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Acoustic band engineering in terahertz quantum-cascade lasers and arbitrary superlattices

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We present theoretical methods for the analysis of acoustic phonon modes in superlattice structures, and terahertz-frequency quantum-cascade lasers (THz QCLs). Our generalised numerical solution of the acoustic-wave equation provides good agreement with experimental pump–probe measurements of the acoustic resonances in a THz QCL. We predict that the detailed layer structure in THz QCLs imprints up to ~ 2 GHz detuning of the acoustic mode spacing, which cannot be seen in analytical models. This effect is strongest in devices with large and abrupt acoustic mismatch between layers. We use an acoustic deformation potential within a density-matrix approach to analyse electron transport induced in a range of the most common THz QCLs active-region design schemes. We conclude that acoustic modes up to ~ 200 GHz are capable of significantly perturbing QCL transport, highlighting their potential for ultra-fast modulation of laser emission.

I. INTRODUCTION

Superlattices consist of periodic layer sequences of two or more materials. Acoustic waves (or phonons) within such structures are perturbed by the variation in acoustic impedance between the materials, causing their dispersion to differ from that of a bulk material. Furthermore, the periodicity of the structure folds the acoustic-wave dispersion into a Brillouin zone, [1, 2] characterised by a set of acoustic stopbands (or eigenmodes).

Vibrational dynamics in superlattices have been studied experimentally using Raman scattering techniques [2–6] and femtosecond pump–probe techniques, where typically longitudinal acoustic (LA) modes [7, 8] or (more recently) transverse modes (TA) [9, 10] have been explored. Recent investigations have also demonstrated the potential for acoustic waves in the ~ 100 GHz range to modulate electron transport and tunnelling [11–13].

Terahertz-frequency quantum-cascade lasers (THz QCLs) [14] are a specific case of interest, in which coherent THz photons are generated using electronic inter-subband transitions within a complex multilayered superlattice. The picosecond electronic lifetimes in THz QCLs potentially enable ultrafast light modulation [15] required for frequency comb generation [16], active mode locking [17], amplitude, frequency [18] and phase stabilisation [19]. THz QCLs thus show potential for applications in metrology [20], high resolution spectroscopy [21, 22] and ultra-fast wireless communications [23].

The most common THz QCL modulation techniques, however, are limited to relatively low bandwidths. For example, direct gain modulation through the applied voltage is, in practice, limited to $\lesssim 35$ GHz owing to parasitic inductance [24, 25]. Other approaches exploit the possibility of controlling effective cavity losses [26, 27], but are also limited owing to parasitic effects within the modulating elements.

In previous work [28], we explored the potential to overcome these limits through ultra-fast modulation of THz QCLs using bulk acoustic waves. Although acoustic phonons have a weaker effect than optical phonons on electron transport in THz QCLs, externally generated acoustic pulses can exploit the picosecond-scale dynamics of strain propagation through the device. However, the complex layer structure within a THz QCL active region perturbs the acoustic velocity across the superlattice structure. As such, it is inaccurate to consider the phonons as having bulk-like dispersion, or even that of a simple Kronig–Penney superlattice. There is also a range of different design schemes for THz QCLs, with varying electronic transport behaviour [29], and it is unclear which scheme most susceptible to acoustic modulation. It is therefore important to develop a detailed and accurate understanding of acoustic phonon dispersion within a QCL, and their effect on electron transport in order to explore and, ultimately, optimise this effect.

We have therefore developed an “envelope function”-like model to study acoustic phonon modes in *arbitrary* semiconductor heterostructures. Although transfer-matrix methods are widely used to find the eigenmodes of wavelike functions in simple structures with well-defined layers, they scale poorly to larger or more complex structures, and are unsuitable for systems with diffuse inter-

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faces. We therefore use a finite-difference discretisation scheme to analyse the acoustic modes in superlattices with arbitrary interface geometries. We couple the acoustic perturbation to the strain in a density-matrix model for electron transport in a THz QCL, and use this to analyse the strength of the acoustic modulation effect in a range of QCL design schemes.

