

Effect of plumes on measuring the large scale circulation in turbulent Rayleigh-Bénard convection

Richard J. A. M. Stevens, Herman J. H. Clercx, and Detlef Lohse

Citation: *Phys. Fluids* **23**, 095110 (2011); doi: 10.1063/1.3620999

View online: <http://dx.doi.org/10.1063/1.3620999>

View Table of Contents: <http://pof.aip.org/resource/1/PHFLE6/v23/i9>

Published by the [American Institute of Physics](#).

Related Articles

Effects of thermal gradients on the intensity of vortices generated in a cylindrical annulus
[Chaos](#) **21**, 043132 (2011)

Horizontal structures of velocity and temperature boundary layers in two-dimensional numerical turbulent Rayleigh-Bénard convection
[Phys. Fluids](#) **23**, 125104 (2011)

Direction of scalar transport in turbulent channel flow
[Phys. Fluids](#) **23**, 115105 (2011)

Internal heating driven convection at infinite Prandtl number
[J. Math. Phys.](#) **52**, 093101 (2011)

Heat transfer and pressure drop through rectangular helical ducts
[J. Renewable Sustainable Energy](#) **3**, 043119 (2011)

Additional information on Phys. Fluids

Journal Homepage: <http://pof.aip.org/>

Journal Information: http://pof.aip.org/about/about_the_journal

Top downloads: http://pof.aip.org/features/most_downloaded

Information for Authors: <http://pof.aip.org/authors>

ADVERTISEMENT



**Running in Circles Looking
for the Best Science Job?**

Search hundreds of exciting
new jobs each month!

<http://careers.physicstoday.org/jobs>

physicstodayJOBS



Effect of plumes on measuring the large scale circulation in turbulent Rayleigh-Bénard convection

Richard J. A. M. Stevens,¹ Herman J. H. Clercx,^{2,3} and Detlef Lohse¹

¹*Physics of Fluids Group, Faculty of Science and Technology, Impact and MESA+ Institutes & Burgers Center for Fluid Dynamics, University of Twente, 7500AE Enschede, The Netherlands*

²*Department of Applied Mathematics, University of Twente, P.O. Box 217, 7500 AE Enschede, The Netherlands*

³*Department of Physics and J. M. Burgers Centre for Fluid Dynamics, Eindhoven University of Technology, P.O. Box 513, 5600 MB Eindhoven, The Netherlands*

(Received 10 January 2011; accepted 12 April 2011; published online 28 September 2011)

We studied the properties of the large-scale circulation (LSC) in turbulent Rayleigh-Bénard (RB) convection by using results from direct numerical simulations in which we placed a large number of numerical probes close to the sidewall. The LSC orientation is determined by either a cosine or a polynomial fit to the azimuthal temperature or azimuthal vertical velocity profile measured with the probes. We study the LSC in $\Gamma = D/L = 1/2$ and $\Gamma = 1$ samples, where D is the diameter and L is the height. For $Pr = 6.4$ in an aspect ratio $\Gamma = 1$ sample at $Ra = 1 \times 10^8$ and 5×10^8 , the obtained LSC orientation is the same, irrespective of whether the data of only 8 or all 64 probes per horizontal plane are considered. In a $\Gamma = 1/2$ sample with $Pr = 0.7$ at $Ra = 1 \times 10^8$, the influence of plumes on the azimuthal temperature and azimuthal vertical velocity profiles is stronger. Due to passing plumes and/or the corner flow, the apparent LSC orientation obtained using a cosine fit can result in a misinterpretation of the character of the large-scale flow. We introduce the relative LSC strength, which we define as the ratio between the energy in the first Fourier mode and the energy in all modes that can be determined from the azimuthal temperature and azimuthal vertical velocity profiles, to further quantify the large-scale flow. For $Ra = 1 \times 10^8$, we find that this relative LSC strength is significantly lower in a $\Gamma = 1/2$ sample than in a $\Gamma = 1$ sample, reflecting that the LSC is much more pronounced in a $\Gamma = 1$ sample than in a $\Gamma = 1/2$ sample. The determination of the relative LSC strength can be applied directly to available experimental data to study high Rayleigh number thermal convection and rotating RB convection. © 2011 American Institute of Physics. [doi:10.1063/1.3620999]

I. INTRODUCTION

Rayleigh-Bénard (RB) convection is the motion of a fluid contained between two parallel plates which is heated from below and cooled from above.^{1–3} A well established feature of the dynamics of the system is the large-scale circulation (LSC). It plays an important role in natural phenomena, including convection in the Arctic ocean, in Earth's outer core, in the interior of gaseous giant planets, and in the outer layer of the Sun. The properties of the LSC have recently been intensively studied in experiments,^{4–24} numerical simulations,^{18,25–28} and models.^{12–14,18,21,24,29–32} For a complete overview of all literature in which certain aspect of the LSC are studied, we refer to the recent review of Ahlers, Grossmann, and Lohse.¹

In experiments, the LSC is measured by using thermistors that are embedded in the sidewall, see e.g., Ref. 33, or by using small thermistors that are placed in the flow at different azimuthal positions and different heights, see e.g., Ref. 19. Since the LSC transports warm (cold) fluid from the bottom (top) plate up (down) the side wall, the thermistors can detect the location of the up-flow (down-flow) by showing a relatively high (low) temperature. In addition, there have also been a number of direct measurements of the LSC by particle image velocimetry (PIV) and laser Doppler

velocimetry (LDV) (see, for example, Refs. 5, 7, and 34) that complement the thermistor method.

In this paper, we investigate the properties of the LSC with results from direct numerical simulations (DNSs). Though DNSs are limited both in Ra and in duration, i.e., in number of LSC turnover times, to smaller values than the experimental analogues, the advantage is that in contrast to the experiments the full spatial information is available. We will take advantage of this in order to verify the algorithms employed in experiments to identify the LSC orientation based on a limited number of probes. We will introduce two existing methods to determine the LSC orientation over time. The first method⁹ determines the LSC orientation from a cosine fit to the azimuthal temperature profile measured with the probes. This method has been extremely successful in revealing important features, i.e., azimuthal meandering, reversals, and cessations, of the LSC.^{9,11,12,17} In the second method, the LSC orientation is determined by using a second order polynomial fit around the maximum and the minimum. Using this method, the sloshing mode of the LSC, which is caused by an off-center motion of the LSC, was discovered.^{19–21} We note that this cannot be obtained by the cosine fit method as this method assumes that there is no off-center motion of the LSC.

So far these procedures have been applied to experimental data where the data of 8 azimuthally equally spaced

probes were available. The benefit of the simulations over the experiments is that it is easy to place a large number of probes in the flow. Here, we placed up to 64 azimuthally equally spaced numerical probes at different heights into the numerical RB sample. With an arrangement of up to 64 probes, we can determine how the extracted information on the LSC and plume dynamics depends on the number of probes that is used. We also visualized the flow by movies that show the flow dynamics in horizontal or vertical planes, see the accompanying supplementary material.³⁵

The paper is organized as follows. In Sec. II, we start with a discussion of the numerical method that has been used. This is followed in Sec. III by a discussion of the traditional methods that are used in experiments to determine the LSC orientation. Based on the results obtained by these methods, we discuss the characteristics of the LSC in a $\Gamma = 1$ (Sec. IV) and $\Gamma = 1/2$ (Sec. V) sample. An important question for both high Ra number^{36–38} and rotating RB convection^{22,23} is whether or not there is a single LSC present. Therefore, we will discuss a new method in Sec. VI, which is based on the energy in the different Fourier modes of the azimuthal temperature and azimuthal vertical velocity profile, to determine whether a single LSC is present. In Sec. VII, we will look into time resolved properties of the LSC. The general conclusions of this paper will be presented in Sec. VIII.

II. NUMERICAL METHOD AND PROCEDURE

The flow is solved by numerically integrating the three-dimensional unsteady Navier-Stokes equations within the Boussinesq approximation. For a detailed discussion of the numerical code, we refer to Refs. 25, 37, 39, and 40. The flow is simulated in a cylindrical sample in order to keep the geometry identical to the one used in most experiments. In Refs. 22, 37, and 38, we have shown that simulation results obtained with this code agree excellent with experimental results. The cases we studied are based on the most common experimental setups that are available, namely $Pr \approx 6.4$ and $Pr \approx 0.7$ at an aspect ratio $\Gamma = D/L$ of 1 and 1/2. A detailed overview of the simulations can be found in Table I.

In the simulations, we placed up to 64 azimuthally equally spaced numerical probes per horizontal plane that provide simultaneous point-wise measurements of the temperature and the three velocity and vorticity components at

TABLE I. The columns from left to right indicate the following: Ra , Pr , Γ , the number of grid points in the azimuthal, radial, and axial directions ($N_\theta \times N_r \times N_z$). The last two columns indicate the relative LSC strength determined using Eq. (2), see Sec. VI, using the data of only 8 ($\bar{S}_m(8)$) and all 64 ($\bar{S}_m(64)$) probes in the horizontal midplane, respectively.

