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Thermal History of the Ecstall Pluton from ⁴⁰Ar/³⁹Ar Geochronology and Thermal Modeling

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1	Thermal history of the Ecstall pluton from ${}^{40}\text{Ar}/{}^{39}\text{Ar}$ geochronology and thermal
2	modeling
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7	Abstract
8	New ${}^{40}\text{Ar}/{}^{39}\text{Ar}$ thermochronology results and thermal modeling support the
9	hypothesis of Hollister et al. (2004), that reheating of the mid-Cretaceous Ecstall pluton
10	by intrusion of the Coast Mountains Batholith (CMB) was responsible for spatially
11	variable remagnetization of the Ecstall pluton. 40 Ar/ 39 Ar cooling ages from hornblende
12	and biotite from 12 locations along the Skeena River across the northern part of the
13	Ecstall pluton decrease with proximity to the Quottoon plutonic complex, the nearest
14	member of the CMB to the Ecstall pluton. The oldest 40 Ar/ 39 Ar cooling ages are found
15	farthest from the Quottoon plutonic complex, and are 90 ± 3 Ma for hornblende, and 77.9
16	\pm 1.2 Ma for biotite. The youngest ${}^{40}\text{Ar}/{}^{39}\text{Ar}$ cooling ages are found closest to the
17	Quottoon plutonic complex, and are 51.6 \pm 1.2 Ma for hornblende, and 45.3 \pm 1.7 Ma for
18	biotite. No obvious relationship between grain size and age is seen in the Ecstall pluton
19	biotites. Spatial trends in ⁴⁰ Ar/ ³⁹ Ar cooling ages are consistent with model results for
20	reheating by a thermal wall at the location of the Quottoon plutonic complex. Although
21	no unique solution is suggested, our results indicate that the most appropriate thermal
22	history for the Ecstall pluton includes both reheating and northeast side up tilting of the
23	Ecstall pluton associated with intrusion of the Quottoon plutonic complex. Estimates of

northward translation from shallow paleomagnetic inclinations in the western part of the
Ecstall pluton are reduced to ~3,000 km, consistent with the Baja-BC hypothesis, when
northeast side up tilting is accounted for.

27 1. Introduction

28 The Baja-BC hypothesis proposes that the westernmost accreted terranes of 29 British Columbia, which comprise the Insular and Intermontane superterranes (figure 1), 30 accreted at low latitudes, and then translated northward up to ~3,000 km for the Insular 31 superterrane, and ~1,100 km for the Intermontane superterrane (Umhoefer 1987, 32 Umhoefer et al. 1997, Cowan et al. 1997). This hypothesis stems from a plethora of 33 shallow paleomagnetic inclinations from rocks of these superterranes (Irving and Wynne, 34 1990). The Baja-BC hypothesis has been controversial due to a lack of supporting 35 geologic evidence (Dickinson 1976, Davis et al. 1978, Wernicke et al. 1992) and 36 ambiguities about the significance of the paleomagnetic data. For example Butler et al. 37 (2006) showed that anomalously shallow paleomagnetic directions from Cretaceous 38 plutons just west of the Ecstall pluton that crystallized at deep crustal levels, ~20 km, 39 could be explained by crustal tilting during exhumation. In contrast, Jurassic plutons 40 further west that crystallized at shallower crustal levels gave concordant directions with 41 cratonic North America (Butler et al. 2006). The Ecstall pluton, an intrusive element of 42 the Insular superterrane, is particularly interesting and controversial because it has 43 paleomagnetic directions that change systematically from west to east. They are 44 anomalously shallow in the west and, if taken at face value, imply poleward translation of 45 \sim 7,000 km relative to North America since the mid-Cretaceous. The steeper 46 paleomagnetic directions from the eastern part of the Ecstall pluton are concordant with

47 results from cratonic North America. Butler et al. (2002) proposed that local scale 48 deformation (i.e. folding) caused the anomalously shallow directions in the western 49 Ecstall pluton, and thus that paleomagnetic directions were not consistent with large-scale 50 northward translation. Harrison (1977) and Harrison et al. (1979) concluded that the 51 Ecstall pluton was reheated by the Quottoon pluton resetting the ages near the Quottoon 52 pluton. Hollister et al. (2004) went on to propose that the Ecstall pluton, and indeed the 53 entire Insular superterrane, was reheated by intrusion and uplift of the Coast Mountains 54 Batholith (CMB), and that reheating reset paleomagnetic directions in the Ecstall pluton 55 by changing the thermo-chemical magnetic remanence held by lamellar magnetism in 56 hematite-ilmenite solid solutions. Hollister et al. (2004) concluded that the steeper 57 directions seen in the eastern part of the Ecstall pluton had been reset by the Eocene 58 reheating, and that the shallow directions in the western Ecstall pluton were unaffected, 59 retaining Cretaceous inclinations, and are therefore consistent with large-scale northward 60 translation. Distinguishing between these competing hypotheses for the Ecstall pluton is 61 critical to understanding the tectonic history of the Ecstall pluton and how it fits into the 62 Baja-BC hypothesis.

The Coast Shear Zone (CSZ) is a large ductile shear zone that has been proposed as capable of accommodating Baja-BC-like translations (Andronicos et al. 1999). The CSZ separates the ~80-50 Ma CMB in the Intermontane superterrane from the ~91 Ma Ecstall pluton in the Insular superterrane (figure 1). A compilation of ⁴⁰Ar/³⁹Ar and K-Ar cooling ages from the Ketchikan area, which is mainly north of the Ecstall pluton, suggests that cooling ages from the Insular supperterrane are reset towards the younger CMB (Hollister et al. 2004). If reheating caused remagnetization close to the CMB, and

there is no structural explanation for shallower than expected directions farther from the
CMB, then large northward translation is suggested by paleomagnetic data from the
Ecstall pluton.

This study uses detailed ${}^{40}\text{Ar}/{}^{39}\text{Ar}$ thermochronology on hornblende and biotite in 73 74 conjunction with thermal modeling to test the reheating hypothesis for the Ecstall pluton 75 in particular. If reheating was experienced by the entire Insular superterrane, it should be 76 recorded by consistent spatial trends in cooling ages in the Ecstall pluton with respect to 77 the Quottoon plutonic complex, the nearest member of the CMB. We use numerical 78 methods, similar to those of Hollister et al. (2004), to model reheating in the crust, and 79 find the type of thermal history that best reproduces the trends in cooling ages across the 80 Ecstall pluton. In addition to reheating, other factors, such as exhumation history, and 81 tilting, are considered, and prove to be important in explaining the cooling age trends 82 found in the Ecstall pluton.

83 2. Methods

84 2.1. 40^{40} Ar/39Ar Geochronology

85 Hornblende and biotite were separated from 12 samples from a transect along the 86 Skeena River (figure 2) using standard separation techniques. Crushed samples were 87 sieved into 4 size fractions, 600-850, 450-600, 300-450, and 250-300 µm. Biotite was 88 picked from each of the four size fractions in order to investigate possible age- grain size 89 relationships due the effects of variable diffusion dimensions on closure temperature (e.g. 90 Wright et al., 1991; Goodwin and Renne, 1991). Hornblende was picked from the 300-91 450 µm size fraction. Samples were irradiated at the OSU TRIGA reactor for 10-20 92 hours. Fish Canyon sanidine at 28.02 Ma (Renne et al. 1998) was used as a fluence

93 monitor. We analyzed single grains of biotite from the largest of the two size fractions, 94 and multi-grain aliquots of biotite from the 2 smallest size fractions, and hornblende from 95 the 300-450 μ m size fraction by step heating in 11-15 steps using a CO₂ laser. Total 96 fusion analyses were also performed on single crystals of biotite from the small size 97 fraction of two samples. The gas released was analyzed on a MAP 215 mass spectrometer 98 by peak-hopping using a Balzers electron multiplier in analog mode. Because biotite age 99 spectra produced by *in vacuo* step heating are subject to artifacts unrelated to Ar 100 concentration gradients (e.g. Gaber et al. 1988; Lo et al. 2000; Min et al. 2001), biotite 101 ages reported are integrated ages, calculated as the mean of all steps weighted by the amount of ³⁹Ar released in each step. For hornblende the principal concern was to obviate 102 103 age bias due to biotite inclusions and thus plateau ages, generally coinciding with 104 uniform Ca/K, were used. Though low-temperature discordance is not typical in our 105 samples, misinterpretation of young step ages due to inclusions or secondary phases with 106 distinct Ca/K has been shown to produce spurious conclusions about diffusive loss from 107 hornblendes (Onstott and Peacock, 1987). A plateau as used herein includes at least 3 108 consecutive steps, which are mutually indistinguishable at 1-sigma and encompass 50% or more of the total ³⁹Ar released. The plateau age is calculated by the inverse variance 109 110 weighted mean of all the plateau steps. Age errors are reported at the 95% confidence 111 level.

112 2.2. Thermal modeling

113 The thermal model utilizes a finite volume approximation to the advection-114 diffusion equation after Patankar (1980):

$$\rho \frac{\partial \phi}{\partial t} + \rho \upsilon \nabla (\phi) = \nabla (D \nabla (\phi)) + H$$
(1)

115 where $\rho = \text{density}$, $\phi = \text{heat}$, $\upsilon = \text{velocity}$, D = diffusion coefficient, and H = heat116 production. Numerically we are solving the full advection-diffusion equation with a 117 specified velocity field; however, because we have no constraints on fluid flow through 118 the Ecstall pluton during reheating and therefore prescribe a zero velocity field, this 119 equation can be simplified to the conduction equation:

120
$$\frac{\partial \phi}{\partial t} = -D\nabla^2 \phi + H$$
 (2)

121 The initial thermal structure of the crust was calculated by assuming a depth distribution 122 of heat-producing radioactive elements. A few distributions of heat production that yield 123 simple analytical solutions to T(y) were investigated to ensure that the numerical steady 124 state reproduces the analytical solution (Figure 3). We chose to use the simplest 125 distribution of heat production in the crust, i.e. constant, for further calculations because 126 the actual distribution is unknown. The heat flux from the mantle, q_m, is held constant 127 and chosen so that temperatures are between 250 and 300 °C at 15 km for a given value 128 of heat production.

