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To cite this article: Baturalp Atakav *et al* 2020 *Mater. Res. Express* 7 026549

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OPEN ACCESS

RECEIVED

5 November 2019

REVISED

28 January 2020

ACCEPTED FOR PUBLICATION

6 February 2020

PUBLISHED

17 February 2020

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Keywords: A356, Sr modification, bifilm, porosity

Abstract

Strontium modification of Al–Si alloys has known to have several beneficial effects such as increased feedability, the formation of fibrous Si and increased mechanical properties. However, in the presence of Sr, during melting and holding durations, the oxide structure of the dross may change which leads to several problems during casting operations. In this work, the amount of Sr was changed and the melt was held for 1 h. Reduced Pressure Test (RPT) was used to assess melt quality change and it was found that cleanliness was increased due to the fading of Sr.

1. Introduction

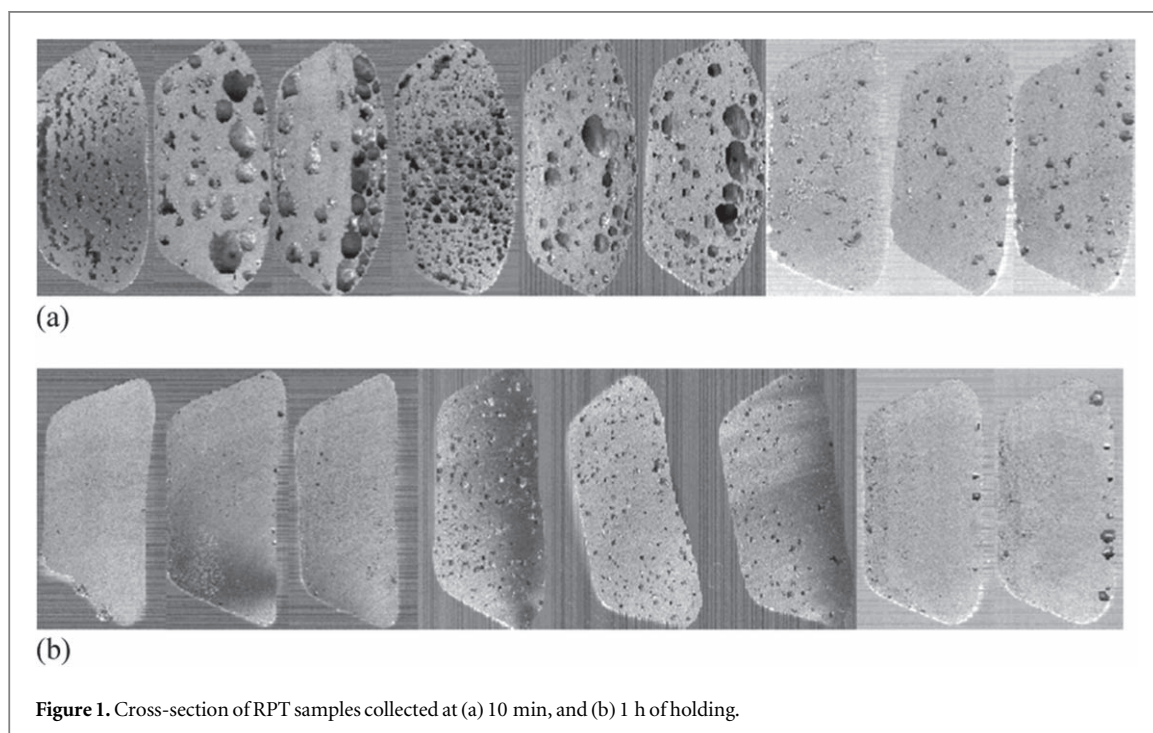
One of the most prominent features of aluminium is its lightweight and variability in its mechanical properties by the addition of alloying elements. A356 alloy generally has high elongation values, good machinability with high strength values. Its ductility can be improved by Ti addition as a grain refiner and Sr addition as Si modifier [1]. However, one of the defects that deteriorate the properties of cast Al-alloys is porosity. Porosity is formed by the presence of bifilms [2, 3]. Turbulence is the major source of bifilm formation. When surface oxide of the melt is entrained into the melt, the two non-wetted sides of the oxides come in contact to form the bifilm defect which deteriorates the properties of the cast part. Therefore, it is important that these defects are not formed, or removed from the melt prior to casting.