Ra	Pr	Γ	$N_\theta \times N_r \times N_z$	$\bar{S}_m(8)$	$\bar{S}_m(64)$
1×10^8	6.4	1.0	$257 \times 129 \times 257$	0.74	0.70
1×10^8	6.4	1.0	$385 \times 193 \times 385$	0.65	0.68
5×10^8	6.4	1.0	$257 \times 129 \times 257$	0.68	0.73
5×10^8	6.4	1.0	$385 \times 193 \times 385$	0.70	0.76
1×10^8	0.7	1/2	$193 \times 65 \times 257$	0.45	0.57
1×10^8	0.7	1/2	$257 \times 97 \times 385$	0.42	0.54
1×10^8	6.4	1/2	$193 \times 65 \times 257$	0.06	0.27

the heights $0.25L$, $0.50L$, and $0.75L$ and a distance $0.45D$ from the cylinder axis. Grid refinement tests were performed because the region close to the sidewall, where the LSC properties are sampled, is most sensitive from a resolution point of view.³⁷ The simulations are fully resolved according to the criteria of Stevens *et al.*³⁷ and the LSC properties we find do not depend on the grid resolution. Note that the azimuthal and radial number of grid points required to get the same resolution with respect to the turbulent length scales is less for the $\Gamma = 1/2$ cases than for the $\Gamma = 1$ cases because for the latter a larger horizontal extent has to be simulated.

III. METHODS TO DETERMINE THE LSC ORIENTATION

Following Ahlers and coworkers,^{1,9,12} the orientation and strength of the LSC can be determined by fitting the function

$$\theta_i = \theta_m + \delta_m \cos(\phi_i - \phi_m) \quad (1)$$

to the temperatures recorded by the numerical probes at the height $z = 0.5L$ and the azimuthal positions $\phi_i = 2i\pi/n_p$, where n_p indicates the number of probes. The three parameters θ_m , δ_m , and ϕ_m are obtained from least square fits. Here, δ_m is a measure of the temperature amplitude of the LSC and ϕ_m is the azimuthal orientation of the LSC at midheight. The azimuthal average of the temperature at the horizontal midplane is given by θ_m . We calculated temperatures θ_t and θ_b , orientations ϕ_t and ϕ_b , and amplitudes δ_t and δ_b for the top and bottom levels at $z = 0.75L$ and $z = 0.25L$ separately by the same method. For experiments,^{1,9,12} exactly this method is applied to the data of 8 equally spaced thermistors, see Figure 1.

A second method that is applied to determine the LSC orientation is to make a polynomial fit around the sensor that records the highest (lowest) temperature.^{19,20} Finally, since we have a large number of numerical probes, i.e., up to 64 azimuthally equally spaced per horizontal level, we also determine the LSC orientation by finding the probe that records the highest (lowest) temperature. Again the LSC orientation based on these two methods is determined separately for all three levels, see Figure 1.

To distinguish the different methods, we introduce a notation with a second index, i.e., $\phi_{*,[c,p,m]}$. Here, c indicates that ϕ is determined using a cosine fit to the azimuthal temperature profile, p that ϕ is determined using a polynomial fit around the maximum (or minimum) observed in the azimuthal profile, and m indicates that the maximum (or minimum) observed in the azimuthal profile is used. Because the numerical probes record both the temperature and vertical velocity component, we use both to determine the LSC orientation. In the rest of the paper, we will use the notation $\phi_{*,*}^T$ to indicate that the orientation is based on the azimuthal temperature profile and $\phi_{*,*}^W$ when it is based on the azimuthal vertical velocity profile. Hence, ϕ has three indices, i.e., $\phi_{1,2}^3$, see Table II for a detailed overview. In the rest of the paper, we will indicate the numerical value of an index when this index is varied.

Because the numerically obtained azimuthal profiles can be very noisy, we applied a moving averaging filter to the

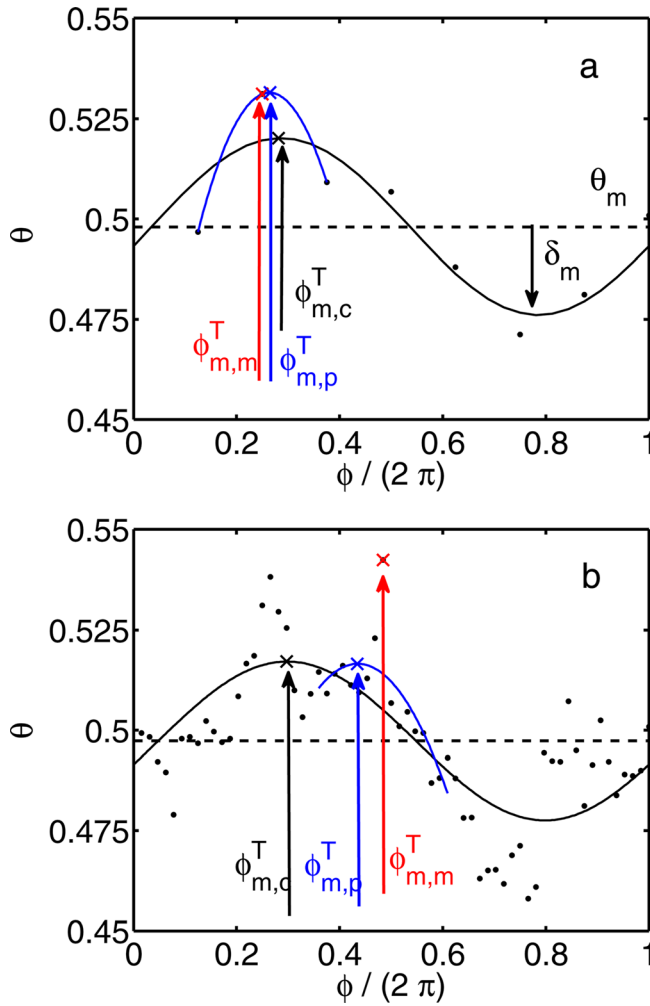


FIG. 1. (Color online) Azimuthal temperature profile averaged over $4\tau_f$ at midheight for $Ra = 5 \times 10^8$, $Pr = 6.4$, and $\Gamma = 1$. The measured data from the numerical probes are indicated by the dots. The solid black line shows the cosine fit (Eq. (1)) to the data with offset θ_m (dashed line) and amplitude δ_m . The black cross indicates the position of $\phi_{m,c}^T$. The red cross indicates the position of the probe that records the highest temperature and thus the position of $\phi_{m,m}^T$. The blue solid line gives the polynomial fit around the maximum. Its maximum, indicated by the blue cross, indicates the position of $\phi_{m,p}^T$. The $\phi(x)$ range that is considered in the polynomial fit is $a/2\pi$. Panels a and b show the procedure applied to the data of 8 and 64 equally spaced probes at midheight, respectively. The corresponding azimuthal vertical velocity profiles are given in Figure 8.

TABLE II. The LSC orientation in this paper is determined from the azimuthal temperature or azimuthal vertical velocity profile with different methods. In addition, the LSC orientation is also determined at different heights. As explained in the text this information is indicated in the notation $\phi_{1,2,3}^T$. In this table, the meaning of the symbols at the index locations 1, 2, and 3 is summarized.

Index	Symbol	Meaning
1	b	Height $0.25L$
1	m	Height $0.50L$
1	t	Height $0.75L$
2	c	Cosine fit
2	p	Polynomial fit
2	m	Maximum
3	T	Azimuthal temperature profile
3	w	Azimuthal vertical velocity profile

data obtained from the numerical probes to eliminate the detection of very small plumes. In experiments, these events are not detected anyhow by thermistors, since these need time to react to temperature changes in the flow. We decided to apply a moving averaging filter of $4\tau_f$, where τ_f is defined with respect to the free-fall velocity U_f as $\tau_f = L/U_f$ (L is the height of the sample). Recently, Bailon-Cuba *et al.*⁴¹ showed the characteristic convective velocity U_c of the LSC is approximately $U_f/5$ for the parameter ranges $Ra = 10^7-10^9$, $\Gamma = 1/2-12$, and $Pr = 0.7$. This means that the LSC turnover time τ_{LSC} defined as $\tau_{LSC} = 2L/U_c$ is about $10\tau_f$.

IV. RESULTS FOR $\Gamma = 1$

Figure 2 shows the typical behavior of the LSC orientation for $Pr = 6.4$ in a $\Gamma = 1$ sample. The figure shows $\phi_{m,2}^T$ and $\phi_{m,2}^w$. In order to show that the LSC orientation based on the temperature and the vertical velocity data is almost identical, we consider first a long averaging time ($50\tau_f$). The results are displayed in Figures 2(a) and 2(b). The similarity is expected since the LSC carries warm fluid from the bottom plate up the sidewall and vice versa. To show the influence of this long time averaging, we show $\phi_{m,2}^w$ based on the

