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Review

Microbial and thermal treatment techniques for degradation of PFAS in biosolids: A focus on degradation mechanisms and pathways

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HIGHLIGHTS

G R A P H I C A L A B S T R A C T

- Thermal degradation of PFAS follows a 3-step random chain-scission pathway.
- Microbial degradation involves C-S bond cleavage, hydroxylation, decarboxylation.
- Nucleophilic substitution and decarboxylation are favoured in liquefaction.
- Catalysts and basic solvents promote PFAS mineralization.

ABSTRACT

Per- and polyfluoroalkyl substances (PFAS) are persistent organic chemicals detected in biosolids worldwide, which have become a significant concern for biosolids applications due to their increasing environmental risks. Hence, it is pivotal to understand the magnitude of PFAS contamination in biosolids and implement effective technologies to reduce their contamination and prevent hazardous aftermaths. Thermal techniques such as pyrolysis, incineration and gasification, and biodegradation have been regarded as impactful solutions to degrade PFAS and transform biosolids into value-added products like biochar. These techniques can mineralize PFAS compounds under specific operating parameters, which can lead to unique degradation mechanisms and pathways. Understanding PFAS degradation mechanisms can pave the way to design the technology and to optimize the process conditions. Therefore, in this review, we aim to review and compare PFAS degradation mechanisms in thermal treatment like pyrolysis, incineration, gasification, smouldering combustion, hydrothermal liquefaction (HTL), and biodegradation. For instance, in biodegradation of perfluorooctane sulfonic acid (PFOS), firstly C –S bond cleavage occurs which is followed by hydroxylation, decarboxylation and defluorination re-

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actions to form perfluoroheptanoic acid. In HTL, PFOS degradation is carried through OH⁻catalyzed series of nucleophilic substitution and decarboxylation reactions. In contrast, thermal PFOS degradation involves a three-step random-chain scission pathway. The first step includes C –S bond cleavage, followed by defluorination of perfluoroalkyl radical, and radical chain propagation reactions. Finally, the termination of chain propagation reactions produces very short-fluorinated units. We also highlighted important policies and strategies employed worldwide to curb PFAS contamination in biosolids.

1. Introduction

Sewage sludge is the by-product of wastewater treatment, which is often treated with processes like anaerobic digestion and lime treatment to meet the standard guidelines for its acceptable usage [1]. This treated sewage sludge is called biosolids. Biosolids are often enriched with essential nutrients like P and N and other essential metals such as Zn, Cu, Co, and Ni for plant growth [2,3]. As a result, biosolids are widely used for agriculture and land rehabilitation applications. Evidently, some European countries, such as Germany and Australia, utilize > 60% of their biosolids for agriculture, while in the USA, approximately 50-55% of biosolids are applied for land applications [4]. The usage of biosolids is expected to increase governments' move toward circular and sustainable economies. Biosolids are considered eco-friendly and sustainable; thus, a circular economy around biosolids could be developed. Biosolids' employment in agriculture can replace inorganic fertilizers that can reduce the greenhouse gas (GHG) emissions related to their production. Approximately 192.5 kg of CO_{2e} can be avoided by replacing 1 tonne of inorganic fertilizers with dry biosolids [4]. The carbon content of biosolids which is nearly 20%, can be converted to renewable energy, energy products, and value-added chemicals using thermochemical techniques such as pyrolysis, hydrothermal liquefaction, and anaerobic digestion. Producing green electricity from biosolids can attract Renewable Energy Credits, which could be valued at around US \$100/tonne of dry biosolids [4]. Considering all applications of biosolids, currently, the total biosolids economy is valued at US\$1.6 billion [2]. Since the usage of biosolids is expected to increase in agriculture, the biosolids economy is also projected to rise by 4.2% in the next decade [2].

Biosolids offer several advantages as nutrients for plant growth and as raw materials to produce green energy, but there are also certain challenges associated with emerging contaminants (ECs) that need to be addressed. For instance, wastewater treatment facilities are not designed to reduce ECs that finally end up in biosolids. Several ECs, including perand polyfluoroalkyl substances (PFAS), have been identified in biosolids [5,6]. PFAS are considered of significant concern due to their persistent and ubiquitous nature and associated environmental risks [7]. PFAS are synthetic fluorinated chemicals made up of strong C-F bonds, which are characterized by extreme resistance to degradation and increase bioaccumulation and mobility potential. Consequently, elevated concentrations of PFAS have been reported in biosolids as well as effluents and influents in wastewater treatment plants. PFAS contamination also increases the cost of biosolids management [8-10]. A survey in the USA revealed that the average cost of biosolids management increased nearly 37% after PFAS regulations to reduce contamination were introduced [2]. Despite such costs, the ecological risks and the toxicological effects of PFAS, it is pivotal to reduce PFAS in biosolids so that they can be converted into a safe product for niche applications.

The application of cost-effective and sustainable technologies is highly desirable to manage PFAS-contaminated biosolids by reducing their environmental risks while maintaining or improving the important physicochemical characteristics of biosolids for advantageous applications [8,11]. Thermochemical techniques such as pyrolysis and gasification have been proved successful to destruct PFAS in biosolids while maintaining the carbon and nutrients contents [12]. Consequently, these techniques have been implemented on the commercial level. For instance, gasification of biosolids at 600 °C has shown to reduce PFAS below the detection limit, producing biochar as the by-product free of PFAS [13]. Similarly, pyrolysis of biosolids at 650 °C has demonstrated to reduce PFAS of varying chain-lengths below the detection limit and produced high-quality biochar with fixed carbon and phosphorous contents [14]. More importantly, these technologies could be self-sustainable and do not require an external energy supply since the syngas produced during the processes could be used to generate energy [13,15].

Several studies have been carried out in recent years that demonstrate the presence of PFAS in biosolids (and other mediums like soil, wastewater and other aquatic systems) and suggest possible technologies to mitigate PFAS and transform biosolids into value-added products [16-18]. A few review articles have been published in recent years, focusing on treatment technologies to destruct PFAS in various wastes including biosolids [19-21]. For example, Garg et al. [22] recently published a review article on various PFAS destruction technologies such as incineration, hydrothermal liquefaction, pyrolysis, thermal hydrolysis, and supercritical water oxidation. Another article by Longendyke et al. [23] reviewed the thermal degradation of PFAS in different mediums like water, sewage sludge, soil and municipal solid waste. These articles have discussed important parameters of thermal technologies and provided valuable information on their role in PFAS degradation. However, less attention has been paid to review PFAS-degradation mechanisms in these treatment technologies and to the best of our knowledge, only one review paper has been published focusing on degradation mechanisms of PFAS in thermal techniques (mainly focusing on pyrolysis and incineration) [24], while no article has critically discussed PFAS-degradation mechanisms in hydrothermal liquefaction and biodegradation. Therefore, the primary objective of the article was to provide and compare critical information about PFAS-degradation mechanisms in biological and thermochemical techniques including hydrothermal liquefaction. Another main objective of the article was to identify the most suitable and efficient technique to mitigate PFAS in biosolids and understand the influence of biosolids composition (presence of metals like Ca and Mg) and the operating parameters of the techniques on PFAS destruction. The article also aimed to review the existing policies and regulations to restrain PFAS contamination in biosolids worldwide. In addition, the critical challenges that limit the understanding of PFAS degradation mechanisms were identified in the article, which could be taken as potential objectives for future studies. The literature for this review article was searched from different databases like Scopus and Google Scholar using individual and collective keywords such as PFAS, biosolids, pyrolysis of biosolids, thermal treatment of biosolids, biodegradation of PFAS, incineration of biosolids, and techniques for PFAS degradation. A special attention was given to include the recent five years publications.

2. Biosolids production and market value

Fig. 1a shows biosolids production by region based on the 2015 population size. It was estimated from data that more than 33 million tonnes of dry biosolids were produced worldwide in 2015. Europe produced the highest amount of biosolids, 14.7 million dry tonnes, which is 43.8% of the total biosolids around the globe [2]. Asia is the second largest biosolids producer, accounts 29.5% of the overall proportion. Biosolids production has been observed the least in the African continent, at only 0.05% [2]. In the same year, Australia reported to

produce 310,000 dry tonnes of biosolids which increased to 349,000 dry tonnes in 2021 [25]. Fig. 1b shows the Australian state-wise production of biosolids in 2019, and Fig. 1c presents the percentage usage of biosolids across Australia, suggesting Victoria is the leading state to produce the maximum amount of biosolids [25]. The major application of biosolids in Australia is agriculture. Some countries around the world utilise 50–60% of biosolids for agriculture [2,26]. Australia has been setting a benchmark for other countries for biosolids applications, it employs 67% biosolids for agriculture, 16% for land rehabilitation, and 8% for landscaping [4]. This is primarily because biosolids contain essential nutrients like N and P and other micronutrients that are readily available for plant uptake [25]. In 2021, the biosolids market around the globe was projected to be valued at around US\$1.6 Bn [27]. The usage of biosolids is expected to increase in agricultural application and revegetation of mine sites [28,29]. In addition, biosolids can also be used as a potential feedstock for several processes like pyrolysis and hydrothermal liquefaction to produce energy and value-added products like biochar [30]. Other biosolids applications that include landscaping and minor horticulture, cement, and brick making also contribute to biosolids' economy [4]. Thus, expecting an increase in the widespread usage of biosolids, its overall market is projected to surge by 4.2% in the next decade, from US\$ 1.6 Bn to US\$2.4 Bn by 2031 [27]. In Australia, total biosolids production was assessed at 371,000 tonnes in 2019 (Fig. 1b). Each tonne of dry biosolids is valued at around US\$100 for agriculture, US\$40 for land rehabilitation and landscaping, and US\$80 for energy production [4]. Based on applications of biosolids, according to Fig. 1, the market value of biosolids in Australia can be estimated at US\$30.97 million. Since agriculture is the primary market for biosolids, it could be valued at US\$24.8 million, while land rehabilitation and landscaping may contribute up to US\$3.50 million to the economy [4]. If diverting the remaining biosolids (9%) for energy production, US\$2.67 million can be further added to the economy.