There is a long going discussion in the literature as to whether Sr modification increases pore formation or not [4–9]. Some researchers claimed that Sr addition alters the surface tension of the melt and thus enhances pore formation. Some conclude that feedability increases with Sr modification and thus porosity is decreased. De Giovanni [10] used x-ray tomography for the visualisation of pores in Sr containing Al–Si alloys. It was found that porosity was increased with increased Sr and pores were associated with intermetallics. Barrirero [11] and Fortini [12] also found similar results. Nampoothiri [13] claimed that Sr was beneficial for eutectic modification, however, porosity was increased and localised particularly in the interdendritic region. They also claimed that by ultrasonic treatment of the melt, bifilms were broken up and oxides had become smaller and less harmful for mechanical properties. Samuel [14] showed that porosity was increased by Sr modification and pores had become more spherical. Nateghian [15] had found that Al₂O₃ was transformed into SrO when Sr content was as low as 50 ppm and after 5 h of holding, these oxides bond to each other which is known as ‘healing’ of the bifilms. Chen [16] reported that bifilm quantity and amount of porosity was increased when A356 was modified with Sr.

As summarised above, the reported results in the literature are based on the findings of the final cast part. In this work, the aim was targeted to characterise the effect of Sr on the quality assessment of liquid metal cleanliness. Therefore, in this work, an excess amount of Sr was added to A356 and pore formation was investigated by means of duration and holding time of the liquid metal. Reduced pressure test (RPT) method was used and bifilm index was measured in order to quantify the porosity and melt cleanliness. Bifilm index is the sum of the maximum length of pores measured in millimetres from the sectioned surface of the RPT samples. A356 alloy was used in the studies and the chemical composition is given in table 1.

Table 1. Chemical composition of A356 (wt%).

Si	Fe	Cu	Mn	Zn	Ti	Al
6.8	0.35	0.02	0.03	0.04	0.04	Rem.

**Figure 1.** Cross-section of RPT samples collected at (a) 10 min, and (b) 1 h of holding.

Excess Sr addition and its effect on A356 is examined in this study. 1 wt% Sr was targeted by using Al–10Sr master alloy where there was no Sr in the melt as can be seen in table 1. Typical addition values are between 200–400 ppm of Sr, therefore the terminology ‘excess’ was used in this work. 2 kg of charge was melted in a graphite crucible in a resistance furnace at 775 °C. Although this temperature is higher than the usual standard applications, for this work, the selection of such high temperature was based on the particular foundry which was working at this temperature. Samples were collected from the melt to be solidified in RPT machine in a steel cup. The dimension of the mould was 34 mm diameter at the bottom, 44 mm diameter on top with a height of 30 mm.

3 consecutive tests were carried out and 3 RPT samples were collected to be solidified in the steel cup under 100 mbar at each time. Consecutive sample collection was carried out one after another, after 10 min and 1 h of holding time. The delay between the RPT sampling was 5 min. Bifilm index was measured from the cross-section of these samples and Weibull statistics were used to evaluate the results.

The cross-section of RPT samples collected after 10 min and 1 h of holding is given in figure 1.

Bifilm index change of the melts cast after 10 min and 1 h of holding of 1 wt% Sr added A356 alloy is given in figure 2.

As can be seen in figure 2, there is a significant difference between the bifilm index of two melts: 10 min and 1 h of holding. The average bifilm index is around 250 mm for 10 min held melt and it is around 50 mm for 1 h held melt. There are five times difference between the quality which indicates that in the presence of excess Sr, holding time of the melt can significantly increase the melt quality.

Another interesting observation is the decrease in bifilm index after the duration of melt as the consecutive castings were followed. This gives another indication that melt quality was improving as the holding time was increased. The decrease in 1 h holding of the melt is more predominant. After the 8th sample, the bifilm index of 1 h and 10 min of holding becomes very close to each other. This shows that the change in bifilm quantity in the presence of Sr is so rapid and after a long period of holding, it stabilises; just like the observation reported for 1 h holding duration, the bifilm index is almost constant around 50 mm.