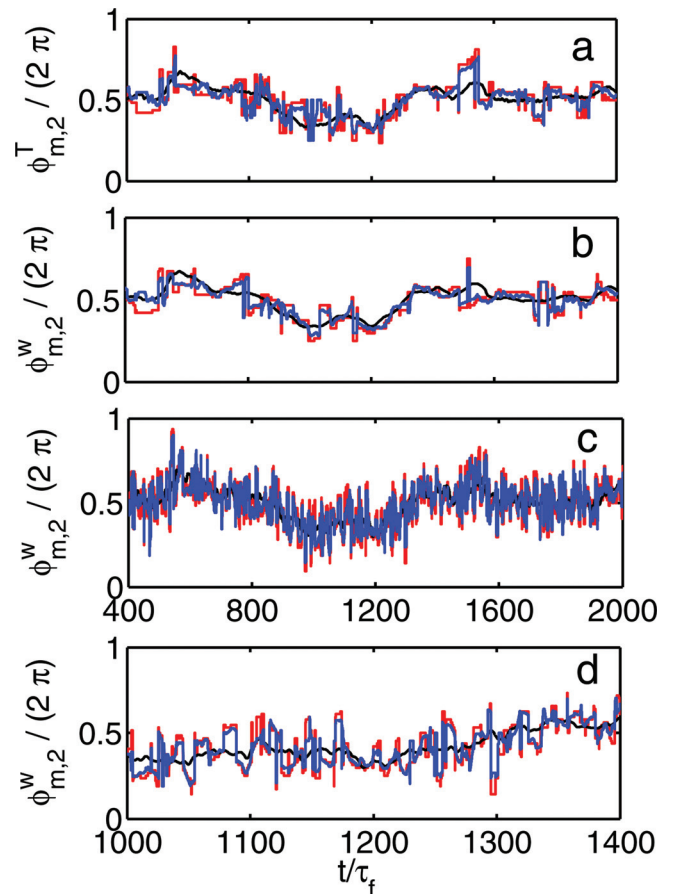


FIG. 2. (Color) The LSC orientation for $Ra = 1 \times 10^8$, $Pr = 6.4$, and $\Gamma = 1$ on the $257 \times 129 \times 257$ grid based on the data of 64 azimuthally equally spaced probes per horizontal level. The black, red, and blue lines indicate $\phi_{m,c}^3$, $\phi_{m,m}^3$, and $\phi_{m,p}^3$, respectively. (a) $\phi_{m,2}^T$ based on the azimuthal temperature profile averaged over $50\tau_f$ (≈ 5 LSC turnover times), (b) $\phi_{m,2}^w$ based on the azimuthal vertical velocity profile averaged over $50\tau_f$, (c) $\phi_{m,2}^w$ based on the azimuthal vertical velocity profile averaged over $4\tau_f$, and (d) enlargement of the graph shown in panel c to reveal more details.

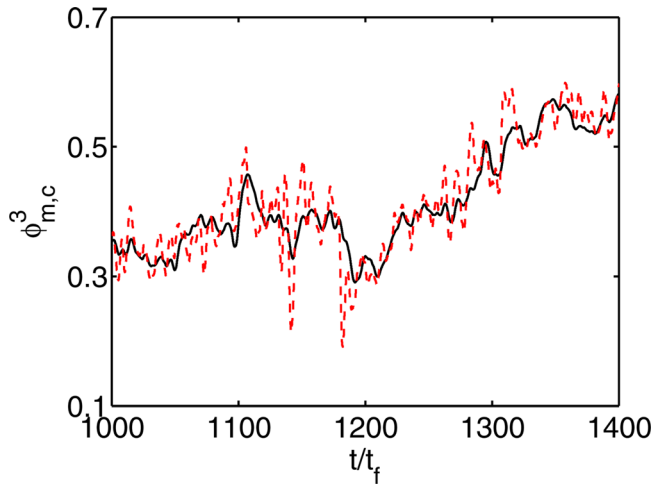


FIG. 3. (Color online) $\phi_{m,c}^w$ (solid black line) and $\phi_{m,c}^T$ (red dashed line) for $Ra=1 \times 10^8$, $Pr=6.4$, and $\Gamma=1$ on the $257 \times 129 \times 257$ grid, and based on the azimuthal vertical velocity and azimuthal temperature profile averaged over $4\tau_f$. Here, the data of all 64 azimuthally equally spaced probes at mid-height have been used.

azimuthal vertical velocity profile after averaging over $4\tau_f$, see Figures 2(c) and 2(d). When no time averaging is applied, the graph looks similar, with some additional peaks due to very small plumes, to the one where the data are averaged over $4\tau_f$. Figure 3 shows that the LSC orientation can be determined more precisely from the vertical velocity than from the temperature, even for this relatively high Pr (i.e., small thermal diffusivity). The difference between the LSC orientation determined from the vertical velocity and the temperature seems to depend on several parameters such as the Ra and the Pr number and the aspect ratio. However, at the moment, we do not have enough numerical data available to systematically study this. For $\Gamma=1$, the obtained LSC orientation at midheight is the same when the data of only 8 or

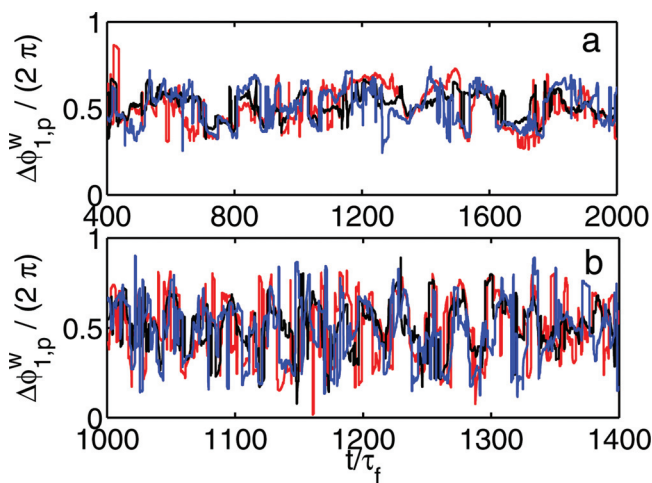


FIG. 4. (Color) The red, black, and blue lines indicate $\Delta\phi_{b,p}^w$, $\Delta\phi_{m,p}^w$, and $\Delta\phi_{t,p}^w$, respectively, for $Ra=1 \times 10^8$, $Pr=6.4$, and $\Gamma=1$ on the $257 \times 129 \times 257$ grid. Panels a and b show $\Delta\phi_{1,p}^w$ when the azimuthal vertical velocity profile is averaged over $50\tau_f$ and $4\tau_f$, respectively. The average of $\Delta\phi_{1,p}^w$ is π and this is in agreement with a cosine fit. The deviations from this value are due to plumes and the off-center motion of the LSC. Here, the data of all 64 azimuthally equally spaced probes per horizontal level have been used.

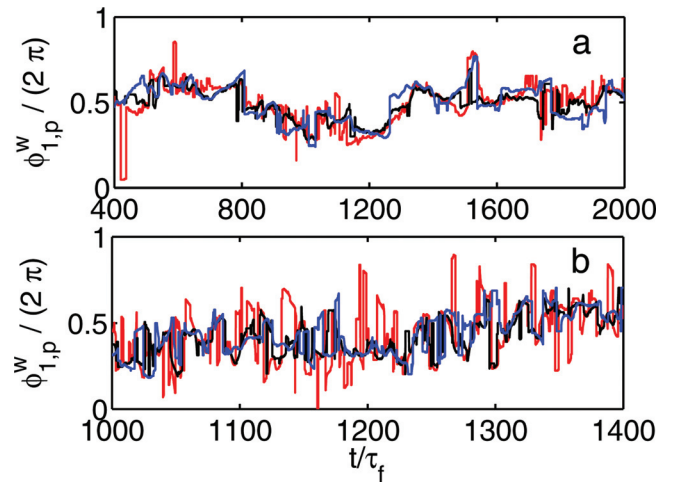


FIG. 5. (Color) The red, black, and blue lines indicate $\phi_{b,p}^w$, $\phi_{m,p}^w$, and $\phi_{t,p}^w$, respectively, for $Ra=1 \times 10^8$, $Pr=6.4$, and $\Gamma=1$ on the $257 \times 129 \times 257$ grid. Panels a and b show $\phi_{1,p}^w$ based on the azimuthal profiles of the vertical velocity averaged over $50\tau_f$ and $4\tau_f$, respectively. The difference between the LSC orientation at the different levels is due to plumes and the torsional motion of the LSC. Here, the data of all 64 azimuthally equally spaced probes per horizontal level have been used.

all 64 probes is used, but not when the data of only 2 probes is used.

From Figure 2, it becomes clear that the LSC orientation, obtained by the polynomial and cosine fit, can differ significantly. This is due to the off-center motion of the LSC.^{19–21} Figure 4 shows $\Delta\phi = \phi_{max} - \phi_{min}$, i.e., the difference between the orientation of the strongest up (ϕ_{max}) and down going motion (ϕ_{min}) obtained using the polynomial fit, fluctuates around $\Delta\phi = \pi$. To quantify the strength of these fluctuations, we calculate $\langle(\Delta\phi_{1,p}^w - \pi)^2\rangle^{1/2}$. The values based on the data of 64 (8) probes per horizontal level for the case presented in Figure 4 are $\langle(\Delta\phi_{t,p}^w - \pi)^2\rangle^{1/2} \approx 1.09(1.04)$, $\langle(\Delta\phi_{b,p}^w - \pi)^2\rangle^{1/2} \approx 0.84(0.77)$, and $\langle(\Delta\phi_{m,p}^w - \pi)^2\rangle^{1/2} \approx 0.84(0.77)$.

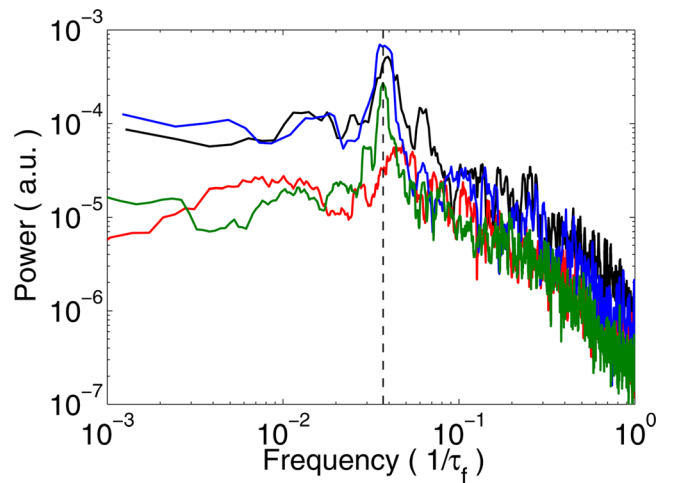


FIG. 6. (Color online) The power spectra of $\phi_{m,c}^w - \phi_{m,p}^w$ shows a maximum around $25\tau_f$, which is indicated by the vertical dashed line. This frequency is caused by plumes that pass the LSC orientation based on the cosine fit on the left and right side. The different spectra are obtained from simulations for $Pr=6.4$ in a $\Gamma=1$ sample for different Ra and resolution, i.e., $Ra=1 \times 10^8$ on a $257 \times 129 \times 257$ (red) and on a $385 \times 193 \times 385$ grid (black), and $Ra=5 \times 10^8$ on a $257 \times 129 \times 257$ (green), and a $385 \times 193 \times 385$ (blue) grid.

