# Using Bayesian Statistics in Operational Testing 

Thuan H. Tran

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USING BAYESIAN STATISTICS
IN OPERATIONAL TESTING
THESIS

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AFIT/GOR/ENS/98M-25

DEPARTMENT OF THE AIR FORCE AIR UNIVERSITY AIR FORCE INSTITUTE OF TECHNOLOGY

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USING BAYESIAN STATISTICS IN OPERATIONAL TESTING

## THESIS

Presented to the Faculty of the Graduate School of Engineering of the Air Force Institute of Technology Air University

In Partial Fulfillment of the Requirements for the Degree of Master of Science in Operations Research

Thuan H. Tran, B.S.
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March 1998

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## Abstract

HQ Air Force Operational Test and Evaluation Center (AFOTEC) is responsible for the operational test and evaluation of major weapon systems during their acquisition phase. In operational testing at AFOTEC, it is often the case that not enough data or samples are available to make high confidence classical inferences on various statistics. The use of Bayesian statistical methods may be a solution in which higher confidence inferences can be made on statistics by using other sources of data.

This research explored the applicability of Bayesian methods to the problem of determining the reliability of a series system, a parallel system, and a bridge system. The time to failure of each component in each system is assumed to be exponentially distributed. A basic exponential case and a basic binomial case are also evaluated.

In general, using simulated data and real data when possible, the Bayesian methods produced confidence intervals that were much tighter than the classical inference methods, thus allowing a decision maker to have higher confidence in making a decision. System level data and aggregated component level data produced a much tighter confidence interval than component level data aggregated to system.

## USING BAYESIAN STATISTICS IN OPERATIONAL TESTING

## I. Introduction

## General Issue

In operational testing at the Air Force Operational Test and Evaluation Center (AFOTEC), it is often the case that not enough data or samples are available to make high confidence classical inferences on various statistics. The use of Bayesian statistical methods may be a solution in which higher confidence inferences can be made on statistics by using other sources of data.

The testing of new weapons systems in the Air Force is divided into two types of testing: Developmental Test and Evaluation (DT\&E) and Operational Test and Evaluation (OT\&E). In developmental testing, the contractor participates directly with the DT\&E test agency and the goal is to produce a workable system. However in the operational testing phase, AFOTEC performs independent tests to ensure the system meets Air Force standards and requirements and is ready for production. Traditionally these two types of testing were separate, but with the new call for streamlined acquisition and reduction of testing funds, AFOTEC has to look at incorporating DT\&E data into OT\&E.

At present, AFOTEC will use DT\&E data only when DT\&E data was collected by sources that are independent of, and
not influenced by, the contractor. Additionally, AFOTEC has to make sure the data from the DT\&E system was from a system configured like the system to be used in OT\&E.

Bayesian statistics incorporates "prior information", such as engineering estimates and DT\&E data, into making statistical inferences. For example, let $f(y \mid U)$ be the probability distribution function (pdf) for the time to failure for a component, where $y$ is the data and $U$ is a parameter of the pdf. To utilize. prior information, Bayesian statistics assume that the parameter $U$ is indeed a random variable in itself, with its own pdf. Bayesian statistics call the distribution of the random variable $U$ an a priori or a prior pdf. This prior pdf is called $g(U)$, which expresses the state of knowledge (or ignorance) about U before any new sample data is analyzed. There are various methodologies to convert prior information, such as engineering estimates and DT\&E data, into a prior distribution. Then given the prior distribution $g(U)$, the probability distribution $f(y \mid U)$, and the new data $y$, Bayes' theorem can be used to calculate the so-called posterior pdf $g(U \mid y)$. The posterior distribution $g(U \mid y)$ is in a sense, the updated prior distribution. The posterior distribution can now be used to update the pdf, $f(y \mid U)$, the time to failure distribution.

Problem Statement
Can a system reliability analysis based on Bayesian statistics using DT\&E data be used to reduce the number of samples and test time needed for OT\&E and provide the same or better confidence levels than classical statistical inference methods?

Research Objectives
The objectives of this research are: 1) to investigate different Bayesian methods and various weighting schemes for using prior information; 2) develop a methodology for using Bayesian statistics with DT\&E data to predict system reliability based on data obtained from a program which is in the process of transition from development to production and compare the results with those obtained from classical statistical methods.

Scope
This research will use DT\&E and OT\&E reliability data obtained from a test program when possible. Simulated reliability data will be used to verify and validate the methodology. This research will concentrate mainly on the exponential case. This research is limited to exploring the applicability of Bayesian statistical methods to the problem of determining the reliability of a series system, a parallel system, and a bridge system. The time to failure
of each component in each system is assumed to be exponentially distributed. A basic exponential case and a basic binomial case are also evaluated. The methodology developed in this research is based on the assumption that both DT\&E and OT\&E data are available. The next chapter will identify and discuss some of the different approaches of Bayesian statistics as well as comparing and contrasting these with the classical inference method.

## II. Literature Review

## Overview

This chapter will begin with the classical statistical inference and Bayesian statistical inference approaches. The chapter concludes with current thinking on the use of Bayesian statistical concepts for the type of reliability analysis found in the literature.

Two Views of Probability
In the classical method, the probability of an event is defined as the relative frequency of an event occurring during repeated runs of an experiment. Let $S$ be the set of all possible outcomes of an experiment. Let $A$ be one of the possible outcomes. The classical method defines the probability of $A$ (the likelihood of outcome $A$ happening) as $P[A]=\lim _{n \rightarrow \infty}(a / n)$, where $a$ is the number of times outcome $A$ occurs during $n$ runs of the experiment. The value of $P[A]$ is an unknown constant that can be estimated if enough runs of the experiment are conducted. This classical view is also known as the "frequentist" viewpoint (14:50).

The Bayesian method defines probability subjectively. In contrast to the classical method, the Bayesian method does not consider $P[A]$ to be an objective estimate of the likelihood of outcome A. Instead the Bayesian method considers $P[A]$ as a rational expression of one individual's
degree of belief that outcome A will occur. Different values of $P[A]$ based on different perceptions of prior experience can be assigned by different individuals. This does not mean the Bayesian method abandons experimentation. Experimentation provides an important tool for an individual to refine their assessment of $P[A]$ (14:50-51).

Consider the following experiment: a coin is flipped, with the outcome to be "head" or "tail" (S = \{head,tail\}). Let the event $A=\{$ head $\}$. To find $P[A]$, the classical method would require $n$ flips of the coin ( $n$ large), count the $m$ occurrences of $A=\{$ head $\}$, and compute $P[A]$ to be approximately $\mathrm{m} / \mathrm{n}$. In contrast, the Bayesian method might declare that $P[A]=0.5$ based on experience with similar coins that a "head" is as likely to occur as a "tail" in any flip. To validate and refine the estimate, a number of experimental flips of the coin would then be made.

There are distinctive differences between classical statistical inference and Bayesian statistical inference methods. The classical statistical inference uses inductive reasoning while the Bayesian method uses deductive reasoning. The Bayesian method takes into account prior information while the classical method only considers the prior information in an informal manner, if at all. The classical method is more restrictive due to the exclusive
use of sample data. To achieve the same level of inferences, the Bayesian method usually requires less sample data as compared to the classical method. When sample data is expensive or difficult to obtain, as reliability data often is, the Bayesian method has the advantage of being able to use prior information. Table 1 summarizes the characteristics of the two approaches.

Table 1. A Summary of Certain Characteristics of the Sampling Theory and Bayesian Methods of Statistical
Inference (6:169)

| Characteristic | Sampling Theory | Bayesian |
| :--- | :--- | :--- |
| Parameter(s) of <br> Interest | Unknown <br> constant (s) | Random Variable(s) |
| Prior Distribution | Does not exist | Exists and <br> explicitly assumed |
| Sampling Model | Assumed | Assumed |
| Posterior <br> Distribution | Does not exist | Explicitly derived |
| Method of <br> Reasoning | Inductive | Deductive |
| Type of Interval <br> Estimate | Confidence <br> interval | Probability <br> interval |
| Role of Past <br> Experience | Not applicable | Applicable <br> Purpose of <br> Sampling <br> Experience <br> Supply data for <br> making inferences <br> Confirm or deny <br> expected <br> performance as <br> predicted from <br> past experience <br> Inferences of |
| More restricted <br> than Bayes' <br> because of <br> exclusive use of <br> sample data | Depends on ability <br> to quantitatively <br> relate past <br> experience to the <br> sample data |  |
| Data | Bayes approach <br> usually requires <br> less because it <br> utilizes relevant <br> past data |  |

Martz and Waller identify four advantages for using the Bayesian method: 1) increased quality of the inferences, provided the prior information accurately reflects the true variation in the parameters; 2) reduction in testing requirements (test time and/or sample size); 3) inferences that are unacceptable must come from incorrect assumptions and not from inadequacies of the method used to provide the inferences; and 4) the rules for manipulating probability statements on components into corresponding statements on system reliability are well known, whereas equivalent rules for manipulation of confidence statements are not (6:172-3). Classical Statistical Inference.

Let the population be defined as the total number of systems in use for a particular system. When it is not practical to test all members of a population, a subset or sample of systems can be selected from the population for testing. The sample is presumed to be randomly selected such that each system having an equal chance of being in the sample.

Two types of inferences can be drawn from the sample. A point estimate approximates the true value of the population parameter with a single value. However, this single value of a point estimate does not provide any information about the uncertainty associated with that
estimate. To account for uncertainty, an interval estimate provides an estimate that the sample statistic is within a certain interval about the true population parameter. Consider the mean of a sample, $\bar{x}$, which is a point estimate of the population mean. Compared with the true population mean $\mu, \bar{x}$ will differ by some unknown sampling error amount ع. Thus $\bar{x}=\mu+\varepsilon$ or $\bar{x}=\mu-\varepsilon$. For large sample sizes, both the sampling distribution and sampling error distribution are approximately normal by the Central Limit Theorem. From this, a confidence interval based on the population standard error, $\sigma$, is developed. The population standard error is the deviations or distances of the population measurements from their mean.

$$
\begin{equation*}
(\bar{x}-z \star \sigma)<\mu<(\bar{x}+z \star \sigma) \tag{1}
\end{equation*}
$$

where $z$ is the critical value associated with a specified probability. The population standard error is usually not known in most cases. However, it can be estimated by using the sample standard error, $s$ with

$$
\begin{align*}
& s=\left(\frac{1}{m}\right) \sum_{i=1}^{m}\left(X_{i}-\bar{X}\right)^{2}  \tag{2}\\
& \text { and } \bar{X}=\left(\frac{1}{m}\right) \sum_{i=1}^{m} X_{i} \tag{3}
\end{align*}
$$

Thus an approximate confidence interval is obtained using s.

Bayesian Statistical Inference
Bayes' Theorem. Bayes' theorem (6:174-5) can be written as:

$$
\begin{equation*}
g(\theta \mid x)=\frac{f(x \mid \theta) g(\theta)}{f(x)} \tag{4}
\end{equation*}
$$

where $\theta$ is the population parameter
$g(\theta \mid x)$ is the posterior probability distribution of $\theta$ given sample data $x$
$g(\theta)$ is the prior probability distribution of $\theta$
$f(x \mid \theta)$ is the probability of observing sample data $x$ given the true parameter $\theta$
$f(x)$ is the marginal probability distribution of $x$. $f(x)$ can be obtained by

$$
f(x)=\begin{aligned}
& \int f(x \mid \theta) g(\theta) d \theta, \theta \text { continuous } \\
& \Sigma f(x \mid \theta) g(\theta), \theta \text { discrete. }
\end{aligned}
$$

The Prior Distribution. Bayesian inference is appropriate only when the prior assessment of $\theta$ is accurate. Great care must be exercised when selecting the prior density $g(\theta)$. The prior density can take any form. However, natural conjugate priors and noninformative priors (also called priors of ignorance) are used in most practical applications. When using a natural conjugate prior, the posterior distribution is in the same family as the prior distribution and can be obtained simply by using analytical tools. When there is little or no information on the value
of a parameter, a noninformative prior is used. The most commonly used is the uniform distribution. For a detailed discussion of the noninformative prior, see Press (8:46-51). For the continuous prior distribution, discretization is often used to allow for more tractable data manipulation. Chay (1) argues that since numerical integration can be done using computer calculations, it is not necessary to approximate continuous prior distributions using discretization. The process of determining the form of $g(\theta)$ is difficult and controversial. When selecting a prior, it must be both reasonable and justifiable.

Bayesian Reliability Testing Approaches. In this section, current approaches in applying Bayesian methods in reliability testing will be addressed.

Chen and Papadopoulos (2) proposed a Bayesian method for a generalized exponential failure model for components in a parallel or series system. The gamma or uniform distribution is used as a prior. The generalized failure models under consideration are the exponential, Weibull, Rayleigh, and as a special case, the extreme value failure model. Sharma and Bhutani (11) considered a parallel system composed of independent and identical components whose failure distribution was exponentially distributed. The exponential distribution is used as a prior. Villacourt and

Mahaney (12) used the Bayesian method to design a reliability demonstration test on a lithography expose tool. The failure times are assumed to be exponentially distributed. The gamma distribution is used as a prior.

Martz, Waller, and Fickas (7) developed a Bayesian procedure for a series system of binomial subsystems and components. Test or prior data (perhaps both or neither) at the system, subsystem, and component level are considered. The beta distribution is used as a prior. The method was used to estimate the overall reliability of an air-to-air heat seeking missile system with five major subsystems and up to nine components per subsystem. Martz and Waller (5) extended the method to cover the case of a complex series/parallel systems of binomial subsystems and components. These methods are very complex and difficult to implement.

Willits, Dietz, and Moore (15) show that for a series-system, reliability estimates using very small sets (less than 10 data points) of binomial test-data, there is no clear advantage of using Bayes interval estimation unless the prior mean system reliability is believed to be within 20 percent of the true system reliability. A classical method for very small samples, the Linstrom-Madden estimator, should be used.

When both prior and current data are available, which is the case in this research, the methods mentioned above in general are not applicable. However, studying these methods provided the general knowledge of understanding how Bayesian statistical methods worked.

In this research, the applicability of Bayesian statistical methods to the problem of determining the reliability of a series system, a parallel system, and a bridge system is being studied. The time to failure of each component in each system is assumed to be exponentially distributed. A basic exponential case and a basic binomial case are also evaluated. There is very little information concerning the use of Bayesian methods to the systems mentioned above in the literature. The methodology being developed in Chapter III is based on the works of the following individuals.

Lemaster (4) studied the applicability of Bayesian method to the problem of determining cruise missile component reliability. The exponential and binomial distributions were used for the failure rate. For the exponential case, a gamma prior is used. For the binomial case, a beta prior is used.

Sharma and Bhutani (10) considered the case for a series system when the failure time for the system is
exponentially distributed. The gamma distribution is used as a prior.

Frickenstein (3) studied the case for a simple system (one component) when the failure time for the system is assumed to be exponentially distributed. The gamma distribution is used as a prior.

The text book, Bayesian Reliability Analysis, written by Martz and Waller (6) is the standard reference work on Bayesian statistical methods and will be used extensively in this research effort. The binomial model developed in Chapter III is based on the methods developed by Lemaster (4) with modifications based on Martz and Waller (6). The exponential model developed in Chapter III is based on the methods developed by Lemaster (4) and by Frickenstein (3) with modifications based on Martz and Waller (6).

Reliability analysis methods for a series system, a parallel system, and a bridge system (with the time to failure of each component in each system is assumed to be exponentially distributed) are developed in Chapter. III utilizing the exponential model. For the series system, the Bayesian methods developed by Sharma and Bhutani (10) will also be modified for use in this research. The next chapter will discuss the methodology used in this research to accomplish the research objectives stated in Chapter I.

## III. Methodology

Overview.
This chapter details the methodology used to accomplish the research objectives stated in Chapter I. The methodology developed in this chapter is based on the assumption that both DT\&E (prior) and OT\&E (current) data are available. A basic binomial model and a basic exponential model are developed first. The basic exponential model is then applied to the problem of determining the reliability of a series system, a parallel system, and a bridge system. The time to failure of each component in each system is assumed to be exponentially distributed. Classical and Bayesian point estimates and confidence intervals obtained from each system will be compared in Chapter IV.

Data Source.
For the basic binomial model, a hypothetical set of missile test data will be used to validate the methodology. For the basic exponential model, the model is applied to data obtained by AFOTEC during a reliability testing of a selected simple system (system is treated as one component) with the time to failure of the system is assumed to be exponentially distributed. This is the only set of true data used in this research. Simulated data will be used to
validate the methodology for a series system, a parallel system, and a bridge system. This research uses a computer program called RAPTOR (Rapid Availability Prototyping for Testing Operational Readiness), which is developed by AFOTEC, to simulate the true system (series, parallel, bridge) mentioned above. RAPTOR is verified and validated by AFOTEC and is an excellent tool for use in this research effort.

The Binomial Model.
This model is appropriate for systems or components that are assumed to have binomial failure distribution. The classical binomial method is given first. Then the Bayesian binomial method is given based on the assumption that both prior data (DT\&E data) and current data (OT\&E data) are available. The model is then applied to a hypothetical missile launch problem in Chapter IV.

The Classical Binomial Method.
The binomial distribution is one of the commonly used distribution in reliability. Consider a missile system that is being tested with the outcome of each test as the missile success or failure to launch. Assuming a missile system has the binomial distribution, the point estimate for the probability of success $p$ (which is the reliability of a missile system) and $80 \%$ confidence interval about $p$ will be
computed. For the binomial distribution, the point estimate using the maximum likelihood estimator is

$$
\begin{equation*}
\widehat{p}=\left(\frac{X}{n}\right) \tag{5}
\end{equation*}
$$

where $X$ is the number of successes from a set of $n$ missile units placed into a test of given duration (6:53). The confidence limits can be approximated by using the $F$ distribution. The $100(1-\gamma) \%$ two-sided confidence interval (TCI) is (6:56)

$$
\begin{equation*}
\left(\frac{X}{X+(n-X+1) F_{1-\gamma / 2}(2 n-2 X+2,2 X)}, \frac{(X+1) F_{1-\gamma / 2}(2 X+2,2 n-2 X)}{(n-X)+(X+1) F_{1-\gamma / 2}(2 X+2,2 n-2 X)}\right) . \tag{6}
\end{equation*}
$$

The Bayesian Binomial Method.
Since they are relatively easy to compute and can be adapted to a number of situations, the family of beta distributions, $B(x, n)$, are used for the binomial case to calculate both the prior and posterior distributions. For example, the analyst's knowledge and experience with the system is utilized to select $x$ and $n$. Thus the analyst can increase or decrease the importance of the prior on the resulting posterior distribution (4:39).

Bayesian Binomial Prior. For the binomial sampling, $a \operatorname{B}\left(x_{0}, n_{0}\right)$ distribution can be used to maximize flexibility and make it easier to calculate the posterior distribution since the $B\left(x_{0}, n_{0}\right)$ distribution is the natural conjugate prior distribution. The parameters $x_{0}$ and $n_{0}$ can
be interpreted as the pseudo number of survivals and pseudo sample size for the prior life test. Here "pseudo" should be thought of as meaning "pretended" (6:265). When the true prior distribution is not of the beta family, Weiler (13) showed that assuming a $B\left(x_{0}, n_{0}\right)$ distribution is acceptable in many practical applications. Weiler was able to show that severe deviations from the beta prior parameter values will result in minor changes in the corresponding posterior distributions. DT\&E data will be used to approximate $\mathrm{x}_{0}$ and $n_{0}$ that fit the $B\left(x_{0}, n_{0}\right)$ distribution. For the missile launch problem in Chapter IV where the outcome of each test is a missile success or failure to launch, $x_{0}$ is the number of successes during DT\&E test and similarly $n_{0}$ is the total number tested.

Bayesian Binomial Posterior. For the $B\left(x_{0}, n_{0}\right)$ prior distribution, the resulting posterior distribution is also a beta distribution of the form $B\left(x+x_{0}, n+n_{0}\right)$, where $x$ is the observed successes and $n$ is the sample size from the test being used to update the prior. The probability density function (6:266) is given as

$$
\begin{equation*}
g\left(p \mid x ; x_{0}, n_{0}\right)=\left(\frac{\Gamma\left(n+n_{0}\right)}{\Gamma\left(x+x_{0}\right) \Gamma\left(n+n_{0}-x-x_{0}\right)}\right) p^{\left(x+x_{0}\right)-1}(1-p)^{\left(n+n_{0}-x-x_{0}\right)-1} \tag{7}
\end{equation*}
$$

where $0<p<1$.

Bayesian Binomial Point Estimate. The mean of the posterior distribution is the Bayesian point estimator. Under the squared error loss function, the Bayesian point estimator is (6:267)

$$
\begin{equation*}
\widehat{p}=\mathrm{E}\left(p \mid \mathrm{x} ; \mathrm{x}_{0}, \mathrm{n}_{0}\right)=\left(\frac{x+x_{0}}{n+n_{0}}\right) . \tag{8}
\end{equation*}
$$

The loss function measures the error sustained by estimating $p$ by $\hat{p}$. The squared error loss function often used in practical application is $(\widehat{p}-p)^{2}(14: 56)$.

Bayesian Binomial Probability Interval. The Bayesian methods use "probability intervals" instead of "confidence intervals". Recall that the classical method assumes that the parameter $p$ estimated is an unknown constant. Thus the estimators of the end points of the confidence interval associated with $p$ estimated are random variables. A classical confidence interval is not an explicit probability statement about $p$. However, it is "the probability that the interval estimator will generate an interval that will contain the true value of $p^{\prime \prime}$ (14:57). In contrast, Bayesian method considers $p$ to be a random variable. Thus a Bayesian probability interval is an explicit probability statement about the value of $p$ (6:208).

Using the $F\left(\mathrm{n}_{1}, \mathrm{n}_{2}\right)$ distribution, the Total Bayesian Probability Interval (TBPI) can be calculated. A 80\%
confidence interval will be calculated. For the $100(1-\gamma) \%$ TBPI, the upper and lower interval endpoints are (6:270)

$$
\begin{equation*}
\binom{\frac{x+x_{0}}{x+x_{0}+\left(n+n_{0}-x-x_{0}\right) F_{1-y / 2}\left(2 n+2 n_{0}-2 x-2 x_{0}, 2 x+2 x_{0}\right)},}{\frac{\left(x+x_{0}\right) F_{1-y / 2}\left(2 x+2 x_{0}, 2 n+2 n_{0}-2 x-2 x_{0}\right)}{n+n_{0}-x-x_{0}+\left(x+x_{0}\right) F_{1-y / 2}\left(2 x+2 x_{0}, 2 n+2 n_{0}-2 x-2 x_{0}\right)}} \tag{9}
\end{equation*}
$$

The Exponential Model.
This model is appropriate for systems or components that are assumed to have exponential failure distribution. The classical exponential method is given first. Then the Bayesian exponential method is given based on the assumption that both prior data (DT\&E data) and posterior data (OT\&E data) are available. In Chapter IV, the model is applied to data obtained by AFOTEC during a reliability testing of a selected simple system with the time to failure of the system is assumed to be exponentially distributed.

The Classical Exponential Method.
The exponential distribution is the most widely used distribution in reliability. Assuming the time to failure of a system or component has the exponential distribution, point estimates for the failure rate $\lambda$ and $80 \%$ confidence intervals on $\lambda$ will be computed. For the exponential distribution, the point estimate of $\lambda$ using the maximum likelihood estimator is

$$
\begin{equation*}
\hat{\lambda}=\left(\frac{f}{T}\right) \tag{10}
\end{equation*}
$$

where $f$ is the number of failures and $T$ is the total test time. The number of failures, $f$, is presumed to be a random variable. The confidence limits can be approximated by using the chi square $\chi^{2}$ distribution. The $100(1-\gamma) \%$ two-sided confidence interval (TCI) is (6:122)

$$
\begin{equation*}
\left(\frac{\chi_{\gamma / 2}^{2}(2 f)}{2 T}, \frac{\chi_{1-\gamma / 2}^{2}(2 f)}{2 T}\right) \tag{11}
\end{equation*}
$$

For the reliability function $R(t)=\exp (-\lambda t)$, the reliability estimator of $R(t)$ for a mission time $t$ is

$$
\begin{equation*}
\widehat{R}(t)=\exp (-\hat{\lambda} t) \tag{12}
\end{equation*}
$$

where $t$ is the mission length.
Equation 12 is also used to calculate an interval estimate of $\widehat{R}(t)$ by using the lower and upper bound of $\hat{\lambda}$ obtained from Equation 11 in place of $\hat{\lambda}$.

The Bayesian Exponential Method.
When examining a continuously operating electronic system, the failure time is often assumed to be exponentially distributed. The distribution of the number of failures, $f$, in fixed total test time, $T$, can be described by the Poisson distribution (6:255) as

$$
\begin{equation*}
p(f \text { failures in total time } T \mid \lambda)=\left(\frac{e^{-\lambda T}(\lambda T)^{f}}{f!}\right) \tag{13}
\end{equation*}
$$

where $\lambda, T>0, f=0,1,2, \ldots$ and assuming that failed items are replaced. This is known as Poisson sampling. Bayesian Exponential Prior. For the Poisson sampling, a gamma prior distribution, $G(\alpha, \beta)$, may be used to maximize flexibility and make it easier to calculate the posterior distribution since the $G(\alpha, \beta)$ distribution is the natural conjugate prior distribution (6:289). The $G(\alpha, \beta)$ prior distribution is probably the most widely used and has the following probability density function:

$$
\begin{equation*}
g(\lambda ; \alpha, \beta)=\left(\frac{\beta^{a} \lambda^{a-1} e^{-\beta \lambda}}{\Gamma(a)}\right) \tag{14}
\end{equation*}
$$

where $\lambda, \alpha$, and $\beta>0$ and $\Gamma(\alpha)$ is the gamma function of $\alpha$.
The shape parameter $\alpha$ can be interpreted as the pseudo number of failures in a prior life test of duration $\beta$ pseudo time units (6:289). The mean and variance of the gamma distribution are

$$
\begin{equation*}
E(\lambda)=\left(\frac{a}{\beta}\right) \tag{15}
\end{equation*}
$$

and $\mathrm{V}(\lambda)=\left(\frac{a}{\beta^{2}}\right)$.
$E(\lambda)$ and $V(\lambda)$ can be estimated using the sample mean and variance of $\lambda$ respectively with $E(\lambda)=\bar{\lambda}$ and $V(\lambda)=s_{\lambda}^{2}$.

Equations 2 and 3 (page 9) are used to compute $\bar{\lambda}$ and $s_{\lambda}^{2}$. Thus $\alpha$ and $\beta$ can be computed as

$$
\begin{align*}
& \alpha=\left(\frac{E^{2}(\lambda)}{V(\lambda)}\right)  \tag{17}\\
& \text { and } \beta=\left(\frac{E(\lambda)}{V(\lambda)}\right) . \tag{18}
\end{align*}
$$

Bayesian Exponential Posterior. For the $G(\alpha, \beta)$ prior distribution, the resulting posterior distribution is a $G(f+\alpha, T+\beta)$, where $f$ is the number of failures and $T$ is the total test time. The probability density function (6:290) is given as

$$
\begin{equation*}
g(\lambda \mid f ; \alpha, \beta)=\left(\frac{(T+\beta)^{f+a} \lambda^{f+\alpha-1} e^{-(T+\beta) \lambda}}{\Gamma(f+a)}\right) \tag{19}
\end{equation*}
$$

where $\lambda>0$. The parameter $(f+\alpha)$ is referred as the combined number of failures and ( $T+\beta$ ) is the combined total test time.

Bayesian Exponential Point Estimate. The mean of the posterior distribution is the Bayesian point estimator. Under the squared error loss function, the Bayesian point estimator is

$$
\begin{equation*}
\hat{\lambda}=\mathrm{E}(\lambda \mid f ; \alpha, \beta)=\left(\frac{f+a}{T+\beta}\right) \tag{20}
\end{equation*}
$$

where $(f+\alpha)$ is the combined number of failures and ( $T+\beta$ ) is the combined total test time (6:292). the $100(1-\gamma) \% \mathrm{TBPI}$, the upper and lower interval endpoints are (6:294)

$$
\begin{equation*}
\left(\frac{\chi_{y / 2}^{2}(2 f+2 a)}{2(t+\beta)}, \frac{\chi_{1-\gamma / 2}^{2}(2 f+2 a)}{2(t+\beta)}\right) \tag{21}
\end{equation*}
$$

For the reliability function $R(t)=\exp (-\lambda t)$, the Bayesian estimator of $R(t)$ for a mission time $t$ is (3:8)

$$
\begin{align*}
\widehat{R}(t) & =E[R(t) \mid f]=\int_{0}^{\infty} \exp (-\lambda t) g(\lambda \mid f ; a, \beta) d \lambda \\
& =\left(\frac{\left(\frac{T}{\beta}\right)+1}{\left(\frac{T}{\beta}\right)+\left(\frac{t}{\beta}\right)+1}\right)^{a+f} \tag{22}
\end{align*}
$$

where $f$ is the number of failures, $T$ is the total test time and $t$ is the mission time.

Another way of computing the Bayesian estimator of $R(t)$ is $\widehat{R}(t)=\exp (-\hat{\lambda} t)$. Both methods should yield very similar result. Mathematically speaking, Equation 22 is selected for use since it is directly derived. The reliability function $R(t)=\exp (-\lambda t)$ is also used to calculate an interval estimate of $\widehat{R}(t)$ by using the lower and upper bound of $\hat{\lambda}$ obtained from Equation 21 in place of $\hat{\lambda}$.

Bayesian Weibull Method. If the true distribution of the time to failure is not exponentially distributed, the Bayesian method can still be developed but it is a lot
harder to do the number calculation. Another frequently used time to failure distribution is the Weibull distribution. The Bayesian Weibull method described below shows how difficult it can be to do this calculation. If the prior distribution of $\lambda$ is the two-parameter Weibull distribution with probability density function (6:300)

$$
\begin{equation*}
g(\lambda ; \alpha, \beta)=\left(\frac{\beta}{a}\right)\left(\frac{\lambda}{a}\right)^{\beta-1} \exp \left(-\left(\frac{\lambda}{a}\right)^{\beta}\right) \quad \lambda, \alpha, \beta>0 \tag{23}
\end{equation*}
$$

where $\alpha$ is the scale parameter and $\beta$ is the shape parameter.
For the Weibull prior distribution, the resulting posterior probability density function (6:300) is given as

$$
\begin{equation*}
g(\lambda \mid f ; \alpha, \beta)=\left(\frac{\lambda^{f+\beta-1} e^{-\lambda T-(\lambda / a)^{\beta}}}{\int_{0}^{\infty} \lambda^{f+\beta-1} e^{-\lambda T-(\lambda / a)^{\beta}} d \lambda}\right) \quad \lambda>0 \tag{24}
\end{equation*}
$$

where $f$ is the number of failures and $T$ is total test time.
For the Weibull prior distribution, the resulting posterior mean $(6: 300)$ is given as

$$
\begin{equation*}
\hat{\lambda}=E(\lambda \mid f ; \alpha, \beta)=\left(\frac{\int_{0}^{\infty} \lambda^{f+\beta} e^{-\lambda T-(\lambda / a)^{\beta}} d \lambda}{\int_{0}^{\infty} \lambda^{f+\beta-1} e^{-\lambda T-(\lambda / a)^{\beta}} d \lambda}\right) \quad \lambda>0 . \tag{25}
\end{equation*}
$$

Both equations given above must be numerically evaluated. Due to the difficulty associated with numerical evaluation, the Weibull prior will not be used in this thesis.

Reliability Analysis of a Series System.
Consider a system composed of $k$ independent components in series configuration. The time to failure of each component is assumed to be exponentially distributed. Let $\lambda_{1}, \lambda_{2}, \ldots, \lambda_{k}$ be the respective constant failure rates of each component. The failure rate for the system is (10:761)

$$
\begin{equation*}
\lambda=\sum_{i=1}^{k} \lambda_{i} \tag{26}
\end{equation*}
$$

This shows that for a system composed of $k$ independent exponentially distributed components in series configuration, the distribution of the failure time of the system is also exponential with failure rate $\lambda$.

The Bayesian Method 1 (10:761-763).
Bayesian Prior Analysis. Assuming that the prior belief about the failure rates $\lambda_{i}(i=1,2, \ldots, k)$ is exponentially distributed with parameter $\theta$. Then the prior belief about $\lambda=\sum_{i=1}^{k} \lambda_{i}$ is defined by a gamma distribution with probability density function (10:761)

$$
\begin{equation*}
g(\lambda)=\left(\frac{\theta^{k} \lambda^{k-1} e^{-\theta \lambda}}{\Gamma(k)}\right) \quad \lambda, \theta, k>0 . \tag{27}
\end{equation*}
$$

The mean and the variance for the failure rate of the system are $E(\lambda)=k / \theta$ and $V(\lambda)=k / \theta^{2}$.

Bayesian Posterior Analysis. For a system with failure time being exponentially distributed with failure rate $\lambda$, then for the accumulated test time $T$, the number of system failures $f$ is Poisson distributed with pdf (10:761)

$$
\begin{equation*}
P(f \mid \lambda)=\left(\frac{(T \lambda)^{f} e^{-T \lambda}}{f!}\right) \quad f=0,1,2, \ldots \tag{28}
\end{equation*}
$$

Thus the posterior probability density function for $\lambda$ given $f$ failures over a time interval ( $0, T$ ) with respect to a gamma prior given above is (10:761-762)

$$
\begin{equation*}
P(\lambda \mid f)=\left(\frac{(T+\theta)^{f+k} e^{-(T+\theta) \lambda} \lambda^{f+k-1}}{\Gamma(f+k)}\right) \quad \lambda,(T+\theta),(f+k)>0 \tag{29}
\end{equation*}
$$

which is also a gamma with parameters $(T+\theta)$ and $(f+k)$. The Bayesian estimator of $\lambda$ given $f$ failure in $T$ hours of testing is (10:762)

$$
\begin{equation*}
\hat{\lambda}=E\left(\lambda|f\rangle=\left(\frac{f+k}{T+\theta}\right)\right. \tag{30}
\end{equation*}
$$

For the reliability function $R(t)=\exp (-\lambda t)$, the Bayesian estimator of $R(t)$ for a mission time $t$ given $f$ failures in $T$ hours of testing is (10:762)

$$
\begin{equation*}
\widehat{R}(t)=E[R(t) \mid f]=\left(\frac{1}{1+\left(\frac{t}{T+\theta}\right)}\right)^{f+k} \tag{31}
\end{equation*}
$$

Using The Exponential Model. This method uses the Exponential Model given above to calculate the classical and Bayesian reliability point estimates, $R_{i}(i=1 \ldots k)$, and
the classical and Bayesian component reliability confidence intervals, $\left(L B_{i}, U B_{i}\right) . ~ L B_{i}$ is the interval lower bound and $U B_{i}$ is the interval upper bound for each component. The next step is to aggregate the appropriate numbers together to obtain the classical and Bayesian system reliability point estimates and the classical and Bayesian system reliability confidence interval, ( $\mathrm{LB}_{s}, \mathrm{UB}_{s}$ ). The system reliability point estimate is

$$
\begin{equation*}
\mathrm{R}_{\mathrm{s}}=\prod_{i=1}^{k} R_{i} \tag{32}
\end{equation*}
$$

The system reliability confidence interval is calculated as

$$
\begin{align*}
& L B_{\mathrm{s}}=\prod_{i=1}^{k} L B_{i}  \tag{33}\\
& \text { and } U B_{\mathrm{s}}=\prod_{i=1}^{k} U B_{i} \tag{34}
\end{align*}
$$

The Exponential Model is also used to calculate the classical and Bayesian reliability point estimates and the classical and Bayesian confidence intervals for the system using component level data aggregated to system level data. This is possible since for a series system with exponential components, the failure rate for the system is also exponential and is the sum of the components' failure rates. Reliability Analysis of a Parallel System.

