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# Gain dynamics in a highly ytterbium-doped potassium double tungstate thin-film amplifier

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## ABSTRACT

Active media with high rare-earth concentrations are essential for small-footprint waveguide amplifiers. When operating at high population inversion, such devices are often affected by undesired energy-transfer processes and thermal effects. In this work, we study a 32- $\mu\text{m}$ -thick epitaxial layer of potassium gadolinium ytterbium double tungstate with a high Yb content of 57at.%, representing an  $\text{Yb}^{3+}$  concentration of  $\sim 3.8 \times 10^{21}$  per cubic centimeter, grown onto an un-doped  $\text{KY}(\text{WO}_4)_2$  substrate. The pump absorption, luminescence decay, and small-signal gain are investigated under intense pumping conditions. Spectroscopic signatures of an energy-transfer process and of quenched ions, as well as thermal effects are observed. We present a gain model which takes into account excessive heat generated due to the abovementioned experimental observations. Based on finite-element calculations, we find that the net gain is significantly reduced due to, firstly, a fraction of  $\text{Yb}^{3+}$  ions not contributing to stimulated emission, secondly, a reduction of population inversion owing to a parasitic energy-transfer process and, thirdly, degradation of the effective transition cross-sections owing to device heating. Nevertheless, a signal enhancement of 8.1 dB was measured from the sample at 981 nm wavelength when pumping at 932 nm. The corresponding signal net gain of  $\sim 800$  dB/cm, which was achieved without thermal management, is promising for waveguide amplifier operating without active cooling.

**Keywords:** Rare-earth-doped materials, integrated optics materials, optical amplifiers, ytterbium lasers.

## 1. INTRODUCTION

Potassium rare-earth double tungstate crystals doped with ytterbium,  $\text{KRE}(\text{WO}_4)_2:\text{Yb}^{3+}$ , have been widely used for microchip [1,2], mode-locked [3], and high-power lasers [4,5]. The  $\text{KRE}(\text{WO}_4)_2:\text{Yb}^{3+}$  gain medium exhibits transition cross-sections significantly higher than those of many other  $\text{Yb}^{3+}$ -doped materials, such as  $\text{YAG}:\text{Yb}^{3+}$  [6,7]. By use of a lattice-engineering approach [8,9,10], a crystalline waveguiding epitaxial layer with high amounts of  $\text{Yb}^{3+}$  ions can be grown onto an undoped  $\text{KY}(\text{WO}_4)_2$  substrate, enabling efficient continuous-wave (CW) [11] and  $Q$ -switched [12,13,14]  $\text{KRE}(\text{WO}_4)_2:\text{Yb}^{3+}$  planar waveguide lasers. By further micro-structuring of the  $\text{KRE}(\text{WO}_4)_2:\text{Yb}^{3+}$  waveguide layer, low-threshold [15], high-efficiency [16], and tunable [17] channel waveguide lasers can be realized. A record-high net gain of 935 dB/cm at 981 nm wavelength was achieved in a  $\text{KRE}(\text{WO}_4)_2$  waveguide amplifier with 47.5at.%  $\text{Yb}^{3+}$ , which is equivalent to a concentration as high as  $\sim 3.0 \times 10^{21} \text{ cm}^{-3}$  [18]. Such a compact waveguide amplifier operating at  $\sim 1000$  nm wavelength is beneficial for scaling of short-reach interconnects in photonic integrated circuits, high-performance computing systems, and data centers [19,20,21,22]. As the net gain achieved in  $\text{KRE}(\text{WO}_4)_2:\text{Yb}^{3+}$  is more than an order-of-magnitude higher than those of other singly-doped  $\text{Nd}^{3+}$  or  $\text{Yb}^{3+}$  gain media [23,24,25,26], it is worthwhile to investigate the gain properties of  $\text{KRE}(\text{WO}_4)_2:\text{Yb}^{3+}$  epitaxial layers with further increased  $\text{Yb}^{3+}$  concentration.

