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# A Harmonic Method for Predicting Shallow-water Tides<sup>1</sup>

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#### ABSTRACT

The development of an objective technique for identifying significant hidden frequencies in the spectrum makes it possible to accurately predict shallow-water tides by harmonic methods. For Anchorage, Alaska, the 114 constituents used include frequencies in every species (cycles per day) from 0 to 12. The larger set of constituents improved the predictions in times of high and low waters, range of tide, and shape of curve. The stationary characteristics of some of the added constituents have been tested with three years of Philadelphia data.

This study was initially designed for a specific purpose—to improve tidal predictions at Anchorage, Alaska. Anchorage is located at the northern end of Cook Inlet near the western end of the Gulf of Alaska. The mean range of tide at Anchorage is about 25 feet. After oil was found in the area, huge deep-draft tankers required more accurate tidal predictions than were available by using the standard U.S. Coast and Geodetic Survey procedures for tidal analysis and prediction (9).

There was no question as to why the problem existed. Those harmonic constants that were determined in the Coast and Geodetic Survey analysis showed large amplitudes for some shallow-water constituents—clear indications of additional significant compound tides that are not included in the routine analysis. The compound tides are associated with the distortion of the sinusoidal shape of the tidal curve as the tidal wave travels over shallow depths(5).

British authorities have had to cope with shallow-water tides to a much greater extent than the U.S. Coast and Geodetic Survey, and therefore they have traditionally used 60 tidal constituents (3) compared with the 37 used by the Coast and Geodetic Survey. In some extreme cases, the 60 constituents do not adequately describe the shape of the curve, and the British have developed a non harmonic modification of their procedures to cope with these tides (4).

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A logical approach, therefore, was to send the Anchorage data to the Tidal Institute and Observatory, University of Liverpool, for analysis and prediction until such time as the Coast and Geodetic Survey could learn the British techniques. However, this did not solve the problem. We were informed that the Tidal Institute routine analysis obviously would not match the shape of the curve and that a continuous record of hourly heights for one year would be required for the nonharmonic method. Inasmuch as the harbor at Anchorage freezes every winter, the required length of record was not available. Although an effort to get a continuous year of record was initiated by installing a pressure gauge on the bottom, there remained an element of doubt as to whether the tidal characteristics remain unchanged during the winter freeze.

Fortunately, recent technical changes in tidal analysis and prediction made possible another approach. Essentially, the principal change provided greater flexibility in both analysis and prediction in that additional constitutents can now be included. Until now there was a constraint to work only with a fixed set of constituents; no others could be readily analyzed for, nor could they be included in, the prediction.

Traditional analysis included (i) a modified Fourier analysis for particular frequencies, (ii) a modification of the results for the interference effects of nearby frequencies, and (iii) an elimination of sideband contributions of frequencies in the same species—the same number of cycles per day (9,3). A least-square analysis in which any combination of frequencies is inserted as a model is now readily accomplished on a computer. A recent study showed that the harmonic constants for the same set of constituents are slightly more accurate than those obtained by the previous Coast and Geodetic Survey or British (Doodson) methods (10).

The Coast and Geodetic Survey tidal predictions until 1964 were made on a mechanical analog computer having gears designed for a fixed set of frequencies. The predictions now made on an electronic computer do not have the above restriction; in this particular study, 114 constituents have been included.

In shallow water, the nonlinear interaction among large-amplitude constituents generates additional constituents whose frequencies are integral sums or differences of the frequencies of known constituents (8). It is necessary to identify the important additional compound tides, include them in a new analysis, and then predict, using the enlarged set of harmonic constants. The availability of the BOMM (1) programs for time-series analysis makes some of these steps relatively easy.

First, a routine 37-constituent analysis was made of 192 days of Anchorage hourly data for the middle of 1964. Using the derived constants, hourly heights were predicted and subtracted from the observations, and then a spectral analysis was made of the residuals. This identified frequency bands of greatest energy in the residuals, and a Fourier analysis, using maximum resolution, was made for these bands. Wherever large values stood out above the continuum



Figure 1. Spectral analysis of Anchorage residuals.

in a plot of the Fourier amplitudes, an effort was made to identify an integral combination of frequencies of constituents that were known to be important and that closely matched the frequencies of these peaks. A new least-square analysis was performed, adding these new frequencies to the original 37. As a check, a new total prediction was prepared, new residuals were determined, and Fourier- and power-spectrum analyses were conducted with these data.