Biosolids' usage contributes to a clean and sustainable economy, and it can reduce GHG emissions in two primary ways. Firstly, the organic content present in biosolids can be successfully converted to produce high-density energy products like biochar and bio-oil via thermochemical processes such as pyrolysis, gasification and hydrothermal liquefaction, and bioenergy using anaerobic digestion (AD). The AD process can produce 600–900 kWhr net energy per tonne of 90% dry biosolids, equating to around 0.6–0.9 tonne of carbon dioxide equivalents (CO_{2e}) if generating the same energy using a coal-fired power plant [4]. Since biosolids can replace non-renewable fuels to generate electricity, they can attract Renewable Energy Credits, which could be valued at around US\$100/tonne of dry biosolids [4]. Secondly, biosolids are enriched with macro and micronutrients and other organic and inorganic matter, they can replace inorganic fertilizers. Therefore, GHG emissions related to the production of fertilizers can be significantly reduced. It has been estimated that approximately 192.5 kg of CO2e can be avoided by replacing 1 tonne of inorganic fertilizers with dry biosolids. In addition, diverting 1-tonne dry biosolids from landfilling for energy production



3

can avoid 5 tonnes of CO_{2e} [4].

Nonetheless, biosolids contain essential nutrients, and their usage for different applications could be considered highly advantageous and sustainable; however, biosolids are often adulterated with various categories of emerging contaminants, such as per- and polyfluoroalkyl substances (PFAS), pharmaceutical and personal care products, endocrine-disrupting chemicals, surfactants, flame retardants, and many other potentially toxic elements [6]. The implications of these contaminants in biosolids are challenging, but PFAS are the most profound concern among all pollutants due to their recalcitrant nature and toxic effects on ecosystems and human health [20,31]. Therefore, finding additional technologies to remove the pollutants of concern and make biosolids safe to use for further applications is a priority. The fate of PFAS in biosolids and mitigation regulations/policies, and technologies have been discussed in detail in following sections.

3. Per- and polyfluoroalkyl substances in biosolids

PFAS are also known as 'forever chemicals' due to the presence of highly stable carbon-fluorine (C - F) bonds. The dissociation energy required for C-F is around 120 kcal/mol, higher than other carbonhalide bonds like C-Cl and C-Br that possess bond dissociation energies of 81 and 46 kcal/mol, respectively [32]. Other bonds like C -C and C –H also require less dissociation energy compared to C – F. In addition, the C – F bond dissociation energy in CF₃ moiety is higher than CF₂ and increases with an increase in surrounding F atoms [33]. For example, Bentel et al. [34] calculated bond dissociation energies for C-F of selected PFAS molecules and revealed that it requires higher energy (117.7–122.7 kJ mol⁻¹) to break C –F in CF₃ compared to CF₂ moiety present in the fluorinated tail (106.8–110.9 kJ mol⁻¹). Consequently, different rates of degradation and defluorination have been reported for different categories of PFAS compounds [34-36]. In PFAS, generally, the atomic radius of a C-F bond shields the perfluorinated carbon atom and C-C bonds along the perfluoroalkyl chain without steric stress. This shielding of the C-C bond by much stronger C-F bonds is one of the primary reasons for greater stability of PFAS compounds and their perseverance in the environment including biosolids or sewage sludge [33]. Fig. 2 shows a general structure of non-polymeric, perfluorinated PFAS substances, comprising hydrophobic tail and hydrophilic head, and dissociation energies required to break C -F bond.

PFAS compounds enter wastewater treatment plants (WWTPs) through many sources such as industries dealing with manufacturing and processing PFAS compounds, municipal wastewater contaminated with PFAS compounds, leachate from landfills containing PFAS-laden wastes, and PFAS-contaminated rainwater [18,37]. The majority of

PFAS compounds, including long-chain and short-chain compounds, enter the treatment facilities from external sources. However, a small proportion of long-chain PFAS compounds can be degraded to generate small-chain PFAS or new intermediate PFAS compounds; their fate and presence primarily depend on the type of treatment process [33,38]. For instance, Schultz et al. [38] determined the concentrations of various PFAS compounds in a wastewater treatment plant, analysing the mass flow of PFAS compounds after each treatment step. The results revealed substantial decreases and increases in some PFAS compounds while others were not affected by the treatment processes. The study reported that the conventional treatment was ineffective in removing 6:2 fluorotelomer sulfonate (6:2FtS) and perfluorooctanoate (PFOA), as the mass flows of these compounds were nearly similar after each step of the treatment [38]. Alternatively, a 2.5 times increase in mass flow for perfluorooctanesulfonate (PFOS), a 2 times increase for perfluorodecanesulfonate (PFDS), and a 4-fold increase in perfluorononanoate (PFNA) was observed after activated sludge treatment, ascribing their generation from the degradation of precursors molecules [38]. If PFAS are not removed in WWTPs with a target technology, there is a high tendency for PFAS to end up in recycled water as well as biosolids.

The removal of PFAS during wastewater treatment and their presence in biosolids primarily depends on their sorption behaviour. Since each PFAS compound exhibits unique physical and chemical properties, its adsorption behaviour onto solid particles is also different [39]. In addition, there are several other factors, such as the pH of biosolids, biosolids composition (total organic carbon, metals, minerals, and other organic and inorganic contaminants), cation and anion exchange capacity, and interaction forces that affect the adsorption of PFAS on biosolids, which ultimately impact their final concentrations in biosolids [39-41]. Fig. S1 represents primary interactions that influence the accumulation of PFAS on biosolids. The probability of PFAS translocation to sludge/biosolids rises with increasing perfluoroalkyl chain lengths, attributing to increasing sorption capacity validated by sorption isotherms, such as Freundlich and Langmuir [42]. Zhang et al. [41] showed that long-chain PFAS, PFOA and PFOS achieved Kf values of 1.13-2.28 and 1.52-3.58, respectively. On the other hand, short-chain PFAS, like PFBA, exhibited lower K_f values in the range of 0.84–1.14 and PFBS in 1.13-1.34, confirming stronger sorption for long-chain PFAS compared to short-chain PFAS [41]. The higher sorption capacity of long-chain PFAS can be attributed to the enhanced hydrophobic and oleophilic character arising from the additional number of carbon-fluorine atoms [39,40]. Low pH and abundance of divalent cations such as Mg²⁺ and Ca²⁺ are known to enhance PFAS adsorption on biosolids [43]. The change in pH greatly influences the organic



Fig. 2. A general structure of nonpolymeric, perfluorinated PFAS substances. A PFAS compound is generally comprised of two components. Firstly, a hydrophobic tail comprises centrally located C-C bonds, which are surrounded by C-F bonds. This hydrophobic tail may contain a variable number of carbon and fluorine atoms. The second is the hydrophilic head that has polar groups like carboxylate and sulfonate group, providing a PFAS compound in a special category, perfluorocarboxylates and perfluorosulfonates, respectively.

| PFAS type | Average F | FAS concent | tration in bios | olids (µg/kg) | | | | | | | | | | | |
|--|---------------------------|-----------------------------|-----------------|----------------------------|-------------------------------|--|-------------------------------|-------------------------------|-----------------------------|--|------------------------------|----------------------------|-----------------------------|-----------------------------|--|
| | Johnson | Pepper | Gallen | Navarro | Schultz | Moodie | Venkatesan | Loganathan | Kundu | Kim | Gallen | Letcher | Guerra | Campo | Armstrong et al. |
| | [18], | et al. | et al.[16] | et al. | et al. | et al.[45] | et al.[55] | et al. [46] | et al.[14] | et al. | et al.[57] | et al. | et al. | et al. | [09] |
| | USA | [2] | Australia | [26] | [38] | Australia | NSA | USA | Australia | [26] | Australia | [58] | [59] | [47] | USA |
| | | USA | | Spain | NSA | | | | | NSA | | Canada | Canada | Spain | |
| Perflourinated sulfonic acids | | | | | | | | | | | | | | | |
| PFBS | 3.40 | 1.90 | NA | 7.72 | NA | 2.30 | 3.40 | NA | 2.20 | 1.10 | 7.40 | 3.07 | NA | 0.78 | NA |
| PFPeS | NA | NA | NA | NA | NA | 0.20 | NA | NA | NA | NA | NA | NA | NA | NA | NA |
| PFHxS | 5.90 | 3.70 | 0.11 | 7.78 | NA | 1.80 | 5.90 | < 2.50 | 0.60 | <lod< td=""><td>NA</td><td>NA</td><td>NA</td><td>0.01</td><td>NA</td></lod<> | NA | NA | NA | 0.01 | NA |
| PFOS | 403.00 | 34.00 | 25.00 | 23.7 | 100.00 | 23.00 | 403.00 | 95.00 | 14.80 | 13.40 | 67.00 | 50.40 | 16.20 | 41.4 | 22.50 |
| PFDS | NA | NA | NA | NA | 91.00 | <lod< td=""><td>NA</td><td>NA</td><td>NA</td><td>3.20</td><td>NA</td><td>NA</td><td>NA</td><td>0.01</td><td>5.61</td></lod<> | NA | NA | NA | 3.20 | NA | NA | NA | 0.01 | 5.61 |
| PFOSA | NA | NA | NA | NA | NA | NA | 20.70 | 21.00 | NA | NA | NA | NA | NA | 0.67 | NA |
| Perfluorinated carboxylic | | | | | | | | | | | | | | | |
| acids | | | | | | | | | | | | | | | |
| PFBA | NA | NA | NA | NA | NA | 0.80 | 2.00 | NA | 2.00 | 0.60 | NA | NA | NA | 399.00 | NA |
| PFPeA | 3.50 | NA | NA | 5.47 | NA | 2.00 | 3.50 | NA | 2.30 | NA | NA | NA | NA | 193.00 | 8.27 |
| PFHxA | 6.20 | 4.20 | 0.50 | 18.4 | NA | 2.80 | 6.20 | NA | 3.70 | 2.30 | 2.60 | NA | NA | 1.33 | 7.71 |
| PFHpA | 3.40 | 1.40 | 0.26 | NA | NA | 0.90 | 3.40 | NA | 1.30 | <lod< td=""><td>NA</td><td>NA</td><td>NA</td><td>6.41</td><td>5.12</td></lod<> | NA | NA | NA | 6.41 | 5.12 |
| PFOA | 3.40 | 4.30 | 6.50 | 6.23 | < 3 | 8.30 | 34.00 | 219.00 | 8.60 | 1.90 | 11.00 | NA | 2.90 | 21.7 | 23.5 |
| PFNA | 9.20 | 1.80 | 1.10 | 3.34 | 06.6 | 0.90 | 9.20 | < 2.50 | NA | 3.90 | 1.20 | NA | 5.00 | 27.2 | 25.10 |
| PFDA | 26.10 | 12.00 | 17.00 | 5.67 | 5.90 | 14.00 | 26.1 | 34.00 | NA | 1.40 | 29.00 | NA | 1.35 | 160.00 | NA |
| PFUnDA | 11.70 | 2.30 | 1.20 | NA | 6.80 | 0.60 | 11.70 | 5.90 | NA | 2.10 | 1.60 | NA | 4.10 | 8.68 | NA |
| PFDoDA | 10.90 | 8.00 | 5.70 | NA | 3.80 | 5.90 | 10.90 | 7.20 | NA | 1.90 | 9.90 | NA | 7.50 | 0.10 | NA |
| Note: NA-not available; LOI PFHDA: Perfluorohentanoic | D-limit of d acid: PFH | letection; F xA: Perfluc | PFBA: Perflu | orobutyric a acid: PFHx | acid; PFBS: 1 S:Perfluoroh | Perfluorobut texanesulfon | anesulfonate; ate: PFNA: F | PFDA: Perflu Perfluoronona | orodecanoic noic acid: P | acid; PFDS FOA: Perflı | 5: Perfluoroo uorooctanoi | decanesulfo c acid: PF(| nate; PFOS. DS: Perfluor | A: Perfluoro ooctane sul | octane sulfonamide; fonate: PFPeA: Per- |