Operating a heavily doped device under high excitation density is challenging. A power-dependent non-exponential decay behavior was reported in  $\text{YbAG}$  crystals, indicating the presence of a parasitic energy-transfer process [27]. Quenched ions with a short excited-state lifetime were identified in various  $\text{Er}^{3+}$ - [28,29,30,31] and  $\text{Yb}^{3+}$ -doped [32,33,34] materials. These ions can induce nonsaturable pump absorption [28,34]. Various abnormalities associated with thermal effects were

reported in thin-disc gain media with high  $\text{Yb}^{3+}$  concentrations. An additional decay process with large heat generation was observed in a  $\text{YAG}:\text{Yb}^{3+}$  laser at high excitation density, resulting in limited gain and reduced laser efficiency [35]. Excessive heat generation leading to the termination of CW operation and a rapid decline in lasing power [36] was observed in a laser based on a  $\text{KLu}(\text{WO}_4)_2:(52\text{at.}\%)\text{Yb}^{3+}$  epitaxial layer. A similar observation was reported from laser experiments in a  $\text{KYb}(\text{WO}_4)_2$  crystal, in which a short pump-pulse duration was needed to minimize thermal effects [37]. Most of these abnormalities were studied based on device performance. There are limited reports on the investigation of their origin [38].

We investigate [39] the gain dynamics in a  $\text{KGd}_{0.43}\text{Yb}_{0.57}(\text{WO}_4)_2$  (i.e., 57at.%  $\text{Yb}^{3+}$ ) epitaxial layer, representing a high ytterbium concentration of  $\sim 3.8 \times 10^{21} \text{ cm}^{-3}$ . Power-dependent luminescence-decay and pump-absorption measurements are performed to identify potential energy-transfer and fast quenching processes. A gain model which accounts for an energy-transfer process, quenched ions, and thermal effects is established. The modeled and experimental gain results are compared to obtain further insight into the achievable gain in  $\text{KGd}_{0.43}\text{Yb}_{0.57}(\text{WO}_4)_2$  without thermal management.

## 2. EXPERIMENTAL

A  $\text{KGd}_{0.43}\text{Yb}_{0.57}(\text{WO}_4)_2$  layer was grown onto a  $\text{KY}(\text{WO}_4)_2$  substrate by liquid-phase epitaxy [6,10], resulting in a layer thickness of  $\sim 32 \mu\text{m}$  after polishing. The sample was mounted on a small holder made of thin copper plates with a clear aperture of  $\sim 8.6 \text{ mm} \times 8.6 \text{ mm}$ . No special thermal management was applied to the sample during all measurements. A confocal luminescence-lifetime measurement setup [40] was used for power-dependent luminescence-decay measurements. The confocal measurement suppresses radiation trapping [41] and allows for investigation of the decay-time behavior under high excitation density. A diode pump laser at 981 nm was modulated at 233 Hz with 50% duty cycle to allow for complete relaxation of the  $\text{Yb}^{3+}$  ions between two excitation pulses. The experimental setup for signal-enhancement measurement included a CW Ti:Sapphire laser at 932 nm for pumping at the local absorption peak of  $\text{KGd}_{0.43}\text{Yb}_{0.57}(\text{WO}_4)_2$  at  $\sim 932 \text{ nm}$ . The signal beam at  $\sim 981 \text{ nm}$ , exploiting the high emission cross-section [6], with a bandwidth  $\leq 1 \text{ nm}$  from a supercontinuum light source passed through a monochromator was mechanically chopped at 233 Hz for lock-in detection to discriminate the detected 981 nm wavelength signal from spontaneous emission produced by the sample and from different background noise sources. A small launched signal power ( $< 100 \text{ nW}$ ) was used to ensure signal amplification within the small-signal-gain regime. Pump and signal beams were combined and focused perpendicularly onto the sample at  $E\parallel N_m$  polarization using a microscope objective (MO). To ensure a good overlap of pump and signal beams, the foci were characterized using a beam profiler and the beam-expander optics were adjusted for optimal beam overlap. The residual optical beams passing through the sample were collected using another MO and directed to a spectrometer equipped with a cooled InGaAs detector. Combination of a pump filter with cutoff wavelength at 950 nm and the spectrometer ensured that only the 981 nm signal was detected. Pump-transmission measurements were performed with only the pump beam switched on, to deduce the pump power absorbed by the sample. Near-infrared luminescence spectra were measured using the same setup by launching only the pump beam. The luminescence spectra were corrected for spectral response of the detection system determined using a calibration lamp.