Consider a system composed of $k$ independent components in parallel configuration. The time to failure of each component is assumed to be exponentially distributed. Let
$\lambda_{i}(i=1 \ldots k)$ be the respective constant failure rate of each component. This method uses the Exponential Model given above to calculate the classical and Bayesian reliability point estimates, $R_{i}(i=1 \quad \ldots k)$, and the classical and Bayesian component reliability confidence intervals, $\left(\mathrm{LB}_{\mathrm{i}}, \mathrm{UB}_{i}\right) . \mathrm{LB}_{\mathrm{i}}$ is the interval lower bound and $\mathrm{UB}_{\mathrm{i}}$ is the interval upper bound for each component. The next step is to aggregate the appropriate numbers together to obtain the classical and Bayesian system reliability point estimates and the classical and Bayesian system reliability confidence intervals, ( $\left.\mathrm{LB}_{s}, \mathrm{UB}_{s}\right)$. The system reliability point estimate is

$$
\begin{equation*}
\mathrm{R}_{\mathrm{s}}=1-\prod_{i=1}^{k}\left(1-R_{i}\right) \tag{35}
\end{equation*}
$$

The system reliability confidence interval is calculated as

$$
\begin{align*}
& L B_{s}=1-\prod_{i=1}^{k}\left(1-L B_{i}\right)  \tag{36}\\
& \text { and } U B_{s}=1-\prod_{i=1}^{k}\left(1-U B_{i}\right) \tag{37}
\end{align*}
$$

For the case of independent and identical components, The Exponential Model is also used to calculate the classical and Bayesian reliability point estimates, $R_{c}$, and the classical and Bayesian confidence intervals, ( $L^{c}, U_{c}$ ) for the component using aggregated component level data. This is possible since the failure rate for each component is the same. The system reliability point estimate is

$$
\begin{equation*}
R_{s}=1-\left(1-R_{c}\right)^{k} . \tag{38}
\end{equation*}
$$

The system reliability confidence interval is calculated as

$$
\begin{align*}
& \mathrm{LB}_{\mathrm{s}}=1-\left(1-L B_{c}\right)^{k}  \tag{39}\\
& \text { and } \mathrm{UB}_{\mathrm{s}}=1-\left(1-\mathrm{UB}_{\mathrm{c}}\right)^{k} \tag{40}
\end{align*}
$$

Reliability Analysis of a Bridge System.
Consider a system composed of 5 independent components given in Figure 1 below. The time to failure of each component is assumed to be exponentially distributed.


Figure 1. Five Components Bridge System.
Let $\lambda_{i}(i=1 \ldots 5)$ be the respective constant failure rate of each component. This method used the Exponential Model given above to calculate the classical and Bayesian reliability point estimates, $\mathrm{R}_{\mathrm{i}}(\mathrm{i}=1$.. 5), and the classical and Bayesian component reliability confidence intervals, $\left(\mathrm{LB}_{\mathrm{i}}, \mathrm{UB}_{\mathrm{i}}\right) . \mathrm{LB}_{\mathrm{i}}$ is the interval lower bound and $\mathrm{UB}_{i}$ is the interval upper bound for each component. The next step is to aggregate the appropriate numbers together to
obtain the classical and Bayesian system reliability point estimates and the classical and Bayesian system reliability confidence interval, ( $\left.\mathrm{LB}_{s}, \mathrm{UB}_{s}\right)$. The system reliability point estimate is (9:422)
$R_{5}=R_{1} R_{4}+R_{2} R_{5}+R_{1} R_{3} R_{5}+R_{2} R_{3} R_{4}-R_{1} R_{2} R_{3} R_{4}-R_{1} R_{2} R_{3} R_{5}-$
$R_{1} R_{2} R_{4} R_{5}-R_{1} R_{3} R_{4} R_{5}-R_{2} R_{3} R_{4} R_{5}+2 R_{1} R_{2} R_{3} R_{4} R_{5}$.
The system reliability confidence interval is calculated as
$\mathrm{LB}_{\mathrm{s}}=\mathrm{LB}_{1} \mathrm{LB}_{4}+\mathrm{LB}_{2} \mathrm{LB}_{5}+\mathrm{LB}_{1} \mathrm{LB}_{3} \mathrm{LB}_{5}+\mathrm{LB}_{2} \mathrm{LB}_{3} \mathrm{LB}_{4}-\mathrm{LB}_{1} \mathrm{LB}_{2} \mathrm{LB}_{3} \mathrm{LB}_{4}$
$-\mathrm{LB}_{1} \mathrm{LB}_{2} \mathrm{LB}_{3} \mathrm{LB}_{5}-\mathrm{LB}_{1} \mathrm{LB}_{2} \mathrm{LB}_{4} \mathrm{LB}_{5}-\mathrm{LB}_{1} \mathrm{LB}_{3} \mathrm{LB}_{4} \mathrm{LB}_{5}-\mathrm{LB}_{2} \mathrm{LB}_{3} \mathrm{LB}_{4} \mathrm{LB}_{5}+$ $2 \mathrm{LB}_{1} \mathrm{LB}_{2} \mathrm{LB}_{3} \mathrm{LB}_{4} \mathrm{LB}_{5}$
and $\mathrm{UB}_{5}=\mathrm{UB}_{1} \mathrm{UB}_{4}+\mathrm{UB}_{2} \mathrm{UB}_{5}+\mathrm{UB}_{1} \mathrm{UB}_{3} \mathrm{UB}_{5}+\mathrm{UB}_{2} \mathrm{UB}_{3} \mathrm{UB}_{4}-$ $\mathrm{UB}_{1} \mathrm{UB}_{2} \mathrm{UB}_{3} \mathrm{UB}_{4}-\mathrm{UB}_{1} \mathrm{UB}_{2} \mathrm{UB}_{3} \mathrm{UB}_{5}-\mathrm{UB}_{1} \mathrm{UB}_{2} \mathrm{UB}_{4} \mathrm{UB}_{5}-\mathrm{UB}_{1} \mathrm{UB}_{3} \mathrm{UB}_{4} \mathrm{UB}_{5}-$ $\mathrm{UB}_{2} \mathrm{UB}_{3} \mathrm{UB}_{4} \mathrm{UB}_{5}+2 \mathrm{UB}_{1} \mathrm{UB}_{2} \mathrm{UB}_{3} \mathrm{UB}_{4} \mathrm{UB}_{5}$.

For the case of independent and identical components, The Exponential Model is also used to calculate the classical and Bayesian reliability point estimates, $R_{c}$, and the classical and Bayesian probability intervals, ( $\mathrm{LB}_{\mathrm{c}}, \mathrm{UB}_{\mathrm{c}}$ ) for the component using aggregated component level data. This is possible since the failure rate for each component is the same. The system reliability point estimate is calculated using Equation 41 above with $R_{c}$ replacing $R_{i}$ (i= 1.. 5). The system reliability confidence interval is calculated using Equations 42 and 43 with $L_{c}$ replacing $L B B i$ ( $i=1 \ldots 5$ ) and $U B_{c}$ replacing $U B_{i}(i=1 \ldots 5)$.

## IV. Results

Overview.
This chapter describes and discusses the results of the calculations using the methodology in Chapter III. Results from a basic binomial case and a basic exponential case are given first. Then results from a series system, a parallel system with independent and identical components, and a parallel system with different independent components are presented. Finally, results from a bridge system with independent and identical components and a bridge system with different independent components are given. The time to failure of each component in each system is assumed to be exponentially distributed. For detailed calculations, see the appropriate appendix. Calculations will be shown in detail the first time presented in the appropriate appendix. Classical and Bayesian point estimates and confidence intervals obtained from each system will be presented and discussed in this chapter.

## The Binomial Model.

Suppose the following data are obtained from a missile test program. For the DT\&E portion of the test, two missiles failed out of 20 missiles launched. For the OT\&E portion of the test, one missile failed out of 12 missiles launched. Assuming the missile system failures may be
modeled with the binomial distribution, point estimates for the probability of success $p$ (which is the reliability of the missile system) and $80 \%$ confidence interval about $p$ will be computed. From the data above, the following results are obtained (for detailed calculation, see Appendix A):

Table 2: Summary of Binomial Results

|  | Classical | Bayesian |
| :---: | :---: | :---: |
| DT\&E |  |  |
| $\widehat{p}$ | $90.00 \%$ |  |
| $80 \%$ Interval | $(75.52 \% \leq p \leq 97.31 \%)$ |  |
| Interval Width | $21.79 \%$ |  |
| OT\&E |  |  |
| $\hat{p}$ | $91.67 \%$ | $90.63 \%$ |
| $80 \%$ Interval | $(71.25 \% \leq p \leq 99.13 \%)$ | $(83.73 \% \leq p \leq 96.39 \%)$ |
| Interval Width | $27.88 \%$ | $12.66 \%$ |

Table 2 shows that the point estimates for the probability of success, $p$, are all very similar. The bounds using classical method are quite large. You are 80\% confident that the true $p$ is between $75.52 \%$ and $97.31 \%$ for DT\&E data and between $71.25 \%$ and $99.13 \%$ for OT\&E data. The strength of Bayesian analysis lies in the posterior analysis as the table shows. Although the estimates of $p$ is very close to the estimates of $p$ using classical method, the Bayesian method yields a much tighter range for the point estimate. The probability is $80 \%$ that the true $p$ is between 83.73\% and 96.39\%. Even though the width of the probability interval is still large, it is a significant improvement
compared to the width of the intervals obtained using classical method.

The Exponential Model.
The following data are obtained from a reliability test program of a selected simple system by AFOTEC (assuming the time to failure of the terminals being tested is exponentially distributed). For the OT\&E portion of the test, five terminals were tested for a period of seven months. The number of operational hours $\left(T_{i}\right)$ and the number of critical failures per terminal $\left(X_{i}\right)$ were recorded and are given in Table 3.

Table 3: OT\&E Data (3:6)

| Terminal $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures |
| :---: | :---: | :---: |
| 1 | 184.3 | 12 |
| 2 | 232.6 | 9 |
| 3 | 172.8 | 9 |
| 4 | 284.4 | 17 |
| 5 | 264.8 | 18 |

For the operational assessment (OA) portion of the test, two terminals were tested. Again the number of operational hours ( $\mathrm{T}_{\mathrm{i}}$ ) and the number of critical failures per terminal $\left(X_{i}\right)$ were recorded and are given in Table 4.

Table 4: OA Data (3:7)

| Terminal $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures |
| :---: | :---: | :---: |
| 1 | 68.5 | 2 |
| 2 | 60.9 | 2 |

The reliability of the system for a mission time $t$ will be estimated and $80 \%$ confidence intervals associated with the estimated system reliability will be computed using the methodology given in Chapter III. Since the time to failure of the terminals being tested is assumed to be exponentially distributed, a gamma prior distribution is assumed. From the data above, the following results are obtained for detailed calculation, see Appendix B):

Table 5: Summary of Exponential Results

|  | Classical | Bayesian |
| :---: | :---: | :---: |
| OT\&E $\widehat{R}(1)$ 80\% Interval Interval Width | $\begin{gathered} 94.45 \% \\ (93.58 \% \leq R \leq 95.29 \%) \\ 1.71 \% \end{gathered}$ |  |
| OA $\widehat{R}(1)$ $80 \%$ Interval Interval Width | $\begin{gathered} 96.96 \% \\ (94.97 \% \leq R \leq 98.66 \%) \\ 3.69 \% \end{gathered}$ | $\begin{gathered} 95.03 \% \\ (93.87 \% \leq R \leq 96.22 \%) \\ 2.35 \% \end{gathered}$ |
| OT\&E $\widehat{R}(1.5)$ $80 \%$ Interval Interval Width | $\begin{gathered} 91.80 \% \\ (90.53 \% \leq R \leq 93.02 \%) \\ 2.49 \% \end{gathered}$ |  |
| ```OA R(1.5) 80% Interval Interval Width``` | $\begin{gathered} 95.47 \% \\ (92.55 \% \leq R \leq 98.00 \%) \\ 5.45 \% \end{gathered}$ | $\begin{gathered} 92.64 \% \\ (90.94 \% \leq R \leq 94.39 \%) \\ 3.45 \% \end{gathered}$ |
| OT\&E $\widehat{R}(2)$ 80\% Interval Interval Width | $\begin{gathered} 89.21 \% \\ (87.58 \% \leq R \leq 90.81 \%) \\ 3.23 \% \end{gathered}$ |  |
|  | $\begin{gathered} 94.01 \% \\ (90.19 \% \leq R \leq 97.34 \%) \\ 7.15 \% \end{gathered}$ | $\begin{gathered} 90.32 \% \\ (88.11 \% \leq R \leq 92.59 \%) \\ 4.48 \% \end{gathered}$ |
| OT\&E $\widehat{R}(2.5)$ 80\% Interval Interval Width | $\begin{gathered} 86.70 \% \\ (84.72 \% \leq R \leq 88.65 \%) \\ 3.93 \% \end{gathered}$ |  |
| $\begin{gathered} \text { OA } \\ \widehat{R}(2.5) \\ \text { 80\% Interval } \\ \text { Interval Width } \end{gathered}$ | $\begin{gathered} 92.56 \% \\ (87.89 \% \leq R \leq 96.68 \%) \\ 8.79 \% \end{gathered}$ | $\begin{gathered} 88.05 \% \\ (85.37 \% \leq R \leq 90.82 \%) \\ 5.45 \% \end{gathered}$ |
| OT\&E $\widehat{R}(3.5)$ $80 \%$ Interval Interval Width | $\begin{gathered} 81.89 \% \\ (79.29 \% \leq R \leq 84.47 \%) \\ 5.18 \% \end{gathered}$ |  |
| OA $\widehat{R}(3.5)$ <br> 80\% Interval <br> Interval Width | $\begin{gathered} 89.75 \% \\ (83.47 \% \leq R \leq 95.39 \%) \\ 11.92 \% \end{gathered}$ | $\begin{gathered} 83.69 \% \\ (80.13 \% \leq R \leq 87.39 \%) \\ 7.26 \% \end{gathered}$ |

Figure 2: Classical and Bayesian Reliability Estimates


Figure 3: Comparison of OA Interval Widths


Figure 2 shows that the $O A$ reliability estimates using the Bayesian method are lower (more conservative) than the OA classical estimates (which consider only the 4 failures in 129.4 hours) for the six different values of $t$.

Figure 3 shows that the strength of Bayesian analysis lies in the posterior analysis. In all six cases, the Bayesian method yields a tighter range for the point estimate. The difference between the $O A$ Bayesian probability interval width and $O A$ classical confidence interval width ranges from $1.34 \%$ to $4.66 \%$ for the mission times being considered. As the mission time increases, the widths of the confidence interval and the probability interval both increase and the gaps between the two intervals get larger.

Reliability Analysis of a Series System.
Consider a system composed of $k=3$ independent components in series configuration. The time to failure of each component is assumed to be exponentially distributed. Let $\lambda_{1}=0.05$ failure per hour, $\lambda_{2}=0.067$ failure per hour, and $\lambda_{3}=0.05$ failure per hour be the respective constant failure rates of each component. The failure rate for the system is

$$
\lambda=\sum_{i=1}^{3} \lambda_{i}=0.05+0.067+0.05=0.167 \text { failure per hour. }
$$

Thus the mean failure time for the system is
$E(\lambda)=\left(\frac{1}{\lambda}\right)=\left(\frac{1}{0.167}\right)=6$ hours.
For the true system, using a mission time, $t$ of one hour, the reliability of components 1,2 , and 3 are
$R_{1}=R_{3}=\exp (-0.05)=95.12 \%$
$R_{2}=\exp (-0.067)=93.52 \%$.
The reliability of the system can be calculated as
$R_{s}=R_{1} \times R_{2} \times R_{3}=95.12 \% \times 93.52 \% \times 95.12 \%=84.62 \%$
or $\mathrm{R}_{\mathrm{s}}=\exp (-\lambda t)=\exp (-0.167)=84.62 \%$.

Using a computer program called RAPTOR (Rapid Availability Prototyping for Testing Operational Readiness), which is developed by AFOTEC, to simulate the true system, the following data are obtained (to review the simulated data, see Appendix C):

Table 6: System Level DT Data

| Run $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures |
| :---: | :---: | :---: |
| 1 | 499.86 | 80 |
| 2 | 449.53 | 78 |
| 3 | 384.76 | 46 |
| 4 | 543.47 | 97 |
| 5 | 591.88 | 75 |

Table 7: System Level OT Data

| Run i | $\mathrm{T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures |
| :---: | :---: | :---: |
| 1 | 87.86 | 13 |
| 2 | 122.92 | 27 |

Table 8: Component Level DT Data

| Run i | $\mathrm{T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures <br> Component 1 | $\mathrm{X}_{\mathrm{i}}$ Failures <br> Component 2 | $\mathrm{X}_{\mathrm{i}}$ Failures <br> Component 3 |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 499.86 | 24 | 28 | 28 |
| 2 | 449.53 | 20 | 37 | 21 |
| 3 | 384.76 | 13 | 20 | 13 |
| 4 | 543.47 | 29 | 39 | 29 |
| 5 | 591.88 | 21 | 33 | 21 |

Table 9: Component Level OT Data

| Run $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures <br> Component 1 | $\mathrm{X}_{\mathrm{i}}$ Failures <br> Component 2 | $\mathrm{X}_{\mathrm{i}}$ Failures <br> Component 3 |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 87.86 | 4 | 5 | 4 |
| 2 | 122.92 | 9 | 10 | 8 |

The reliability of the system for a mission time $t$ will be estimated and $80 \%$ confidence intervals associated with the estimated system reliability will be computed using the methodology given in Chapter III. From the data above, the following results are obtained (for detailed calculation, see Appendix D):

Table 10: System Reliability Using System Level Data

|  | Classical Method | Bayesian Method 1 | Bayesian Method |
| :---: | :---: | :---: | :---: |
| DTEE R(I) $80 \% \mathrm{CI} / \mathrm{PI}$ Width | $\begin{gathered} 85.88 \% \\ (85.01 \%, 86.74 \%) \\ 1.73 \% \end{gathered}$ |  |  |
| OT\&E R(1) $80 \% \mathrm{CI} / \mathrm{PI}$ Width | $\begin{gathered} 82.72 \% \\ (79.53 \%, 85.86 \%) \\ 6.33 \% \\ \hline \end{gathered}$ | $\begin{gathered} 81.62 \% \\ (85.53 \%) \end{gathered}$ | $\begin{gathered} 84.31 \% \\ (82.10 \%, 86.46 \%) \\ 4.36 \% \\ \hline \end{gathered}$ |
| DT\&E R(1.5) $80 \% \mathrm{CI} / \mathrm{PI}$ Width | $\begin{gathered} 79.58 \% \\ (78.38 \%, 80.78 \%) \\ 2.40 \% \end{gathered}$ |  |  |
| OTGE R(1.5) $80 \% \mathrm{CI} / \mathrm{PI}$ Width | $\begin{gathered} 75.23 \% \\ (70.92 \%, 79.56 \%) \\ 6.33 \% \end{gathered}$ | $\begin{gathered} 73.77 \% \\ (79.11 \%) \end{gathered}$ | $\begin{gathered} 77.43 \% \\ (74.40 \%, 80.39 \%) \\ 5.99 \% \\ \hline \end{gathered}$ |
| DT\&E R(2) $80 \% \mathrm{CI} / \mathrm{PI}$ Width | $\begin{gathered} 73.75 \% \\ (72.27 \%, 75.23 \%) \\ 2.96 \% \\ \hline \end{gathered}$ |  |  |
| ```OT&E R(2) 80% CI/PI Width``` | $\begin{gathered} 68.42 \% \\ (63.24 \%, 73.72 \%) \\ 10.48 \% \end{gathered}$ | $\begin{gathered} 66.69 \% \\ (73.16 \%) \end{gathered}$ | $\begin{gathered} 71.11 \% \\ (67.41 \%, 74.75 \%) \\ 7.34 \% \end{gathered}$ |
| DT\&E R(2.5) $80 \% \mathrm{CI} / \mathrm{PI}$ Width | $\begin{gathered} 68.34 \% \\ (66.63 \%, 70.07 \%) \\ 3.44 \% \\ \hline \end{gathered}$ |  |  |
| OT\&E R(2.5) $80 \% \mathrm{CI} / \mathrm{PI}$ Width | $\begin{gathered} 62.22 \% \\ (56.40 \%, 68.30 \%) \end{gathered}$ | $\begin{gathered} 60.30 \% \\ (67.67 \%) \end{gathered}$ | $\begin{gathered} 65.32 \% \\ (61.08 \%, 69.51 \%) \\ 8.43 \% \end{gathered}$ |
| DTGE R(3) $80 \% \mathrm{CI} / \mathrm{PI}$ Width | $\begin{gathered} 63.33 \% \\ (61.43 \%, 65.26 \%) \\ 3.83 \% \\ \hline \end{gathered}$ |  |  |
| OT\&E R(3) $80 \% \mathrm{CI} / \mathrm{PI}$ Width | $\begin{gathered} 56.59 \% \\ (50.29 \%, 63.29 \%) \\ 13 \% \end{gathered}$ | $\begin{gathered} 54.54 \% \\ (62.59 \%) \end{gathered}$ | $\begin{gathered} 60.01 \% \\ (55.35 \%, 64.63 \%) \\ 9.28 \% \end{gathered}$ |

* The Value in () in Bayesian1 collumn is combined DT \& OT.

Table 11: System Reliability Using Component Level Data

|  | $\begin{gathered} \text { Classical } \\ \text { Method } \\ \hline \end{gathered}$ | Bayesian Method | True R |
| :---: | :---: | :---: | :---: |
| DT\&E $\mathrm{R}(I)$ $80 \% \mathrm{CI} / \mathrm{PI}$ Width | $\begin{gathered} 85.88 \% \\ (84 \cdot 37 \%, 87.35 \%) \\ 2.98 \% \end{gathered}$ |  | 84.62\% |
| OT\&E R(1) $80 \% \mathrm{CI} / \mathrm{PI}$ Width | $\begin{gathered} 82.72 \% \\ (77.21 \%, 88.07 \%) \\ 10.86 \% \\ \hline \end{gathered}$ | $\begin{gathered} 84.98 \% \\ (82.15 \%, 87.94 \%) \\ 5.79 \% \end{gathered}$ | 84.62\% |
| DT\&E R(1.5) $80 \% \mathrm{CI} / \mathrm{PI}$ Width | $\begin{gathered} 79.58 \% \\ (77.51 \%, 81.64 \%) \\ 4.13 \% \\ \hline \end{gathered}$ |  | 77.84\% |
| OT\&E R(I.5) $808 \mathrm{CI} / \mathrm{PI}$ Width | $\begin{gathered} 75.23 \% \\ (67.85 \%, 82.65 \%) \\ 14.8 \% \end{gathered}$ | $\begin{gathered} 78.35 \% \\ (74.47 \%, 82.47 \%) \\ 8 \% \\ \hline \end{gathered}$ | 77.84\% |
| DT\&E R(2) $80 \% \mathrm{CI} / \mathrm{PI}$ Width | $\begin{gathered} 73.75 \% \\ (71.21 \%, 76.31 \%) \\ 5.1 \% \\ \hline \end{gathered}$ |  | 71.61\% |
| ```OT&E R(2) 80% CI/PI Width``` | $\begin{gathered} 68.42 \% \\ (59.63 \%, 77.56 \%) \\ 17.93 \% \end{gathered}$ | $\begin{gathered} 72.24 \% \\ (67.50 \%, 77.35 \%) \\ 9.85 \% \end{gathered}$ | 71.61\% |
| DTEE R(2.5) $80 \% \mathrm{CI} / \mathrm{PI}$ Width | $\begin{gathered} 68.34 \% \\ (65.40 \%, 71.32 \%) \\ 5.92 \% \\ \hline \end{gathered}$ |  | 65.87\% |
| OT\&E R(2.5) $80 \% \mathrm{CI} / \mathrm{PI}$ Width | $\begin{gathered} 62.22 \% \\ (52.39 \%, 72.79 \%) \\ 20.4 \% \end{gathered}$ | $\begin{gathered} 66.61 \% \\ (61.17 \%, 72.54 \%) \\ 11.37 \% \end{gathered}$ | 65.87\% |
| DTGE R(3) $80 \% \mathrm{CI} / \mathrm{PI}$ Width | $\begin{gathered} 63.34 \% \\ (60.08 \%, 66.66 \%) \\ 6.58 \% \end{gathered}$ |  | 60.59\% |
| OTGE R(3) $80 \% \mathrm{CI} / \mathrm{PI}$ Width | $\begin{gathered} 56.60 \% \\ (46.03 \%, 68.31 \%) \\ 22.28 \% \end{gathered}$ | $\begin{gathered} 61.42 \% \\ (55.45 \%, 68.02 \%) \\ 12.57 \% \end{gathered}$ | 60.59\% |

Figure 4: OT\&E Reliability using Bayesian Method 1

## OT\&E Reliability Using Bayesian Method 1



Figure 4 shows that using Bayesian method 1 (Bayesian method 1 only gives a reliability estimate), the reliability estimates using only OT\&E data are lower than the true reliability. The gaps between the true reliability and the OT\&E reliability estimates for the mission times being considered range from 3.01\% to 6.01\%. Since the true reliability of the system is known, you would want the reliability estimates of the system to be as close to the true reliability as possible. The results obtained above using only OT\&E data are not very good.

The reliability estimates using combined OT\&E and DT\&E data are higher than the true reliability. The gaps between the true reliability and the reliability estimates for the mission times being considered range from $0.91 \%$ to $2 \%$. The deviations from the true reliability are still significant.

However, the results are much better than just using OT\&E data. The rest of the the results below used the methodology for the exponential model given in Chapter III.

Figure 5: Classical \& Bayesian Reliability Estimates


Figure 5 shows that the DT\&E classical reliability estimates are higher than the true reliability. The deviations range from $1.26 \%$ to $2.74 \%$ for the mission times being considered. The deviations are considered to be significant. The OT\&E reliability estimates using the Bayesian method are higher than the OT\&E classical estimates and closer to the true reliability for the five different values of $t$ at both the system level and component level. The OT\&E reliability estimates using the classical method are lower than the true reliability. The deviations range
from 1.9\% to $4 \%$ for the mission times being considered. Again, the deviations are considered to be significant.

The OT\&E reliability estimates using the Bayesian method are all very close (less than 1\%) to the true reliability. The OT\&E reliability estimates using system level data underestimated the true reliability with deviations ranging from $0.31 \%$ to 0.58 for the mission times being considered. Using component level data, the OT\&E reliability estimates overestimated the true reliability with deviations ranging from $0.36 \%$ to $0.83 \%$ for the mission times being considered.

Figure 6: Comparison of OT\&E Interval Widths (System Level)


Figure 7: Comparison of OT\&E Interval Widths (Component Level)


Figures 6 and 7 show the strength of Bayesian analysis lies in the posterior analysis. In all five cases, the Bayesian method yields much tighter ranges for the point estimate at both the system and component level. At the system level, the difference between the OT\&E Bayesian probability interval width and OT\&E classical confidence interval width ranges from $1.97 \%$ to $3.72 \%$ for the mission times being considered. At the component level, the difference ranges from 5.07\% to 9.71\%. System level reliability estimates yield tighter intervals than component level aggregated to system. For the mission times being considered, the difference ranges from $4.53 \%$ to $9.28 \%$ for OT\&E classical confidence interval widths and from 1.43\% to $3.29 \%$ for OT\&E Bayesian probability interval widths.

Reliability Analysis of a Parallel System with Independent and Identical Components.

Consider a system composed of 3 independent and identical components arranged in a parallel configuration. The time to failure of each component is assumed to be exponentially distributed. Let $\lambda=0.05$ failure per hour be the constant failure rate of each component. For the true system, using a mission time, $t$ of one hour, the reliability of components 1,2 , and 3 are

$$
R_{c}=R_{1}=R_{2}=R_{3}=\exp (-0.05)=95.12298 .
$$

The reliability of the system can be calculated as

$$
R_{s}=1-\left(1-R_{c}\right)^{3}=1-(1-95.12 \%)^{3}=99.9884 \% .
$$

Using a computer program called RAPTOR, which is developed by AFOTEC, to simulate the true system, the following data are obtained (to review the simulated data, see Appendix E):

Table 12: Aggregated Component Level DT Data

| Run $i$ | $T_{i}$ Hours | $X_{i}$ Failures |
| :---: | :---: | :---: |
| 1 | $1,493.82$ | 79 |
| 2 | $1,463.13$ | 75 |
| 3 | $1,492.59$ | 66 |
| 4 | $1,490.85$ | 70 |
| 5 | $1,490.58$ | 81 |

Table 13: Aggregated Component Level OT Data

| Run $i$ | $T_{i}$ Hours | $X_{i}$ Failures |
| :---: | :---: | :---: |
| 1 | 373.26 | 22 |
| 2 | 346.62 | 15 |

Table 14: Component Level DT Data

| Run i | $\mathrm{T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures <br> Component 1 | $\mathrm{X}_{\mathrm{i}}$ Failures <br> Component 2 | $\mathrm{X}_{\mathrm{i}}$ Failures <br> Component 3 |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 497.94 | 24 | 35 | 20 |
| 2 | 487.71 | 26 | 30 | 19 |
| 3 | 497.53 | 22 | 21 | 23 |
| 4 | 496.95 | 20 | 19 | 31 |
| 5 | 496.86 | 23 | 28 | 30 |

Table 15: Component Level OT Data

| Run $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $X_{i}$ Failures <br> Component 1 | $X_{i}$ Failures <br> Component 2 | $X_{i}$ Failures <br> Component 3 |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 124.42 | 7 | 8 | 7 |
| 2 | 115.54 | 3 | 6 | 6 |

The reliability of the system for a mission time $t$ will be estimated and $80 \%$ confidence intervals associated with the estimated system reliability will be computed using the methodology given in Chapter III. From the data above, the following results are obtained (for detailed calculation, see Appendix F):

Table 16: System Reliability Using Aggregated Data

|  | Classical Method | Bayesian Method | True R |
| :---: | :---: | :---: | :---: |
|  | $\begin{gathered} 99.989 \% \\ (99.986 \%, 99.991 \%) \\ 0.005 \% \end{gathered}$ |  | 99.988\% |
|  | $\begin{gathered} 99.987 \% \\ (99.978 \%, 99.994 \%) \\ 0.016 \% \end{gathered}$ | $\begin{gathered} 99.988 \% \\ (99.985 \%, 99.991 \%) \\ 0.006 \% \end{gathered}$ | 99.988\% |
| $\begin{gathered} \text { DT R(5) } \\ 80 \% \mathrm{CI} / \mathrm{PI} \\ \text { Width } \\ \hline \end{gathered}$ | $\begin{gathered} 98.922 \% \\ (98.720 \%, 99.100 \%) \\ 0.38 \% \end{gathered}$ |  | 98.918\% |
| OT R(5) $80 \% \mathrm{CI} / \mathrm{PI}$ Width | $\begin{gathered} 98.837 \% \\ (98.069 \%, 99.367 \%) \\ 1.298 \% \end{gathered}$ | $\begin{gathered} 98.906 \% \\ (98.604 \%, 99.161 \%) \\ 0.557 \% \end{gathered}$ | 98.918\% |
| $\begin{gathered} \text { DT R(10) } \\ 80 \% \mathrm{CI} / \mathrm{PI} \\ \text { Width } \\ \hline \end{gathered}$ | $\begin{gathered} 93.930 \% \\ (92.956 \%, 94.823 \%) \\ 1.867 \% \end{gathered}$ |  | 93.910\% |
| $\begin{gathered} \text { OT } \mathrm{R}(10) \\ 80 \% \mathrm{CI} / \mathrm{PI} \\ \text { Width } \end{gathered}$ | $\begin{gathered} 93.508 \% \\ (89.972 \%, 96.217 \%) \\ 6.245 \% \end{gathered}$ | $\begin{gathered} 93.865 \% \\ (92.394 \%, 95.133 \%) \\ 2.739 \% \end{gathered}$ | 93.910\% |
| $\begin{gathered} \text { DT } \mathrm{R}(15) \\ 80 \% \mathrm{CI} / \mathrm{PI} \\ \text { Width } \\ \hline \end{gathered}$ | $\begin{gathered} 85.355 \% \\ (83.335 \%, 87.259 \%) \\ 3.924 \% \end{gathered}$ |  | 85.314\% |
| $\begin{gathered} \text { OT R(15) } \\ \text { 80\% CI/PI } \\ \text { Width } \\ \hline \end{gathered}$ | $\begin{gathered} 84.480 \% \\ (77.491 \%, 90.355 \%) \\ 12.864 \% \end{gathered}$ | $\begin{gathered} 85.238 \% \\ (82.202 \%, 87.937 \%) \\ 5.735 \% \end{gathered}$ | 85.314\% |

Table 17: System Reliability Using Component Level Data

|  | Classical Method | Bayesian Method | True R |
| :---: | :---: | :---: | :---: |
| DT R (1) | 99.989\% |  | 99.988\% |
| $80 \% \mathrm{CI} / \mathrm{PI}$ | $\begin{gathered} (99.984 \%, 99.992 \%) \\ 0.008 \% \end{gathered}$ |  |  |
| OT R (1) | 99.988\% | 99.988\% | 99.988\% |
| 80\% CI/PI | (99.969\%,99.997\%) | (99.980\%, 99.994\%) |  |
| Width | 0.028\% | 0.014\% |  |
| DT R (5) | 98.927\% |  | 98.918\% |
| 80\% CI/PI | (98.567\%,99.222\%) |  |  |
| Width | 0.655\% |  |  |
| OT R (5) | 98.871\% | 98.880\% | 98.918\% |
| 80\% CI/PI | (97.412\%,99.641\%) | (98.225\%, 99.369\%) |  |
| Width | 2.229\% | 1.144\% |  |
| DT R (10) | 93.962\% |  | 93.910\% |
| 80\% CI/PI | (92.228\%, 95.452\%) |  |  |
| Width | 3.224\% |  |  |
| OT R (10) | 93.699\% | 93.772\% | 93.910\% |
| 80\% CI/PI | (87.227\%,97.748\%) | (90.690\%, 96.225\%) |  |
| Width | 10.521\% | 5.535\% |  |
| DT R (15) | 85.429\% |  | 85.314\% |
| 80\% CI/PI | (81.881\%, 88.644\%) |  |  |
| Width | 6.763\% |  |  |
| OT R(15) | 84.920\% | 85.129\% | 85.314\% |
| 80\% CI/PI | (72.587\%,93.991\%) | (78.908\%, 90.377\%) |  |
| Width | 21.404\% | 11.469\% |  |

Figure 8: Classical and Bayesian Reliability Estimates


Figure 8 shows that the DT\&E classical reliability estimates slightly overestimate the true reliability. The deviations range from $0.001 \%$ to $0.12 \%$ for the mission times being considered. The deviations are considered to be insignificant. The OT\&E reliability estimates using the classical method underestimated the true reliability. The deviations range from $0 \%$ to $0.83 \%$ for the mission times being considered. The deviations are considered to be not too bad.

The OT\&E reliability estimates using the Bayesian method are all very close (less than $0.2 \%$ ) to the true reliability. The OT\&E reliability estimates using aggregated component level data underestimated the true reliability with deviations ranging from $0 \%$ to $0.08 \%$ for the mission times being considered. Using component level data, the OT\&E reliability estimates also underestimated the true reliability with deviations ranging from $0 \%$ to $0.19 \%$ for the mission times being considered. The OT\&E reliability estimates using the Bayesian method are closer to the true reliability than the classical OT\&E reliability estimates.

Figure 9: Comparison of OT\&E Interval Widths (Aggregated Level)


Figure 10: Comparison of OT\&E Interval Widths (Component Level)


Figures 9 and 10 again show the strength of Bayesian analysis. In all six cases, the Bayesian method yields much tighter ranges for the point estimate at both the aggregated level and component level. At the aggregated component level, the difference between the OT\&E Bayesian probability interval width and OT\&E classical confidence interval width ranges from $0.01 \%$ to $7.13 \%$ for the mission times being considered. At the component level, the difference ranges from 0.01\% to 9.94\%. Aggregated component level reliability estimates yield tighter intervals than component levels aggregated to system. For the mission times being considered, the difference ranges from $0.01 \%$ to $8.54 \%$ for OT\&E classical confidence interval widths and from $0.01 \%$ to 5.73\% for OT\&E Bayesian probability interval widths. Reliability Analysis of a Parallel System with Different Independent Components.