Fig. 1 shows the comparative power spectra with residuals from 37 and 114 constituents, respectively. The solid line below the dotted line shows that a significant improvement has been made in every species.

Fig. 2 shows the results of Fourier analysis near two cycles per day for the



Figure 2. High-resolution Fourier analysis near 2 cycles per day; Anchorage. Top: Residuals from 37 constituents. Bottom: Residuals from 114 constituents.



Figure 3. High-resolution Fourier analysis near 5 cycles per day: Anchorage. Top: Residuals from 37 constituents. Bottom: Residuals from 114 constituents.

two sets of residuals. Although a major portion of the energy has been removed, it is obvious that some remains. In a recent paper on tidal cusps (7), it was shown that the continuum rises in cusps near the large tidal lines. There are indications of a systematic residual midway between the groups (identified by the first two digits of the Doodson number), including speeds of about  $28.2^{\circ}$ ,  $28.7^{\circ}$ ,  $29.2^{\circ}$ , and  $29.8^{\circ}$  per hour. Combinations of constituents significantly more contrived than those used would be required to approximate these speeds, and this has not been done because the cusps are now believed to include both line-line and line-noise interactions (W. H. Munk, personal communication).

Fig. 3. shows a comparable Fourier analysis of the residuals near five cycles per day. No other study has been found in which this portion of the spectrum has been examined for tidal lines. There is significantly less evidence of a cusp in the final residuals than in Fig. 2; this could have been anticipated from the spectral analysis in Fig. 1. Furthermore, cusps are found adjacent to large tidal lines; these do not occur at five cycles per day.

Table I identifies all of the 114 constituents and shows their amplitudes. The subscript at the right of the name indicates the number of cycles per day.

### Table I. Anchorage Tidal Constituents.

$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Name	Source	Doodson No.	Speed	Amplitude
$ \begin{array}{llllllllllllllllllllllllllllllllllll$				(°/hr)	(feet)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Sa		056.555	.0410686	.519
$\begin{array}{llllllllllllllllllllllllllllllllllll$	Ssa		057.555	.0821373	.182
$\begin{array}{llllllllllllllllllllllllllllllllllll$	Mm		065.455	.5443747	.139
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	MSf		073.555	1.0158958	.347
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Mf		075.555	1.0980331	.101
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	2Q1		125.755	12.8542862	.041
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	σ1		127.555	12.9271398	.129
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Q1		135.655	13.3986609	.210
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	<i>Q</i> <sub>1</sub>		137.455	13.4715145	.030
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0,		145.555	13.9430356	1.197
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	MP,	$M_{2} - P_{1}$	147.555	14.0251729	.236
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	M,	2 1	155.655	14.4966939	.169
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Y1		157.455	14.5695476	.026
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	P <sub>1</sub>		163.555	14.9589314	.588
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	S,		164.555*	15.0000000*	.119
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	K		165.555	15.0410686	2.238
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	I		175.455	15.5854433	.088
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2 PO,	$2P_{1} - O_{1}$	181.555	15.9748272	.060
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	SO,	$S_{a} = O_{1}$	183.555	16.0569644	.225
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	00,		185.555	16.1391017	.084
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2 NS	$2 N_{o} - S_{o}$	217.755	26.8794590	.072
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2 NK 2 S	$2N_{a} + K_{a} - 2S_{a}$	219.755	26.9615963	.136
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	MNS	$M_{2} + N_{2} - S_{2}$	227.655	27.4238337	.162
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	MNK 2 S	$M_{2} + N_{2} + K_{2} - 2S_{2}$	229.655	27.5059710	.107
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2 MS 2 K	$2M_{a} + S_{a} - 2K_{a}$	233.555	27.8039338	.066
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2 N		235.755	27.8953548	.368
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	<i>H</i> a		237.555	27.9682084	.683
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	N		245.655	28.4397295	1.830
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	<i>v</i>		247.455	28.5125831	.493
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2KN 2S	$2 K_{2} + N_{2} - 2 S_{2}$	249.655	28.6040041	.072
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	OP	$O_1 + P_1$	253.555	28.9019669	.145
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	M	1 1	255.555	28.9841042	11.039
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	MKS	$M_2 + K_2 - S_2$	257.555	29.0662415	.108
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	M 2 (KS),	$M_{2} + 2K_{2} - 2S_{2}$	259.555	29.1483788	.087
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2 SN (MK)	$2S_{a}+N_{a}-M_{a}-K_{a}$	261.655	29.3734880	.095
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	λ		263.655	29.4556253	.274
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	L		265.455	29.5284789	.573
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Τ		272.556	29.9589333	.128
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	S		273.555	30.0000000	2.937
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	R		274.554	30.0410667	.200
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	K		275.555	30.0821373	.922
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	MSN	$M_{a} + S_{a} - N_{a}$	283.455	30.5443747	.208
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2 KM (SN)	$2K_{2} + M_{2} - S_{2} - N_{2}$	287.455	30.7086493	.054
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2 SM	2S. – M	291.555	31.0158958	.181
$NO_2$ $N_2 + O_1$ 335.655 42.3827651 .101	SKM	$S_{a} + K_{a} - M_{a}$	293.555	31.0980331	.073
	NO	$N_2 + O_1$	335.655	42.3827651	.101