## 3. GAIN MODEL

Since the energy-level scheme of the  $\text{Yb}^{3+}$  ion consists only of the  $^2\text{F}_{7/2}$  ground-state and the  $^2\text{F}_{5/2}$  excited-state manifolds, a two-level system is used to model the gain and loss of optical beams. The  $\text{Yb}^{3+}$  ions excited to the upper Stark level of the  $^2\text{F}_{5/2}$  manifold undergo a rapid relaxation to the lower Stark level of the same manifold. The gain model is modified from [28]. It takes into account two distinct classes of  $\text{Yb}^{3+}$  ions, namely active ions and quenched ions, which both participate in pump absorption. The active ions decay by infrared luminescence to the ground state with an excited-state luminescence lifetime  $\tau_a$ . The quenched ions have a non-radiative lifetime  $\tau_q$  which is significantly shorter than  $\tau_a$ . The total density of active and quenched ions residing in the ground state and excited state follows

$$N_{0a/q} + N_{1a/q} = f_{a/q} N_{\text{Yb}} \quad (1)$$

where  $N_{\text{Yb}}$  is the density of  $\text{Yb}^{3+}$  ions and  $N_0$  and  $N_1$  are the respective density of ions in the ground state and excited state. The subscripts  $a$  and  $q$  indicate active and quenched ions, respectively.  $f_{a/q}$  represents the fraction of active or quenched ions, with the boundary condition of  $f_a + f_q = 1$ . The rate constants of absorption and stimulated emission on the 932 nm pump transition,  $R_{p,01}$  and  $R_{p,10}$ , and the 981 nm signal transition,  $R_{s,01}$  and  $R_{s,10}$ , respectively, are calculated as [42,43]

$$R_{p,01} = I_p \sigma_{abs}(\lambda_p, T) \cdot \frac{\lambda_p}{hc}, \quad R_{p,10} = I_p \sigma_{em}(\lambda_p, T) \cdot \frac{\lambda_p}{hc}, \quad R_{s,01} = I_s \sigma_{abs}(\lambda_s, T) \cdot \frac{\lambda_s}{hc}, \quad R_{s,10} = I_s \sigma_{em}(\lambda_s, T) \cdot \frac{\lambda_s}{hc} \quad (2)$$

where  $I$  represents the intensity,  $h$  is Planck's constant, and  $c$  is the speed of light.  $\sigma_{abs}$  and  $\sigma_{em}$  are the effective absorption and emission cross-sections, respectively, at wavelength  $\lambda$  and temperature  $T$ . The subscripts  $p$  and  $s$  denote pump and signal, respectively. Considering that both pump and signal beams possess a Gaussian beam profile in the  $x$ - $y$  plane, their lateral intensity profiles,  $I_{p,s}$ , can be modeled with

$$I_{p,s} = \left(2P_{p,s} / \pi w_{p,s}^2\right) \exp\left[-2(x^2 + y^2) / w_{p,s}^2\right] \quad (3)$$

where  $P$  represents the optical power and  $w$  denotes the Gaussian beam waist. The parameters  $N$ ,  $\sigma$ ,  $R$ , and  $I$  in Eqs. (1)–(3) are spatially dependent. The  $xyz$  discretization for these parameters is taken into account. The rate equations which govern the change of density of the  $\text{Yb}^{3+}$  ions in the two energy levels are