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Quantification of different PFAS detected in biosolids worldwide.

Table 1

matter surface charge of biosolids. At low pH, the overall surface charge is positive, and the quantity of cationic chemical species increases that can interact with anionic polar head groups of PFAS [42]. The results from different studies have shown that polyvalent cations compared to monovalent cations like Na⁺ exhibit stronger attraction with interfacial layer and thus can increase adsorption of PFAS on biosolids [39,43,44].

A number of studies (however, limited in many countries) demonstrated the presence of various types of PFAS in biosolids across the world, reporting a concentration between 0.11 and 403 μ g kg⁻¹ [5,16, 18,26,45]. Table 1 summarizes the worldwide distribution of selected PFAS in biosolids. It was observed from these studies (in Table 1) that the quantities of long-chain PFAS, such as PFOS, PFDS, PFOA, and PFDA were consistently higher in the majority of biosolids compared to other counterparts. For example, Venkatesan and Halden [46] found 403 µg kg⁻¹ of PFOS and 34 µg kg⁻¹ of PFOA in biosolids, while the concentrations of PFBS and PFBA were reported to be 3.4 and 2 μ g kg⁻¹, respectively. Similarly, Loganathan et al. [46] achieved 95 µg kg⁻¹ PFOS and 219 µg kg⁻¹ PFOA in biosolids that were several times higher than PFNA, PFDA, and PFOSA. Though PFOS (in 2009) and PFOA (in 2019), their salts and related compounds were added to the Stockholm Convention's list of persistent organic pollutants, and their production is restricted in European Union, but some countries still produce these PFAS [47]. PFOS and PFOA can also be generated from precursor compounds during wastewater treatment and accumulate in biosolids. Since primary applications of biosolids are agriculture and land rehabilitation, PFAS contaminated biosolids constitute a significant source of PFAS for soil contamination and are highly prone to be taken up by roots and other parts of plants [48,49]. There are several pieces of evidence of PFAS uptake by plants in biosolids amended soil, which has been discussed in detail by Ghisi et al. [20] and Mei et al. [50]. Once PFAS accumulate in plants, they can translocate to corresponding food chains and ultimately to humans. The toxic effects of PFAS exposure on human health are well known and have been linked to kidney and testicular cancers, endocrine dysfunction, liver malfunction, immunotoxicity, hypothyroidism, and many other diseases [51-53].

Despite being aware of the toxic effects of PFAS, very less attention has been paid to implement strict regulations and policies to limit PFAS contamination in biosolids. A few countries from Europe, such as Germany, Denmark, Netherlands, Sweden, the USA, and Australia have taken some critical steps to restrict PFAS concentration in biosolids. For instance, Germany has set a PFAS limit of 100 µg kg⁻¹ in biosolids as well as in soil. Denmark has set a PFAS limit of 400 μ g kg⁻¹ in soil, while Sweden set the PFAS limit of 3 µg kg⁻¹ for sensitive land use (gardens and residentials) and 20 μ g kg⁻¹ for less sensitive land use (offices and industrial). On the other hand, the Netherlands adopted a unique approach to PFAS regulation, limiting the use of only PFOS and PFOA in soil by 0.9 and 0.8 μ g kg⁻¹, respectively. The USA has set the PFAS limit of 70 ng L⁻¹ for drinking water but has been carrying out risk assessment analyzing the effects of PFAS in biosolids-amended soil, so might bring new regulations in the near future. In 2017, Canada restricted the use of agricultural soil containing PFAS above 10 µg kg⁻¹. In Australia, though biosolids do not have an upper limit, the environment authority has recommended considering ecological direct (for PFOS-1000 µg kg⁻¹, for PFOA-10000 µg kg⁻¹) and indirect exposure values (for PFOS-10 ng g⁻¹) when performing the risk assessment for the land applications of biosolids [54]. In addition, Queensland state of Australia took further steps to limit PFAS and issued PFAS trigger values in soils in the range of $1-10 \ \mu g \ kg^{-1}$, which need to be evaluated after biosolids application.

The guidelines and policies presented above can be considered effective in evaluating PFAS contamination and regulating the usage of contaminated biosolids. However, additional imperative actions are required to prevent PFAS accumulation in biosolids and cost-effective and sustainable technologies to eradicate PFAS from biosolids. The most inexpensive and impactful approach could be the reduction or prohibition of primary PFAS sources, which can be achieved either by restricting the production of PFAS and seeking feasible alternative

fluoropentanoic acid; PFPeS: Perfluoropentane sulfonate; PFDoDA: Perfluorododecanoate; PFUnDA: Perfluoroundecanoate

chemicals or setting a PFAS limit on industrial discharge points to prevent/reduce their occurrence in WWTPs. Another efficient solution to mitigate PFAS involves the application of advanced thermochemical technologies such as incineration, gasification, hydrothermal liquefaction, pyrolysis, and microbial degradation. The potential of these techniques to destroy PFAS in biosolids has been discussed in the next section.

4. Technologies for PFAS removal from biosolids

Several technologies, including thermochemical processes, electrochemical, water oxidation, adsorption, membrane filtration, photolytic and photocatalytic degradation, and biological treatment, have been used to mitigate PFAS compounds from various waste streams. However, mainly thermochemical techniques such as incineration, gasification, combustion, hydrothermal liquefaction (HTL), pyrolysis, and biodegradation have been reported to remove PFAS from biosolids

Table 2

Operating characteristics, advantages and disadvantages of technologies employed for PFAS-biosolids treatment.

| Technique | Operating parameters | Advantages | Disadvantages |
|------------------------------|---|---|---|
| Biodegradation | -time: 1–150 days -room temperature -additives like Fe (III) -anaerobic or aerobic bacteria | -cost-effective -degrades 50–60% PFAS -does not require pre-drying of biosolids -low environmental risks | -takes a long time to degrade PFAS -lower PFAS degradation efficiency -low availability of microbes |
| Hydrothermal liquefaction | -temperature: 150–350 °C -time: 30 min- 6 h -pressure: 5–20 MPa -inert gas | -does not require pre-drying of biosolids -low temperature -suitable to degrade PFCA | -energy-intensive -expensive post- treatment -requirement of special reactors -does not degrade PFSA |
| Smouldering Combustion | -temperature: 200–1200 °C -oxygen (5–20%) -air flux: 0.1–4 cm/min -porous medium required | -low cost -requires less energy input -effective for PFAS destruction (>99%) | -requires pre-drying of biosolids -releases toxic gases |
| Incineration | -temperature: 800–1000 °C -time: 30 min -oxygen or air -atmospheric pressure | -biosolids volume reduction -potential energy recovery -highly efficient for PFAS degradation (>99%) -generation of stable ash | -high capital investment -high operating costs -toxic gases and hazardous emissions -requires pre-drying of biosolids |
| Gasification | -temperature: $> 600 ^{\circ}C$ -time: $> 30 ^{\circ}min$ -gasifying agent, CO_2 or steam -atmospheric pressure | -suitable to degrade all types of PFAS -> 99% degradation efficiency -biosolids volume reduction | -formation of volatile PFAS -energy-intensive -high capital investment -requires mechanical dewatering and pre- drying of biosolids |
| Pyrolysis | -temperature: 200–700 °C -time: 30 min- 6 h -inert gas -atmospheric pressure | -suitable to degrade all types of PFAS -highly efficient for PFAS degradation (>99%) -low environmental risks, such as GHG emissions -biosolids volume reduction | -energy-intensive -high capital investment -requires mechanical dewatering and pre- drying of biosolids |

[61–63]. Table 2 shows the operating conditions, advantages, and disadvantages of these technologies for PFAS-biosolids treatment, whereas Table 3 presents the performance of different techniques for PFAS destruction in various matric conditions.