\* Doodson uses 164.556 with a speed of 15.0000020.

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Name	Source	Doodson No.	Speed	Amplitude
			(°/hr)	(feet)
2MK.t.	$2 M_{o} - K_{i}$	345.555	42.9271398	.311
M	21	355.555	43.4761563	.084
SO.	$S_{a} + O_{b}$	363.555	43.9430356	.157
MK.	$M_{a} + K_{a}$	365.555	44.0251729	.218
SK.	$S_{a} + K_{a}$	383.555	45.0410686	.141
N.	2 N.	435.755	56.8794590	093
3MS	$3M_{\star} - S_{\star}$	437.555	56,9523127	117
MN	$M_{\star} \pm N_{\star}$	445 655	57 4238337	280
MNKS	$M_1 + N_2 + K_3 - S_3$	447 655	57 5059710	085
M.	1112 + 112 + 112 02	455 555	57.9682084	.005
SN	$S \perp N$	463 655	58 4397295	079
KN	$K \perp N$	465 655	58 5218668	134
MS	$M \downarrow S$	473 555	58 9841042	520
MK	$M_2 + 0_2$ M + K	475 555	50 0662415	.550
GI	$S_1 I_2 + I_2$	102 155	50 5204700	.125
SL4	$S_2 + L_2$	401 555	60.000000	.050
MNO	MINIO	525 655	71 2669602	.001
2MO	$N_1 + N_2 + O_1$	545 555	71.3000093	.077
2 MD	$2 N_2 + O_1$	545.555	71.9112440	.141
MNIZ	$3W_2 - F_1$	547.555	71.9955815	.064
MD	$N_2 + N_2 + N_1$	000.000	72.4049023	.061
2MP <sub>5</sub>	$2 N_2 + P_1$	363.333	72.9271398	.134
2 M K <sub>5</sub>	$2 N_2 + K_1$	565.555	73.0092770	.198
MSK <sub>5</sub>	$M_2 + S_2 + K_1$	383.333	74.0251728	.097
3 KM <sub>5</sub>	$K_2 + K_1 + M_2$	585.555	74.1073100	.042
3NKS <sub>6</sub>	$3N_2 + K_2 - S_2$	627.855	85.4013258	.081
2 NM <sub>6</sub>	$2N_2 + M_2$	635.755	85.8635632	.090
2 NMKS <sub>6</sub>	$2N_2 + M_2 + K_2 - S_2$	637.755	85.9457005	.102
2 MN <sub>6</sub>	$2M_2 + N_2$	645.655	86.4079380	.281
2MNKS <sub>6</sub>	$2M_2 + N_2 + K_2 - S_2$	647.655	86.4900752	.098
M <sub>6</sub>		655.555	86.9523127	.507
MSN <sub>6</sub>	$M_2 + S_2 + N_2$	663.655	87.4238337	.093
MKN <sub>6</sub>	$M_2 + K_2 + N_2$	665.655	87.5059710	.127
2 MS <sub>6</sub>	$2M_2 + S_2$	673.555	87.9682084	.483
2 MK <sub>6</sub>	$2M_2 + K_2$	675.555	88.0503457	.146
NSK <sub>6</sub>	$N_2 + S_2 + K_2$	683.655	88.5218668	.104
2 SM <sub>6</sub>	$2S_2 + M_2$	691.555	88.9841042	.090
MSK <sub>6</sub>	$M_2 + S_2 + K_2$	693.555	89.0662415	.057
S <sub>6</sub>		6E1.555**	90.0000000	.006
2 MNO <sub>7</sub>	$2M_2 + N_2 + O_1$	735.655	100.3509735	.059
2 NMK <sub>7</sub>	$2 N_2 + M_2 + K_1$	745.755	100.9046318	.079
2 MSO <sub>7</sub>	$2M_2 + S_2 + O_1$	763.555	101.9112440	.095
MSKO <sub>7</sub>	$\mathbf{M_2} + \mathbf{S_2} + \mathbf{K_2} + \mathbf{O_1}$	783.555	103.0092771	.067
$2(MN)_8\ldots\ldots$	$2M_2 + 2N_2$	835.755	114.8476674	.053
3 MN <sub>8</sub>	$3M_2 + N_2$	845.655	115.3920422	.125
3MNKS <sub>8</sub>	$3M_2 + N_2 + K_2 - S_2$	847.655	115.4741795	.062
M <sub>8</sub>		855.555	115.9364169	.160