Consider a system composed of 3 different independent components arranged in a parallel configuration. The time to failure of each component is assumed to be exponentially distributed. Let $\lambda_{1}=0.1$ failure per hour, $\lambda_{2}=0.05$ failure per hour, and $\lambda_{3}=0.025$ failure per hour be the respective constant failure rates of each component. For the true system, using a mission time, $t$ of one hour, the reliability of components 1, 2, and 3 are
$R_{1}=\exp (-0.100)=\mathbf{9 0 . 4 8 \%}$
$R_{2}=\exp (-0.050)=95.12 \%$
$R_{3}=\exp (-0.025)=97.53 \%$.
The reliability of the system can be calculated as
$R_{s}=1-\left(1-R_{1}\right)\left(1-R_{2}\right)\left(1-R_{3}\right)$
$=1-(1-0.9048)(1-0.9512)(1-0.9753)=99.9885 \%$.
Using a computer program called RAPTOR, which is developed by AFOTEC, to simulate the true system, the following data are obtained (to review the simulated data, see Appendix G):

Table 18: Component Level DT Data

| Run i | $\mathrm{T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathbf{i}}$ Failures <br> Component 1 | $\mathrm{X}_{\mathbf{i}}$ Failures <br> Component 2 | $\mathrm{X}_{i}$ Failures <br> Component 3 |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 488.03 | 55 | 27 | 10 |
| 2 | 498.15 | 53 | 30 | 8 |
| 3 | 498.39 | 44 | 24 | 12 |
| 4 | 496.55 | 36 | 26 | 9 |
| 5 | 496.36 | 60 | 33 | 9 |

Table 19: Component Level OT Data

| Run i | $\mathrm{T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures <br> Component 1 | $\mathrm{X}_{\mathrm{i}}$ Failures <br> Component 2 | $\mathrm{X}_{1}$ Failures <br> Component 3 |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 122.22 | 13 | 9 | 3 |
| 2 | 113.29 | 8 | 8 | 4 |

The reliability of the system for a mission time $t$ will be estimated and $80 \%$ confidence intervals associated with the estimated system reliability will be computed using the methodology given in Chapter III. From the data above, the following results are obtained (for detailed calculation, see Appendix H):

Table 20: System Reliability Using Component Level Data

|  | Classical Method | Bayesian Method | True R |
| :---: | :---: | :---: | :---: |
| DT R(1) <br> 80\% CI/PI <br> Width <br> 0 R | $\begin{gathered} 99.99 \% \\ (99.986 \%, 99.993 \%) \\ 0.007 \% \end{gathered}$ |  | 99.989\% |
| OT R(1) 80\% CI/PI Width | $\begin{gathered} 99.983 \% \\ (99.957 \%, 99.995 \%) \\ 0.038 \% \end{gathered}$ | $\begin{gathered} 99.989 \% \\ (99.983 \%, 99.994 \%) \\ 0.011 \% \end{gathered}$ | 99.989\% |
| DT R(5) 80\% CI/PI Width | $\begin{gathered} 99.106 \% \\ (98.776 \%, 99.371 \%) \\ 0.595 \% \end{gathered}$ |  | 98.977\% |
|  | $\begin{gathered} 98.495 \% \\ (96.682 \%, 99.503 \%) \\ 2.821 \% \end{gathered}$ | $\begin{gathered} 99.062 \% \\ (98.584 \%, 99.428 \%) \\ 0.844 \% \end{gathered}$ | 98.977\% |
| $\begin{gathered} \text { DT R(10) } \\ 80 \% \mathrm{CI} / \mathrm{PI} \\ \text { Width } \end{gathered}$ | $\begin{gathered} 95.189 \% \\ (93.661 \%, 96.496 \%) \\ 2.835 \% \end{gathered}$ |  | 94.498\% |
| $\begin{gathered} \text { OT R(10) } \\ 80 \% \mathrm{CI} / \mathrm{PI} \\ \text { Width } \end{gathered}$ | $\begin{gathered} 92.202 \% \\ (84.868 \%, 97.087 \%) \\ 12.219 \% \end{gathered}$ | $\begin{gathered} 94.974 \% \\ (92.813 \%, 96.722 \%) \\ 3.909 \% \end{gathered}$ | 94.498\% |
| $\begin{gathered} \text { DT R(15) } \\ 80 \% \mathrm{CI} / \mathrm{PI} \\ \text { Width } \\ \hline \end{gathered}$ | $\begin{gathered} 88.792 \% \\ (85.7 \%, 91.578 \%) \\ 5.878 \% \end{gathered}$ |  | 87.183\% |
| $\begin{gathered} \text { OT R(15) } \\ 80 \% \mathrm{CI} / \mathrm{PI} \\ \text { Width } \end{gathered}$ | $\begin{gathered} 82.457 \% \\ (69.464 \%, 92.678 \%) \\ 23.214 \% \end{gathered}$ | $\begin{gathered} 88.323 \% \\ (84.066 \%, 91.935 \%) \\ 7.869 \% \end{gathered}$ | 87.183\% |

Figure 11 shows that the DT\&E classical reliability estimates overestimated the true reliability. The deviations range from $0.001 \%$ to $1.61 \%$ for the mission times being considered. The deviations are considered to be significant. The OT\&E reliability estimates using the classical method underestimated the true reliability. The deviations range from $0.006 \%$ to $5.87 \%$ for the mission times being considered. The deviations are again considered to be significant.

Using component level data, the OT\&E reliability estimates overestimated the true reliability with deviations ranging from $0 \%$ to $1.14 \%$ for the mission times being considered. While the deviations are still large, the OT\&E reliability estimates using the Bayesian method are much closer to the true reliability than the classical OT\&E reliability estimates.

Figure 11: Classical and Bayesian Reliability Estimates


Figure 12 once again shows the strength of Bayesian analysis. In all six cases, the Bayesian method yields much tighter ranges for the point estimate. The difference between the OT\&E Bayesian probability interval width and OT\&E classical confidence interval width ranges from 0.03\% to $15.35 \%$ for the mission times being considered.

Figure 12: Comparison of OT\&E Interval Widths


Reliability Analysis of a Bridge System with Independent and Identical Components.

Consider a system composed of 5 independent and identical components given in Figure 1 (page 30). The time to failure of each component is assumed to be exponentially distributed. Let $\lambda=0.05$ failure per hour be the constant failure rate of each component. For the true system, using a mission time, $t$ of one hour, the reliability of components 1, 2, 3, 4, and 5 are
$R_{c}=R_{1}=R_{2}=R_{3}=R_{4}=R_{5}=\exp (-0.05)=95.12 \%$.
The reliability of the system can be calculated as
$R_{s}=R_{1} R_{4}+R_{2} R_{5}+R_{1} R_{3} R_{5}+R_{2} R_{3} R_{4}-R_{1} R_{2} R_{3} R_{4}-R_{1} R_{2} R_{3} R_{5}-$
$R_{1} R_{2} R_{4} R_{5}-R_{1} R_{3} R_{4} R_{5}-R_{2} R_{3} R_{4} R_{5}+2 R_{1} R_{2} R_{3} R_{4} R_{5}=99.50 \%$.

Using a computer program called RAPTOR to simulate the true system, the following data are obtained (to review the simulated data, see Appendix I):

Table 21: Aggregated Component Level DT Data

| Run $i$ | $T_{i}$ Hours | $X_{i}$ Failures |
| :---: | :---: | :---: |
| 1 | $2,496.85$ | 136 |
| 2 | $2,486.35$ | 123 |
| 3 | 2461.30 | 124 |
| 4 | 2493.05 | 125 |
| 5 | 2498.40 | 130 |

Table 22: Aggregated Component Level OT Data

| Run $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures |
| :---: | :---: | :---: |
| 1 | 618.85 | 30 |
| 2 | 604.10 | 26 |

Table 23: Component Level DT Data

| Run $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\mathrm{C} 1 \mathrm{X}_{\mathrm{i}}$ | $\mathrm{C} 2 \mathrm{X}_{\mathrm{i}}$ | $\mathrm{C} 3 \mathrm{X}_{\mathrm{i}}$ | $\mathrm{C} 4 \mathrm{X}_{\mathrm{i}}$ | $\mathrm{C} 5 \mathrm{X}_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 499.37 | 32 | 21 | 35 | 25 | 23 |
| 2 | 497.27 | 28 | 17 | 24 | 27 | 27 |
| 3 | 492.26 | 27 | 28 | 25 | 20 | 24 |
| 4 | 498.61 | 26 | 27 | 22 | 23 | 27 |
| 5 | 499.68 | 27 | 23 | 33 | 25 | 22 |

Table 24: Component Level OT Data

| Run $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\mathrm{C} 1 \mathrm{X}_{\mathrm{i}}$ | $\mathrm{C} 2 \mathrm{X}_{\mathrm{i}}$ | $\mathrm{C} 3 \mathrm{X}_{\mathrm{i}}$ | $\mathrm{C} 4 \mathrm{X}_{\mathrm{i}}$ | $\mathrm{C} 5 \mathrm{X}_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 123.77 | 7 | 6 | 8 | 3 | 6 |
| 2 | 120.82 | 6 | 5 | 6 | 4 | 5 |

The reliability of the system for a mission time $t$ will be estimated and $80 \%$ confidence intervals associated with the estimated system reliability will be computed using the methodology given in Chapter III. From the data above, the following results are obtained (for detailed calculation, see Appendix J):

Table 25: System Reliability Using Aggregated Data

|  | Classical Method | Bayesian Method | True R |
| :---: | :---: | :---: | :---: |
| DT R(1) 80\% CI/PI Width | $\begin{gathered} 99.48 \% \\ (99.42 \%, 99.53 \%) \\ 0.11 \% \end{gathered}$ |  | 99.50\% |
| $\begin{gathered} \text { OT R(I) } \\ 80 \% \mathrm{CI} / \mathrm{PI} \\ \text { Width } \end{gathered}$ | $\begin{gathered} 99.58 \% \\ (99.43 \%, 99.71 \%) \\ 0.28 \% \end{gathered}$ | $\begin{gathered} 99.49 \% \\ (99.44 \%, 99.54 \%) \\ 0.1 \% \end{gathered}$ | 99.50\% |
| DT R(4) 80\% CI/PI Width | $\begin{gathered} 92.39 \% \\ (91.67 \%, 93.07 \%) \\ 1.4 \% \end{gathered}$ |  | 92.74\% |
| $\begin{gathered} \text { OT } \mathrm{R}(4) \\ 80 \% \mathrm{CI} / \mathrm{PI} \\ \text { Width } \end{gathered}$ | $\begin{gathered} 93.82 \% \\ (91.70 \%, 95.62 \%) \\ 3.92 \% \end{gathered}$ | $\begin{gathered} 92.52 \% \\ (91.85 \%, 93.16 \%) \\ 1.31 \% \\ \hline \end{gathered}$ | 92.74\% |
| $\begin{gathered} \text { DT } \mathrm{R}(7) \\ 80 \% \mathrm{CI} / \mathrm{PI} \\ \text { Width } \end{gathered}$ | $\begin{gathered} 79.95 \% \\ (78.29 \%, 81.55 \%) \\ 3.26 \% \end{gathered}$ |  | 80.76\% |
| $\begin{gathered} \text { OT } \mathrm{R}(7) \\ 80 \% \mathrm{CI} / \mathrm{PI} \\ \text { Width } \end{gathered}$ | $\begin{gathered} 83.36 \% \\ (78.37 \%, 87.80 \%) \\ 9.43 \% \end{gathered}$ | $\begin{gathered} 80.25 \% \\ (78.70 \%, 81.75 \%) \\ 3.05 \% \end{gathered}$ | 80.76\% |
| $\begin{gathered} \text { DT R(10) } \\ 80 \% \mathrm{CI} / \mathrm{PI} \\ \text { Width } \end{gathered}$ | $\begin{gathered} 65.75 \% \\ (63.35 \%, 68.13 \%) \\ 4.78 \% \end{gathered}$ |  | 66.95\% |
| $\begin{gathered} \text { OT } \mathrm{R}(10) \\ 80 \% \mathrm{CI} / \mathrm{PI} \\ \text { Width } \\ \hline \end{gathered}$ | $\begin{gathered} 70.86 \% \\ (63.47 \%, 77.91 \%) \\ 14.44 \% \end{gathered}$ | $\begin{gathered} 66.21 \% \\ (63.94 \%, 68.43 \%) \\ 4.49 \% \end{gathered}$ | 66.95\% |

Table 26: System Reliability Using Component Level Data

|  | Classical Method | Bayesian Method | True R |
| :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { DT } \mathrm{R}(1) \\ 80 \% \mathrm{CI} / \mathrm{PI} \\ \text { Width } \end{gathered}$ | $\begin{gathered} 99.50 \% \\ (99.38 \%, 99.61 \%) \\ 0.23 \% \end{gathered}$ |  | 99.50\% |
| $\begin{gathered} \text { OT } \mathrm{R}(I) \\ 80 \% \mathrm{CI} / \mathrm{PI} \\ \text { Width } \end{gathered}$ | $\begin{gathered} 99.63 \% \\ (99.24 \%, 99.85 \%) \\ 0.61 \% \end{gathered}$ | $\begin{gathered} 99.52 \% \\ (99.38 \%, 99.65 \%) \\ 0.27 \% \end{gathered}$ | 99.50\% |
| DT $\mathrm{R}(4)$ $80 \% \mathrm{CI} / \mathrm{PI}$ Width | $\begin{gathered} 92.64 \% \\ (91.01 \%, 94.10 \%) \\ 3.09 \% \end{gathered}$ |  | 92.74\% |
| $\begin{gathered} \text { OT } \mathrm{R}(4) \\ 80 \% \mathrm{CI} / \mathrm{PI} \\ \text { Width } \end{gathered}$ | $\begin{gathered} 94 \% \\ (89.18 \%, 97.66 \%) \\ 8.48 \% \end{gathered}$ | $\begin{gathered} 92.87 \% \\ (90.91 \%, 94.67 \%) \\ 3.76 \% \end{gathered}$ | 92.74\% |
|  | $\begin{gathered} 80.48 \% \\ (76.76 \%, 83.98 \%) \\ 7.22 \% \end{gathered}$ |  | 80.76\% |
| OT $\mathrm{R}(7)$ 80\% CI/PI Width | $\begin{gathered} 84.65 \% \\ (72.73 \%, 93.18 \%) \\ 20.45 \% \end{gathered}$ | $\begin{gathered} 81.05 \% \\ (76.50 \%, 85.40 \%) \\ 8.90 \% \end{gathered}$ | 80.76\% |
| $\begin{gathered} \text { DT } \mathrm{R}(10) \\ 80 \% \mathrm{CI} / \mathrm{PI} \\ \text { Width } \end{gathered}$ | $\begin{gathered} 66.52 \% \\ (61.16 \%, 71.79 \%) \\ 10.63 \% \\ \hline \end{gathered}$ |  | 66.95\% |
| $\begin{gathered} \text { OT } \mathrm{R}(10) \\ 80 \% \mathrm{CI} / \mathrm{PI} \\ \text { Width } \end{gathered}$ | $\begin{gathered} 72.81 \% \\ (55.66 \%, 87.02 \%) \\ 31.36 \% \end{gathered}$ | $\begin{gathered} 67.39 \% \\ (60.78 \%, 74.03 \%) \\ 13.25 \% \end{gathered}$ | 66.95\% |

Figure 13: Classical and Bayesian Reliability Estimates



#### Abstract

Figure 13 shows that the DT\&E classical reliability estimates underestimated the true reliability. The deviations range from $0.02 \%$ to $1.2 \%$ for the mission times being considered. The deviations are considered to be significant. The OT\&E reliability estimates using the classical method overestimated the true reliability. The deviations range from $0.08 \%$ to $5.86 \%$ for the mission times being considered. The deviations are again considered to be significant.

The OT\&E reliability estimates using the Bayesian method are all very close (less than 1\%) to the true reliability. The OT\&E reliability estimates using aggregated component level data underestimated the true reliability with deviations ranging from $0.01 \%$ to $0.74 \%$ for the mission times being considered. Using component level data, the OT\&E reliability estimates overestimated the true reliability with deviations ranging from $0.02 \%$ to $0.44 \%$ for the mission times being considered. While the deviations are still significant, the OT\&E reliability estimates using the Bayesian method are much closer to the true reliability than the classical OT\&E reliability estimates.


Figure 14: Comparison of OT\&E Interval Widths (Aggregated Level)


Figure 15: Comparison of OT\&E Interval Widths (Component Level)


Figures 14 and 15 again show the strength of Bayesian analysis. In all seven cases, the Bayesian method yields much tighter ranges for the point estimate at both the aggregated level and component level. At the aggregated component level, the difference between the OT\&E Bayesian probability interval width and OT\&E classical confidence interval width ranges from $0.18 \%$ to $9.95 \%$ for the mission times being considered. At the component level, the difference ranges from 0.34\% to 18.11\%. Aggregated component level reliability estimates yield tighter intervals than component level aggregated to system. For the mission times being considered, the difference ranges from $0.33 \%$ to $16.92 \%$ for OT\&E classical confidence interval widths and from $0.17 \%$ to $8.76 \%$ for OT\&E Bayesian probability interval widths.

Reliability Analysis of a Bridge System with Different Independent Components.

Consider a system composed of 5 independent components given in Figure 1 (page 30). The time to failure of each component is assumed to be exponentially distributed. Let $\lambda_{1}=0.1$ failure per hour, $\lambda_{2}=0.05$ failure per hour, $\lambda_{3}=$ 0.033 failure per hour, $\lambda_{4}=0.025$ failure per hour, and $\lambda_{5}$ $=0.02$ failure per hour be the respective constant failure rates of each component.

For the true system, using a mission time, $t$ of one hour, the reliability of components $1,2,3,4$, and 5 are
$R_{1}=\exp (-0.10)=90.48 \%$
$R_{2}=\exp (-0.05)=95.12 \%$
$R_{3}=\exp (-0.033)=96.75 \%$
$R_{4}=\exp (-0.025)=97.53 \%$
$R_{5}=\exp (-0.20)=98.02 \%$.
The reliability of the system can be calculated as
$R_{s}=R_{1} R_{4}+R_{2} R_{5}+R_{1} R_{3} R_{5}+R_{2} R_{3} R_{4}-R_{1} R_{2} R_{3} R_{4}-R_{1} R_{2} R_{3} R_{5}-$ $R_{1} R_{2} R_{4} R_{5}-R_{1} R_{3} R_{4} R_{5}-R_{2} R_{3} R_{4} R_{5}+2 R_{1} R_{2} R_{3} R_{4} R_{5}=99.48 \%$.

Using a computer program called RAPTOR, which is developed by AFOTEC, to simulate the true system, the following data are obtained (to review the simulated data, see Appendix K):

Table 27: Component Level DT Data

| Run $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\mathrm{C} 1 \mathrm{X}_{\mathrm{i}}$ | $\mathrm{C} 2 \mathrm{X}_{\mathrm{i}}$ | $\mathrm{C} 3 \mathrm{X}_{\mathrm{i}}$ | $\mathrm{C} 4 \mathrm{X}_{\mathrm{i}}$ | $\mathrm{C} 5 \mathrm{X}_{i}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 499.09 | 51 | 19 | 22 | 15 | 13 |
| 2 | 490.55 | 41 | 23 | 21 | 12 | 9 |
| 3 | 497.97 | 44 | 30 | 17 | 6 | 8 |
| 4 | 495.31 | 52 | 26 | 18 | 12 | 10 |
| 5 | 498.76 | 48 | 25 | 22 | 18 | 15 |

Table 28: Component Level OT Data

| Run $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\mathrm{C} 1 \mathrm{X}_{\mathrm{i}}$ | $\mathrm{C} 2 \mathrm{X}_{\mathrm{i}}$ | $\mathrm{C} 3 \mathrm{X}_{\mathrm{i}}$ | $\mathrm{C} 4 \mathrm{X}_{\mathrm{i}}$ | $\mathrm{C} 5 \mathrm{X}_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 124.09 | 11 | 10 | 5 | 1 | 1 |
| 2 | 119.96 | 12 | 3 | 3 | 4 | 1 |

The reliability of the system for a mission time $t$ will be estimated and $80 \%$ confidence intervals associated with the estimated system reliability will be computed using the methodology given in Chapter III. From the data above, the following results are obtained (for detailed calculation, see Appendix L):

Table 29: System Reliability Using Component Level Data

|  | Classical Method | Bayesian Method | True R |
| :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { DT R(1) } \\ 80 \% \mathrm{CI} / \mathrm{PI} \\ \text { Width } \end{gathered}$ | $\begin{gathered} 99.50 \% \\ (99.38 \%, 99.59 \%) \\ 0.21 \% \end{gathered}$ |  | 99.48\% |
| $\begin{gathered} \text { OT R(1) } \\ 80 \% \mathrm{CI} / \mathrm{PI} \\ \text { Width } \end{gathered}$ | $\begin{gathered} 99.51 \% \\ (99.14 \%, 99.76 \%) \\ 0.62 \% \end{gathered}$ | $\begin{gathered} 99.50 \% \\ (99.33 \%, 99.65 \%) \\ 0.32 \% \end{gathered}$ | 99.48\% |
| $\begin{gathered} \text { DT } \mathrm{R}(4) \\ 80 \% \mathrm{CI} / \mathrm{PI} \\ \text { Width } \\ \hline \end{gathered}$ | $\begin{gathered} 93.08 \% \\ (91.64 \%, 94.37 \%) \\ 2.73 \% \end{gathered}$ |  | 92.97\% |
| OT $\mathrm{R}(4)$ $80 \% \mathrm{CI} / \mathrm{PI}$ Width | $\begin{gathered} 93.52 \% \\ (89.08 \%, 96.70 \%) \\ 7.62 \% \end{gathered}$ | $\begin{gathered} 93.24 \% \\ (91.06 \%, 95.12 \%) \\ 4.06 \% \end{gathered}$ | 92.97\% |
| DT R(7) 80\% CI/PI Width | $\begin{gathered} 82.21 \% \\ (78.92 \%, 85.27 \%) \\ 6.35 \% \end{gathered}$ |  | 82.13\% |
| $\begin{gathered} \text { OT } \mathrm{R}(7) \\ 80 \% \mathrm{CI} / \mathrm{PI} \\ \text { Width } \end{gathered}$ | $\begin{gathered} 83.58 \% \\ (73.88 \%, 91.23 \%) \\ 17.35 \% \end{gathered}$ | $\begin{gathered} 82.71 \% \\ (77.73 \%, 87.16 \%) \\ 9.43 \% \end{gathered}$ | 82.13\% |
| $\begin{gathered} \text { DT } \mathrm{R}(10) \\ 80 \% \mathrm{CI} / \mathrm{PI} \\ \text { Width } \\ \hline \end{gathered}$ | $\begin{gathered} 69.82 \% \\ (64.97 \%, 74.52 \%) \\ 9.55 \% \end{gathered}$ |  | $69.86 \%$ |
| $\begin{gathered} \text { OT } \mathrm{R}(10) \\ 80 \% \mathrm{CI} / \mathrm{PI} \\ \text { Width } \\ \hline \end{gathered}$ | $\begin{gathered} 72.29 \% \\ (58.41 \%, 84.44 \%) \\ 26.03 \% \end{gathered}$ | $\begin{gathered} 70.71 \% \\ (63.34 \%, 77.61 \%) \\ 14.27 \% \end{gathered}$ | 69.86\% |

Figure 16: Classical and Bayesian Reliability Estimates


Figure 16 shows that the DT\&E classical reliability estimates are very close to the true reliability. The deviations range from $-0.04 \%$ to $0.11 \%$ for the mission times being considered. The deviations are considered to be insignificant. The OT\&E reliability estimates using the classical method overestimated the true reliability. The deviations range from $0.03 \%$ to $2.43 \%$ for the mission times being considered. The deviations are considered to be significant.

Using component level data, the OT\&E reliability estimates overestimated the true reliability with deviations ranging from $0.02 \%$ to $0.85 \%$ for the mission times being considered. While the deviations are still large, the OT\&E reliability estimates using the Bayesian method are much
closer to the true reliability than the classical OT\&E reliability estimates.

Figure 17: Comparison of OT\&E Interval Widths


Figure 17 once again shows the strength of Bayesian analysis. In all seven cases, the Bayesian method yields much tighter ranges for the point estimate. The difference between the OT\&E Bayesian probability interval width and OT\&E classical confidence interval width ranges from 0.3\% to $11.76 \%$ for the mission times being considered. Summary.

The overall trend from the results obtained in this chapter is that the Bayesian methods used in this research produced much shorter confidence intervals compared to the classical methods. Another trend is that system level data and aggregated component level data yield tighter confidence intervals than component level data aggregated to system.

For the simulated systems considered in this research, the Bayesian reliability point estimates are much closer to the true reliability of the system as compared to the classical reliability estimates.

## v. Conclusions

The results in Chapter IV show that the Bayesian methods used in this research produced much shorter confidence intervals about the reliability point estimates for a variety of systems than the traditional classical methods. This research shows that meaningful results (in the form of shorter confidence intervals) can be obtained by simply applying Bayesian techniques to consecutive test phases.

The binomial model shows that while the OT\&E point estimates are similar (90.63\% vs. 91.67\%), the Bayesian method produced a much tighter confidence interval (12.66\% vs. 27.88\%), thus making it easier for managerial decision-making. The exponential model applied to a real set of data again shows that the Bayesian method produced smaller confidence intervals.

For a series system with exponential components, using simulated data for a 3-component system, the Bayesian method produced tighter confidence intervals. The reliability point estimates using the Bayesian method are closer to the true reliability of the system as compared to the classical reliability point estimates. System level reliability estimates yield much tighter confidence intervals than component level aggregated to system. From the results in

Chapter IV, note that the Bayesian Method 1 only produced the reliability point estimates. Thus this method might not useful for a decision maker.

For a parallel system with independent and identical components, using simulated data for a 3-component system, the Bayesian method again produced tighter confidence intervals. The reliability point estimates using the Bayesian method are again closer to the true reliability of the system as compared to the classical reliability point estimates. Aggregated component level reliability estimates yield much tighter confidence intervals than component level aggregated to system.

For a parallel system with different independent components, using simulated data for a 3-component system, the Bayesian method once again produced tighter confidence intervals. The reliability point estimates using the Bayesian method are again closer to the true reliability of the system as compared to the classical reliability point estimates.

For a bridge system given in Figure 1 (page 30) with independent and identical components, using simulated data, the Bayesian method again produced much tighter confidence intervals. The reliability point estimates using the Bayesian method are closer to the true reliability of the
system as compared to the classical reliability point estimates. Aggregated component level reliability estimates yield a much tighter confidence intervals than component level aggregated to system.

For a bridge system given in Figure 1 (page 30) with different independent components, using simulated data, the Bayesian method once again produced much tighter confidence intervals. The reliability point estimates using the Bayesian method are much closer to the true reliability of the system as compared to the classical reliability point estimates.

In summary, the results of this research show that the Bayesian method produced a much tighter confidence interval as compared to the classical method for OT\&E data. System level data and aggregated component level data will yield a tighter confidence interval than component level data aggregated to system. For multiphase test process commonly implemented by agencies such as AFOTEC, the Bayesian method will work with using all the previous test data as prior information for the current test. However, it is up to the analysts to determine if the previous test data are representative of the current test. Otherwise, you are comparing apples to oranges and the results obtained are meaningless.

## Appendix A: Calculation For The Binomial Model.

The Classical Binomial Method.
Suppose the following data are obtained from a missile program. For the DT\&E portion of the test, two missiles failed out of 20 missiles launched. For the OT\&E portion of the test, one missile failed out of 12 missiles launched. Assuming the data have the binomial distribution, point estimates for the probability of success $P$ and $80 \%$ confidence interval about $p$ will be computed. The point estimate of $p$ for DT\&E and OT\&E are

DT\&E: $\quad \widehat{p}=\left(\frac{18}{20}\right)=90.00 \%$
OT\&E: $\widehat{p}=\left(\frac{11}{12}\right)=91.67 \%$.
The 80\% TCI are
DT\&E: (75.52\%,97.31\%)
Lower bound: $\left(\frac{18}{18+(20-18+1) F_{1-0.2 / 2}(2 \times 20-2 \times 18+2,2 \times 18)}\right)$

$$
=\left(\frac{18}{18+3 F_{0.9}(6,36)}\right)=\left(\frac{18}{18+3 \times 1.95}\right)=0.7552
$$

Upper bound: $\left(\frac{(18+1) F_{1-0.2 / 2}(2 \times 18+2,2 \times 20-2 \times 18)}{(20-18)+(18+1) F_{1-0.2 / 2}(2 \times 18+2,2 \times 20-2 \times 18)}\right)$

$$
=\left(\frac{19 F_{0.9}(38,4)}{2+19 F_{0.9}(38,4)}\right)=\left(\frac{19 \times 3.81}{2+19 \times 3.81}\right)=0.9731
$$

OT\&E: (71.25\%,99.13\%)
Lower bound: $\left(\frac{11}{11+(12-11+1) F_{1-0.2 / 2}(2 \times 12-2 \times 11+2,2 \times 11)}\right)$

$$
=\left(\frac{11}{11+2 F_{0.9}(4,22)}\right)=\left(\frac{11}{11+2 \times 2.22}\right)=0.7125
$$

Upper bound: $\left(\frac{(11+1) F_{1-0.2 / 2}(2 \times 11+2,2 \times 12-2 \times 11)}{(12-11)+(11+1) F_{1-0.2 / 2}(2 \times 11+2,2 \times 12-2 \times 11)}\right)$

$$
=\left(\frac{12 F_{0.9}(24,2)}{1+12 F_{0.9}(24,2)}\right)=\left(\frac{12 \times 9.45}{1+12 \times 9.45}\right)=0.9913
$$

The Bayesian Binomial Method.
There are two failures out of 20 missiles launched during $D T \& E$, thus $x_{0}=18$ and $n_{0}=20$ and the $B(18,20)$ prior distribution is used. There is one failure out of 12 missiles launched during $O T \& E$, thus $x=11$ and $n=12$.

The mean of the posterior distribution is the Bayesian point estimator. Under the squared error loss function, the Bayesian point estimator is

$$
\widehat{p}=E\left(p \mid x ; x_{0}, n_{0}\right)=\left(\frac{x+x_{0}}{n+n_{0}}\right)=\left(\frac{11+18}{12+20}\right)=\left(\frac{29}{32}\right)=90.63 \% .
$$

For the $80 \%$ TBPI, the upper and lower interval endpoints are (83.73\%,96.39\%).

Lower bound:

$$
\begin{aligned}
& \left(\frac{11+18}{11+18+(12+20-11-18) F_{1-0.2 / 2}(2 \times 12+2 \times 20-2 \times 11-2 \times 18,2 \times 11+2 \times 18)}\right) \\
& =\left(\frac{29}{29+3 F_{0.9}(6,58)}\right)=\left(\frac{29}{29+3 \times 1.88}\right)=0.8373
\end{aligned}
$$

Upper bound:

$$
\begin{aligned}
& \left(\frac{(11+18) F_{1-0.2 / 2}(2 \times 11+2 \times 18,2 \times 12+2 \times 20-2 \times 11-2 \times 18)}{12+20-11-18+(11+18) F_{1-0.2 / 2}(2 \times 11+2 \times 18,2 \times 12+2 \times 20-2 \times 11-2 \times 18)}\right) \\
& =\left(\frac{29 F_{0.9}(58,6)}{3+29 F_{0.9}(58,6)}\right)=\left(\frac{29 \times 2.76}{3+29 \times 2.76}\right)=0.9639
\end{aligned}
$$

Appendix B: Calculation For The Exponential Model.
The Classical Exponential Method.
The following data are obtained from a reliability test program.

Table B1: OT\&E Data (3:6)

| Terminal $i$ | $T_{i}$ Hours | $X_{i}$ Failures | $\widehat{\lambda}_{i}=X_{i} / T_{i}$ |
| :---: | :---: | :---: | :---: |
| 1 | 184.3 | 12 | 0.06511 |
| 2 | 232.6 | 9 | 0.03869 |
| 3 | 172.8 | 9 | 0.05208 |
| 4 | 284.4 | 17 | 0.05977 |
| 5 | 264.8 | 18 | 0.06798 |

Table B2: OA Data (3:7)

| Terminal $i$ | $T_{i}$ Hours | $X_{i}$ Failures |
| :---: | :---: | :---: |
| 1 | 68.5 | 2 |
| 2 | 60.9 | 2 |

Assuming the time to failure of the terminals have the exponential distribution, point estimates for the failure rate $\lambda$ and $80 \%$ confidence interval about $\lambda$ will be computed.

$$
\text { OT\&E: } \hat{\lambda}=\left(\frac{f_{1}}{T_{1}}\right)=\left(\frac{65}{1138.9}\right)=0.05707
$$

$\mathrm{OA}: \quad \hat{\lambda}=\left(\frac{f_{2}}{T_{2}}\right)=\left(\frac{4}{129.4}\right)=0.03091$
where $f_{1}=65$ is the number of failures and $T_{1}=1138.9$ is the total test time from Table B 1 and $f_{2}=4$ is the number of failures and $T_{2}=129.4$ is the total test time from Table B2.

The $80 \%$ two-sided confidence intervals (TCI) are OT\&E: $\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 65)}{2 \times 1138.9}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 65)}{2 \times 1138.9}\right)=\left(\frac{\chi_{0.1}^{2}(130)}{2277.8}, \frac{\chi_{0.9}^{2}(130)}{2277.8}\right)$
$=\left(\frac{109.81}{2277.8}, \frac{151.05}{2277.8}\right)=(0.04821,0.06631)$
OA: $\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 4)}{2 \times 129.4}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 4)}{2 \times 129.4}\right)=\left(\frac{\chi_{0.1}^{2}(8)}{258.8}, \frac{\chi_{0.9}^{2}(8)}{258.8}\right)$
$=\left(\frac{3.49}{258.8}, \frac{13.36}{258.8}\right)=(0.01349,0.05163)$
The reliability estimators of $R(t)$ for a mission time $t$ $=1$ hour are

OT\&E: $\widehat{R}(t)=94.45 \%$
$\widehat{R}(t)=\exp (-\hat{\lambda} t)=\exp (-0.05707 \times 1)=0.9445$
$\mathrm{OA}: \widehat{R}(t)=96.96 \%$
$\widehat{R}(t)=\exp (-\hat{\lambda} t)=\exp (-0.03091 \times 1)=0.9696$.
The $80 \%$ two-sided confidence intervals (TCI) are
OT\&E: (93.58\%,95.29\%)
$\exp (-0.06631 \times 1) \leq \widehat{R}(1) \leq \exp (-0.04821 \times 1)$
ㅇA: (94.97\%,98.66\%)
$\exp (-0.05163 \times 1) \leq \widehat{R}(1) \leq \exp (-0.01349 \times 1)$.
The Bayesian Exponential Method.
Bayesian Exponential Prior. OT\&E data are used to obtain a gamma prior. The mean and variance of the gamma distribution are $\mathrm{E}(\boldsymbol{\lambda})=\boldsymbol{\alpha} / \boldsymbol{\beta}$ and $\mathrm{V}(\lambda)=\boldsymbol{\alpha} / \boldsymbol{\beta}^{2} . \mathrm{E}(\lambda)$ and $\mathrm{V}(\lambda)$ can be estimated using the sample mean and variance of $\lambda$ respectively. Thus $\boldsymbol{\alpha}$ and $\boldsymbol{\beta}$ can be computed as $\boldsymbol{\alpha}=$ $E^{2}(\lambda) / V(\lambda)$ and $\beta=E(\lambda) / V(\lambda)$.

From Table B1:
$\widehat{E}(\lambda)=\bar{\lambda}=0.05673$ and $\widehat{V}(\lambda)=s_{\lambda}{ }^{2}=0.00014$.
These yielded the parameter estimates $\alpha=\left(\frac{0.05673^{2}}{0.00014}\right)=23.28$ and $\beta=\left(\frac{0.05673}{0.00014}\right)=405.21$.

Bayesian Exponential Posterior Analysis. The mean of the posterior distribution is the Bayesian point estimator. Under the squared error loss function, the Bayesian point estimator is

$$
\hat{\lambda}=E(\lambda \mid f ; \alpha, \beta)=\left(\frac{f+a}{T+\beta}\right)=\left(\frac{4+23.28}{129.4+405.21}\right)=0.05103 .
$$

The $80 \%$ two-sided probability interval (TBPI) is

$$
\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 4+2 \times 23.28)}{2(129.4+405.21)}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 4+2 \times 23.28)}{2(129.4+405.21)}\right)
$$

$$
=\left(\frac{41.18}{1069.22}, \frac{67.67}{1069.22}\right)=(0.03852,0.06329) .
$$

The Bayesian estimator of $R(t)$ for $t=1$ hour is

$$
\begin{aligned}
\widehat{R}(t)= & \left(\frac{\left(\frac{T}{\beta}\right)+1}{\left(\frac{T}{\beta}\right)+\left(\frac{t}{\beta}\right)+1}\right)^{a+f}= \\
& \left(\frac{\left(\frac{129.4}{405.21}\right)+1}{\left(\frac{129.4}{405.21}\right)+\left(\frac{1}{405.21}\right)+1}\right)^{23.28+4}=95.03 \%
\end{aligned}
$$

The 80\% two-sided probability interval (TBPI) is

$$
\exp (-0.06329 \times 1) \leq \widehat{R}(1) \leq \exp (-0.03852 \times 1)
$$

(93.87\% $\leq \widehat{R}(1) \leq 96.22 \%)$.

