



Full length article

# Nucleation and growth of Ag<sub>3</sub>Sn in Sn-Ag and Sn-Ag-Cu solder alloys

Y. Cui<sup>a</sup>, J.W. Xian<sup>a,\*</sup>, A. Zois<sup>a</sup>, K. Marquardt<sup>a</sup>, H. Yasuda<sup>b</sup>, C.M. Gourlay<sup>a</sup>

<sup>a</sup> Department of Materials, Imperial College London, London. SW7 2AZ. UK

<sup>b</sup> Department of Materials Science & Engineering, Kyoto University, Sakyo-ku, Kyoto, 606-8501, Japan



## ARTICLE INFO

## Keywords:

Soldering  
Undercooling  
Solidification  
Synchrotron radiation  
Intermetallic compounds (IMCs)

## ABSTRACT

Large Ag<sub>3</sub>Sn plates in solder joints can affect the reliability of electronics, however, the factors affecting their nucleation and morphology are not well understood. Here, the faceted solidification of Ag<sub>3</sub>Sn was studied as a function of melt undercooling, revealing transitions from single crystal {001} plates to cyclic twinned plates and then to highly branched structures created by twin mediated branching. Real-time X-ray imaging proved that Ag<sub>3</sub>Sn cyclic twins come from a common point, indicating they initiate in the process of nucleation or in the very early stages of growth in the undercooled melt. Soldering to copper substrates significantly catalysed Ag<sub>3</sub>Sn nucleation. This is shown to be due to constitutional supercooling generated by Ag solute rejection into the liquid ahead of the Cu<sub>6</sub>Sn<sub>5</sub> reaction layer, with additional contributions from geometrical catalysis in the grooves between Cu<sub>6</sub>Sn<sub>5</sub> scallops and heterogeneous nucleation of Ag<sub>3</sub>Sn on Cu<sub>6</sub>Sn<sub>5</sub>. The relative ease of Ag<sub>3</sub>Sn nucleation on the Cu<sub>6</sub>Sn<sub>5</sub> reaction layer is responsible for the large plates often reported in electronic solder joints.

## 1. Introduction

Silver is a key component in many electronic solder alloys. In the era of leaded solders, Sn-3.5Ag was used in applications where Sn-37Pb was unsuitable including when soldering to thick-film silver conductors. During the transition to Pb-free solders, the use of Sn-3.5Ag has continued and new Ag-containing solders have become widespread, often based on Sn-Ag-Cu (SAC) compositions due to the ubiquity of copper substrates. These include the first generation Pb-free solders SAC387 and SAC305 [1,2], the second generation alloys SAC0307 and SAC105 [3–5], and emerging third generation alloys which typically add Bi and/or Sb to near-eutectic Sn-Ag-Cu compositions [6–9]. In all these solders, the intermetallic compound (IMC) Ag<sub>3</sub>Sn forms during solidification in a eutectic reaction and, sometimes, also as a primary solidification phase. Since all these solders are eutectic or hypoeutectic compositions, the formation of primary Ag<sub>3</sub>Sn occurs when the liquid supercools with respect to the β-Sn liquidus due to nucleation difficulties of the β-Sn phase [10–12].

Extensive work has explored the formation of eutectic Ag<sub>3</sub>Sn and three types of morphologies have been identified: plate-like, needle-like and spheroidal Ag<sub>3</sub>Sn. One body of work has applied unidirectional solidification under controlled conditions to show that there is a plate to rod eutectic growth transition with increasing growth velocity [13–17]. Another body of work has shown that cooling rate in castings and solder

joints [18–22] plays a significant role in the size and morphology of Ag<sub>3</sub>Sn: a fine distribution of spheroidal Ag<sub>3</sub>Sn particles was observed at higher cooling rate (17–24 °C/s) while coarse needle-like and plate-like Ag<sub>3</sub>Sn were formed at low cooling rate (~0.1 °C/s). Increasing the volume fraction of eutectic Ag<sub>3</sub>Sn provides enhanced strength [23] and improves resistance to creep and thermal fatigue [24–28], and a finer eutectic Ag<sub>3</sub>Sn lengthscale improves creep resistance further [29,30].

The role of primary Ag<sub>3</sub>Sn plates on solder joint reliability is less clear than for eutectic Ag<sub>3</sub>Sn. Some investigators found large primary Ag<sub>3</sub>Sn to be detrimental to mechanical performance [11,31–33]. Other studies have indicated that the role of large Ag<sub>3</sub>Sn plates depends on their location in the joint: they are detrimental when aligned in the direction of crack propagation, whereas large plates can enhance thermal fatigue life when aligned such that they block or arrest an advancing crack [34]. An additional factor is that the solubility of Ag is negligible in the β-Sn and Cu<sub>6</sub>Sn<sub>5</sub> phases [35]. Thus, almost all Ag atoms go into Ag<sub>3</sub>Sn and the formation of primary Ag<sub>3</sub>Sn ties up Ag atoms that would otherwise form small eutectic Ag<sub>3</sub>Sn [36], reducing the volume fraction of effective strengthening particles.

Prior work has focussed on finding ways to prevent the formation of primary Ag<sub>3</sub>Sn plates [37–39]. Reducing the Ag content in the alloy is a simple method to prevent their formation; with a silver content less than 3 wt.% in SAC alloys large Ag<sub>3</sub>Sn formation can be substantially reduced even under extremely slow cooling conditions (0.02 °C/s) [37].

\* Corresponding author.

E-mail address: [j.xian@imperial.ac.uk](mailto:j.xian@imperial.ac.uk) (J.W. Xian).

<https://doi.org/10.1016/j.actamat.2023.118831>

Received 6 October 2022; Received in revised form 15 February 2023; Accepted 5 March 2023

Available online 6 March 2023

1359-6454/© 2023 The Authors. Published by Elsevier Ltd on behalf of Acta Materialia Inc. This is an open access article under the CC BY license (<http://creativecommons.org/licenses/by/4.0/>).

However, Ag contents of 3 wt.% or higher may be desirable for performance in thermal cycling [5]. Primary  $\text{Ag}_3\text{Sn}$  can also be reduced or completely suppressed at sufficiently high cooling rate in freestanding solder balls with near-eutectic ternary Sn-Ag-Cu composition [37,38], although there is often limited scope for altering the cooling rate in a soldering process. Since primary  $\text{Ag}_3\text{Sn}$  forms as the liquid supercools with respect to the  $\beta$ -Sn liquidus, primary  $\text{Ag}_3\text{Sn}$  plates can also be suppressed by additions that promote the nucleation of the  $\beta$ -Sn phase [39]. For example, Kang et al. [38] demonstrated that dilute Zn additions to Sn-3.8Ag-0.7Cu reduce the undercooling for  $\beta$ -Sn and prevent  $\text{Ag}_3\text{Sn}$  formation in alloys with near-eutectic Ag content and low cooling rate ( $0.02\text{ }^\circ\text{C/s}$ ).

For Sn-Ag-Cu solders, primary  $\text{Ag}_3\text{Sn}$  typically grows with a faceted plate morphology [12,40-43]. Kim et al. [40] observed  $\text{Ag}_3\text{Sn}$  plates at the top of the interfacial reaction layer with different growth stages varying from faceted dendrites to hopper crystals and simple plate morphologies in Sn-3.9Ag-0.6Cu solder joints. Gong et al. [42] reported that  $\text{Ag}_3\text{Sn}$  plates in Sn-3.8Ag-0.7Cu/Cu joints nucleate preferably near the solder/substrate interface. Through in-situ synchrotron X-ray imaging of Sn-3.5Ag/Cu joints, Ma et al. [44] proposed three growth patterns for  $\text{Ag}_3\text{Sn}$  plates: linear, Y and X shape. It was interpreted later by Mueller et al. [45] that the multiplate formations do not necessarily develop into all six directions. Mueller et al. [45] also observed star-shaped  $\text{Ag}_3\text{Sn}$  morphology in Sn-5Ag solders which they attributed to its pseudo-hexagonal structure with the main plate facet and two perpendicular in-plane growth directions indexed using a hexagonal unit cell. However, the detailed mechanisms affecting the formation of these  $\text{Ag}_3\text{Sn}$  morphologies remain ambiguous, and the difference in  $\text{Ag}_3\text{Sn}$  nucleation and growth between freestanding balls and solder joints is also unclear.

This work was conducted to build a deeper understanding of the nucleation and growth of primary  $\text{Ag}_3\text{Sn}$  crystals in solder balls and in joints on Cu substrates. We first study binary Sn-Ag solder balls and focus on (i) the nucleation undercooling for  $\text{Ag}_3\text{Sn}$ , (ii) the  $\text{Ag}_3\text{Sn}$  nucleation location, and (iii) the influence of melt undercooling on the growth of  $\text{Ag}_3\text{Sn}$  crystals. We then explore how factors (i)-(iii) are affected by the presence of Cu solute, pre-existing  $\text{Cu}_6\text{Sn}_5$  primary crystals, a  $\text{Cu}_6\text{Sn}_5$  reaction layer, and the nucleation of  $\beta$ -Sn.

## 2. Methods

### 2.1. Sample preparation

Sn-5Ag, Sn-3.5Ag, Sn-3Ag-0.5Cu, Sn-3Ag-1Cu and Sn-4Ag-0.5Cu (wt.%) alloys were made by melting 99.999% Sn with 99.9% Ag and Sn-10 wt.% Cu master alloy. The mixture was heated to  $300\text{ }^\circ\text{C}$  in a clay-bonded graphite crucible in a resistance furnace. After holding for 2 h, the melt was stirred with an  $\text{Al}_2\text{O}_3$  rod and then poured into a steel mould. Alloys were rolled to  $\sim 30\text{ }\mu\text{m}$  foils, punched into  $\text{O} 1.6\text{ mm}$  discs and reflowed in a ROL-1 tacky flux on a hotplate at  $280\text{ }^\circ\text{C}$  to form  $\sim 500\text{ }\mu\text{m}$  diameter spheres due to surface tension. The balls were then used in one of three forms: (i) as freestanding balls, (ii) as single balls soldered to a copper substrate on one side, or (iii) as a  $2 \times 2$  ball array joining copper to copper.

### 2.2. Differential scanning calorimetry (DSC)

To apply controlled cooling conditions and measure the nucleation temperature of the  $\text{Ag}_3\text{Sn}$  and  $\beta$ -Sn phases, the  $500\text{ }\mu\text{m}$  balls and joints were melted and solidified in a Mettler Toledo DSC in aluminium pans under a nitrogen atmosphere. The standard reflow profile used was to heat to a peak temperature of  $280\text{ }^\circ\text{C}$  for Sn-5Ag and  $230\text{ }^\circ\text{C}$  for all other solder compositions, hold for 10 min, and then cool at a rate of  $5\text{ K/min}$ .  $>20$  samples were studied for each composition. In Sn-5Ag,  $>80$  samples were studied to obtain data on the distribution of undercoolings and to explore the undercooling-microstructure relationship for primary

**Table 1**

Crystal structures of  $\text{Ag}_3\text{Sn}$  and  $\text{Cu}_6\text{Sn}_5$  assumed in this work.

Crystals	Space group	Pearson symbol	Lattice parameters	Ref.
$\text{Ag}_3\text{Sn}$	PmmnZ	<i>oP8</i>	$a = 4.7823\text{ \AA}$ , $b = 5.9975\text{ \AA}$ , $c = 5.1639\text{ \AA}$	[52]
$\text{Cu}_6\text{Sn}_5$	$\text{P}6_3/\text{mmc}$	<i>hP4</i>	$a = 4.1920\text{ \AA}$ , $b = 4.1920\text{ \AA}$ , $c = 5.0370\text{ \AA}$	[53]

$\text{Ag}_3\text{Sn}$  over a wide range.

In another series of experiments, the influence of cooling rate was studied in Sn-5Ag using the same parameters but cooling at one of five rates: 0.05, 0.2, 1.2, 5 and  $20\text{ K/min}$  ( $8.3 \times 10^{-4}$ ,  $3.3 \times 10^{-3}$ ,  $2.0 \times 10^{-2}$ ,  $8.3 \times 10^{-2}$  and  $3.3 \times 10^{-1}\text{ K/s}$ ).

The liquidus temperature of  $\text{Ag}_3\text{Sn}$  in Sn-5Ag was measured by cyclic DSC using a method similar to that in previous studies [35,46-48]. The system was heated at  $1.2\text{ K/min}$  to a temperature where a mixture of liquid and  $\text{Ag}_3\text{Sn}$  is known to exist ( $242\text{ }^\circ\text{C}$ ), and was then isothermally held for 30 min. The system was then heated at  $1.2\text{ K/min}$  to  $280\text{ }^\circ\text{C}$  and cooled at  $5\text{ K/min}$  to  $150\text{ }^\circ\text{C}$ , ending the first cycle. The isothermal holding temperature for the subsequent cycle was set to be  $2\text{ }^\circ\text{C}$  higher than the previous one. The presence of an endothermic peak on heating was taken to indicate that some  $\text{Ag}_3\text{Sn}$  remained at the prior isothermal holding temperature. The absence of an endothermic peak on heating indicated all  $\text{Ag}_3\text{Sn}$  had melted at the prior isothermal holding temperature. The liquidus temperature was defined as the average of the holding temperatures either side of the transition from an endothermic peak to no endothermic peak. This gave an  $\text{Ag}_3\text{Sn}$  liquidus in Sn-5Ag of  $247 \pm 1\text{ }^\circ\text{C}$ . This method is overviewed in more detail in the Supplementary Information.

To explore a much higher cooling rate, some Sn-3.5Ag/Cu joints were heated to  $230\text{ }^\circ\text{C}$  on a hot plate, held for 10 min and then quenched in water.

### 2.3. Optical and electron microscopy

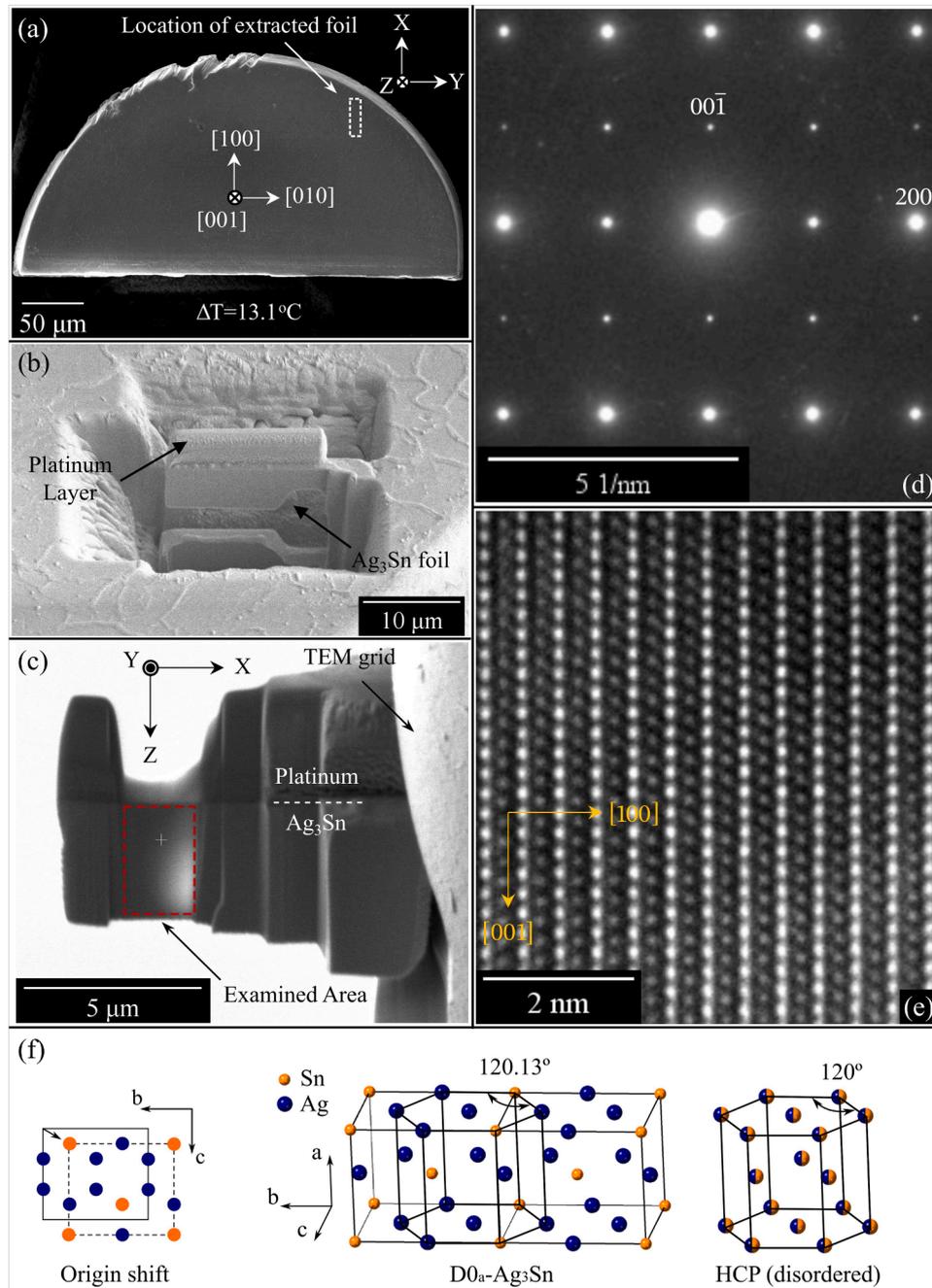
Samples were mounted in Struers VersoCit acrylic cold mounting resin and then ground to 4000 grit with SiC paper followed by polishing with colloidal silica on a nap cloth for 6 min.