129 We approximate the Quottoon plutonic complex as a thermal wall after Hollister 130 et al. (2004). The thermal wall extends from 0 to 40 km depth and is 5 km thick, ~half the 131 average width of the Quottoon plutonic complex. The boundary at the outer edge of the 132 thermal wall, right boundary, is a zero flux boundary, approximating the center of a 133 cooling intrusion. The left boundary is also a zero flux boundary. The surface boundary is 134 held at 0 °C. The lower boundary, 40 km, is held at a constant heat flux from the mantle, 135 q_m. The effect of latent heat of crystallization is approximated by implementing an 136 effective heat capacity during the crystallization temperature interval after Webber 137 (1999):

(3)

138 $Cp_{eff} = Cp + q_{LH}/(T_1-T_2)$

139 where Cp is the heat capacity, q_{LH} is the latent heat of crystallization, and T_1 - T_2 is the temperature interval over which crystallization occurs. We take T1-T2 to be 100 °C (750 -140 141 650 °C), and q_{LH} to be 80 Cal/g. When temperatures in the thermal boundary are between 142 750 and 650 °C, Cp_{eff} replaces Cp in the calculations, which lowers the thermal 143 diffusivity and slows cooling during this interval. We prescribe an initial temperature for 144 the thermal wall of 700 °C, which is the temperature used for the thermal wall in Hollister 145 et al. (2004). Care was taken to ensure that the discretization scheme led to consistent and 146 stable results. All model parameters are listed in table 1, and a schematic illustration of 147 the thermal model is included in electronic annex EA-1.

148 2.3. 40 Ar/ 39 Ar age modeling

Given a model thermal history, cooling ages are modeled by solving the diffusionequation using polar coordinates after Morton and Mayers (2005):

151
$$\frac{\partial C}{\partial t} = \frac{D}{r^{\alpha}} \frac{\partial}{\partial r} \left(r^{\alpha} \frac{\partial C}{\partial r} \right) + P$$
(4)

where C is concentration of argon, D is the diffusion coefficient, P is production of ⁴⁰Ar by decay of ⁴⁰K, r is the radius, and $\alpha = 0$, 1, or 2 for plane, cylindrical, or spherical symmetry, respectively. Biotite is modeled using cylindrical geometry, and hornblende using spherical geometry, as is generally assumed (e.g. Harrison, 1981; Grove and Harrison, 1996). We assume a zero concentration boundary at the edge of the crystal (c.f., Baxter et al., 2002). The diffusion coefficient follows the Arrhenius relationship: $D = D_0 \exp(E_a/RT)$ (5)

159 where E_a is the activation energy for argon diffusion, R is the gas constant, T is the 160 temperature, which is obtained from the thermal model, and D_0 is the pre-exponential

161	factor corresponding to a frequency factor of D_0/a^2 , where a is the diffusion dimension.
162	Values of E_a and D_0 are taken from Harrison (1981) for hornblende, and Grove and
163	Harrison (1996) for biotite. Diffusion parameters for biotite may have a compositional
164	dependence, and the composition of biotites from the Ecstall pluton varies from ~45-50%
165	annite. For this reason model ages are calculated using both diffusion parameters from
166	Grove and Harrison (1996), which should bracket those of the biotites from the Ecstall
167	pluton. We assume values for effective diffusion dimension, a, of 40 μm for hornblende,
168	which is consistent with Harrison (1981), and 500 μ m for biotite, which is consistent with
169	the largest grain dimensions, and gives reasonable closure temperatures if we are to
170	assume that biotite retains ⁴⁰ Ar before reheating at 15 km depth. At the start of the model,
171	91 Ma, we assume zero concentration of radiogenic 40 Ar and a uniform concentration of
172	40 K. 40 Ar is allowed to grow into the crystal, and diffuse out depending on the
173	temperature, which in turn depends on location. This method of forward modeling allows
174	us to investigate the effects of exhumation history on calculated cooling age.
175	3. Results
	10

176 3.1^{40} Ar/³⁹Ar Geochronology

The overall trend in ⁴⁰Ar/³⁹Ar ages from the Ecstall pluton is very similar to the Hollister et al. (2004) compilation of ⁴⁰Ar/³⁹Ar and K-Ar ages for the Ketchikan region, with minor differences explained by different definitions of distance from the thermal boundary (Figure 4). In this study distance is measured to the nearest edge of the Quottoon plutonic complex, and in Hollister et al. (2004) distances are calculated by projecting sample locations onto a linear transect perpendicular to the trend of the Coast Shear Zone. Because of the different measurement techniques, the samples from Butler et

184 al. (2002), which are from the same locations as 008, and 001 in this study, plot \sim 4, and 185 \sim 3 km further from the thermal boundary, respectively, in the Hollister et al. (2004) compilation than in this study. In the western part of the Ecstall pluton, ${}^{40}\text{Ar}/{}^{39}\text{Ar}$ ages for 186 hornblende are between 90 \pm 3 and 79.2 \pm 0.7 Ma (table 2). Biotite 40 Ar/ 39 Ar ages from 187 188 this part of the Ecstall pluton are about 10 Ma younger than the hornblende cooling ages, 189 and are between 77.9 \pm 1.2 and 68.9 \pm 1.1 Ma (table 2). 190 Closer than about 14 km from the Quottoon plutonic complex the average 191 difference in ages between biotite and hornblende increases. This may be a result of biotite losing radiogenic ⁴⁰Ar by diffusion at lower temperatures than hornblende; 192

however, age spectra remain mostly flat (Figure 5). Four size fractions of biotite were
analyzed, and no clear relationship between grain size and age is seen. In many cases the
smallest grain size gives the youngest age, but all size fractions are generally within error
of each other (figure 4).

Hornblende from the Ecstall pluton shows evidence of reheating closer than about
8 km from the Quottoon plutonic complex with a distinct decrease in cooling ages.
Hornblende age spectra commonly show evidence of minor surface-correlated excess

200 argon in the form of anomalously old ages in low temperature heating steps (figure 6),

201 but all yield plateaus interpreted as cooling ages. Isochrons exhibiting supra-atmospheric

202 initial 40 Ar/ 36 Ar ratios are also indicative of excess argon (EA-2). There is no obvious

spatial trend in amounts of excess argon like that observed by Baxter et al. (2002).

204 3.2. Modeling

When the thermal wall is set to 700 °C at the start of the model, and then allowed to cool with latent heat release of 80 Cal/g between 750-650 °C, the thermal structure of

207 the crust returns to near steady state by ~ 20 Ma (Figures 7 and 8); however, even after 40 208 Ma the total energy in the system is still elevated by $\sim 5\%$. Advection of heat by fluids 209 may be an important factor that could increase cooling efficiency, however, because we 210 have no real constraints on fluid flow through the Ecstall pluton we have ignored these 211 effects, i.e. the model assumes that conduction controlled heat flow. This assumption is 212 consistent with the thermal model of Hollister et al. (2004), and with the first-order 213 observation that most of the Ecstall pluton shows little evidence of pervasive post-214 crystallization fluid interaction, although without a detailed isotopic study (e.g. Gordon et 215 al. (2009)), we cannot preclude fluid interaction at the time of reheating. For the purposes of calculating model ${}^{40}\text{Ar}/{}^{39}\text{Ar}$ ages the temperatures given by the thermal model are used 216 217 for 58-18 Ma (i.e. emplacement of Quottoon plutonic complex at ~58 Ma (Gehrels et al. 218 1991)), and the steady state geotherm is assumed for all other times. 219 Assuming a depth of emplacement of 27 km (7.4 - 8.4 kbar, Butler et al. 2002), a 220 depth of reheating of 15 km as used in Hollister et al. (2004), and exhumation rates of 221 ~ 0.3 km/Ma except for a 5 Ma interval (58 – 53 Ma) during and after reheating when 222 depth is held constant, the modeled age trends are broadly consistent with the data (figure 223 9a) using published diffusion parameters for hornblende and biotite (table 1). The model 224 ages are reset at approximately the same distances from the thermal boundary, and the general shape of the trend is similar for the parts of the Ecstall pluton that are clearly 225 226 affected by reheating (i.e. <14 km and <8 km from the thermal boundary, for biotite, and 227 hornblende respectively). Some misfit occurs, particularly in the distance at which 228 hornblende ages are affected. This misfit could be reduced by a longer duration of 229 reheating, or greater depth during reheating. Changing the initial conditions of the model,

i.e. depth of emplacement, depth of reheating, and exhumation rate, all affect how
accurately the model ages reproduce the measured ages, but the shape of the model age
trend does not change.