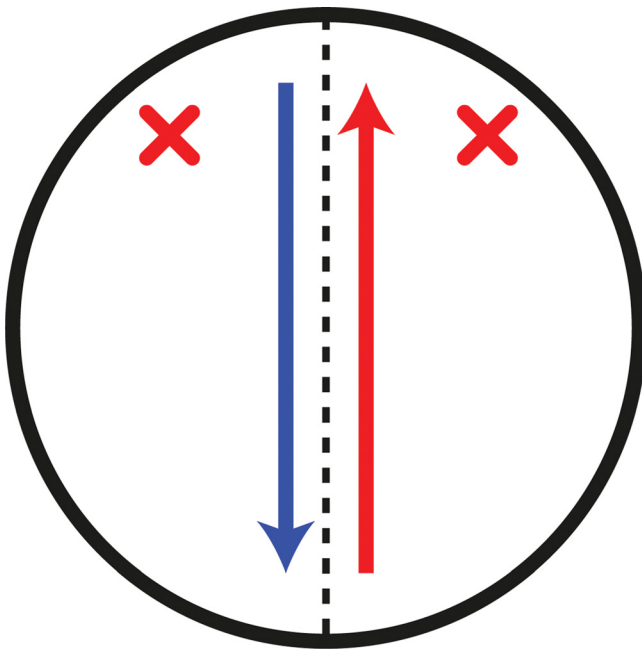


FIG. 7. (Color online) Sketch of the top view on the RB sample. The dotted line indicates the orientation of the LSC based on the cosine fit and the red (up-pointing) and blue (down-pointing) arrows indicated the flow direction close to the bottom and top plate, respectively. Strong plumes are detected alternately on the left and right side of the LSC, see crosses, with a specific frequency, see also Figure 2.

$\approx 1.11(1.01)$. Because the fluctuation strength is the same when the data of 8 and 64 equally spaced probes per horizontal level are considered, we conclude that the use of 8 probes is sufficient to capture these statistics in a $\Gamma = 1$ sample. In Figure 5, it is shown that the LSC orientation, obtained using the polynomial fit method, can be different at the different heights. We note that the same is observed when the LSC orientation based on a cosine fit is considered. This indicates that the LSC is not always flowing straight up and down, but is also moving in the azimuthal direction, and thus performs twisting motions.⁶ We note that some phenomena, like the drift of the LSC due to the Coriolis force, see Ref. 10, can be analyzed using the LSC orientation based on the polynomial and cosine method, because in this case, only the long term drift of the LSC is important.

More remarkably is the presence of a specific frequency of approximately $25\tau_f$ in the signal $\phi_{m,c}^w - \phi_{m,p}^w$, see Figure 6. This specific frequency seems to be related to the frequency in which plumes are passing the horizontal midplane,⁴² which in our case shows up in the frequency in which plumes are detected on the left and right hand side of the LSC orientation based on the cosine fit, see Figure 7. This frequency might also be related to the low frequency mode found already in Ref. 43 or to the off-center oscillation of the LSC.²² We find this frequency in our simulations for $Pr = 6.4$ in a $\Gamma = 1$ sample. We note that we also find this frequency when we do not apply any time averaging on the data before we determine the LSC orientation. Actually one can already see this phenomenon in Figure 2(d) where $\phi_{m,p}^w$ fluctuates around $\phi_{m,c}^w$ with a typical period of about $25\tau_f$. Further confirmation is obtained when the temporal behavior of the data obtained

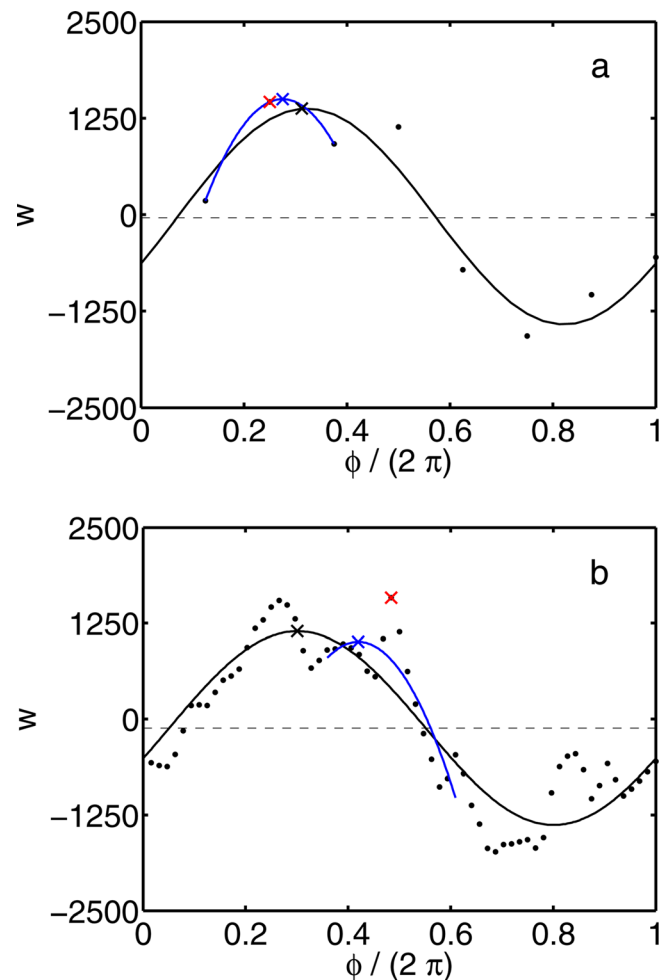


FIG. 8. (Color online) Snapshot of the azimuthal vertical velocity profile averaged over $4\tau_f$ for $Pr = 6.4$ in a $\Gamma = 1$ sample at $Ra = 5 \times 10^8$. The symbols have the same meaning as indicated in Figure 1. Panel a indicates the obtained profile using the data of 8 probes and panel b the profile as it is obtained from the data of 64 probes. The accompanying movies can be found in the supplementary material (Ref. 35) (enhanced online) [URL: <http://dx.doi.org/10.1063/1.3620999.1>].

from the 64 probes at midheight is shown in a movie, see the supplementary material.³⁵ The movie is based on the data obtained from the simulation on the $385 \times 193 \times 385$ grid at $Ra = 5 \times 10^8$ with $Pr = 6.4$ in a $\Gamma = 1$ sample. The movie shows a passing plume at $t \approx 2412$, see the snapshot of the movie in Figure 8(b), which is indicated by the two peak structure around the maximum position obtained by the cosine fit. When this plume is passed, the double peak structure disappears. Subsequently, the LSC orientation based on the polynomial fit method is smoothly passing the LSC orientation based on the cosine fit. Thus showing an off-center motion of the LSC. We note that having a large number of probes is essential to confirm these plume events. To show this, we made a movie of the same time interval, see the supplementary material³⁵ and the snapshot in Figure 8(a), with the data of only 8 probes. From these movies and Figure 8(a), we conclude that it is impossible to see the double peak structure when the data of only 8 probes is used and therefore we cannot distinguish the off-center motion of the LSC from passing plumes, when the plumes stretches over two rows of thermistors.

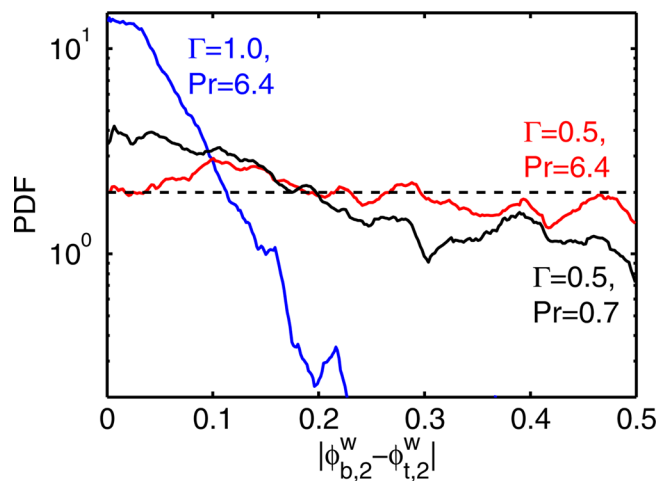


FIG. 9. (Color online) The PDF of $|\varphi_{b,c}^w - \varphi_{t,c}^w|$ for $Ra = 1 \times 10^8$. The PDF for $Pr = 6.4$ and $\Gamma = 1$ is given in blue. The red and black line give the PDF for $Pr = 6.4$ and $Pr = 0.7$ in the $\Gamma = 1/2$ geometry, respectively.