Polarised optical microscopy was used to reveal different orientations of  $\text{Ag}_3\text{Sn}$  plates, taking advantage of the optical anisotropy of orthorhombic  $\text{Ag}_3\text{Sn}$ . For scanning electron microscopy (SEM), a Zeiss Sigma field emission gun SEM fitted with Bruker e-FlashHR electron backscatter diffraction (EBSD) detector and XFlash 6130 energy-dispersive spectrometry (EDS) detector were used. Bruker Esprit 2.2 software, combined with the Orientation Imaging Microscopy (OIM<sup>TM</sup>) Data Analysis software and MTEX 4.4 Toolbox within MATLAB<sup>TM</sup>9.2 (Mathworks, USA), were applied to analyse the growth habits of  $\text{Ag}_3\text{Sn}$  single crystals, the orientation relationships in twinned crystals, and the orientation relationships between  $\text{Ag}_3\text{Sn}$  and the  $\text{Cu}_6\text{Sn}_5$  reaction layer.

The crystal structures for  $\text{Ag}_3\text{Sn}$  and  $\text{Cu}_6\text{Sn}_5$  assumed in this study are listed in Table 1. While the  $\text{Cu}_6\text{Sn}_5$  phase present at room temperature is likely to be superstructure ordered monoclinic  $\eta'$  and/or  $\eta''$  [49-51], we use the high temperature parent hexagonal phase  $\eta$ - $\text{Cu}_6\text{Sn}_5$  for indexing because this phase was present during solidification. Throughout this paper, all unit cell wireframes in Figures were plotted based on the Euler angles measured by EBSD.

To study the 3D morphology of  $\text{Ag}_3\text{Sn}$  and the local geometrical features of the  $\text{Cu}_6\text{Sn}_5$  reaction layer,  $\beta$ -Sn was selectively etched in a solution with 5% NaOH and 3.5% orthonitrophenol at  $80\text{ }^\circ\text{C}$  for approximately 6 h. Extracted crystals were collected and placed on a stub for further study by analytical SEM.

To identify the main facets, electron transparent samples were milled from extracted  $\text{Ag}_3\text{Sn}$  single crystal plates using a focused ion beam (FIB) of a TFS Helios 5 CX DualBeam FIB-SEM. The lamellae were used to



**Fig. 1.** (a)  $\text{Ag}_3\text{Sn}$  single crystal plate extracted from Sn-5Ag cooled at 0.05 K/min where  $\text{Ag}_3\text{Sn}$  nucleated at 13.1 °C undercooling. (b)  $\text{Ag}_3\text{Sn}$  foil milled from  $\text{Ag}_3\text{Sn}$  plate using FIB. (c)  $\text{Ag}_3\text{Sn}$  foil attached to TEM grid, where a red box highlights the examined area in TEM. (d) Selected area electron diffraction pattern (SAED) along  $[0\bar{1}0]$ . (e) High resolution TEM image along  $[0\bar{1}0]$ . (f) Orthorhombic  $\text{Ag}_3\text{Sn}$  structure compared with a hexagonal close-packed unit cell.

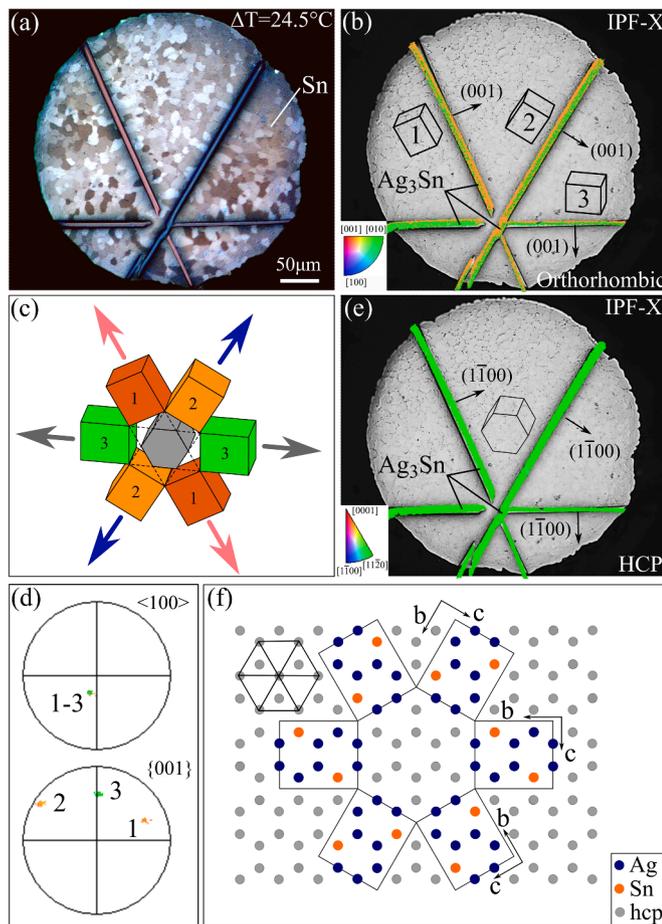
determine the facet orientations using selected area electron diffraction (SAED) in a TFS Talos F200i transmission electron microscope (TEM).

#### 2.4. Real time X-ray imaging

Sn-4Ag-0.5Cu solders were rolled down to  $\sim 100 \mu\text{m}$  foils before being punched into discs with a diameter of  $\sim 500 \mu\text{m}$ . The disc foils were then placed on a  $\sim 100 \mu\text{m}$  thick Cu-OSP printed circuit board (PCB) with flux and mounted between  $\text{SiO}_2$  glass sheets that held the sample perpendicular to the X-ray beam. A first soldering process was carried out on a hot plate before synchrotron experiments to ensure proper joining. The synchrotron experiments were conducted at BL20XU in the Spring-8 synchrotron under 1 atm pressure of nitrogen gas using

the same apparatus as in Ref. [54–56]. An X-ray beam energy of 29 KeV was used. The imaging unit incorporated a phosphor screen and a CMOS camera, resulting in a field of view of  $1038 \mu\text{m} \times 1038 \mu\text{m}$  ( $2048 \times 2048$  pixels) with a resolution of  $0.507 \mu\text{m}$ . The imaging exposure time was  $\sim 400$  ms per frame recorded at 2 frames per second. A thermocouple was placed near the sample in the furnace to record the cooling curves and the temperatures were calibrated by the eutectic onset melting temperature. The peak temperature was 246 °C and the cooling rate was  $\sim 0.3$  K/s prior to the nucleation of  $\beta\text{-Sn}$ .

After solidification, the synchrotron sample was soaked in acetone to remove the  $\text{SiO}_2$  plates and the sample was then mounted in Struers VersoCit acrylic cold mounting resin, polished to an OPS finish, and studied by EBSD. The surface microstructure could then be correlated



**Fig. 2.** Cyclic twinned  $\text{Ag}_3\text{Sn}$  in a Sn-5Ag ball with  $24.5^\circ\text{C}$  undercooling cooled at 5 K/min. (a) Polarised optical microscope image of three interpenetrating  $\text{Ag}_3\text{Sn}$  plates, each having a single colour. (b) EBSD IPF-X map superimposed on the optical image with unit cell wireframes plotted next to each plate. (c) The three  $\text{Ag}_3\text{Sn}$  unit cell wireframes from (b) translated into a ring. Growth arrow colours correspond to the polarised image in (a); unit cell colours correspond to the IPF-X colouring in (b). (d)  $\langle 100 \rangle$  and  $\{001\}$  pole figures of the three cyclic twinned orientations. (e) EBSD IPF-X map of the  $\text{Ag}_3\text{Sn}$  indexed with hexagonal unit cell. (f) Hexagonal close-packed atoms (grey) superimposed with ordered Ag (blue) and Sn (orange) atoms from the three cyclic twinned  $\text{Ag}_3\text{Sn}$  orientations.

with the projected X-ray images from the in-situ image sequence.

### 3. Results and discussion

#### 3.1. $\text{Ag}_3\text{Sn}$ in binary Sn-Ag freestanding balls

##### 3.1.1. Crystallography of $\text{Ag}_3\text{Sn}$ plates

$\text{Ag}_3\text{Sn}$  commonly grew as faceted single crystal plates. As an example, Fig. 1(a) is an extracted  $\text{Ag}_3\text{Sn}$  plate from a Sn-5Ag solder ball cooled at 0.05 K/min where the nucleation undercooling for  $\text{Ag}_3\text{Sn}$  was measured to be  $13.1^\circ\text{C}$ . To identify the main facet of the plate, combined FIB-TEM analysis was performed. A foil was prepared by FIB milling of the extracted plate surface in the geometry and orientation shown in Fig. 1(a) and (b), followed by Pt-deposition of the foil sample into a TEM grid (Fig. 1(c)). The TEM-SAED pattern from the thin foil sample in Fig. 1(d) was indexed with  $\langle 010 \rangle$  being the zone axis. Thus, the plate is orientated as indicated by the annotated coordinate system on Fig. 1(a), and  $\langle 001 \rangle$  is the main facet. Note that  $\text{Ag}_3\text{Sn}$  is orthorhombic where  $\langle 100 \rangle \neq \langle 010 \rangle \neq \langle 001 \rangle$ . Similar FIB-TEM analysis on multiple other  $\text{Ag}_3\text{Sn}$  plates measured the same result with  $\langle 001 \rangle$  as the main facet of the plate.

$\text{Ag}_3\text{Sn}$  has the  $\text{D0}_a$  structure type [52] which is a chemically-ordered derivative of the HCP structure with a small orthorhombic distortion [57] as shown in Fig. 1(f). The image in Fig. 1(e), which comes from the region of the SAED pattern, contains clear  $\{100\}$  planes which correspond to the close-packed  $\{0001\}$  plane in the pseudo-hexagonal structure.

SEM-based EBSD on  $\text{Ag}_3\text{Sn}$  was prone to orientation misindexing due to the hexagonal pseudo-symmetry in Fig. 1(f). For example, using Hough transform-based auto-indexing, extracted  $\text{Ag}_3\text{Sn}$  plates such as that in Fig. 1(a) auto-indexed as three orientations implying a facet of  $\langle 001 \rangle$ ,  $\langle 021 \rangle$  or  $\langle 02\bar{1} \rangle$ . However, FIB-TEM showed that the main facet was always  $\langle 001 \rangle$  which easily allowed the correct orientation to be selected from the three candidate orientations in EBSD.

##### 3.1.2. Cyclic twinned $\text{Ag}_3\text{Sn}$ crystals

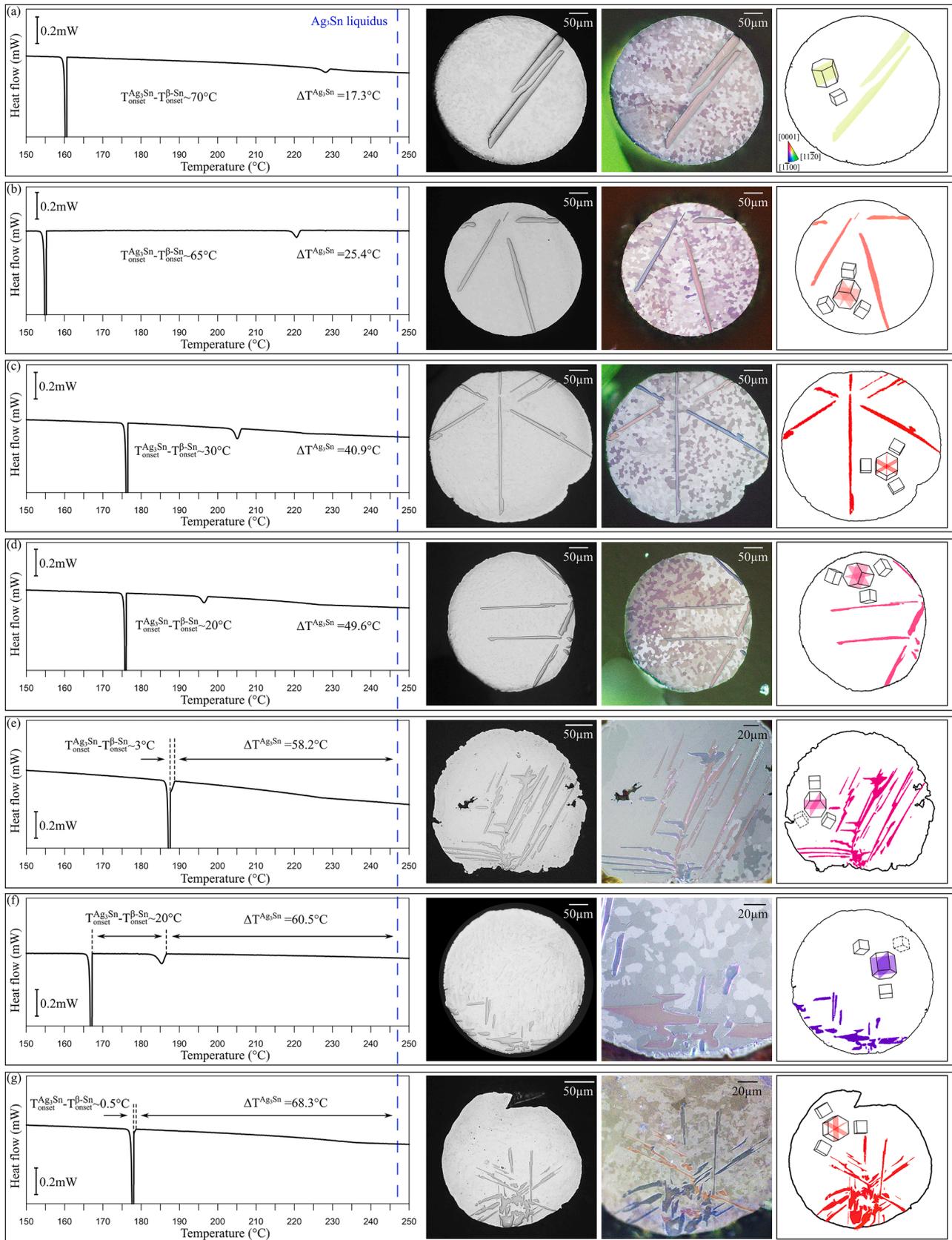
Another common growth morphology was cyclic twinned  $\text{Ag}_3\text{Sn}$  plates. Fig. 2 shows a typical example in a Sn-5Ag solder ball cooled at 1.2 K/min with nucleation undercooling of  $24.5^\circ\text{C}$ . Three interpenetrating plates span the entire solder ball. Fig. 2(a) is a polarised optical micrograph revealing three different colours of  $\text{Ag}_3\text{Sn}$  where each plate has one colour (salmon, blue or brown), indicating that each plate corresponds to a different crystallographic orientation. Three  $\text{Ag}_3\text{Sn}$  orientations were measured by EBSD mapping but, as shown in the IPF-X map in Fig. 2(b), there is strong orientation misindexing between the three orientations in the map. However, according to the FIB-TEM analysis in Section 3.1.1, the main facet of each  $\text{Ag}_3\text{Sn}$  plate is  $\{001\}$  and therefore, the corresponding orientation of each plate could be assigned as plotted next to each plate in Fig. 2(b). This reveals that there is a cyclic twinning relationship between the three  $\text{Ag}_3\text{Sn}$  plates involving multiple  $60^\circ$  rotations about the common  $\langle 100 \rangle$  direction, and the three twinned orthorhombic orientations form a combined pseudo-hexagonal symmetry, as shown in Fig. 2(c) and (d).