$$\begin{aligned} \frac{dN_{1a/q}}{dt} &= (R_{p,01} + R_{s,01})N_{0a/q} - (R_{p,10} + R_{s,10})N_{1a/q} \\ &\quad - \frac{N_{1a/q}}{\tau_{a/q}} - 2W_{ET}(N_{1a/q})^2 \end{aligned} \quad (4)$$

$$\frac{dN_{0a/q}}{dt} = -\frac{dN_{1a/q}}{dt} \quad (5)$$

Besides the pump and signal transitions which are typical for the rate equations of  $\text{Yb}^{3+}$ -doped materials, the model includes an energy-transfer (ET) process identified in our pump-dependent luminescence-decay measurements. The physical origin of this ET process is currently unknown. However, since the luminescence-decay curves exhibit the typical shape of a Bernoulli curve, see Eq. (7), we chose Grant's model [44] which assumes an infinitely fast energy-migration rate. The ET process is taken into account by the term  $2W_{ET}N_{1a}^2$ , where  $W_{ET}$  is the macroscopic ET parameter. This is similar to a cooperative-upconversion process between two neighboring  $\text{Yb}^{3+}$  ions or an energy-transfer-upconversion process between neighboring  $\text{Er}^{3+}$  ions in the upper amplifier level [28]. Consequently, the evolution of excited-state population density after cut-off of pump power during luminescence-decay measurements is modeled with [45]

$$\frac{dN_{1a}(t)}{dt} = -\frac{N_{1a}(t)}{\tau_a} - 2W_{ET}N_{1a}^2(t) \quad (6)$$

which can be solved as

$$N_{1a}(t) = \frac{N_{1a}(0) \exp(-t/\tau_a)}{1 + 2W_{ET}N_{1a}(0)\tau_a [1 - \exp(-t/\tau_a)]} \quad (7)$$

$N_{1a}(0)$  represents the density of active excited ions at time zero. It can be estimated by varying the excitation conditions. The value of  $W_{ET}$  can be quantified via simultaneous fitting of luminescence-decay curves measured under different excitation conditions. The solutions of Eqs. (4)–(5) can be simplified in the case of small-signal amplification. The quenched ions only participate in the absorption of pump and signal photons. Under CW pumping, the steady-state condition  $dN/dt = 0$  applies. Thus,  $N_{1a}$  in Eq. (4) can be solved as

$$N_{1a} = \frac{-B_a + \sqrt{B_a^2 - 4AC_a}}{2A} \quad (8)$$

where

$$A = 2W_{ET}, \quad B_a = R_{p,10} + R_{p,01} + \frac{1}{\tau_a}, \quad C_a = -f_a N_{Yb} R_{p,01} \quad (9)$$

for calculations including the ET process, and

$$N_{1a} = \frac{R_{p,01}}{R_{p,01} + R_{p,10} + \tau_a^{-1}} \quad (10)$$

for calculations excluding the ET process. The evolution of pump power  $P_p$  and signal power  $P_s$  along the propagation direction  $z$  is calculated according to

$$\frac{dP_p}{dz} = \left[ \sigma_{em,p} N_{1a} - \sigma_{abs,p} (N_{0a} + f_q N_{Yb}) \right] P_p - \alpha_p P_p \quad (11)$$

$$\frac{dP_s}{dz} = \left[ \sigma_{em,s} N_{1a} - \sigma_{abs,s} (N_{0a} + f_q N_{Yb}) \right] P_s - \alpha_s P_s \quad (12)$$

where  $\alpha_{p/s}$  is the propagation-loss coefficient in the medium and  $\sigma_{abs/em,p/s}$  denotes  $\sigma_{abs/em}(\lambda_{p/s}, T)$ . Since the propagation loss for devices made of KRE(WO<sub>4</sub>)<sub>2</sub>:Yb<sup>3+</sup> at ~1000 nm wavelength is typically < 0.04 dB/cm [15], both  $\alpha_p$  and  $\alpha_s$  are considered to be negligible (i.e.,  $\alpha_p = \alpha_s = 0$ ) as compared to the absorption and emission terms in Eqs. (11)–(12).