4.1. Biological degradation of PFAS-biosolids

Biodegradation is one of the ecofriendly and cost-effective techniques to degrade PFAS present in biosolids. Biodegradation of PFAS primarily depends on the structural complexity of PFAS, the composition of microbes and operating conditions. Biotransformation of PFAS either in aerobic or anaerobic conditions using bacterial species like Pseudomonas and Acidimicrobium and fungal species such as Phanerochaete chrysosporium have been reported in previous studies [73,74]. Microbes generally use PFAS compounds as the carbon source and can promote their defluorination when applied for iron reduction using NH₄⁺ or H₂ as electron donors. A study demonstrated PFAS degradation (PFOA and PFOS) using pure Acidimicrobium sp. strain A6 and mixed culture (Ralstonia, Bacillus, Acidimicrobium, Aciditerrimonas, and Desulfosporosinus), Fe (III) as electron acceptor and NH₄⁺ as electron donor over 100 days of incubation [62]. The results showed 50% PFOA removal using mixed culture and 33% with pure culture. It was further noticed that the pure culture and enrichment culture showed different mechanisms of PFOA degradation since, in the former scenario, only one intermediate product that is perfluorohexanoic acid (PFHxA), was detected, while in the latter case, four intermediate compounds, perfluorobutanoic acid (PFBA), perfluoropentanoic acid (PFPeA), perfluorohexanoic acid (PFHxA), and perfluoroheptanoic acid (PFHpA) were observed. No PFOA degradation was observed in the absence of NH₄⁺. Similarly, the mixed culture showed higher degradation of PFOS compared to the pure culture, which was 47% and 23%, respectively [62]. In a separate study, Huang et al. [73] carried out anaerobic degradation of PFOA-biosolids using Acidimicrobium sp. strain A6 enrichment culture and Fe (III)-NH₄⁺ enrichment medium with an incubation period of 150 days. The results showed a significant reduction in PFOA between 60 and 150 days, while the concentration of short-chain PFCAs like PFBA, PFPeA, PFHxA and PFHpA, as well as total fluorine content, consistently increased, indicating the successful microbial degradation of PFOA in biosolids [73]. Another study demonstrated the biotransformation of PFOAAmS and PFOSAmS with incubation of soil microcosms for 142 days and observed slow but noticeable degradation of PFOAAmS into PFOA (30%) and the conversion of PFOSAmS into PFOS (3%), FOSA (<0.005%), and perfluoroctanesulfonamidoamido amine (PFOSAm)- 10% [75].

For PFAS biodegradation, a microbe requires to transport PFAS into the cell; needs to produce an active enzyme to catalyze C-F bond cleavage; requires sensing the toxic fluoride ion; a fluoride-proton antiporter to eliminate fluoride ion from the cell. While these components are vital for PFAS biodegradation, a physiological barrier makes PFAS biodegradation an unfavorable process. For instance, polychlorinated compounds can act as preferrable electron acceptors because of the positive redox potential for dechlorination that usually ranges between + 250 and + 600 mV, making it favorable to accept electrons via an electron transport chain [76]. On the other hand, polyfluorinated compounds exhibit negative redox potential for their reduction, making them unable to serve as final electron acceptors [77]. However, PFAS can be microbially degraded in cometabolism with the addition of potential electron donors and acceptors. In such conditions, microbes are known to degrade PFAS, mainly via defluorination process that releases fluoride anion. High-level of defluorination may result in high intracellular fluoride concentrations. Fluoride shows intrinsic cellular toxicity, it can bind to critical enzymes (such as ATPases and pyrophosphatase) even at a low concentration of 0.1 mM and inhibits cellular metabolism [78]. Therefore, it is important for a microbe to develop a high tolerance to fluoride. Generally, bacteria like Pseudomonas sp. are known to contain two types of proteins, fluoride/protein

Table 3

Performance of different techniques for PFAS destruction in various waste.

| Technique | Operating parameters | Matrix conditions | Target PFAS type | Concentration | Major products | Conversion Efficiency | Reference |
|------------------------------|---|-------------------|---------------------|---------------|--|--------------------------|-----------|
| Biodegradation | Acidimicrobium sp. strain A6, 100 | Anaerobic | PFOA | 100 mg/kg | HFBA; PFPeA; PFHxA; PFHpA | 50% | [62] |
| Biodegradation | Acidimicrobium sp. strain A6, 100 | Anaerobic | PFOS | 100 mg/kg | HFBA; PFBS | 47% | [62] |
| Biodegradation | Pseudomonas plecoglossicida 2.4-D, | Aerobic soil | PFOS | 1000 mg/kg | NA | 75% | [64] |
| Biodegradation | Pseudomonas plecoglossicida 2.4-D, | Aerobic | PFOS | 1000 mg/kg | PFHpA | 100% | [64] |
| Biodegradation | Mixed culture, 180 days | Aerobic soil | 6:2 FTOH | 2.9 mg/kg | PFPeA; 5:3 Acid; PFHxA; 5:2 setoh: 6:2 etoh: peba | 67% | [65] |
| Biodegradation | Mixed culture, 180 days | Aerobic sludge | 6:2 FTOH | 2.8 mg/kg | 6:2 FTUA; 5:2 sFTOH; 6:2 FTCA: 5:3 Acid: PFHxA | 60% | [65] |
| Hydrothermal liquefaction | Batch reactor, T-350 °C, P- 16.5 MPa, t-1.5 h, 2.5 M NaOH | NR | PFOS | 50 mg/L | NA | 100% | [66] |
| Hydrothermal liquefaction | Batch reactor, T-350 °C, P- 16.5 MPa, t-1.5 h, 1 M NaOH | NR | PFOS | 50 mg/L | NA | 80% | [66] |
| Hydrothermal | Batch reactor, T-350 °C, P- 21.9 MPa, t-6 h, 9.61 mM Fe | NR | PFHpS | 1.46 μΜ | NA | 100% | [67] |
| Hydrothermal | Batch reactor, T-500 °C, P-35 MPa, | NR | PFOS | 28.6 mg/L | NA | 70% | [68] |
| Hydrothermal | Batch reactor, T-500 °C, P-35 MPa, t-1 h H ₂ O ₂ NaF | NR | PFHpS | 0.31 mg/L | NA | 55% | [68] |
| Hydrothermal | Batch reactor, T-300 °C, P-35 MPa, | Sewage | PFOA | 20 ng | NA | 100% | [69] |
| Hydrothermal | Batch reactor, T-300 °C, P-35 MPa, t-1 h | Sewage | PFHpA | 20 ng | NA | 100% | [69] |
| Hydrothermal | Batch reactor, T-300 °C, P-35 MPa, | Sewage | PFHxA | 20 ng | NA | 100% | [69] |
| Pyrolysis | Pilot-scale reactor (63.6 kg/h), T- 650 °C | Biosolids | PFOA | 86.70 ng/g | NA | 100% | [17] |
| Pyrolysis | Pilot-scale reactor (63.6 kg/h), T- | Biosolids | PFOS | 25.10 ng/g | NA | 100% | [17,70] |
| Pyrolysis | Batch reactor, T-700 °C, 10 min, Granular activated carbon | Sewage | PFOA | 49.4 mg/g | NA | > 99% | [70] |
| Pyrolysis | Batch reactor, T-700 °C, 10 min, Granular activated carbon | Sewage | PFOS | 10 mg/g | NA | > 99% | [70] |
| Pyrolysis | Batch reactor, T-700 °C, 10 min, Granular activated carbon | Sewage | PFHxA | 47.3 mg/g | NA | > 99% | [70] |
| Pyrolysis | Semi-pilot plant, T-600 °C, Granular | Biosolids | PFBS | 2.20 ng/g | NA | 74% | [14] |
| Pyrolysis | Semi-pilot plant, T-600 °C, Granular | Biosolids | PFOS | 14.78 ng/g | NA | 98% | [14] |
| Pyrolysis | Semi-pilot plant, T-600 °C, Granular | Biosolids | PFHxA | 3.65 ng/g | NA | 84% | [14] |
| Pyrolysis | Semi-pilot plant, T-600 °C, Granular | Biosolids | PFOA | 8.63 ng/g | NA | 96% | [14] |
| Smouldering Combustion | T- $>$ 900 °C, air flux-5 cm/s, velocity-0 24–0 71 cm/min | Soil | PFBA | 0.003 mg/kg | NA | > 99% | [71] |
| Smouldering | T- $>$ 900 °C, air flux-5 cm/s, velocity-0.24–0.71 cm/min | Soil | PFHxS | 0.009 mg/kg | NA | > 99% | [71] |
| Smouldering | T- > 900 °C, air flux-5 cm/s, velocity-0.24-0.71 cm/min | Soil | PFOA | 0.0003 mg/ | NA | > 99% | [71] |
| Incineration | Tube furnace, air, T-500 °C, Granular activated carbon | NR | PFBA | NR | NA | > 99% | [72] |
| Incineration | Tube furnace, air, T-500 °C, Granular activated carbon | NR | PFOA | NR | NA | > 99% | [72] |
| Incineration | Tube furnace, air, T-500 °C, Granular activated carbon | NR | PFOS | NR | NA | > 99% | [72] |

Note: NA-not analyzed; NR-not reported

antiporter and CrcB-type that help to transport fluoride from the inside to the outside of the cell [79].

Microbial degradation of PFAS may involve a series of reductive defluorination, decarboxylation, hydroxylation, and hydrogenation reactions. PFAS compounds also contain C-S (sulfonate) and C-C (carboxylate) bonds which are considered weaker than the C-F bond and may undergo one-electron reduction or oxidation to generate a carbon-centered radical, followed by hydroxylation. Fig. 3a presents PFOS and PFOA degradation by *Ensifer adhaerens*. As shown in this figure, PFOS firstly undergoes C-S (sulfonate) bond cleavage and releases SO₃ to produce perfluorooctane, followed by hydroxylation,

decarboxylation and defluorination reactions to form perfluoroheptanoic acid. On the other hand, PFOA firstly undergoes decarboxylation reaction to form perfluoroheptane which further undergoes hydroxylation and defluorination reactions to generate perfluoroheptanoic acid. Following this pathway, PFAS is degraded onecarbon short compared to the initial PFAS and the carbon is lost in the form of CO₂. Fig. 3b shows a proposed mechanism of PFOA defluorination. In this pathway, the first microbial enzymatic cleavage occurs at the C_1 - C_2 bond to form a carbon-centered radical, followed by radical quenching to produce a C_7 pefluorinated alcohol. Then the alcoholic compound undergoes non-enzymatic and rapid defluorination and



Fig. 3. (a) Biodegradation mechanisms of PFOS and PFOA by *Ensifer adhaerens* strain M1. (b) A proposed mechanism for the complete defluorination of perfluorooctanoate. (c) Proposed biotransformation pathways of perfluoro (4-methylpent-2-enoic acid) (PFMeUPA) and (d) 4,5,5,5-tetrafluoro-4-(trifluoromethyl)– 2pentenoic acid (FTMeUPA).