The scatter of the data was also analysed by Weibull distributions which are given in figures 3 and 4. In these figures, P is the probability calculated by Hazen method [17]. As can be seen in figure 3, The reproducibility of the bifilm index for 10 min and 1 h holding time is almost the same. Nevertheless, the difference between the values is almost five times and the data are parallel to each other.

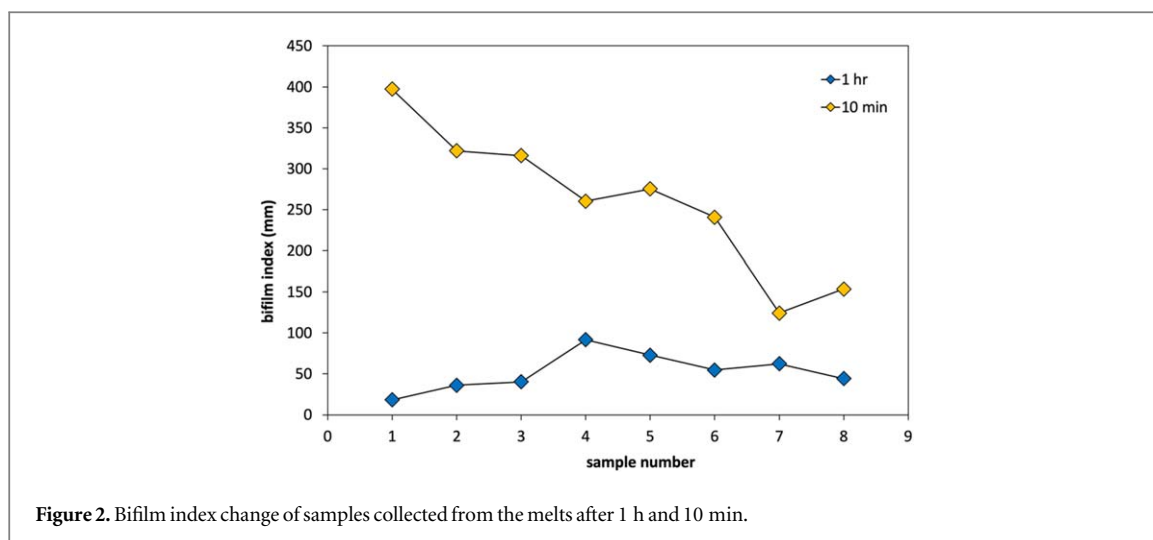


Figure 2. Bifilm index change of samples collected from the melts after 1 h and 10 min.