† 2 MK3 is named MO3 in Admiralty Manual of Tides, p. 68.

\*\* According to Doodson code, E = +6 and  $\overline{I} = -6$  above and below base 5.

Name	Source	Doodson No.	Speed (°/hr)	Amplitude (feet)
2 MSN <sub>8</sub>	$2M_2 + S_2 + N_3$	863,655	116,4079380	088
2 MNK <sub>8</sub>	$2M_2 + N_2 + K_2$	865.655	116.4900752	.055
3 MS <sub>8</sub>	$3M_2 + S_2$	873.555	116.9523127	.230
3 MK <sub>8</sub>	$3M_2 + K_2$	875.555	117.0344500	.056
MSNK <sub>8</sub>	$M_2 + S_2 + N_2 + K_2$	883.655	117.5059710	.083
$2(MS)_8$	$2M_2 + 2S_2$	891.555	117.9682084	.087
2 MSK <sub>8</sub>	$2M_2 + S_2 + K_2$	893.555	118.0503457	.046
2M2NK,	$2 M_2 + 2 N_2 + K_1$	945.755	129.8887360	.036
3MNK,	$3M_2 + N_2 + K_1$	955.655	130.4331108	.015
4 MK <sub>9</sub>	$4M_2 + K_1$	965.555	130.9774855	.023
3MSK,	$3M_2 + S_2 + K_1$	983.555	131.9933813	.039
4 MN <sub>10</sub>	$4M_2 + N_2$	$\overline{10}45.655$	144.3761464	.051
M <sub>10</sub>	$5 M_2$	1055.555	144.9205211	.055
3MNS <sub>10</sub>	$3M_2 + N_2 + S_2$	1063.655	145.3920422	.065
4 MS <sub>10</sub>	$4M_2 + S_2$	1073.555	145.9364169	.103
2 MNSK <sub>10</sub>	$2M_2 + N_2 + S_2 + K_2$	1083.655	146.4900752	.052
3 M 2 S <sub>10</sub>	$3M_2 + 2S_2$	1091.555	146.9523127	.060
4 MSK <sub>11</sub>	$4M_2 + S_2 + K_1$	1183.555	160.9774855	.033
4 MNS <sub>12</sub>	$4M_2 + N_2 + S_2$	1263.655	174.3761464	.051
5 MS <sub>12</sub>	$5M_{2} + S_{2}$	1273.555	174.9205211	.056
3MNKS <sub>12</sub>	$3M_2 + N_2 + K_2 + S_2$	1283.655	175.4741795	.042
4M 2S <sub>12</sub>	$4M_{2} + 2S_{2}$	1291.555	175.9364169	.045

Table I. Anchorage Tidal Constituents (continued).