## Appendix C. Simulated Data For Series System.

## DT Data Run \#1

| Time | Component Failure | Time | Component Failure |
| :---: | :---: | :---: | :---: |
| 4.06 | C3 | 244.08 | C1 |
| 6.20 | C2 | 245.78 | C3 |
| 12.19 | C2 | 247.35 | C3 |
| 15.64 | C1 | 262.18 | C2 |
| 16.39 | C1 | 278.38 | C1 |
| 22.66 | C2 | 279.89 | C1 |
| 39.58 | C1 | 280.96 | C3 |
| 43.63 | C3 | 282.47 | C2 |
| 44.47 | C3 | 288.81 | C2 |
| 49.98 | C2 | 296.84 | C3 |
| 53.87 | C 2 | 308.01 | C1 |
| 57.15 | C1 | 308.60 | C1 |
| 71.94 | C1 | 310.25 | C2 |
| 72.13 | C1 | 316.96 | C3 |
| 73.51 | C3 | 329.51 | C1 |
| 77.89 | C3 | 333.17 | C2 |
| 82.85 | C2 | 336.92 | C3 |
| 91.34 | C1 | 340.08 | C2 |
| 93.36 | C3 | 343.54 | C1 |
| 101.92 | C3 | 362.98 | C2 |
| 106.49 | C2 | 369.64 | C2 |
| 113.87 | C1 | 373.05 | C2 |
| 114.93 | C2 | 379.03 | C2 |
| 127.01 | C1 | 395.63 | C3 |
| 139.00 | C3 | 396.23 | C3 |
| 141.46 | C2 | 400.42 | C1 |
| 145.83 | C1 | 407.82 | C2 |
| 149.97 | C3 | 411.09 | C2 |
| 151.10 | C2 | 415.78 | C2 |
| 169.35 | C2 | 421.76 | C3 |
| 178.76 | C1 | 426.12 | C1 |
| 197.32 | C3 | 430.44 | C1 |
| 197.58 | C2 | 433.82 | C1 |
| 198.19 | C3 | 444.57 | C3 |
| 199.98 | C3 | 461.05 | C2 |
| 200.04 | C1 | 485.22 | C2 |
| 226.10 | C3 | 495.04 | C3 |
| 227.85 | C2 | 496.78 | C3 |
| 228.57 | C3 | 497.25 | C1 |
| 239.47 | C3 | 499.86 | C3 |

DT Data Run \#2

| Time | Component Failure | Time | Component Failure |
| :---: | :---: | :---: | :---: |
| 12.04 | C3 | 227.72 | C3 |
| 12.07 | C1 | 255.18 | C3 |
| 18.71 | C3 | 255.70 | C2 |
| 24.93 | C2 | 261.48 | C3 |
| 31.60 | C2 | 267.05 | C2 |
| 32.47 | C3 | 274.55 | C1 |
| 32.66 | C3 | 276.86 | C1 |
| 37.16 | C1 | 281.57 | C1 |
| 37.68 | C3 | 281.73 | C2 |
| 41.33 | C3 | 286.19 | C3 |
| 53.45 | C2 | 286.56 | C1 |
| 64.13 | C1 | 296.05 | C3 |
| 73.42 | C1 | 296.35 | C2 |
| 75.56 | C1 | 298.56 | C2 |
| 87.54 | C2 | 301.29 | C3 |
| 87.78 | C2 | 301.38 | C1 |
| 88.24 | C2 | 308.87 | C1 |
| 93.96 | C2 | 313.78 | C2 |
| 97.05 | C2 | 318.71 | C1 |
| 99.47 | C2 | 323.07 | C3 |
| 135.04 | C2 | 323.64 | C3 |
| 139.54 | C2 | 336.32 | C1 |
| 154.84 | C1 | 337.83 | C1 |
| 159.06 | C3 | 351.36 | C1 |
| 161.17 | C2 | 353.18 | C1 |
| 165.41 | C1 | 353.51 | C2 |
| 173.80 | C2 | 363.70 | C3 |
| 183.58 | C2 | 366.73 | C2 |
| 185.59 | C2 | 374.64 | C2 |
| 187.10 | C3 | 376.48 | C2 |
| 189.16 | C2 | 388.35 | C2 |
| 195.88 | C3 | 396.67 | C2 |
| 198.87 | C3 | 397.31 | C1 |
| 199.44 | C2 | 398.38 | C2 |
| 204.14 | C2 | 398.81 | C2 |
| 206.88 | C2 | 403.77 | C2 |
| 207.29 | C2 | 404.07 | C3 |
| 224.62 | C1 | 410.53 | C3 |
| 225.61 | C2 | 449.53 | C2 |

DT Data Run \#3

| Time | Component <br> Failure | Time | Component <br> Failure |
| :---: | :---: | :---: | :---: |
| 12.73 | C 2 | 171.78 | C 1 |
| 16.97 | C 1 | 176.02 | C 3 |
| 21.21 | C 3 | 207.53 | C 2 |
| 51.23 | C 2 | 220.65 | C 1 |
| 55.53 | C 2 | 224.89 | C 3 |
| 68.30 | C 1 | 225.93 | C 2 |
| 72.54 | C 3 | 272.35 | C 2 |
| 73.78 | C 2 | 276.70 | C 1 |
| 74.04 | C 1 | 280.94 | C 3 |
| 78.29 | C 3 | 285.39 | C 2 |
| 98.37 | C 1 | 301.25 | C 1 |
| 101.92 | C 2 | 305.49 | C 3 |
| 102.61 | C 3 | 308.09 | C 2 |
| 103.04 | C 2 | 324.04 | C 2 |
| 119.60 | C 2 | 330.31 | C 2 |
| 128.83 | C 2 | 330.52 | C 2 |
| 135.90 | C 1 | 348.70 | C 2 |
| 137.39 | C 1 | 363.13 | C 1 |
| 140.14 | C 3 | 367.37 | C 3 |
| 141.63 | C 3 | 372.01 | C 2 |
| 159.47 | C 1 | 377.28 | C 2 |
| 163.71 | C 3 | 380.51 | C 1 |
| 165.49 | C 2 | 384.76 | C 3 |

## DT Data Run \#4

| Time | Component <br> Failure | Time | Component <br> Failure | Time | Component <br> Failure |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2.18 | C 2 | 137.72 | C 3 | 334.87 | C 2 |
| 2.39 | C 2 | 142.78 | C 2 | 338.17 | C 2 |
| 2.91 | C 1 | 155.78 | C 1 | 366.00 | C 1 |
| 3.12 | C 3 | 155.98 | C 3 | 366.21 | C 3 |
| 3.18 | C 1 | 187.69 | C 2 | 400.51 | C 2 |
| 3.39 | C 3 | 190.38 | C 1 | 405.11 | C 2 |
| 15.20 | C 2 | 190.58 | C 3 | 406.97 | C 2 |
| 20.27 | C 1 | 201.10 | C 2 | 407.45 | C 2 |
| 20.95 | C 2 | 206.01 | C 2 | 421.23 | C 2 |
| 27.89 | C 2 | 214.66 | C 2 | 432.10 | C 2 |
| 27.93 | C 1 | 224.39 | C 2 | 435.24 | C 2 |
| 28.13 | C 3 | 227.45 | C 2 | 435.88 | C 1 |
| 37.18 | C 1 | 242.22 | C 2 | 436.09 | C 3 |
| 37.39 | C 3 | 248.19 | C 2 | 446.39 | C 2 |
| 38.87 | C 2 | 250.25 | C 1 | 446.49 | C 1 |
| 42.58 | C 2 | 250.45 | C 3 | 446.69 | C 3 |
| 51.82 | C 1 | 268.14 | C 1 | 450.89 | C 1 |
| 52.03 | C 3 | 268.34 | C 3 | 451.09 | C 3 |
| 53.20 | C 2 | 274.50 | C 2 | 461.14 | C 2 |
| 56.77 | C 1 | 274.68 | C 1 | 473.75 | C 2 |
| 56.98 | C 3 | 274.88 | C 3 | 475.42 | C 2 |
| 62.50 | C 2 | 286.21 | C 1 | 517.25 | C 2 |
| 70.94 | C 1 | 286.41 | C 3 | 532.99 | C 2 |
| 71.14 | C 3 | 299.19 | C 1 | 534.02 | C 1 |
| 82.07 | C 2 | 299.39 | C 3 | 534.22 | C 3 |
| 83.33 | C 1 | 303.27 | C 1 | 534.39 | C 2 |
| 83.54 | C 3 | 303.47 | C 3 | 540.14 | C 1 |
| 103.14 | C 2 | 322.96 | C 1 | 540.35 | C 3 |
| 109.42 | C 1 | 323.17 | C 3 | 542.63 | C 1 |
| 109.63 | C 3 | 326.91 | C 2 | 542.83 | C 3 |
| 116.83 | C 2 | 330.92 | C 1 | 543.27 | C 1 |
| 137.52 | C 1 | 331.12 | C 3 | 543.47 | C 3 |

DT Data Run \#5

| Time | Component Failure | Time | Component Failure |
| :---: | :---: | :---: | :---: |
| 2.04 | C2 | 349.24 | C2 |
| 2.72 | C1 | 377.55 | C2 |
| 3.40 | C3 | 379.54 | C1 |
| 7.41 | C2 | 380.22 | C3 |
| 9.88 | C1 | 387.73 | C2 |
| 10.56 | C3 | 396.03 | C1 |
| 27.19 | C2 | 396.71 | C3 |
| 36.25 | C1 | 417.28 | C2 |
| 36.93 | C3 | 434.15 | C1 |
| 133.50 | C2 | 434.83 | C3 |
| 145.89 | C2 | 437.04 | C1 |
| 146.74 | C2 | 437.72 | C3 |
| 148.39 | C2 | 443.40 | C2 |
| 178.00 | C1 | 456.58 | C2 |
| 178.68 | C3 | 457.24 | C1 |
| 188.27 | C2 | 457.92 | C3 |
| 194.52 | C1 | 459.69 | C2 |
| 195.20 | C3 | 465.66 | C1 |
| 195.65 | C1 | 466.34 | C3 |
| 196.33 | C3 | 483.97 | C2 |
| 197.85 | C1 | 499.04 | C2 |
| 198.53 | C3 | 503.40 | C1 |
| 234.22 | C2 | 504.08 | C3 |
| 234.27 | C2 | 509.51 | C2 |
| 243.58 | C2 | 516.97 | C1 |
| 251.03 | C1 | 517.65 | C3 |
| 251.71 | C3 | 521.73 | C2 |
| 284.65 | C2 | 525.92 | C2 |
| 297.02 | C 2 | 551.90 | C2 |
| 312.30 | C1 | 555.80 | C2 |
| 312.37 | C1 | 556.38 | C1 |
| 312.98 | C3 | 557.06 | C3 |
| 313.04 | C3 | 563.60 | C2 |
| 324.77 | C1 | 572.05 | C2 |
| 325.45 | C3 | 590.64 | C2 |
| 325.61 | C2 | 591.20 | C1 |
| 327.78 | C2 | 591.88 | C3 |
| 342.93 | C2 |  |  |

## OT Data Runs \#1 and \#2

| OT Data Run \#1 |  | OT Data Run \#2 |  |
| :---: | :---: | :---: | :---: |
| Time | Component Failure | Time | Component Failure |
| 11.88 | C2 | 27.30 | C2 |
| 15.85 | C1 | 31.95 | C2 |
| 19.81 | C3 | 36.40 | C1 |
| 24.52 | C2 | 41.05 | C3 |
| 30.77 | C2 | 42.60 | C1 |
| 32.69 | C1 | 45.94 | C2 |
| 36.65 | C3 | 47.25 | C3 |
| 40.69 | C2 | 47.72 | C2 |
| 41.03 | C1 | 58.60 | C2 |
| 44.99 | C3 | 61.25 | C1 |
| 54.26 | C1 | 63.62 | C1 |
| 58.22 | C3 | 65.90 | C3 |
| 87.86 | C2 | 68.27 | C3 |
|  |  | 76.87 | C2 |
|  |  | 78.14 | C1 |
|  |  | 82.79 | C3 |
|  |  | 87.02 | C2 |
|  |  | 88.69 | C2 |
|  |  | 92.19 | C2 |
|  |  | 102.49 | C1 |
|  |  | 105.31 | C2 |
|  |  | 107.14 | C3 |
|  |  | 116.03 | C1 |
|  |  | 118.26 | C1 |
|  |  | 120.68 | C3 |
|  |  | 122.91 | C3 |
|  |  | 122.92 | C1 |

Appendix D. Calculation For Series System Reliability.
Consider a system composed of $k=3$ independent components in series configuration. The time to failure of each component is assumed to be exponentially distributed. Let $\lambda_{1}=0.05, \lambda_{2}=0.067$, and $\lambda_{3}=0.05$ be the respective constant failure rates (failure per hour) of each component. The failure rate for the system is

$$
\lambda=\sum_{i=1}^{3} \lambda_{i}=0.05+0.067+0.05=0.167 \text { failure per hour. }
$$

Thus the mean failure for the system is

$$
E(\lambda)=\left(\frac{1}{\lambda}\right)=\left(\frac{1}{0.167}\right)=6 \text { hours. }
$$

For the true system, using a mission time, $t$ of one hour, the reliability of components 1,2 , and 3 are
$R_{1}=R_{3}=\exp (-0.05)=95.12 \%$
$\mathrm{R}_{2}=\exp (-0.067)=93.52 \%$.
The reliability of the system can be calculated as
$R_{s}=R_{1} \times R_{2} \times R_{3}=95.12 \% \times 93.52 \% \times 95.12 \%=84.62 \%$
or $R_{s}=\exp (-\lambda t)=\exp (-0.167)=84.62 \%$.
Using a computer program called RAPTOR, which is developed by AFOTEC, to simulate the true system, the following data are obtained (to review the simulated data, see Appendix C):

Table D1: System Level DT Data

| Run $i$ | $T_{i}$ Hours | $X_{i}$ Failures | $\widehat{\lambda_{i}}=X_{i} / T_{i}$ |
| :---: | :---: | :---: | :---: |
| 1 | 499.86 | 80 | 0.16005 |
| 2 | 449.53 | 78 | 0.17352 |
| 3 | 384.76 | 46 | 0.11956 |
| 4 | 543.47 | 97 | 0.17848 |
| 5 | 591.88 | 75 | 0.12672 |

Table D2: System Level OT Data

| Run $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures | ${\hat{\lambda_{i}}}_{\mathrm{i}}=\mathrm{X}_{\mathrm{i}} / \mathrm{T}_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: |
| 1 | 87.86 | 13 | 0.14796 |
| 2 | 122.92 | 27 | 0.21966 |

Table D3: Component 1 DT Data

| Run $i$ | $T_{i}$ Hours | $X_{i}$ Failures | $\widehat{\lambda_{i}}=X_{i} / T_{i}$ |
| :---: | :---: | :---: | :---: |
| 1 | 499.86 | 24 | 0.04801 |
| 2 | 449.53 | 20 | 0.04449 |
| 3 | 384.76 | 13 | 0.03379 |
| 4 | 543.47 | 29 | 0.05336 |
| 5 | 591.88 | 21 | 0.03548 |

Table D4: Component 1 OT Data

| Run $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures | $\widehat{\lambda_{i}}=\mathrm{X}_{\mathrm{i}} / \mathrm{T}_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: |
| 1 | 87.86 | 4 | 0.04553 |
| 2 | 122.92 | 9 | 0.07322 |

Table D5: Component 2 DT Data

| Run $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\bar{X}_{i}$ Failures | $\overline{\lambda_{i}}=\mathrm{X}_{\mathrm{i}} / \mathrm{T}_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: |
| 1 | 499.86 | 28 | 0.05602 |
| 2 | 449.53 | 37 | 0.08231 |
| 3 | 384.76 | 20 | 0.05198 |
| 4 | 543.47 | 39 | 0.07176 |
| 5 | 591.88 | 33 | 0.05576 |

Table D6: Component 2 OT Data

| Run $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures | $\overline{\lambda_{i}}=\mathrm{X}_{\mathrm{i}} / \mathrm{T}_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: |
| 1 | 87.86 | 5 | 0.05691 |
| 2 | 122.92 | 10 | 0.08135 |

Table D7: Component 3 DT Data

| Run $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures | $\widehat{\lambda_{i}}=\mathrm{X}_{\mathrm{i}} / \mathrm{T}_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: |
| 1 | 499.86 | 28 | 0.05602 |
| 2 | 449.53 | 21 | 0.04672 |
| 3 | 384.76 | 13 | 0.03379 |
| 4 | 543.47 | 29 | 0.05336 |
| 5 | 591.88 | 21 | 0.03548 |

Table D8: Component 3 OT Data

| Run $i$ | $T_{i}$ Hours | $X_{i}$ Failures | $\widehat{\lambda}_{i}=X_{i} / T_{i}$ |
| :---: | :---: | :---: | :---: |
| 1 | 87.86 | 4 | 0.04553 |
| 2 | 122.92 | 8 | 0.06508 |

The Bayesian Method 1.
Bayesian Prior Analysis. Assuming that the prior belief about the failure rates $\lambda_{i}(i=1,2,3)$ is exponentially distributed with parameter $\theta$. Then the prior belief about $\lambda=\sum_{i=1}^{3} \lambda_{i}$ is defined by a gamma distribution with pdf given in Equation 27. The mean of the system is $E(\lambda)=k / \theta$. With $E(\lambda)=6$ from above, solving for $\theta$ to obtain $\theta=\left(\frac{k}{E(\lambda)}\right)=\left(\frac{3}{6}\right)=0.5$.

Bayesian Posterior Analysis.
At the system level OT data, there are 40 failures ( $f_{2}$ $=40$ ) observed during the total test time $T_{2}=210.78$ hours, $k=3$ and $\lambda=0.167$ failure per hour. Thus

$$
\hat{\lambda}=\mathrm{E}(\lambda \mid f)=\left(\frac{f+k}{T+\theta}\right)=\left(\frac{40+3}{210.78+0.5}\right)=0.20352 .
$$

At the system level OT data, there are 40 failures ( $f_{2}$
$=40$ ) observed during the total test time $T_{2}=210.78$ hours, $k=3$ and $\lambda=0.167$ failure per hour. Thus

$$
\widehat{R}(t)=\left(\frac{1}{1+\left(\frac{1}{210.78+0.5}\right)}\right)^{40+3}=0.8162 .
$$

Computations Using The Exponential Model.
The Classical Exponential Method. Assuming the time to failure of each component has the exponential distribution, point estimates for the failure rate $\lambda$ and $80 \%$ confidence intervals about $\lambda$ will be computed.

System Level DT: $\hat{\lambda}=\left(\frac{f_{1}}{T_{1}}\right)=\left(\frac{376}{2469.5}\right)=0.15226$
System Level OT: $\hat{\lambda}=\left(\frac{f_{2}}{T_{2}}\right)=\left(\frac{40}{210.78}\right)=0.18977$
Component $1 \mathrm{DT}: \hat{\lambda}=\left(\frac{f_{3}}{T_{3}}\right)=\left(\frac{107}{2469.5}\right)=0.04333$
Component 1 OT: $\hat{\lambda}=\left(\frac{f_{4}}{T_{4}}\right)=\left(\frac{13}{210.78}\right)=0.06168$
Component 2 DT: $\hat{\lambda}=\left(\frac{f_{5}}{T_{5}}\right)=\left(\frac{157}{2469.5}\right)=0.06358$
Component 2 OT: $\hat{\lambda}=\left(\frac{f_{6}}{T_{6}}\right)=\left(\frac{15}{210.78}\right)=0.07116$
Component $3 \mathrm{DT}: \quad \hat{\lambda}=\left(\frac{f_{7}}{T_{7}}\right)=\left(\frac{112}{2469.5}\right)=0.04535$
Component 3 OT: $\hat{\lambda}=\left(\frac{f_{8}}{T_{8}}\right)=\left(\frac{12}{210.78}\right)=0.05693$
where $f_{1}=376$ is the number of failures and $T_{1}=2469.5$ is the total test time from Table D1 and similarly $f_{2}=40$ and $T_{2}=210.78$ from Table $D 2, f_{3}=107$ and $T_{3}=2469.5$ from Table D3, $f_{4}=13$ and $T_{4}=210.78$ from Table D4, $f_{5}=157$ and $T_{5}=2469.5$ from Table D5, $f_{6}=15$ and $T_{6}=210.78$ from Table D6, $f_{7}=112$ and $T_{7}=2469.5$ from Table $D 7, f_{8}=12$ and $T_{8}=$ 210.78 from Table D8.

The $80 \%$ two-sided confidence intervals (TCI) are
System Level DT: (0.14229,0.16240)
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 376)}{2 \times 2469.5}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 376)}{2 \times 2469.5}\right)=\left(\frac{702.75}{4939}, \frac{802.11}{4939}\right)$
System Level OT: (0.15248,0.22910)
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 40)}{2 \times 210.78}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 40)}{2 \times 210.78}\right)=\left(\frac{64.28}{421.56}, \frac{96.58}{421.56}\right)$
Component $1 \mathrm{DT}:(0.03806,0.04878)$
$-\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 107)}{2 \times 2469.5}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 107)}{2 \times 2469.5}\right)=\left(\frac{187.95}{4939}, \frac{240.9}{4939}\right)$
Component 1 OT: $(0.04102,0.08436)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 13)}{2 \times 210.78}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 13)}{2 \times 210.78}\right)=\left(\frac{17.29}{421.56}, \frac{35.56}{421.56}\right)$
Component $2 \mathrm{DT}:(0.05717,0.07016)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 157)}{2 \times 2469.5}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 157)}{2 \times 2469.5}\right)=\left(\frac{282.34}{4939}, \frac{346.51}{4939}\right)$
Component 2 OT: $(0.04886,0.09549)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 15)}{2 \times 210.78}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 15)}{2 \times 210.78}\right)=\left(\frac{20.6}{421.56}, \frac{40.26}{421.56}\right)$
Component 3 DT: $(0.03996,0.05093)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 112)}{2 \times 2469.5}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 112)}{2 \times 2469.5}\right)=\left(\frac{197.34}{4939}, \frac{251.52}{4939}\right)$
Component 3 OT: $(0.03715,0.07875)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 12)}{2 \times 210.78}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 12)}{2 \times 210.78}\right)=\left(\frac{15.66}{421.56}, \frac{33.2}{421.56}\right)$
The reliability estimators of $R(t)$ for $t=1$ hour are

System Level DT: $\widehat{R}(t)=\exp (-0.15226 \times 1)=\mathbf{8 5 . 8 8 \%}$
System Level OT: $\widehat{R}(t)=\exp (-0.18977 \times 1)=\mathbf{8 2 . 7 2 \%}$
Component $1 \mathrm{DT}: \widehat{R_{1}}(t)=\exp (-0.04333 \times 1)=95.76 \%$
Component 1 OT: $\widehat{R_{1}}(t)=\exp (-0.06168 \times 1)=94.02 \%$
Component $2 \mathrm{DT}: \widehat{R_{2}}(t)=\exp (-0.06358 \times 1)=93.84 \%$
Component 2 OT: $\widehat{R_{2}}(t)=\exp (-0.07116 \times 1)=93.13 \%$
Component $3 \mathrm{DT}: \widehat{R_{3}}(t)=\exp (-0.04535 \times 1)=95.57 \%$
Component 3 OT: $\widehat{R_{3}}(t)=\exp (-0.05693 \times 1)=94.47 \%$
Component Level Aggregated to System DT: $\widehat{R}(t)=\mathbf{8 5 . 8 8 \%}$
$\widehat{R}(t)=R_{1} * R_{2} * R_{3}=0.9576 * 0.9384 * 0.9557=0.8588$
Component Level Agaregated to System $O T: \widehat{R}(t)=\mathbf{8 2 . 7 2 \%}$
$\widehat{R}(t)=\mathrm{R}_{1} * \mathrm{R}_{2} * \mathrm{R}_{3}=0.9402 * 0.9313 * 0.9447=0.8272$.
The 80\% two-sided confidence intervals (TCI) are
System Level DT: (85.01\%,86.74\%)
$\exp (-0.16240 \times 1) \leq \widehat{R}(1) \leq \exp (-0.14229 \times 1)$
System Level OT: (79.53\%,85.86\%)
$\exp (-0.22910 \times 1) \leq \widehat{R}(1) \leq \exp (-0.15248 \times 1)$
Component 1 DT: (95.24\%,96.27\%)
$\exp (-0.04878 \times 1) \leq \widehat{R}(1) \leq \exp (-0.03806 \times 1)$
Component 1 OT: (91.91\%,95.98\%)
$\exp (-0.08436 \times 1) \leq \widehat{R}(1) \leq \exp (-0.04102 \times 1)$
Component 2 DT: ( $93.22 \%, 94.44 \%$ )
$\exp (-0.07016 \times 1) \leq \widehat{R}(1) \leq \exp (-0.05717 \times 1)$
Component 2 OT: (90.89\%,95.23\%)
$\exp (-0.09549 \times 1) \leq \widehat{R}(1) \leq \exp (-0.04886 \times 1)$
Component 3 DT: (95.03\%,96.08\%)
$\exp (-0.05093 \times 1) \leq \widehat{R}(1) \leq \exp (-0.03996 \times 1)$
Component 3 OT: ( $92.43 \%, 96.35 \%$ )
$\exp (-0.07875 \times 1) \leq \widehat{R}(1) \leq \exp (-0.03715 \times 1)$
Component Level Aggregated to System DT:
(84.37\%,87.35\%)

Lower Bound $=0.9524 * 0.9322 * 0.9503=0.8437$
Upper Bound $=0.9627 * 0.9444 * 0.9608=0.8735$
Component Level Agaregated to System OT:
(77.21\%, 88.07\%)

Lower Bound $=0.9191 * 0.9089 * 0.9243=0.7721$
Upper Bound $=0.9598 * 0.9523 * 0.9635=0.8807$.
The Bayesian Exponential Method.
Bayesian Exponential Prior.
For the system level data, from Table D1:
$\widehat{E}(\lambda)=\bar{\lambda}=0.15166$ and $\hat{V}(\lambda)=s_{\lambda}{ }^{2}=0.00073$.

These yielded the parameter estimates
$\alpha=\left(\frac{0.15166^{2}}{0.00073}\right)=31.51$ and $\beta=\left(\frac{0.15166}{0.00073}\right)=207.76$.
For Component 1 data, from Table D3:
$\widehat{E}(\lambda)=\bar{\lambda}=0.04303$ and $\widehat{V}(\lambda)=s_{\lambda}{ }^{2}=0.00007$.
These yielded the parameter estimates
$\alpha=\left(\frac{0.04303^{2}}{0.00007}\right)=26.83$ and $\beta=\left(\frac{0.04303}{0.00007}\right)=623.58$.
For Component 2 data, from Table D5:
$\widehat{E}(\lambda)=\bar{\lambda}=0.06356$ and $\widehat{V}(\lambda)=\mathrm{s}^{2}{ }^{2}=0.00017$.
These yielded the parameter estimates
$\alpha=\left(\frac{0.06356^{2}}{0.00017}\right)=23.76$ and $\beta=\left(\frac{0.06356}{0.00017}\right)=373.88$.
For Component 3 data, from Table D7:
$\widehat{E}(\lambda)=\bar{\lambda}=0.04507$ and $\widehat{V}(\lambda)=s_{\lambda}^{2}=0.0001$.
These yielded the parameter estimates
$\alpha=\left(\frac{0.04507^{2}}{0.0001}\right)=20.31$ and $\beta=\left(\frac{0.04507}{0.0001}\right)=450.7$.
Bayesian Exponential Posterior Analysis.
System Level: $\hat{\lambda}=\left(\frac{40+31.51}{210.78+207.76}\right)=0.17086$.
Component 1: $\quad \hat{\lambda}=\left(\frac{13+26.83}{210.78+623.58}\right)=0.04774$.
Component 2: $\quad \hat{\lambda}=\left(\frac{15+23.76}{210.78+373.88}\right)=0.06630$.
Component 3: $\quad \hat{\lambda}=\left(\frac{12+20.31}{210.78+450.7}\right)=0.04885$.
The $80 \%$ two-sided probability intervals (TBPI) are System Level: $\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 40+2 \times 31.51)}{2(210.78+207.76)}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 40+2 \times 31.51)}{2(210.78+207.76)}\right)$
$=\left(\frac{121.8}{837.08}, \frac{165.06}{837.08}\right)=(0.14551,0.19718)$.

Component 1: $\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 13+2 \times 26.83)}{2(210.78+623.58)}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 13+2 \times 26.83)}{2(210.78+623.58)}\right)$
$=\left(\frac{63.38}{1668.72}, \frac{95.48}{1668.72}\right)=(0.03798,0.05722)$.
Component 2: $\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 15+2 \times 23.76)}{2(210.78+373.88)}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 15+2 \times 23.76)}{2(210.78+373.88)}\right)$
$=\left(\frac{61.59}{1169.32}, \frac{93.27}{1169.32}\right)=(0.05267,0.07976)$.
Component 3: $\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 12+2 \times 20.31)}{2(210.78+450.7)}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 12+2 \times 20.31)}{2(210.78+450.7)}\right)$
$=\left(\frac{50}{1322.96}, \frac{78.86}{1322.96}\right)=(0.03779,0.05961)$.
The Bayesian estimators of $R(t)$ for $t=1$ hour are
System Level: $\widehat{R}(t)=\mathbf{8 4 . 3 1 \%}$

$$
\widehat{R}(t)=\left(\frac{\left(\frac{210.78}{207.76}\right)+1}{\left(\frac{210.78}{207.76}\right)+\left(\frac{1}{207.76}\right)+1}\right)^{31.51+40}
$$

Component 1: $\widehat{R}(t)=95.34 \%$

$$
\widehat{R}(t)=\left(\frac{\left(\frac{210.78}{623.58}\right)+1}{\left(\frac{210.78}{623.58}\right)+\left(\frac{1}{623.58}\right)+1}\right)^{26.83+13}
$$

Component 2: $\widehat{R}(t)=93.59 \%$

$$
\widehat{R}(t)=\left(\frac{\left(\frac{210.78}{373.88}\right)+1}{\left(\frac{210.78}{373.88}\right)+\left(\frac{1}{373.88}\right)+1}\right)^{23.76+15}
$$

Component 3: $\widehat{R}(t)=95.24 \%$

$$
\widehat{R}(t)=\left(\frac{\left(\frac{210.78}{450.7}\right)+1}{\left(\frac{210.78}{450.7}\right)+\left(\frac{1}{450.7}\right)+1}\right)^{20.31+12}
$$

Component Level Agaregated to System: $\widehat{R}(t)=84.98 \%$
$\widehat{R}(t)=0.9534 * 0.9359 * 0.9524=0.8498$
The 80\% two-sided probability intervals (TBPI) are
System Level: $(\mathbf{8 2 . 1 0 \%} \leq \widehat{R}(1) \leq \mathbf{8 6 . 4 6 \%})$
$\exp (-0.19718 \times 1) \leq \widehat{R}(1) \leq \exp (-0.14551 \times 1)$.
Component 1: $(94.44 \% \leq \widehat{R}(1) \leq 96.27 \%)$
$\exp (-0.05722 \times 1) \leq \widehat{R}(1) \leq \exp (-0.03798 \times 1)$.
Component 2: $(92.33 \% \leq \widehat{R}(1) \leq 94.87 \%)$
$\exp (-0.07976 \times 1) \leq \widehat{R}(1) \leq \exp (-0.05267 \times 1)$.
Component 3: $(94.21 \% \leq \widehat{R}(1) \leq 96.29 \%)$
$\exp (-0.05961 \times 1) \leq \widehat{R}(1) \leq \exp (-0.03779 \times 1)$.
Component Level Aggregated to System:
( $82.15 \% \leq \widehat{R}(1) \leq 87.94 \%)$
$0.9444 * 0.9233 * 0.9421 \leq \widehat{R}(1) \leq 0.9627 * 0.9487 * 0.9629$.