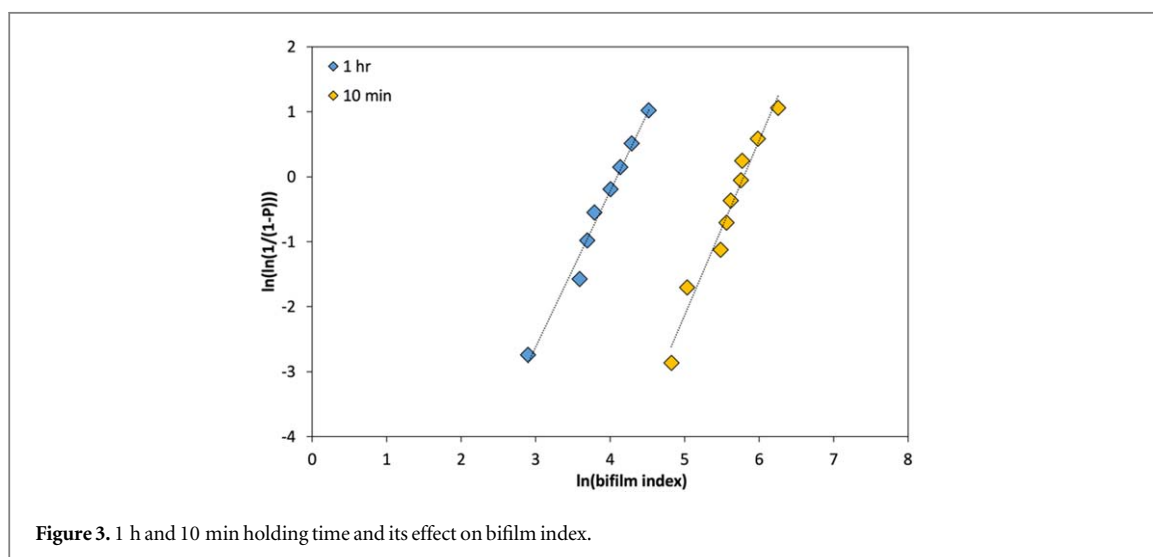


Figure 3. 1 h and 10 min holding time and its effect on bifilm index.

Bifilm index is measured by the pore length from the cross-section of RPT samples. In addition, the number of bifilm can also be calculated. These results are given in figure 4 which is quite similar to bifilm index measurements.