To account for thermal effects, the power per unit volume deposited as heat in the device is determined by [46,47]

$$Q_{th}(x, y, z) = \eta_h \alpha_{abs,p} I_p(0) \exp(-\alpha_{abs,p} z) \quad (13)$$

where  $\eta_h$  is the fractional heat load and  $\alpha_{abs,p}$  is the pump-absorption coefficient with a magnitude given by the expression within the square bracket in Eq. (11).  $I_p(0)$  represents the incident pump intensity at  $z = 0$  with a Gaussian profile as described by Eq. (3). The fractional heat load  $\eta_h$  represents the fraction of absorbed pump power per unit volume which is converted into heat. It consists of the fractional heat loads originating in the quantum defect,  $\eta_{QD}$ , the ET process,  $\eta_{ET}$ , and the rapid quenching process,  $\eta_q$ :

$$\eta_h = f_a (\eta_{QD} + \eta_{ET}) + f_q \eta_q \quad (14)$$

The quantum defect is defined by the fractional amount of absorbed photon energy which is converted to heat due to the difference of energy between the absorbed and emitted photons

$$\eta_{QD} = 1 - \lambda_p / \lambda_m \quad (15)$$

where  $\lambda_m$  is the mean emission wavelength estimated using

$$\lambda_m(T) = \int \lambda \sigma_{em}(\lambda, T) d\lambda / \int \sigma_{em}(\lambda, T) d\lambda \quad (16)$$

$\lambda_m$  is chosen, because, in contrast to a laser, an amplifier operating in the small-signal-gain regime does not possess a single dominating emission wavelength. The chosen values are  $\eta_{QD} = \eta_{ET} = 6.4\%$  and  $\eta_q = 100\%$  (for further explanations, see the Appendix). The temperature profile of the sample is governed by the heat-conduction equation and the boundary conditions between sample and external environment where heat exchange occur [48],

$$-k_{th} \nabla^2 T(x, y, z) = Q_{th}(x, y, z) \quad (17)$$

$$\frac{\partial T}{\partial n} = h_T (T_{ext} - T) \quad (18)$$

where  $k_{th}$  is the thermal conductivity,  $n$  is the normal to the boundary surface,  $h_T$  is the heat transfer coefficient, and  $T_{ext}$  is the external temperature of the thermal contact. The three-dimensional optical-beam and thermal profiles were solved using a finite-element method. Material parameters are given in [39].

## 4. RESULTS AND DISCUSSION

Luminescence-decay curves under different pump power  $P_p$  are shown in Fig. 1(a). At a low  $P_p$  of 1.44 mW, the decay curve is close to an exponential decay. With increasing  $P_p$ , the detected decay curves exhibit an increasingly non-exponential decay, indicating that an ET process is present. By simultaneously fitting the eight decay curves shown in Fig. 1(a) using Eq. (7), a  $W_{ET}$  value of  $1.3 \times 10^{-18}$  cm<sup>3</sup>/s is extracted. The presence of an energy-transfer process in an Yb<sup>3+</sup>-activated material is intriguing, as the Yb<sup>3+</sup> ion has only two manifolds within the 4f sub-shell. A power-dependent non-exponential decay behavior similar to that observed in the present work was reported in YbAG crystals [27] and was attributed to cooperative energy transfer from two Yb<sup>3+</sup> ions to an Yb<sup>2+</sup> ion. However, the presence of Yb<sup>2+</sup> has not been reported in KRE(WO<sub>4</sub>)<sub>2</sub>:Yb<sup>3+</sup>, although it is known to exist in certain as-grown crystals such as YAG:Yb<sup>3+</sup> [49] and LuAG:Yb<sup>3+</sup> [50]. Since the experimental data can be well described by Bernoulli's Eq. (7), the energy transfer is possibly caused by cooperative upconversion involving two neighboring excited Yb<sup>3+</sup> ions, jointly emitting one green photon [51]. However, we have detected only very weak green upconversion luminescence. At present, the exact physical mechanism responsible for the observed behavior remains unclear.