233 4. Discussion

234 The age spectra for both hornblende and biotite are generally flat, even when slow 235 cooling can be assumed, and reheating is suggested by thermal modeling. Biotite and 236 hornblende are both hydrous minerals that are unstable during *in vacuo* laser heating, and 237 for this reason may not produce meaningful release patterns that reflect spatial Ar 238 isotopic gradients (e.g. Gaber et al. 1988; Grove and Harrison, 1996; Lee et al. 1991). In 239 particular, Lee et al. 1991 suggest that breakdown of hornblende, and formation of new 240 phases during in vacuo laser heating homogenizes the Ar released, and therefore it is 241 unlikely that original spatial gradients in Ar over any one hornblende grain will be 242 preserved. Thus, a flat age spectrum given by in vacuo laser heating of hornblende and biotite does not in itself preclude diffusive loss of ⁴⁰Ar. 243

The lack of a grain size effect in 40 Ar/ 39 Ar ages of biotite from the Ecstall pluton 244 245 could be an indication that effective diffusion dimension is smaller than the smallest 246 grain size analyzed. It could also be explained by fragments of larger grains being 247 confused for small grain sizes. We made every effort to pick euhedral grains, but it is 248 possible that a significant number of our small grains were actually fragments of larger 249 grains. This could also explain why there are a few instances where single grains of approximately the same size yield 40 Ar/ 39 Ar ages that are not within error of each other 250 251 (i.e. samples 001, Sk-9, and 008).

252	Agreement between the modeled and observed trends in hornblende ages might
253	be improved if the duration of reheating is longer. Rusmore et al. (2005) showed that
254	magmatism in the Central gneiss complex, south of our study area and just east of the
255	Quottoon plutonic complex, was nearly continuous from 90-67 Ma, followed by rapid
256	cooling of the entire complex at ~52 Ma. Closest to our study area, the Quottoon
257	plutonic complex gives a U-Pb zircon age of 58.6 ± 0.8 Ma (Gehrels et al. 1991). The
258	youngest and westernmost members of the Quottoon plutonic complex in nearby areas
259	give ages of ~59-55 Ma, (summarized in Crawford et al. 1999). Crawford et al. (1999)
260	conclude that the Quottoon plutonic complex was emplaced as a series of individual
261	intrusions which would increase the duration of reheating relative to a single intrusion.
262	Also, the timing of metamorphism in the Central Gneiss Complex indicates relatively
263	high temperatures until ~52 Ma (Rusmore et al. 2006). An increase in the duration of
264	reheating would increase maximum temperatures reached near the thermal boundary, and
265	increase the distance at which hornblende ${}^{40}\text{Ar}/{}^{39}\text{Ar}$ ages are affected. It would also
266	increase the distance at which biotite ages are affected; however, discrete intrusions
267	would have a smaller effect at greater distances. The apparent misfit between observed
268	and modeled age trends might also arise from lower Ar diffusivity in biotite than
269	predicted by the experimental kinetic parameters we employed. Villa and Puxeddu
270	(1994), for example, suggested that biotite retains argon at higher temperatures in nature
271	than in laboratory diffusion experiments. Modeling biotite with a higher activation
272	energy, or lower D_0 , has the effect of improving the fit of modeled age trends with the
273	observed biotite ages; however, as noted in Villa and Puxeddu (1994), the uncertainties in

the temperature and duration of the reheating event are limiting factors in our ability tocome to the same conclusion.

The greatest misfit between observed and modeled 40 Ar/ 39 Ar age trends occurs far 276 277 from the thermal wall where cooling ages are either not affected, or only partially 278 affected by reheating. In this region, the trend in measured cooling ages is steeper than 279 the modeled trend, which is flat. Since this part of the Ecstall pluton is not expected to be 280 affected by reheating according to the thermal model, there must be some other 281 explanation for the trend in observed ages for both hornblende and biotite. One 282 possibility is tilting after uplift through the hornblende and biotite closure isotherms. The trend in ⁴⁰Ar/³⁹Ar ages in the unheated parts of the Ecstall pluton is approximately linear 283 284 for both hornblende and biotite, although there are only 3 locations beyond 14 km to 285 constrain the trend where biotite is not expected to be affected by reheating. To explain a 286 sloping linear trend in cooling ages by uplift and tilting, simple trigonometry leads to a 287 relation between exhumation rate, ER, and tilt angle, B:

288

$$\sin(\beta) = ER^*M \tag{6}$$

289 where M is the slope of the linear trend (see EA-3 for an illustration). This relation is true 290 for the simplest case, where exhumation and uplift through both closure isotherms occurs 291 before tilting. For the case when tilting and exhumation through closure isotherms are 292 occurring simultaneously, the exhumation rate will not be constant across the tilting 293 body, and the age relationship due to exhumation and tilting will deviate from linear. In 294 the simplest case, for a given slope in cooling ages, greater exhumation rates imply more 295 tilting. This relation is similar to methods using cooling histories obtained from single 296 grains using apatite fission track modeling (Stockli et al., 2001), or multiple diffusion

domain modeling on potassium feldspar (Wong and Gans, 2003) to infer pre-exhumation
temperature gradients in samples from a roughly horizontal transect, indicating a depth
difference between those samples prior to exhumation.

Our ${}^{40}\text{Ar}/{}^{39}\text{Ar}$ results and existing geobarometry can be used to constrain the 300 magnitude of tilting affecting the Ecstall pluton. Differences in ⁴⁰Ar/³⁹Ar ages between 301 302 hornblende and biotite at a single location unaffected by reheating provide a measure of 303 exhumation rate if we assume the Ecstall pluton was emplaced below the biotite closure 304 isotherm. Al-in-hornblende barometry indicates that the Ecstall pluton was emplaced at 305 \sim 27-31 km depth (7.4-8.4 kbar, Butler et al. 2002), which is well below the nominal 306 biotite closure isotherm of ~300 to 350 °C in most geothermal gradients, including our 307 modeled geothermal gradient. Exhumation rates calculated using the differences in hornblende and biotite ${}^{40}\text{Ar}/{}^{39}\text{Ar}$ ages from locations unaffected by reheating, assuming 308 309 emplacement below the hornblende closure isotherm and the modeled geothermal 310 gradient, are $\sim 0.25 - 1.2$ km/Ma. A maximum constraint on tilting can be given by 311 pressure estimates across the pluton. Al-in-hornblende barometry gives pressure 312 estimates that range from 7.4-8.4 kbar across the Ecstall pluton (Butler et al. 2002). 313 Although there is no distinct trend in pressure estimates across the Ecstall pluton, the 314 95% confidence limits ($\pm \sim 1$ kbar) allow a depth contrast of up to ~ 10 km across the 315 Ecstall pluton. This constraint limits the maximum amount of tilting to $\sim 27^{\circ}$. 316 The effect of tilting can be easily incorporated into the diffusion model. Three 317 scenarios, each of which changes only the timing of tilting relative to reheating, are: 1) 318 tilt before reheating, 2) tilt after reheating, and 3) tilt occurring before, during, and after

reheating (figure 7). We assume exhumation, and tilt rates, that are slow enough not to

320 affect the geothermal gradient (i.e. no part of the Ecstall pluton is exhumed faster than ~ 1 321 km/Ma). The modeled ages match the data well when 25° of tilting is included (figure 9). 322 The best fit occurs when tilting occurs before, during, and after reheating. The solution is 323 not unique, as the length and temperature of the reheating event, as well as the structure 324 of the Quottoon plutonic complex, and timing and rate of tilting have all been greatly simplified. However, the good fit of the model to the data suggests that ${}^{40}\text{Ar}/{}^{39}\text{Ar}$ ages in 325 326 the Ecstall pluton are best explained by a thermal history that includes both reheating and 327 tilting. Figure 10 illustrates the effects of changing uplift rate and tilt angle on the 328 modeled cooling age trends when the tilt rate, start depth, and time of tilting (tilting is 329 finished at 48 Ma) remain constant. Higher tilt angles and lower exhumation rates give 330 steeper cooling age trends. If the Al-in-hornblende constraints are ignored, higher tilt 331 angles accompanied by higher exhumation rates may produce even better agreement with ⁴⁰Ar/³⁹Ar ages (Figure 10). A consequence of tilting occurring during exhumation 332 333 through closure isotherms is that uplift rates are increased towards the deeper portion of 334 the Ecstall pluton (i.e. toward the east in this tilting scenario). The increase in uplift rates 335 results in flattening of the modeled age trend toward the Quottoon plutonic complex, an 336 effect that is clearest in models that omit reheating by the Quottoon plutonic complex 337 (Figure 11). Also shown in figure 11 are the same cooling age trends when tilting occurs 338 after uplift through both closure isotherms. These trends are straight, except for the very 339 western part of the hornblende trend, which is already above the hornblende closure 340 isotherm.

341 5. Conclusions

342	The trend in ${}^{40}\text{Ar/}{}^{39}\text{Ar}$ ages from the Ecstall pluton is very similar to the Hollister
343	et al. (2004) compilation of ${}^{40}\text{Ar}/{}^{39}\text{Ar}$ and K-Ar ages for the Ketchikan region showing
344	that the regional trend is resolved at the single pluton scale. The trends in ${}^{40}\text{Ar}/{}^{39}\text{Ar}$ ages
345	across the Ecstall pluton are consistent with model results for reheating by the Quottoon
346	plutonic complex. This result broadly supports Hollister et al. (2004)'s hypothesis that
347	thermally sensitive features of the Insular superterrane, such as paleomagnetism, have
348	been modified by intrusion of the Coast Mountains Batholith. Mineralogic changes that
349	affect magnetic properties, and therefore the timing of acquisition of some components of
350	remanent magnetization, have also been documented in parts of the Ecstall pluton that
351	have been affected by reheating (Brownlee et al. 2010). This combination of results
352	suggests that paleomagnetic data from closer than ~14 km to the Quottoon plutonic
353	complex have been affected by reheating, and do not record ambient field conditions at
354	the time of emplacement of the Ecstall pluton.