Appendix E. Simulated Data For Parallel System With
Independent And Identical Components.

| Time | Component Failure | Time | Component Failure |
| :---: | :---: | :---: | :---: |
| 12.04 | C3 | 282.71 | C2 |
| 12.06 | C1 | 289.01 | C 2 |
| 18.71 | C3 | 291.78 | C3 |
| 32.47 | C3 | 296.17 | C1 |
| 33.23 | C2 | 304.14 | C2 |
| 37.16 | C1 | 306.46 | C2 |
| 37.35 | C1 | 311.16 | C2 |
| 41.36 | C3 | 315.75 | C1 |
| 42.37 | C1 | 316.15 | C2 |
| 46.02 | C1 | 316.49 | C3 |
| 62.38 | C2 | 326.02 | C2 |
| 68.33 | C3 | 331.25 | C2 |
| 77.62 | C3 | 331.31 | C3 |
| 79.76 | C3 | 334.20 | C2 |
| 107.82 | C2 | 335.24 | C1 |
| 108.15 | C2 | 342.72 | C1 |
| 108.76 | C2 | 351.61 | C3 |
| 116.38 | C2 | 352.56 | C1 |
| 120.51 | C2 | 355.99 | C2 |
| 123.73 | C2 | 356.56 | C2 |
| 159.04 | C3 | 370.17 | C1 |
| 163.75 | C1 | 371.68 | C1 |
| 165.04 | C3 | 385.22 | C1 |
| 171.15 | C2 | 387.04 | C1 |
| 175.61 | C3 | 396.62 | C2 |
| 192.46 | C3 | 404.57 | C3 |
| 192.59 | C1 | 414.25 | C2 |
| 199.20 | C2 | 424.79 | C2 |
| 201.88 | C2 | 427.24 | C2 |
| 205.62 | C1 | 431.17 | C1 |
| 206.64 | C2 | 442.25 | C1 |
| 214.41 | C1 | 443.08 | C2 |
| 217.39 | C1 | 444.53 | C1 |
| 220.35 | C2 | 444.94 | C3 |
| 226.62 | C2 | 445.11 | C1 |
| 230.28 | C2 | 451.56 | C3 |
| 230.81 | C2 | 458.01 | C3 |
| 246.24 | C1 | 495.84 | C2 |
| 251.66 | C3 | 497.94 | C3 |
| 255.25 | C2 | 497.94 | C2 |

DT Data Run \#2

| Time | Component Failure | Time | Component Failure |
| :---: | :---: | :---: | :---: |
| 4.20 | C3 | 275.50 | C2 |
| 4.58 | C1 | 281.06 | C1 |
| 6.07 | C2 | 290.49 | C3 |
| 17.53 | C2 | 295.71 | C2 |
| 18.43 | C1 | 304.23 | C1 |
| 34.77 | C3 | 306.66 | C1 |
| 46.48 | C3 | 313.05 | C2 |
| 57.70 | C2 | 336.41 | C2 |
| 62.53 | C3 | 336.81 | C1 |
| 68.69 | C1 | 337.86 | C3 |
| 75.71 | C2 | 344.63 | C1 |
| 90.38 | C3 | 351.90 | C2 |
| 90.50 | C1 | 361.93 | C1 |
| 91.35 | C2 | 363.04 | C1 |
| 93.99 | C3 | 365.05 | C2 |
| 94.21 | C1 | 368.64 | C2 |
| 105.29 | C3 | 389.02 | C3 |
| 107.87 | C1 | 391.29 | C1 |
| 110.82 | C3 | 398.75 | C2 |
| 114.35 | C3 | 403.27 | C2 |
| 135.40 | C2 | 415.59 | C2 |
| 142.04 | C1 | 425.97 | C3 |
| 142.34 | C1 | 427.24 | C1 |
| 153.25 | C1 | 428.28 | C2 |
| 159.69 | C 2 | 429.95 | C1 |
| 161.91 | C1 | 431.16 | C1 |
| 168.85 | C2 | 441.17 | C2 |
| 170.29 | C2 | 449.38 | C2 |
| 177.01 | C3 | 451.03 | C3 |
| 208.26 | C1 | 455.09 | - C 2 |
| 216.50 | C3 | 458.15 | C2 |
| 218.39 | C1 | 459.00 | C2 |
| 224.21 | C2 | 459.80 | C1 |
| 230.03 | C3 | 463.57 | C2 |
| 230.64 | C1 | 464.11 | C1 |
| 248.50 | C2 | 475.82 | C3 |
| 270.19 | C3 | 487.71 | C2 |
| 274.10 | C2 |  |  |

## DT Data Run \#3

| Time | Component Failure | Time | Component Failure |
| :---: | :---: | :---: | :---: |
| 9.08 | C2 | 255.75 | C3 |
| 12.18 | C3 | 259.70 | C1 |
| 26.30 | C1 | 261.80 | C3 |
| 40.09 | C3 | 266.50 | C1 |
| 40.41 | C3 | 288.06 | C2 |
| 61.50 | C2 | 288.64 | C3 |
| 61.75 | C3 | 292.05 | C2 |
| 64.21 | C2 | 294.44 | C3 |
| 69.80 | C3 | 295.71 | C1 |
| 71.06 | C3 | 334.44 | C2 |
| 71.24 | C1 | 334.85 | C2 |
| 74.24 | C2 | 336.79 | C2 |
| 105.08 | C2 | 356.86 | C1 |
| 110.15 | C2 | 357.14 | C1 |
| 110.28 | C3 | 366.86 | C3 |
| 122.39 | C1 | 367.70 | C3 |
| 123.14 | C2 | 371.11 | C1 |
| 134.03 | C3 | 376.81 | C3 |
| 138.38 | C3 | 378.97 | C2 |
| 142.06 | C3 | 380.16 | C1 |
| 168.67 | C1 | 381.50 | C1 |
| 169.65 | C3 | 385.48 | C1 |
| 172.87 | C1 | 389.79 | C1 |
| 179.59 | C2 | 392.03 | C1 |
| 189.06 | C3 | 401.88 | C2 |
| 189.37 | C1 | 436.54 | C2 |
| 192.59 | C2 | 448.39 | C3 |
| 217.46 | C2 | 448.48 | C1 |
| 220.53 | C2 | 460.88 | C1 |
| 221.95 | C2 | 494.32 | C3 |
| 233.27 | C1 | 494.72 | C1 |
| 237.80 | C2 | 495.58 | C3 |
| 251.11 | C3 | 497.53 | C1 |

DT Data Run \#4

| Time | Component Failure | Time | Component Failure |
| :---: | :---: | :---: | :---: |
| 7.12 | C3 | 250.70 | C3 |
| 22.95 | C1 | 256.25 | C1 |
| 36.55 | C1 | 262.69 | C1 |
| 37.98 | C3 | 278.48 | C2 |
| 55.79 | C3 | 280.28 | C3 |
| 59.30 | C2 | 281.44 | C2 |
| 70.99 | C3 | 286.02 | C3 |
| 77.46 | C1 | 291.79 | C3 |
| 96.21 | C2 | 299.82 | C2 |
| 100.76 | C3 | 300.73 | C3 |
| 104.27 | C2 | 302.40 | C3 |
| 105.69 | C1 | 321.65 | C3 |
| 112.94 | C2 | 324.77 | C3 |
| 120.84 | C3 | 327.33 | C3 |
| 124.10 | C2 | 338.50 | C1 |
| 125.88 | C1 | 349.24 | C2 |
| 130.52 | C2 | 357.36 | C1 |
| 130.76 | C3 | 360.37 | C3 |
| 144.16 | C1 | 365.21 | C2 |
| 150.61 | C3 | 366.03 | C2 |
| 154.18 | C3 | 366.04 | C1 |
| 156.54 | C1 | 380.64 | C2 |
| 163.03 | C1 | 389.64 | C2 |
| 166.15 | C1 | 418.84 | C3 |
| 167.21 | C1 | 427.39 | C1 |
| 179.93 | C2 | 429.46 | C3 |
| 195.27 | C3 | 437.45 | C3 |
| 201.07 | C3 | 449.55 | C1 |
| 203.93 | C2 | 455.18 | C3 |
| 204.56 | C2 | 455.99 | C1 |
| 205.88 | C3 | 475.72 | C3 |
| 215.39 | C3 | 479.32 | C3 |
| 228.63 | C2 | 491.46 | C1 |
| 243.40 | C1 | 494.00 | C3 |
| 245.96 | C3 | 496.95 | C2 |

## DT Data Run \#5

| Time | Component Failure | Time | Component Failure |
| :---: | :---: | :---: | :---: |
| 10.07 | C1 | 311.09 | C1 |
| 38.94 | C1 | 311.42 | C1 |
| 51.73 | C3 | 312.23 | C3 |
| 57.02 | C3 | 317.40 | C1 |
| 59.39 | C1 | 321.72 | C2 |
| 73.67 | C2 | 325.49 | C2 |
| 77.17 | C2 | 338.23 | C1 |
| 79.56 | C 2 | 343.49 | C2 |
| 81.77 | C1 | 346.16 | C3 |
| 83.79 | C2 | 351.11 | C3 |
| 102.76 | C2 | 359.99 | C2 |
| 111.46 | C1 | 364.48 | C3 |
| 113.76 | C2 | 367.25 | C2 |
| 117.40 | C3 | 373.64 | C1 |
| 120.92 | C2 | 374.40 | C3 |
| 140.39 | C1 | 376.93 | C2 |
| 140.93 | C3 | 384.09 | C2 |
| 143.52 | C3 | 394.25 | C1 |
| 143.67 | C3 | 401.81 | C2 |
| 150.00 | C1 | 402.77 | C3 |
| 153.58 | C1 | 417.35 | C3 |
| 157.12 | C1 | 418.39 | C3 |
| 160.97 | C 2 | 422.69 | C3 |
| 164.65 | C3 | 425.16 | C2 |
| 185.65 | C3 | 426.57 | C2 |
| 186.87 | C3 | 437.34 | C1 |
| 188.08 | C1 | 438.51 | C1 |
| 190.84 | C2 | 442.89 | C2 |
| 192.22 | C3 | 443.85 | C3 |
| 197.47 | C3 | 444.85 | C1 |
| 199.83 | C2 | 447.39 | C3 |
| 200.71 | C1 | 449.22 | C2 |
| 202.67 | C2 | 455.79 | C3 |
| 203.83 | C1 | 457.86 | C1 |
| 215.12 | C3 | 460.98 | C3 |
| 222.97 | C3 | 462.83 | C1 |
| 243.53 | C3 | 479.77 | C2 |
| 266.85 | C3 | 486.68 | C2 |
| 275.75 | C2 | 490.60 | C2 |
| 276.66 | C3 | 496.86 | C3 |
| 302.19 | C2 |  |  |

OT Data Runs \#1 and \#2

| OT Data Run \#1 |  | OT Data Run \#2 |  |
| :---: | :---: | :---: | :---: |
| Time | Component <br> Failure | Time | Component <br> Failure |
| 4.06 | C3 | 11.34 | C3 |
| 8.27 | C 2 | 18.10 | C 3 |
| 15.64 | C 1 | 29.26 | C 3 |
| 16.26 | C 2 | 35.38 | C 2 |
| 17.01 | C 2 | 36.41 | C 3 |
| 29.60 | C 1 | 51.17 | C 3 |
| 40.19 | C 2 | 55.38 | C 1 |
| 43.63 | C 3 | 75.49 | C 1 |
| 44.47 | C 3 | 79.78 | C 2 |
| 57.77 | C 2 | 84.86 | C 1 |
| 62.95 | C 2 | 88.63 | C 2 |
| 66.03 | C 1 | 96.55 | C 3 |
| 73.51 | C 3 | 103.25 | C 2 |
| 73.69 | C 3 | 111.41 | C 2 |
| 80.82 | C 1 | 115.54 | C 2 |
| 85.21 | C 1 |  |  |
| 92.91 | C 3 |  |  |
| 100.67 | Cl |  |  |
| 101.59 | C 2 |  |  |
| 110.15 | C 2 |  |  |
| 123.20 | Cl |  |  |
| 124.42 | C 3 |  |  |

Appendix F. Calculation For Parallel System Reliability With Independent and Identical Components.

Consider a system composed of $k=3$ independent and identical components in parallel configuration. The time to failure of each component is assumed to be exponentially distributed. Let $\lambda=0.05$ failure per hour be the respective constant failure rates of each component.

For the true system, using a mission time, $t$ of one hour, the reliability of components 1, 2, and 3 are
$R_{c}=R_{1}=R_{2}=R_{3}=\exp (-0.05)=95.12 \%$.
The reliability of the system can be calculated as
$R_{s}=1-\left(1-R_{c}\right)^{3}=1-(1-95.12 \%)^{3}=99.9884 \%$.
Using a computer program called RAPTOR, which is developed by AFOTEC, to simulate the true system, the following data are obtained (to review the simulated data, see Appendix E):

Table Fl: Aggregated Components DT Data

| Run $i$ | $T_{i}$ Hours | $X_{i}$ Failures | $\widehat{\lambda}_{i}=X_{i} / T_{i}$ |
| :---: | :---: | :---: | :---: |
| 1 | $1,493.82$ | 79 | 0.05289 |
| 2 | $1,463.13$ | 75 | 0.05126 |
| 3 | $1,492.59$ | 66 | 0.04422 |
| 4 | $1,490.85$ | 70 | 0.04695 |
| 5 | $1,490.58$ | 81 | 0.05434 |

Table F2: Aggregated Components OT Data

| Run $i$ | $T_{i}$ Hours | $X_{i}$ Failures | $\hat{\lambda}_{i}=X_{i} / T_{i}$ |
| :---: | :---: | :---: | :---: |
| 1 | 373.26 | 22 | 0.05894 |
| 2 | 346.62 | 15 | 0.04328 |

Table F3: Component 1 DT Data

| Run $i$ | $T_{i}$ Hours | $X_{i}$ Failures | $\widehat{\lambda_{i}}=X_{i} / T_{i}$ |
| :---: | :---: | :---: | :---: |
| 1 | 497.94 | 24 | 0.04820 |
| 2 | 487.71 | 26 | 0.05331 |
| 3 | 497.53 | 22 | 0.04422 |
| 4 | 496.95 | 20 | 0.04025 |
| 5 | 496.86 | 23 | 0.04629 |

Table F4: Component 1 OT Data

| Run $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures | $\widehat{\lambda_{i}}=\mathrm{X}_{i} / T_{i}$ |
| :---: | :---: | :---: | :---: |
| 1 | 124.42 | 7 | 0.05626 |
| 2 | 115.54 | 3 | 0.02597 |

Table F5: Component 2 DT Data

| Run $i$ | $T_{i}$ Hours | $X_{i}$ Failures | $\widehat{\lambda_{i}}=X_{i} / T_{i}$ |
| :---: | :---: | :---: | :---: |
| 1 | 497.94 | 35 | 0.07029 |
| 2 | 487.71 | 30 | 0.06151 |
| 3 | 497.53 | 21 | 0.04221 |
| 4 | 496.95 | 19 | 0.03823 |
| 5 | 496.86 | 28 | 0.05635 |

Table F6: Component 2 OT Data

| Run $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures | $\hat{\lambda}_{i}=\mathrm{X}_{\mathrm{i}} / \mathrm{T}_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: |
| 1 | 124.42 | 8 | 0.06430 |
| 2 | 115.54 | 6 | 0.05193 |

Table F7: Component 3 DT Data

| Run $i$ | $T_{i}$ Hours | $X_{i}$ Failures | $\widehat{\lambda_{i}}=X_{i} / T_{i}$ |
| :---: | :---: | :---: | :---: |
| 1 | 497.94 | 20 | 0.04017 |
| 2 | 487.71 | 19 | 0.03896 |
| 3 | 497.53 | 23 | 0.04623 |
| 4 | 496.95 | 31 | 0.06238 |
| 5 | 496.86 | 30 | 0.06038 |

Table F8: Component 3 OT Data

| Run $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures | $\widehat{\lambda_{i}}=\mathrm{X}_{\mathrm{i}} / \mathrm{T}_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: |
| 1 | 124.42 | 7 | 0.05626 |
| 2 | 115.54 | 6 | 0.05193 |

The Classical Exponential Method. Assuming the time to failure of each component has the exponential distribution, point estimates for the failure rate $\lambda$ and $80 \%$ confidence interval about $\lambda$ will be computed.

Component Aggregated DT: $\hat{\lambda}=\left(\frac{371}{7430.97}\right)=0.04993$
Component Aggregated OT: $\hat{\lambda}=\left(\frac{37}{719.88}\right)=0.05140$
Component 1 DT: $\hat{\lambda}=\left(\frac{f_{3}}{T_{3}}\right)=\left(\frac{115}{2476.99}\right)=0.04643$
Component 1 OT: $\hat{\lambda}=\left(\frac{f_{4}}{T_{4}}\right)=\left(\frac{10}{239.96}\right)=0.04167$
Component $2 \mathrm{DT}: \quad \hat{\lambda}=\left(\frac{f_{5}}{T_{5}}\right)=\left(\frac{133}{2476.99}\right)=0.05369$
Component 2 OT: $\hat{\lambda}=\left(\frac{f_{6}}{T_{6}}\right)=\left(\frac{14}{239.96}\right)=0.05834$
Component $3 \mathrm{DT}: \quad \hat{\lambda}=\left(\frac{f_{7}}{T_{7}}\right)=\left(\frac{123}{2476.99}\right)=0.04966$
Component 3 OT: $\hat{\lambda}=\left(\frac{f_{8}}{T_{8}}\right)=\left(\frac{13}{239.96}\right)=0.05418$
where $f_{1}=371$ is the number of failures and $T_{1}=7430.97$ is the total test time from Table F1 and similarly $f_{2}=37$ and $\mathrm{T}_{2}=719.88$ from Table $\mathrm{F} 2, \mathrm{f}_{3}=115$ and $\mathrm{T}_{3}=2476.99$ from Table $\mathrm{F} 3, f_{4}=10$ and $T_{4}=239.96$ from Table $F 4, f_{5}=133$ and $T_{5}=2476.99$ from Table $\mathrm{F} 5, f_{6}=14$ and $T_{6}=239.96$ from Table $\mathrm{F} 6, f_{7}=123$ and $T_{7}=2476.99$ from Table $\mathrm{F} 7, f_{8}=13$ and $\mathrm{T}_{8}=239.96$ from Table F8.

The $80 \%$ two-sided confidence intervals (TCI) are
Component Agaregated DT: (0.04664,0.05328)
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 371)}{2 \times 7430.97}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 371)}{2 \times 7430.97}\right)=\left(\frac{693.08}{14861.94}, \frac{791.78}{14861.94}\right)$
Component Aggregated OT: (0.04091,0.06248)
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 37)}{2 \times 719.88}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 37)}{2 \times 719.88}\right)=\left(\frac{58.9}{1439.76}, \frac{89.96}{1439.76}\right)$
Component $1 \mathrm{DT}:(0.04097,0.05206)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 115)}{2 \times 2476.99}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 115)}{2 \times 2476.99}\right)=\left(\frac{202.98}{4953.98}, \frac{257.88}{4953.98}\right)$
Component 1 OT: $(0.02593,0.05920)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 10)}{2 \times 239.96}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 10)}{2 \times 239.96}\right)=\left(\frac{12.44}{479.92}, \frac{28.41}{479.92}\right)$
Component $2 \mathrm{DI}:(0.04782,0.05974)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 133)}{2 \times 2476.99}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 133)}{2 \times 2476.99}\right)=\left(\frac{236.90}{4953.98}, \frac{295.95}{4953.98}\right)$
Component 2 OT: $(0.03946,0.07901)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 14)}{2 \times 239.96}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 14)}{2 \times 239.96}\right)=\left(\frac{18.94}{479.92}, \frac{37.92}{479.92}\right)$
Component $3 \mathrm{DT}:(0.04401,0.05548)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 123)}{2 \times 2476.99}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 123)}{2 \times 2476.99}\right)=\left(\frac{218.04}{4953.98}, \frac{274.82}{4953.98}\right)$
Component $3 \mathrm{OT}:(0.03603,0.07410)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 13)}{2 \times 239.96}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 13)}{2 \times 239.96}\right)=\left(\frac{17.29189}{479.92}, \frac{35.56317}{479.92}\right)$

The reliability estimators of $R(t)$ for $t=1$ hour are Component Aggregated DT:
$\widehat{R_{c}}(t)=\exp (-0.04993 \times 1)=95.13 \%$
Component Aggregated OT:
$\widehat{R_{c}}(t)=\exp (-0.05140 \times 1)=94.99 \%$
Component $1 \mathrm{DT}: \widehat{R_{1}}(t)=\exp (-0.04643 \times 1)=95.46 \%$
Component 1 OT: $\widehat{R_{1}}(t)=\exp (-0.04167 \times 1)=95.92 \%$
Component $2 \mathrm{DT}: \widehat{R_{2}}(t)=\exp (-0.05369 \times 1)=94.77 \%$
Component 2 OT: $\widehat{R_{2}}(t)=\exp (-0.05834 \times 1)=94.33 \%$
Component $3 \mathrm{DT}: \widehat{R_{3}}(t)=\exp (-0.04966 \times 1)=95.16 \%$
Component $3 \mathrm{OT}: \widehat{R_{3}}(t)=\exp (-0.05418 \times 1)=94.73 \%$
Aggregated Component to System DT: $\widehat{R}(t)=99.9885 \%$
$\widehat{R}(t)=1-\left(1-\mathrm{R}_{c}\right)^{3}=1-(1-95.13 \%)^{3}=0.999885$
Agqregated Component to System OT: $\widehat{R}(t)=99.9874 \%$
$\widehat{R}(t)=1-\left(1-R_{c}\right)^{3}=1-(1-94.99 \%)^{3}=0.999874$
Component Level Agaregated to System DT:
$\widehat{R}(t)=1-\left(1-R_{1}\right)\left(1-R_{2}\right)\left(1-R_{3}\right)$
$=1-(1-0.9546)(1-0.9477)(1-0.9516)=99.9885 \%$
Component Level Agaregated to System OT:
$\widehat{R}(t)=1-\left(1-R_{1}\right)\left(1-R_{2}\right)\left(1-R_{3}\right)$
$=1-(1-0.9592)(1-0.9433)(1-0.9473)=99.9878 \%$.

The $80 \%$ two-sided confidence intervals (TCI) are Aggregated Component DT: (94.81\%,95.44\%)
$\exp (-0.05328 \times 1) \leq \widehat{R}(1) \leq \exp (-0.04664 \times 1)$
Aggregated Component OT: (93.94\%,95.99\%)
$\exp (-0.06248 \times 1) \leq \widehat{R}(1) \leq \exp (-0.04091 \times 1)$
Component $1 \mathrm{DT}:(94.93 \%, 95.99 \%)$
$\exp (-0.05206 \times 1) \leq \widehat{R}(1) \leq \exp (-0.04097 \times 1)$
Component 1 OT: (94.25\%,97.44\%)
$\exp (-0.05920 \times 1) \leq \widehat{R}(1) \leq \exp (-0.02593 \times 1)$
Component $2 \mathrm{DT}:(94.20 \%, 95.33 \%)$
$\exp (-0.05974 \times 1) \leq \widehat{R}(1) \leq \exp (-0.04782 \times 1)$
Component 2 OT: (92.40\%,96.13\%)
$\exp (-0.07901 \times 1) \leq \widehat{R}(1) \leq \exp (-0.03946 \times 1)$
Component 3 DT: ( $94.60 \%, 95.69 \%$ )
$\exp (-0.05548 \times 1) \leq \widehat{R}(1) \leq \exp (-0.04401 \times 1)$
Component 3 OT: $(92.86 \%, 96.46 \%)$
$\exp (-0.07410 \times 1) \leq \widehat{R}(1) \leq \exp (-0.03603 \times 1)$
Aggregated Component to System DT:
(99.9860\%,99.9905\%)

Lower Bound $=1-(1-0.9481)^{3}=0.999860$
Upper Bound $=1-(1-0.9544)^{3}=0.999905$
Aggregated Component to System OT:
(99.9778\%,99.9936\%)

Lower Bound $=1-(1-0.9394)^{3}=0.999778$
Upper Bound $=1-(1-0.9599)^{3}=0.999936$

## Component Level Agaregated to System DT:

(99.9841\%, 99.9919\%)

Lower Bound $=1-\left(1-L_{1}\right)\left(1-\mathrm{LB}_{2}\right)\left(1-\mathrm{LB}_{3}\right)$
$=1-(1-0.9493)(1-0.9420)(1-0.9460)=0.999841$
Upper Bound $=1-\left(1-\mathrm{UB}_{1}\right)\left(1-\mathrm{UB}_{2}\right)\left(1-\mathrm{UB}_{3}\right)$
$=1-(1-0.9599)(1-0.9533)(1-0.9569)=0.999919$
Component Level Agaregated to System OT:
(99.9688\%, $99.9965 \%$ )

Lower Bound $=1-\left(1-L B_{1}\right)\left(1-L B_{2}\right)\left(1-L B_{3}\right)$
$=1-(1-0.9425)(1-0.9240)(1-0.9286)=0.999688$
Upper Bound $=1-\left(1-U B_{1}\right)\left(1-U B_{2}\right)\left(1-U B_{3}\right)$
$=1-(1-0.9744)(1-0.9613)(1-0.9646)=0.999965$.
The Bayesian Exponential Method.
Bayesian Exponential Prior.
For the component aggregated data, from Table F1:
$\widehat{E}(\lambda)=\bar{\lambda}=0.04993$ and $\widehat{V}(\lambda)=s_{\lambda}{ }^{2}=0.00002$.
These yielded the parameter estimates
$\alpha=\left(\frac{0.04993^{2}}{0.00002}\right)=139.59$ and $\beta=\left(\frac{0.04993}{0.00002}\right)=2795.66$.

For Component 1 data, from Table F3:
$\widehat{E}(\lambda)=\bar{\lambda}=0.04645$ and $\widehat{V}(\lambda)=s_{\lambda}^{2}=0.00002$.
These yielded the parameter estimates
$\alpha=\left(\frac{0.04645^{2}}{0.00002}\right)=92.19$ and $\beta=\left(\frac{0.04645}{0.00002}\right)=1984.67$.

For Component 2 data, from Table F5:
$\widehat{E}(\lambda)=\bar{\lambda}=0.05372$ and $\widehat{V}(\lambda)=s_{\lambda}{ }^{2}=0.00018$.
These yielded the parameter estimates
$\alpha=\left(\frac{0.05372^{2}}{0.00018}\right)=16.15$ and $\beta=\left(\frac{0.05372}{0.00018}\right)=300.71$.
For Component 3 data, from Table F7:
$\widehat{E}(\lambda)=\bar{\lambda}=0.04962$ and $\widehat{V}(\lambda)=s_{\lambda}{ }^{2}=0.00012$.

These yielded the parameter estimates
$\alpha=\left(\frac{0.04962^{2}}{0.00012}\right)=19.97$ and $\beta=\left(\frac{0.04962}{0.00012}\right)=402.48$.
Bayesian Exponential Posterior Analysis.
Agaregated Component: $\hat{\lambda}=\left(\frac{37+139.59}{719.88+2795.66}\right)=0.05023$.
Component 1: $\hat{\lambda}=\left(\frac{10+92.19}{239.96+1984.67}\right)=0.04594$.
Component 2: $\hat{\lambda}=\left(\frac{14+16.15}{239.96+300.71}\right)=0.05576$.
Component 3: $\hat{\lambda}=\left(\frac{13+19.97}{239.96+402.48}\right)=0.05132$.
The $80 \%$ two-sided probability intervals (TBPI) are
Aggregated Component:
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 37+2 \times 139.59)}{2(719.88+2795.66)}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 37+2 \times 139.59)}{2(719.88+2795.66)}\right)$
$=\left(\frac{319.41}{7031.08}, \frac{387.45}{7031.08}\right)=(0.04543,0.05511)$.

Component 1: $\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 10+2 \times 92.19)}{2(239.96+1984.67)}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 10+2 \times 92.19)}{2(239.96+1984.67)}\right)$
$=\left(\frac{178.58}{4449.26}, \frac{230.28}{4449.26}\right)=(0.04014,0.05176)$.
Component 2: $\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 14+2 \times 16.15)}{2(239.96+300.71)}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 14+2 \times 16.15)}{2(239.96+300.71)}\right)$
$=\left(\frac{46.46}{1081.34}, \frac{74.4}{1081.34}\right)=(0.04296,0.06880)$.
Component 3: $\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 13+2 \times 19.97)}{2(239.96+402.48)}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 13+2 \times 19.97)}{2(239.96+402.48)}\right)$
$=\left(\frac{50.88}{1284.88}, \frac{79.97}{1284.88}\right)=(0.03960,0.06224)$.
The Bayesian estimators of $R(t)$ for $t=1$ hour are Agaregated Component: $\widehat{R}(t)=95.10 \%$

$$
\widehat{R}(t)=\left(\frac{\left(\frac{719.88}{2795.66}\right)+1}{\left(\frac{719.88}{2795.66}\right)+\left(\frac{1}{2795.66}\right)+1}\right)^{139.59+37}
$$

Component 1: $\widehat{R}(t)=95.51 \%$

$$
\widehat{R}(t)=\left(\frac{\left(\frac{239.96}{1984.67}\right)+1}{\left(\frac{239.96}{1984.67}\right)+\left(\frac{1}{1984.67}\right)+1}\right)^{92.19+10}
$$

Component 2: $\widehat{R}(t)=94.58 \%$

$$
\widehat{R}(t)=\left(\frac{\left(\frac{239.96}{300.71}\right)+1}{\left(\frac{239.96}{300.71}\right)+\left(\frac{1}{300.71}\right)+1}\right)^{16.15+14}
$$

Component 3: $\widehat{R}(t)=95.00 \%$

$$
\widehat{R}(t)=\left(\frac{\left(\frac{239.96}{402.48}\right)+1}{\left(\frac{239.96}{402.48}\right)+\left(\frac{1}{402.48}\right)+1}\right)^{19.97+13}
$$

Aggregated Component to System: $\widehat{R}(t)=99.9882 \%$
$\widehat{R}(t)=1-\left(1-R_{c}\right)^{3}=1-(1-95.10 \%)^{3}=0.999882$
Component Level Aggregated to System: $\widehat{R}(t)=99.9878 \%$
$\widehat{R}(t)=1-(1-0.9551)(1-0.9458)(1-0.9500)$
The $80 \%$ two-sided probability intervals (TBPI) are Agaregated Component: $(94.64 \% \leq \widehat{R}(1) \leq 95.56 \%)$
$\exp (-0.05511 \times 1) \leq \widehat{R}(1) \leq \exp (-0.04543 \times 1)$.
Component 1: $(94.96 \% \leq \widehat{R}(1) \leq 96.07 \%)$
$\exp (-0.05176 \times 1) \leq \widehat{R}(1) \leq \exp (-0.04014 \times 1)$.
Component 2: $\quad(93.35 \% \leq \widehat{R}(1) \leq 95.80 \%)$
$\exp (-0.06880 \times 1) \leq \widehat{R}(1) \leq \exp (-0.04296 \times 1)$.
Component 3: (93.97\% $\leq \widehat{R}(1) \leq 96.12 \%)$
$\exp (-0.06224 \times 1) \leq \widehat{R}(1) \leq \exp (-0.03960 \times 1)$.
Agaregated Component to System: (99.9846\%,99.9913\%)
Lower Bound $=1-(1-0.9464)^{3}=0.999846$
Upper Bound $=1-(1-0.9556)^{3}=0.999913$
Component Level Aggregated to System:
(99.9798\%,99.9936\%)

Lower Bound $=1-\left(1-L B_{1}\right)\left(1-L B_{2}\right)\left(1-L B_{3}\right)$
$=1-(1-0.9496)(1-0.9335)(1-0.9397)=0.999798$
Upper Bound $=1-\left(1-\mathrm{UB}_{1}\right)\left(1-\mathrm{UB}_{2}\right)\left(1-\mathrm{UB}_{3}\right)$
$=1-(1-0.9607)(1-0.9580)(1-0.9612)=0.999936$.

Appendix G. Simulated Data For Parallel System With

## Different Independent Components.

DT Data Run \#1

| Time | Component <br> Failure | Time | Component <br> Failure | Time | Component <br> Failure |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 6.03 | C 1 | 177.73 | C 2 | 328.02 | C 1 |
| 9.36 | C 1 | 180.72 | C 2 | 328.93 | C 1 |
| 21.91 | C 1 | 184.44 | C 1 | 337.22 | C 2 |
| 24.08 | C 3 | 187.58 | C 1 | 351.00 | C 1 |
| 28.79 | C 1 | 189.41 | C 1 | 354.85 | C 2 |
| 33.23 | C 2 | 189.68 | C 1 | 365.39 | C 2 |
| 33.42 | C 2 | 201.89 | C 1 | 367.84 | C 2 |
| 38.45 | C 2 | 209.57 | C 2 | 371.18 | C 1 |
| 41.87 | C 3 | 226.86 | C 1 | 376.72 | C 1 |
| 43.37 | C 1 | 240.59 | C 1 | 377.86 | C 1 |
| 49.15 | C 3 | 243.74 | C 1 | 383.68 | C 2 |
| 65.41 | C 2 | 249.69 | C 2 | 384.25 | C 2 |
| 74.71 | C 2 | 251.30 | C 1 | 386.30 | C 3 |
| 76.85 | C 2 | 261.09 | C 1 | 390.86 | C 2 |
| 102.23 | C 1 | 262.25 | C 1 | 397.32 | C 2 |
| 102.40 | C 1 | 264.60 | C 1 | 404.24 | C 1 |
| 102.70 | C 1 | 267.10 | C 1 | 405.30 | C 1 |
| 106.51 | C 1 | 274.40 | C 2 | 418.69 | C 1 |
| 108.57 | C 1 | 276.84 | C 1 | 424.05 | C 1 |
| 110.18 | C 1 | 279.60 | C 3 | 427.08 | C 1 |
| 133.90 | C 1 | 284.25 | C 1 | 429.30 | C 1 |
| 136.90 | C 1 | 284.26 | C 2 | 434.15 | C 1 |
| 140.04 | C 3 | 285.73 | C 1 | 437.05 | C 1 |
| 151.32 | C 1 | 290.06 | C 3 | 437.24 | C 2 |
| 156.12 | C 2 | 296.62 | C 1 | 443.94 | C 1 |
| 161.19 | C 3 | 301.54 | C 1 | 444.49 | C 2 |
| 165.34 | C 1 | 304.56 | C 2 | 446.56 | C 1 |
| 171.86 | C 1 | 305.03 | C 3 | 448.34 | C 1 |
| 172.97 | C 2 | 306.18 | C 3 | 457.56 | C 1 |
| 173.20 | C 1 | 322.17 | C 2 | 488.03 | C 1 |
| 177.59 | C 1 | 323.68 | C 2 |  |  |

DT Data Run \#2

| Time | Component <br> Failure | Time | Component <br> Failure | Time | Component <br> Failure |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 3.90 | C 2 | 196.14 | C 3 | 340.60 | C 1 |
| 7.23 | C 3 | 201.56 | C 1 | 365.29 | C 1 |
| 7.61 | C 2 | 203.70 | C 2 | 366.46 | C 2 |
| 7.82 | C 1 | 213.24 | C 1 | 369.83 | C 1 |
| 14.65 | C 1 | 217.15 | C 1 | 381.72 | C 1 |
| 17.42 | C 1 | 219.19 | C 2 | 389.02 | C 1 |
| 18.91 | C 2 | 236.49 | C 2 | 398.17 | C 1 |
| 22.44 | C 2 | 242.73 | C 1 | 399.58 | C 2 |
| 34.50 | C 1 | 243.28 | C 1 | 407.08 | C 2 |
| 46.64 | C 1 | 249.64 | C 2 | 409.67 | C 2 |
| 46.79 | C 1 | 253.23 | C 2 | 413.71 | C 1 |
| 52.25 | C 1 | 256.43 | C 3 | 416.37 | C 1 |
| 56.58 | C 1 | 257.41 | C 1 | 416.42 | C 2 |
| 61.16 | C 1 | 275.39 | C 1 | 417.14 | C 1 |
| 84.34 | C 1 | 277.64 | C 1 | 418.10 | C 1 |
| 85.06 | C 1 | 283.34 | C 2 | 424.77 | C 1 |
| 85.10 | C 2 | 283.80 | C 1 | 432.10 | C 2 |
| 95.32 | C 3 | 296.04 | C 2 | 439.16 | C 1 |
| 112.01 | C 1 | 296.34 | C 1 | 440.17 | C 2 |
| 115.58 | C 3 | 298.74 | C 2 | 443.43 | C 1 |
| 118.78 | C 1 | 299.96 | C 2 | 447.82 | C 2 |
| 124.60 | C 2 | 302.78 | C 1 | 452.04 | C 1 |
| 130.93 | C 1 | 306.89 | C 1 | 454.71 | C 2 |
| 140.08 | C 3 | 309.74 | C 1 | 458.89 | C 2 |
| 156.14 | C 1 | 322.13 | C 1 | 468.41 | C 1 |
| 164.75 | C 2 | 323.67 | C 1 | 471.86 | C 1 |
| 166.15 | C 2 | 324.09 | C 1 | 481.86 | C 2 |
| 166.29 | C 1 | 326.37 | C 1 | 482.41 | C 1 |
| 177.87 | C 1 | 328.53 | C 1 | 498.15 | C 1 |
| 186.36 | C 2 | 328.59 | C 2 |  |  |
| 191.28 | C 3 | 330.33 | C 3 |  |  |
|  |  |  |  |  |  |

## DT Data Run \#3

| Time | Component Failure | Time | Component Failure |
| :---: | :---: | :---: | :---: |
| 2.47 | C2 | 274.65 | C1 |
| 3.89 | C2 | 279.05 | C3 |
| 6.14 | C3 | 283.69 | C1 |
| 12.44 | C1 | 288.17 | C1 |
| 19.74 | C2 | 289.58 | C1 |
| 24.37 | C2 | 292.01 | C1 |
| 30.43 | C2 | 296.44 | C 2 |
| 37.23 | C2 | 306.05 | C1 |
| 37.56 | C1 | 311.49 | C2 |
| 52.17 | C1 | 313.14 | C3 |
| 54.17 | C1 | 330.60 | C3 |
| 57.07 | C1 | 330.62 | C1 |
| 58.99 | C3 | 332.40 | C3 |
| 64.06 | C2 | 343.77 | C1 |
| 78.26 | C1 | 347.58 | C1 |
| 78.47 | C1 | 356.96 | C1 |
| 79.43 | C1 | 363.66 | C3 |
| 100.52 | C1 | 370.35 | C1 |
| 100.66 | C1 | 371.06 | C2 |
| 107.65 | C1 | 387.09 | C3 |
| 108.07 | C1 | 392.95 | C1 |
| 112.62 | C1 | 394.49 | C1 |
| 117.15 | C1 | 394.51 | C1 |
| 125.21 | C2 | 395.85 | C1 |
| 148.12 | C2 | 401.96 | C2 |
| 149.47 | C2 | 416.91 | C1 |
| 152.94 | C1 | 419.24 | C1 |
| 153.45 | C2 | 421.87 | C2 |
| 155.09 | C1 | 425.12 | C1 |
| 155.69 | C2 | 427.82 | C1 |
| 183.32 | C1 | 434.34 | C1 |
| 190.35 | C2 | 435.53 | C2 |
| 203.84 | C3 | 441.33 | C1 |
| 228.08 | C1 | 446.11 | C1 |
| 228.64 | C3 | 455.95 | C1 |
| 231.15 | C3 | 464.17 | C2 |
| 236.29 | C2 | 474.43 | C2 |
| 236.76 | C3 | 481.60 | C1 |
| 245.00 | C1 | 488.36 | C2 |
| 269.60 | C2 | 498.39 | C1 |