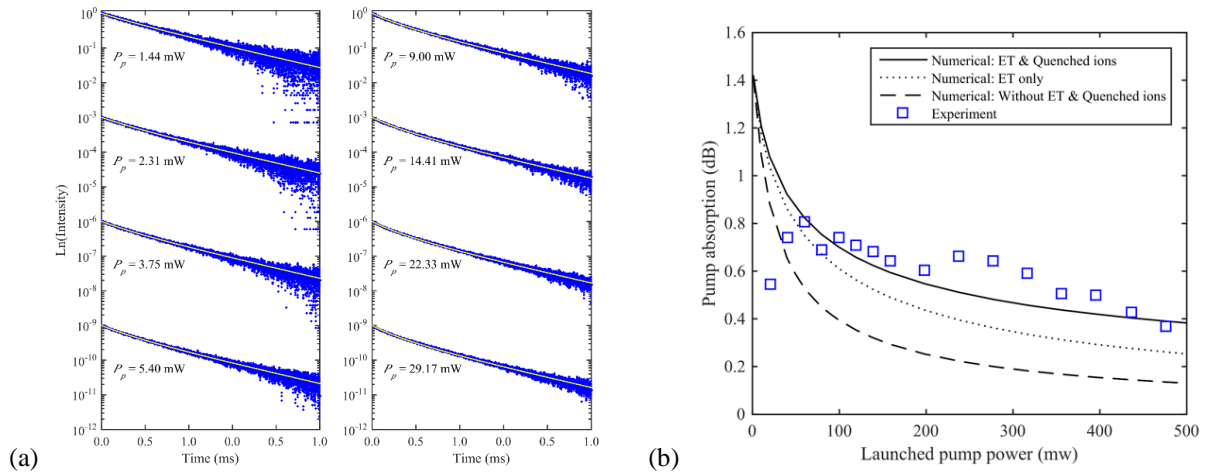


Figure 1. (a) Luminescence-decay curves (blue) measured with different launched diode-laser power  $P_p$ . The yellow lines represent fitted curves using Eq. (7). (b) Comparison of experimental pump-absorption data (squares) and pump-absorption results calculated with various settings (lines). The dashed line represents the modeled result without considering the ET process and quenched ions (i.e.,  $W_{ET} = 0$  and  $f_q = 0$ ). The dotted line shows the modeled result which accounts for the ET process but not the quenched ions (i.e.,  $W_{ET} = 1.3 \times 10^{-18}$  cm<sup>3</sup>s<sup>-1</sup> and  $f_q = 0$ ). The solid line is calculated with the consideration of both the ET process and quenched ions ( $W_{ET} = 1.3 \times 10^{-18}$  cm<sup>3</sup>s<sup>-1</sup> and  $f_q = 0.15$ ). (Figure taken from Ref. [39].)

It is apparent from Eq. (13) that heat generation in the sample depends on absorbed pump power. The pump absorption at 932 nm wavelength is investigated by comparing experimental and numerical results. The measured data points of pump absorption versus launched pump power are plotted in Fig. 1(b) as squares. The pump absorption is defined as

$$A_p = -10 \log_{10} \left[ \frac{P_p(t_{layer})}{P_p(0)} \right] \quad (19)$$

where  $P_p(0)$  is the launched Ti:Sapphire pump power at the front surface.  $P_p(t_{layer})$  is the residual pump power at the rear surface. The calculated pump absorption using various sets of parameters are shown as lines in Fig. 1(b). These results take into account the pump-induced heating, the changes of effective transition cross-sections due to temperature-dependent Boltzmann populations and transition linewidths, as well as thermal conductivities due to the heat generated.