Further insights can be gained by reanalysing the EBSD map using the pseudo-hexagonal unit cell as shown in Fig. 2(e). From this, we see that all three plates share the same pseudo-hexagonal orientation, and the facets of all plates correspond to the  $\{1\bar{1}00\}$  planes of the pseudo-hexagonal unit cell. A similar phenomenon was reported by Mueller et al. [45], from which they concluded that all the plates originated from a common centre.

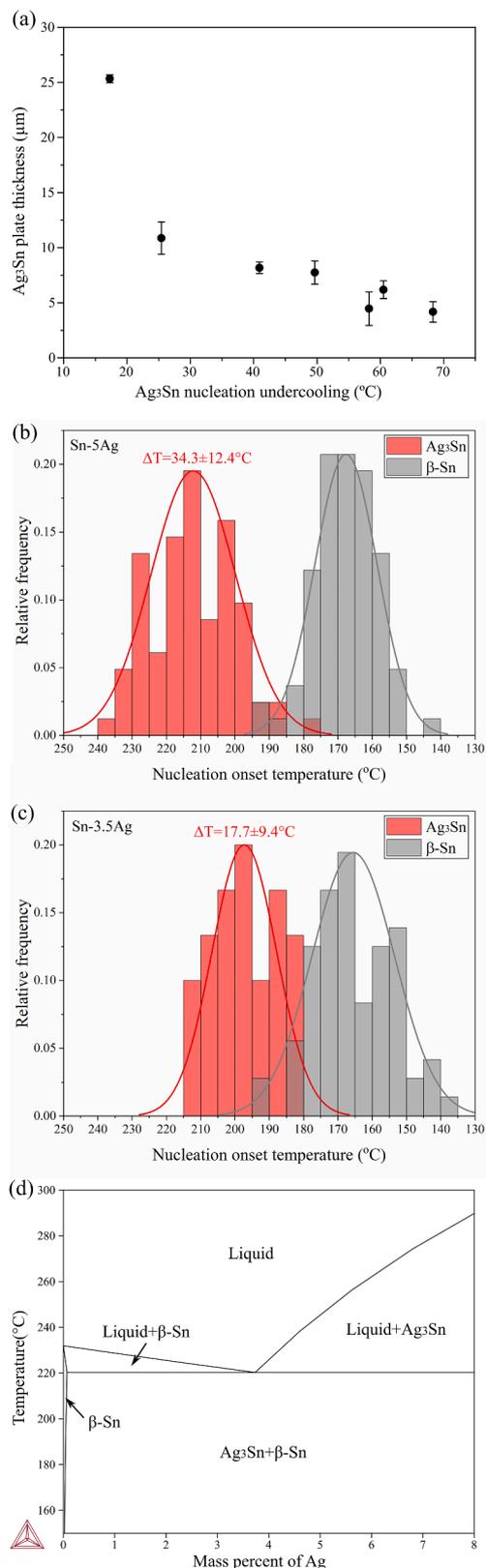
The cyclic twin can be visualised by superimposing the atoms of the three orthorhombic  $\text{Ag}_3\text{Sn}$  orientations onto a hexagonal close-packed structure, as in Fig. 2(f) forming a ring consistent with the measured orientations in Fig. 2(c). The near-perfect matching between the  $\text{Ag}_3\text{Sn}$  and HCP atomic sites in Fig. 2(f) is due to  $\text{Ag}_3\text{Sn}$  having a small orthorhombic distortion of only  $\sim 0.13^\circ$  from an HCP structure. The simple arrangement in Fig. 2(f) is intended to show the symmetry of the cyclic twin and does not indicate anything about the atomic structure of the common growth centre. Potential cyclic twin formation mechanisms are discussed in Section 3.1.5 after presenting the dependence of cyclic twinning on the imposed cooling rate and the  $\text{Ag}_3\text{Sn}$  nucleation undercooling in the next sections.

##### 3.1.3. Effect of $\text{Ag}_3\text{Sn}$ undercooling on growth morphology

Fig. 3 overviews the role of undercooling on the growth of primary  $\text{Ag}_3\text{Sn}$  in Sn-5Ag balls with a constant imposed cooling rate of 5 K/min. Results from seven balls are presented with  $\text{Ag}_3\text{Sn}$  nucleation undercoolings ranging from  $\sim 17 - 68^\circ\text{C}$ . The figure is arranged such that the  $\text{Ag}_3\text{Sn}$  nucleation undercooling becomes deeper by  $\sim 10^\circ\text{C}$  in each row from Fig. 3(a) to (g) (except Fig. 3(f)). For each Sn-5Ag ball, the DSC cooling curve is plotted with the measured  $\text{Ag}_3\text{Sn}$  liquidus temperature highlighted and the  $\text{Ag}_3\text{Sn}$  undercooling marked. The SEM image, polarised optical microscope image and EBSD IPF-Z map of the primary  $\text{Ag}_3\text{Sn}$  are also shown. The orthorhombic and pseudo-HCP unit cells from Fig. 1(f) are plotted on the IPF-Z maps to show the relationship between the measured orientations. As can be seen,  $\text{Ag}_3\text{Sn}$  grew as a



**Fig. 3.** Microstructures of  $\text{Ag}_3\text{Sn}$  with different nucleation undercooling in Sn-5Ag cooled at 5 K/min. DSC cooling traces highlighting the  $\text{Ag}_3\text{Sn}$  liquidus temperature (blue dashed line) and  $\text{Ag}_3\text{Sn}$  undercooling. Polarised optical images showing  $\text{Ag}_3\text{Sn}$  regions with the same orientation. EBSD IPF-Z maps plotted after indexing with an HCP structure. The hexagonal and orthorhombic unit cell wireframes are plotted from Euler angles with the hexagonal  $\{1100\}$  planes highlighted.



**Fig. 4.** (a) Ag<sub>3</sub>Sn plate thickness versus undercooling measured from Fig. 3 using the orientation from EBSD to account for sectioning effects. (b)-(c) Histogram of nucleation onset temperature for Ag<sub>3</sub>Sn (red) and β-Sn (grey) in 82 Sn-5Ag (b) and 30 Sn-3.5Ag (c) solder balls with fitted normal distribution curves and mean Ag<sub>3</sub>Sn nucleation undercooling and standard deviations. Both compositions were cooled at 5 K/min. (d) Sn-Ag phase diagram at the Sn-rich side [61].

single crystal plate at the smallest undercoolings (<20 °C). With deepening undercooling to ~25 °C, three plates formed each with a different single colour in polarised light imaging and all with the same pseudo-HCP orientation in EBSD mapping, with the three orthorhombic orientations related by multiple 60° rotations around (100) similar to Fig. 2. Thus, the three plates grew from a common origin. Note that the examples in Fig. 3(b) and Fig. 2 are at a similar Ag<sub>3</sub>Sn undercooling and have a similar cyclic twinned Ag<sub>3</sub>Sn plate microstructure but the nucleation point is further from the cross-section in Fig. 3(b) than in Fig. 2, which will be the general case for a random cross-section.

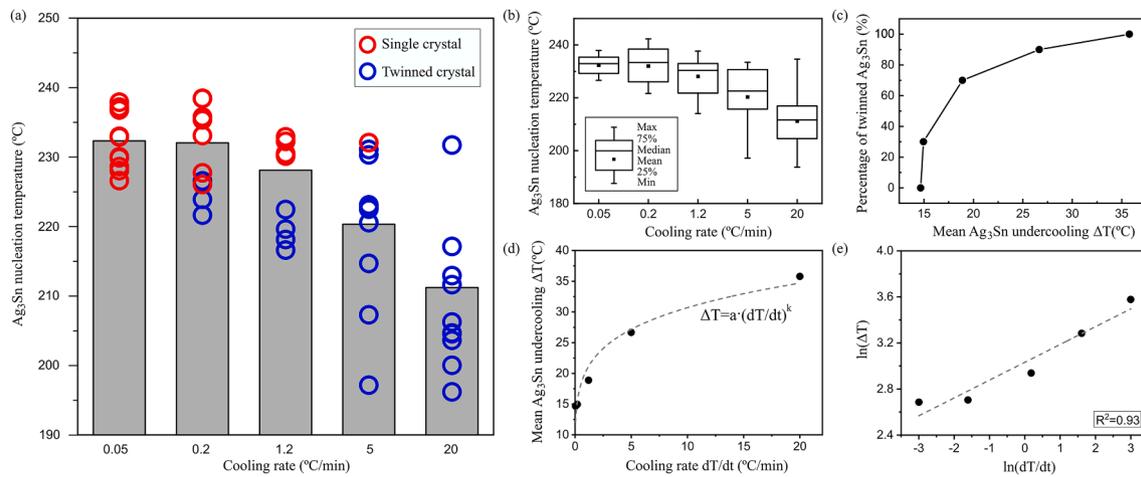
When the undercooling exceeded ~40 °C, there were still three colours observed in polarised light imaging but the Ag<sub>3</sub>Sn plates also branched during growth and formed parallel plates. Such branching became more frequent at deeper undercooling. For example, there is one parallel plate in Fig. 3(c) and (d), and multiple parallel plates in Fig. 3(e)-(g).

When examining Fig. 3, note that parallel plates always have the same single colour in polarised light imaging (and nonparallel plates always have a different colour), all plates are consistent with {001} facets, and all plates within one ball share the same pseudo-HCP orientation indicating a single Ag<sub>3</sub>Sn nucleation event per sample. Combining all parts of Fig. 3 we can see how the undercooling, which determines the growth velocity, affects crystal growth: (i) at the smallest undercoolings Ag<sub>3</sub>Sn grew as single crystal plates; (ii) as the undercooling deepened Ag<sub>3</sub>Sn grew as cyclic twinned plates where the twinning occurred only at the start of growth; (iii) at deeper undercooling, the cyclic twinned plates additionally branched during growth by twin-mediated branching resulting in multiple parallel plates; and (iv) the extent of twin-mediated branching increased as the undercooling became deeper resulting in more complicated and irregular shapes.

At deeper undercoolings, the nucleation of β-Sn started to affect the growth of Ag<sub>3</sub>Sn, as shown in Fig. 3(e)-(g). For Fig. 3(e) and (g), there is a small temperature (and time) interval between the nucleation of Ag<sub>3</sub>Sn and β-Sn, allowing the Ag<sub>3</sub>Sn to retain its growth shape from rapid growth by being ‘quenched’ by rapid β-Sn growth. For example, from the cooling curve in Fig. 3(e) the undercooling for primary Ag<sub>3</sub>Sn is 58.20 °C, and β-Sn formed soon (~3 °C) after Ag<sub>3</sub>Sn nucleation. In contrast, Fig. 3(f) shows a sample with similar Ag<sub>3</sub>Sn undercooling (60.50 °C) but different β-Sn nucleation temperature which is ~20 °C below Ag<sub>3</sub>Sn nucleation allowing more time for Ag<sub>3</sub>Sn growth and coarsening.

The Ag<sub>3</sub>Sn plate thickness was measured for the plates in Fig. 3(a)-(g) correcting the 2D measurements by accounting for the tilt angle between the (001) plate normal and the sectioning plane using the Euler angles obtained from EBSD. The Ag<sub>3</sub>Sn plate thickness is plotted versus undercooling in Fig. 4(a). The plate thickness decreases as the undercooling becomes deeper and there is also an effect of the temperature interval between the nucleation of Ag<sub>3</sub>Sn and β-Sn (as indicated in Fig. 3) which determines the growth time for Ag<sub>3</sub>Sn. In general, the plate thickness decreases with decreasing temperature interval and, comparing the primary Ag<sub>3</sub>Sn crystals with similar undercooling but significantly different growth time in Fig. 3(e) and (f), it is clear that Ag<sub>3</sub>Sn plates have the tendency to coarsen during growth.

The competition between β-Sn nucleation and primary Ag<sub>3</sub>Sn nucleation is overviewed in Fig. 4(b)-(c) as histograms of the measured nucleation onset temperature of Ag<sub>3</sub>Sn and β-Sn in Sn-5Ag and Sn-3.5Ag solder balls. The Sn-Ag binary phase diagram at the Sn-rich side from Thermo-Calc TCSD4.1 is given in Fig. 4(d). For Sn-5Ag the measured nucleation temperatures for Ag<sub>3</sub>Sn and β-Sn both follow Gaussian distributions due to the stochastic nature of the nucleation event, and the two distributions have only a small fraction of their tails overlapping indicating that, in most Sn-5Ag solder balls, the chance of primary Ag<sub>3</sub>Sn nucleation being interrupted by β-Sn nucleation is fairly small. However, for Sn-3.5Ag as the Ag<sub>3</sub>Sn liquidus temperature decreases to 215 °C, the distribution for Ag<sub>3</sub>Sn shifts to lower temperature and starts to have a large fraction overlapping with β-Sn such that once a Sn-3.5Ag ball



**Fig. 5.** (a) Ag<sub>3</sub>Sn nucleation in Sn-5Ag at five cooling rates. Grey bars are mean temperature superimposed with the nucleation temperature of Ag<sub>3</sub>Sn from 10 individual samples in red (single crystal) and blue (twinned crystal) circles. (b) Box plot of the measured Ag<sub>3</sub>Sn nucleation onset temperature at different cooling rates. (c) Percentage of twinned Ag<sub>3</sub>Sn versus the mean undercooling from different cooling rates. (d-e) The relationship between mean undercooling for Ag<sub>3</sub>Sn nucleation and cooling rate. ( $a = 18.6$ ,  $k = 0.17$  for the fitting curve).

enters the overlapping region, the nucleation of  $\beta$ -Sn may happen first and prevent primary Ag<sub>3</sub>Sn from forming. This competition between the nucleation of Ag<sub>3</sub>Sn and  $\beta$ -Sn also changes the mean value of nucleation undercooling measured for primary Ag<sub>3</sub>Sn: for Sn-5Ag the measured undercooling for Ag<sub>3</sub>Sn is  $34.3 \pm 12.4$  °C, and for Sn-3.5Ag it is almost halved:  $17.7 \pm 9.4$  °C, indicating that it is more difficult to achieve deep Ag<sub>3</sub>Sn undercooling in Sn-3.5Ag due to the interruption by  $\beta$ -Sn nucleation.

In this study, the nucleation of primary Ag<sub>3</sub>Sn in freestanding solder balls was measured to be stochastic and relatively deep (Fig. 4), which indicates nucleation difficulties for primary Ag<sub>3</sub>Sn similar to those for  $\beta$ -Sn. This finding is significantly different to statements in the literature that the nucleation and ensuing growth of Ag<sub>3</sub>Sn occurs with minimal undercooling [11,12,34,37,38,41,58-60]. One reason for this discrepancy is the different sample mass used in past work. For example, in the DTA study of Moon et al. [35] their samples were much larger (2 g) than solder balls and their primary Ag<sub>3</sub>Sn exhibited undercooling  $\leq 5$  °C.