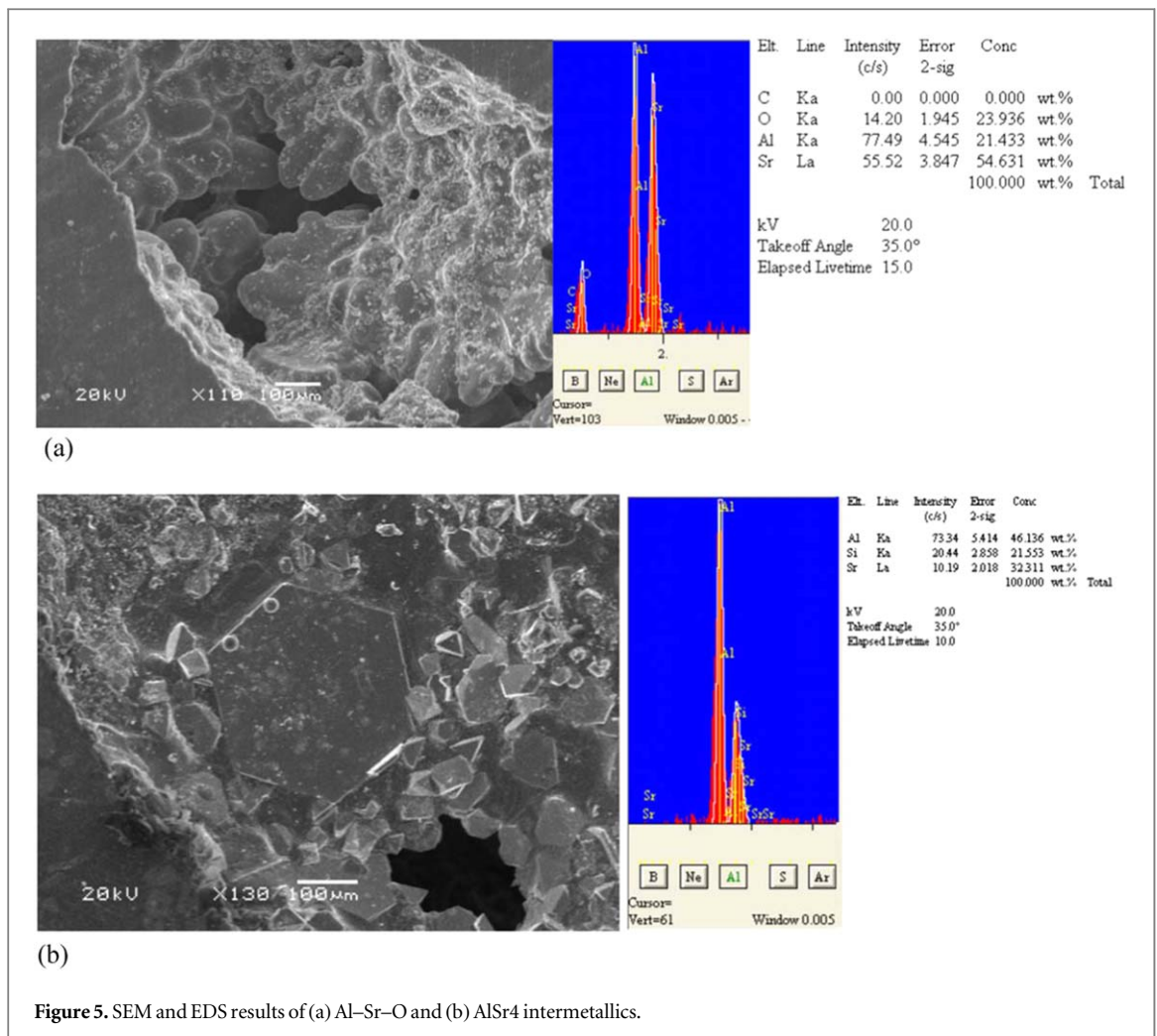
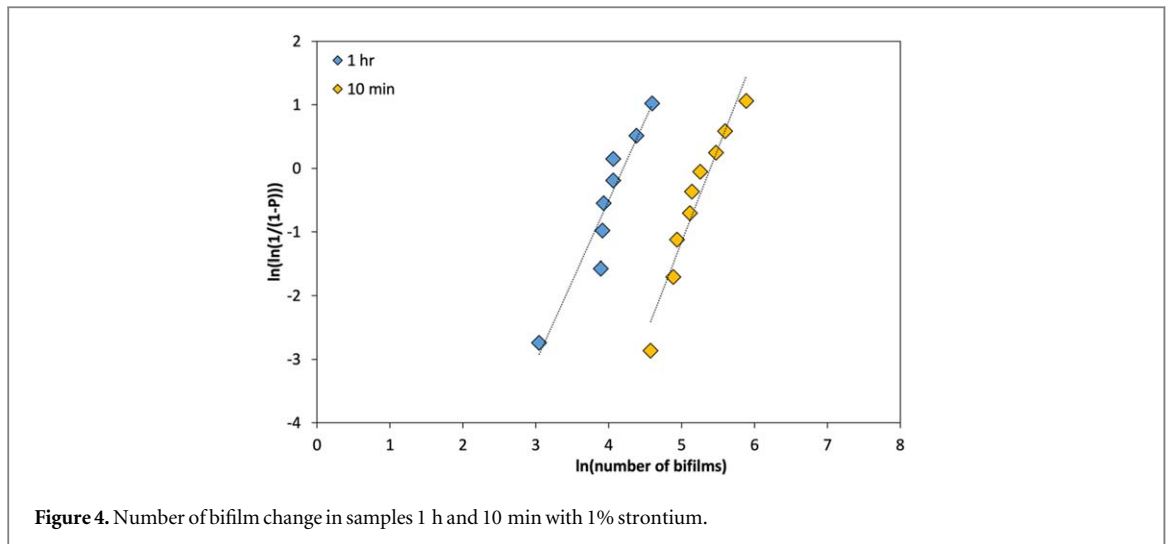
As seen from figure 3, the change in the number of bifilms after 1 h of holding time reveals that actually the number of bifilms were decreased which caused the increase in the melt quality. A possible reason for the decreased number of bifilms can be explained by the formation of $\text{SrO} \cdot \text{Al}_2\text{O}_3$ spinel oxide which sediments to the bottom of the crucible. SEM images and EDS analysis in figure 5 shows SrO and presence of Al–Sr and Al–Si–Sr intermetallics. The main observation can be seen on the RPT samples cross-sections (figure 1) where the size of pores is getting smaller and the number of pores is decreasing. Uludag [18] had reported a similar finding where the Sr modified melt had shown an increased number of smaller pores. Liu [8] also reported the same findings. Additionally, hydrogen builds up in between the bifilms may result in the floatation of bifilms to the surface which also increases melt cleanliness. Denton [19] had shown that hydrogen pick-up was increased in Sr modified melts. Eguskiza [20] had shown that Sr was fading after 5 h of holding.

Sr modification leads to smaller, fragmented and higher number of bifilms. Hence, bifilm index is decreased which leads to improved melt quality. It was found that the size of pores decrease and the number of pores increase as the holding duration of Sr-containing A356 is increased. Thus, melt quality starts to increase.

