urban WW	Yes	10	Baeza et al. (2017)
MFC	300	Urine	Yes	432	Ieropoulos et al. (2016)
MFC	1000	Artificial and real WW	Yes	50	Liang et al. (2018)
MFC	700	Domestic WW	Yes	18	Valladares Linares et al. (2019)
MES <sup>1</sup>	1500	Municipal WW	Yes	336	He et al. (2019)

492 <sup>1</sup>The reactor indicated as Microbial Electrochemical System (MES), showed setup similar to an MFC.

493

494 Few examples of commercial applications of BES technology have been reported so far (e.g., Plant-e,  
 495 spinoff of Wageningen University, Netherlands; Cambrian Water), mainly related to the production of  
 496 bioenergy using MFCs, or hydrogen production using MECs. The cost of construction materials  
 497 (membrane and electrodes, mainly) is still a hard-to-overcome issue (Foley et al., 2010; Pant et al., 2011),  
 498 and only large-scale commercialization of BESs could lower those costs. An alternative could be  
 499 represented by the adoption of natural materials in place of membranes and electrodes (Goglio et al.,  
 500 2019), but these still offer far lower performance than engineered or conventional materials. Based on  
 501 these considerations, major drops of the materials' costs (i.e., membranes) are needed in order to allow  
 502 BES to become an established technology for GW denitrification.

503

#### 504 **4.7. Biosensing**

505 Recently, much attention has been attracted by the development of BES-based biosensors for  
 506 environmental monitoring (Capodaglio et al., 2016; Ivars-Barceló et al., 2018). Therefore, research has  
 507 also addressed specific applications for contaminant detection and monitoring in GW. Velasquez-Orta et  
 508 al. (2017) designed an MFC-based biosensor for the online monitoring of fecal and organic pollution in  
 509 shallow wells, obtaining responsive increases in current output; the system was sensitive to temperature

510 fluctuations but not to changes in salinity or modifications of external resistance (and longer wiring for  
511 electrodes' connections). Field tests highlighted the influence on measurements of water level  
512 oscillations in wells, causing air exposition at the cathode (Velasquez-Orta et al., 2017).

513 Organic matter presence in aquifers undergoing bioremediation was ascertained by an increase  
514 in current density in BES-based biosensors; current quickly dropped when organic matter presence  
515 ceased, suggesting that the system was able to monitor subsurface microbial activity during *in situ*  
516 bioremediation (Williams et al., 2010). Electrodes produced a detectable current, despite the long  
517 distance between anode and cathode (6 m), with electron transfer attributed to *Geobacter* species  
518 (Williams et al., 2010).

519 Bio-current generated by a bioanode poised at +0.2 V vs. SHE was reported being linearly  
520 correlated with the increase in the concentration of biogenic Fe(II), serving as an indicator. Fe(II) is a  
521 widely used chemical in GW remediation, and the system showed it could monitor its concentration in a  
522 reliable way (Feng et al., 2013). A BES-based arsenite (As) biosensor was developed by Webster et al.  
523 (2014) using an engineered *Shewanella oneidensis* strain. The sensor allowed an As detection limit of 40  
524  $\mu\text{M}$  and a linear range up to 100  $\mu\text{M}$ . Another BES-based biosensor, able to monitor  $\text{NO}_3^-$  in real-time  
525 was proposed by Su et al. (2019); it was however designed for monitoring secondary WWTP effluents,  
526 hence requiring organic matter as the driving energy input. As such, this design could not be suitable for  
527 GW monitoring. Biosensors developed to monitor microbial activity in anoxic sediments (Wardman et  
528 al., 2014) could, however, with some setup modifications, be applied to GW monitoring.

529 The development of BES-based biosensors is of extreme interest to the research community, due  
530 to the possibility of operating in off-grid and decentralized applications, and their suitability for *in situ*  
531 and on-site test monitoring, in addition to their faster response time and lack of advanced technological  
532 skills requirements, compared to conventional analytical techniques (Grattieri et al., 2017). BES-based  
533 biosensors could ideally complement any remediation processes, allowing low-cost, long-term  
534 monitoring of underground processes. Specifically, the applications developed by Williams et al. (2010)  
535 and Wardman et al. (2014) could properly assist *in situ* bioelectroremediation. Distance between

536 electrodes would not be of concern, as it minimally, or not at all, affects sensing ability as reported in  
537 Velasquez-Orta et al. (2017) and Williams et al. (2010).

538

## 539 **5. Conclusions**

540 Among different technologies applicable for *in situ* treatment of contaminated GW, BESs showed to be  
541 a suitable and feasible option. Analysis of the different setups reported so far in literature highlighted the  
542 crucial need of robust and proper BES design for operation in a harsh and challenging environment such  
543 as an aquifer, and that simple adaptation of *ex situ* BES setups may not be sufficient to achieve the desired  
544 results.

545 Research in the field so far focused mainly on denitrification and hydrocarbons removal, showing  
546 excellent results due to the interaction of microbial metabolism and poised electrodes. In the near future  
547 there will likely be a shift of focus towards emerging topics such as interactions between multiple  
548 contaminants (both reduced and oxidized), accurate estimation of energy consumption for *in situ* BES  
549 remediation, development of reliable models to simulate and predict process behavior and the possible  
550 combination of BESs with PRBs for passive remediation of contaminated plumes. *In situ* process  
551 monitoring with biosensors is also emerging as an active investigation field. Integration of research gaps  
552 in existing BES technology could lead to the rapid development of reliable and resilient systems for *in*  
553 *situ* bioelectroremediation.

554

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565

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