DT Data Run \#4

| Time | Component Failure | Time | Component Failure |
| :---: | :---: | :---: | :---: |
| 1.07 | C2 | 254.11 | C1 |
| 9.19 | C1 | 259.43 | C1 |
| 10.02 | C2 | 260.10 | C1 |
| 11.54 | C3 | 266.24 | C2 |
| 11.68 | C2 | 275.53 | C1 |
| 14.80 | C2 | 280.58 | C2 |
| 17.36 | C2 | 283.27 | C 2 |
| 33.90 | C1 | 288.07 | C2 |
| 43.33 | C1 | 288.67 | C1 |
| 50.04 | C3 | 296.32 | C2 |
| 50.40 | C2 | 297.52 | C2 |
| 51.32 | C1 | 300.02 | C3 |
| 51.73 | C1 | 300.80 | C1 |
| 59.03 | C1 | 302.24 | C3 |
| 67.39 | C3 | 309.28 | C1 |
| 85.41 | C3 | 323.91 | C1 |
| 89.71 | C1 | 336.46 | C3 |
| 95.02 | C1 | 357.20 | C2 |
| 106.10 | C1 | 381.58 | C2 |
| 108.87 | C2 | 389.83 | C3 |
| 110.09 | C1 | 406.69 | C2 |
| 113.31 | C1 | 411.97 | C1 |
| 123.58 | C1 | 415.72 | C1 |
| 126.61 | C2 | 417.64 | C1 |
| 130.21 | C2 | 435.36 | C1 |
| 141.32 | C1 | 438.08 | C1 |
| 144.89 | C2 | 441.96 | C1 |
| 157.24 | C1 | 445.27 | C1 |
| 161.29 | C2 | 448.37 | C3 |
| 164.69 | C1 | 452.14 | C2 |
| 208.39 | C1 | 454.89 | C1 |
| 208.97 | C1 | 463.03 | C2 |
| 215.92 | C1 | 467.94 | C1 |
| 216.81 | C1 | 496.10 | C 2 |
| 234.96 | C2 | 496.55 | C 2 |
| 239.33 | C 2 |  |  |

## DT Data Run \#5

| Time | Component <br> Failure | Time | Component <br> Failure | Time | Component <br> Failure |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0.17 | C 1 | 136.39 | C 1 | 311.20 | C 1 |
| 11.94 | C 3 | 139.84 | C 1 | 313.51 | C 1 |
| 12.00 | C 2 | 141.80 | C 1 | 319.84 | C 2 |
| 15.77 | C 2 | 151.48 | C 1 | 319.96 | C 2 |
| 17.13 | C 1 | 156.22 | C 1 | 320.31 | C 1 |
| 33.77 | C 2 | 159.43 | C 1 | 328.99 | C 2 |
| 34.84 | C 1 | 166.95 | C 2 | 334.68 | C 2 |
| 37.31 | C 1 | 167.06 | C 1 | 336.05 | C 1 |
| 43.99 | C 1 | 168.03 | C 1 | 339.66 | C 2 |
| 47.63 | C 1 | 168.91 | C 1 | 344.45 | C 2 |
| 50.27 | C 2 | 176.16 | C 1 | 345.21 | C 2 |
| 52.59 | C 1 | 180.09 | C 1 | 353.47 | C 1 |
| 53.61 | C 3 | 181.48 | C 1 | 364.79 | C 3 |
| 59.96 | C 2 | 198.49 | C 1 | 368.50 | C 1 |
| 62.89 | C 1 | 202.00 | C 2 | 371.28 | C 2 |
| 67.11 | C 2 | 211.50 | C 1 | 384.22 | C 2 |
| 71.75 | C 1 | 216.34 | C 1 | 400.70 | C 2 |
| 83.43 | C 1 | 226.76 | C 2 | 404.40 | C 1 |
| 90.72 | C 1 | 235.59 | C 1 | 409.07 | C 2 |
| 91.24 | C 1 | 236.75 | C 2 | 414.83 | C 1 |
| 93.38 | C 1 | 239.91 | C 1 | 417.70 | C 1 |
| 103.97 | C 1 | 247.21 | C 1 | 425.99 | C 3 |
| 104.68 | C 1 | 256.07 | C 2 | 426.65 | C 1 |
| 110.20 | C 2 | 257.26 | C 1 | 442.94 | C 1 |
| 110.35 | C 3 | 257.53 | C 1 | 449.73 | C 1 |
| 111.37 | C 2 | 258.07 | C 2 | 451.98 | C 1 |
| 112.83 | C 1 | 264.20 | C 2 | 451.99 | C 1 |
| 114.60 | C 1 | 271.22 | C 2 | 452.57 | C 1 |
| 117.70 | C 2 | 273.63 | C 1 | 474.32 | C 3 |
| 121.11 | C 1 | 281.84 | C 2 | 479.76 | C 1 |
| 123.04 | C 3 | 282.96 | C 3 | 479.79 | C 2 |
| 126.10 | C 2 | 283.17 | C 2 | 480.37 | C 1 |
| 131.07 | C 2 | 283.24 | C 1 | 491.62 | C 1 |
| 133.41 | C 3 | 310.37 | C 1 | 496.36 | C 1 |

OT Data Runs \#1 and \#2

| OT Data Run \#1 |  | OT Data Run \#2 |  |
| :---: | :---: | :---: | :---: |
| Time | Component <br> Failure | Time | Component <br> Failure |
| 7.82 | C 1 | 5.58 | C 1 |
| 8.11 | C 3 | 12.85 | C 2 |
| 8.27 | C 2 | 14.31 | C 3 |
| 22.23 | C 2 | 27.61 | C 2 |
| 22.99 | C 2 | 27.78 | C 1 |
| 24.08 | C 3 | 32.47 | C 1 |
| 27.60 | C 1 | 36.89 | C 1 |
| 36.39 | C 1 | 47.72 | C 2 |
| 36.81 | C 1 | 60.70 | C 1 |
| 46.17 | C 2 | 62.34 | C 2 |
| 51.33 | C 1 | 70.50 | C 2 |
| 51.35 | C 2 | 74.63 | C 2 |
| 66.15 | C 2 | 85.33 | C 1 |
| 66.33 | C 2 | 86.59 | C 2 |
| 70.65 | C 1 | 89.67 | C 1 |
| 72.85 | C 1 | 91.98 | C 2 |
| 80.58 | C 1 | 105.08 | C 3 |
| 85.55 | C 2 | 109.31 | C 3 |
| 96.34 | C 1 | 113.13 | C 1 |
| 96.94 | C 3 | 113.29 | C 3 |
| 100.62 | C 1 |  |  |
| 106.24 | C 1 |  |  |
| 108.08 | C 2 |  |  |
| 112.81 | Cl |  |  |
| 122.22 | Cl |  |  |

Appendix H. Calculation For Parallel System Reliability With Different Independent Components.

Consider a system composed of $k=3$ different components in parallel configuration. The time to failure of each component is assumed to be exponentially distributed. Let $\lambda_{1}=0.1, \lambda_{2}=0.05$, and $\lambda_{3}=0.025$ be the respective constant failure rates (failure per hour) of each component.

For the true system, using a mission time, $t$ of one hour, the reliability of components 1, 2, and 3 are

$$
\begin{aligned}
& R_{1}=\exp (-0.100)=90.48 \% \\
& R_{2}=\exp (-0.050)=95.12 \% \\
& R_{3}=\exp (-0.025)=97.53 \% .
\end{aligned}
$$

The reliability of the system can be calculated as

$$
R_{s}=1-\left(1-R_{1}\right)\left(1-R_{2}\right)\left(1-R_{3}\right)
$$

$$
=1-(1-0.9048)(1-0.9512)(1-0.9753)=99.9885 \% .
$$

Using a computer program called RAPTOR, which is developed by AFOTEC, to simulate the true system, the following data are obtained (to review the simulated data, see Appendix G):

Table HI: Component 1 DT Data

| Run $i$ | $T_{i}$ Hours | $X_{i}$ Failures | $\overline{\lambda_{i}}=X_{i} / T_{i}$ |
| :---: | :---: | :---: | :---: |
| 1 | 488.03 | 55 | 0.11270 |
| 2 | 498.15 | 53 | 0.10639 |
| 3 | 498.39 | 44 | 0.08828 |
| 4 | 496.55 | 36 | 0.07250 |
| 5 | 496.36 | 60 | 0.12088 |

Table H2: Component 1 OT Data

| Run $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures | $\widehat{\lambda_{i}}=\mathrm{X}_{\mathrm{i}} / \mathrm{T}_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: |
| 1 | 122.22 | 13 | 0.10637 |
| 2 | 113.29 | 8 | 0.07062 |

Table H3: Component 2 DT Data

| Run $i$ | $T_{i}$ Hours | $X_{i}$ Failures | $\widehat{\lambda_{i}}=X_{i} / T_{i}$ |
| :---: | :---: | :---: | :---: |
| 1 | 488.03 | 27 | 0.05532 |
| 2 | 498.15 | 30 | 0.06022 |
| 3 | 498.39 | 24 | 0.04816 |
| 4 | 496.55 | 26 | 0.05236 |
| 5 | 496.36 | 33 | 0.06648 |

Table H4: Component 2 OT Data

| Run $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures | $\overline{\lambda_{i}}=\mathrm{X}_{\mathrm{i}} / \mathrm{T}_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: |
| 1 | 122.22 | 9 | 0.07364 |
| 2 | 113.29 | 8 | 0.07062 |

Table H5: Component 3 DT Data

| Run $i$ | $T_{i}$ Hours | $X_{i}$ Failures | $\widehat{\lambda_{i}}=X_{i} / T_{i}$ |
| :---: | :---: | :---: | :---: |
| 1 | 488.03 | 10 | 0.02049 |
| 2 | 498.15 | 8 | 0.01606 |
| 3 | 498.39 | 12 | 0.02408 |
| 4 | 496.55 | 9 | 0.01813 |
| 5 | 496.36 | 9 | 0.01813 |

Table H6: Component 3 OT Data

| Run $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures | $\widehat{\lambda}_{i}=\mathrm{X}_{\mathrm{i}} / \mathrm{T}_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: |
| 1 | 122.22 | 3 | 0.02455 |
| 2 | 113.29 | 4 | 0.03531 |

The Classical Exponential Method.
Assuming the time to failure of each component has the exponential distribution, point estimates for the failure rate $\lambda$ and $80 \%$ confidence intervals about $\lambda$ will be computed.

Component 1 DT: $\hat{\lambda}=\left(\frac{f_{1}}{T_{1}}\right)=\left(\frac{248}{2477.48}\right)=0.10010$
Component 1 OT: $\hat{\lambda}=\left(\frac{f_{2}}{T_{2}}\right)=\left(\frac{21}{235.51}\right)=0.08917$

Component 2 DT: $\quad \hat{\lambda}=\left(\frac{f_{3}}{T_{3}}\right)=\left(\frac{140}{2477.48}\right)=0.05651$
Component 2 OT: $\hat{\lambda}=\left(\frac{f_{4}}{T_{4}}\right)=\left(\frac{17}{235.51}\right)=0.07218$
Component 3 DT: $\quad \hat{\lambda}=\left(\frac{f_{5}}{T_{5}}\right)=\left(\frac{48}{2477.48}\right)=0.01938$
Component 3 OT: $\quad \hat{\lambda}=\left(\frac{f_{6}}{T_{6}}\right)=\left(\frac{7}{235.51}\right)=0.02972$
where $f_{1}=248$ is the number of failures and $T_{1}=2477.48$ is the total test time from Table H1, $f_{2}=21$ and $T_{2}=235.51$ from Table $H 2, f_{3}=140$ and $T_{3}=2477.48$ from Table $H 3, f_{4}=$ 17 and $T_{4}=235.51$ from Table $H 4, f_{5}=48$ and $T_{5}=2477.48$ from Table H5, $f_{6}=7$ and $T_{6}=235.51$ from Table H6.

The 80\% two-sided confidence intervals (TCI) are
Component $1 \mathrm{DT}:(0.09205,0.10833)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 248)}{2 \times 2477.48}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 248)}{2 \times 2477.48}\right)=\left(\frac{456.09}{4954.96}, \frac{536.77}{4954.96}\right)$
Component 1 OT: $(0.06532,0.11484)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 21)}{2 \times 235.51}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 21)}{2 \times 235.51}\right)=\left(\frac{30.77}{471.02}, \frac{54.09}{471.02}\right)$
Component 2 DT: $(0.05048,0.06271)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 140)}{2 \times 2477.48}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 140)}{2 \times 2477.48}\right)=\left(\frac{250.13}{4954.96}, \frac{310.72}{4954.96}\right)$
Component 2 OT: $(0.05085,0.09533)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 17)}{2 \times 235.51}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 17)}{2 \times 235.51}\right)=\left(\frac{23.95}{471.02}, \frac{44.9}{471.02}\right)$
Component 3 DT: $(0.01589,0.02303)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 48)}{2 \times 2477.48}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 48)}{2 \times 2477.48}\right)=\left(\frac{78.73}{4954.96}, \frac{114.13}{4954.96}\right)$
Component 3 OT: $(0.01654,0.04472)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 7)}{2 \times 235.51}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 7)}{2 \times 235.51}\right)=\left(\frac{7.79}{471.02}, \frac{21.06}{471.02}\right)$
The reliability estimators of $R(t)$ for $t=1$ hour are
Component $1 \mathrm{DT}: \widehat{R_{1}}(t)=\exp (-0.10010 \times 1)=90.48 \%$
Component 1 OT: $\widehat{R_{1}}(t)=\exp (-0.08917 \times 1)=91.47 \%$
Component $2 \mathrm{DT}: \widehat{R_{2}}(t)=\exp (-0.05651 \times 1)=94.51 \%$
Component 2 OT: $\widehat{R_{2}}(t)=\exp (-0.07218 \times 1)=93.04 \%$
Component $3 \mathrm{DT}: \widehat{R_{3}}(t)=\exp (-0.01938 \times 1)=98.08 \%$
Component $3 \mathrm{OT}: \widehat{R_{3}}(t)=\exp (-0.02972 \times 1)=97.07 \%$
Component Level Agaregated to System $D T: \widehat{R}(t)=99.998$
$\widehat{R}(t)=1-(1-0.9048)(1-0.9451)(1-0.9808)$
Component Level Aggregated to System OT:
$\widehat{R}(t)=1-(1-0.9147)(1-0.9304)(1-0.9707)$
$=99.9826 \%$.
The $80 \%$ two-sided confidence intervals (TCI) are
Component 1 DT: $(89.73 \%, 91.21 \%)$
$\exp (-0.10833 \times 1) \leq \widehat{R}(1) \leq \exp (-0.09205 \times 1)$
Component 1 OT: (89.15\%,93.68\%)
$\exp (-0.11484 \times 1) \leq \widehat{R}(1) \leq \exp (-0.06532 \times 1)$
Component 2 DT: (93.92\%,95.08\%)
$\exp (-0.06271 \times 1) \leq \widehat{R}(1) \leq \exp (-0.05048 \times 1)$
Component 2 OT: $(90.91 \%, 95.04 \%)$
$\exp (-0.09533 \times 1) \leq \widehat{R}(1) \leq \exp (-0.05085 \times 1)$
Component 3 DT : $(97.72 \%, 98.42 \%)$
$\exp (-0.02303 \times 1) \leq \widehat{R}(1) \leq \exp (-0.01589 \times 1)$
Component 3 от: $(95.63 \%, 98.36 \%)$
$\exp (-0.04472 \times 1) \leq \widehat{R}(1) \leq \exp (-0.01654 \times 1)$
Component Level Agaregated to System DT:
(99.9858\%,99.9932\%)

Lower Bound $=1-(1-0.8973)(1-0.9392)(1-0.9772)$
Upper Bound $=1-(1-0.9121)(1-0.9508)(1-0.9842)$
Component Level Aggregated to System OT:
(99.9569\%, 99.9949\%)

Lower Bound $=1-(1-0.8915)(1-0.9091)(1-0.9563)$
Upper Bound $=1-(1-0.9368)(1-0.9504)(1-0.9836)$.
The Bayesian Exponential Method.
Bayesian Exponential Prior.
For Component 1 data, from Table H1:
$\widehat{E}(\lambda)=\bar{\lambda}=0.10015$ and $\widehat{V}(\lambda)=s_{\lambda}{ }^{2}=0.00038$.

These yielded the parameter estimates
$\alpha=\left(\frac{0.10015^{2}}{0.00038}\right)=26.40$ and $\beta=\left(\frac{0.10015}{0.00038}\right)=263.55$.
For Component 2 data, from Table H3:
$\widehat{E}(\lambda)=\bar{\lambda}=0.05651$ and $\widehat{V}(\lambda)=s_{\lambda}{ }^{2}=0.00005$.
These yielded the parameter estimates
$\alpha=\left(\frac{0.05651^{2}}{0.00005}\right)=63.87$ and $\beta=\left(\frac{0.05651}{0.00005}\right)=1130.2$.
For Component 3 data, from Table H5:
$\widehat{E}(\lambda)=\bar{\lambda}=0.01938$ and $\widehat{V}(\lambda)=s_{\lambda}{ }^{2}=0.00001$.
These yielded the parameter estimates
$\alpha=\left(\frac{0.01938^{2}}{0.00001}\right)=37.56$ and $\beta=\left(\frac{0.01938}{0.00001}\right)=1938$.
Bayesian Exponential Posterior Analysis.
Component 1: $\hat{\lambda}=\left(\frac{21+26.4}{235.51+263.55}\right)=0.09498$.
Component 2: $\hat{\lambda}=\left(\frac{17+63.87}{235.51+1130.2}\right)=0.05922$.
Component 3: $\hat{\lambda}=\left(\frac{7+37.56}{235.51+1938}\right)=0.02050$.
The $80 \%$ two-sided probability intervals (TBPI) are
Component 1: $\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 21+2 \times 26.4)}{2(235.51+263.55)}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 21+2 \times 26.4)}{2(235.51+263.55)}\right)$
$=\left(\frac{76.91}{998.12}, \frac{111.94}{998.12}\right)=(0.07706,0.11216)$.
Component 2: $\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 17+2 \times 63.87)}{2(235.51+1130.2)}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 17+2 \times 63.87)}{2(235.51+1130.2)}\right)$
$=\left(\frac{138.47}{2731.42}, \frac{184.38}{2731.42}\right)=(0.05070,0.06750)$.
Component 3: $\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 7+2 \times 37.56)}{2(235.51+1938)}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 7+2 \times 37.56)}{2(235.51+1938)}\right)$
$=\left(\frac{72.39}{4347.02}, \frac{106.47}{4347.02}\right)=(0.01665,0.02449)$.

The Bayesian estimators of $R(t)$ for $t=1$ hour are Component 1: $\widehat{R}(t)=90.95 \%$

$$
\widehat{R}(t)=\left(\frac{\left(\frac{235.51}{263.55}\right)+1}{\left(\frac{235.51}{263.55}\right)+\left(\frac{1}{263.55}\right)+1}\right)^{26.4+21}
$$

Component 2: $\widehat{R}(t)=94.25 \%$

$$
\widehat{R}(t)=\left(\frac{\left(\frac{235.51}{1130.2}\right)+1}{\left(\frac{235.51}{1130.2}\right)+\left(\frac{1}{1130.2}\right)+1}\right)^{63.87+17}
$$

Component 3: $\widehat{R}(t)=97.97 \%$

$$
\widehat{R}(t)=\left(\frac{\left(\frac{235.51}{1938}\right)+1}{\left(\frac{235.51}{1938}\right)+\left(\frac{1}{1938}\right)+1}\right)^{37.56+7}
$$

Component Level Aggregated to System: $\widehat{R}(t)=99.9894 \%$
$\widehat{R}(t)=1-(1-0.9095)(1-0.9425)(1-0.9797)$.
The $80 \%$ two-sided probability intervals (TBPI) are Component 1: (89.39\% $\leq \widehat{R}(1) \leq 92.58 \%)$
$\exp (-0.11216 \times 1) \leq \widehat{R}(1) \leq \exp (-0.07706 \times 1)$.
Component 2: $(93.47 \% \leq \widehat{R}(1) \leq 95.06 \%)$
$\exp (-0.06750 \times 1) \leq \widehat{R}(1) \leq \exp (-0.05070 \times 1)$.
Component 3: $(97.58 \% \leq \widehat{R}(1) \leq 98.35 \%)$
$\exp (-0.02449 \times 1) \leq \widehat{R}(1) \leq \exp (-0.01665 \times 1)$.
Component Level Aggregated to System: (99.9832\%,99.994\%)
Lower Bound $=1$ - (1-0.8939)(1-0.9347)(1-0.9758)
Upper Bound $=1-(1-0.9258)(1-0.9506)(1-0.9835)$.

Appendix I. Simulated Data For A Bridge System With
Independent And Identical Components.
DT Data Run \#1

| Time | Fail | Time | Fail | Time | Fail | Time | Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6.66 | C 5 | 139.79 | C 2 | 260.39 | C 3 | 384.83 | C 5 |
| 12.04 | C 3 | 140.33 | C 2 | 264.41 | C 2 | 386.05 | C 2 |
| 12.06 | C 1 | 142.74 | C 3 | 266.69 | C 2 | 391.94 | C 4 |
| 20.96 | C 1 | 149.49 | C 5 | 270.53 | C 1 | 394.66 | C 3 |
| 25.80 | C 3 | 158.44 | C 1 | 271.10 | C 1 | 401.82 | C 4 |
| 25.99 | C 3 | 164.77 | C 2 | 271.47 | C 3 | 403.74 | C 1 |
| 29.44 | C 4 | 167.16 | C 4 | 275.73 | C 5 | 407.75 | C 3 |
| 31.02 | C 3 | 171.06 | C 2 | 277.59 | C 4 | 407.96 | C 4 |
| 31.76 | C 5 | 182.30 | C 4 | 277.71 | C 1 | 420.43 | C 3 |
| 33.23 | C 2 | 185.90 | C 1 | 279.82 | C 1 | 424.30 | C 4 |
| 34.66 | C 3 | 188.21 | C 1 | 282.18 | C 5 | 428.60 | C 3 |
| 43.96 | C 3 | 189.61 | C 5 | 292.90 | C 5 | 430.08 | C 5 |
| 46.09 | C 3 | 192.67 | C 3 | 298.96 | C 5 | 433.07 | C 3 |
| 50.10 | C 1 | 192.92 | C 1 | 303.40 | C 5 | 437.72 | C 5 |
| 50.43 | C 1 | 194.60 | C 5 | 306.61 | C 1 | 441.39 | C 1 |
| 51.04 | C 1 | 195.77 | C 2 | 312.40 | C 1 | 445.33 | C 3 |
| 56.41 | C 4 | 201.01 | C 2 | 313.09 | C 5 | 447.24 | C 2 |
| 58.66 | C 1 | 201.87 | C 4 | 317.51 | C 4 | 447.41 | C 5 |
| 60.53 | C 4 | 202.79 | C 1 | 319.45 | C 2 | 450.87 | C 5 |
| 61.88 | C 1 | 203.96 | C 2 | 320.35 | C 5 | 464.21 | C 4 |
| 67.88 | C 1 | 209.42 | C 5 | 322.77 | C 4 | 466.10 | C 3 |
| 78.68 | C 2 | 211.44 | C 2 | 323.89 | C 5 | 466.32 | C 3 |
| 89.25 | C 2 | 212.15 | C 3 | 326.18 | C 1 | 468.33 | C 5 |
| 96.73 | C 1 | 219.26 | C 5 | 332.49 | C 3 | 485.42 | C 4 |
| 107.96 | C 4 | 219.83 | C 5 | 336.40 | C 3 | 486.10 | C 4 |
| 113.57 | C 1 | 222.17 | C 4 | 341.22 | C 4 | 490.04 | C 1 |
| 117.30 | C 2 | 223.68 | C 4 | 354.70 | C 1 | 490.37 | C 1 |
| 119.98 | C 2 | 224.57 | C 1 | 360.58 | C 3 | 491.49 | C 4 |
| 124.74 | C 2 | 226.39 | C 1 | 361.05 | C 1 | 492.86 | C 2 |
| 125.37 | C 3 | 229.76 | C 3 | 365.46 | C 4 | 494.52 | C 3 |
| 126.60 | C 1 | 237.22 | C 4 | 372.13 | C 3 | 495.03 | C 4 |
| 129.59 | C 1 | 247.40 | C 3 | 380.68 | C 1 | 495.29 | C 3 |
| 133.52 | C 2 | 257.93 | C 3 | 381.88 | C 3 | 495.50 | C 3 |
| 139.08 | C 3 | 259.89 | C 5 | 383.66 | C 4 | 498.06 | C 3 |
|  |  |  |  |  |  | 499.37 | C 3 |

DT Data Run \#2

| Time | Component Failure | Time | Component Failure | Time | Component Failure |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 4.36 | C2 | 131.29 | C2 | 344.14 | C5 |
| 4.51 | C1 | 134.68 | C3 | 345.53 | C1 |
| 6.77 | C4 | 146.27 | C4 | 351.96 | C2 |
| 7.22 | C1 | 147.67 | C5 | 353.05 | C3 |
| 8.43 | C1 | 150.14 | C5 | 359.08 | C2 |
| 12.33 | C3 | 151.84 | C1 | 368.48 | C1 |
| 12.69 | C5 | 157.55 | C4 | 372.65 | C5 |
| 18.40 | C5 | 162.11 | C5 | 372.68 | C2 |
| 19.66 | C4 | 165.01 | C4 | 379.50 | C4 |
| 20.53 | C3 | 165.05 | C1 | 383.91 | C3 |
| 21.38 | C3 | 166.16 | C3 | 387.88 | C2 |
| 22.73 | C4 | 167.51 | C1 | 390.46 | C5 |
| 25.95 | C3 | 168.83 | C2 | 398.52 | C5 |
| 27.04 | C4 | 173.24 | C5 | 409.40 | C1 |
| 29.43 | C2 | 174.81 | C2 | 413.68 | C3 |
| 37.07 | C1 | 176.95 | C2 | 416.10 | C2 |
| 43.19 | C5 | 195.96 | C1 | 416.42 | C4 |
| 50.09 | C3 | 196.87 | C4 | 418.07 | C1 |
| 52.26 | C5 | 198.22 | C4 | 418.60 | C5 |
| 64.90 | C4 | 199.84 | C3 | 424.48 | C1 |
| 76.03 | C5 | 202.09 | C1 | 426.34 | C4 |
| 79.50 | C4 | 215.72 | C5 | 427.27 | C2 |
| 83.22 | C3 | 228.84 | C5 | 433.87 | C3 |
| 86.45 | C1 | 228.97 | C3 | 436.88 | C5 |
| 89.05 | C1 | 229.03 | C1 | 437.44 | C3 |
| 90.71 | C3 | 229.58 | C1 | 439.65 | C2 |
| 94.35 | C5 | 230.82 | C1 | 442.77 | C2 |
| 95.79 | C1 | 241.36 | C1 | 443.83 | C2 |
| 95.87 | C5 | 271.43 | C1 | 443.93 | C3 |
| 96.05 | C3 | 274.81 | C5 | 446.19 | C4 |
| 97.80 | C5 | 282.22 | C1 | 451.99 | C4 |
| 109.38 | C3 | 282.96 | C1 | 456.79 | C4 |
| 110.57 | C4 | 287.80 | C4 | 457.42 | C4 |
| 111.47 | C1 | 289.59 | C4 | 467.93 | C3 |
| 117.46 | C3 | 290.93 | C5 | 473.89 | C1 |
| 117.48 | C2 | 308.02 | C5 | 477.44 | C3 |
| 119.12 | C1 | 310.90 | C3 | 477.97 | C5 |
| 119.12 | C4 | 313.61 | C1 | 481.49 | C4 |
| 123.30 | C4 | 335.89 | C3 | 486.24 | C4 |
| 124.37 | C2 | 337.22 | C4 | 490.82 | C5 |
| 126.57 | C5 | 337.25 | C4 | 497.27 | C5 |

## DT Data Run \#3

| Time | Component Failure | Time | Component Failure | Time | Component Failure |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2.96 | C2 | 209.14 | C3 | 363.63 | C5 |
| 4.04 | C2 | 215.08 | C4 | 370.63 | C3 |
| 5.75 | C4 | 220.14 | C3 | 370.89 | C5 |
| 12.68 | C2 | 221.98 | C1 | 376.93 | C2 |
| 16.24 | C2 | 227.31 | C3 | 380.55 | C3 |
| 33.59 | C1 | 231.32 | C5 | 380.57 | C5 |
| 37.24 | C1 | 238.67 | C2 | 385.48 | C1 |
| 38.44 | C1 | 240.93 | C5 | 386.03 | C4 |
| 48.96 | C2 | 241.09 | C5 | 387.73 | C5 |
| 55.34 | C3 | 241.26 | C2 | 397.54 | C2 |
| 68.16 | C2 | 244.01 | C4 | 403.20 | C1 |
| 69.77 | C2 | 244.84 | C2 | 404.23 | C1 |
| 79.30 | C4 | 245.51 | C1 | 408.53 | C1 |
| 81.39 | C1 | 247.55 | C4 | 408.92 | C3 |
| 85.81 | C4 | 262.06 | C5 | 410.34 | C3 |
| 86.40 | C2 | 263.28 | C5 | 411.08 | C5 |
| 88.56 | C4 | 267.35 | C3 | 412.12 | C2 |
| 90.60 | C5 | 268.55 | C4 | 412.25 | C5 |
| 97.14 | C5 | 268.64 | C5 | 418.46 | C2 |
| 97.65 | C3 | 273.88 | C5 | 418.58 | C5 |
| 103.04 | C4 | 275.38 | C1 | 422.00 | C2 |
| 103.96 | C3 | 275.81 | C2 | 426.65 | C3 |
| 137.42 | C1 | 277.54 | C4 | 429.11 | C4 |
| 140.36 | C5 | 278.22 | C1 | 429.70 | C1 |
| 147.29 | C1 | 278.93 | C2 | 430.40 | C2 |
| 148.69 | C3 | 279.98 | C3 | 431.59 | C5 |
| 149.72 | C2 | 286.78 | C2 | 434.30 | C4 |
| 149.80 | C3 | 291.53 | C5 | 434.67 | C1 |
| 152.45 | C3 | 300.53 | C3 | 438.59 | C1 |
| 153.95 | C1 | 301.34 | C5 | 441.21 | C4 |
| 163.35 | C4 | 310.11 | C2 | 450.70 | C4 |
| 164.02 | C1 | 326.98 | C3 | 457.12 | C 4 |
| 166.31 | C3 | 327.32 | C3 | 457.21 | C3 |
| 173.01 | C2 | 329.63 | C2 | 457.94 | C1 |
| 178.30 | C2 | 333.29 | C3 | 459.89 | C1 |
| 186.75 | C3 | 336.91 | C5 | 461.63 | C1 |
| 192.89 | C1 | 340.68 | C5 | 466.28 | C2 |
| 196.39 | C1 | 350.62 | C4 | 472.38 | C4 |
| 198.78 | C1 | 354.13 | C3 | 474.14 | C2 |
| 201.63 | C5 | 358.68 | C5 | 475.16 | C4 |
| 203.02 | C1 | 363.56 | C2 | 476.14 | C1 |
|  |  |  |  | 492.26 | C3 |

DT Data Run \#4

| Time | Component Failure | Time | Component Failure | Time | Component Failure |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 9.99 | C4 | 179.08 | C5 | 341.36 | C3 |
| 14.23 | C5 | 182.59 | C2 | 349.36 | C5 |
| 14.24 | C5 | 184.75 | C3 | 351.70 | C1 |
| 23.47 | C3 | 186.46 | C4 | 357.70 | C4 |
| 24.44 | C5 | 192.17 | C3 | 366.46 | C4 |
| 25.32 | C1 | 192.27 | C2 | 371.11 | C2 |
| 28.88 | C5 | 196.37 | C1 | 382.98 | C3 |
| 30.50 | C1 | 209.78 | C3 | 384.09 | C5 |
| 32.08 | C3 | 218.92 | C2 | 390.94 | C5 |
| 32.86 | C4 | 222.44 | C2 | 391.66 | C1 |
| 38.49 | C2 | 224.64 | C5 | 394.03 | C3 |
| 40.20 | C4 | 226.48 | C1 | 397.11 | C2 |
| 41.35 | C4 | 227.60 | C4 | 397.88 | C2 |
| 41.83 | C4 | 231.42 | C1 | 400.00 | C4 |
| 42.61 | C2 | 233.02 | C5 | 406.06 | C3 |
| 44.88 | C1 | 243.07 | C1 | 419.63 | C5 |
| 47.21 | C2 | 243.08 | C1 | 419.94 | C3 |
| 59.71 | C1 | 247.54 | C3 | 425.22 | C3 |
| 63.46 | C5 | 249.07 | C3 | 428.58 | C1 |
| 64.38 | C1 | 259.52 | C3 | 432.91 | C2 |
| 80.78 | C2 | 260.99 | C1 | 434.18 | C1 |
| 84.46 | C2 | 262.70 | C5 | 435.45 | C5 |
| 91.49 | C4 | 276.34 | C4 | 436.52 | C1 |
| 99.18 | C2 | 286.19 | C2 | 436.58 | C5 |
| 103.74 | C2 | 286.85 | C2 | 447.31 | C4 |
| 108.38 | C4 | 291.65 | C1 | 448.34 | C3 |
| 109.49 | C1 | 292.46 | C2 | 452.06 | C1 |
| 109.73 | C2 | 292.62 | C3 | 453.11 | C1 |
| 112.68 | C5 | 292.92 | C4 | 457.29 | C4 |
| 118.74 | C1 | 298.54 | C5 | 457.46 | C4 |
| 124.77 | C5 | 298.93 | C5 | 462.20 | C2 |
| 129.61 | C1 | 300.74 | C1 | 462.78 | C4 |
| 130.63 | C2 | 302.56 | C2 | 464.59 | C5 |
| 131.63 | C2 | 302.72 | C2 | 478.08 | C5 |
| 140.39 | C3 | 303.75 | C2 | 480.56 | C5 |
| 146.45 | C5 | 311.16 | C1 | 486.78 | C1 |
| 151.21 | C3 | 319.74 | C3 | 487.90 | C3 |
| 158.31 | C4 | 320.36 | C2 | 491.72 | C4 |
| 163.06 | C5 | 322.40 | C3 | 493.38 | C3 |
| 166.08 | C4 | 326.34 | C4 | 493.77 | C4 |
| 176.23 | C2 | 327.79 | C5 | 498.61 | C5 |
| 177.60 | C1 | 337.68 | C5 |  |  |

DT Data Run \#5

| Time | Fail | Time | Fail | Time | Fail | Time | Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.66 | C 1 | 100.21 | C 5 | 230.54 | C 1 | 361.06 | C 3 |
| 2.46 | C 1 | 101.18 | C 3 | 237.16 | C 3 | 362.47 | C 4 |
| 9.64 | C 3 | 107.58 | C 1 | 250.45 | C 3 | 362.49 | C 3 |
| 11.34 | C 2 | 108.34 | C 3 | 259.24 | C 5 | 366.30 | C 2 |
| 15.24 | C 5 | 110.96 | C 1 | 261.30 | C 3 | 372.01 | C 3 |
| 15.76 | C 2 | 113.82 | C 5 | 269.72 | C 2 | 379.40 | C 3 |
| 16.99 | C 1 | 116.24 | C 5 | 271.63 | C 3 | 387.26 | C 3 |
| 18.92 | C 4 | 136.24 | C 4 | 283.72 | C 1 | 387.52 | C 2 |
| 19.35 | C 1 | 136.89 | C 1 | 284.86 | C 3 | 394.09 | C 1 |
| 23.96 | C 1 | 137.38 | C 3 | 287.11 | C 3 | 398.00 | C 2 |
| 27.71 | C 5 | 143.38 | C 2 | 290.48 | C 1 | 402.96 | C 2 |
| 32.46 | C 3 | 144.89 | C 2 | 293.61 | C 1 | 408.64 | C 1 |
| 39.19 | C 4 | 146.83 | C 2 | 298.03 | C 5 | 412.57 | C 4 |
| 41.84 | C 4 | 148.11 | C 2 | 298.94 | C 4 | 413.73 | C 3 |
| 42.73 | C 3 | 148.17 | C 4 | 303.67 | C 5 | 418.63 | C 4 |
| 46.14 | C 1 | 150.91 | C 2 | 304.29 | C 3 | 424.71 | C 2 |
| 51.54 | C 1 | 153.87 | C 4 | 304.86 | C 2 | 429.67 | C 4 |
| 53.34 | C 4 | 157.99 | C 1 | 312.43 | C 3 | 429.92 | C 2 |
| 54.58 | C 5 | 159.91 | C 5 | 312.70 | C 5 | 432.24 | C 3 |
| 58.58 | C 2 | 165.49 | C 3 | 318.07 | C 1 | 432.71 | C 4 |
| 59.05 | C 1 | 166.48 | C 5 | 330.95 | C 2 | 449.61 | C 5 |
| 62.97 | C 4 | 170.87 | C 4 | 339.34 | C 4 | 457.91 | C 5 |
| 63.89 | C 3 | 177.89 | C 3 | 343.35 | C 4 | 462.61 | C 5 |
| 70.26 | C 3 | 181.20 | C 3 | 344.37 | C 5 | 462.62 | C 3 |
| 70.93 | C 2 | 182.23 | C 2 | 345.96 | C 3 | 465.37 | C 1 |
| 83.10 | C 1 | 184.71 | C 3 | 350.78 | C 5 | 469.82 | C 5 |
| 84.92 | C 4 | 199.68 | C 1 | 351.37 | C 4 | 485.61 | C 5 |
| 88.38 | C 3 | 201.85 | C 3 | 351.86 | C 1 | 491.02 | C 4 |
| 89.47 | C 2 | 214.69 | C 4 | 352.32 | C 4 | 492.67 | C 2 |
| 89.86 | C 1 | 218.13 | C 4 | 354.27 | C 4 | 496.42 | C 5 |
| 98.77 | C 2 | 221.07 | C 2 | 354.44 | C 1 | 499.68 | C 5 |
| 98.82 | C 3 | 223.39 | C 1 | 358.72 | C 3 |  |  |
| 99.94 | C 4 | 225.80 | C 5 | 360.41 | C 1 |  |  |

OT Data Runs \#1 and \#2

| OT Data Run \#1 |  | OT Data Run \#2 |  |
| :---: | :---: | :---: | :---: |
| Time | Component Failure | Time | Component Failure |
| 4.06 | C3 | 0.87 | C2 |
| 8.27 | C2 | 8.85 | C3 |
| 12.04 | C3 | 9.38 | C1 |
| 12.80 | C3 | 15.50 | C2 |
| 15.64 | C1 | 17.54 | C1 |
| 22.23 | C 2 | 19.63 | C2 |
| 35.98 | C3 | 28.30 | C2 |
| 36.82 | C3 | 29.50 | C1 |
| 39.57 | C5 | 33.68 | C2 |
| 39.80 | C2 | 40.37 | C4 |
| 44.76 | C5 | 42.48 | C4 |
| 52.07 | C1 | 44.47 | C4 |
| 52.25 | C1 | 47.61 | C5 |
| 59.55 | C5 | 58.12 | C3 |
| 62.05 | C4 | 69.32 | C5 |
| 63.94 | C5 | 76.44 | C1 |
| 65.86 | C3 | 76.90 | C5 |
| 71.46 | C1 | 79.17 | C3 |
| 77.51 | C4 | 87.49 | C5 |
| 78.45 | C2 | 90.62 | C5 |
| 80.02 | C1 | 98.37 | C3 |
| 88.39 | C3 | 103.75 | C1 |
| 89.69 | C2 | 116.16 | C3 |
| 93.16 | C1 | 120.20 | C4 |
| 95.46 | C5 | 120.63 | C3 |
| 104.13 | C1 | 120.82 | C1 |
| 108.31 | C5 | 122.92 | C1 |
| 108.52 | C2 |  |  |
| 114.59 | C4 |  |  |
| 123.77 | C3 |  |  |

Appendix J. Calculation For A Bridge System Reliability With Independent And Identical Components.