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hydroxylation reactions to generate C7 carboxylic acid. One cycle of these reactions reduces the PFAS-chain by one carbon; however, C₇ carboxylic acid can undergo the same cycle to form C₆ carboxylic acid and subsequently, creating more shorter chains. Fig. 3c and d show biotransformation pathways of perfluoro (4-methylpent-2-enoic acid) (PFMeUPA) and 4,5,5,5-tetrafluoro-4-(trifluoromethyl)- 2pentenoic acid (FTMeUPA) using microbes such as Dehalococcoides mccartyi and Dehalobacter restrictus [35]. Major degradation pathways were found to be defluorination and hydrogenation. In PFMeUPA biodegradation, the first step involves defluorination that is occurred by C –F bond cleavage at sp² carbons of the double bond despite having higher bond dissociation energy (BDE) compared to tertiary $sp^3 C - F$ bond. This could be mainly because the C = C bond may favor the binding of metal center-containing defluorinating enzymes to initiate reductive defluorination. On the contrary, FTMeUPA lacks sp² C -F bonds and contains sp³ C –F bonds, so reductive defluorination is most likely to occur at tertiary $sp^3 C - F$ bonds (has low BDE) instead of primary sp^3 C-F bond [35]. The hydrogenation pathway occurs simultaneously with reductive defluorination in both PFMeUPA and FTMeUPA biodegradation, reaction 2 and reaction 4 in Fig. 3c and d, respectively. The hydrogenation products were found recalcitrant to reductive defluorination since their concentrations were steady [35].

Another biological approach for the decomposition of PFAS is enzyme-catalyzed oxidative humification reactions (ECOHRs). Enzymes such as peroxidases and laccases can be used to catalyze oxidative reactions that break down the PFAS into smaller, less toxic compounds [81,82]. The mechanism of ECOHRs involves the generation of reactive oxygen species by the enzymes, which can then react with the PFAS to break down their carbon-fluorine bonds [81,82]. A study demonstrated PFOA treatment with laccase and hydroxybenzotriazole for 157 days and showed that 50% of PFOA was decomposed [82]. The authors did not detect any shorter carbon-chain PFCA as degradation products, but partially fluorinated shorter-chain alcohols and aldehydes were identified [82]. These partially fluorinated compounds are likely the result of PFOA degradation through a combination of free radical decarboxylation, rearrangement, and coupling processes [82]. Fluoride was found in the reaction solution, indicating a 28.2% defluorination during the treatment [82]. The study suggests that PFOA can potentially transform during humification, and ECOHRs may be a viable option for PFOA remediation.

Though the biodegradation of PFAS is an eco-friendly and cheaper option, it cannot degrade all kinds of PFAS compounds from biosolids and takes a longer period to degrade PFAS. Moreover, biodegradation pathways are assumed based on the identification of intermediate compounds, while some of them remain unidentified. Therefore, more accurate approaches are necessary to analyze all intermediate compounds generated during the process and identify the precise bond cleavage to understand the stepwise degradation mechanism. Additionally, limited microbes have been tested to degrade PFAS in different streams, especially biosolids. Since each microbe exhibits unique enzymatic machinery to break chemical bonds, more studies are required to explore different microbes, either in pure culture or in combination with other microbes, to understand their degradation pathways. To determine the effects of biosolids composition, for example, the presence of potentially toxic elements or metal ions on microbial activity would be interesting since it can further impact PFAS destruction.

4.2. Hydrothermal liquefaction treatment of PFAS-biosolids

Hydrothermal liquefaction (HTL) is a well-known technology utilised to recover energy from biomass feedstocks at a temperature range of 250-350 °C and pressure of 10-25 MPa [83]. HTL generally utilizes a solvent like water and methanol that influences the decomposition of the feedstock significantly, and thus the final products depend primarily on the operating parameters and the solvent used. A number of studies have been carried out to demonstrate the potential of the HTL process for bio-oil production using different types of biomass feedstocks, including sewage sludge and biosolids [84-86]. HTL is conducted in the presence of a solvent and is thus considered more suitable and economical for wet feedstocks like biosolids. Biosolids contain a high amount of moisture (80-85%) and can be directly used in HTL without drying [87]. The primary product of HTL of biosolids or sewage sludge is biocrude oil, and the PFAS present in the feedstock are depolymerised during the process, and most of them end up in the biocrude oil. Operating parameters like temperature and residence time play an important role in the destruction of a specific class of PFAS. For instance, Yu et al. [88] demonstrated the effect of temperature and residence time on PFAS degradation in the HTL process. The results showed that low temperatures of 260 and 300 °C and residence time of 30 min were capable to achieve > 99% degradation of PFOA and 8:2 FTUCA, but no degradation was detected for PFOS. However, increasing the temperature to 350 °C and residence time to 90 min could achieve a maximum degradation of 34% for PFOS and 67% for 8:2 FTS [88]. The main pathway for the degradation of PFOA was attributed to defluorination, while the presence of metal ions like Ca^{2+} might promote the cleavage of the C-F bond and form stable inorganic fluoride minerals such as $CaF_{2(s)}$ [88]. Another study reported similar results for PFAS destruction in HTL, which showed that PFCAs were completely degraded at 300 °C; however, an increase in the concentration of PFSA compounds was noticed [69].

During the HTL process, PFAS are expected to degrade through OH catalyzed series of nucleophilic substitution and decarboxylation reactions. The highly electronegative fluorine atom creates a strong dipole

when bonded to carbon creating an affinity for the solvated electron to attack the relative positive charge (δ +) of the carbon atom presenting a viable mechanism for the reductive attack which can potentially overcome the bond dissociation energy of the C-F bond and the associated shielding to other forms of a chemical attack. The small size of a solvated electron may be the reason for its propensity to access the C -F bond as a nucleophile without being repelled by the helix of fluorine atoms shielding the C - F and C - C bonds in the perfluoroalkyl chain [66]. The proposed mechanism of PFOS degradation is shown in Fig. 4. In PFOS hydrothermal degradation, the first step involves OH⁻ substitution with a sulfonate headgroup, forming an unstable perfluorinated alcohol compound. In the second step, the unstable alcohol intermediate undergoes rapid HF elimination to generate a ketonic intermediate compound. Further, the ketonic compound undergoes a hydration reaction and eliminates another F to form PFOA. In subsequent reactions, PFOA undergoes decarboxylation reactions, releasing 2 F in each reaction and forming short-chain perfluorocarboxylates like PFPeA. In PFOS degradation, the first reaction involving the cleavage of the sulfonate group is the rate-limiting step. The reactivity of PFOS is lower compared to the reactions initiated with PFOA since decarboxylation reactions were found to occur more frequently compared to the cleavage of the sulfonate group [66].

The results discussed above suggest that the HTL process is highly advantageous to destruct PFCA compounds in biosolids but has shown less efficacy in degrading PFSA compounds. Therefore, advancement in HTL is inevitable to accomplish the complete destruction of PFAS in biosolids that generally contain a mixture of PFCA and PFSA species. This can be achieved by employing alkaline HTL, such as NaOH [66,86]. Wu et al. [66] conducted HTL of PFOS in the presence of 1 M NaOH, a temperature range of 200 - 350 °C, and pressure between 2 and 16.5 MPa. The results revealed up to 80% of PFOS defluorination after 90 min at 350 °C. The addition of strong basic solvents like NaOH and dimethyl sulfoxide (DMSO) promotes the decomposition of PFAS in near-critical and supercritical water conditions. Interestingly, NaOH catalyzes the decarboxylation of long-chain PFAS like PFOS and PFOA as well as short-chain PFAS such as PFPeA. A recent study published in the



Fig. 4. Proposed mechanism of PFOS degradation in the hydrothermal liquefaction process. Adapted with permission [66]. Copyright (2019) American Chemical Society.

journal Science revealed that decarboxylation is the key first step of the defluorination of PFCAs like PFOA, and the fluorine atoms originating from the PFOA destruction are recovered as fluoride ions [89]. The fluoride ions content increases proportionally to the decrease in PFOA concentration, indicating that most of the perfluoroalkyl fluorines are defluorinated and mineralized rather than being transformed to smaller-chain PFAS or being lost as volatile fluorocarbons. The destruction of short-chain PFCAs (C=2–3) like trifluoroacetate (C=2) is slower compared to long-chain PFCAs like PFOA. It is possibly because of the instability of the CF₃ anion that hinders decarboxylation reaction which either slows down the degradation or directs it towards a different degradation mechanism. Where the degradation of long-chain PFCAs is shortened by one carbon each and generates volatile CF₃CF₂H, the degradation of trifluoroacetate takes place by a different, non-single-carbon shortening mechanism [89].

In PFOA degradation, decarboxylation is the rate-limiting step and a series of defluorination reactions are low-barrier reactions. Fig. 5 shows the proposed PFCA degradation mechanism under basic conditions like in the presence of DMSO or NaOH. Density functional theory (DFT) results showed that the initial decarboxylation of PFOA requires an activation energy of 28 kcal/mol to produce an intermediate anion (INT1 in the figure) compound which releases a fluoride ion to form perfluoroalkene (INT2) like perfluoro-1-heptene [89]. This perfluoroalkene undergoes hydroxylation under no enthalpic barriers ($\Delta G =$ -44.3 kcal/mol) to produce an enol intermediate product (INT3), taking place especially on the terminal position because hydroxylation on the internal side of the alkene has an enthalpy barrier of 8.9 kcal/mol [89]. The enol product undergoes fluoride elimination to form α , β -unsaturated acyl fluoride (INT4) through retro 1,4-conjugate addition, followed by an enthalpically barrierless fluoride elimination to form 1, 3-diketone compound (INT5). Hydroxide again adds INT5 on the ketone carbonyl side to generate an intermediate product that further undergoes fragmentation to form an equivalent of PFCA three carbons shorter than the initial PFCA. For example, if eight-carbon PFOA undergoes this degradation cycle, it will degrade to PFPeA by losing one carbon as CO_2 and two carbons as fluoroacetic acid.