In considering the amplitudes, it is important to remember that, although a tidal prediction is a summation of cosine curves, the high and low waters occur when the sum of the first derivatives is equal to zero. In the first derivative, each constituent is weighted according to its speed. Therefore, 2MS<sub>6</sub>, with an amplitude of about one-half foot, contributes as much to the times of high and low waters as a diurnal constituent having an amplitude of three feet.

There are two problems concerning these results that need to be explored. First, as the number of interactions to obtain a particular frequency increases, the number of combinations that add up to this frequency also increases. For example, the Coast and Geodetic Survey uses  $2 \text{ MK}_3$  for the frequency that is named MO<sub>3</sub> by the British. Although the speeds are the same, the node factors and phase corrections are not. In seeking to identify a peak in the high resolution Fourier plot, the tendency is to accept the first combination of constituents that satisfies the data; there may be a more logical one that has not been discovered and, in any case, the multiplicity of satisfactory combinations is bound to introduce some error due to the different corrections for the longitude of the moon's node. Inasmuch as equilibrium relationships are not necessarily valid, there does not seem to be any way to resolve the problem except, possibly, by analyzing a large number of consecutive years of data and empirically determining node corrections.

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Furthermore, are these constituents part of a stationary process? That is, if the harmonic constants are used for future predictions, will they fit the phenomena at that time? This is the characteristic that made reliable tidal predictions possible many years ago. The easiest way to check this point is to compare the harmonic constants derived from different series of data. Data were not available to do this for Anchorage, but the same procedure was used with three years of Philadelphia data (1946, 1952, and 1957) for a smaller set of constituents (Table II). The set of constituents was determined from only the 1957 data.

Using subjective criteria, 16 of the original 37 constituents were unsatisfactory as compared with 9 of the added 24 constituents (roughly a similar ratio). Traditionally, the Coast and Geodetic Survey omits from its predictions analyzed constituents that have amplitudes of less than .03 foot because the phase tends to be unreliable for such small constituents. Of the original 16 poor values, six are larger than .03 foot. However, five of these are long-period constituents (Sa, Ssa, Mm, Mf, and MSf), and it has been shown (6, 7) that the continuum rises sharply in the low frequencies, making the .03-foot limit too low in this portion of the frequency spectrum. This left one unsatisfactory routine constituent,  $2N_2$ , and two unsatisfactory new constituents,  $KN_4$ and MKN<sub>6</sub>, that were greater than .03 foot. A study of all unsatisfactory new constituents showed that the sum of  $K_2$  and  $N_2$  appeared in six of the nine. Furthermore, there appeared to be for these six constituents a consistent pattern in the phase relationships that indicated that a very small change in

	Amplitude —			Phase lag* —		
	1946	1952	1957	1946	1952	1957
	(feet)	(feet)	(feet)			
Mm	0.187	0.067	0.048	16.3	72.2	335.0
MSf	0.166	0.056	0.146	19.8	67.9	348.8
Mf	0.045	0.123	0.108	80.8	292.6	304.6
Ssa	0.129	0.123	0.153	44.6	115.3	1.0
Sa	0.370	0.153	0.267	104.5	55.6	91.2
$MP_1$ †	0.027	0.042	0.039	308.2	308.2	294.0
$\chi_1^{\dagger}$	0.022	0.020	0.036	119.5	146.3	155.4
KP <sub>1</sub> †	0.024	0.011	0.037	123.1	355.2	76.8
$2Q_1$	0.013	0.003	0.031	343.0	100.0	140.1
Q <sub>1</sub>	0.030	0.051	0.031	230.3	225.2	209.3
<i>Q</i> <sub>1</sub>	0.018	0.013	0.030	225.8	81.3	199.8
O <sub>1</sub>	0.264	0.289	0.266	199.0	198.6	202.0
M <sub>1</sub>	0.019	0.008	0.018	342.0	15.2	252.3
P <sub>1</sub>	0.067	0.061	0.096	222.2	207.7	195.6
K <sub>1</sub>	0.316	0.331	0.342	212.7	209.2	211.1
S <sub>1</sub>	0.089	0.065	0.081	170.4	175.5	151.5
$J_1 \dots \dots \dots$	0.030	0.006	0.010	257.5	130.7	108.2

Table II. Tidal Constants; Philadelphia.