Model results indicate that ${}^{40}\text{Ar}/{}^{39}\text{Ar}$ cooling age trends in the Ecstall pluton are 355 356 best explained by a combination of reheating and tilting. In detail, the fit of our data to 357 specific thermal models is limited by uncertainties in diffusion parameters, including the 358 diffusive lengthscales in the biotite and hornblende analyzed. Although a unique fit to the 359 data is not possible without knowing more about the structure of the Quottoon plutonic 360 complex and the timing and temperatures during emplacement of the Quottoon plutonic 361 complex, we can constrain the maximum amount of tilting experienced by the Ecstall 362 pluton to $\sim 27^{\circ}$ by the pressures indicated by Al-in-hornblende barometry (Butler et al. 363 2002). If the paleomagnetic directions from the western part of the Ecstall pluton, >14 km 364 from the thermal boundary, are corrected for 25° of northeast side up tilting (tilt axis

azimuth of 340°), the northward translation implied by the shallow inclinations is

substantially decreased from ~7,000 km to ~3,000 km, an estimate that is consistent with
the Baja-BC hypothesis.

Trends in ${}^{40}\text{Ar}/{}^{39}\text{Ar}$ ages that have been affected by tilting and reheating by the 368 369 Coast Mountains Batholith may be found in other plutons of the Insular superterrane that 370 were emplaced at depths of ~20 km or more. Spatially detailed thermochronometry and 371 thermobarometry will therefore be a necessary prerequisite to correctly interpreting 372 paleomagnetic data from plutonic rocks in this region and critically testing the Baja-BC 373 hypothesis. 374 Acknowledgements 375 This work was funded by NSF grant #EAR-0440029. We are grateful to Mark 376 Harrison, Cameron Davidson, Scott Bogue, and Peter Reiners, whose careful reviews 377 significantly improved the manuscript. We thank Lincoln Hollister for immeasurable help 378 in conceiving the project, field work logistics, and bringing the Ecstall pluton back to life; 379 Peter Freeman and Courtney Hart for assistance in the field; and Tim Becker for 380 assistance in the BGC Ar lab. 381 References 382 Andronicos, C.L., Hollister, L.S., Davidson, C., and Chardon, D., 1999, Kinematics and 383 tectonic significance of transpressive structures within the Coast Plutonic Complex, 384 British Columbia: Journal of Structural Geology, v. 21, p. 229-243. 385 Baldwin, S.L., Harrison, T.M., and Fitz Gerald, J.D., 1990, Diffusion of ⁴⁰Ar in 386 metamorphic hornblende: Contributions to Mineralogy and Petrology, v. 105, p. 691-

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 p. 70-79.
- 510 Figure Captions
- 511 Figure 1. Generalized geologic map of northeast British Columbia after Hollister and
- 512 Andronicos (2006). The Insular superterrane is located west of the Coast Shear Zone
- 513 (CSZ), and the Intermontane superterrane is located east of the CSZ. The Coast
- 514 Mountains Batholith is made up of 80-50 Ma plutons and located adjacent to the CSZ in
- 515 the Intermontane superterrane. The Quottoon plutonic complex is indicated by QP, and
- 516 includes plutonic rocks nearest the CSZ in this view. The Ecstall pluton is outlined. Box
- 517 indicates area of figure 2.
- 518 Figure 2. Generalized geologic map of the study area of the Ecstall pluton along the
- 519 Skeena River near Prince Rupert, British Columbia. Sample locations are indicated by
- 520 black dots, and labeled with sample names used in the text. Dashed lines a, and b are
- 521 examples of how distances to the Quottoon plutonic complex were measured. Geologic

relations are after Hutchison et al. (1982), and structures are after Butler et al. (2002), andCrawford et al. (1987).

524 Figure 3. Geotherms produced by 3 distributions of heat production in the crust. Thick 525 lines represent the steady state achieved by the numerical calculation, and the dashed 526 white lines are the analytic solutions for each distribution of heat production and heat flux from the mantle, q_m, which can be found in Turcotte and Schubert (2002). The black 527 528 curve is the steady state geotherm used in the modeling. Also shown are the closure 529 temperature ranges for biotite and hornblende calculated using diffusion parameters from 530 table 1, and cooling rates of 1 and 20 °C/Ma. The modeled depths of the Ecstall pluton 531 during emplacement and reheating are also shown. Figure 4. 40 Ar/ 39 Ar results from this study (diamonds) and the compilation of 40 Ar/ 39 Ar 532 533 and K-Ar results from the Ketchikan region of Hollister et al. (2004), (circles and 534 squares). As discussed in the text, the square symbols are samples 008, and 001, from 535 Butler et al. (2002), which are from the same locations as 008, and 001 in this study, but 536 they plot ~4 and ~3 km further from the thermal boundary due to the different methods of 537 measuring distance to the thermal boundary used in this study vs. Hollister et al. (2004). 538 The inset shows only results from this study. For samples from this study, symbol size 539 corresponds to grain size fraction analyzed. The gray error bars are 2σ . 540 Figure 5. Representative biotite age spectra from three samples, 008, 001, and Sk-5 at 541 21.1 km, 6.8 km, and 3.9 km from the thermal boundary, respectively. Single grain and 542 multi-grain examples are shown.

Figure 6. Representative hornblende age spectra from >14 km, 14-8 km, and <8 km from
the thermal boundary.

- 545 Figure 7. Thermal model results at 91, 58, 53, and 18 Ma. Lines a, b, c, and d are the
- 546 locations of sample transects for 4 different scenarios of exhumation and tilt.
- 547 Figure 8. Thermal model results at the depth of reheating, 15 km. a) Temperature vs.
- 548 distance from the Quottoon plutonic complex at 10,000 a, 1, 5, 10, and 40 Ma after
- 549 reheating (after 58 Ma). b) Temperature vs. time at the center of the thermal boundary (-5
- km), and 0.5, 5, 10, 15, 20, and 25 km from the edge of the thermal boundary.

551 Hornblende and biotite closure temperatures calculated from diffusion parameters in table

- 552 1 and using 1 and 20 °C/Ma cooling rates are shown.
- 553 Figure 9. 4^{40} Ar/ 39 Ar ages and model age trends for the 4 uplift and tilt scenarios in figure 7
- 554 plotted vs. distance from the Quottoon plutonic complex. black diamonds- hornblende,
- 555 white diamonds- biotite. Symbol size corresponds to grain size fraction analyzed.
- 556 Diffusion parameters used in the model are from Harrison (1981) for hornblende, and
- 557 Grove and Harrison (1996) for biotite. Model cooling age trends are shown as solid lines
- 558 (black- hornblende, gray- biotite) with dashed lines representing the ages calculated using
- 559 diffusion parameters plus or minus their reported errors. For hornblende the diffusion
- 560 parameters plus reported error plots on top of the solid line. a) no tilt, b) tilt before
- 561 reheating, c) tilt after reheating, and d) tilt before, during, and after reheating.
- 562 Figure 10. Model results for a variety of exhumation rates and tilt angles. The position
- 563 during reheating is the same for all models. This is achieved by stopping exhumation
- once the reheating depth is reached, which results in holding the deeper, and more eastern
- 565 parts of the Ecstall pluton in the biotite partial retention zone for longer periods when
- 566 higher exhumation rates are assumed. For all, the tilt rate is 1° /Ma, and tilting ends at 48
- 567 Ma (10 Ma after the start of reheating), thus tilting begins earlier for higher tilt angles.

568	Figure 11. Model results when reheating is not included. When tilting occurs during
569	uplift through closure isotherms, the age trends flatten toward the east as exhumation
570	rates are increased due to tilting. The effect of holding the deeper parts of the Ecstall
571	pluton in the biotite partial retention zone is seen by a steepening of the biotite model age
572	trend at ~14 km when 0.4 km/Ma exhumation rate is assumed. When tilting occurs only
573	after exhumation of the entire pluton through both closure isotherms (i.e. constant
574	exhumation rate until entire pluton is above ~15 km depth, followed by tilting), the age
575	trends are straight lines, as predicted by the relation between exhumation rate, tilt angle,
576	and slope of the age trend.
577	Table 1. Model parameters used for the thermal model and the diffusion/ age model.
578	Thermal model parameters were chosen to be similar to Hollister et al. (2004). Diffusion
579	parameters are from (a) Harrison, 1981, (b) Grove and Harrison, 1996.
580	Table 2. ${}^{40}\text{Ar}/{}^{39}\text{Ar}$ results. Errors are 2σ . Data from individual steps can be found in the
581	electronic annex.

Thermal model parameters				
Total width	50 km			
Total depth	40 km			
Grid spacing (dx, and dy)	0.5 km			
Total duration	40 Ma			
Time step	10,000 yr			
Density (ρ)	$2,700 \text{ g/cm}^3$			
Heat capacity (c)	1100 kJ/°C			
Thermal conductivity (K)	2.5 mW/km °C	.5 mW/km °C		
Heat production (H)	$1.0 \ \mu W/m^3$			
Latent heat production (q)	80 Cal/g			
Latent heat interval (T_1-T_2)	100 °C (750-650	°C)		
Heat flux in from mantle (f_m)	20 mW/km^2			
Temperature at surface	0 °C			
Temperature at thermal wall	700 °C			
Thickness of thermal wall	5 km			
Diffusion model parameters	Hornblende	Biotite		
Total duration	91 Ma	91 Ma		
Time step	65,000 yr	65,000 yr		
⁴⁰ K decay constant	5.543 e-10 /yr	5.543 e-10 /y		
Branching ratio	0.117	0.117		
Grain size radius (r)	250 µm	250 µm		
Grid spacing (dr)	10 µm	10 µm		
Geometry	Sphere	Cylinder		
Diffusion	parameters			
Activation energy 1 (Ea)	64.1 ± 1.7	47.1 ± 1.5		
	kcal/mol (a)	kcal/mol (b)		
Preexponential factor 1 (d_0)	0.024 +/-	0.075 +/-		
-	0.053/0.011	0.97/0.042		
	cm^2/s (a)	cm^2/s (b)		
Activation energy 2 (Ea)		50.5 ± 2.2		
		kcal/mol (b)		
Preexponential factor $2 (d_0)$		0.403 +/-		
-		0.933/0.282		
		cm^2/s (b)		
Effective diffusion dimension (a)	40 µm	500 µm		
	Table 1.			