HTL might be the most suitable process for sustainable biosolids management since does not require the pre-drying of biosolids. However, HTL might not be the best process to mitigate PFAS completely from biosolids. Alkaline HTL has shown promising results for PFOS removal, but primary studies have been conducted using aqueous mediums and soil, thus demanding future studies on PFAS mitigation from biosolids. In addition, the short-chain PFAS compounds generated during the HTL process finally end up in the biocrude oil. Therefore, extraction of PFAS from biocrude oil and their safe disposal is another substantial challenge and might need additional technology, which can make biosolids management more expensive. Moreover, PFAS destruction pathways in HTL are not very clear; therefore, a thorough corroboration should be conducted to understand the destruction mechanism, which can open doors to develop innovative strategies to enhance PFAS destruction and make the HTL process highly efficient.

4.3. Thermal degradation of PFAS-biosolids

Smouldering combustion (SC) is a developing process for biosolids management. SC is a slow, flameless and self-sustained thermal technique operated by the heat generated from the fuel's oxidation [90]. SC generally requires a porous material that allows a high surface area for reaction and permeability for oxygen/air. The main products of biosolids SC are gases (primarily CO and CO₂) and solid residue (char), while the parameters such as sand/biosolids ratio, biosolids moisture content, and forced air flux play a critical role in the process [90]. This process has not been extensively explored for biosolids management, and very few studies have been published. For example, Rashwan et al.



Fig. 5. Proposed PFCA degradation mechanism under a basic condition like in the presence of DMSO or NaOH. The cycle showing a three-carbon shortening of the original PFCA of n carbons, with one carbon lost as CO_2 (converted to CO_3^{2-}) and two carbons lost to fluoroacetic acid, which readily degrades under these reaction conditions.

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[91] carried out SC of biosolids (with a moisture content of 71–84%) mixed with sand in a fixed bed stainless steel column at a preheating temperature of 200 °C (preheating phase was varied from 1 to 4 h) and an air flux rate of 1.6–8.1 cm/s. The oxygen introduction started the smouldering process and increased the temperature up to 650 °C, and further combustion was sustained by the energy released by biosolids. The results showed that sand/biosolids mass ratios from 1.7 to 11 g/g that provided the lowest energy content up to 0.28 kJ/g of the mixtures were capable to achieve a self-sustainable SC process. In addition, increasing the air flux rate and energy content of the mixtures improved smouldering robustness [91]. However, emissions and the char left from the process were not quantified and characterized.

SC of biosolids containing PFAS has not been reported so far; however, destruction of PFAS-contaminated soil and granular activated carbon (GAC) has been reported during the SC process. For instance, Duchesne et al. [71] successfully demonstrated PFAS destruction in soil and GAC during the SC. The authors prepared the samples using 175 mg PFAS/kg GAC-sand and 4 mg PFAS/kg soil and conducted SC in a stainless-steel column (height of 21-28 cm and diameter of 16 cm) at a preheating temperature of 260 °C and an air flux rate of 5 cm/s [71]. The results showed > 99% of PFAS destruction in both samples after the SC, whereas a small quantity of PFAS was also observed in emissions. PFAS destruction starts in the preheating phase since short-chain PFAS compounds start generating before reaching the peak temperature (e.g., 900 °C), suggesting there is sufficient energy to break down the sulfonate headgroup and volatilize a small fraction of PFAS [71]. A similar study was carried out by Major [92] to examine the PFAS-GAC and PFAS-soil destruction during SC in a stainless-steel column (height of 60 cm and diameter of 16 cm) at a preheating temperature of 260 °C and an air flux rate of 5 cm/s and achieved excellent results for PFAS removal. Three PFAS compounds, namely PFOA, PFOS and PFHxS, with initial concentrations of 590, 140 and 240 mg/kg, respectively, were present in the sample mixtures, while after the SC process, no PFAS was detected in the solid residue but noticeable quantities of PFAS were observed in the emissions. PFAS compounds in smoldering combustion can be degraded via several pathways including H/F exchange and dissociation of the functional groups, PFOS desulfonation and defluorination. During smoldering combustion, PFOS can transform into PFOA and shorter-chain perfluorinated carboxylic acids can break down the C4-C9 compounds to C2 and C3 chain lengths. The analysis confirmed the occurrence of H/F exchanges on PFBA, PFPA and PFpeA. The detection of 6:2 fluorotelomer sulfonate also indicated that PFOS underwent four consecutive H/F exchanges [71].

However, the technology is still in its infancy, and more research is required to determine the optimum parameters to obtain the maximum PFAS removal at the minimum cost and environmental risks. The technology could prove expensive if it requires a long period of ignition/ preheating phase, which consumes more energy. Therefore, efforts should be made to reduce the ignition time. Alternative porous materials that provide a suitable energy balance can make the SC process selfsustainable and reduce the total cost of biosolids management. As mentioned earlier, PFAS destruction could be started in the preheating phase, and a comprehensive study should be conducted to understand the fate of different types of PFAS under varying preheating temperatures. In addition, more attention should be paid to examine the environmental risks associated with the emissions and quantify the total mass loss in the process. The technology has shown promising results at the laboratory scale; hence, it would be interesting to determine its feasibility at the pilot scale.

Gasification is also a commercialized technology used for biosolids management. The technology has been successfully used in Germany, Japan, the USA and Australia to convert biosolids into syngas and biochar and simultaneously mitigate emerging organic contaminants [17]. Similar to pyrolysis and incineration, gasification is an energy-intensive technology that requires high temperatures of around 600–900 °C, pre-drying of biosolids and a limited supply of oxygen. Gasification of

biosolids has been used to generate biochar at a large scale, but the fate of PFAS has not been explored thoroughly during the process. A study showed that 200 °C was an adequate temperature to initiate the gasification of PFOA, while a range of 400-600 °C is required to gasify PFOS compounds, owing to the stability of sulfonic compounds over carboxylic acids [24]. Gasification of PFAS-biosolids has been demonstrated at a pilot-scale in the Queensland state of Australia. Logan City Council has been operating a gasifier at 600 °C in a low oxygen environment to convert biosolids (-PFAS) into biogas and biochar [7]. The gasification plant also utilizes the energy recovered from syngas for drying and heating processes. It can recover and reuse almost 70% of the energy in biosolids, while the rest of the energy required is provided by an onsite solar array, making the facility energy neutral. Thermal treatment at high temperatures in the gasification of PFAS-biosolids followed by combustion of the hydrogen-rich syngas stream in a thermal oxidizer could potentially destroy PFAS by mineralizing them into shorter PFAS molecules or less recalcitrant constituents. The reports suggest that gasification of PFAS-biosolids destructs nearly all PFAS compounds since the produced biochar showed PFAS quantities below the detection limit [7]. However, it is a challenging task to understand the PFAS degradation mechanism and evaluate potential products of incomplete destruction due to the complex composition of PFAS and biosolids. Hence, experimental and computational studies using sole PFAS molecules can be conducted to estimate destruction mechanisms and pathways under varying parameters. Because gasification also involves thermal treatment and oxygen, PFAS are supposed to follow similar degradation pathways of pyrolysis and incineration which are discussed in the following sections.

Incineration is a renowned thermochemical waste-to-energy technology that involves the combustion of feedstocks into heat, gas and ash [93]. It is one of the prominent approaches employed for waste management, including biosolids. Incineration is an energy-intensive technology and generally requires a high temperature (800-1000 °C) to destruct PFAS-biosolids [23]. For instance, the Tahuna wastewater treatment plant in Dunedin city council of New Zealand operates biosolids incineration at 830 °C [94], and over 200 plants are used in the incineration of sewage sludge in the USA [23]. However, employing PFAS-contaminated sludge or biosolids in incineration has rarely been studied. Since biosolids contain high moisture content of up to 85%, it requires pre-drying prior to incineration. The composition of resultant products depends mainly on the incineration conditions like temperature, oxygen content and moisture. However, the presence of PFAS in biosolids may result in extra hazardous emissions of volatile or mobile products [95]. Incineration of polytetrafluoroethylene (PTFE) between the temperature range of 750 and 1050 °C has been shown to produce major products like CF4, C2F6, CHF3, tetrafluoroethene, hexafluoropropene [93]. In addition, it has been argued that greenhouse gases produced during the incineration of PTFE contain C-F bonds, which absorb electromagnetic radiations in the range 1000–1400 $\rm cm^{\text{-}1}$, indicating its significant potential for global warming [93]. Yamada et al. [96] investigated the incineration of a polyester/cellulose fabric substrate treated with a fluorotelomer-based acrylic polymer at 1000 °C and 2 s residence time. The study aimed to examine the release of PFOA from the incineration of the fluorotelomer polymer. The results revealed that the fluorotelomer polymer was completely degraded at the studied incineration conditions, and no PFOA was detected [96]. A similar study was performed by Taylor et al. [97] to determine the fate of fluorotelomer-based polymers in incineration at 1000 °C, 2 s residence time, a varying amount of hydrogen fluoride (3.2-6.6 mg dscm⁻¹) and 7% of oxygen. At all operating parameters studied, fluorotelomer-based polymers were completely destroyed, and no PFOA was detected [97].

PFAS-biosolids mineralisation pathways in incineration are less explored so far. Garcia et al. [98] carried out thermal degradation of PTFE at 850 °C in the presence and absence of oxygen and the results revealed the occurrence of C_2F_4 and C_3F_6 in the gases, while numerous fluorinated semi-volatiles such as benzovl fluoride were noticed in oxygen-free thermal degradation and benzenepentafluoro was observed in the presence of oxygen [98]. Fig. S2 shows the possible mechanism of PTFE destruction. The thermal degradation of PTFE begins slowly at around 250 °C, consisting of random chain cleavage, followed by depolymerisation. The formation of fluorinated and perfluorocarbon compounds can be attributed to the cleavage of C-C bonds in PTFE. C₃F₆ was found to be the major product between 750 °C and 1050 °C temperatures of PTFE incineration, mainly because the monomer C2F4 could react to generate C₃F₆ [98]. It was further noticed that oxygen-free conditions favored the formation of C₃F₆, whereas, in the presence of oxygen, C₃F₆ decomposed to C₂F₆. This was evident from the results that indicated a decrease in the concentration of C3F6 in oxygen-dominant conditions, meanwhile, the quantities of C₂F₆ and CH₄ were found to be increased and no C2F4 was detected, primarily attributing to the reaction of C_2F_4 and C_3F_6 with oxygen. C_2F_4 and C_3F_6 after reacting with oxygen can also form CF₄ and CO₂ [98]. In addition, the thermal degradation of PTFE also releases perfluorocarbon compounds and fluorinated semi-volatiles, toluene, 2-hexanol, 3-penten-2-one, and 3penten-2-ol. Thermal destruction can completely transform PTFE into F (as HF), CO₂ and H₂O [99].