## Table II. Tidal Constants, Philadelphia (continued).

	Amplitude —		Phase lag*			
	1946	1952	1957	1946	1952	1957
	(feet)	(feet)	(feet)			
00,	0.010	0.010	0.003	210.2	195.9	205.2
MSN <sub>2</sub> †	0.020	0.020	0.038	281.9	267.4	282.9
2 N <sub>2</sub>	0.084	0.080	0.041	332.4	59.3	48.5
μ2	0.158	0.168	0.138	175.5	164.6	174.5
N <sub>2</sub>	0.403	0.425	0.417	29.8	31.9	31.5
<i>v</i> <sub>2</sub>	0.143	0.145	0.120	33.9	21.8	22.4
M <sub>2</sub>	2.583	2.676	2.506	47.1	44.8	45.3
λ <sub>2</sub>	0.090	0.095	0.061	52.8	58.2	55.7
L <sub>2</sub>	0.221	0.238	0.283	52.2	70.0	56.4
T <sub>2</sub>	0.032	0.026	0.015	68.7	74.9	227.2
S <sub>2</sub>	0.322	0.346	0.328	83.9	79.8	78.2
R <sub>2</sub>	0.019	0.005	0.016	29.2	191.4	237.4
K <sub>2</sub>	0.108	0.094	0.078	73.9	75.4	60.1
2 SM <sub>2</sub>	0.014	0.019	0.022	316.6	326.7	266.1
$2 \text{NP}_3^{\dagger} \dots$	0.015	0.015	0.016	143.4	337.5	8.2
NO <sub>3</sub> †	0.022	0.019	0.024	77.0	100.8	77.8
SO <sub>3</sub> †	0.026	0.026	0.030	145.4	125.9	131.0
M <sub>3</sub>	0.025	0.029	0.014	194.7	170.3	37.9
MK <sub>3</sub>	0.081	0.083	0.068	124.7	120.9	125.6
2 MK <sub>3</sub>	0.080	0.088	0.068	97.1	95.8	95.7
ML <sub>4</sub> †	0.046	0.061	0.056	343.5	348.4	337.3
SL <sub>4</sub> †	0.014	0.019	0.028	26.6	51.8	26.2
$MK_4^{\dagger}$	0.032	0.034	0.026	17.5	16.4	6.2
MN <sub>4</sub>	0.121	0.122	0.114	336.0	334.3	330.9
MS <sub>4</sub>	0.098	0.115	0.095	33.6	26.3	25.3
M <sub>4</sub>	0.345	0.378	0.311	350.3	346.1	346.1
S <sub>4</sub>	0.007	0.006	0.010	359.4	328.8	73.5
MNO <sub>5</sub> †	0.022	0.022	0.017	349.0	342.0	336.7
2 MO <sub>5</sub> †	0.044	0.053	0.039	355.3	342.0	346.7
2 MP <sub>5</sub> †	0.028	0.031	0.021	28.1	26.6	7.9
$2MK_{5}$ †	0.051	0.055	0.045	7.8	0.5	358.1
MNK <sub>5</sub> †	0.018	0.023	0.020	49.3	313.9	326.0
$2 MN_6 \dagger \dots$	0.076	0.071	0.075	195.5	188.4	179.2
2 ML <sub>6</sub> †	0.046	0.060	0.061	205.1	209.0	189.0
$2 MS_6^{\dagger} \dots$	0.063	0.068	0.059	243.4	239.0	229.5
MSL <sub>6</sub> †	0.018	0.024	0.033	235.7	272.2	245.7
S <sub>6</sub>	0.004	0.000	0.005	324.7	297.0	33.6
M <sub>6</sub>	0.148	0.159	0.138	206.4	205.0	196.4
$2(MN)_8$ †	0.018	0.022	0.015	108.4	124.2	118.1
3MN <sub>8</sub> †	0.048	0.045	0.041	131.7	129.0	120.4
3ML <sub>8</sub> †	0.024	0.033	0.025	153.5	130.2	117.1
3MS <sub>8</sub> †	0.038	0.041	0.033	187.1	174.3	171.9
2 MSL <sub>8</sub> †	0.012	0.020	0.021	183.7	195.9	178.4
M	0.059	0.067	0.052	146.3	146.8	140.9

\* Referred to 75°W (g).