$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Hornblende step heating results							
	Sample	Grain size (µm)	Distance from Quottoon Pluton (km)	Plateau age (Ma)	Integrated age (Ma)	MSWD	Ρ	# of steps in plateau
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Sk-4A Sk-5A Sk-6A Sk-7A	300-425 250-425 300-425 300-425	3.5 3.9 5.9 6.1	51.6 ± 1.2 54.4 ± 0.5 55.4 ± 1.1 57.1 ± 1.7	51.7 ± 0.9 55.0 ± 0.7 55.2 ± 0.6 57.3 ± 0.8	2.21 1.68 2.8 3.19	0.01 0.15 0.01 0	all 5 of 10 7 of 11 10 of 11
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Sk-8B 001 001 Sk-10B	300-425 300-425 250-425 425-600	6.3 6.8 6.8 7.6	57.4 ± 1.3 70.5 ± 1.1 67 ± 2 68 ± 2	62.1 ± 1.7 66.5 ± 1.0 68.5 ± 1.2 71.6 ± 1.5	1.14 1 2.24 3.63	0.33 0.44 0.05 0.01	4 of 11 13 of 14 6 of 14 5 of 11
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Sk-10B Sk-9A Sk-9B	250-300 250-425 300-425	7.6 10.6 10.6	69.5 ± 1.2 75.9 ± 0.7 77.3 ± 0.7	70.1 ± 1.3 77.1 ± 0.8 78 ± 0.8	0.61 1.27 0.78	0.79 0.24 0.65	10 of 11 11 of 12 11 of 12
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	SK-3A Sk-2A Sk-1A Sk-1A	300-425 300-425 300-425 250-425	13.4 16.4 17.3 17.3	79.3 ± 0.6 83.4 ± 1.2 83.1 ± 1.7 79.2 ± 0.7	79.5 ± 0.8 83.7 ± 1.3 83 ± 1.3 78.3 ± 0.8	1.28 1.03 1.85 0.94	0.23 0.41 0.05 0.46	11 of 12 11 of 12 11 of 12 6 of 12
Biolite step freating results Distance from Quottoon Pluton (km) Integrated age (Ma) Plateau age (Ma) MSWD P # of steps in plateau Sk-5A 425-850 3.9 47.1 ± 0.8 47.2 ± 0.7 0.64 0.78 all Sk-5A 425-850 3.9 47.7 ± 1.0 47.8 ± 0.8 0.21 1 all Sk-5A 250-425 3.9 46.2 ± 1.5 46.6 ± 1.3 0.53 0.87 all Sk-6A 600-850 5.9 47.9 ± 0.9 47.7 ± 0.7 0.48 0.92 all Sk-6A 425-600 5.9 46.2 ± 1.1 47.8 ± 0.7 0.83 0.61 all Sk-6A 425-600 5.9 48.1 ± 0.6 48.4 ± 0.5 0.6 0.8 100 of 13 Sk-7A 300-425 6.1 45.3 ± 1.7 47 ± 5 2.72 0 all Sk-7A 300-425 6.1 48.2 ± 0.6 49.1 ± 0.6 1.74 0.07 10 of 13 Sk-7A 300-425 6.1 48.6 ± 0.9 <td>008 008 008</td> <td>300-425 250-425 250-425</td> <td>20.1 20.1 20.1</td> <td>83.1 ± 1.3 85.7 ± 1.1 90 ± 3</td> <td>83.8 ± 1.4 86.6 ± 1.3 92 ± 2</td> <td>1.68 0.51 2</td> <td>0.08 0.88 0.04</td> <td>11 of 12 10 of 13 10 of 12</td>	008 008 008	300-425 250-425 250-425	20.1 20.1 20.1	83.1 ± 1.3 85.7 ± 1.1 90 ± 3	83.8 ± 1.4 86.6 ± 1.3 92 ± 2	1.68 0.51 2	0.08 0.88 0.04	11 of 12 10 of 13 10 of 12
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Diotite St	ep neating re	Sulls					
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Sample	grain size (µm)	Distance from Quottoon Pluton (km)	Integrated age (Ma)	Plateau age (Ma)	MSWD	Р	# of steps in plateau
Sk-5A $425-850$ 3.9 47.7 ± 1.0 47.8 ± 0.8 0.21 1 1 all Sk-5A $250-425$ 3.9 46.2 ± 1.5 46.6 ± 1.3 0.53 0.87 all Sk-6A $600-850$ 5.9 46.2 ± 1.5 46.6 ± 1.3 0.53 0.87 all Sk-6A $600-850$ 5.9 47.9 ± 0.9 47.7 ± 0.7 0.48 0.92 all Sk-6A $425-600$ 5.9 48.2 ± 1.1 47.8 ± 0.7 0.83 0.61 all Sk-6A $300-425$ 5.9 48.1 ± 0.6 48.4 ± 0.5 0.6 0.8 $10 \text{ of } 13$ Sk-6A $250-300$ 5.9 48.1 ± 0.6 48.2 ± 0.5 1.68 0.08 $11 \text{ of } 13$ Sk-7A $300-425$ 6.1 45.3 ± 1.7 47 ± 5 2.72 0 all Sk-7A $300-425$ 6.1 48.2 ± 0.6 48.7 ± 0.5 1.44 0.16 $11 \text{ of } 13$ Sk-7A $300-425$ 6.1 48.2 ± 0.6 48.7 ± 0.5 1.44 0.16 $11 \text{ of } 13$ Sk-7A $300-425$ 6.3 48.6 ± 0.9 50.7 ± 0.9 0.81 0.6 $9 \text{ of } 13$ OO1 $600-850$ 6.8 52.2 ± 1.1 51.7 ± 0.9 0.81 0.6 $9 \text{ of } 13$ OO1 $600-850$ 6.8 52.2 ± 0.8 52.4 ± 0.8 0.66 0.58 $12 \text{ of } 13$ OO1 $425-600$ 6.8 51.5 ± 0.6 51.3 ± 1.0 2.46 0.66 $3 \text{ of } 11$ <td>Sk-5A</td> <td>425-850</td> <td>3.9</td> <td>47.1 ± 0.8</td> <td>47.2 ± 0.7</td> <td>0.64</td> <td>0.78</td> <td>all</td>	Sk-5A	425-850	3.9	47.1 ± 0.8	47.2 ± 0.7	0.64	0.78	all
Sk-6A200-4235.946.2 \pm 1.340.6 \pm 1.340.0 \pm 1.00.030.030.07allSk-6A600-8505.947.9 \pm 0.947.7 \pm 0.70.480.92allSk-6A425-6005.946 \pm 247.1 \pm 1.60.490.89allSk-6A425-6005.948.2 \pm 1.147.8 \pm 0.70.830.61allSk-6A425-6005.948.1 \pm 0.648.4 \pm 0.50.60.810 of 13Sk-6A250-3005.948.1 \pm 0.648.4 \pm 0.51.680.0811 of 13Sk-7A300-4256.145.3 \pm 1.747 \pm 52.720allSk-7A300-4256.150 \pm 248.8 \pm 1.60.230.99allSk-7A300-4256.148.2 \pm 0.648.7 \pm 0.51.440.1611 of 13Sk-7A300-4256.348.6 \pm 0.950.7 \pm 0.90.810.69 of 13OO1600-8506.850.1 \pm 1.650.2 \pm 1.30.211allOO1600-8506.850.1 \pm 1.650.2 \pm 1.30.211allOO1425-6006.850.1 \pm 1.650.2 \pm 1.30.211allOO1425-6006.852.2 \pm 0.852.4 \pm 0.80.660.5812 of 13OO1425-6006.853.1 \pm 0.753.1 \pm 0.60.570.93allOO1425-6006.853.	SK-5A	425-850	3.9	47.7 ± 1.0	47.8 ± 0.8	0.21		all
Sk-GA600-8505.947.9 \pm 0.947.7 \pm 0.70.480.92allSk-GA425-6005.946 \pm 247.1 \pm 1.60.490.89allSk-GA425-6005.948.2 \pm 1.147.8 \pm 0.70.830.61allSk-GA300-4255.948.1 \pm 0.648.4 \pm 0.50.60.810 of 13Sk-GA250-3005.948.1 \pm 0.648.2 \pm 0.51.680.0811 of 13Sk-7A300-4256.145.3 \pm 1.747 \pm 52.720allSk-7A300-4256.150 \pm 248.8 \pm 1.60.230.99allSk-7A300-4256.148.2 \pm 0.648.7 \pm 0.51.440.1611 of 13Sk-7A300-4256.348.6 ± 0.950.7 ± 0.90.810.69 of 13OO1600-8506.856.8 ± 1.058.1 ± 1.01.910.077 of 11OO1600-8506.850.1 ± 1.650.2 ± 1.30.211allOO1425-6006.852.2 ± 0.852.4 ± 0.80.860.5812 of 13OO1425-6006.851.5 ± 0.851.6 ± 0.80.730.7112 of 13OO1425-8506.852.2 ± 0.852.4 ± 0.50.670.93allOO1425-85010.656.5 ± 0.656.7 ± 0.51.40.17allSk-9A425-85010.655.5 ± 0.656.7 ± 0.51.40.17all<	Sk-6A	600-850	5.9	40.2 ± 1.3 46.5 ± 1.2	40.0 ± 1.3 47.3 ± 1.0	0.55	0.07	all