The result calculated without both ET process and quenched ions [dashed line in Fig. 1(b)] show a more intense saturation of pump absorption than the experimental results. The ET process, as identified in the previous sub-section, serves as an additional decay channel from the excited state. Therefore, the pump absorption (dotted line) is increased because a larger amount of ions is available in the ground state. Additional nonsaturable pump absorption is addressed by considering that ~15% of the Yb<sup>3+</sup> ions are rapidly quenched, in addition to the ET process. In Al<sub>2</sub>O<sub>3</sub>:Yb<sup>3+</sup>, a similar nonsaturable absorption was observed and attributed to 11% of Yb<sup>3+</sup> ions being quenched at a dopant concentration of  $6.6 \times 10^{20}$  cm<sup>-3</sup> [34]. The pump absorption calculated under consideration of these two factors is shown as a solid line in Fig. 1(b) and is in reasonable agreement with the experimental results.

Figure 2(a) shows the near-infrared luminescence spectra at various launched pump-power values  $P_p$ . Three emission peaks are observed at  $\sim 981$  nm,  $\sim 1000$  nm, and  $\sim 1023$  nm wavelengths, which correspond to the  $E_{10} \rightarrow E_{00}$ ,  $E_{10} \rightarrow E_{01}$ , and  $E_{10} \rightarrow E_{02}$  transitions, respectively, see the inset of Fig. 2(a). With increasing pump power, a smoothing emission spectrum is observed and the emission peaks at 1000 nm and 1023 nm wavelengths become less distinguishable. In addition, the ratio of the magnitude of the 981 nm emission peak to that of the 1000 nm emission peak decreases with increasing  $P_p$ . Analysis of the spectra was performed via multiple-peak fitting by assuming three Lorentzian peaks. The full-width-at-half-maximum (FWHM) values for the emission peak at 981 nm for different  $P_p$  values are plotted in Fig. 2(b). A significant increase in FWHM is evident. The linewidth broadening is in line with the temperature-dependent behavior of the emission cross-section spectra [6], signifying that a thermal effect is present in the gain medium even under low  $P_p$ .

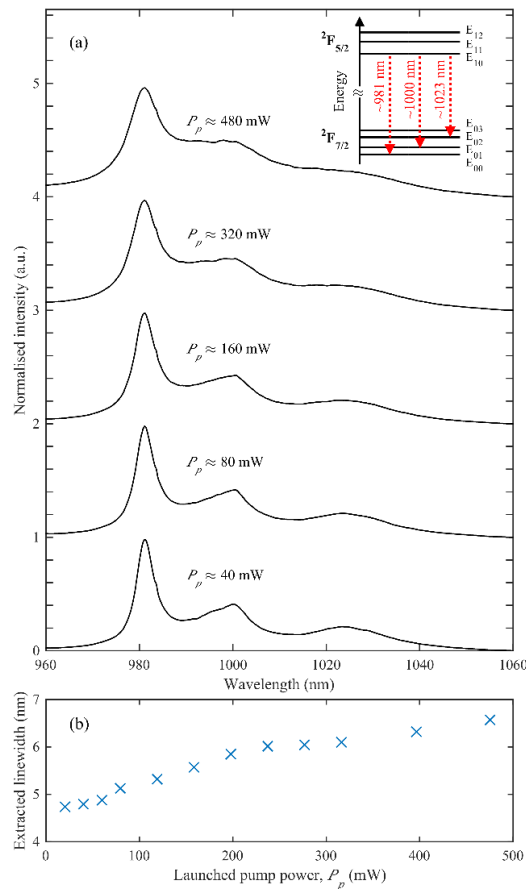


Figure 2. (a) Normalized luminescence spectra recorded with different Ti:Sapphire launched pump power  $P_p$ . The inset illustrates the relevant transitions contributing to a large part of the observed emission at the corresponding wavelength. (b) Evolution of the linewidth (FWHM) of the decomposed peak at  $\sim 981$  nm with increasing  $P_p$ . (Figure taken from Ref. [39].)