† Not included in original 37 constituents.

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speed could make the harmonic constants acceptable. The sum of  $M_2$  and  $L_2$  varies from the sum of  $K_2$  and  $N_2$  by .009°/hr (one cycle in about 4.5 years). These speeds are too close together to be separated with only one year of data. When the change in speed was made on the six constituents and the data were reanalyzed, the constants for all became satisfactory, leaving only 3 of the added 24 constituents unsatisfactory; all three are less than .03 foot. Furthermore, a new spectral analysis of the residuals showed a lower level of energy in species 4, 6, and 8—the species containing the six modified constituents—thereby indicating an improvement in fitting the data by virtue of the changed speeds.

In retrospect, it is now obvious why the combination of  $M_2$  and  $L_2$  should have been given preference over  $N_2$  and  $K_2$ . In equilibrium theory, the four largest semidiurnal constituents are  $M_2$ ,  $S_2$ ,  $N_2$ , and  $K_2$ , in that order.  $L_2$ is only  $22^{\circ}/_{\circ}$  of  $K_2$ . Hence, the choice of species-2 constituents was limited to the first four in trying various combinations to match the frequencies where high resolution Fourier analysis showed large peaks. However, the analysis for Philadelphia shows  $L_2$  to be roughly three times larger than  $K_2$ . Therefore, it is obvious that larger interactions should be expected from the sum of  $M_2$  and  $L_2$  than from  $N_2$  and  $K_2$ .

Essentially then, 3 of 24 new constituents are unsatisfactory compared with 16 of the original 37—an amazing improvement considering that the 37 include the major constituents that are not subject to question. These results raise questions as to whether some corrections in the speeds of the smaller standard constituents may be indicated. At one time the manpower requirements for successive analyses of a large number of years of data made such a study virtually impossible. The present availability of both computer programs for analysis and data in a format compatible with computers makes such a study

Table III. Comparisons of observations and predictions for May, July, and October 1964; Anchorage.

No. of constituents in predictions	37	114
Time differences (predobs.)		
High water (hours)	-0.13	-0.03
Low water (hours)	-0.35	-0.19
Ratio, obs./pred.		
Mean range	1.05	1.01
Tide level minus sea level		
Observed (feet)	-1.09	-1.09
Predicted (feet)	70	-1.00
Residual variance (192 days, 1964)		
in feet <sup>2</sup>	.9767	.2954
$^{\circ}/_{\circ}$ of original variance	1.33	0.40

now only a modest effort; plans for future tidal research in ESSA will include this study.

Tables III and IV show comparisons of observations and predictions for Anchorage and Philadelphia, respectively. If the time differences were smaller and if the ratio of observed range to predicted range were closer to 1.00, the fit would be better. Tide level minus sea level is a measure of

distortion of the the curve from a pure cosine curve, primarily due to the contributions of compound constituents. An optimum fit would show identical values for observed and predicted values. The residual variance, which should be as small as possible, is significant only as a comparative number. The absolute numbers depend primarily on the range of tide and the energy in

Table IV. Co	omparisons	of obser	vations	and pre-
dictions for	January, N	Iarch, J	uly, and	October
1957; Phila	adelphia.			

37	61
-0.18	-0.14
-0.33	-0.28
1.06	1.04
-0.23	-0.23
-0.12	-0.14
.3467	.3299
8.49	8.08
	$\begin{array}{c} 37 \\ -0.18 \\ -0.33 \\ 1.06 \\ -0.23 \\ -0.12 \\ .3467 \\ 8.49 \end{array}$

the meteorological continuum. The improvement in practical predictions by using more constituents is clearly shown in the results presented in Tables III and IV.

The use of "harmonic" in the title warrants some explanation. Even though annual or seasonal node corrections (amplitude factors and phase corrections) are applied to lunar constituents by all organizations preparing tidal tables, the predictions are ordinarily regarded as harmonic if subsequent corrections are not added to the derived times, the heights of high and low waters, or both. It is used in the title of this paper in this sense to differentiate the procedure from Doodson's shallow-water technique (4). Doodson (2) developed a purely harmonic set of constituents (calling the usual method, "quasi-harmonic"), but he never used the method for practical tidal predictions.

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