Sk-6A $425-600$ 5.9 46 ± 2 47.1 ± 1.6 0.49 0.89 allSk-6A $425-600$ 5.9 48.2 ± 1.1 47.8 ± 0.7 0.83 0.61 allSk-6A $300-425$ 5.9 48.1 ± 0.6 48.4 ± 0.5 0.6 0.8 $10 \text{ of } 13$ Sk-6A $250-300$ 5.9 48.1 ± 0.6 48.2 ± 0.5 1.68 0.08 $11 \text{ of } 13$ Sk-7A $300-425$ 6.1 45.3 ± 1.7 47 ± 5 2.72 0 allSk-7A $300-425$ 6.1 48.2 ± 0.6 48.7 ± 0.5 1.44 0.16 $11 \text{ of } 13$ Sk-7A $300-425$ 6.1 48.2 ± 0.6 48.7 ± 0.5 1.44 0.16 $11 \text{ of } 13$ Sk-7A $300-425$ 6.1 48.2 ± 0.6 49.1 ± 0.6 1.74 0.07 $10 \text{ of } 13$ Sk-7A $300-425$ 6.3 48.6 ± 0.9 50.7 ± 0.9 0.81 0.6 $9 \text{ of } 13$ OO1 $600-850$ 6.8 52 ± 1.1 51.7 ± 0.9 0.54 0.89 allOO1 $600-850$ 6.8 50.1 ± 1.6 51.3 ± 1.0 2.46 0.06 $3 \text{ of } 11$ OO1 $425-600$ 6.8 52.2 ± 0.8 52.4 ± 0.8 0.86 0.58 $12 \text{ of } 13$ OO1 $425-650$ 6.8 53.1 ± 0.7 53.1 ± 0.6 0.57 0.93 allOO1 $425-850$ 6.8 53.1 ± 0.7 53.1 ± 0.6 0.57 0.93 allOO1 $250-425$ 6.8 <td< td=""><td>Sk-6A</td><td>600-850</td><td>5.9</td><td>47.9 ± 0.9</td><td>47.7 ± 0.7</td><td>0.48</td><td>0.92</td><td>all</td></td<>	Sk-6A	600-850	5.9	47.9 ± 0.9	47.7 ± 0.7	0.48	0.92	all
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Sk-6A	425-600	5.9	46 ± 2	47.1 ± 1.6	0.49	0.89	all
Sk-6A $300-425$ 5.9 48.1 ± 0.6 48.4 ± 0.5 0.6 0.8 $10 \text{ of } 13$ Sk-6A $250-300$ 5.9 48.1 ± 0.6 48.2 ± 0.5 1.68 0.08 $11 \text{ of } 13$ Sk-7A $300-425$ 6.1 45.3 ± 1.7 47 ± 5 2.72 0 allSk-7A $300-425$ 6.1 50 ± 2 48.8 ± 1.6 0.23 0.99 allSk-7A $300-425$ 6.1 48.2 ± 0.6 48.7 ± 0.5 1.44 0.16 $11 \text{ of } 13$ Sk-7A $300-425$ 6.1 48.2 ± 0.6 49.1 ± 0.6 1.74 0.07 $10 \text{ of } 13$ Sk-7A $250-300$ 6.1 48.6 ± 0.9 50.7 ± 0.9 0.81 0.6 $9 \text{ of } 13$ OO1 $600-850$ 6.8 56.8 ± 1.0 58.1 ± 1.0 1.91 0.07 $7 \text{ of } 11$ OO1 $600-850$ 6.8 52 ± 1.1 51.7 ± 0.9 0.54 0.89 allOO1 $425-600$ 6.8 50.1 ± 1.6 50.2 ± 1.3 0.21 1 allOO1 $425-600$ 6.8 52.2 ± 0.8 52.4 ± 0.8 0.86 0.58 $12 \text{ of } 13$ OO1 $425-600$ 6.8 51.5 ± 0.8 51.6 ± 0.8 0.73 0.71 $12 \text{ of } 13$ OO1 $425-600$ 6.8 51.5 ± 0.8 52.4 ± 0.8 0.66 0.56 1.14 0.17 allOO1 $425-850$ 6.8 51.5 ± 0.6 50.7 ± 0.5 1.4 0.17 all<	Sk-6A	425-600	5.9	48.2 ± 1.1	47.8 ± 0.7	0.83	0.61	all
Sk-6A250-300 5.9 48.1 ± 0.6 48.2 ± 0.5 1.68 0.08 $11 \text{ of } 13$ Sk-7A $300-425$ 6.1 45.3 ± 1.7 47 ± 5 2.72 0 allSk-7A $300-425$ 6.1 50 ± 2 48.8 ± 1.6 0.23 0.99 allSk-7A $300-425$ 6.1 48.2 ± 0.6 48.7 ± 0.5 1.44 0.16 $11 \text{ of } 13$ Sk-7A $250-300$ 6.1 48.2 ± 0.6 49.1 ± 0.6 1.74 0.07 $10 \text{ of } 13$ Sk-8B $300-425$ 6.3 48.6 ± 0.9 50.7 ± 0.9 0.81 0.6 $9 \text{ of } 13$ OO1 $600-850$ 6.8 52 ± 1.1 51.7 ± 0.9 0.54 0.89 allOO1 $600-850$ 6.8 50.1 ± 1.6 50.2 ± 1.3 0.21 1 allOO1 $425-600$ 6.8 52.2 ± 0.8 52.4 ± 0.8 0.86 0.58 $12 \text{ of } 13$ OO1 $425-600$ 6.8 51.5 ± 0.8 51.6 ± 0.8 0.73 0.71 $12 \text{ of } 13$ OO1 $425-600$ 6.8 51.5 ± 0.8 52.4 ± 0.8 0.86 0.58 $12 \text{ of } 13$ OO1 $425-600$ 6.8 51.5 ± 0.8 52.4 ± 0.8 0.86 0.58 $12 \text{ of } 13$ OO1 $425-850$ 6.8 51.5 ± 0.6 51.3 ± 1.0 2.46 0.06 $3 \text{ of } 11$ OO1 $250-425$ 6.8 54.3 ± 1.5 54.3 ± 1.3 0.44 0.95 allSk-9A <t< td=""><td>Sk-6A</td><td>300-425</td><td>5.9</td><td>48.1 ± 0.6</td><td>48.4 ± 0.5</td><td>0.6</td><td>0.8</td><td>10 of 13</td></t<>	Sk-6A	300-425	5.9	48.1 ± 0.6	48.4 ± 0.5	0.6	0.8	10 of 13
Sk-7A $300-425$ 6.1 45.3 ± 1.7 47 ± 5 2.72 0 allSk-7A $300-425$ 6.1 50 ± 2 48.8 ± 1.6 0.23 0.99 allSk-7A $300-425$ 6.1 48.2 ± 0.6 48.7 ± 0.5 1.44 0.16 $11 \text{ of } 13$ Sk-7A $250-300$ 6.1 48 ± 0.6 49.1 ± 0.6 1.74 0.07 $10 \text{ of } 13$ Sk-8B $300-425$ 6.3 48.6 ± 0.9 50.7 ± 0.9 0.81 0.6 $9 \text{ of } 13$ OO1 $600-850$ 6.8 52 ± 1.1 51.7 ± 0.9 0.54 0.89 allOO1 $600-850$ 6.8 52 ± 1.1 51.7 ± 0.9 0.54 0.89 allOO1 $425-600$ 6.8 50.1 ± 1.6 50.2 ± 1.3 0.21 1 allOO1 $425-600$ 6.8 52.2 ± 0.8 52.4 ± 0.8 0.86 0.58 $12 \text{ of } 13$ OO1 $425-600$ 6.8 51.5 ± 0.8 51.6 ± 0.8 0.73 0.71 $12 \text{ of } 13$ OO1 $250-300$ 6.8 53.1 ± 0.7 53.1 ± 0.6 0.57 0.93 allOO1 $250-425$ 6.8 54.3 ± 1.5 54.3 ± 1.3 0.44 0.95 allSk-9A $425-850$ 10.6 55.5 ± 0.6 56.7 ± 0.5 1.4 0.17 allSk-9A $250-425$ 10.6 55.5 ± 0.6 55.9 ± 0.5 0.52 0.84 $9 \text{ of } 11$ Sk-9B $300-425$ 10.6	Sk-6A	250-300	5.9	48.1 ± 0.6	48.2 ± 0.5	1.68	0.08	11 of 13
Sk-7A $300-425$ 6.1 50 ± 2 48.8 ± 1.6 0.23 0.99 allSk-7A $300-425$ 6.1 48.2 ± 0.6 48.7 ± 0.5 1.44 0.16 11 of 13Sk-7A $250-300$ 6.1 48 ± 0.6 49.1 ± 0.6 1.74 0.07 10 of 13Sk-8B $300-425$ 6.3 48.6 ± 0.9 50.7 ± 0.9 0.81 0.6 9 of 13OO1 $600-850$ 6.8 56.8 ± 1.0 58.1 ± 1.0 1.91 0.07 7 of 11OO1 $600-850$ 6.8 52 ± 1.1 51.7 ± 0.9 0.54 0.89 allOO1 $425-600$ 6.8 50.1 ± 1.6 50.2 ± 1.3 0.21 1 allOO1 $425-600$ 6.8 52.2 ± 0.8 52.4 ± 0.8 0.66 3 of 11OO1 $300-425$ 6.8 51.5 ± 0.8 51.6 ± 0.8 0.73 0.71 12 of 13OO1 $250-300$ 6.8 53.1 ± 0.7 53.1 ± 0.6 0.57 0.93 allOO1 $250-425$ 6.8 54.3 ± 1.5 54.3 ± 1.3 0.44 0.95 allSk-9A $425-850$ 10.6 56.5 ± 0.6 56.7 ± 0.5 1.4 0.17 allSk-9A $250-425$ 10.6 55.5 ± 0.6 55.9 ± 0.5 0.52 0.84 9 of 11Sk-9B $300-425$ 10.6 55.5 ± 0.6 55.8 ± 0.5 1.51 0.15 9 of 11Sk-9B $600-850$ 10.6 58.2 ± 0.5 58	Sk-7A	300-425	6.1	45.3 ± 1.7	47 ± 5	2.72	0	all
Sk-7A $300-425$ 6.1 48.2 ± 0.6 48.7 ± 0.5 1.44 0.16 11.0113 Sk-7A $250-300$ 6.1 48 ± 0.6 49.1 ± 0.6 1.74 0.07 $10 of 13$ Sk-8B $300-425$ 6.3 48.6 ± 0.9 50.7 ± 0.9 0.81 0.6 $9 of 13$ OO1 $600-850$ 6.8 56.8 ± 1.0 58.1 ± 1.0 1.91 0.07 $7 of 11$ OO1 $600-850$ 6.8 52 ± 1.1 51.7 ± 0.9 0.54 0.89 allOO1 $425-600$ 6.8 52 ± 1.1 51.3 ± 1.0 2.46 0.06 $3 of 11$ OO1 $425-600$ 6.8 52.2 ± 0.8 52.4 ± 0.8 0.86 0.58 $12 of 13$ OO1 $425-600$ 6.8 51.5 ± 0.8 51.6 ± 0.8 0.73 0.71 $12 of 13$ OO1 $250-300$ 6.8 53.1 ± 0.7 53.1 ± 0.6 0.57 0.93 allOO1 $425-850$ 6.8 54.3 ± 1.5 54.3 ± 1.3 0.44 0.95 allOO1 $425-850$ 10.6 56.5 ± 0.6 56.7 ± 0.5 1.4 0.17 allSk-9A $425-850$ 10.6 55.5 ± 0.6 56.7 ± 0.5 0.67 0.75 allSk-9B $300-425$ 10.6 55.5 ± 0.6 55.9 ± 0.5 0.52 0.84 $9 of 11$ Sk-9B $600-850$ 10.6 58.3 ± 1.0 59.6 ± 0.8 1.64 0.13 $7 of 11$ Sk-9B $600-850$ 10.6 <td< td=""><td>SK-7A</td><td>300-425</td><td>6.1</td><td>50 ± 2</td><td>48.8 ± 1.6</td><td>0.23</td><td>0.99</td><td>all</td></td<>	SK-7A	300-425	6.1	50 ± 2	48.8 ± 1.6	0.23	0.99	all