Since thermal destruction of PFAS can result in a number of smaller to larger end products, it is essential to measure the treatment efficacy and understand the degree of PFAS mineralization. To enhance the efficacy, surrogates like HF or CF₄, and C₂F₄ can be used to indicate the mineralization extent of PFAS since these are dominant end products of PFAS thermal degradation. However, there are some challenges associated with these surrogates. The application of HF can be complicated because it is reactive to the silica-based lining of the reactor and could form SiF₄. On the other hand, if CF₄ is used individually as a surrogate, it might be unsuitable to understand complete PFAS defluorination for inert thermal degradation because no CF4 was detected, and the primary short-chain product was C₂F₄. The challenge with C₂F₄ as a surrogate arises in the presence of oxygen because it can react with oxygen and produce CF. Therefore, to avoid the underestimation of PFAS mineralization, a mixture of surrogates with the most common end products (compounds) including HF or CF₄, and C₂F₄ should be considered in the targeted analysis [93].

Pyrolysis is a well-known thermochemical process to convert biomass/biosolids into value-added products like biochar and bio-oil [83,100,101]. Pyrolysis operating parameters such as feedstock composition, temperature, heating rate, and residence time play a decisive role in the fate of PFAS destruction. Studies have shown that pyrolysis at temperatures ranging from 250° to 800°C can effectively degrade various PFAS compounds, including PFOA and PFOS [17,23]. At temperatures above 650 °C, most PFAS are completely demineralized [14].

Pyrolysis of PFAS-biosolids and sewage sludge has been thoroughly studied and has achieved excellent results in removing all types of PFAS compounds. For instance, Thoma et al. [17] carried out pyrolysis of PFAS-biosolids around 650 °C and a residence time of 19 min. The results showed that the pyrolysis system achieved 99.9% PFAS removal, and no PFAS compound was detected in the biochar. The gas-phase analysis confirmed the presence of fluorine-containing gases like hydrogen fluoride, hydrogen chloride, and other carbon-fluorine compounds [17]. The distribution of PFAS in bio-oil was not estimated in the study; therefore, it would be interesting in the future to examine the fate of PFAS in bio-oil as well. Another study performed pyrolysis of PFAS-biosolids at 500–600 °C and obtained more than 90% removal of PFOA and PFOS [14].

The mechanisms involved in the thermal decomposition of PFAS are mainly: cleavage of intramolecular bonds, hydrolysis, radical reactions, homolytic cleavage, and oxidation [23]. In pyrolysis, PFAS compounds are generally pyrolyzed in organofluorine products distributed in pyrolytic products. Since pyrolysis is a temperature-dependent technique, less stable bonds in PFAS compounds require lower temperatures (200–500 °C) to degrade, while strong bonds require high temperatures (500–900 °C) to initiate the degradation. For example, perfluoroether carboxylic acids need a lower temperature (200–300 °C) to decompose than PFCAs with the same number of fluorinated carbons, demonstrating that the presence of ether bonds makes the molecule weaker [24]. Similarly, PFCA compounds are considered less stable than PFSA and thus require 200 °C for the former and 450 °C for the latter category to initiate the decomposition.

The destruction of any PFAS compound is completely dependent on the strength and types of chemical bonds in the PFAS structure and the bond dissociation energies (BDE) required to break them. Recently, Alinezhad et al. compared PFAS degradation of several polyfluorinated compounds (N-MeFOSAA, 8:2 FTS, PFOAB, PFOAAmS, PFOSB, and PFOSAmS), perfluoroalkyl compounds (PFOS, PFOA) and fluorinated ether compounds (HFPO-DA and 6:2 Cl-PFAES) in the presence of air and inert environment [102]. The results reported nearly complete degradation (>99%) for all PFAS compounds at 500 °C under both conditions. The minimum temperature required to decompose more than 30% of PFOA and PFOS alternatives was found to be 200 °C. The authors further revealed that among all the studied PFAS compounds, polyfluorinated compounds were thermally most unstable compounds (compared to fluorinated ether compounds and perfluoroalkyl compounds) because of the presence of a nonfluorinated moiety that can readily undergo side-chain stripping. Thermal degradation of PFAS compounds (for example, PFOA and PFOS) has been recommended to follow a three-step random-chain scission pathway [103]. The possible degradation mechanism is shown in Fig. 6.

Thermal degradation of PFOA can be initiated with a homolytic cleavage of weaker C - C bond, while in PFOS, the C - S bond next to the sulfonate group could be a preferrable target since it has less BDE compared to the C-F bond [104]. This first step of degradation initiation with C-C bond cleavage in PFOA generates a nonfluorinated moiety and a perfluoroalkyl biradical $C_7F_{14;}$ and $C\,{-}S$ bond cleavage in PFOS forms a nonfluorinated moiety and a perfluoroalkyl biradical C₈F₁₆. The second step is called chain propagation which involves the defluorination of perfluoroalkyl radical and radical chain propagation reactions, resulting in the formation of shorter-chained perfluoroalkyl radicals. Subsequently, the perfluoroalkyl radicals can recombine with carboxyl groups to generate PFCA intermediates. The last step is called termination which comprises the termination of chain propagation reactions to produce very short fluorinated units as the end products [104]. The pyrolysis of PFOA and PFOS at 500 °C produces a similar type of fluorinated products such as perfluoro-1-heptene (C_7F_{14}), 1 H-perfluorohexane perfluoro1-hexene $(C_6HF_{13}),$ $(C_6F_{12}),$ perfluoro-1-butene (C₄F₈), hexafluoropropene (C₃F₆), and tetrafluoroethylene (C₂F₄). The compounds can be generated following a random chain scission mechanism as explained previously. In addition, the pyrolysis of PFOS produced long-chain perfluoroalkanes, including perfluorooctane (C_8F_{18}) and perfluoroheptane (C_7F_{16}), following a chain-scission and recombination mechanism [102].

Thermal degradation of cationic (PFOAAmS) and zwitterionic (PFOSB) PFAS compounds has been found to yield PFOA and PFOS [103]. Fig. 7 presents two thermal decomposition mechanisms of polyfluoroalkyl sulfonamides: (i) a radical-mediated mechanism involving end-chain scission and random-chain scission to form PFOA and homologues and (ii) a chain-stripping mechanism where the nonfluorinated moiety is eliminated. In the first pathway, the thermal decomposition of PFOSB follows multistep radical chain reactions similar to PFOS which include initiation, chain propagation, and termination reactions. However, compared to PFOS, in PFOSB, two types of initiation reactions can be favored; (a) end-chain scission: where PFAS are cleaved from the bond between the nonfluorinated side chain and perfluoroalkyl chain, producing a perfluoroalkyl radical that further undergoes C radical oxidation to form PFOA [105]. The second initiation reaction is random-chain scission that involves a C-C bond cleavage at apparently random locations on the perfluoroalkyl chain.

a) Initiation

c) Termination

2RCF₁· -



Fig. 6. Possible "unzip" decomposition pathways of perfluoroalkyl substances during thermal treatment. Reproduced with permission [102]. Copyright (2022) American Chemical Society.



Fig. 7. Thermal decomposition pathways of polyfluoroalkyl sulfonamides. Reproduced with permission [103]. Copyright (2021) American Chemical Society.

The resultant perfluoroalkyl radicals also undergo C radical oxidation to form perfluoroalkyl carboxylic acids of different chain lengths, such as PFHpA and PFHxA [103].

The second thermal decomposition mechanism of polyfluoroalkyl sulfonamides involves the degradation of the nonfluorinated moiety which produces PFOS and other polyfluoroalkyl substances, as shown in Fig. 7. A similar thermal decomposition mechanism has been suggested for anionic polyfluoroalkyl substances, namely, N-MeFOSAA and 8:2

FTS [103]. The thermal degradation of 8:2 FTS also starts with the end-chain scission step, followed by the recombination step where the perfluoroalkyl radical recombines with the sulfonate group and transforms into PFOS [103].

In addition, the concentration of metal ions (such as Ca^{2+} , which may act as catalysts) in biosolids significantly influences PFAS degradation [106]. Ca(OH)₂ has been demonstrated to mineralize PFAS compounds such as PFOS and PTFE and produce CaF₂ [107,108]. The

application of Ca(OH)₂ also reduces the pollution of acidic gases during the thermal degradation of PFAS compounds [107]. Fig. S3 shows the possible mechanism of mineralization for PFOS during the thermal treatment of Ca(OH12-containing sludge. Results have shown that temperature and heating play a pivotal role in the mineralization of PFAS. At a lower temperature (400 °C), CaF2 was found after 3 min of thermal treatment and reached 50% of transformation efficiency. The total fluorine content was increased when the temperature varied from 300° to 600°C. This is mainly because this temperature range may enhance the diffusion process of fluoride into Ca-containing reactants to form CaF₂ (pathway (III) in Fig. S3) and promote the capture of gas products by the Ca-reactant (pathway V in Fig. S3). But at temperatures of 600 and 900 °C, Ca₅(PO₄)₃F was also observed in addition to CaF₂ after 1 min of the treatment, reaching 71% and 68% of transformation efficiency, respectively. This could be attributed to the reduction in the concentration of CaF₂ at higher temperatures. Ca(OH)₂ molecule contains two hydrogen and previous studies have shown that C-F bonds can be converted to C - H bonds via a hydrodefluorination reaction [66]. Hence, there is a possibility of a hydrodefluorination reaction between PFOS and Ca(OH)₂ where each fluorine of the perfluoroalkyl chain can be replaced by hydrogen of Ca(OH)₂. Hydrodefluorination reaction may initiate at alpha carbon, proximate to the sulfonic headgroup and may continue through the perfluoroalkyl chain to the terminal trifluoromethyl moiety, as shown in Eq. (1).

$$CF_{3}-(CF_{2})_{6}-CF_{2}-SO_{3}K+Ca(OH)_{2}\rightarrow CF_{3}-(CF_{2})_{6}-CHF-SO_{3}K+CaF_{2}$$
(1)

On the other hand, metal oxide like CaO forms a face-centered cubic crystal structure and the heat treatment induces cleavage of CaO crystal structure and creates reducing sites for contacting molecules such as PFOS [107]. The constant heat treatment continues to generate more reducing sites for PFOS molecules. Subsequently, PFOS would degrade to produce fluorinated carbon radicals which are considered more reactive than PFOS molecules and therefore, react with CaO to form CaF₂. Mineralization of PTFE, PFOA and FOSA is also considered to occur in a similar way to PFOS; however, the temperature range can have a different influence. For instance, PTFE was readily mineralized in the presence of $Ca(OH)_2$ at 400 °C, achieving an 80% of fluorine transformation ratio which is higher than PFOS and PFOA [108].