### 3.1.4. Effects of cooling rate on growth morphology

Fig. 5 is a summary of the relationship between cooling rate, nucleation undercooling and twinning frequency in Sn-5Ag. The mean nucleation temperature for Ag<sub>3</sub>Sn from 10 Sn-5Ag balls for each cooling rate is plotted in grey in Fig. 5(a). For each cooling rate, 10 samples with a range of undercooling were examined and the results are indicated by the red (single crystal) and blue (cyclic twinned) circles with respect to their Ag<sub>3</sub>Sn nucleation onset temperature. At the lowest cooling rate (0.05 K/min), all Ag<sub>3</sub>Sn were single crystals. With increasing cooling rate (0.2, 1.2 and 5 K/min), more Ag<sub>3</sub>Sn grew as twinned crystals which tended to form at lower temperature compared to the single crystals, i.e. the twinned crystals formed at deeper undercooling. At the highest cooling rate (20 K/min), all Ag<sub>3</sub>Sn formed as twinned crystals. In order to visualise the nucleation temperature data, Fig. 5(b) is a box plot for all the nucleation onset temperatures collected from the five cooling rates. We can see that, although for each cooling rate there is a wide range between the minimum and maximum value, the median and the mean value from each group give a clear trend that, with increasing cooling rate, the onset temperature for Ag<sub>3</sub>Sn nucleation decreases. The mean undercooling at different cooling rates was calculated from Fig. 5(b) with the liquidus temperature for Ag<sub>3</sub>Sn in Sn-5Ag measured as 247 °C with the cyclic DSC experiment. Fig. 5(c) quantifies the relationship between the twinning frequency and undercooling: the deeper the undercooling, the more likely that Ag<sub>3</sub>Sn grows as a twinned crystal.

Furthermore, in Fig. 5(b) the range of Ag<sub>3</sub>Sn nucleation temperatures

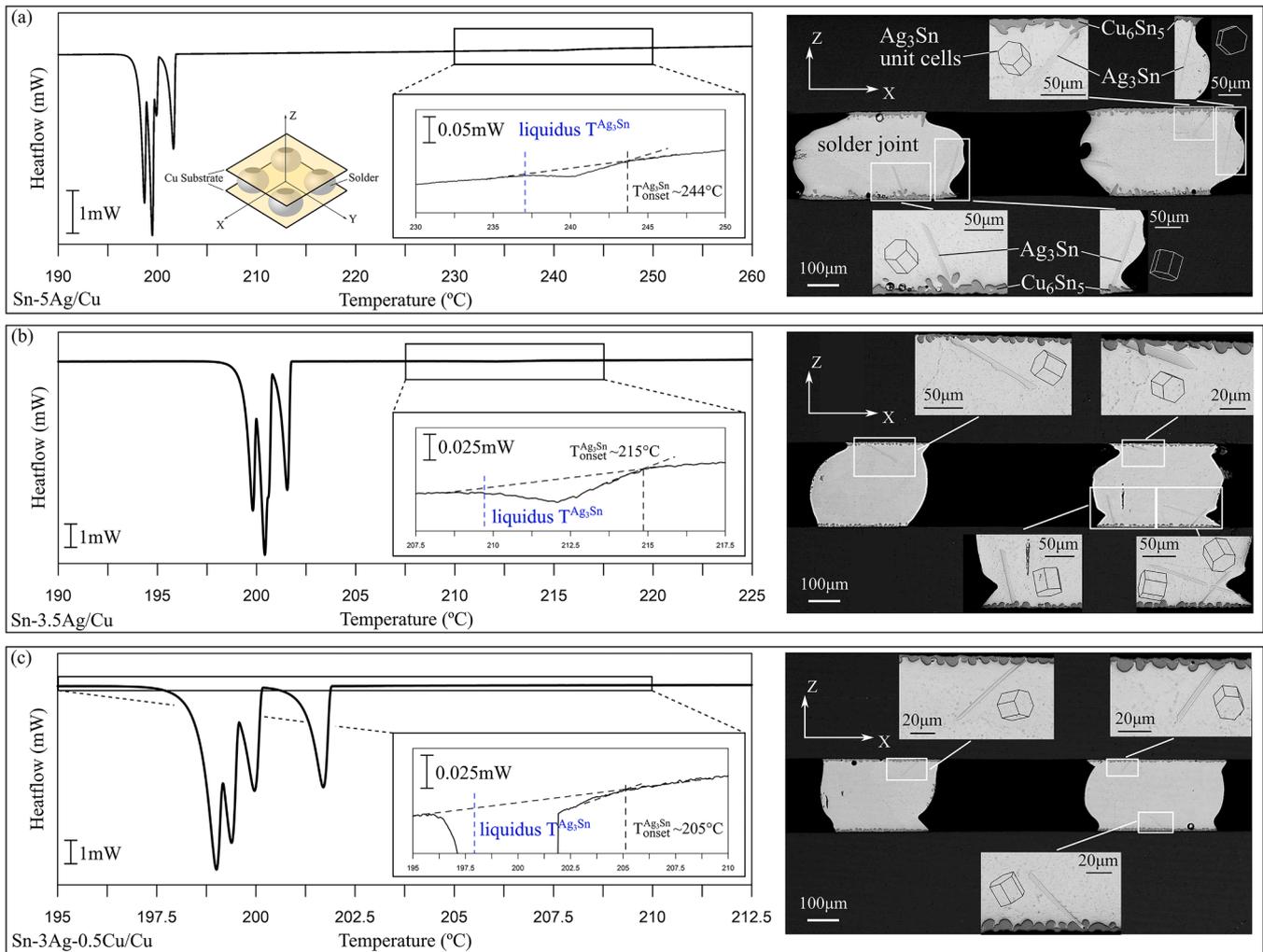
at each cooling rate indicates that the nucleation of Ag<sub>3</sub>Sn in each small ( $\sim 500$   $\mu\text{m}$  diameter) ball is independent and stochastic, but the whole group of statistical data in Fig. 5(b) reveals a clear trend between the nucleation undercooling and cooling rate: the higher the cooling rate, the deeper the undercooling that is reached in the melt. The relationship between the measured undercooling for Ag<sub>3</sub>Sn and cooling rate are plotted in Fig. 5(d) and (e): the mean nucleation undercooling increases with cooling rate with a near-linear increase of  $\ln(\Delta T)$  with respect to  $\ln(dT/dt)$ , as shown with the logarithmic coordinates in Fig. 5(e). A similar relationship has also been reported in other systems [62-64].

### 3.1.5. Origins of cyclic twinning in Ag<sub>3</sub>Sn

From the previous sections, we see that cyclic twinning depends mostly on the undercooling at which Ag<sub>3</sub>Sn nucleates, with deeper undercoolings promoting cyclic twin formation. We next consider possible mechanisms leading to cyclic twinned Ag<sub>3</sub>Sn.

Cyclic twins in Ag<sub>3</sub>Sn are three interpenetrating plates that emanate from a common centre (Fig. 2). Thus, cyclic twinning is expected to originate during the nucleation process and/or the very early stages of growth in the undercooled melt. Indeed, towards the end of this paper, we present real-time synchrotron imaging of Ag<sub>3</sub>Sn cyclic twin growth in a solder joint on a copper substrate that directly proves that the cyclic twin grows from a common point from the earliest time that the crystal could be resolved.

From Fig. 1(f), we note that the atomic positions in the Ag<sub>3</sub>Sn crystal structure are almost identical to the HCP structure and that the lower symmetry orthorhombic structure arises mostly from chemical order in the crystal structure. Thus, one possibility is that cyclic twinning in Ag<sub>3</sub>Sn emerges from chemical disorder at the start of solidification. There are various ways that this might happen. One is that the nucleus structure may be chemically disordered or have imperfect chemical ordering, raising the symmetry to hexagonal. Another way is that disorder trapping may occur in the early stages of growth if the initial solid-liquid interface velocity is sufficiently high that equilibrium chemical ordering is not achieved when atoms join the advancing interface at high undercooling [65,66]. This too could result in initial growth with metastable hexagonal symmetry. It may not be necessary to have full disorder trapping, a high density of growth defects may be enough to give the first nanoscale solid hexagonal rather than orthorhombic symmetry. The subsequent growth of the equilibrium orthorhombic Ag<sub>3</sub>Sn structure from an HCP-like centre could occur in various ways. For example, the hexagonal structure could transform into orthorhombic Ag<sub>3</sub>Sn by a disorder-order type reaction, or orthorhombic



**Fig. 6.** DSC cooling curves and microstructures of  $2 \times 2$  solder joint arrays with Cu substrates: (a) Sn-5Ag, (b) Sn-3.5Ag and (c) Sn-3Ag-0.5Cu. The calculated  $\text{Ag}_3\text{Sn}$  liquidus temperature is highlighted in blue dashed lines with nucleation onset temperature indicated by the extrapolation method. Orientations of the  $\text{Ag}_3\text{Sn}$  plates were plotted using hexagonal unit cell wireframes measured by EBSD.

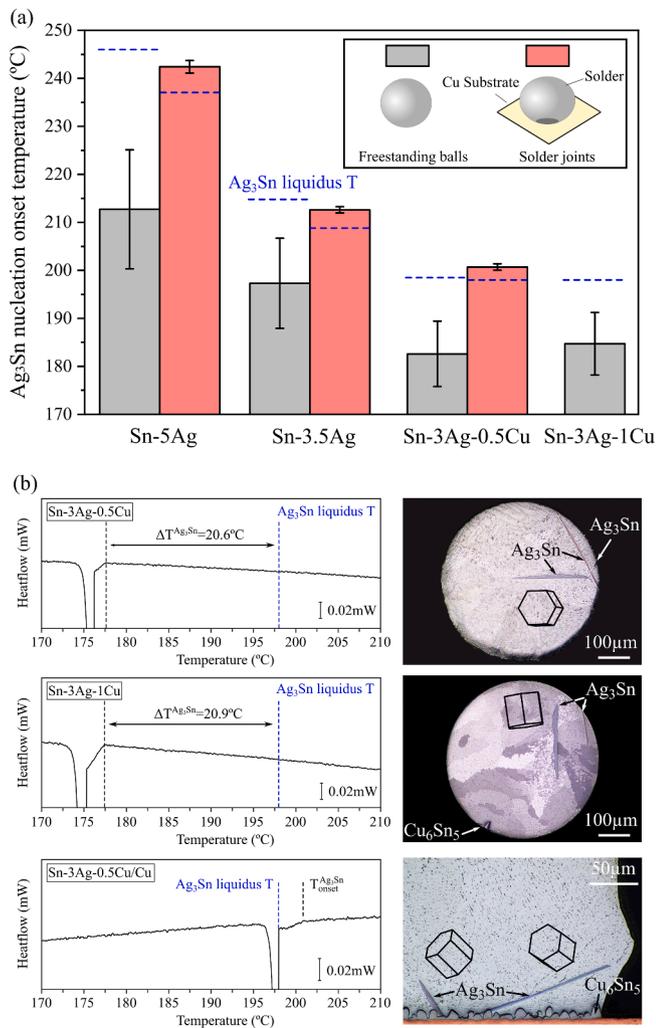
$\text{Ag}_3\text{Sn}$  could nucleate on the HCP centre and grow off epitaxially. Both would result in the three orientations of  $\text{Ag}_3\text{Sn}$  growing from a common centre, each one a variant of the following orientation relationship (OR) with respect to a single HCP orientation. To obtain evidence for or against these ideas, future research could study the local structure and chemical ordering at the centre of  $\text{Ag}_3\text{Sn}$  cyclic twins with atomic resolution characterisation techniques.

$$\{001\}_{\text{Ag}_3\text{Sn}} \parallel \{10\bar{1}0\}_{\text{HCP}} \ \& \ \langle 100 \rangle_{\text{Ag}_3\text{Sn}} \parallel \langle 0001 \rangle_{\text{HCP}}$$

A second possibility is that cyclic twinning may be related to growth twinning in the early stages of growth without chemical disorder at the start of solidification. Our results in Fig. 3(d-g) show that growth twinning occurred away from the nucleation point when the bulk undercooling reached  $\sim 50^\circ\text{C}$ , resulting in complex-shaped branched crystals. It is feasible that similar growth twinning could occur close to the nucleation point at smaller undercooling generating three orientations in the very early stages of solidification. The driving force for growth twinning seems to be related to the preferred growth directions of  $\text{Ag}_3\text{Sn}$ . This orthorhombic phase is constrained by crystal symmetry to grow as a  $\{001\}$  plate (Fig. 1(a)-(e)) which produces quasi-2D growth. Multiple growth twinning in the very early stages of solidification would create another two orientations and allow the twinned crystal to grow more effectively in 3D when there is a high driving force (undercooling) for growth. Presumably, this is also the origin of twin-mediated

branching during growth far from the nucleation point that leads to the complex branched growth shapes at deeper undercooling in Fig. 3 (e)-(g).

It is instructive to compare our findings with previous work on cyclic twinning in other phases.  $\text{Ag}_3\text{Sn}$  has similarities to cyclic twinning in other low symmetry intermetallics with a close structural relationship to a higher symmetry crystal structure, and that form during solidification as a primary phase. In these cases, the cyclic twins usually contain all variants of the orientation relationship with the higher symmetry structure. For example, cyclic twins in monoclinic  $\text{Al}_{13}\text{Fe}_4$  contain ten orientations each rotated  $\sim 36^\circ$  around a common  $\langle 010 \rangle$  and are the ten variants of the orientation relationship with a decagonal quasicrystal to which  $\text{Al}_{13}\text{Fe}_4$  is an approximant [67–69]. In another example, cyclic twins in rhombohedral  $\text{Al}_8\text{Mn}_5$  contain four orientations each rotated  $\sim 90^\circ$  around the three common  $\langle 1\bar{1}02 \rangle$  and are the four variants of the orientation relationship with a higher symmetry cubic gamma brass ( $\text{Cu}_5\text{Zn}_8$ ) [70]. In  $\text{Ag}_3\text{Sn}$ , the cyclic twin contains three orientations that are the three variants of the orientation relationship to the higher symmetry HCP structure. All could form by mechanisms similar to those outlined above although further work is required to explore if the detailed mechanisms are the same in all these cases. It is clear that cyclic twinning is a common feature of solidification when an intermetallic compound differs from a higher symmetry crystal structure only by a small distortion and different chemical ordering (e.g. Fig. 1(f) in the case



**Fig. 7.** (a) Mean and standard deviation nucleation onset temperature for  $\text{Ag}_3\text{Sn}$  in Sn-5Ag, Sn-3.5Ag, Sn-3Ag-0.5Ag and Sn-3Ag-1Cu freestanding solder balls (grey) and corresponding joints with Cu substrates (red). The calculated liquidus temperature is highlighted in blue dashed lines. (b) Cooling curves and microstructures for one Sn-3Ag-0.5Cu, Sn-3Ag-1Cu and Sn-3Ag-0.5Cu/Cu samples. Liquidus temperature and undercooling are marked. Polarised optical images superimposed with the orientations of  $\text{Ag}_3\text{Sn}$  plates plotted in hexagonal unit cell wireframes measured by EBSD.

of  $\text{Ag}_3\text{Sn}$ .