Sk-7A250-3000.140 ± 0.043.1 ± 0.01.740.0710 of 13Sk-8B300-4256.348.6 ± 0.9 50.7 ± 0.9 0.810.69 of 13OO1600-8506.8 56.8 ± 1.0 58.1 ± 1.0 1.910.077 of 11OO1600-8506.8 52 ± 1.1 51.7 ± 0.9 0.540.89allOO1425-6006.8 52 ± 1.1 51.7 ± 0.9 0.540.89allOO1425-6006.8 $52.\pm 1.1$ 51.3 ± 1.0 2.460.063 of 11OO1300-4256.8 52.2 ± 0.8 52.4 ± 0.8 0.860.5812 of 13OO1250-3006.8 51.5 ± 0.8 51.6 ± 0.8 0.730.7112 of 13OO1425-8506.8 53.1 ± 0.7 53.1 ± 0.6 0.570.93allOO1250-4256.8 54.3 ± 1.5 54.3 ± 1.3 0.440.95allSk-9A425-85010.6 59.1 ± 0.6 59.2 ± 0.5 0.670.75allSk-9A250-42510.6 55.5 ± 0.6 55.9 ± 0.5 0.520.849 of 11Sk-9B300-42510.6 55.5 ± 0.6 55.8 ± 0.5 1.510.159 of 11Sk-9B600-85010.6 58.3 ± 1.0 59.6 ± 0.8 1.640.137 of 11Sk-9B600-85010.6 58.2 ± 0.5 58.3 ± 0.4 0.930.52allSk-9B600-85010.6 $58.2 \pm $	SK-7A Sk-7A	250-300	0.1	40.2 ± 0.0	40.7 ± 0.5	1.44	0.10	10 of 13
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Sk-8B	300-425	6.3	48.6 ± 0.0	50.7 ± 0.9	0.81	0.6	9 of 13
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	001	600-850	6.8	56.8 ± 1.0	58.1 ± 1.0	1.91	0.07	7 of 11
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	001	600-850	6.8	52 ± 1.1	51.7 ± 0.9	0.54	0.89	all
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	001	425-600	6.8	50.1 ± 1.6	50.2 ± 1.3	0.21	1	all
OO1 $300-425$ 6.8 52.2 ± 0.8 52.4 ± 0.8 0.86 0.58 $12 \text{ of } 13$ OO1 $250-300$ 6.8 51.5 ± 0.8 51.6 ± 0.8 0.73 0.71 $12 \text{ of } 13$ OO1 $425-850$ 6.8 53.1 ± 0.7 53.1 ± 0.6 0.57 0.93 allOO1 $250-425$ 6.8 54.3 ± 1.5 54.3 ± 1.3 0.44 0.95 allSk-9A $425-850$ 10.6 56.5 ± 0.6 56.7 ± 0.5 1.4 0.17 allSk-9A $425-850$ 10.6 59.1 ± 0.6 59.2 ± 0.5 0.67 0.75 allSk-9A $425-850$ 10.6 55 ± 1.3 55.1 ± 1.1 0.28 0.99 allSk-9A $250-425$ 10.6 55.5 ± 0.6 55.9 ± 0.5 0.52 0.84 $9 \text{ of } 11$ Sk-9B $300-425$ 10.6 55.5 ± 0.6 55.8 ± 0.5 1.51 0.15 $9 \text{ of } 11$ Sk-9B $600-850$ 10.6 58.3 ± 1.0 59.6 ± 0.8 1.64 0.13 $7 \text{ of } 11$ Sk-9B $600-850$ 10.6 58.2 ± 0.5 58.3 ± 0.4 0.93 0.52 allSk-9B $600-850$ 10.6 58.2 ± 0.5 58.3 ± 0.4 0.93 0.52 all	001	425-600	6.8	49.9 ± 1.6	51.3 ± 1.0	2.46	0.06	3 of 11
OO1 $250-300$ 6.8 51.5 ± 0.8 51.6 ± 0.8 0.73 0.71 $12 \text{ of } 13$ OO1 $425-850$ 6.8 53.1 ± 0.7 53.1 ± 0.6 0.57 0.93 allOO1 $250-425$ 6.8 54.3 ± 1.5 54.3 ± 1.3 0.44 0.95 allSk-9A $425-850$ 10.6 56.5 ± 0.6 56.7 ± 0.5 1.4 0.17 allSk-9A $425-850$ 10.6 59.1 ± 0.6 59.2 ± 0.5 0.67 0.75 allSk-9A $250-425$ 10.6 55 ± 1.3 55.1 ± 1.1 0.28 0.99 allSk-9B $300-425$ 10.6 55.5 ± 0.6 55.9 ± 0.5 0.52 0.84 $9 \text{ of } 11$ Sk-9B $250-300$ 10.6 55.5 ± 0.6 55.8 ± 0.5 1.51 0.15 $9 \text{ of } 11$ Sk-9B $600-850$ 10.6 58.3 ± 1.0 59.6 ± 0.8 1.64 0.13 $7 \text{ of } 11$ Sk-9B $600-850$ 10.6 58.2 ± 0.5 58.3 ± 0.4 0.93 0.52 allSk-9B $600-850$ 10.6 58.2 ± 0.5 58.3 ± 0.4 0.93 0.52 allSk-9B $600-850$ 10.6 58.2 ± 0.5 58.3 ± 0.4 0.93 0.52 all	001	300-425	6.8	52.2 ± 0.8	52.4 ± 0.8	0.86	0.58	12 of 13
$OO1$ $425-850$ 6.8 53.1 ± 0.7 53.1 ± 0.6 0.57 0.93 all $OO1$ $250-425$ 6.8 54.3 ± 1.5 54.3 ± 1.3 0.44 0.95 all $Sk-9A$ $425-850$ 10.6 56.5 ± 0.6 56.7 ± 0.5 1.4 0.17 all $Sk-9A$ $425-850$ 10.6 59.1 ± 0.6 59.2 ± 0.5 0.67 0.75 all $Sk-9A$ $250-425$ 10.6 55 ± 1.3 55.1 ± 1.1 0.28 0.99 all $Sk-9B$ $300-425$ 10.6 55.5 ± 0.6 55.9 ± 0.5 0.52 0.84 9 of 11 $Sk-9B$ $250-300$ 10.6 55.5 ± 0.6 55.8 ± 0.5 1.51 0.15 9 of 11 $Sk-9B$ $600-850$ 10.6 58.3 ± 1.0 59.6 ± 0.8 1.64 0.13 7 of 11 $Sk-9B$ $600-850$ 10.6 58.2 ± 0.5 58.3 ± 0.4 0.93 0.52 all $Sk-9B$ $600-850$ 10.6 58.6 ± 4.5 58.3 ± 0.4 0.93 0.52 all	001	250-300	6.8	51.5 ± 0.8	51.6 ± 0.8	0.73	0.71	12 of 13
OOT $230-425$ 6.6 54.3 ± 1.3 54.3 ± 1.3 0.44 0.95 an Sk-9A $425-850$ 10.6 56.5 ± 0.6 56.7 ± 0.5 1.4 0.17 all Sk-9A $425-850$ 10.6 59.1 ± 0.6 59.2 ± 0.5 0.67 0.75 all Sk-9A $250-425$ 10.6 55 ± 1.3 55.1 ± 1.1 0.28 0.99 all Sk-9B $300-425$ 10.6 55.5 ± 0.6 55.9 ± 0.5 0.52 0.84 9 of 11Sk-9B $250-300$ 10.6 55.5 ± 0.6 55.8 ± 0.5 1.51 0.15 9 of 11Sk-9B $600-850$ 10.6 58.3 ± 1.0 59.6 ± 0.8 1.64 0.13 7 of 11Sk-9B $600-850$ 10.6 58.2 ± 0.5 58.3 ± 0.4 0.93 0.52 all	001	425-850	6.8	53.1 ± 0.7	53.1 ± 0.6	0.57	0.93	all
Sk-9A425-85010.6 50.3 ± 0.6 50.7 ± 0.5 1.4 0.17 all Sk-9A425-85010.6 59.1 ± 0.6 59.2 ± 0.5 0.67 0.75 all Sk-9A250-42510.6 55 ± 1.3 55.1 ± 1.1 0.28 0.99 all Sk-9B300-42510.6 55.5 ± 0.6 55.9 ± 0.5 0.52 0.84 9 of 11Sk-9B250-30010.6 55.5 ± 0.6 55.8 ± 0.5 1.51 0.15 9 of 11Sk-9B600-85010.6 58.3 ± 1.0 59.6 ± 0.8 1.64 0.13 7 of 11Sk-9B600-85010.6 58.2 ± 0.5 58.3 ± 0.4 0.93 0.52 all	SKOA	200-420	0.0	54.3 ± 1.3	54.3 ± 1.3	0.44	0.95	all
Sk-9A250-42510.6 55 ± 1.3 55.1 ± 1.1 0.280.99allSk-9B300-42510.6 55.5 ± 0.6 55.9 ± 0.5 0.520.849 of 11Sk-9B250-30010.6 55.5 ± 0.6 55.8 ± 0.5 1.510.159 of 11Sk-9B600-85010.6 58.3 ± 1.0 59.6 ± 0.8 1.640.137 of 11Sk-9B600-85010.6 58.2 ± 0.5 58.3 ± 0.4 0.930.52all	Sk-9A	425-850	10.0	50.5 ± 0.0 59 1 + 0 6	50.7 ± 0.5 59 2 + 0 5	0.67	0.17	all
Sk-9B $300-425$ 10.6 55.5 ± 0.6 55.9 ± 0.5 0.52 0.84 $9 \text{ of } 11$ Sk-9B $250-300$ 10.6 55.5 ± 0.6 55.8 ± 0.5 1.51 0.15 $9 \text{ of } 11$ Sk-9B $600-850$ 10.6 58.3 ± 1.0 59.6 ± 0.8 1.64 0.13 $7 \text{ of } 11$ Sk-9B $600-850$ 10.6 58.2 ± 0.5 58.3 ± 0.4 0.93 0.52 allSk-9B $600-850$ 10.6 58.2 ± 0.5 58.3 ± 0.4 0.93 0.52 all	Sk-9A	250-425	10.6	55 ± 1.3	55.1 + 1.1	0.28	0.99	all
Sk-9B250-30010.6 55.5 ± 0.6 55.8 ± 0.5 1.510.159 of 11Sk-9B600-85010.6 58.3 ± 1.0 59.6 ± 0.8 1.640.137 of 11Sk-9B600-85010.6 58.2 ± 0.5 58.3 ± 0.4 0.930.52allSk-9B600-85010.6 58.6 ± 4.5 58.3 ± 0.4 0.930.52all	Sk-9B	300-425	10.6	55.5 ± 0.6	55.9 ± 0.5	0.52	0.84	9 of 11
Sk-9B 600-850 10.6 58.3 ± 1.0 59.6 ± 0.8 1.64 0.13 7 of 11 Sk-9B 600-850 10.6 58.2 ± 0.5 58.3 ± 0.4 0.93 0.52 all Sk-9B 600-850 10.6 58.2 ± 0.5 58.3 ± 0.4 0.93 0.52 all	Sk-9B	250-300	10.6	55.5 ± 0.6	55.8 ± 0.5	1.51	0.15	9 of 11
Sk-9B 600-850 10.6 58.2 ± 0.5 58.3 ± 0.4 0.93 0.52 all	Sk-9B	600-850	10.6	58.3 ± 1.0	59.6 ± 0.8	1.64	0.13	7 of 11
	Sk-9B	600-850	10.6	58.2 ± 0.5	58.3 ± 0.4	0.93	0.52	all