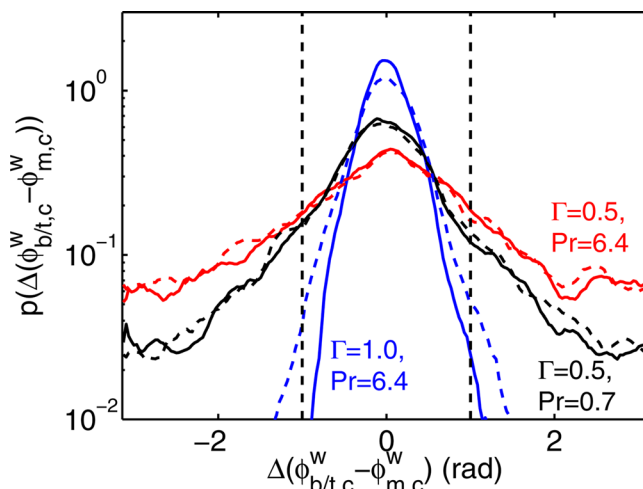


FIG. 11. (Color online) The PDF of $\varphi_{b/t,c}^w - \varphi_{m,c}^w$ for $Ra = 1 \times 10^8$, see text for details. The dashed and solid lines indicate the PDF based on the data of only 8 or all 64 probes equally spaced probes per horizontal level, respectively. The vertical dashed lines indicate the definition of the SRS according to Xi and Xia (Ref. 16) and Weiss and Ahlers (Ref. 46).

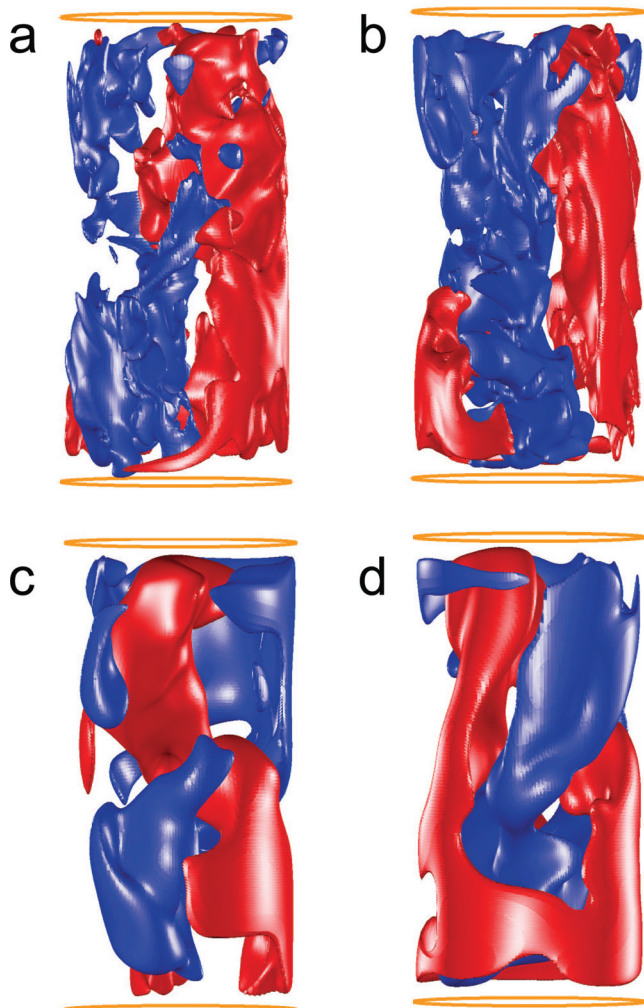


FIG. 10. (Color) Snapshot of the regions with the strongest, i.e., $w \geq 0.35w_{max}$, up (red) and down-flow (blue) for $Ra = 1 \times 10^8$ and $\Gamma = 1/2$. (a) $Pr = 0.7$, SRS, (b) $Pr = 0.7$, very strong corner flows, (c) $Pr = 6.4$, DRS, (d) $Pr = 6.4$, strong plume/torsional motion. Supplementary movies that offer a full three dimensional view are provided in the supplementary material (Ref. 35) (enhanced online) [URL: <http://dx.doi.org/10.1063/1.3620999.2>].

In summary, in a $\Gamma = 1$ sample, the obtained LSC orientation using a cosine and polynomial fit is the same when the data of only 8 or all 64 azimuthally equally spaced probes per horizontal level are used. Because the azimuthal temperature profile is only an indirect measure of the LSC orientation, we find that the LSC orientation can be determined with more precision from the azimuthal vertical velocity profile. In addition, we find that many of its interesting phenomena like azimuthal meandering, reversals, cessations, and the sloshing mode of the LSC look the same when the data of only 8 or all 64 azimuthally equally spaced probes per horizontal level are considered. However, only with the data of 64 equally spaced probes per horizontal level, the effect of passing plumes on the azimuthal temperature and azimuthal vertical velocity profiles can be identified.

V. RESULTS FOR $\Gamma = 1/2$

We now come to the $\Gamma = 1/2$ case. For this geometry, Verzicco and Camussi²⁵ have used the data accessibility provided by DNS to show that the large scale circulation can be either in a single-roll state (SRS) or in a double-roll state (DRS). Subsequently, a model introduced by Stringano and Verzicco²⁶ found that the switching between the DRS and the SRS can influence the Nusselt number and can thus be a possible reason for the bimodal behavior of Nusselt found in some experiments, see e.g. Refs. 44 and 45.

The first extensive experimental study on the transition between the SRS and the DRS was performed by Xi and Xia.¹⁶ They studied flow mode transition in samples of aspect ratio 1, 1/2, and 1/3. Figure 10 of their paper¹⁶ shows the percentages of the time the flow spends in either the SRS or the DRS. In addition, they showed that the heat transfer in the SRS is higher than in the DRS. Recently, Weiss and Ahlers⁴⁶ have also experimentally investigated the switching between the SRS and the DRS, but now over a much larger range of Ra than Xi and Xia.¹⁶ The conclusion of this work

is summarized in Figure 11 of Ref. 46. That figure shows that the SRS is more dominant at higher Ra and smaller Pr . They note that they find a good agreement with the results of Xi and Xia in the Ra number range in which both experiments overlap. In addition, the work of Xi and Xia¹⁶ and Weiss and Ahlers⁴⁶ showed that the flow state cannot always be defined as SRS or DRS. This is particularly important for $Ra \lesssim 3 \times 10^9$. For example, for $Ra = 1 \times 10^8$ and $Pr = 4.38$, the flow state is undefined for about 50% of the time according to Weiss and Ahlers.⁴⁶

In this paper, we will qualitatively confirm these experimental and numerical findings. We will restrict ourselves to this relatively low Ra number regime, namely to $Ra = 1 \times 10^8$: First, in order to directly compare with the $\Gamma = 1$ case of Sec. IV, second, because current high Ra number simulations^{37,47} are too limited in the number of turnover times to obtain sufficient statistics on the different flow states.

Our simulations confirm Weiss and Ahlers's⁴⁶ finding that there is more disorder in a $\Gamma = 1/2$ sample than in a $\Gamma = 1$ sample. We find that in this low Ra number regime, it is important to have a large number of probes to accurately represent the azimuthal temperature and azimuthal vertical velocity profiles to analyze the flow. In this regime, we see that deflection of plumes due to corner rolls and other plumes happens more often than in a $\Gamma = 1$ sample. These effects can be observed in the supplementary movies for $\Gamma = 1/2$ at $Ra = 1 \times 10^8$ and $Pr = 0.7$ and $Pr = 6.4$.³⁵ In the movies that show horizontal cuts at the heights $0.25L$, $0.50L$, and $0.75L$, one can see that the hot and cold regions interchange more often in a $\Gamma = 1/2$ sample than in a $\Gamma = 1$ sample.

In order to determine whether there is a SRS or a DRS in this geometry, we determined the probability density function (PDF) of the quantity $|\phi_{b,c}^w - \phi_{t,c}^w|$. When this PDF peaks

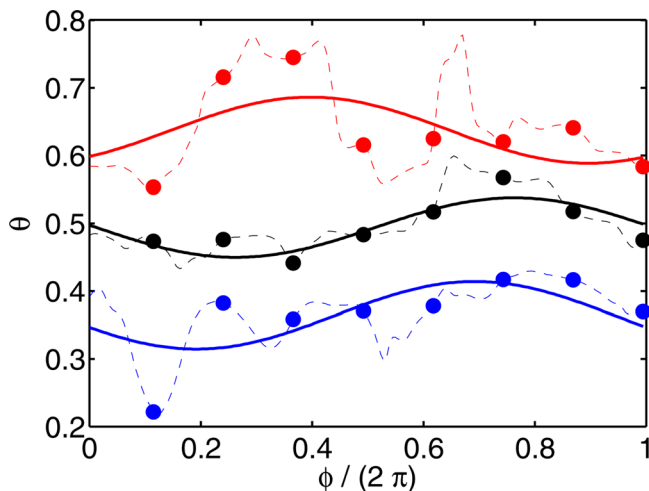


FIG. 12. (Color online) Red (top), black (middle), and blue (bottom) data indicate the azimuthal temperature profile at the heights $0.25L$, $0.50L$, and $0.75L$, respectively, for the flow state indicated in Figure 10(b). The dots indicate the data of 8 azimuthally equally spaced probes per horizontal plane. Based on the cosine fits (solid lines) obtained from this probe data, this state would be identified as a DRS, while Figure 10(b) shows that it is in fact a SRS with a strong corner flow. The dashed lines show that a higher azimuthal resolution can resolve the double peak structure of the corner flow and the main flow. The temperatures at $0.25L$ ($0.75L$) have been raised (lowered) by 0.1 for clarity.

around zero, it means that the fluid is flowing straight up and this indicates the presence of a SRS. When there is a DRS, the PDF should peak around π . Figure 9 shows that for $Pr = 6.4$ in a $\Gamma = 1$ sample, the PDF peaks around zero and this confirms the dominance of the SRS in this geometry. For $Pr = 0.7$ in a $\Gamma = 1/2$ sample, the figure shows that there is a small peak around zero, but it is much less pronounced than for the $\Gamma = 1$ case. For $Pr = 6.4$ in a $\Gamma = 1/2$ sample, the figure shows that the PDF is nearly uniform, which would suggest that neither the SRS nor the DRS is dominant. This agrees with the results of Weiss and Ahlers,⁴⁶ since they find that for $Pr = 4.38$ and $Ra \lesssim 3 \times 10^9$, the flow state is poorly defined and no state dominates. Figure 10 reveals the origin of these nearly uniform PDFs in the $\Gamma = 1/2$ sample by showing three-dimensional visualizations of the regions where the vertical velocities are strongest. An analysis of these (and similar figures) revealed that the uniform PDF is due to the possibility of different flow states, i.e., the SRS (Figure 10(a)) with $|\phi_{b,c}^w - \phi_{t,c}^w| \simeq 0$, the DRS (Figure 10(c)) with $|\phi_{b,c}^w - \phi_{t,c}^w| = \pi$, strong corner flows (Figure 10(b)) which can have any $|\phi_{b,c}^w - \phi_{t,c}^w|$, and strong plume and/or torsional motions (Figure 10(d)) which also can have any $|\phi_{b,c}^w - \phi_{t,c}^w|$.