The experimental and modeled signal-enhancement results are shown in Fig. 3(a). The maximum signal enhancement measured at  $\sim 475$  mW launched pump power is 8.13 dB. The modeled signal enhancement under consideration of the ET process, 15% quenched ions, and thermal effects is in reasonable agreement with the experimental results. The calculation shows that  $T_p$  can rise from  $27^\circ\text{C}$  with pump off to  $62.8^\circ\text{C}$  at  $P_l = 475$  mW. Considering in Eq. (22) the reduced absorption cross-section of  $1.058 \times 10^{-19} \text{ cm}^2$  calculated at  $T_p = 62.8^\circ\text{C}$ , a total signal absorption of 5.59 dB is deduced. Consequently, a peak net-gain value of 2.54 dB, or 793.75 dB/cm, is obtained based on the signal-enhancement data.

Comparison of the modeled gain in Fig. 3(b) reveals a marked difference in gain performance when considering the usual gain model for  $\text{Yb}^{3+}$ -doped media and our proposed model. The usual gain model does not include an ET process and quenched ions, hence the heat generation is mainly owing to the quantum defect which is inherently low in  $\text{Yb}^{3+}$ -doped devices. The peak gain deduced from such a model (dashed line) is  $\sim 1900$  dB/cm at  $P_l = 500$  mW. Our gain model includes

an ET process, which causes depletion of the excited-state population. Consideration of 15% of quenched ions implies that only the remaining 85% of active ions are participating in the signal-amplification process. The increased heating reduces the transition cross-sections. The gain calculated with the proposed model (solid line) is effectively clamped to  $\sim 820$  dB/cm at 500 mW of launched pump power. Nevertheless, the net gain per unit length is more than an order of magnitude higher than in other Yb<sup>3+</sup>- or Nd<sup>3+</sup>-doped waveguide amplifiers [23,24,25,26] and comparable to the modal gain of III-V semiconductor amplifiers.

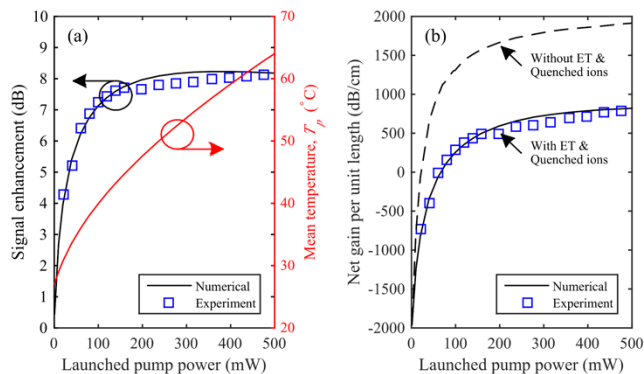


Figure 3. (a) Experimental and modeled signal enhancement. The calculated mean temperature within the pump volume is shown on the right y-axis. (b) Corresponding results of net gain per unit length. The net gain per unit length calculated without considering the ET process and quenched ions is shown in (b) as a dashed line. (Figure taken from Ref. [39].)

## 5. SUMMARY

The optical properties of a KGd<sub>0.43</sub>Yb<sub>0.57</sub>(WO<sub>4</sub>)<sub>2</sub> epitaxial film with an Yb<sup>3+</sup> concentration as high as  $\sim 3.8 \times 10^{21}$  cm<sup>-3</sup> were examined. A parasitic energy-transfer process and quenched ions were observed under intense excitation conditions, and the relevant parameters were quantified. The broadening of emission spectra signifies the presence of thermal effects even at low pump power. A gain model which takes into account the energy-transfer process, quenched ions, and thermal effects provides insight into the impact of these non-desired effects on the attainable gain in an epitaxial film with high Yb<sup>3+</sup> concentration. The temperature of the pumped volume may elevate to  $>60^\circ\text{C}$ . A peak signal enhancement of 8.13 dB is obtained at 981 nm. A peak net-gain of  $\sim 800$  dB/cm is attainable.

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