Liming (the addition of calcium hydroxide) of biosolids is a common treatment aimed at reducing odor and immobilizing potentially toxic elements. The addition of lime to biosolids can help to increase the pH of biosolids, which in turn, can promote the stabilization of organic matter and the reduction of pathogens. The occurrence of lime in biosolids can further enhance the decomposition or destruction of PFAS during the pyrolysis process, following the different destruction pathways discussed above [107,108]. Therefore, pyrolysis could be a preferred solution to mitigate PFAS contamination in limed-biosolids.

Apart from the solid waste stream like biosolids, it is important to understand PFAS degradation in liquid waste streams like groundwater and wastewater. In this regard, photo-induced processes have a substantial tendency to enhance PFAS degradation, which mainly targets C-F bond breakage and has no effect on the surrounding H₂O molecules [109]. PFAS degradation mechanisms under photo-induced processes usually occur on electronic-excited surfaces [109]. Real-time time-dependent density functional theory (RT-TDDFT) calculations are highly advantageous to examine the reaction dynamics of photo-induced PFAS degradation. A recent study demonstrated RT-TDDFT calculations for photo-induced PFOA degradation under a variety of optical fields and observed unique dissociation dynamics of different C-F bonds as a function of time [109]. For instance, before the irradiation, all C-F bonds in PFOA had an initial length of ~ 1.35 Å but after the irradiation, C – F bonds showed minor to major oscillations [109]. Particularly, the C3-F14 bond initially contracted up to the time of 12 fs but rises constantly thereafter, whereas other C-F bonds showed continuous oscillation from the beginning (1 fs) to the end (35 fs) before the

breakage of C3 - F14 and C1 - F10 bonds [109]. Overall, the study revealed that photo-induced PFAS degradation is quite selective for C -F bond cleavage without affecting the surrounding H₂O molecules.

Another promising approach for PFAS remediation is through the use of hydrated electrons. Hydrated electrons are highly reactive species that can reduce the C-F bonds in PFAS, leading to their degradation [110,111]. Hydrated electrons can be generated through various means, such as the radiolysis of water or the use of chemical reducing agents. In the presence of PFAS, hydrated electrons can selectively attack the C-F bonds, breaking them down into smaller, less toxic compounds. The initial degradation stage requires the conversion of a C-C bond resembling an alkane into a C = C bond resembling an alkene within the PFAS molecule [111]. This process is triggered by the trans elimination of F atoms bonded to C atoms located next to each other [111]. A recent study explored the degradation mechanism of PFOS and PFOA with hydrated electrons in water using ab initio molecular dynamics (AIMD) simulations and revealed that the activation barrier for C-F bond dissociation in PFOS is three times greater than that in PFOA [110]. Before reacting with PFAS, the hydrated electron undergoes the transition from a localized state to a delocalized state several times [110]. In the beginning, the hydrated electron delocalizes over C3 and C4 atoms of a PFOS molecule and then the spin density localizes at the C3 centre (the dissociation site) and cleaves the C-F bond [110]. To get more information on the comparative degradation of PFOS and PFOA, C-F bond distances were calculated from pre-created cavity simulations for the hydrated electron. The results revealed that in the start, the C-F bond fluctuated around 1.35 Å but at the end of the simulation, the distance of the C – F bond was stretched to 3 Å, indicating the complete dissociation. The degradation of PFOA with the hydrated electron is carried out by two primary reaction pathways that involve H/F exchange and chain shortening [110]. On the other hand, the presence of a sulfonic functional group in PFOS leads to the C3 and C4 carbon centres having the lowest bond dissociation energy among all C-F bonds, resulting in a distinct degradation process that differs significantly from PFOA degradation [110].

5. Conclusions and the way forward

This article reviews and compares the primary technologies used for PFAS destruction in biosolids. Among all the techniques, thermochemical processes like pyrolysis and gasification have emerged as efficient solutions to mitigate PFAS and convert biosolids into a sustainable product called biochar that can be applied for agricultural applications. On the other hand, smouldering combustion and biodegradation cannot degrade all PFAS completely but are highly economical compared to pyrolysis and gasification. Moreover, each technique follows a unique pathway for PFAS degradation. Thermal degradation of PFOS involves a three-step random-chain scission pathway that includes C-S bond cleavage, followed by defluorination of perfluoroalkyl radical, radical chain propagation reactions, and finally the termination of chain propagation reactions to produce very short-fluorinated units. The presence of oxygen could influence the end-products in the emissions. For example, the thermal degradation of PTFE in oxygen-free conditions favors the formation of C₃F₆ whereas, in the presence of oxygen, C₃F₆ is transformed to C₂F₆. The addition of catalysts like Ca(OH)₂ promotes hydrodefluorination reactions and enhances PFAS degradation. In HTL, PFOS degradation is carried through OH- catalyzed series of nucleophilic substitution and decarboxylation reactions whereas microbial PFAS degradation firstly involves C-S bond cleavage followed by hydroxylation, decarboxylation and defluorination reactions to form perfluoroheptanoic acid (PFHpA). Basic solvents like NaOH and DMSO promote decarboxylation reactions and improve the degradation of PFAS in the HTL process.

Destruction of PFAS-biosolids in thermochemical techniques especially pyrolysis and gasification is remarkable that can remove up to 99% of PFAS and its understanding has been progressing in an upright direction. However, there is still a large scope to further understand the fate of PFAS in these thermochemical techniques. For instance, biosolids are usually contaminated with a mixture of varying proportions of PFAS compounds and may require different temperature ranges to destroy long-chain PFAS compounds, such as PFDA and PFUnDA. Therefore, more studies are required to optimize the operating conditions of thermochemical techniques considering the mixtures of diverse PFAS compounds. In addition to this, the composition of biosolids, especially, the presence of divalent cations like Ca^{2+} and Mg^{2+} enhances the thermal degradation of PFAS. Hence, more studies can be designed to study the effect of other mono or divalent cations, or other contaminants present in biosolids since considerable concentrations of contaminants like PPCPs have been reported in biosolids. Moreover, the addition of certain catalysts targeting the dissociation of C -F bonds can be highly advantageous to enhance the thermal degradation of PFAS. Currently, noncatalytic pyrolysis has been widely studied for PFAS destruction and less attention has been paid to employ the catalysts. Bentel et al. [34] revealed that it requires higher energy (117.7–122.7 kJ mol⁻¹) to break the C-F bond in the CF₃ moiety of PFAS compared to the CF₂ moiety present in the fluorinated tail (106.8–110.9 kJ mol⁻¹). Hence, catalysts can be designed to break the C –F bond in CF₂ moiety to further reduce the activation energy and increase the PFAS destruction rate. Employing catalysts in pyrolysis can decrease the required temperature for the process, reducing the energy input demand.

The formation of undesirable by-products or intermediate PFAS products is not completely known in biological and thermochemical techniques. Thus, future studies should focus on the identification of byproducts or intermediate PFAS products, which can also help to completely understand the mechanism of PFAS destruction. Meanwhile, studies should also emphasize the characterization and identification of the incomplete combustion products of PFAS under different operating parameters since the understanding of the generation of incomplete combustion by-products is almost completely unknown. The outcomes of these studies could be crucial to estimate the associated environmental risks of the emissions generated from these technologies and developing possible measures to mitigate them.

The analysis of intermediate PFAS compounds during pyrolysis or gasification causes a substantial barrier to understand their degradation mechanism. For example, quantifying PFAS in bio-oil or gases in realtime is a great challenge. Hence, more advanced sampling and analytical methods are required to develop the accurate measurement and identification of incomplete combustion by-products or intermediate PFAS products. Particularly, at the pilot-scale, there is a lack of knowledge about the efficiency of treatment processes for thermal degradation products of PFAS. Evaluation of total fluorine measurements in ash and gaseous emissions in PFAS treatment processes would be a key which would require analytical techniques that can close the fluorine mass balance. Analysis of trace amounts of PFAS in ash is a major challenge since the instrumentation detection limits for total fluorine are high. Therefore, to detect the trace level of PFAS in ash, concentration methods are required for the sample preparation.

Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

Data Availability

No data was used for the research described in the article.

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Environmental Implications

Per- and polyfluoroalkyl substances (PFAS) are persistent organic chemicals and are considered one of the most hazardous pollutants on earth. They possess high environmental risks to human health, plants, and terrestrial and aquatic animals. In this manuscript, we have reported PFAS contamination in biosolids and the physicochemical properties of PFAS and biosolids responsible for PFAS accumulation in biosolids. We reviewed thermochemical and biological processes for PFAS degradation and critically discussed PFAS degradation mechanisms for each technology. We also highlighted the major challenges of these technologies and suggested possible solutions to improve them. We believe this manuscript could be of high interest if published in the Journal of Hazardous Materials.

Appendix A. Supporting information

Supplementary data associated with this article can be found in the online version at doi:10.1016/j.jhazmat.2023.131212.

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