To better compare our results with the results of Weiss and Ahlers⁴⁶ we also determined the PDF of the quantity $\phi_{b/t,c}^w - \phi_{m,c}^w$, see Figure 11. Here, $\phi_{b/t,c}^w$ means that both $\phi_{b,c}^w$ and $\phi_{t,c}^w$ are compared with $\phi_{m,c}^w$ to construct the PDF. A similar PDF for higher Ra , based on experimental data, can be found in Figure 21 of Weiss and Ahlers.⁴⁶ Figure 11 shows this PDF based on the data of only 8 and all 64 equally spaced probes per horizontal level for the cases of Figure 9. First of all, Figure 11 shows that the DRS is much more pronounced for $Pr = 6.4$ than for $Pr = 0.7$, which is in agreement with the results of Weiss and Ahlers⁴⁶ and the results shown in Figure 9. Second, a comparison of the PDFs in Figure 11 reveals that the PDFs based on the data of 8 and all 64 equally spaced probes are almost identical. The largest difference is visible for $Pr = 6.4$ in a $\Gamma = 1$ sample. Here, the PDF based on the data of 64 equally spaced probes is more confined in the SRS region than the one based on 8 equally spaced probes, because the larger number of probes reduces "random" fluctuations in the obtained LSC orientation.

Furthermore, and this is the main issue here, for this relatively low Ra , sometimes the data of three rows of 8 thermistors can give misleading hints for the actual flow state of the system due to the effect of passing plumes and corner rolls on the azimuthal profiles. The importance of these effects is shown in Figure 12. This figure shows that based on the data of 8 azimuthally equally spaced probes at each horizontal level the flow structure shown in Figure 10(b), which is a SRS with a strong corner flow, would be identified as a DRS. In addition, the figure shows that the full azimuthal temperature profiles reveal that a higher azimuthal resolution (e.g., 64 instead of only 8 probes) could resolve the double peak structure (originating from the coexistence of the SRS with some corner flow), which makes it possible to distinguish this state from a real DRS.

We note that the experiments of Weiss and Ahlers⁴⁶ show that for $Pr = 4.38$ and $Ra \lesssim 3 \times 10^9$, the flow state is

undefined for about 50% of the time. In the experiments, the SRS only establishes itself for higher Ra , where the flow state is much better defined, as the area of the corner flow becomes smaller and smaller.²⁴ It is therefore likely that the examples presented here are primarily important in the low Ra number regime investigated here and are much less common in the higher Ra number regime considered in most experiments. We stress however that one does not know *a priori* whether one is in a difficult case or in a case where the method works fine. Therefore, we feel that it is important to realize that there are some limitations in the methods to determine the flow state from three rows of 8 equally spaced thermistors. An example of such a difficult case is the breakdown of the LSC when a strong rotation is applied around the cylinder axis.^{22,23}

VI. THE RELATIVE LSC STRENGTH

The instantaneous temperature profiles in Figure 12 show that the LSC is not always clearly present, meaning that the cosine fit becomes poor. In order to study this in more detail, we introduce the concept of the relative LSC strength, which we define as the strength of the LSC, i.e., the cosine mode, with respect to the strength of the plumes and turbulent fluctuations, i.e., the fluctuations around the cosine fit.

A convenient way to define a relative LSC strength that is independent of the number of probes is to determine the energy in the different Fourier modes of the azimuthal temperature or the azimuthal vertical velocity profile. In order to obtain a relative LSC strength \bar{S}_k with a number between 0 and 1, we normalize the energy in the first Fourier mode, i.e., the cosine mode, as follows:

$$\bar{S}_k = \text{Max} \left(\left(\frac{\sum_{t_b}^{t_e} E_1}{\sum_{t_b}^{t_e} E_{tot}} - \frac{1}{N} \right) / \left(1 - \frac{1}{N} \right), 0 \right). \quad (2)$$

Here $\sum_{t_b}^{t_e} E_1$ indicates the sum of the energy in the first Fourier mode over time, i.e., from the beginning of the simula-

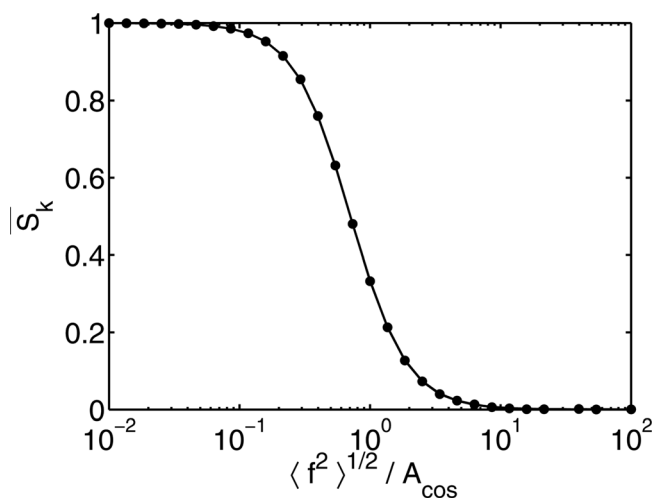


FIG. 13. The relative strength of the LSC \bar{S}_k versus the relative noise level $\langle f^2 \rangle^{1/2} / A_{cos}$, calculated from the stochastic model (Eq. (3)). For strong noise $\bar{S}_k < 0.5$ and the SRS is defined to break down.

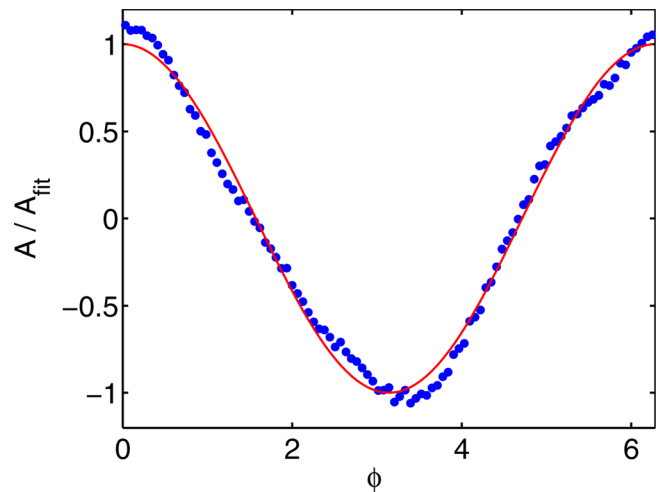


FIG. 14. (Color online) The azimuthal vertical velocity profile after averaging with respect to the orientation of the LSC, which was obtained using a cosine fit, is indicated by the dots. The method has been applied to the data of all 64 probes in the horizontal midplane obtained in the simulation at $Pr = 6.4$, $Ra = 1 \times 10^8$, and $\Gamma = 1/2$. The solid line indicates a pure cosine profile.

tion $t = t_b$ to the end of the simulation $t = t_e$, $\sum_{t_b}^{t_e} E_{tot}$ is the sum of the total energy in all Fourier modes over time, and N is the total number of Fourier modes that can be determined. Note that the factor $1/N$ is only used to subtract the part of energy coming from the equi-distribution among all the modes. The number of Fourier modes N that can be determined is $n_p/2$, where $n_p = 2^i$ is the number of probes and i is an integer. The subscript k ($= b, m, t$) indicates the height level in the sample at which the relative LSC strength is determined.

Here, we will only determine \bar{S}_k for the middle row of thermistors, thus only S_m . We note that the LSC amplitude δ_m and the phase ϕ_m of the first Fourier mode are identical to the ones determined when using the least square fit in Eq. (1). We moreover note that the quantity \bar{S}_k is *not* time resolved and thus does not allow to study the switching between the SRS and DRS.⁴⁶ Results on time-resolved relative LSC strengths will be presented in Sec. VII.

The normalization in Eq. (2) has been chosen such that the relative LSC strength S_m always has a value between 0 and 1: The value 1 indicates that the azimuthal profile is a pure cosine profile, which is a signature of the LSC according to Ref. 9, and the value 0 indicates that the magnitude of the cosine mode is equal to (or weaker than) the value expected from a random noise signal. $\bar{S}_m \gg 0.5$ indicates that the cosine fit on average is a reasonable approximation of the data, as then most energy in the signal is in the first Fourier mode, i.e., the cosine mode. In contrast, $\bar{S}_m \ll 0.5$ indicates that most energy is in the higher Fourier modes, meaning that the application of a cosine fit to the data becomes questionable. Somehow arbitrary, we define the SRS as dominant once $\bar{S}_m > 0.5$.