Another important example for electronic soldering is the cyclic twinning of tetragonal  $\beta$ -Sn during solidification of ball grid array solder joints [71–75]. This involves three orientations related by  $\sim 60^\circ$  rotations around a common (100) axis [74], giving the cyclic twin pseudo-hexagonal character. Similar to  $\text{Ag}_3\text{Sn}$ , cyclic twinning in  $\beta$ -Sn is promoted by deeper nucleation undercooling [71]. Lehman et al. [74] proposed that cyclic twinning in  $\beta$ -Sn starts at the nucleation stage and presented a pseudo/metastable hexagonal nucleus structure with a Cu or Ag atom at its centre. This nucleus structure is simpler and requires less atomic organisation than the stable  $\beta$ -Sn structure, which is analogous to a simpler chemically-disordered HCP nucleus for  $\text{Ag}_3\text{Sn}$ . However,  $\text{Ag}_3\text{Sn}$  is a simpler case since orthorhombic  $\text{Ag}_3\text{Sn}$  differs from the higher symmetry HCP structure only by chemical ordering (Fig. 1(f)).

### 3.2. $\text{Ag}_3\text{Sn}$ in Sn-Ag-Cu alloys and joints on copper substrates

The effects of soldering to a Cu substrate are presented in Fig. 6 using Sn-5Ag/Cu, Sn-3.5Ag/Cu and Sn-3Ag-0.5Cu/Cu joints as examples. For each composition, a  $2 \times 2$  array of joints was used, similar to the inset

sketch in Fig. 6(a), and reflowed in the DSC by holding for 10 min at the peak temperature (280 °C for Sn-5Ag/Cu, and 230 °C for Sn-3.5Ag/Cu and Sn-3Ag-0.5Cu/Cu) before cooling at 5 K/min in the DSC. In each case four peaks associated with  $\beta$ -Sn nucleation and growth can be identified in the DSC traces while the four primary  $\text{Ag}_3\text{Sn}$  peaks are smeared into one broad peak highlighted in the black boxes in the enlarged insets. Examination of the microstructures in Fig. 6 reveals that all  $\text{Ag}_3\text{Sn}$  grew as simple plates similar to Fig. 1(a) and 3(a), and there were commonly multiple plates in the cross-section that all grew from the  $\text{Cu}_6\text{Sn}_5$  reaction layer, either the top or bottom layer or both. EBSD confirmed that all these plates are independent and correspond to different pseudo-HCP orientations, as shown in the unit cell wireframes plotted next to the plates, indicating multiple  $\text{Ag}_3\text{Sn}$  nucleation events in these joints. From Fig. 6, we can conclude that soldering to a Cu substrate in a DSC caused multiple  $\text{Ag}_3\text{Sn}$  nucleation events, simple  $\text{Ag}_3\text{Sn}$  plates without twinning, and a much narrower range of  $\text{Ag}_3\text{Sn}$  nucleation temperatures than in freestanding Sn-Ag balls in Fig. 3 and 4.

To understand how soldering to a Cu substrate catalyses  $\text{Ag}_3\text{Sn}$  nucleation compared with freestanding Sn-Ag balls (Fig. 6 versus Figs. 3 and 4), the relative importance of Cu solute, primary  $\text{Cu}_6\text{Sn}_5$  crystals and the  $\text{Cu}_6\text{Sn}_5$  layer are considered next by comparing freestanding balls and joints of Sn-5Ag, Sn-3.5Ag, Sn-3Ag-0.5Cu and Sn-3Ag-1Cu (wt.%). Note that Sn-3Ag-1Cu is hypereutectic with respect to the  $\text{Cu}_6\text{Sn}_5$  liquidus and primary  $\text{Cu}_6\text{Sn}_5$  forms before the  $\text{Ag}_3\text{Sn}$  liquidus temperature is reached.

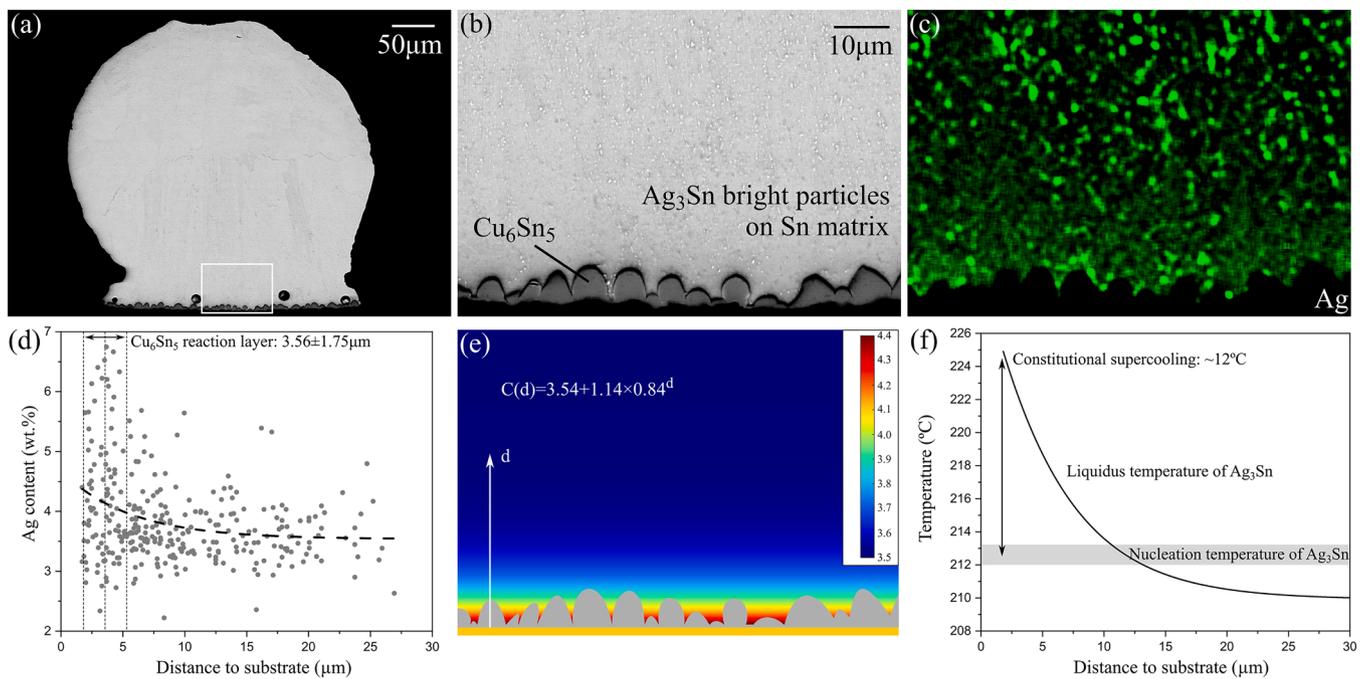
Fig. 7(a) summarises all the measured nucleation onset temperatures for freestanding balls (grey) and Cu-substrate joints (red), together with their corresponding liquidus temperatures (blue dashed lines) for primary  $\text{Ag}_3\text{Sn}$ .

For freestanding balls in Fig. 7(a), Sn-5Ag had a deeper mean  $\text{Ag}_3\text{Sn}$  undercooling than the other three compositions because there is less interruption from  $\beta$ -Sn nucleation as discussed in Section 3.1.3. Sn-3.5Ag and Sn-3Ag-0.5Cu freestanding balls had similar mean  $\text{Ag}_3\text{Sn}$  nucleation undercooling (i.e. the temperature interval between the blue dashed line and the grey bar in Fig. 7(a)) and standard deviation, indicating that Cu solute in the liquid does not significantly affect the  $\text{Ag}_3\text{Sn}$  nucleation undercooling. Similarly, Sn-3Ag-0.5Cu and Sn-3Ag-1Cu freestanding balls had similar mean nucleation undercooling and deviation range, indicating that the presence of  $\text{Cu}_6\text{Sn}_5$  primary crystals does not significantly affect the  $\text{Ag}_3\text{Sn}$  nucleation undercooling.

For solder joints with Cu substrates, the  $\text{Ag}_3\text{Sn}$  nucleation onset temperature is significantly higher than for the corresponding solder ball compositions with much narrower variation range and, similar to Fig. 6, all joints nucleated above their calculated  $\text{Ag}_3\text{Sn}$  liquidus temperature.

Three specific examples are shown in Fig. 7(b) to further illustrate these points. The first two are freestanding balls of Sn-3Ag-0.5Cu and Sn-3Ag-1Cu where the  $\text{Ag}_3\text{Sn}$  nucleated at similar undercooling and  $\beta$ -Sn nucleation occurred at  $1\sim 2^\circ\text{C}$  below. The  $\text{Ag}_3\text{Sn}$  plates have different colours under polarised optical microscopy indicating multiple  $\text{Ag}_3\text{Sn}$  (orthorhombic) orientations and EBSD showed these to have one pseudo-HCP orientation that is plotted as a wireframe, indicating a single  $\text{Ag}_3\text{Sn}$  nucleation event in each ball. In Sn-3Ag-1Cu, primary  $\text{Cu}_6\text{Sn}_5$  is also present as labelled but it is located far from the  $\text{Ag}_3\text{Sn}$  and no simple orientation relationship was measured between primary  $\text{Cu}_6\text{Sn}_5$  and  $\text{Ag}_3\text{Sn}$  in this or any other sample investigated, further showing that primary  $\text{Cu}_6\text{Sn}_5$  did not significantly affect the nucleation of primary  $\text{Ag}_3\text{Sn}$ . The third example shows a Sn-3Ag-0.5Cu/Cu joint with multiple (two) independent  $\text{Ag}_3\text{Sn}$  plates and an  $\text{Ag}_3\text{Sn}$  nucleation onset temperature that is significantly higher than in the freestanding solder balls.

From Fig. 7, it can be concluded that solder joints on Cu substrates resulted in multiple  $\text{Ag}_3\text{Sn}$  nucleation events (Figs. 6 and 7(b)) and nucleation onset temperatures that were significantly higher than their corresponding solder balls and with much narrower variation range (Fig. 7(a)). This contrasts with Cu solute and the presence of primary



**Fig. 8.** (a) The microstructure of a quenched Sn-3.5Ag/Cu joint. (b) Enlarged view of the white box area in (a). (c) The EDX Ag map of the same area as (b). (d) Ag content from multiple EDX point analysis versus measured distance to the Cu substrate. The Ag distribution is fitted with the black dashed line. The thickness of  $\text{Cu}_6\text{Sn}_5$  is plotted with vertical grey dotted lines. (e) A contour plot showing the change of Ag content near the  $\text{Cu}_6\text{Sn}_5$  reaction layer calculated from the black dashed line in (d). The function of the fitted line is also marked. (f) The change of  $\text{Ag}_3\text{Sn}$  liquidus temperature with distance from the Cu substrate. The measured  $\text{Ag}_3\text{Sn}$  nucleation temperature range from Fig. 7 is highlighted in grey and the constitutional supercooling is highlighted close to the  $\text{Cu}_6\text{Sn}_5$  reaction layer.

$\text{Cu}_6\text{Sn}_5$  crystals which had little effect on  $\text{Ag}_3\text{Sn}$  nucleation and shows that it is the  $\text{Cu}_6\text{Sn}_5$  reaction layer that promotes the nucleation of  $\text{Ag}_3\text{Sn}$ .

To assess the  $\text{Ag}_3\text{Sn}$  nucleation undercooling in joints, we need to consider the change in liquid composition due to copper substrate dissolution. The liquidus temperature for each composition was calculated using the Thermo-Calc TCSD4.1 database assuming that Cu solute is fully saturated in the melt at the peak temperature during holding, which is reasonable as previous experiments and calculations confirmed that, for 500  $\mu\text{m}$  solder balls, 10 min are enough for Cu to saturate into the melt from the substrate [76,77]. Assuming uniform saturated melts, the calculated  $\text{Ag}_3\text{Sn}$  liquidus temperature is plotted for all compositions as blue dashed lines in Figs. 6, 7(a) and 7(b). In all cases, the  $\text{Ag}_3\text{Sn}$  nucleation onset temperature is above this  $\text{Ag}_3\text{Sn}$  liquidus temperature, making the nucleation undercooling appear negative which is unphysical. This shows that the assumption of a uniform liquid composition is invalid and we need to also consider the variation in Ag content in the liquid due to the growth of  $\text{Cu}_6\text{Sn}_5$  layer.

In order to investigate the Ag solute field in the liquid before  $\text{Ag}_3\text{Sn}$  nucleation, Sn-3.5Ag/Cu joints were heated to 230  $^\circ\text{C}$ , held for 10 min and then quenched in water. The cross section of such a solder joint is shown in Fig. 8(a) where no primary  $\text{Ag}_3\text{Sn}$  plates formed. The enlarged BSE image in Fig. 8(b) highlights the small  $\text{Ag}_3\text{Sn}$  eutectic particles in the bulk and between the scallops of the  $\text{Cu}_6\text{Sn}_5$  reaction layer. EDX elemental mapping of the same area in Fig. 8(c) reveals a highly heterogeneous Ag composition field caused by the liquid solidifying to produce a mixture of  $\text{Ag}_3\text{Sn}$  particles containing  $\sim 73$  wt.% Ag and  $\beta$ -Sn containing  $\sim 0.07$  wt.% Ag (calculated with Ref [61]). Note in Fig. 8(c) that the EDX map implies that the top  $\text{Ag}_3\text{Sn}$  particles are much larger than they are in Fig. 8(b); for more quantitative analysis EDX point analysis is required.

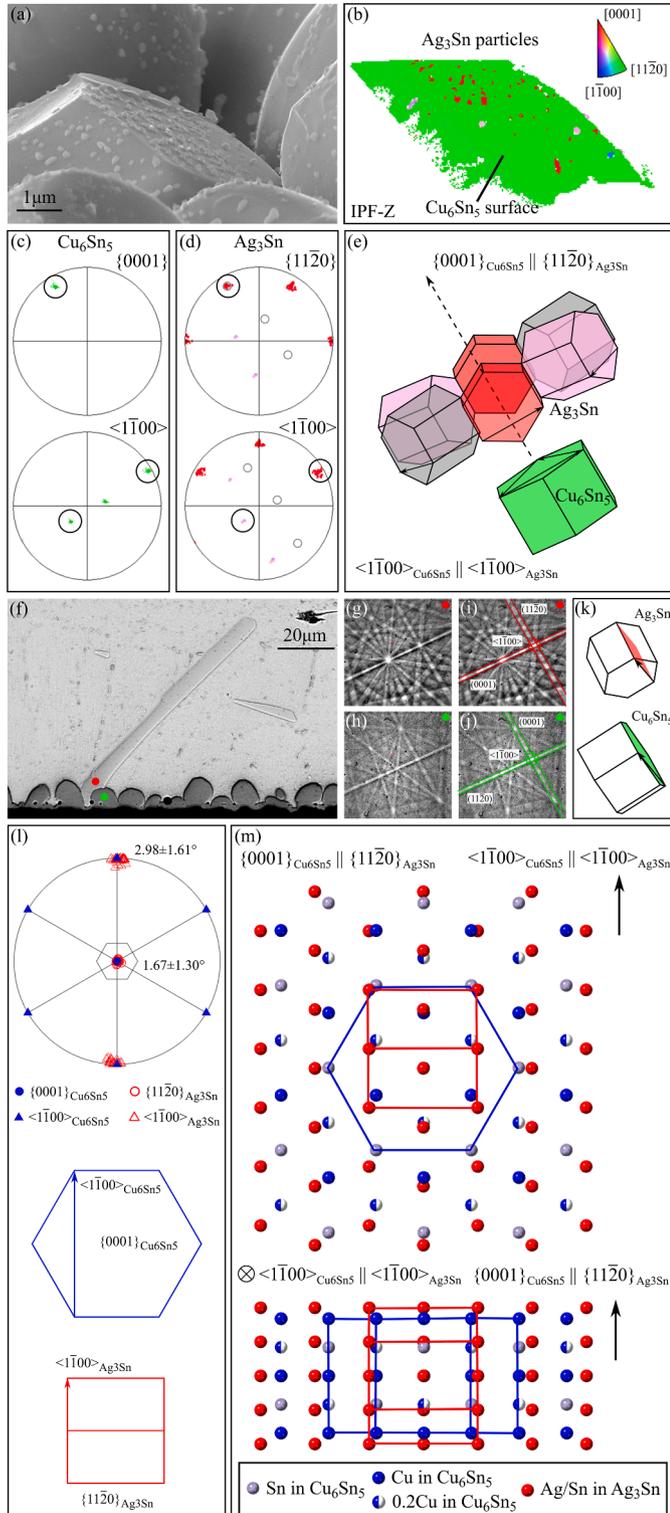
To quantify the original liquid solute field, averaging of more than 300 chemical analysis points near the bottom of the solder joint was performed. The individual data points are plotted in Fig. 8(d) as composition versus distance to the Cu substrate. The average thickness

of the  $\text{Cu}_6\text{Sn}_5$  reaction layer was measured to be  $3.56 \pm 1.75$   $\mu\text{m}$  and is highlighted with the dashed lines. The data points between these lines correspond to points located in the gaps between the  $\text{Cu}_6\text{Sn}_5$  crystals/scallops. The large scatter in the data is due to different amounts of  $\text{Ag}_3\text{Sn}$  and  $\beta$ -Sn phases in the electron interaction volume at each measurement point and averaging is required to access the original liquid composition. All the data points were fitted with the thick dashed line which describes the distribution of Ag content with respect to the distance to the substrate. As can be seen, the Ag content decreases with increasing distance from the substrate and, for the area far from the substrate, the mean Ag content is close to 3.5 wt.% which is consistent with the bulk composition. The function of the fitted curve is written in Fig. 8(e), together with a contour plot of this change of Ag content and a sketch of the  $\text{Cu}_6\text{Sn}_5$  layer from the same region and scale of Fig. 8(b). From Fig. 8(e), we see how Ag solute was rejected into the liquid during  $\text{Cu}_6\text{Sn}_5$  layer growth and accumulated naturally in the gaps and valleys between  $\text{Cu}_6\text{Sn}_5$  scallops due to the scallop growth shape. This rejection of Ag is consistent with there being negligible solubility for Ag in the  $\text{Cu}_6\text{Sn}_5$  phase [35].