Biotite step heating results cont'd							
Sample	grain size (µm)	Distance from Quottoon Pluton (km)	Integrated age (Ma)	Plateau age (Ma)	MSWD	Ρ	# of steps in plateau
Sk-3A Sk-3A	300-425 250-300	13.4 13.4	64.5 ± 0.7 61.9 ± 0.9	67.4 ± 1.8 64.4 ± 0.8	2.36 0.61	0.02 0.75	8 of 11 8 of 11
Sk-3A	600-850	13.4	62 ± 0.8	62 ± 2	3.08	0.01	6 of 14
SK-JA	200 425	13.4	69.0 ± 1.0	00.1 ± 0.0 70.1 ± 1.4	1.40	0.2	0 01 11 8 of 11
Sk-2A Sk-2A	250-425	16.4	68.0 ± 1.1	70.1 ± 1.4 69.6 + 1.0	2.3	0.02	8 of 11
Sk-2A	600-850	16.4	70.0 ± 1.1	719 ± 7.0	3 79	0.54	6 of 11
Sk-2A	425-600	16.4	68.9 ± 1.1	69.3 + 1.1	1.03	0.41	9 of 11
Sk-1A	300-425	17.3	73.0 ± 1.1	74.3 ± 1.6	2.31	0.02	8 of 11
Sk-1A	250-300	17.3	73.5 ± 1.2	75.5 ± 1.2	0.22	0.98	8 of 11
Sk-1A	600-850	17.3	70.3 ± 1.1	70.3 ± 1.8	3.34	0	9 of 11
Sk-1A	600-850	17.3	75.2 ± 1.6	75.1 ± 1.4	0.24	0.99	all
Sk-1A	600-850	17.3	75.6 ± 1.6	75.8 ± 1.4	0.74	0.72	all
Sk-1A	425-600	17.3	75.0 ± 1.4	75.4 ± 1.3	1.22	0.27	all
Sk-1A	425-850	17.3	76.8 ± 0.9	77.2 ± 0.8	0.4	0.92	9 of 11
SK-1A	425-850	17.3	74.0 ± 0.8	74.3 ± 0.7	0.85	0.56	9 0f 11 9 of 11
008	200-420	20.1	70.0 ± 1.2 76.0 ± 1.2	12 ± 1.1 761 ± 1.2	0.23	0.96	0 UI II 2011
008	250-300	20.1	70.0 ± 1.2 75.8 + 1.2	70.1 ± 1.2 75 9 + 1 1	1.65	0.75	10 of 11
008	600-850	20.1	73.0 ± 1.2 73.8 + 1.4	73.6 ± 1.1	0.48	0.00	all
008	600-850	20.1	77.4 ± 1.2	77.3 ± 1.2	1.07	0.38	all
008	425-600	20.1	74.9 ± 1.4	75.8 ± 1.2	1.77	0.06	all
008	425-600	20.1	75.7 ± 1.7	76 ± 1.5	0.29	0.99	all
008	250-425	20.1	77.4 ± 1.5	77.2 ± 1.2	1.34	0.18	all
008	425-850	20.1	77.9 ± 1.2	78.0 ± 0.9	1.16	0.28	all
Biotite to	tal fusion res	sults					
	Grain	Distance from	Total fusion	Weighted			
Sample	size (um)	Quottoon	age (Ma)	mean (Ma)	MSV	/D	р
	0120 (µ111)	Pluton (km)	ugo (ma)	moun (ma)			
001	250-425	6.8	51.9 ± 0.4				
001	250-425	6.8	51.6 ± 0.4				
001	250-425	6.8	53 ± 0.7				
001	250-425	0.0	53.2 ± 0.7 52.2 ± 0.7				
001	250-425	6.8	52.2 ± 0.7 52.6 + 1.6	52 ± 1	2.2	1	0.02
001	250-425	6.8	52.0 ± 1.0 52.2 ± 0.5				
001	250-425	6.8	52.3 ± 0.4				
001	250-425	6.8	52.4 ± 0.5				
001	250-425	6.8	52.5 ± 0.4				
008	250-425	20.1	75 ± 0.6				
008	250-425	20.1	77.2 ± 0.7				
008	250-425	20.1	75.3 ± 0.6				
008	250-425	20.1	76.1 ± 0.6				
008	250-425	20.1	/6./±0.6	76.3 ± 1.6	5.1	2	0
008	250-425	20.1	10.3 ± 0.1 77 5 ± 0.5				
	200-420	∠0.1 20.1	77.3 ± 0.3 75.6 ± 0.5				
008	250-425	20.1	76.8 ± 0.5				
008	250-425	20.1	77.4 ± 0.6				
			Table 2.				



Brownlee and Renne, Figure 1





Brownlee and Renne, Figure 3



Brownlee and Renne, Figure 4

Biotite Age Spectra



Brownlee et al. Figure 5



Brownlee et al. Figure 6



Brownlee and Renne, Figure 7



Brownlee and Renne, Figure 8



Brownlee and Renne, Figure 9



Brownlee and Renne, Figure 10