To further demonstrate these properties of \bar{S}_k , we analyze the test function

$$\theta_i(j) = A_{cos} \cos(\phi_i + j/100) + f(j). \quad (3)$$

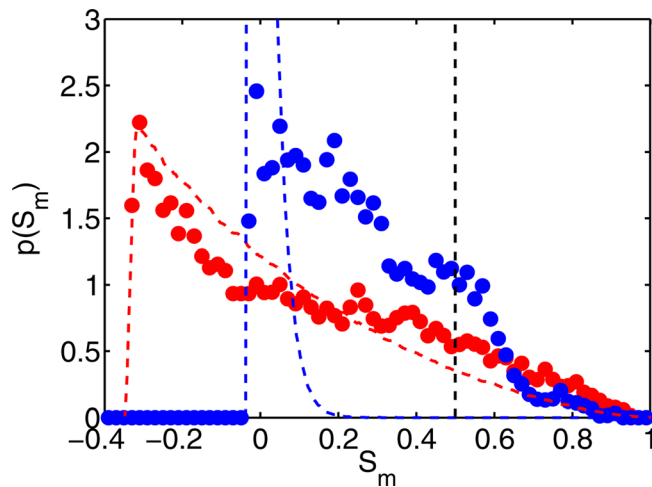


FIG. 15. (Color online) PDFs of the relative LSC strength at midheight for $Ra = 1 \times 10^8$, $Pr = 6.4$, and $\Gamma = 0.5$. The red ($-\frac{1}{3} \leq S_m(t) \leq 1$, i.e. the lower set of filled circles) and blue ($-\frac{1}{31} \leq S_m(t) \leq 1$, i.e. the higher set of filled circles) data points indicate the PDF based on the azimuthal vertical velocity profile sampled with only 8 and all 64 probes, respectively. The colored dashed lines give the corresponding PDFs based on a purely random signal. The vertical dashed lines at $S_m = 0.5$ indicate the region $0.5 \leq S_m \leq 1.0$ where the first Fourier modes contains at least 50% of the energy of the azimuthal vertical velocity profile.

Here, $\phi_i = 2i\pi/n_p$ and $f(j)$ is a set of Gaussian distributed random numbers with a certain standard deviation $\langle f^2 \rangle^{1/2}$, the “time” j is varied between 1 and 125 000, and the noise is supposed to model the effect of turbulent fluctuations around the cosine fit. The result for the relative strength \bar{S}_k of the LSC as function of the noise level is shown in Figure 13. Indeed, $1 \geq \bar{S}_k \geq 0$ and $\bar{S}_k > 0.5$ only if the noise is smaller than the amplitude, $\langle f^2 \rangle^{1/2}/A_{cos} \ll 1$.

We now come back to the numerical data of our simulations. For each simulation, we calculated the relative LSC strength \bar{S}_m based on the instantaneous azimuthal vertical velocity profiles at midheight based on the data of either only 8 or all 64 probes at the horizontal midplane. We show the results for two aspect ratios, two Rayleigh numbers, and two Prandtl numbers in Table I. For $\Gamma = 1$, the flow is clearly in the SRS, as indicated by $\bar{S}_m \geq 0.65$. For $\Gamma = 1/2$, the SRS is less dominant, in particular for the large Prandtl number case $Pr = 6.4$, where the SRS hardly occurs. This confirms our conclusions of Sec. V where we stated that the SRS is not always present in the $\Gamma = 1/2$ sample.

Another method used in the literature^{9,46} to identify the flow pattern is to average the azimuthal profile with respect to the LSC orientation. This method assumes that the deviations from the cosine fit are due to turbulent fluctuations. It will work for cases for which \bar{S}_m is large. However, when \bar{S}_m is low, this method gives misleading results as is shown in Figure 14 where we apply it to above discussed data for $Pr = 6.4$ in the $\Gamma = 1/2$ sample, where the relative LSC strength using the data of all 64 probes in the horizontal level is $\bar{S}_m = 0.27$ (see Table I): The average profile obtained with the method of Refs. 9 and 46 cannot be distinguished from the ones obtained from the cases where \bar{S}_m is larger and therefore the method cannot be used to claim the dominance of the SRS.

VII. TIME RESOLVED RELATIVE LSC STRENGTH

The relative LSC strength can also be calculated on instantaneous azimuthal temperature and vertical velocity profiles. We demonstrate this by constructing the PDF of the relative LSC strength at midheight $S_m(t)$ for instantaneous azimuthal temperature and vertical velocity profiles using the definition

$$S_m(t) = \left(\frac{E_1(t)}{E_{tot}(t)} - \frac{1}{N} \right) / \left(1 - \frac{1}{N} \right). \quad (4)$$

The only difference with respect to Eq. (2) is that $E_1(t)$ and $E_{tot}(t)$ and thus $S_m(t)$ are time dependent and that we have dropped the criterion that the minimal value should be 0. The reason for the latter is that we want to prevent strange jumps in the PDFs of S_m at 0. For 8 probes, we have $-\frac{1}{3} \leq S_m(t) \leq 1$ and for 64 probes we have $-\frac{1}{31} \leq S_m(t) \leq 1$. Note that these intervals follow directly from Eq. (4) by filling in the limiting cases, i.e., $E_1(t)/E_{tot}(t) = 0$ and $E_1(t)/E_{tot}(t) = 1$, and by using the relation $N = n_p/2$, where n_p is the number of probes, see Sec. VI.

Figure 15 shows the PDFs for S_m based on the measurement of the vertical velocity by only 8 or all 64 equally spaced probes at midheight in the simulation with $Ra = 1 \times 10^8$, $Pr = 6.4$, and in the $\Gamma = 0.5$ sample. In addition, for both cases, we determined the distribution of $S_m(t)$ for a random signal. When we compare the PDFs based on the simulation data with the distributions obtained for random signals, we see that the difference is relatively small when the data of only 8 probes is considered, whereas a much larger difference is obtained when the data of all 64 probes is taken into account. Figure 15 thus clearly shows that it can be beneficial to use more than 8 azimuthally equally spaced probes, since it becomes much easier to show that certain events are statistically relevant.

VIII. CONCLUSIONS

We studied the LSC dynamics in DNS simulations by investigating the azimuthal temperature and vertical velocity profiles obtained from 64 equally spaced numerical probes at three different heights. For $Pr = 6.4$ in a $\Gamma = 1$ sample, we find that the azimuthal profile is well presented with the data of 8 numerical probes, a number normally used in experiments, as the LSC orientation obtained by a cosine fit is the same when the data of 8 and 64 probes is considered. We find that the improved azimuthal resolution (64 instead of 8 probes in the sidewall at one height) can reveal the effect of the plumes.

In agreement with the findings of Xi and Xia¹⁶ and Weiss and Ahlers,⁴⁶ we find that there is more disorder present in the $\Gamma = 1/2$ sample than in the $\Gamma = 1$ sample. For the $\Gamma = 1/2$ case, we also show that when the azimuthal temperature profile is only determined from 8 probes per horizontal level, a SRS can erroneously be identified as a DRS, because the azimuthal resolution is too small to distinguish between the structure of the corner flow and the main roll. Here, we again stress that this result is obtained in the relatively low Ra number regime. The experimental results of Weiss and

Ahlers⁴⁶ show that for the low Ra number regime the flow state is undefined for about 50% of the time. For $\Gamma = 1/2$, the SRS only establishes itself for higher Ra , where the flow state is much better defined.⁴⁶ It is therefore likely that the examples presented here are primarily important in this low Ra number regime investigated here and are much less common in the higher Ra number regime.

We quantified the LSC strength relative to the turbulent fluctuations by determining the ratio between the energy in the first Fourier mode and the energy in all Fourier modes of the azimuthal temperature and azimuthal vertical velocity profiles. We find that the relative LSC strength at $Ra = 1 \times 10^8$ is considerably lower in the $\Gamma = 1/2$ sample than in the $\Gamma = 1$ sample, i.e., that the SRS is much less pronounced in the $\Gamma = 1/2$ sample than in the $\Gamma = 1$ sample. This determination of the relative LSC strength can be applied directly to available experimental data to determine whether the SRS is present in high Ra number thermal convection and in rotating RB convection.

ACKNOWLEDGMENTS

We gratefully acknowledge various discussions with Guenter Ahlers over this line of research and his helpful comments on our manuscript. We also acknowledge discussions with Stefan Weiss and Eric Brown. We thank R. Verzicco for providing us with the numerical code. The work is supported by the Foundation for Fundamental Research on Matter (FOM) and the National Computing Facilities (NCF), both sponsored by NWO. The computations have been performed on the Huygens supercomputer of SARA in Amsterdam.