Consider a system composed of 5 independent and identical components given in Figure 1 (page 30). The time to failure of each component is assumed to be exponentially distributed. Let $\lambda=0.05$ failure per hour be the respective constant failure rates of each component.

For the true system, using a mission time, $t$ of one hour, the reliability of components $1,2,3,4$, and 5 are
$R_{c}=R_{1}=R_{2}=R_{3}=R_{4}=R_{5}=\exp (-0.05)=95.12 \%$.
The reliability of the system can be calculated as
$R_{5}=R_{1} R_{4}+R_{2} R_{5}+R_{1} R_{3} R_{5}+R_{2} R_{3} R_{4}-R_{1} R_{2} R_{3} R_{4}-R_{1} R_{2} R_{3} R_{5}-$ $R_{1} R_{2} R_{4} R_{5}-R_{1} R_{3} R_{4} R_{5}-R_{2} R_{3} R_{4} R_{5}+2 R_{1} R_{2} R_{3} R_{4} R_{5}=99.50 \%$.

Using a computer program called RAPTOR, which is developed by AFOTEC, to simulate the true system, the following data are obtained (to review the simulated data, see Appendix I):

Table J1: Aggregated Components DT Data

| Run $i$ | $T_{i}$ Hours | $X_{i}$ Failures | $\widehat{\lambda}_{i}=X_{i} / T_{i}$ |
| :---: | :---: | :---: | :---: |
| 1 | $2,496.85$ | 136 | 0.05447 |
| 2 | $2,486.35$ | 123 | 0.04947 |
| 3 | $2,461.3$ | 124 | 0.05038 |
| 4 | $2,493.05$ | 125 | 0.05014 |
| 5 | $2,498.4$ | 130 | 0.05203 |

Table J2: Aggregated Components OT Data

| Run $i$ | $T_{i}$ Hours | $X_{i}$ Failures | $\widehat{\lambda_{i}}=X_{i} / T_{i}$ |
| :---: | :---: | :---: | :---: |
| 1 | 618.85 | 30 | 0.04848 |
| 2 | 604.1 | 26 | 0.04304 |

Table J3: Component 1 DT Data

| Run $i$ | $T_{i}$ Hours | $X_{i}$ Failures | $\widehat{\lambda_{i}}=X_{i} / T_{i}$ |
| :---: | :---: | :---: | :---: |
| 1 | 499.37 | 32 | 0.06408 |
| 2 | 497.27 | 28 | 0.05631 |
| 3 | 492.26 | 27 | 0.05485 |
| 4 | 498.61 | 26 | 0.05215 |
| 5 | 499.68 | 27 | 0.05404 |

Table J4: Component 1 OT Data

| Run i | $\mathrm{T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures | $\widehat{\lambda_{i}}=\mathrm{X}_{\mathrm{i}} / \mathrm{T}_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: |
| 1 | 123.77 | 7 | 0.05656 |
| 2 | 120.82 | 6 | 0.04966 |

Table J5: Component 2 DT Data

| Run $i$ | $T_{i}$ Hours | $X_{i}$ Failures | $\hat{\lambda}_{i}=X_{i} / T_{i}$ |
| :---: | :---: | :---: | :---: |
| 1 | 499.37 | 21 | 0.04205 |
| 2 | 497.27 | 17 | 0.03419 |
| 3 | 492.26 | 28 | 0.05688 |
| 4 | 498.61 | 27 | 0.05415 |
| 5 | 499.68 | 23 | 0.04603 |

Table J6: Component 2 OT Data

| Run $i$ | $T_{i}$ Hours | $X_{i}$ Failures | $\hat{\lambda}_{i}=X_{i} / T_{i}$ |
| :---: | :---: | :---: | :---: |
| 1 | 123.77 | 6 | 0.04848 |
| 2 | 120.82 | 5 | 0.04138 |

Table J7: Component 3 DT Data

| Run i | $\mathrm{T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures | $\overline{\lambda_{i}}=\mathrm{X}_{\mathrm{i}} / \mathrm{T}_{i}$ |
| :---: | :---: | :---: | :---: |
| 1 | 499.37 | 35 | 0.07009 |
| 2 | 497.27 | 24 | 0.04826 |
| 3 | 492.26 | 25 | 0.05079 |
| 4 | 498.61 | 22 | 0.04412 |
| 5 | 499.68 | 33 | 0.06604 |

Table J8: Component 3 OT Data

| Run $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures | $\widehat{\lambda}_{i}=\mathrm{X}_{\mathrm{i}} / \mathrm{T}_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: |
| 1 | 123.77 | 8 | 0.06464 |
| 2 | 120.82 | 6 | 0.04966 |

Table J9: Component 4 DT Data

| Run $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures | $\widehat{\lambda_{i}}=\mathrm{X}_{i} / \mathrm{T}_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: |
| 1 | 499.37 | 25 | 0.05006 |
| 2 | 497.27 | 27 | 0.05430 |
| 3 | 492.26 | 20 | 0.04063 |
| 4 | 498.61 | 23 | 0.04613 |
| 5 | 499.68 | 25 | 0.05003 |

Table J10: Component 4 OT Data

| Run $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures | $\widehat{\lambda_{i}}=\mathrm{X}_{\mathrm{i}} / \mathrm{T}_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: |
| 1 | 123.77 | 3 | 0.02424 |
| 2 | 120.82 | 4 | 0.03311 |

Table J11: Component 5 DT Data

| Run $i$ | $T_{i}$ Hours | $X_{i}$ Failures | $\hat{\lambda}_{i}=X_{i} / T_{i}$ |
| :---: | :---: | :---: | :---: |
| 1 | 499.37 | 23 | 0.04606 |
| 2 | 497.27 | 27 | 0.05430 |
| 3 | 492.26 | 24 | 0.04876 |
| 4 | 498.61 | 27 | 0.05415 |
| 5 | 499.68 | 22 | 0.04403 |

Table J12: Component 5 OT Data

| Run $i$ | $T_{i}$ Hours | $X_{i}$ Failures | $\widehat{\lambda_{i}}=X_{i} / T_{i}$ |
| :---: | :---: | :---: | :---: |
| 1 | 123.77 | 6 | 0.04848 |
| 2 | 120.82 | 5 | 0.04138 |

The Classical Exponential Method.
Assuming the time to failure of each component has the exponential distribution, point estimates for the failure rate $\lambda$ and $80 \%$ confidence intervals about $\lambda$ will be computed.

Component Aggregated DT: $\hat{\lambda}=\left(\frac{638}{12435.95}\right)=0.05130$
Component Aggregated OT: $\hat{\lambda}=\left(\frac{56}{1222.95}\right)=\mathbf{0 . 0 4 5 7 9}$

Component 1 DT: $\hat{\lambda}=\left(\frac{f_{3}}{T_{3}}\right)=\left(\frac{140}{2487.19}\right)=0.05629$
Component 1 OT: $\hat{\lambda}=\left(\frac{f_{4}}{T_{4}}\right)=\left(\frac{13}{244.59}\right)=0.05315$
Component $2 \mathrm{DT}: \hat{\lambda}=\left(\frac{f_{5}}{T_{5}}\right)=\left(\frac{116}{2487.19}\right)=0.04664$
Component 2 OT: $\hat{\lambda}=\left(\frac{f_{6}}{T_{6}}\right)=\left(\frac{11}{244.59}\right)=0.04497$
Component $3 \mathrm{DT}: \quad \hat{\lambda}=\left(\frac{f_{7}}{T_{7}}\right)=\left(\frac{139}{2487.19}\right)=0.05589$
Component 3 OT: $\hat{\lambda}=\left(\frac{f_{8}}{T_{8}}\right)=\left(\frac{14}{244.59}\right)=0.05724$
Component 4 DT: $\quad \hat{\lambda}=\left(\frac{f_{g}}{T_{9}}\right)=\left(\frac{120}{2487.19}\right)=0.04825$
Component 4 OT: $\hat{\lambda}=\left(\frac{f_{10}}{T_{10}}\right)=\left(\frac{7}{244.59}\right)=0.02862$
Component $5 \mathrm{DT}: \quad \hat{\lambda}=\left(\frac{f_{11}}{T_{11}}\right)=\left(\frac{123}{2487.19}\right)=0.04945$
Component 5 OT: $\hat{\lambda}=\left(\frac{f_{12}}{T_{12}}\right)=\left(\frac{11}{244.59}\right)=0.04497$
where $f_{1}=638$ is the number of failures and $T_{1}=12435.95$ is the total test time from Table $J 1, f_{2}=56$ and $T_{2}=$ 1222.95 from Table J2, $f_{3}=140$ and $T_{3}=2487.19$ from Table J3, $f_{4}=13$ and $T_{4}=244.59$ from Table J4, $f_{5}=116$ and $T_{5}=$ 2487.19 from Table $\mathrm{J} 5, f_{6}=11$ and $T_{6}=244.59$ from Table J6, $f_{7}=139$ and $T_{7}=2487.19$ from Table J7, $f_{8}=14$ and $T_{8}=$ 244.59 from Table J8, $f_{9}=120$ and $T_{9}=2487.19$ from Table J9, $f_{10}=7$ and $T_{10}=244.59$ from Table J10, $f_{11}=123$ and $T_{11}$
$=2487.19$ from Table J11, $f_{12}=11$ and $T_{12}=244.59$ from Table J12.

The $80 \%$ two-sided confidence intervals (TCI) are
Component Agaregated DT: (0.04872,0.05392)
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 638)}{2 \times 12435.95}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 638)}{2 \times 12435.95}\right)=\left(\frac{1211.7}{24871.9}, \frac{1341.15}{24871.9}\right)$
Component Aggregated OT: $(0.03815,0.05379)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 56)}{2 \times 1222.95}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 56)}{2 \times 1222.95}\right)=\left(\frac{93.3}{2445.9}, \frac{131.56}{2445.9}\right)$
Component 1 DT: $(0.05028,0.06247)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 140)}{2 \times 2487.19}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 140)}{2 \times 2487.19}\right)=\left(\frac{250.13}{4974.38}, \frac{310.72}{4974.38}\right)$
Component 1 OT: $(0.03535,0.07270)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 13)}{2 \times 244.59}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 13)}{2 \times 244.59}\right)=\left(\frac{17.29}{489.18}, \frac{35.56}{489.18}\right)$
Component 2 DT: ( $0.04118,0.05227)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 116)}{2 \times 2487.19}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 116)}{2 \times 2487.19}\right)=\left(\frac{204.86}{4974.38}, \frac{260}{4974.38}\right)$
Component 2 OT: $(0.02870,0.06299)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 11)}{2 \times 244.59}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 11)}{2 \times 244.59}\right)=\left(\frac{14.04}{489.18}, \frac{30.81}{489.18}\right)$
Component 3 DT: $(0.04990,0.06204)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 139)}{2 \times 2487.19}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 139)}{2 \times 2487.19}\right)=\left(\frac{248.24}{4974.38}, \frac{308.61}{4974.38}\right)$
Component $3 \mathrm{OT}:(0.03872,0.07751)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 14)}{2 \times 244.59}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 14)}{2 \times 244.59}\right)=\left(\frac{18.94}{489.18}, \frac{37.92}{489.18}\right)$
Component $4 \mathrm{DT}:(0.04270,0.05397)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 120)}{2 \times 2487.19}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 120)}{2 \times 2487.19}\right)=\left(\frac{212.39}{4974.38}, \frac{268.47}{4974.38}\right)$
Component 4 OT: $(0.01592,0.04306)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 7)}{2 \times 244.59}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 7)}{2 \times 244.59}\right)=\left(\frac{7.79}{489.18}, \frac{21.06}{489.18}\right)$
Component 5 DT: $(0.04383,0.05525)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 123)}{2 \times 2487.19}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 123)}{2 \times 2487.19}\right)=\left(\frac{218.04}{4974.38}, \frac{274.82}{4974.38}\right)$
Component $5 \mathrm{OT}:(0.02870,0.06912)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 11)}{2 \times 244.59}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 11)}{2 \times 244.59}\right)=\left(\frac{14.04}{489.18}, \frac{33.81}{489.18}\right)$.
The reliability estimators of $R(t)$ for $t=1$ hour are
Component Agaregated DT:
$\widehat{R_{c}}(t)=\exp (-0.05130 \times 1)=95.00 \%$
Component Agqreqated OT:
$\widehat{R_{c}}(t)=\exp (-0.04579 \times 1)=95.52 \%$
Component $1 \mathrm{DT}: \widehat{R_{1}}(t)=\exp (-0.05629 \times 1)=94.53 \%$
Component 1 OT: $\widehat{R_{1}}(t)=\exp (-0.05315 \times 1)=\mathbf{9 4 . 8 2 \%}$
Component 2 DT: $\widehat{R_{2}}(t)=\exp (-0.04664 \times 1)=95.44 \%$
Component $2 \mathrm{OT}: \widehat{R_{2}}(t)=\exp (-0.04497 \times 1)=95.60 \%$
Component $3 \mathrm{DT}: \widehat{R_{3}}(t)=\exp (-0.05589 \times 1)=94.57 \%$

Component 3 OT: $\widehat{R_{3}}(t)=\exp (-0.05724 \times 1)=94.44 \%$
Component $4 \mathrm{DT}: \widehat{R_{4}}(t)=\exp (-0.04825 \times 1)=95.29 \%$
Component 4 OT: $\widehat{R_{4}}(t)=\exp (-0.02862 \times 1)=97.18 \%$
Component $5 \mathrm{DT}: \widehat{R_{5}}(t)=\exp (-0.04945 \times 1)=95.18 \%$
Component 5 OT: $\widehat{R_{5}}(t)=\exp (-0.04497 \times 1)=95.60 \%$
Substitute the appropriate values into $\widehat{R}(t)=R_{1} R_{4}+R_{2} R_{5}$ $+R_{1} R_{3} R_{5}+R_{2} R_{3} R_{4}-R_{1} R_{2} R_{3} R_{4}-R_{1} R_{2} R_{3} R_{5}-R_{1} R_{2} R_{4} R_{5}-R_{1} R_{3} R_{4} R_{5}-$ $R_{2} R_{3} R_{4} R_{5}+2 R_{1} R_{2} R_{3} R_{4} R_{5}$ to obtained the following:

Agaregated Component to System DT: $\widehat{R}(t)=99.48 \%$
Aggregated Component to System OT: $\widehat{R}(t)=99.58 \%$
Component Level Aggregated to System DT: $\widehat{R}(t)=99.50 \%$
Component Level Aggreqated to System $\mathrm{OT}: \widehat{R}(t)=99.63 \%$.
The $80 \%$ two-sided confidence intervals (TCI) are
Agareqated Component DT: (94.75\%,95.25\%)
$\exp (-0.05392 \times 1) \leq \widehat{R}(1) \leq \exp (-0.04872 \times 1)$
Aggregated Component $O T:(94.76 \%, 96.26 \%)$
$\exp (-0.05379 \times 1) \leq \widehat{R}(1) \leq \exp (-0.03815 \times 1)$
Component 1 DT: (93.95\%,95.10\%)
$\exp (-0.06247 \times 1) \leq \widehat{R}(1) \leq \exp (-0.05028 \times 1)$
Component 1 OT: ( $92.99 \%, 96.53 \%$ )
$\exp (-0.07270 \times 1) \leq \widehat{R}(1) \leq \exp (-0.03535 \times 1)$
Component 2 DT: (94.91\%,95.97\%)
$\exp (-0.05227 \times 1) \leq \widehat{R}(1) \leq \exp (-0.04118 \times 1)$
Component 2 OT: (93.90\%,97.17\%)
$\exp (-0.06299 \times 1) \leq \widehat{R}(1) \leq \exp (-0.02870 \times 1)$
Component 3 DT: (93.99\%,95.13\%)
$\exp (-0.06204 \times 1) \leq \widehat{R}(1) \leq \exp (-0.04990 \times 1)$
Component 3 OT: ( $92.54 \%, 96.20 \%$ )
$\exp (-0.07751 \times 1) \leq \widehat{R}(1) \leq \exp (-0.03872 \times 1)$
Component 4 DT: ( $94.75 \%, 95.82 \%$ )
$\exp (-0.05397 \times 1) \leq \widehat{R}(1) \leq \exp (-0.04270 \times 1)$
Component 4 OT: (95.79\%,98.42\%)
$\exp (-0.04306 \times 1) \leq \widehat{R}(1) \leq \exp (-0.01592 \times 1)$
Component 5 DT: ( $94.63 \%, 95.71 \%$ )
$\exp (-0.05525 \times 1) \leq \widehat{R}(1) \leq \exp (-0.04383 \times 1)$
Component 5 OT: (93.32\%,97.17\%)
$\exp (-0.06912 \times 1) \leq \widehat{R}(1) \leq \exp (-0.02870 \times 1)$
Substitute the appropriate values into $\widehat{R}(t)=R_{1} R_{4}+R_{2} R_{5}$ $+R_{1} R_{3} R_{5}+R_{2} R_{3} R_{4}-R_{1} R_{2} R_{3} R_{4}-R_{1} R_{2} R_{3} R_{5}-R_{1} R_{2} R_{4} R_{5}-R_{1} R_{3} R_{4} R_{5}-$ $R_{2} R_{3} R_{4} R_{5}+2 R_{1} R_{2} R_{3} R_{4} R_{5}$ to obtained the following:

Aggregated Component to System DT: (99.42\%,99.53\%)
Agaregated Component to System OT: (99.43\%,99.71\%)
Component Level Aggregated to System DT:
(99.38\%, 99.61\%)

Component Level Aggregated to System OT:
(99.24\%, 99.85\%).

The Bayesian Exponential Method.
Bayesian Exponential Prior.
For the component aggregated data, from Table JI:
$\widehat{E}(\lambda)=\bar{\lambda}=0.051298$ and $\widehat{V}(\lambda)=s_{\lambda}{ }^{2}=0.000004$.

These yielded the parameter estimates
$\alpha=\left(\frac{0.051298^{2}}{0.000004}\right)=657.87$ and $\beta=\left(\frac{0.051298}{0.000004}\right)=12824.5$.
For Component 1 data, from Table J3:
$\widehat{E}(\lambda)=\bar{\lambda}=0.05628$ and $\widehat{V}(\lambda)=s_{\lambda}{ }^{2}=0.00002$.
These yielded the parameter estimates
$\alpha=\left(\frac{0.05628^{2}}{0.00002}\right)=150.85$ and $\beta=\left(\frac{0.05628}{0.00002}\right)=2680.14$.
For Component 2 data, from Table J5:
$\widehat{E}(\lambda)=\bar{\lambda}=0.04666$ and $\widehat{V}(\lambda)=s_{\lambda}{ }^{2}=0.00008$.
These yielded the parameter estimates
$\alpha=\left(\frac{0.04666^{2}}{0.00008}\right)=25.92$ and $\beta=\left(\frac{0.04666}{0.00008}\right)=555.48$.
For Component 3 data, from Table J7:
$\widehat{E}(\lambda)=\bar{\lambda}=0.05586$ and $\widehat{V}(\lambda)=s_{\lambda}{ }^{2}=0.00013$.
These yielded the parameter estimates
$\alpha=\left(\frac{0.05586^{2}}{0.00013}\right)=23.64$ and $\beta=\left(\frac{0.05586}{0.00013}\right)=423.19$.
For Component 4 data, from Table J9:
$\widehat{E}(\lambda)=\bar{\lambda}=0.04823$ and $\widehat{V}(\lambda)=s_{\lambda}{ }^{2}=0.00003$.
These yielded the parameter estimates
$\alpha=\left(\frac{0.04823^{2}}{0.00003}\right)=89.47$ and $\beta=\left(\frac{0.04823}{0.00003}\right)=1855$.
For Component 5 data, from Table J11:
$\widehat{E}(\lambda)=\bar{\lambda}=0.04946$ and $\widehat{V}(\lambda)=s_{\lambda}{ }^{2}=0.00002$.
These yielded the parameter estimates
$\alpha=\left(\frac{0.04946^{2}}{0.00002}\right)=111.19$ and $\beta=\left(\frac{0.04946}{0.00002}\right)=2248.09$.
Bayesian Exponential Posterior Analysis.
Aggregated Component: $\hat{\lambda}=\left(\frac{56+657.87}{1222.95+12824.5}\right)=0.05082$.
Component 1: $\hat{\lambda}=\left(\frac{13+150.85}{244.59+2680.14}\right)=0.05602$.
Component 2 $: \hat{\lambda}=\left(\frac{11+25.92}{244.59+555.48}\right)=0.04614$.
Component 3: $\hat{\lambda}=\left(\frac{14+23.64}{244.59+423.19}\right)=0.05637$.
Component 4: $\hat{\lambda}=\left(\frac{7+89.47}{244.59+1855}\right) \quad=0.04595$.
Component 5: $\hat{\lambda}=\left(\frac{11+111.19}{244.59+2248.09}\right)=0.04902$.
The 80\% two-sided probability intervals (TBPI) are
Aggregated Component:
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 56+2 \times 657.87)}{2(1222.95+12824.5)}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 56+2 \times 657.87)}{2(1222.95+12824.5)}\right)$
$=\left(\frac{1359.7}{28094.9}, \frac{1496.64}{28094.9}\right)=(0.04840,0.05327)$.

Component $1:\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 13+2 \times 150.85)}{2(244.59+2680.14)}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 13+2 \times 150.85)}{2(244.59+2680.14)}\right)$
$=\left(\frac{294.68}{5849.46}, \frac{360.17}{5849.46}\right)=(0.05038,0.06157)$.
Component 2: $\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 11+2 \times 25.92)}{2(244.59+555.48)}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 11+2 \times 25.92)}{2(244.59+555.48)}\right)$
$=\left(\frac{58.01}{1600.14}, \frac{88.85}{1600.14}\right)=(0.03625,0.05553)$.
Component 3: $\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 14+2 \times 23.64)}{2(244.59+423.19)}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 14+2 \times 23.64)}{2(244.59+423.19)}\right)$
$=\left(\frac{59.8}{1335.56}, \frac{91.06}{1335.56}\right)=(0.04477,0.06818)$.
Component 4 : $\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 7+2 \times 89.47)}{2(244.59+1855)}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 7+2 \times 89.47)}{2(244.59+1855)}\right)$
$=\left(\frac{167.35}{4199.18}, \frac{217.5}{4199.18}\right)=(0.03985,0.05180)$.
Component 5: $\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 11+2 \times 111.19)}{2(244.59+2248.09)}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 11+2 \times 111.19)}{2(244.59+2248.09)}\right)$
$=\left(\frac{216.15}{4985.36}, \frac{272.7}{4985.36}\right)=(0.04336,0.05470)$.
The Bayesian estimators of $R(t)$ for $t=1$ hour are Aggregated Component: $\widehat{R}(t)=95.05 \%$

$$
\widehat{R}(t)=\left(\frac{\left(\frac{1222.95}{12824.5}\right)+1}{\left(\frac{1222.95}{12824.5}\right)+\left(\frac{1}{12824.5}\right)+1}\right)^{657.87+56}
$$

Component 1: $\widehat{R}(t)=94.55 \%$

$$
\widehat{R}(t)=\left(\frac{\left(\frac{244.59}{2680.14}\right)+1}{\left(\frac{244.59}{2680.14}\right)+\left(\frac{1}{2680.14}\right)+1}\right)^{150.85+13}
$$

Component 2: $\widehat{R}(t)=\mathbf{9 5 . 4 9 \%}$

$$
\widehat{R}(t)=\left(\frac{\left(\frac{244.59}{555.48}\right)+1}{\left(\frac{244.59}{555.48}\right)+\left(\frac{1}{555.48}\right)+1}\right)^{25.92+11}
$$

Component 3: $\widehat{R}(t)=94.52 \%$

$$
\widehat{R}(t)=\left(\frac{\left(\frac{244.59}{423.19}\right)+1}{\left(\frac{244.59}{423.19}\right)+\left(\frac{1}{423.19}\right)+1}\right)^{23.64+14}
$$

Component 4: $\widehat{R}(t)=95.51 \%$

$$
\widehat{R}(t)=\left(\frac{\left(\frac{244.59}{1855}\right)+1}{\left(\frac{244.59}{1855}\right)+\left(\frac{1}{1855}\right)+1}\right)^{89.47+7}
$$

Component 5: $\widehat{R}(t)=\mathbf{9 5 . 2 2 \%}$

$$
\widehat{R}(t)=\left(\frac{\left(\frac{244.59}{2248.09}\right)+1}{\left(\frac{244.59}{2248.09}\right)+\left(\frac{1}{2248.09}\right)+1}\right)^{111.19+11}
$$

Substitute the appropriate values into $\widehat{R}(t)=R_{1} R_{4}+R_{2} R_{5}$ $+R_{1} R_{3} R_{5}+R_{2} R_{3} R_{4}-R_{1} R_{2} R_{3} R_{4}-R_{1} R_{2} R_{3} R_{5}-R_{1} R_{2} R_{4} R_{5}-R_{1} R_{3} R_{4} R_{5}-$ $R_{2} R_{3} R_{4} R_{5}+2 R_{1} R_{2} R_{3} R_{4} R_{5}$ to obtained the following:

Aggregated Component to System: $\widehat{R}(t)=99.49 \%$
Component Level Aggregated to System: $\widehat{R}(t)=\mathbf{9 9 . 5 2 \%}$.
The $80 \%$ two-sided probability intervals (TBPI) are
Aggregated Component: $(\mathbf{9 4 . 8 1 \%} \leq \widehat{R}(1) \leq 95.28 \%)$
$\exp (-0.05327 \times 1) \leq \widehat{R}(1) \leq \exp (-0.04840 \times 1)$.
Component 1: $(94.03 \% \leq \widehat{R}(1) \leq 95.09 \%)$
$\exp (-0.06157 \times 1) \leq \widehat{R}(1) \leq \exp (-0.05038 \times 1)$.
Component 2: $(94.60 \% \leq \widehat{R}(1) \leq 96.44 \%)$
$\exp (-0.05553 \times 1) \leq \widehat{R}(1) \leq \exp (-0.03625 \times 1)$.
Component 3: $\quad(93.41 \% \leq \widehat{R}(1) \leq 95.62 \%)$
$\exp (-0.06818 \times 1) \leq \widehat{R}(1) \leq \exp (-0.04477 \times 1)$.
Component 4: $(94.95 \% \leq \widehat{R}(1) \leq 96.09 \%)$
$\exp (-0.05180 \times 1) \leq \widehat{R}(1) \leq \exp (-0.03985 \times 1)$.
Component 5: $(94.68 \% \leq \widehat{R}(1) \leq 95.76 \%)$
$\exp (-0.05470 \times 1) \leq \widehat{R}(1) \leq \exp (-0.04336 \times 1)$.
Substitute the appropriate values into $\widehat{R}(t)=R_{1} R_{4}+R_{2} R_{5}$
$+R_{1} R_{3} R_{5}+R_{2} R_{3} R_{4}-R_{1} R_{2} R_{3} R_{4}-R_{1} R_{2} R_{3} R_{5}-R_{1} R_{2} R_{4} R_{5}-R_{1} R_{3} R_{4} R_{5}-$ $\mathrm{R}_{2} \mathrm{R}_{3} \mathrm{R}_{4} \mathrm{R}_{5}+2 \mathrm{R}_{1} \mathrm{R}_{2} \mathrm{R}_{3} \mathrm{R}_{4} \mathrm{R}_{5}$ to obtained the following:

Aggregated Component to System: (99.44\%,99.54\%)
Component Level Agaregated to System: (99.38\%,99.65\%).

Appendix K. Simulated Data For A Bridge System With
Different Independent Components.

## DT Data Run \#1

| Time | Fail | Time | Fail | Time | Fail | Time | Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6.03 | C 1 | 134.00 | C 1 | 246.06 | C 4 | 368.17 | C 5 |
| 16.66 | C 5 | 135.49 | C 1 | 250.50 | C 3 | 370.91 | C 4 |
| 18.06 | C 3 | 149.91 | C 1 | 253.23 | C 3 | 378.72 | C 4 |
| 18.58 | C 1 | 153.05 | C 1 | 261.18 | C 1 | 382.44 | C 1 |
| 31.40 | C 3 | 153.22 | C 3 | 267.25 | C 5 | 382.74 | C 3 |
| 31.68 | C 3 | 154.03 | C 3 | 270.00 | C 1 | 392.26 | C 3 |
| 33.15 | C 1 | 154.61 | C 2 | 273.13 | C 4 | 394.56 | C 1 |
| 33.23 | C 2 | 154.88 | C 1 | 275.26 | C 1 | 404.38 | C 1 |
| 36.88 | C 2 | 168.43 | C 4 | 278.04 | C 4 | 409.59 | C 3 |
| 39.22 | C 3 | 174.94 | C 1 | 283.04 | C 2 | 413.48 | C 1 |
| 46.64 | C 1 | 178.08 | C 1 | 283.18 | C 1 | 418.01 | C 2 |
| 51.07 | C 5 | 185.65 | C 1 | 285.32 | C 2 | 424.22 | C 3 |
| 51.28 | C 1 | 190.69 | C 3 | 285.89 | C 2 | 425.01 | C 1 |
| 56.41 | C 5 | 198.01 | C 1 | 292.50 | C 2 | 427.08 | C 4 |
| 57.23 | C 5 | 199.16 | C 1 | 300.20 | C 4 | 430.78 | C 2 |
| 58.75 | C 5 | 201.52 | C 1 | 309.56 | C 1 | 436.65 | C 3 |
| 58.89 | C 4 | 204.01 | C 1 | 313.11 | C 4 | 439.46 | C 5 |
| 67.14 | C 4 | 204.54 | C 2 | 317.32 | C 4 | 440.66 | C 2 |
| 73.58 | C 4 | 213.75 | C 1 | 319.43 | C 3 | 447.63 | C 1 |
| 77.80 | C 5 | 214.40 | C 2 | 329.52 | C 1 | 453.97 | C 1 |
| 90.92 | C 1 | 219.63 | C 2 | 332.56 | C 1 | 454.82 | C 5 |
| 92.80 | C 5 | 220.05 | C 3 | 334.78 | C 1 | 456.28 | C 3 |
| 105.35 | C 1 | 221.16 | C 1 | 335.50 | C 3 | 462.14 | C 1 |
| 107.39 | C 3 | 222.58 | C 2 | 339.62 | C 1 | 464.38 | C 1 |
| 119.24 | C 5 | 223.35 | C 4 | 344.19 | C 3 | 468.20 | C 1 |
| 119.37 | C 1 | 230.07 | C 2 | 346.51 | C 1 | 474.33 | C 1 |
| 125.88 | C 1 | 232.06 | C 1 | 349.14 | C 1 | 475.25 | C 5 |
| 127.22 | C 1 | 240.86 | C 1 | 353.52 | C 2 | 478.31 | C 2 |
| 129.60 | C 1 | 241.15 | C 1 | 355.06 | C 3 | 479.17 | C 1 |
| 132.66 | C 3 | 243.04 | C 4 | 357.07 | C 2 | 499.09 | C 2 |


| Time | Component <br> Failure | Time | Component <br> Failure | Time <br> Component <br> Failure |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 11.59 | C 1 | 171.92 | C 1 | 285.74 | C 1 |
| 12.80 | C 1 | 179.22 | C 1 | 286.81 | C 1 |
| 17.46 | C 2 | 181.59 | C 2 | 299.44 | C 2 |
| 27.87 | C 1 | 188.38 | C 1 | 305.57 | C 2 |
| 35.62 | C 1 | 190.77 | C 3 | 306.92 | C 2 |
| 39.53 | C 1 | 192.12 | C 1 | 313.42 | C 3 |
| 40.82 | C 2 | 194.66 | C 3 | 326.50 | C 5 |
| 42.43 | C 4 | 195.49 | C 1 | 357.10 | C 3 |
| 43.35 | C 5 | 196.26 | C 1 | 369.98 | C 4 |
| 46.11 | C 5 | 202.67 | C 3 | 374.32 | C 1 |
| 58.12 | C 2 | 204.10 | C 1 | 376.79 | C 3 |
| 61.71 | C 2 | 205.55 | C 3 | 377.61 | C 3 |
| 65.11 | C 1 | 206.34 | C 4 | 379.47 | C 3 |
| 68.73 | C 4 | 210.76 | C 1 | 393.84 | C 5 |
| 71.05 | C 3 | 211.40 | C 5 | 395.29 | C 3 |
| 77.82 | C 3 | 212.66 | C 2 | 396.50 | C 2 |
| 83.59 | C 1 | 215.04 | C 1 | 411.47 | C 3 |
| 89.93 | C 1 | 218.49 | C 1 | 412.58 | C 3 |
| 91.82 | C 2 | 222.49 | C 4 | 412.62 | C 2 |
| 94.53 | C 2 | 229.88 | C 2 | 414.42 | C 2 |
| 96.31 | C 3 | 230.52 | C 5 | 415.28 | C 1 |
| 98.13 | C 3 | 230.85 | C 4 | 423.83 | C 1 |
| 102.47 | C 1 | 234.85 | C 1 | 441.89 | C 1 |
| 106.57 | C 1 | 247.80 | C 5 | 454.39 | C 1 |
| 107.42 | C 2 | 248.72 | C 3 | 458.56 | C 3 |
| 109.43 | C 1 | 252.85 | C 2 | 461.91 | C 4 |
| 110.96 | C 1 | 253.62 | C 1 | 461.98 | C 4 |
| 111.38 | C 1 | 255.32 | C 2 | 462.04 | C 2 |
| 113.66 | C 1 | 259.60 | C 1 | 469.00 | C 5 |
| 115.82 | C 1 | 263.34 | C 1 | 470.35 | C 1 |
| 116.73 | C 5 | 265.63 | C 3 | 473.91 | C 1 |
| 127.89 | C 1 | 268.53 | C 2 | 484.30 | C 3 |
| 132.20 | C 2 | 268.90 | C 1 | 489.34 | C 1 |
| 140.65 | C 4 | 270.99 | C 2 | 490.55 | C 2 |
| 141.09 | C 3 | 273.04 | C 4 |  |  |
| 158.80 | C 4 | 285.02 | C 4 |  |  |
|  |  |  |  |  |  |