Combining the measured Ag profile in Fig. 8(d) and (e) with calculations of the  $\text{Ag}_3\text{Sn}$  liquidus temperature for these compositions in Thermo-Calc TCSD4.1, the relation between the  $\text{Ag}_3\text{Sn}$  liquidus temperature and distance from the Cu substrate was obtained and is plotted in Fig. 8(f). The range of measured nucleation temperatures for  $\text{Ag}_3\text{Sn}$  in Sn-3.5Ag/Cu joints in Fig. 7(a) is also plotted on Fig. 8(f) as a grey band. We see that the only locations where  $\text{Ag}_3\text{Sn}$  could have nucleated in undercooled liquid are  $< \sim 10$   $\mu\text{m}$  from the Cu substrate. Thus, thermodynamically, we can infer that  $\text{Ag}_3\text{Sn}$  must have nucleated on or near the  $\text{Cu}_6\text{Sn}_5$  reaction layer in all joints on Cu substrates in Figs. 6 and 7(a) because their  $\text{Ag}_3\text{Sn}$  nucleation temperatures are all above the liquidus temperature of the bulk (far field) liquid. This is a form of constitutional supercooling (up to  $\sim 12$   $^\circ\text{C}$  in Fig. 8(f)) with respect to the  $\text{Ag}_3\text{Sn}$  liquidus temperature due to the local accumulation of Ag solute in the liquid during diffusion ahead of the  $\text{Cu}_6\text{Sn}_5$  layer. Nucleation of  $\text{Ag}_3\text{Sn}$  on the  $\text{Cu}_6\text{Sn}_5$  layer is also consistent with all  $\text{Ag}_3\text{Sn}$  plates being in

contact with the  $\text{Cu}_6\text{Sn}_5$  layer in the micrographs in Fig. 6.

Fig. 8(f) also shows that, when  $\text{Ag}_3\text{Sn}$  nucleates on/near the  $\text{Cu}_6\text{Sn}_5$  layer in constitutionally supercooled liquid, the plate can only grow up to  $\sim 10\ \mu\text{m}$  in supercooled liquid and further plate growth then depends on the rate of external heat extraction which is slow for DSC cooling at 5 K/min. This is consistent with  $\text{Ag}_3\text{Sn}$  growing as single crystal plates (without growth twinning) in all joints on Cu in Fig. 6.



(caption on next column)

Fig. 9. (a)  $70^\circ$  tilt view of numerous  $\text{Ag}_3\text{Sn}$  particles on a  $\text{Cu}_6\text{Sn}_5$  reaction layer surface after dissolving  $\beta$ -Sn from quenched Sn-3.5Ag/Cu joint. (b) EBSD IPF-Z map of the  $\text{Cu}_6\text{Sn}_5$  surface in (a) with both  $\text{Ag}_3\text{Sn}$  and  $\text{Cu}_6\text{Sn}_5$  indexed using their corresponding hexagonal structure. (c)-(d) Pole figures for the  $\text{Cu}_6\text{Sn}_5$  and  $\text{Ag}_3\text{Sn}$  in (b) with parallel planes and directions highlighted in black circles. The  $\{11\bar{2}0\}$  and  $\langle 1\bar{1}00 \rangle$  for the grey unit cell in (e) was also plotted with grey circles. (e) The measured orientation relationship between  $\text{Ag}_3\text{Sn}$  and  $\text{Cu}_6\text{Sn}_5$ . Three  $\text{Ag}_3\text{Sn}$  orientation variants of the OR were plotted with two of them measured (red and pink) and one calculated (grey). (f) Primary  $\text{Ag}_3\text{Sn}$  growing from  $\text{Cu}_6\text{Sn}_5$  reaction layer with the same orientation relationship. The two crystals are marked in red and green. (g)-(h) The Kikuchi patterns from the  $\text{Ag}_3\text{Sn}$  and  $\text{Cu}_6\text{Sn}_5$  crystals in (f). In (i)-(j) selected parallel planes and directions are indexed on the Kikuchi patterns. (k) Unit cell wireframes of the two crystals with highlighted parallel planes and directions. (l) Summary of the OR by projecting the  $\{11\bar{2}0\}$  and  $\langle 1\bar{1}00 \rangle$  of  $\text{Ag}_3\text{Sn}$  orientations into pole figures with respect to the orientations of  $\text{Cu}_6\text{Sn}_5$ . (m) Atomic projection of  $\text{Ag}_3\text{Sn}$  and  $\text{Cu}_6\text{Sn}_5$  on their parallel planes with unit cells highlighted.

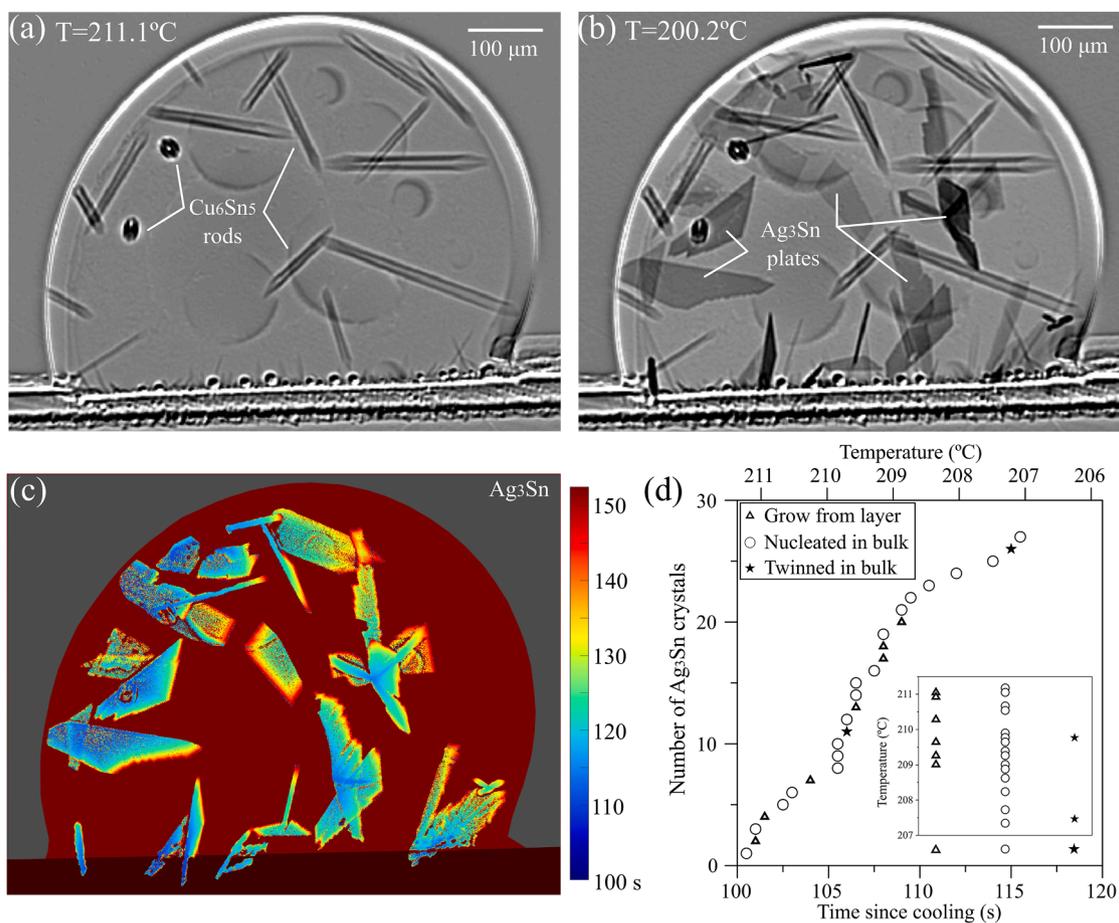
The relatively small solute-corrected nucleation undercooling for  $\text{Ag}_3\text{Sn}$  of  $\sim 12^\circ\text{C}$  (Fig. 8(f)) with narrow variation range for Sn-3.5Ag/Cu joints (Fig. 7(a)) indicates that the nucleation site itself also has a relatively higher potency and possibly higher number density than in free-standing balls. Thus, orientation relationships (ORs) between the  $\text{Cu}_6\text{Sn}_5$  layer and  $\text{Ag}_3\text{Sn}$  were explored. As revealed by Fig. 9(a), many small  $\text{Ag}_3\text{Sn}$  particles were sometimes attached to the  $\text{Cu}_6\text{Sn}_5$  reaction layer surface in quenched samples, and direct EBSD on these particles revealed that many of them shared the same OR with the  $\text{Cu}_6\text{Sn}_5$ , as can be seen in Fig. 9(a)-(e). Fig. 9(a) is a  $70^\circ$  tilted image of a faceted  $\text{Cu}_6\text{Sn}_5$  crystal in the reaction layer with multiple nanoscale  $\text{Ag}_3\text{Sn}$  on the surface. The EBSD IPF-Z map in Fig. 9(b) shows that there are three pseudo-HCP orientations indexed for the 49  $\text{Ag}_3\text{Sn}$  particles: 43  $\text{Ag}_3\text{Sn}$  in red, 5 in pink and 1 in purple. In the pole figures in Fig. 9(c) the  $\{0001\}$  plane of  $\text{Cu}_6\text{Sn}_5$  is parallel to a  $\{11\bar{2}0\}$  plane of the red and pink pseudo-HCP  $\text{Ag}_3\text{Sn}$  with two  $\langle 1\bar{1}00 \rangle$  directions of  $\text{Cu}_6\text{Sn}_5$  parallel to one of the  $\langle 1\bar{1}00 \rangle$  directions in each of the red and pink pseudo-HCP  $\text{Ag}_3\text{Sn}$  respectively, as highlighted by black circles. This orientation relationship can be written as:

$$\{11\bar{2}0\}_{\text{Ag}_3\text{Sn}} \parallel \{0001\}_{\text{Cu}_6\text{Sn}_5} \ \& \ \langle 1\bar{1}00 \rangle_{\text{Ag}_3\text{Sn}} \parallel \langle 1\bar{1}00 \rangle_{\text{Cu}_6\text{Sn}_5}$$

The OR is also plotted with the unit cell wireframes in Fig. 9(e). Theoretically, there should be three  $\text{Ag}_3\text{Sn}$  pseudo-HCP orientation variants corresponding to this OR. The missing one was calculated and is plotted in grey in Fig. 9(e) with its  $\{11\bar{2}0\}$  planes and  $\langle 1\bar{1}00 \rangle$  directions also plotted as small grey circles in pole figures in Fig. 9(d). There is only one  $\text{Ag}_3\text{Sn}$  particle (coloured in purple) at the bottom right of the surface that does not share this OR or any other simple OR with the  $\text{Cu}_6\text{Sn}_5$  crystal.

It is then natural to ask whether large  $\text{Ag}_3\text{Sn}$  plates nucleate on the  $\text{Cu}_6\text{Sn}_5$  layer with the same OR. Note that the  $\text{Ag}_3\text{Sn}$  plates are large and contact numerous different  $\text{Cu}_6\text{Sn}_5$  crystals in the  $\text{Cu}_6\text{Sn}_5$  reaction layer at the same time so we would not expect to find the nucleation OR between  $\text{Ag}_3\text{Sn}$  plates and most of the  $\text{Cu}_6\text{Sn}_5$  scallops they contact on the reaction layer. Nevertheless, the OR was measured between some primary  $\text{Ag}_3\text{Sn}$  plates and  $\text{Cu}_6\text{Sn}_5$  in the reaction layer. Fig. 9(f)-(k) gives an example. In Fig. 9(f), a large primary  $\text{Ag}_3\text{Sn}$  plate has the OR with a contacting  $\text{Cu}_6\text{Sn}_5$  grain. Fig. 9(g)-(j) are the Kikuchi patterns taken from the red and green points in Fig. 9(f) with selected parallel planes and directions indexed. Since the (001) facet of  $\text{Ag}_3\text{Sn}$  can be inferred from Fig. 9(f), the correct orthorhombic orientation can be deduced from the pseudo-HCP orientation as discussed with Figs. 1 and 2. The unit cell wireframes of the two orientations are plotted in Fig. 9(k) with the parallel planes and directions highlighted. The OR can be written in terms of orthorhombic  $\text{Ag}_3\text{Sn}$ :

$$\{010\}_{\text{Ag}_3\text{Sn}} \parallel \{0001\}_{\text{Cu}_6\text{Sn}_5} \ \& \ (001)_{\text{Ag}_3\text{Sn}} \parallel \langle 1\bar{1}00 \rangle_{\text{Cu}_6\text{Sn}_5}$$



**Fig. 10.** Synchrotron radiography of Ag<sub>3</sub>Sn plate solidification in a Sn-4Ag-0.5Cu/Cu joint (a) A frame at 211 °C when only primary Cu<sub>6</sub>Sn<sub>5</sub> crystals are present. (b) A frame at 200 °C after the nucleation and growth of Ag<sub>3</sub>Sn crystals and prior to  $\beta$ -Sn nucleation. (c) A processed image where each Ag<sub>3</sub>Sn pixel is coloured by its Ag<sub>3</sub>Sn formation time in seconds. (d) Total number of Ag<sub>3</sub>Sn crystals versus time, with an inset comparing the nucleation temperatures of different Ag<sub>3</sub>Sn types.