- ¹G. Ahlers, S. Grossmann, and D. Lohse, "Heat transfer and large scale dynamics in turbulent Rayleigh-Bénard convection," *Rev. Mod. Phys.* **81**, 503 (2009).
- ²G. Ahlers, "Turbulent convection," *Physics* **2**, 74 (2009).
- ³D. Lohse and K. Q. Xia, "Small-scale properties of turbulent Rayleigh-Bénard convection," *Annu. Rev. Fluid Mech.* **42**, 335 (2010).
- ⁴J. Niemela, L. Skrbek, K. R. Sreenivasan, and R. J. Donnelly, "The wind in confined thermal turbulence," *J. Fluid Mech.* **449**, 169 (2001).
- ⁵K.-Q. Xia, C. Sun, and S. Q. Zhou, "Particle image velocimetry measurement of the velocity field in turbulent thermal convection," *Phys. Rev. E* **68**, 066303 (2003).
- ⁶D. Funfschilling and G. Ahlers, "Plume motion and large scale circulation in a cylindrical Rayleigh-Bénard cell," *Phys. Rev. Lett.* **92**, 194502 (2004).
- ⁷C. Sun, K. Q. Xia, and P. Tong, "Three-dimensional flow structures and dynamics of turbulent thermal convection in a cylindrical cell," *Phys. Rev. E* **72**, 026302 (2005).
- ⁸C. Sun, H. D. Xi, and K. Q. Xia, "Azimuthal symmetry, flow dynamics, and heat transport in turbulent thermal convection in a cylinder with an aspect ratio of 0.5," *Phys. Rev. Lett.* **95**, 074502 (2005).
- ⁹E. Brown and G. Ahlers, "Rotations and cessations of the large-scale circulation in turbulent Rayleigh-Bénard convection," *J. Fluid Mech.* **568**, 351 (2006).
- ¹⁰E. Brown and G. Ahlers, "Effect of the Earth's Coriolis force on turbulent Rayleigh-Bénard convection in the laboratory," *Phys. Fluids* **18**, 125108 (2006).
- ¹¹H. D. Xi and K. Q. Xia, "Cessations and reversals of the large-scale circulation in turbulent thermal convection," *Phys. Rev. E* **75**, 066307 (2007).
- ¹²E. Brown and G. Ahlers, "Large-scale circulation model for turbulent Rayleigh-Bénard convection," *Phys. Rev. Lett.* **98**, 134501 (2007).
- ¹³E. Brown and G. Ahlers, "A model of diffusion in a potential well for the dynamics of the large-scale circulation in turbulent Rayleigh-Bénard convection," *Phys. Fluids* **20**, 075101 (2008).

- ¹⁴E. Brown and G. Ahlers, "Azimuthal asymmetries of the large-scale circulation in turbulent Rayleigh-Bénard convection," *Phys. Fluids* **20**, 105105 (2008).
- ¹⁵D. Funfschilling, E. Brown, and G. Ahlers, "Torsional oscillations of the large-scale circulation in turbulent Rayleigh-Bénard convection," *J. Fluid Mech.* **607**, 119139 (2008).
- ¹⁶H. D. Xi and K. Q. Xia, "Flow mode transitions in turbulent thermal convection," *Phys. Fluids* **20**, 055104 (2008).
- ¹⁷H. D. Xi and K. Q. Xia, "Azimuthal motion, reorientation, cessation, and reversal of the large-scale circulation in turbulent thermal convection: A comparison between aspect ratio one and one-half geometries," *Phys. Rev. E* **78**, 036326 (2008).
- ¹⁸R. P. J. Kunnen, H. J. H. Clercx, and B. J. Geurts, "Breakdown of large-scale circulation in turbulent rotating convection," *Europhys. Lett.* **84**, 24001 (2008).
- ¹⁹H. D. Xi, S. Q. Zhou, Q. Zhou, T. S. Chan, and K. Q. Xia, "Origin of temperature oscillations in turbulent thermal convection," *Phys. Rev. Lett.* **102**, 044503 (2009).
- ²⁰Q. Zhou, H. D. Xi, S. Q. Zhou, C. Sun, and K. Q. Xia, "Oscillations of the large-scale circulation in turbulent Rayleigh-Bénard convection: The sloshing mode and its relationship with the torsional mode," *J. Fluid Mech.* **630**, 367 (2009).
- ²¹E. Brown and G. Ahlers, "The origin of oscillations of the large-scale circulation of turbulent Rayleigh-Bénard convection," *J. Fluid Mech.* **638**, 383 (2009).
- ²²J.-Q. Zhong, R. J. A. M. Stevens, H. J. H. Clercx, R. Verzicco, D. Lohse, and G. Ahlers, "Prandtl-, Rayleigh-, and Rossby-number dependence of heat transport in turbulent rotating Rayleigh-Bénard convection," *Phys. Rev. Lett.* **102**, 044502 (2009).
- ²³R. J. A. M. Stevens, J.-Q. Zhong, H. J. H. Clercx, G. Ahlers, and D. Lohse, "Transitions between turbulent states in rotating Rayleigh-Bénard convection," *Phys. Rev. Lett.* **103**, 024503 (2009).
- ²⁴K. Sugiyama, R. Ni, R. J. A. M. Stevens, T. S. Chan, S.-Q. Zhou, H.-D. Xi, C. Sun, S. Grossmann, K.-Q. Xia, and D. Lohse, "Flow reversals in thermally driven turbulence," *Phys. Rev. Lett.* **105**, 034503 (2010).
- ²⁵R. Verzicco and R. Camussi, "Numerical experiments on strongly turbulent thermal convection in a slender cylindrical cell," *J. Fluid Mech.* **477**, 19 (2003).
- ²⁶G. Stringano and R. Verzicco, "Mean flow structure in thermal convection in a cylindrical cell of aspect-ratio one half," *J. Fluid Mech.* **548**, 1 (2006).
- ²⁷M. Kaczorowski and C. Wagner, "Analysis of the thermal plumes in turbulent Rayleigh-Bénard convection based on well-resolved numerical simulations," *J. Fluid Mech.* **618**, 89 (2009).
- ²⁸P. Mishra, A. De, M. Verma, and V. Eswaran, "Dynamics of reorientations and reversals of large-scale flow in Rayleigh-Bénard convection," *J. Fluid Mech.* **668**, 480 (2011).
- ²⁹K. R. Sreenivasan, A. Bershadskii, and J. Niemela, "Mean wind and its reversals in thermal convection," *Phys. Rev. E* **65**, 056306 (2002).
- ³⁰R. Benzi, "Flow reversal in a simple dynamical model of turbulence," *Phys. Rev. Lett.* **95**, 024502 (2005).
- ³¹F. Fontenele Araujo, S. Grossmann, and D. Lohse, "Wind reversals in turbulent Rayleigh-Bénard convection," *Phys. Rev. Lett.* **95**, 084502 (2005).
- ³²C. Resagk, R. du Puits, A. Thess, F. V. Dolzhansky, S. Grossmann, F. Fontenele Araujo, and D. Lohse, "Oscillations of the large scale wind in turbulent thermal convection," *Phys. Fluids* **18**, 095105 (2006).
- ³³E. Brown, A. Nikolaenko, and G. Ahlers, "Reorientation of the large-scale circulation in turbulent Rayleigh-Bénard convection," *Phys. Rev. Lett.* **95**, 084503 (2005).
- ³⁴H.-D. Xi, Q. Zhou, and K.-Q. Xia, "Azimuthal motion of the mean wind in turbulent thermal convection," *Phys. Rev. E* **73**, 056312 (2006).
- ³⁵See supplementary material at <http://dx.doi.org/10.1063/1.3620999> for movies that show the flow dynamics in horizontal or vertical planes.
- ³⁶D. Funfschilling, E. Bodenschatz, and G. Ahlers, "Search for the 'ultimate state' in turbulent Rayleigh-Bénard convection," *Phys. Rev. Lett.* **103**, 014503 (2009).
- ³⁷R. J. A. M. Stevens, R. Verzicco, and D. Lohse, "Radial boundary layer structure and Nusselt number in Rayleigh-Bénard convection," *J. Fluid Mech.* **643**, 495 (2010).
- ³⁸S. Weiss, R. Stevens, J.-Q. Zhong, H. Clercx, D. Lohse, and G. Ahlers, "Finite-size effects lead to supercritical bifurcations in turbulent rotating Rayleigh-Bénard convection," *Phys. Rev. Lett.* **105**, 224501 (2010).
- ³⁹R. Verzicco and P. Orlandi, "A finite-difference scheme for three-dimensional incompressible flow in cylindrical coordinates," *J. Comput. Phys.* **123**, 402 (1996).

- ⁴⁰R. Verzicco and R. Camussi, "Prandtl number effects in convective turbulence," *J. Fluid Mech.* **383**, 55 (1999).
- ⁴¹J. Bailon-Cuba, M. Emran, and J. Schumacher, "Aspect ratio dependence of heat transfer and large-scale flow in turbulent convection," *J. Fluid Mech.* **655**, 152 (2010).
- ⁴²E. Villiermaux, "Memory-induced low frequency oscillations in closed convection boxes," *Phys. Rev. Lett.* **75**, 4618 (1995).
- ⁴³B. Castaing, G. Gunaratne, F. Heslot, L. Kadanoff, A. Libchaber, S. Thomae, X. Z. Wu, S. Zaleski, and G. Zanetti, "Scaling of hard thermal turbulence in Rayleigh-Bénard convection," *J. Fluid Mech.* **204**, 1 (1989).
- ⁴⁴P.-E. Roche, B. Castaing, B. Chabaud, and B. Hebral, "Prandtl and Rayleigh numbers dependences in Rayleigh-Bénard convection," *Europhys. Lett.* **58**, 693 (2002).
- ⁴⁵P.-E. Roche, F. Gauthier, R. Kaiser, and J. Salort, "On the triggering of the ultimate regime of convection," *New J. Phys.* **12**, 085014 (2010).
- ⁴⁶S. Weiss and G. Ahlers, "Turbulent Rayleigh-Bénard convection in a cylindrical container with aspect ratio $\Gamma = 0.50$ and Prandtl number $Pr = 4.38$," *J. Fluid. Mech.* **676**, 5 (2011).
- ⁴⁷R. J. A. M. Stevens, D. Lohse, and R. Verzicco, "Prandtl number dependence of heat transport in high Rayleigh number thermal convection," *J. Fluid. Mech.* (to be published).