## DT Data Run \#3

| Time | Component <br> Failure | Time | Component <br> Failure | Time | Component <br> Failure |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1.41 | C 1 | 160.90 | C 2 | 375.72 | C 3 |
| 7.29 | C 3 | 169.54 | C 2 | 380.98 | C 3 |
| 8.93 | C 1 | 180.54 | C 1 | 384.56 | C 3 |
| 15.20 | C 2 | 182.31 | C 1 | 390.91 | C 3 |
| 23.93 | C 2 | 198.68 | C 1 | 391.00 | C 1 |
| 24.83 | C 2 | 200.50 | C 1 | 391.32 | C 2 |
| 38.72 | C 1 | 201.10 | C 1 | 400.48 | C 1 |
| 46.53 | C 1 | 220.33 | C 4 | 402.32 | C 2 |
| 50.34 | C 1 | 222.58 | C 1 | 404.66 | C 5 |
| 51.13 | C 2 | 231.44 | C 5 | 408.31 | C 4 |
| 59.72 | C 1 | 235.47 | C 5 | 409.49 | C 2 |
| 65.58 | C 1 | 243.10 | C 2 | 414.94 | C 1 |
| 70.22 | C 5 | 243.74 | C 1 | 416.24 | C 1 |
| 73.84 | C 4 | 249.61 | C 2 | 416.31 | C 1 |
| 77.92 | C 2 | 252.36 | C 2 | 419.10 | C 2 |
| 80.99 | C 3 | 258.72 | C 4 | 422.68 | C 2 |
| 80.99 | C 2 | 271.75 | C 1 | 426.22 | C 2 |
| 81.05 | C 3 | 275.02 | C 1 | 426.80 | C 1 |
| 83.69 | C 2 | 277.05 | C 5 | 435.44 | C 3 |
| 88.17 | C 1 | 287.67 | C 4 | 441.74 | C 1 |
| 90.51 | C 1 | 292.83 | C 5 | 442.35 | C 1 |
| 96.39 | C 1 | 295.49 | C 3 | 445.02 | C 1 |
| 103.22 | C 1 | 296.63 | C 1 | 451.33 | C 1 |
| 103.60 | C 2 | 310.30 | C 3 | 455.83 | C 1 |
| 105.91 | C 1 | 315.67 | C 2 | 457.19 | C 2 |
| 112.90 | C 1 | 316.78 | C 2 | 458.45 | C 1 |
| 116.65 | C 2 | 320.29 | C 3 | 459.87 | C 1 |
| 126.22 | C 2 | 324.26 | C 3 | 461.43 | C 1 |
| 127.22 | C 1 | 327.27 | C 1 | 463.48 | C 5 |
| 144.20 | C 3 | 332.30 | C 1 | 466.94 | C 3 |
| 145.90 | C 2 | 340.06 | C 2 | 474.84 | C 2 |
| 147.47 | C 5 | 345.05 | C 3 | 478.73 | C 3 |
| 152.86 | C 1 | 358.16 | C 1 | 488.40 | C 4 |
| 159.59 | C 3 | 360.81 | C 1 | 495.40 | C 2 |
| 159.82 | C 2 | 368.93 | C 2 | 497.97 | C 1 |

## DT Data Run \#4

| Time | Component Failure | Time | Component Failure | Time | Component Failure |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0.22 | C1 | 147.31 | C2 | 309.30 | C2 |
| 0.67 | C4 | 152.25 | C4 | 320.00 | C1 |
| 3.65 | C1 | 158.28 | C5 | 326.05 | C1 |
| 16.32 | C1 | 167.07 | C5 | 330.21 | C2 |
| 19.52 | C2 | 169.02 | C3 | 330.35 | C5 |
| 30.00 | C5 | 174.94 | C2 | 331.48 | C1 |
| 38.34 | C1 | 183.38 | C1 | 331.98 | C1 |
| 40.80 | C2 | 186.99 | C1 | 351.89 | C 2 |
| 46.32 | C1 | 187.80 | C4 | 354.28 | C1 |
| 49.32 | C2 | 189.02 | C5 | 361.43 | C4 |
| 50.08 | C3 | 189.94 | C4 | 362.59 | C1 |
| 55.09 | C1 | 191.47 | C1 | 362.72 | C2 |
| 64.39 | C4 | 199.83 | C2 | 366.47 | C1 |
| 65.60 | C1 | 203.21 | C1 | 376.66 | C1 |
| 66.95 | C1 | 210.58 | C3 | 378.74 | C2 |
| 67.51 | C1 | 210.59 | C3 | 379.84 | C1 |
| 74.37 | C5 | 214.07 | C2 | 388.36 | C3 |
| 75.71 | C1 | 214.64 | C1 | 397.50 | C2 |
| 78.55 | C1 | 216.86 | C1 | 402.61 | C1 |
| 86.86 | C1 | 219.45 | C1 | 402.89 | C3 |
| 86.87 | C1 | 222.68 | C2 | 404.92 | C2 |
| 91.08 | C5 | 225.89 | C3 | 423.19 | C1 |
| 91.80 | C1 | 236.74 | C1 | 428.51 | C4 |
| 92.30 | C2 | 237.05 | C2 | 429.30 | C3 |
| 96.83 | C4 | 240.41 | C1 | 431.57 | C2 |
| 98.62 | C1 | 240.59 | C4 | 434.60 | C3 |
| 100.03 | C1 | 240.99 | C1 | 438.24 | C1 |
| 106.39 | C4 | 241.17 | C2 | 440.71 | C1 |
| 106.40 | C1 | 241.55 | C4 | 447.17 | C3 |
| 107.29 | C1 | 245.77 | C2 | 450.31 | C5 |
| 116.25 | C3 | 265.82 | C1 | 464.64 | C3 |
| 118.98 | C1 | 268.15 | C1 | 464.67 | C3 |
| 127.47 | C3 | 271.20 | C4 | 465.08 | C1 |
| 128.22 | C1 | 278.93 | C5 | 465.85 | C1 |
| 130.74 | C3 | 279.34 | C2 | 471.07 | C1 |
| 131.84 | C1 | 288.12 | C5 | 487.62 | C1 |
| 132.45 | C3 | 292.76 | C1 | 491.53 | C3 |
| 141.67 | C2 | 294.07 | C2 | 495.31 | C2 |
| 144.92 | C2 | 295.04 | C1 |  |  |
| 146.64 | C3 | 300.05 | C2 |  |  |


| DT DataRun \#5 <br> Time <br> Component <br> Failure | Time | Component <br> Failure | Time | Component <br> Failure |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0.67 | C 2 | 166.70 | C 2 | 322.14 | C 2 |
| 0.82 | C 3 | 175.46 | C 4 | 323.43 | C 5 |
| 7.46 | C 2 | 183.11 | C 3 | 325.20 | C 1 |
| 9.39 | C 2 | 186.66 | C 2 | 329.85 | C 1 |
| 10.75 | C 1 | 192.37 | C 5 | 337.16 | C 2 |
| 11.20 | C 4 | 197.14 | C 1 | 338.71 | C 1 |
| 11.56 | C 3 | 197.29 | C 3 | 339.89 | C 1 |
| 13.02 | C 2 | 197.48 | C 5 | 346.68 | C 3 |
| 17.47 | C 5 | 205.10 | C 2 | 349.52 | C 5 |
| 17.70 | C 1 | 209.58 | C 2 | 358.04 | C 1 |
| 30.01 | C 5 | 210.49 | C 1 | 359.73 | C 1 |
| 37.85 | C 2 | 213.39 | C 3 | 367.10 | C 3 |
| 44.40 | C 1 | 223.49 | C 4 | 367.43 | C 5 |
| 48.36 | C 4 | 232.47 | C 2 | 373.47 | C 5 |
| 53.53 | C 1 | 237.11 | C 1 | 374.25 | C 1 |
| 53.64 | C 1 | 237.44 | C 1 | 380.21 | C 1 |
| 61.29 | C 5 | 239.24 | C 3 | 381.77 | C 2 |
| 61.65 | C 4 | 240.12 | C 2 | 385.44 | C 4 |
| 62.00 | C 1 | 241.92 | C 2 | 388.47 | C 4 |
| 63.82 | C 3 | 242.26 | C 1 | 390.76 | C 1 |
| 66.33 | C 2 | 244.28 | C 4 | 391.40 | C 1 |
| 69.25 | C 3 | 253.14 | C 4 | 392.34 | C 4 |
| 73.82 | C 1 | 253.66 | C 1 | 392.80 | C 1 |
| 73.87 | C 3 | 256.45 | C 2 | 403.73 | C 4 |
| 74.55 | C 1 | 258.81 | C 2 | 406.00 | C 3 |
| 74.64 | C 1 | 262.10 | C 3 | 408.46 | C 1 |
| 78.55 | C 3 | 267.99 | C 5 | 409.87 | C 2 |
| 78.99 | C 5 | 269.02 | C 3 | 411.74 | C 1 |
| 85.24 | C 5 | 275.07 | C 1 | 422.27 | C 2 |
| 106.44 | C 5 | 278.08 | C 4 | 437.73 | C 4 |
| 108.23 | C 1 | 279.08 | C 2 | 441.40 | C 1 |
| 109.67 | C 1 | 280.21 | C 1 | 443.16 | C 1 |
| 112.07 | C 1 | 283.38 | C 4 | 444.36 | C 4 |
| 114.33 | C 3 | 290.57 | C 2 | 462.58 | C 1 |
| 118.03 | C 1 | 290.79 | C 1 | 466.10 | C 2 |
| 122.81 | C 3 | 294.19 | C 4 | 468.55 | C 3 |
| 149.15 | C 2 | 295.60 | C 1 | 473.70 | C 3 |
| 149.39 | C 1 | 298.09 | C 2 | 474.43 | C 1 |
| 149.73 | C 3 | 301.78 | C 1 | 478.64 | C 4 |
| 150.20 | C 5 | 309.33 | C 3 | 482.65 | C 5 |
| 151.99 | C 1 | 312.76 | C 1 | 492.94 | C 4 |
| 157.39 | C 1 | 318.88 | C 3 | 498.76 | C 1 |
| 161.74 | C 1 | 321.82 | C 1 |  |  |
|  |  |  |  |  |  |

OT Data Runs \#1 and \#2

| OT Data Run \#1 |  | OT Data Run \#2 |  |
| :---: | :---: | :---: | :---: |
| Time | Component Failure | Time | Component Failure |
| 6.08 | C3 | 22.69 | C1 |
| 7.82 | C1 | 23.44 | C5 |
| 8.27 | C2 | 27.11 | C1 |
| 9.03 | C2 | 30.16 | C3 |
| 14.80 | C1 | 34.43 | C1 |
| 18.06 | C3 | 37.63 | C2 |
| 32.21 | C2 | 38.51 | C1 |
| 33.01 | C1 | 41.76 | C2 |
| 33.05 | C2 | 42.56 | C4 |
| 38.23 | C2 | 44.49 | C1 |
| 44.42 | C3 | 50.43 | C2 |
| 47.53 | C1 | 53.33 | C4 |
| 47.62 | C1 | 57.57 | C4 |
| 57.23 | C1 | 61.55 | C4 |
| 59.43 | C1 | 67.96 | C1 |
| 66.62 | C3 | 78.81 | C1 |
| 67.16 | C1 | 89.34 | C1 |
| 76.87 | C2 | 93.12 | C1 |
| 78.42 | C1 | 104.07 | C3 |
| 85.43 | C2 | 106.78 | C1 |
| 96.68 | C2 | 116.38 | C1 |
| 96.96 | C1 | 117.95 | C1 |
| 98.93 | C5 | 119.96 | C3 |
| 109.81 | C2 |  |  |
| 113.89 | C3 |  |  |
| 114.65 | C1 |  |  |
| 120.78 | C2 |  |  |
| 124.09 | C 4 |  |  |

Appendix L. Calculation For A Bridge System Reliability With Different Independent Components.

Consider a system composed of 5 different independent components given in Figure 1 (page 30). The time to failure of each component is assumed to be exponentially distributed. Let $\lambda_{1}=0.1, \lambda_{2}=0.05, \lambda_{3}=0.033, \lambda_{4}=0.025$, and $\lambda_{5}=0.02$ be the respective constant failure rates (failure per hour) of each component.

For the true system, using a mission time, $t$ of one hour, the reliability of components $1,2,3,4$, and 5 are
$R_{1}=\exp (-0.10)=90.48 \%$
$R_{2}=\exp (-0.05)=95.12 \%$
$R_{3}=\exp (-0.033)=96.75 \%$
$\mathrm{R}_{4}=\exp (-0.025)=97.53 \%$
$R_{5}=\exp (-0.02)=98.02 \%$.
The reliability of the system can be calculated as
$R_{s}=R_{1} R_{4}+R_{2} R_{5}+R_{1} R_{3} R_{5}+R_{2} R_{3} R_{4}-R_{1} R_{2} R_{3} R_{4}-R_{1} R_{2} R_{3} R_{5}-$ $R_{1} R_{2} R_{4} R_{5}-R_{1} R_{3} R_{4} R_{5}-R_{2} R_{3} R_{4} R_{5}+2 R_{1} R_{2} R_{3} R_{4} R_{5}=99.48 \%$.

Using a computer program called RAPTOR, which is developed by AFOTEC, to simulate the true system, the following data are obtained (to review the simulated data, see Appendix K):

Table L1: Component 1 DT Data

| Run $i$ | $T_{i}$ Hours | $X_{i}$ Failures | $\widehat{\lambda}_{i}=X_{i} / T_{i}$ |
| :---: | :---: | :---: | :---: |
| 1 | 499.09 | 51 | 0.10219 |
| 2 | 490.55 | 41 | 0.08358 |
| 3 | 497.97 | 44 | 0.08836 |
| 4 | 495.31 | 52 | 0.10499 |
| 5 | 498.76 | 48 | 0.09624 |

Table L2: Component 1 OT Data

| Run $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures | $\widehat{\lambda_{i}}=\mathrm{X}_{\mathrm{i}} / \mathrm{T}_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: |
| 1 | 124.09 | 11 | 0.08865 |
| 2 | 119.96 | 12 | 0.10003 |

Table L3: Component 2 DT Data

| Run $i$ | $T_{i}$ Hours | $X_{i}$ Failures | $\widehat{\lambda}_{i}=X_{i} / T_{i}$ |
| :---: | :---: | :---: | :---: |
| 1 | 499.09 | 19 | 0.03807 |
| 2 | 490.55 | 23 | 0.04689 |
| 3 | 497.97 | 30 | 0.06025 |
| 4 | 495.31 | 26 | 0.05249 |
| 5 | 498.76 | 25 | 0.05012 |

Table L4: Component 2 OT Data

| Run $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures | $\widehat{\lambda_{i}}=\mathrm{X}_{\mathrm{i}} / \mathrm{T}_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: |
| 1 | 124.09 | 10 | 0.08059 |
| 2 | 119.96 | 3 | 0.02501 |

Table L5: Component 3 DT Data

| Run $i$ | $T_{i}$ Hours | $X_{i}$ Failures | $\bar{\lambda}_{i}=X_{i} / T_{i}$ |
| :---: | :---: | :---: | :---: |
| 1 | 499.09 | 22 | 0.04408 |
| 2 | 490.55 | 21 | 0.04281 |
| 3 | 497.97 | 17 | 0.03414 |
| 4 | 495.31 | 18 | 0.03634 |
| 5 | 498.76 | 22 | 0.04411 |

Table L6: Component 3 OT Data

| Run $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures | $\widehat{\lambda}_{i}=\mathrm{X}_{\mathrm{i}} / \mathrm{T}_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: |
| 1 | 124.09 | 5 | 0.04029 |
| 2 | 119.96 | 3 | 0.02501 |

Table L7: Component 4 DT Data

| Run $i$ | $T_{i}$ Hours | $X_{i}$ Failures | $\widehat{\lambda}_{i}=X_{i} / T_{i}$ |
| :---: | :---: | :---: | :---: |
| 1 | 499.09 | 15 | 0.03006 |
| 2 | 490.55 | 12 | 0.02446 |
| 3 | 497.97 | 6 | 0.01205 |
| 4 | 495.31 | 12 | 0.02423 |
| 5 | 498.76 | 18 | 0.03609 |

Table L8: Component 4 OT Data

| Run $i$ | $\mathrm{~T}_{\mathrm{i}}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures | $\widehat{\lambda_{i}}=\mathrm{X}_{\mathrm{i}} / \mathrm{T}_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: |
| 1 | 124.09 | 1 | 0.00807 |
| 2 | 119.96 | 4 | 0.03334 |

Table L9: Component 5 DT Data

| Run $i$ | $T_{i}$ Hours | $X_{i}$ Failures | $\widehat{\lambda_{i}}=X_{i} / T_{i}$ |
| :---: | :---: | :---: | :---: |
| 1 | 499.09 | 13 | 0.02605 |
| 2 | 490.55 | 9 | 0.01835 |
| 3 | 497.97 | 8 | 0.01607 |
| 4 | 495.31 | 10 | 0.02019 |
| 5 | 498.76 | 15 | 0.03008 |

Table L10: Component 5 OT Data

| Run i | $\mathrm{T}_{i}$ Hours | $\mathrm{X}_{\mathrm{i}}$ Failures | $\widehat{\lambda_{i}}=\mathrm{X}_{\mathrm{i}} / \mathrm{T}_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: |
| 1 | 124.09 | 1 | 0.00806 |
| 2 | 119.96 | 1 | 0.00834 |

## The Classical Exponential Method.

Assuming the time to failure of each component has the exponential distribution, point estimates for the failure rate $\lambda$ and $80 \%$ confidence intervals about $\lambda$ will be computed.

Component $1 \mathrm{DT}: \quad \hat{\lambda}=\left(\frac{f_{1}}{T_{1}}\right)=\left(\frac{236}{2481.68}\right)=0.09510$
Component 1 OT: $\hat{\lambda}=\left(\frac{f_{2}}{T_{2}}\right)=\left(\frac{23}{244.05}\right)=0.09424$

Component $2 \mathrm{DT}: \hat{\lambda}=\left(\frac{f_{3}}{T_{3}}\right)=\left(\frac{123}{2481.68}\right)=0.04956$ Component 2 OT: $\hat{\lambda}=\left(\frac{f_{4}}{T_{4}}\right)=\left(\frac{13}{244.05}\right)=0.05327$ Component $3 \mathrm{DT}: \quad \hat{\lambda}=\left(\frac{f_{5}}{T_{5}}\right)=\left(\frac{100}{2481.68}\right)=0.04030$ Component 3 OT: $\hat{\lambda}=\left(\frac{f_{6}}{T_{6}}\right)=\left(\frac{8}{244.05}\right)=0.03278$ Component $4 \mathrm{DT}: \quad \hat{\lambda}=\left(\frac{f_{7}}{T_{7}}\right)=\left(\frac{63}{2481.68}\right)=0.02539$ Component 4 OT: $\hat{\lambda}=\left(\frac{f_{8}}{T_{8}}\right)=\left(\frac{5}{244.05}\right)=0.02049$ Component $5 \mathrm{DT}: \quad \hat{\lambda}=\left(\frac{f_{9}}{T_{9}}\right)=\left(\frac{55}{2481.68}\right)=0.02216$ Component 5 OT: $\hat{\lambda}=\left(\frac{f_{10}}{T_{10}}\right)=\left(\frac{2}{244.59}\right)=0.00820$
where $f_{1}=236$ is the number of failures and $T_{1}=2481.68$ is the total test time from Table L1 and similarly $f_{2}=23$ and $T_{2}=244.05$ from Table L2, $f_{3}=123$ and $T_{3}=2481.68$ from Table L3, $f_{4}=13$ and $T_{4}=244.05$ from Table L4, $f_{5}=100$ and $T_{5}=2481.68$ from Table L5, $f_{6}=8$ and $T_{6}=244.05$ from Table L6, $f_{7}=63$ and $T_{7}=2481.68$ from Table L7, $f_{8}=5$ and $T_{8}=$ 244.05 from Table L8, $f_{9}=55$ and $T_{9}=2481.68$ from Table L9, $f_{10}=2$ and $T_{10}=244.05$ from Table L10.

The $80 \%$ two-sided confidence intervals (TCI) are
Component 1 DT: $(0.08726,0.10311)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 236)}{2 \times 2481.68}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 236)}{2 \times 2481.68}\right)=\left(\frac{433.08}{4963.36}, \frac{511.78}{4963.36}\right)$
Component 1 OT: $(0.07010,0.12014)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 23)}{2 \times 244.05}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 23)}{2 \times 244.05}\right)=\left(\frac{34.22}{488.1}, \frac{58.64}{488.1}\right)$
Component $2 \mathrm{DT}:(0.04393,0.05537)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 123)}{2 \times 2481.68}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 123)}{2 \times 2481.68}\right)=\left(\frac{218.04}{4963.36}, \frac{274.82}{4963.36}\right)$
Component 2 OT: $(0.03543,0.07286)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 13)}{2 \times 244.05}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 13)}{2 \times 244.05}\right)=\left(\frac{17.29}{488.1}, \frac{35.56}{488.1}\right)$
Component $3 \mathrm{DT}:(0.03523,0.04554)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 100)}{2 \times 2481.68}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 100)}{2 \times 2481.68}\right)=\left(\frac{174.84}{4963.36}, \frac{226.02}{4963.36}\right)$
Component 3 OT: $(0.01908,0.04823)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 8)}{2 \times 244.05}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 8)}{2 \times 244.05}\right)=\left(\frac{9.31}{488.1}, \frac{23.54}{488.1}\right)$
Component 4 DT: $(0.02138,0.02956)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 63)}{2 \times 2481.68}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 63)}{2 \times 2481.68}\right)=\left(\frac{106.13}{4963.36}, \frac{146.72}{4963.36}\right)$
Component 4 OT: $(0.00997,0.03275)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 5)}{2 \times 244.05}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 5)}{2 \times 244.05}\right)=\left(\frac{4.87}{488.1}, \frac{15.99}{488.1}\right)$
Component $5 \mathrm{DT}:(0.01843,0.02607)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 55)}{2 \times 2481.68}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 55)}{2 \times 2481.68}\right)=\left(\frac{91.47}{4963.36}, \frac{129.39}{4963.36}\right)$
Component 5 OT: $(0.00218,0.01594)$
$\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 2)}{2 \times 244.05}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 2)}{2 \times 244.05}\right)=\left(\frac{1.06}{488.1}, \frac{7.78}{488.1}\right)$.

The reliability estimators of $R(t)$ for $t=1$ hour are
Component 1 DT: $\widehat{R_{1}}(t)=\exp (-0.09510 \times 1)=90.93 \%$
Component 1 OT: $\widehat{R_{1}}(t)=\exp (-0.09424 \times 1)=91.01 \%$
Component $2 \mathrm{DT}: \widehat{R_{2}}(t)=\exp (-0.04956 \times 1)=95.17 \%$
Component 2 OT: $\widehat{R_{2}}(t)=\exp (-0.05327 \times 1)=94.81 \%$
Component $3 \mathrm{DT}: \widehat{R_{3}}(t)=\exp (-0.04030 \times 1)=96.05 \%$
Component 3 OT: $\widehat{R_{3}}(t)=\exp (-0.03278 \times 1)=96.78 \%$
Component $4 \mathrm{DT}: \widehat{R_{4}}(t)=\exp (-0.02539 \times 1)=97.49 \%$
Component $4 \mathrm{OT}: \widehat{R_{4}}(t)=\exp (-0.02049 \times 1)=97.97 \%$
Component 5 DT: $\widehat{R_{5}}(t)=\exp (-0.02216 \times 1)=97.81 \%$
Component 5 OT: $\widehat{R_{5}}(t)=\exp (-0.00820 \times 1)=99.18 \%$
Substitute the appropriate values into $\widehat{R}(t)=R_{1} R_{4}+R_{2} R_{5}$
$+R_{1} R_{3} R_{5}+R_{2} R_{3} R_{4}-R_{1} R_{2} R_{3} R_{4}-R_{1} R_{2} R_{3} R_{5}-R_{1} R_{2} R_{4} R_{5}-R_{1} R_{3} R_{4} R_{5}-$ $R_{2} R_{3} R_{4} R_{5}+2 R_{1} R_{2} R_{3} R_{4} R_{5}$ to obtained the following:

Component Level Aggregated to System DT : $\widehat{R}(t)=99.50 \%$
Component Level Agaregated to System $O T: \widehat{R}(t)=99.51 \%$.
The $80 \%$ two-sided confidence intervals (TCI) are
Component 1 DT: $(90.20 \%, 91.64 \%)$
$\exp (-0.10311 \times 1) \leq \widehat{R}(1) \leq \exp (-0.08726 \times 1)$
Component 1 OT: ( $88.68 \%, 93.23 \%$ )
$\exp (-0.12014 \times 1) \leq \widehat{R}(1) \leq \exp (-0.07010 \times 1)$
Component 2 DT: (94.61\%,95.70\%)
$\exp (-0.05537 \times 1) \leq \widehat{R}(1) \leq \exp (-0.04393 \times 1)$
Component 2 OT: (92.97\%,96.52\%)
$\exp (-0.07286 \times 1) \leq \widehat{R}(1) \leq \exp (-0.03543 \times 1)$
Component 3 DT: $(95.55 \%, 96.54 \%)$
$\exp (-0.04554 \times 1) \leq \widehat{R}(1) \leq \exp (-0.03523 \times 1)$
Component 3 OT: ( $95.29 \%, 98.11 \%$ )
$\exp (-0.04823 \times 1) \leq \widehat{R}(1) \leq \exp (-0.01908 \times 1)$
Component 4_DT: (97.09\%,97.89\%)
$\exp (-0.02956 \times 1) \leq \widehat{R}(1) \leq \exp (-0.02138 \times 1)$
Component 4 OT: $(96.78 \%, 99.01 \%)$
$\exp (-0.03275 \times 1) \leq \widehat{R}(1) \leq \exp (-0.00997 \times 1)$
Component 5 DT: $(97.43 \%, 98.17 \%)$
$\exp (-0.02607 \times 1) \leq \widehat{R}(1) \leq \exp (-0.01843 \times 1)$
Component 5 OT: ( $98.42 \%, 99.78 \%$ )
$\exp (-0.01594 \times 1) \leq \widehat{R}(1) \leq \exp (-0.00218 \times 1)$
Substitute the appropriate values into $\widehat{R}(t)=R_{1} R_{4}+R_{2} R_{5}$
$+R_{1} R_{3} R_{5}+R_{2} R_{3} R_{4}-R_{1} R_{2} R_{3} R_{4}-R_{1} R_{2} R_{3} R_{5}-R_{1} R_{2} R_{4} R_{5}-R_{1} R_{3} R_{4} R_{5}-$
$R_{2} R_{3} R_{4} R_{5}+2 R_{1} R_{2} R_{3} R_{4} R_{5}$ to obtained the following:
Component Level Aggregated to System DT:
(99.38\%, 99.59\%)

Component Level Aggregated to System OT:
(99.14\%, 99.76\%) .

The Bayesian Exponential Method.
Bayesian Exponential Prior.
For Component 1 data, from Table L1:
$\widehat{E}(\lambda)=\bar{\lambda}=0.09507$ and $\widehat{V}(\lambda)=s_{\lambda}^{2}=0.00008$.
These yielded the parameter estimates
$\alpha=\left(\frac{0.09507^{2}}{0.00008}\right)=112.98$ and $\beta=\left(\frac{0.09507}{0.00008}\right)=1188.38$.

For Component 2 data, from Table L3:
$\widehat{E}(\lambda)=\bar{\lambda}=0.04956$ and $\widehat{V}(\lambda)=s_{\lambda}{ }^{2}=0.00007$.
These yielded the parameter estimates
$\alpha=\left(\frac{0.04956^{2}}{0.00007}\right)=35.09$ and $\beta=\left(\frac{0.04956}{0.00007}\right)=708$.

For Component 3 data, from Table L5:
$\widehat{E}(\lambda)=\bar{\lambda}=0.04030$ and $\widehat{V}(\lambda)=s_{\lambda}{ }^{2}=0.00002$.
These yielded the parameter estimates
$\alpha=\left(\frac{0.04030^{2}}{0.00002}\right)=81.21$ and $\beta=\left(\frac{0.04030}{0.00002}\right)=2015$.

For Component 4 data, from Table L7:
$\widehat{E}(\lambda)=\bar{\lambda}=0.02538$ and $\hat{V}(\lambda)=s_{\lambda}{ }^{2}=0.00008$.

These yielded the parameter estimates
$\alpha=\left(\frac{0.02538^{2}}{0.00008}\right)=8.05$ and $\beta=\left(\frac{0.02538}{0.00008}\right)=317.25$.

For Component 5 data, from Table L9:
$\widehat{E}(\lambda)=\bar{\lambda}=0.02215$ and $\widehat{V}(\lambda)=s_{\lambda}{ }^{2}=0.00003$.

These yielded the parameter estimates
$\alpha=\left(\frac{0.02215^{2}}{0.00003}\right)=16.35$ and $\beta=\left(\frac{0.02215}{0.00003}\right)=738.33$.
Bayesian Exponential Posterior Analysis.
Component 1: $\hat{\lambda}=\left(\frac{23+112.98}{244.05+1188.38}\right)=0.09493$.
Component 2: $\hat{\lambda}=\left(\frac{13+35.09}{244.05+708}\right) \quad=0.05051$.
Component 3: $\hat{\lambda}=\left(\frac{8+81.21}{244.05+2015}\right) \quad=0.03949$.
Component 4: $\hat{\lambda}=\left(\frac{5+8.05}{244.05+317.25}\right)=0.02325$.
Component 5: $\hat{\lambda}=\left(\frac{2+16.35}{244.05+738.33}\right)=0.01868$.
The $80 \%$ two-sided probability intervals (TBPI) are
Component 1: $\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 23+2 \times 112.98)}{2(244.05+1188.38)}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 23+2 \times 112.98)}{2(244.05+1188.38)}\right)$
$=\left(\frac{241.63}{2864.86}, \frac{301.23}{2864.86}\right)=(0.08434,0.10515)$.
Component 2 : $\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 13+2 \times 35.09)}{2(244.05+708)}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 13+2 \times 35.09)}{2(244.05+708)}\right)$
$=\left(\frac{78.73}{1904.1}, \frac{114.13}{1904.1}\right)=(0.04135,0.05994)$.
Component 3: $\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 8+2 \times 81.21)}{2(244.05+2015)}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 8+2 \times 81.21)}{2(244.05+2015)}\right)$
$=\left(\frac{154.29}{4518.1}, \frac{202.57}{4518.1}\right)=(0.03415,0.04484)$.
Component 4: $\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 5+2 \times 8.05)}{2(244.05+317.25)}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 5+2 \times 8.05)}{2(244.05+317.25)}\right)$
$=\left(\frac{17.29}{1122.6}, \frac{35.56}{1122.6}\right)=(0.01540,0.03168)$.

Component 5: $\left(\frac{\chi_{0.2 / 2}^{2}(2 \times 2+2 \times 16.35)}{2(244.05+738.33)}, \frac{\chi_{1-0.2 / 2}^{2}(2 \times 2+2 \times 16.35)}{2(244.05+738.33)}\right)$
$=\left(\frac{25.64}{1964.76}, \frac{47.21}{1964.76}\right)=(0.01305,0.02403)$.
The Bayesian estimators of $R(t)$ for $t=1$ hour are
Component 1: $\widehat{R}(t)=90.95 \%$

$$
\widehat{R}(t)=\left(\frac{\left(\frac{244.05}{1188.38}\right)+1}{\left(\frac{244.05}{1188.38}\right)+\left(\frac{1}{1188.38}\right)+1}\right)^{112.98+23}
$$

Component 2: $\widehat{R}(t)=\mathbf{9 5 . 0 8 \%}$

$$
\widehat{R}(t)=\left(\frac{\left(\frac{244.05}{708}\right)+1}{\left(\frac{244.05}{708}\right)+\left(\frac{1}{708}\right)+1}\right)^{35.09+13}
$$

Component 3: $\widehat{R}(t)=96.13 \%$

$$
\widehat{R}(t)=\left(\frac{\left(\frac{244.05}{2015}\right)+1}{\left(\frac{244.05}{2015}\right)+\left(\frac{1}{2015}\right)+1}\right)^{81.21+8}
$$

Component 4: $\widehat{R}(t)=97.70 \%$

$$
\widehat{R}(t)=\left(\frac{\left(\frac{244.05}{317.25}\right)+1}{\left(\frac{244.05}{317.25}\right)+\left(\frac{1}{317.25}\right)+1}\right)^{8.05+5}
$$

Component 5: $\widehat{R}(t)=98.15 \%$

$$
\widehat{R}(t)=\left(\frac{\left(\frac{244.05}{738.33}\right)+1}{\left(\frac{244.05}{738.33}\right)+\left(\frac{1}{738.33}\right)+1}\right)^{16.35+2}
$$

Substitute the appropriate values into $\widehat{R}(t)=R_{1} R_{4}+R_{2} R_{5}$ $+R_{1} R_{3} R_{5}+R_{2} R_{3} R_{4}-R_{1} R_{2} R_{3} R_{4}-R_{1} R_{2} R_{3} R_{5}-R_{1} R_{2} R_{4} R_{5}-R_{1} R_{3} R_{4} R_{5}-$ $R_{2} R_{3} R_{4} R_{5}+2 R_{1} R_{2} R_{3} R_{4} R_{5}$ to obtained the following:

Component Level Agaregated to System: $\widehat{R}(t)=99.50 \%$.
The $80 \%$ two-sided probability intervals (TBPI) are
Component 1: $(90.02 \% \leq \widehat{R}(1) \leq 91.91 \%)$
$\exp (-0.10515 \times 1) \leq \widehat{R}(1) \leq \exp (-0.08434 \times 1)$.
Component 2: $(94.18 \% \leq \widehat{R}(1) \leq 95.95 \%)$
$\exp (-0.05994 \times 1) \leq \widehat{R}(1) \leq \exp (-0.04135 \times 1)$.
Component 3: $(95.62 \% \leq \widehat{R}(1) \leq 96.64 \%)$
$\exp (-0.04484 \times 1) \leq \widehat{R}(1) \leq \exp (-0.03415 \times 1)$.
Component 4: $(96.88 \% \leq \widehat{R}(1) \leq 98.47 \%)$
$\exp (-0.03168 \times 1) \leq \widehat{R}(1) \leq \exp (-0.01540 \times 1)$.
Component 5: $(97.63 \% \leq \widehat{R}(1) \leq 98.70 \%)$
$\exp (-0.02403 \times 1) \leq \widehat{R}(1) \leq \exp (-0.01315 \times 1)$.
Substitute the appropriate values into $\widehat{R}(t)=R_{1} R_{4}+R_{2} R_{5}$ $+R_{1} R_{3} R_{5}+R_{2} R_{3} R_{4}-R_{1} R_{2} R_{3} R_{4}-R_{1} R_{2} R_{3} R_{5}-R_{1} R_{2} R_{4} R_{5}-R_{1} R_{3} R_{4} R_{5}-$ $R_{2} R_{3} R_{4} R_{5}+2 R_{1} R_{2} R_{3} R_{4} R_{5}$ to obtained the following:

Component Level Aggregated to System: (99.33\%,99.65\%).

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## Vita

Captain Thuan H. Tran was born on in h. He and his family arrived in America in June 1986. He graduated from high school (Dickinson High School) in Jersey City, New Jersey, in 1989 and attended the United States Air Force Academy Preparatory School in Colorado Springs, Colorado. With the assistance of an Air Force Reserve Officers Training Corps federal scholarship, he earned a Bachelor of Science degree in Mathematics from Stevens Institute of Technology in 1993.

Before arriving at AFIT in August 1996, Captain Tran was a Weapon System Analyst at the B-2 Combined Test Force, B-2 Operational Test Team, Edwards AFB, California.

As a follow-on to his work at AFIT, Captain Tran has been assigned to Headquarters, Air Force Material Command (AFMC), where he will be an analyst at the AFMC Study and Analysis Group in Wright-Patterson AFB, Ohio.

Captain Tran is an honor graduate of the United States Air Force Academy Preparatory School. He is also graduated with high honor from Stevens Institute of Technology. He is a member of the Omega Rho honor society. Captain Tran is single.

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