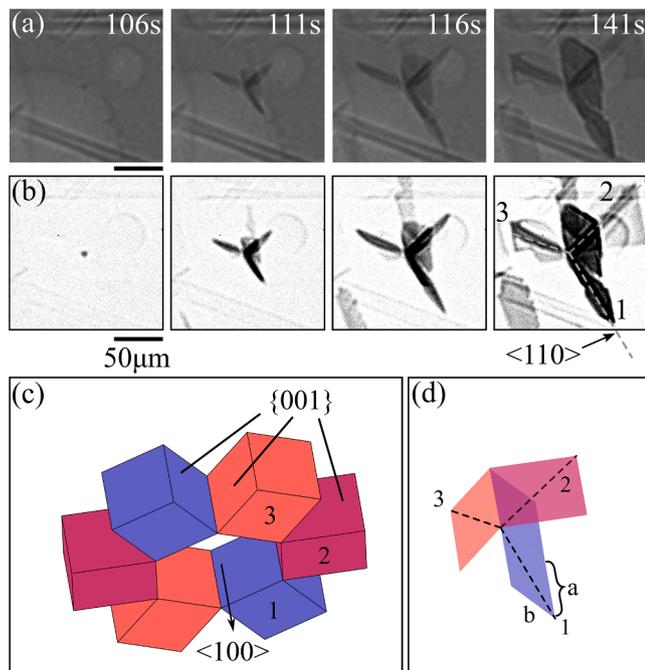
To assess the reproducibility of this OR, Fig. 9(l) summarises this OR over 53 Ag<sub>3</sub>Sn crystals (both eutectic particles and primary plates) by projecting the parallel  $\{11\bar{2}0\}$  plane and  $\langle 1\bar{1}00 \rangle$  direction of pseudo-HCP Ag<sub>3</sub>Sn into the standard pole figure of Cu<sub>6</sub>Sn<sub>5</sub>, with the deviation annotated for the parallel plane and direction. Furthermore, the superimposed crystal lattice of the two phases in Fig. 9(m) indicates a relatively low atomic mismatch with this orientation relationship, particularly along the parallel row  $\langle 1\bar{1}00 \rangle_{\text{Ag}_3\text{Sn}} \parallel \langle 1\bar{1}00 \rangle_{\text{Cu}_6\text{Sn}_5}$  which is the vertical direction in the upper part of Fig. 9(m). However, the match is less good along other directions and the overall match is significantly worse than potent nucleants in other systems such as PdSn<sub>4</sub> and  $\alpha$ -CoSn<sub>3</sub> for  $\beta$ -Sn [78,79], TiB<sub>2</sub> for  $\alpha$ -Al or Al<sub>3</sub>Ti [80,81], and Zr for  $\alpha$ -Mg [82,83]. Thus, it seems that Cu<sub>6</sub>Sn<sub>5</sub> is not a highly potent nucleant for Ag<sub>3</sub>Sn but is the lowest energy interface available for heterogeneous nucleation in the location where the liquid is constitutionally supercooled.

Previous work has shown that the Cu<sub>6</sub>Sn<sub>5</sub> layer also catalyses the nucleation of  $\beta$ -Sn in solder joints [84]. It was shown by FIB-tomography that the triple points between Cu<sub>6</sub>Sn<sub>5</sub> scallops have a 3D shape similar to conical cavities which are known to be catalytic to nucleation [85]. Thus, three factors probably combine to promote Ag<sub>3</sub>Sn nucleation on Cu<sub>6</sub>Sn<sub>5</sub> in the reaction layer: (i) constitutional supercooling which causes the maximum melt supercooling to exist between the scallops in the Cu<sub>6</sub>Sn<sub>5</sub> layer and enable Ag<sub>3</sub>Sn nucleation at a temperature higher than the liquidus temperature of the bulk liquid away from the layer; (ii) geometrical catalysis from the conical cavity-like shapes between Cu<sub>6</sub>Sn<sub>5</sub> scallops in the reaction layer; and (iii) a relatively good atomic match between Ag<sub>3</sub>Sn and Cu<sub>6</sub>Sn<sub>5</sub> for the nucleation OR.

### 3.3. Synchrotron study of Ag<sub>3</sub>Sn nucleation and growth

Fig. 10 overviews synchrotron radiography results of the nucleation and growth kinetics of primary IMCs in a Sn-4Ag-0.5Cu/Cu joint. Fig. 10 (a) is a snapshot at  $T = 211.1^\circ\text{C}$  when numerous primary Cu<sub>6</sub>Sn<sub>5</sub> have formed in the liquid as hollow rods (similar to Ref. [55]) and no Ag<sub>3</sub>Sn has yet nucleated. Note that Fig. 10(a) is a through-thickness averaged radiograph and the volume fraction of Cu<sub>6</sub>Sn<sub>5</sub> is much lower than it may appear from the projected image. Fig. 10(b) is a snapshot at lower temperature of  $T = 200.2^\circ\text{C}$  when multiple Ag<sub>3</sub>Sn plates had nucleated and grown in the bulk and near the solder-substrate. There was no evidence of Ag<sub>3</sub>Sn nucleating on the primary Cu<sub>6</sub>Sn<sub>5</sub>, consistent with the results with bulk solder joints.

To visualise and quantify the growth kinetics of the Ag<sub>3</sub>Sn plates, in Fig. 10(c), pixels containing Ag<sub>3</sub>Sn have been coloured by the time at which they first became solid Ag<sub>3</sub>Sn. As we can see, most Ag<sub>3</sub>Sn are single crystals growing from a nucleation point (blue) into a faceted plate. A few Ag<sub>3</sub>Sn share a common growth centre, indicating cyclic twinning. For example, in the centre-right of Fig. 10(c), note the dark blue three-pointed star emanating from a common centre and growing into three plates of increasingly 'hot' colours. Thus, similar to bulk samples earlier in this paper, Ag<sub>3</sub>Sn grew as single crystal plates and as cyclic twinned plates in the synchrotron samples. However, there was additionally a significant difference: in bulk solder joints (e.g. Fig. 6) Ag<sub>3</sub>Sn nucleation occurred almost exclusively on the Cu<sub>6</sub>Sn<sub>5</sub> reaction layer whereas, in the thin synchrotron samples, Ag<sub>3</sub>Sn nucleation occurred both on the Cu<sub>6</sub>Sn<sub>5</sub> reaction layer and throughout the 'bulk'. We can infer that the Ag<sub>3</sub>Sn that appear to be in the bulk are actually



**Fig. 11.** (a) Synchrotron X-ray image sequence of the nucleation and growth of twinned primary  $\text{Ag}_3\text{Sn}$  in a Sn-4Ag-0.5Cu/Cu joint. (b) Images subtracted from a frame shortly before 106 s showing three plates grow from a common point.  $\text{Ag}_3\text{Sn}$  plates appear dark. (c) Cyclic  $\text{Ag}_3\text{Sn}$  unit cells showing three twinned orientations, as measured by post-mortem EBSD. (d) Three  $\{001\}_{\text{Ag}_3\text{Sn}}$  planes taken from the unit cells resemble the growth of actual  $\text{Ag}_3\text{Sn}$  plates in (b).

attached to (and nucleated on) the cell walls since the  $\text{Ag}_3\text{Sn}$  did not move under gravity despite being significantly denser than the liquid. Thus, the thin sample geometry affected the nucleation of  $\text{Ag}_3\text{Sn}$ , with many  $\text{Ag}_3\text{Sn}$  nucleation events forming on the walls of the cell. A further factor is that the ratio of the area of substrate to the volume of solder is much smaller in thin-sample synchrotron experiments than in solder joints, promoting  $\text{Ag}_3\text{Sn}$  nucleation away from the  $\text{Cu}_6\text{Sn}_5$  layer. Fig. 10 (d) summarises the nucleation sequence of different types of  $\text{Ag}_3\text{Sn}$  crystals. Most of the single crystal  $\text{Ag}_3\text{Sn}$  plates growing from the reaction layer (triangles) tended to form at an earlier stage compared to the two cyclic twinned crystals (stars) observed forming in the bulk. The remaining single crystal plates nucleating on the cell walls (circles) nucleated throughout the whole time/temperature range.

Fig. 11 plots the detailed growth process of one of the cyclic twinned  $\text{Ag}_3\text{Sn}$  crystals by combined in-situ X-ray imaging and post-mortem EBSD. The in-situ radiography at different growth stages in Fig. 11(a) and (b) directly proves that the crystal comes from a common centre followed by growth into three large plates. Note that the greyscale depends on the thickness of  $\text{Ag}_3\text{Sn}$  where thicker and overlapping  $\text{Ag}_3\text{Sn}$  regions appear darker. The same three plates were identified on the surface of the specimen and EBSD was applied to measure their orientations. The measured orthorhombic unit cells from the three plates are plotted in Fig. 11(c). They are cyclicly twinned with  $60^\circ$  to each other along a common  $\langle 100 \rangle$ , and form a combined hexagonal symmetry similar to Fig. 2.

Combining information from the in-situ imaging in Fig. 11(a) and (b) with the crystallographic orientations from EBSD in Fig. 11(c), the  $\{001\}$  planes from the three unit cells are plotted in Fig. 11(d) aligned along their common  $\langle 100 \rangle$  twin axis with one of their  $\langle 110 \rangle$  directions highlighted with black dashed lines emanating from a nucleation point. Note in Fig. 11(d) that the plates match well with the plate shapes in Fig. 11(a) and (b), that the three plates are rectangular (in 3D) with their edges parallel to the  $\langle 100 \rangle$  and  $\langle 010 \rangle$  directions consistent with Fig. 1(a), and that each plate has a tendency of thickening along the  $\langle 110 \rangle$

direction emanating from the common centre. Plate 1 and 2 stopped growing due to the interruption of the nearby  $\text{Cu}_6\text{Sn}_5$  rods while plate 3 stops growing as it impinged on the cell wall.

Even with the significant differences in the synchrotron experiments related to the sample geometry and cooling conditions (e.g. the catalytic cell walls, different area to volume effects and local temperature gradient), the key findings are consistent with the solder joints in Figs. 6 and 7. The primary  $\text{Cu}_6\text{Sn}_5$  did not promote  $\text{Ag}_3\text{Sn}$  nucleation, while the  $\text{Cu}_6\text{Sn}_5$  reaction layer was catalytic for  $\text{Ag}_3\text{Sn}$  nucleation such that all  $\text{Ag}_3\text{Sn}$  growing from the reaction layer were single crystal plates, while cyclic twinned crystals nucleated in the bulk at relatively deeper undercooling (Fig. 10(d)). The real-time X-ray imaging proves that cyclic twins grow from a common point, indicating that cyclic twinning of  $\text{Ag}_3\text{Sn}$  occurred either in the process of nucleation or in the very early stages of growth as discussed in Section 3.1.5.

#### 4. Conclusions

This work has revealed the following new insights into the nucleation and growth of primary  $\text{Ag}_3\text{Sn}$  in 500 $\mu\text{m}$  solder balls and solder joints on copper substrates.

In freestanding Sn-Ag balls, the undercooling for  $\text{Ag}_3\text{Sn}$  nucleation is more stochastic than reported/assumed in past work, spanning the range  $\sim 10\text{--}70$  K. At the smallest undercoolings,  $\text{Ag}_3\text{Sn}$  grew as single crystal plates with  $\{001\}$  as the main facet. Deepening of the undercooling promoted  $\text{Ag}_3\text{Sn}$  cyclic twinning and, as the undercooling became deeper still, additional twin-mediated growth branching became increasingly common.

Cyclic twinned  $\text{Ag}_3\text{Sn}$  crystals are three interpenetrating plates linked by  $60^\circ$  rotations about a common  $\langle 100 \rangle$  axis, forming a combined hexagonal symmetry related to the pseudo-HCP structure of  $\text{Ag}_3\text{Sn}$ . The three plates emanate from a common centre in the undercooled melt. Possible formation mechanisms include (i) the development of chemical disorder in the process of nucleation or in the very early stages of growth, which would raise the crystal symmetry from orthorhombic to hexagonal, and/or (ii) multiple growth twinning in the early stages of growth to enable the  $\text{Ag}_3\text{Sn}$  to grow in 3D in six directions rather than as a quasi-2D plate.

There is a competition between the nucleation of  $\beta\text{-Sn}$  and  $\text{Ag}_3\text{Sn}$ . When  $\beta\text{-Sn}$  nucleates first, primary  $\text{Ag}_3\text{Sn}$  is completely suppressed. This can happen even for deep  $\beta\text{-Sn}$  undercoolings due to the stochastic nature of nucleation in both phases in freestanding balls.

Soldering to copper substrates significantly catalysed  $\text{Ag}_3\text{Sn}$  nucleation, resulting in multiple independent  $\text{Ag}_3\text{Sn}$  single crystal plates growing from the  $\text{Cu}_6\text{Sn}_5$  reaction layer with significantly higher nucleation onset temperature and narrower variation range compared to freestanding solder balls. Cu solute and primary  $\text{Cu}_6\text{Sn}_5$  appear to have no significant effect on the nucleation of  $\text{Ag}_3\text{Sn}$ . Instead, it is the  $\text{Cu}_6\text{Sn}_5$  reaction layer that promotes  $\text{Ag}_3\text{Sn}$  nucleation due to (i) constitutional supercooling generated by Ag solute rejection into the liquid between the scallops of the  $\text{Cu}_6\text{Sn}_5$  reaction layer, (ii) geometrical catalysis in the grooves between  $\text{Cu}_6\text{Sn}_5$  scallops and (iii) heterogeneous nucleation of  $\text{Ag}_3\text{Sn}$  on  $\text{Cu}_6\text{Sn}_5$  with the reproducible orientation relationship (OR):  $\{11\bar{2}0\}_{\text{Ag}_3\text{Sn}} \parallel \{0001\}_{\text{Cu}_6\text{Sn}_5}$ , with  $\langle 1\bar{1}00 \rangle_{\text{Ag}_3\text{Sn}} \parallel \langle 1\bar{1}00 \rangle_{\text{Cu}_6\text{Sn}_5}$ .

The catalysis of  $\text{Ag}_3\text{Sn}$  nucleation in solder joints results in more  $\text{Ag}_3\text{Sn}$  growing as single crystal plates and fewer growing as cyclic twinned  $\text{Ag}_3\text{Sn}$  crystals in joints compared with freestanding balls.

#### Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

## Acknowledgements

This work was partially funded by the UKEPSRC Grant EP/R018863/1. The authors acknowledge use of characterization facilities within the Harvey Flower Electron Microscopy Suite, Department of Materials, Imperial College London. Synchrotron experiments were performed on BL20XU at SPring-8 in Hyogo, Japan, under grant numbers 2015A1675 and 2020A1491.

## Supplementary materials

Supplementary material associated with this article can be found, in the online version, at doi:10.1016/j.actamat.2023.118831.