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References

- [1] Sigworth G K and Kuhn T A 2007 Grain refinement of aluminum casting alloys *Int. J. Met.* **1** 31–40
- [2] Campbell J 2003 *Castings*
- [3] Dispinar D and Campbell J 2004 Critical assessment of reduced pressure test: I. Porosity phenomena *Int. J. Cast Met. Res.* **17** 280–6
- [4] Farhoodi B, Raiszadeh R and Ghanaatian M-H 2014 Role of double oxide film defects in the formation of gas porosity in commercial purity and Sr-containing Al alloys *J. Mater. Sci. Technol.* **30** 154–62
- [5] Espinoza-Cuadra J, Gallegos-Acevedo P, Mancha-Molinar H and Picado A 2010 Effect of Sr and solidification conditions on characteristics of intermetallic in Al-Si 319 industrial alloys *Mater. Des.* **31** 343–56

- [6] Timelli G, Caliarì D and Rakhmonov J 2016 Influence of process parameters and Sr addition on the microstructure and casting defects of LPDC A356 alloy for engine blocks *J. Mater. Sci. Technol.* **32** 515–23
- [7] Uludağ M, Çetin R, Dispınar D and Tiryakiođlu M 2018 The effects of degassing, grain refinement & Sr-addition on melt quality-hot tear sensitivity relationships in cast A380 aluminum alloy *Eng. Fail. Anal.* **90** 90–102
- [8] Liu L, Samuel A M, Samuel F H, Doty H W and Valtierra S 2003 Influence of oxides on porosity formation in Sr-treated Al–Si casting alloys *J. Mater. Sci.* **38** 1255–67
- [9] Samuel A M, Pennors A, Villeneuve C, Samuel F H, Doty H W and Valtierra S 2000 Effect of cooling rate and Sr-modification on porosity and Fe–intermetallics formation in Al–6.5% Si–3.5% Cu–Fe alloys *Int. J. Cast Met. Res.* **13** 231–53
- [10] De Giovanni M, Warnett J M, Williams M A and Srirangam P 2017 3D imaging and quantification of porosity and intermetallic particles in strontium modified Al–Si alloys *J. Alloys Compd.* **727** 353–61
- [11] Barrirero J et al 2016 Cluster formation at the Si/liquid interface in Sr and Na modified Al–Si alloys *Scr. Mater.* **117** 16–9
- [12] Fortini A, Lattanzi L, Merlin M and Garagnani G L 2018 Comprehensive evaluation of modification level assessment in Sr-modified aluminium alloys *Int. J. Met.* **12** 697–711
- [13] Nampoothiri J, Balasundar I, Raj B, Murty B S and Ravi K R 2018 ‘Porosity alleviation and mechanical property improvement of strontium modified A356 alloy by ultrasonic treatment *Mater. Sci. Eng. A* **724** 586–93
- [14] Samuel A M, Doty H W, Valtierra S and Samuel F H 2017 Porosity formation in Al–Si sand mold castings *Int. J. Met.* **11** 812–22
- [15] Nateghian M, Raiszadeh R and Doostmohammadi H 2012 Behavior of double-oxide film defects in Al-0.05 wt pct Sr alloy *Metall. Mater. Trans. B* **43** 1540–9
- [16] Chen Q and Griffiths W D 2017 The effect of Sr modifier additions on double oxide film defects in 2L99 alloy castings *Metall. Mater. Trans. A* **48** 5688–98
- [17] Kirtay S and Dispınar D 2012 Effect of ranking selection on the Weibull modulus estimation *Gazi Univ. J. Sci.* **25** 175–87
- [18] Uludağ M, Çetin R, Dispınar D and Tiryakiođlu M 2017 Characterization of the effect of melt treatments on melt quality in Al-7 wt % Si–Mg alloys *Metals (Basel)*. **7** 157
- [19] Denton J R and Spittle J A 1985 Solidification and susceptibility to hydrogen absorption of Al–Si alloys containing strontium *Mater. Sci. Technol.* **1** 305–11
- [20] Eguskiza S, Niklas A, Fernández-Calvo A I, Santos F and Djurdjevic M 2015 Study of strontium fading in Al-Si-Mg AND Al–Si–Mg–Cu alloy by thermal analysis *Int. J. Met.* **9** 43–50