## References

- [1] C.M. Miller, I.E. Anderson, J.F. Smith, A viable tin-lead solder substitute: Sn-Ag-Cu, *J. Electron. Mater.* 23 (7) (1994) 595–601.
- [2] N.-C. Lee, *Lead-free Soldering—Where the World is Going*, Society of Manufacturing Engineers, 2000.
- [3] D.A. Shnawah, M.F.M. Sabri, I.A. Badruddin, A review on thermal cycling and drop impact reliability of SAC solder joint in portable electronic products, *Microelectron. Reliab.* 52 (1) (2012) 90–99.
- [4] P. Darbandi, et al., The effect of cooling rate on grain orientation and misorientation microstructure of SAC105 solder joints before and after impact drop tests, *J. Electron. Mater.* 43 (7) (2014) 2521–2529.
- [5] R.J. Coyle, K. Sweatman, B. Arfaei, Thermal fatigue evaluation of Pb-free solder joints: results, lessons learned, and future trends, *JOM* 67 (10) (2015) 2394–2415.
- [6] R. Coyle, et al., A collaborative industrial consortia program for characterizing thermal fatigue reliability of third generation Pb-free alloys, in: SMTA International, 2016.
- [7] R. Coyle, et al., Enhancing thermal fatigue reliability of Pb-free solder alloys with additions of bismuth and antimony, in: SMTA International, 2020, pp. 6–19.
- [8] S. Belyakov, et al., Microstructure and damage evolution during thermal cycling of Sn-Ag-Cu solders containing antimony, *J. Electron. Mater.* 50 (3) (2021) 825–841.
- [9] S. Ahmed, et al., Effects of aging on SAC-Bi solder materials, in: 15th IEEE International Conference on Thermal and Thermomechanical Phenomena in Electronic Systems (ITherm), 2016.
- [10] Moore, A. and R. Elliott, *Interface undercooling during eutectic solidification*. 1968.
- [11] D.W. Henderson, et al., Ag<sub>3</sub>Sn plate formation in the solidification of near ternary eutectic Sn-Ag-Cu alloys, *J. Mater. Res.* 17 (11) (2002) 2775–2778.
- [12] H.Y. Lu, H. Balkan, K.S. Ng, Effect of Ag content on the microstructure development of Sn-Ag-Cu interconnects, *J. Mater. Sci. Mater. Electron.* 17 (3) (2006) 171–178.
- [13] J. Campbell, *The Solidification of Metals*, 110, Iron and Steel Institute, Publication, 1968, p. 18.
- [14] J. Bromley, F. Vnuak, R. Smith, Mechanical properties of Sn-Ag<sub>3</sub>Sn alloys, *J. Mater. Sci.* 18 (10) (1983) 3143–3153.
- [15] H. Esaka, K. Shinozuka, M. Tamura, Evolution of Structure Unidirectionally Solidified Sn-Ag<sub>3</sub>Sn Eutectic Alloy, *Mater. Trans.* 46 (5) (2005) 916–921.
- [16] M. Şahin, E. Çadırli, The effects of temperature gradient and growth rate on the microstructure of directionally solidified Sn-3.5 Ag eutectic solder, *J. Mater. Sci. Mater. Electron.* 23 (2) (2012) 484–492.
- [17] N. Hou, et al., Ag<sub>3</sub>Sn Morphology Transitions During Eutectic Growth in Sn-Ag Alloys, *Metall. Mater. Trans. A* (2023).
- [18] J.-M. Song, et al., Crystallization, morphology and distribution of Ag<sub>3</sub>Sn in Sn-Ag-Cu alloys and their influence on the vibration fracture properties, *Mater. Sci. Eng.: A* 466 (1–2) (2007) 9–17.
- [19] R. Sidhu, N. Chawla, Three-dimensional microstructure characterization of Ag<sub>3</sub>Sn intermetallics in Sn-rich solder by serial sectioning, *Mater. Charact.* 52 (3) (2004) 225–230.
- [20] R. Sidhu, N. Chawla, Three-dimensional (3D) visualization and microstructure-based modeling of deformation in a Sn-rich solder, *Scr. Mater.* 54 (9) (2006) 1627–1631.
- [21] F. Ochoa, J. Williams, N. Chawla, Effects of cooling rate on the microstructure and tensile behavior of a Sn-3.5 wt.% Ag solder, *J. Electron. Mater.* 32 (12) (2003) 1414–1420.
- [22] F. Ochoa, X. Deng, N. Chawla, Effects of cooling rate on creep behavior of a Sn-3.5 Ag alloy, *J. Electron. Mater.* 33 (12) (2004) 1596–1607.
- [23] J. Keller, et al., Mechanical properties of Pb-free SnAg solder joints, *Acta Mater.* 59 (7) (2011) 2731–2741.
- [24] M. Abtey, G. Selvaduray, Lead-free solders in microelectronics, *Mater. Sci. Eng.: R: Rep.* 27 (5–6) (2000) 95–141.
- [25] E. Dalton, et al., Accelerated temperature cycling induced strain and failure behaviour for BGA assemblies of third generation high Ag content Pb-free solder alloys, *Mater. Des.* 154 (2018) 184–191.
- [26] M.N. Collins, E. Dalton, J. Punch, Microstructural influences on thermomechanical fatigue behaviour of third generation high Ag content Pb-Free solder alloys, *J. Alloy. Compd.* 688 (2016) 164–170.
- [27] S. Xu, et al., Interfacial intermetallic growth and mechanical properties of carbon nanotubes reinforced Sn<sub>3.5</sub>Ag<sub>0.5</sub>Cu solder joint under current stressing, *J. Alloy. Compd.* 595 (2014) 92–102.
- [28] W. Plumbridge, C. Gagg, The mechanical properties of lead-containing and lead-free solders—Meeting the environmental challenge, *Proc. Inst. Mech. Eng. Part L J. Mater. Des. Appl.* 214 (3) (2000) 153–161.
- [29] Y. Xu, et al., Intermetallic size and morphology effects on creep rate of Sn-3Ag-0.5 Cu solder, *Int. J. Plast.* 137 (2021), 102904.
- [30] T. Gu, C.M. Gourlay, T.B. Britton, The role of lengthscale in the creep of Sn-3Ag-0.5 Cu solder microstructures, *J. Electron. Mater.* 50 (3) (2021) 926–938.
- [31] K. Kim, S. Huh, K. Sugauma, Effects of cooling speed on microstructure and tensile properties of Sn-Ag-Cu alloys, *Mater. Sci. Eng.: A* 333 (1–2) (2002) 106–114.
- [32] S. Chang, S. Wu, Damping characteristics of Sn-3Ag-0.5 Cu and Sn-37 Pb solders studied by dynamic mechanical analysis, *Scr. Mater.* 63 (10) (2010) 957–960.
- [33] F. Lin, et al., Evolution of Ag<sub>3</sub>Sn at Sn-3.0 Ag-0.3 Cu-0.05 Cr/Cu joint interfaces during thermal aging, *J. Alloy. Compd.* 509 (23) (2011) 6666–6672.
- [34] S.K. Kang, et al., The microstructure, thermal fatigue, and failure analysis of near-ternary eutectic Sn-Ag-Cu solder joints, *Mater. Trans.* 45 (3) (2004) 695–702.
- [35] K.-W. Moon, et al., Experimental and thermodynamic assessment of Sn-Ag-Cu solder alloys, *J. Electron. Mater.* 29 (10) (2000) 1122–1136.
- [36] L. Snugovsky, et al., Some aspects of nucleation and growth in Pb free Sn-Ag-Cu solder, *Mater. Sci. Technol.* 21 (1) (2005) 53–60.
- [37] S.K. Kang, et al., Ag<sub>3</sub>Sn plate formation in the solidification of near-ternary eutectic Sn-Ag-Cu, *JOM* 55 (6) (2003) 61–65.
- [38] S.K. Kang, et al., Controlling Ag<sub>3</sub>Sn plate formation in near-ternary-eutectic Sn-Ag-Cu solder by minor Zn alloying, *JOM* 56 (6) (2004) 34–38.
- [39] I.E. Anderson, Development of Sn-Ag-Cu and Sn-Ag-Cu-X alloys for Pb-free electronic solder applications, *Lead-Free Electron. Solder.* (2006) 55–76.
- [40] K. Kim, S. Huh, K. Sugauma, Effects of intermetallic compounds on properties of Sn-Ag-Cu lead-free soldered joints, *J. Alloy. Compd.* 352 (1–2) (2003) 226–236.
- [41] S.K. Kang, et al., Formation of Ag<sub>3</sub>Sn plates in Sn-Ag-Cu alloys and optimization of their alloy composition, in: 53rd Electronic Components and Technology Conference, 2003. Proceedings, IEEE, 2003.
- [42] J. Gong, et al., Formation of Ag<sub>3</sub>Sn plates in SnAgCu solder bumps, *Mater. Sci. Eng.: A* 527 (10–11) (2010) 2588–2591.
- [43] J. Xian, et al., Anisotropic thermal expansion of Ni<sub>3</sub>Sn<sub>4</sub>, Ag<sub>3</sub>Sn, Cu<sub>6</sub>Sn<sub>5</sub> and βSn, *Intermetallics* 91 (2017) 50–64.
- [44] H. Ma, et al., In-situ study on growth behavior of Ag<sub>3</sub>Sn in Sn-3.5 Ag/Cu soldering reaction by synchrotron radiation real-time imaging technology, *J. Alloys Compd.* 537 (2012) 286–290.
- [45] M. Mueller, et al., Morphologies of Primary Cu<sub>6</sub>Sn<sub>5</sub> and Ag<sub>3</sub>Sn Intermetallics in Sn-Ag-Cu Solder Balls, *IEEE Transact. Compon., Packag. Manufact. Technol.* 10 (1) (2019) 18–29.
- [46] R. Wu, J. Perepezko, Liquidus temperature determination in multicomponent alloys by thermal analysis, *Metall. Mater. Trans. A* 31 (2) (2000) 497–501.
- [47] S. Belyakov, C. Gourlay, Recommended values for the βSn solidus line in Sn-Bi alloys, *Thermochim. Acta* 654 (2017) 65–69.
- [48] J. Xian, et al., Heterogeneous nucleation of Cu<sub>6</sub>Sn<sub>5</sub> in Sn-Cu-Al solders, *J. Alloys Compd.* 619 (2015) 345–355.
- [49] A.-K. Larsson, L. Stenberg, S. Lidin, The superstructure of domain-twinned η'-Cu<sub>6</sub>Sn<sub>5</sub>, *Acta Crystallogr., Sect. B: Struct. Sci.* 50 (6) (1994) 636–643.
- [50] A. Leineweber, C. Wieser, W. Hügel, Crystal structure of incommensurate η'-Cu<sub>1</sub>.235Sn intermetallic, *Zeitschrift für Kristallographie-Crystalline Materials* 235 (10) (2020) 445–457.
- [51] A. Leineweber, C. Wieser, W. Hügel, Cu<sub>6</sub>Sn<sub>5</sub> intermetallic: reconciling composition and crystal structure, *Scr. Mater.* 183 (2020) 66–70.
- [52] P.J. Rossi, N. Zotov, E.J. Mittemeijer, Redetermination of the crystal structure of the Ag<sub>3</sub>Sn intermetallic compound, *Zeitschrift für Kristallographie-Crystalline Materials* 231 (1) (2016) 1–9.
- [53] A. Gangulee, G. Das, M. Bever, An x-ray diffraction and calorimetric investigation of the compound Cu<sub>6</sub>Sn<sub>5</sub>, *Metall. Trans. A* 4 (9) (1973) 2063–2066.
- [54] G. Zeng, et al., *Solidification of Sn-0.7 Cu-0.15 Zn solder: in situ observation*, *Metall. Mater. Trans. A* 45 (2) (2014) 918–926.
- [55] M. Sallah, et al., In situ imaging of microstructure formation in electronic interconnections, *Sci. Rep.* 7 (1) (2017) 1–11.
- [56] J. Xian, et al., Influence of Ni on the refinement and twinning of primary Cu<sub>6</sub>Sn<sub>5</sub> in Sn-0.7 Cu-0.05 Ni, *Intermetallics* 102 (2018) 34–45.
- [57] H. Yu, et al., Defect structures in solution-grown single crystals of the intermetallic compound Ag<sub>3</sub>Sn, *J. Mater. Sci.* 53 (7) (2018) 5317–5328.
- [58] H.-W. Chiang, K. Chang, J.-Y. Chen, The effect of Ag content on the formation of Ag<sub>3</sub>Sn plates in Sn-Ag-Cu lead-free solder, *J. Electron. Mater.* 35 (12) (2006) 2074–2080.
- [59] F. Gao, H. Nishikawa, T. Takemoto, Intermetallics evolution in Sn-3.5 Ag based lead-free solder matrix on an OSP Cu finish, *J. Electron. Mater.* 36 (12) (2007) 1630–1634.
- [60] V. Vasudevan, et al., Slow cycle fatigue creep performance of Pb-Free (LF) solders, in: Proceedings 57th Electronic Components and Technology Conference, 2007.
- [61] *Thermo-Calc Software TCSD solder alloy solutions database version 4.1*.
- [62] J. Nyílty, Kinetics of nucleation in solutions, *J. Cryst. Growth* 3 (1968) 377–383.
- [63] J. Xian, et al., Cu<sub>6</sub>Sn<sub>5</sub> crystal growth mechanisms during solidification of electronic interconnections, *Acta Mater.* 126 (2017) 540–551.
- [64] G. Wanbing, et al., DSC study on the undercooling of droplet solidification of metal melt, *Chin. Sci. Bull.* 50 (9) (2005) 929.

- [65] W.J. Boettinger, M.J. Aziz, Theory for the trapping of disorder and solute in intermetallic phases by rapid solidification, *Acta Metall.* 37 (12) (1989) 3379–3391.
- [66] D.M. Herlach, Dendrite growth kinetics in undercooled melts of intermetallic compounds, *Cryst.* 5 (3) (2015) 355–375.
- [67] L.A. Bendersky, J.W. Cahn, Special grain boundaries based on local symmetries, *J. Mater. Sci.* 41 (23) (2006) 7683–7690.
- [68] Y. Cui, C.M. Gourlay, Growth twinning and morphology of Al45Cr7 and Al13Fe4, *J. Alloys Compd.* 893 (2022), 162318.
- [69] E. Louis, R. Mora, J. Pastor, *Nature of star-shaped clusters of FeAl<sub>3</sub> in aluminium–iron alloys*, *Metal Sci.* 14 (12) (1980) 591–594.
- [70] G. Zeng, J.W. Xian, C.M. Gourlay, Nucleation and growth crystallography of Al8Mn5 on B2-Al(Mn,Fe) in AZ91 magnesium alloys, *Acta Mater.* 153 (2018) 364–376.
- [71] B. Arfaei, N. Kim, E.J. Cotts, Dependence of Sn grain morphology of Sn-Ag-Cu solder on solidification temperature, *J. Electron. Mater.* 41 (2) (2012) 362–374.
- [72] A.A. Daszki, C.M. Gourlay, On the 3-D shape of interlaced regions in Sn-3Ag-0.5Cu solder balls, *J. Electron. Mater.* 50 (3) (2021) 808–817.
- [73] J. Han, F. Guo, Effects of impurities on double twinning nucleation and grain refinement of Sn-based solder joints, *J. Mater. Sci. Mater. Electron.* 29 (10) (2018) 8031–8038.
- [74] L.P. Lehman, et al., Cyclic twin nucleation in tin-based solder alloys, *Acta Mater.* 58 (10) (2010) 3546–3556.
- [75] Z.L. Ma, et al., Nucleation and twinning in tin droplet solidification on single crystal intermetallic compounds, *Acta Mater.* 150 (2018) 281–294.
- [76] M. Huang, F. Yang, Size effect model on kinetics of interfacial reaction between Sn-xAg-yCu solders and Cu substrate, *Sci. Rep.* 4 (1) (2014) 1–9.
- [77] C. Ho, et al., Theoretical and experimental determination of Cu diffusivity in eutectic Sn–Ag system at 235–280 °C, *Thin. Solid. Films* 572 (2014) 238–244.
- [78] S. Belyakov, C. Gourlay, Heterogeneous nucleation of βSn on NiSn<sub>4</sub>, PdSn<sub>4</sub> and PtSn<sub>4</sub>, *Acta Mater.* 71 (2014) 56–68.
- [79] Z. Ma, et al., Harnessing heterogeneous nucleation to control tin orientations in electronic interconnections, *Nat. Commun.* 8 (1) (2017) 1–10.
- [80] P. Schumacher, et al., New studies of nucleation mechanisms in aluminium alloys: implications for grain refinement practice, *Mater. Sci. Technol.* 14 (5) (1998) 394–404.
- [81] Y. Cui, et al., Solidification orientation relationships between Al<sub>3</sub>Ti and TiB<sub>2</sub>, *Acta Mater.* 186 (2020) 149–161.
- [82] M. Qian, D. StJohn, M. Frost, Heterogeneous nuclei size in magnesium–zirconium alloys, *Scr. Mater.* 50 (8) (2004) 1115–1119.
- [83] G. Peng, Y. Wang, Z. Fan, Competitive heterogeneous nucleation between Zr and MgO particles in commercial purity magnesium, *Metall. Mater. Trans. A* 49 (6) (2018) 2182–2192.
- [84] J. Xian, et al., Nucleation of tin on the Cu<sub>6</sub>Sn<sub>5</sub> layer in electronic interconnections, *Acta Mater.* 123 (2017) 404–415.
- [85] D. Turnbull, Kinetics of heterogeneous nucleation, *J. Chem. Phys.* 18 (2) (1950) 198–203.