In Section II, we present our theoretical model for acoustic phonon modes in arbitrary heterostructures and in Section III, we validate this against experimental pump-probe measurements of a THz QCL structure [28]. In Section IV, we use the model to simulate and analyse the acoustic phonon mode structure in three exemplar THz QCL active region designs, along with several superlattice structures with diffuse layer profiles. We demonstrate the advantages of using a finite-difference eigenvalue calculation compared with a more commonly used transfer-matrix approach [8]. We also demonstrate that the acoustic mode frequencies in THz QCLs are aperiodic, as a result of the complex multi-layer heterostructures used in their active regions. In Section V, we consider the effect of acoustic phonon modes on electron transport in THz QCLs by employing a density matrix transport model [30, 31]. We discuss prospects for acoustic modulation of THz emission from QCLs and predict the QCL design schemes that would be most susceptible to the effect.

II. ENVELOPE-FUNCTION MODEL OF ACOUSTIC PHONON MODES IN ARBITRARY HETEROSTRUCTURES

The starting point for our model is the acoustic wave equation [32]:

$$\frac{\partial}{\partial z} v_s^2(z) \frac{\partial}{\partial z} p(z, t) - \frac{\partial^2}{\partial t^2} p(z, t) = 0 \quad (1)$$

where the acoustic-wave pressure $p(z, t)$ depends on position z (in the growth direction) and time t . Here, $v_s(z)$ is acoustic velocity, which due to variation of heterostructure materials, has a z -dependent profile.

This equation can be solved using a variable separation method (Fourier method), closely resembling the envelope function approach, which is commonly employed for solving the Schrödinger equation. If we assume $p(z, t) = p_0 \psi(z) \exp(-i\omega t)$, where p_0 is the wave amplitude, ω is the angular frequency and $\psi(z)$ is the envelope of the acoustic wave, equation (1) folds into:

$$-\frac{\partial}{\partial z} v_s^2(z) \frac{\partial}{\partial z} \psi(z) = \omega^2 \psi(z) \quad (2)$$

Analytical solutions of Equation (2) are possible for an ideal acoustic cavity of length d , consisting of a homogeneous bulk medium with $v_s(z) = v_{\text{bulk}}$, surrounded by impenetrable reflective surfaces, such that $\psi(0) = \psi(d) = 0$. By assuming a plane-wave form of the normalised

acoustic wave function, $\psi(z) = \exp(iqz)$, standing-wave solutions to Equation (2) are found, with equidistant wave vectors, $q_n = n\pi/d$ and corresponding frequencies:

$$\omega_{\text{bulk},n} = \frac{n\pi v_{\text{bulk}}}{d} \quad (3)$$

where n is an integer representing phonon mode index.

For periodic superlattice structures, the phonon mode is no longer confined to specific wave vectors, For a period length d_{sl} , the normalized acoustic wave functions take a Bloch form, such that $\psi_q(z) = u_q(z) \exp(iqz)$. This consists of an envelope function, with the same periodicity as the superlattice, $u_q(z + d_{\text{sl}}) = u_q(z)$, multiplied by a plane-wave $\exp(iqz)$, with arbitrary wave vector q . The latter can be understood as a steady rotation in the complex plane, as the wave function extends across the length of the structure.

The periodic nature of the structure allows the phonon dispersion to be folded into the first Brillouin zone such that $|q| \leq q_B$, where $q_B = \pi/d_{\text{sl}}$. Two sets of symmetry points can be defined within this zone: Brillouin Zone Centre (BZC) modes with $q = 0$, and Brillouin Zone Edge (BZE) modes with $q = \pi/d_{\text{sl}}$, and represent cases where $\psi(z) = \pm \psi(z + d_{\text{sl}})$. It is important to note that the BZC and BZE wave vectors are identical to those for standing waves in an ideal cavity of length $d = d_{\text{sl}}$. Indeed, it is a fundamental result of the Bloch model that the eigenmodes of an isolated unit-cell of a periodic system provide a close approximation to the BZE and BZC solutions for a periodic structure [32]. It is, therefore, desirable to find a computationally efficient means of computing the single-period eigenmodes. There are some limitations to this single-period approach: only the BZC/BZE standing-wave solutions can be computed, and the width of the frequency stopband around these points cannot be determined. Although a more generalised periodic solver would be required to overcome these limitations, our approach allows rapid and direct computation of the solutions, and can be applied to arbitrary heterostructures including those with poorly-defined interfaces.

Eq. 2 can be discretised using a finite-difference approximation by defining samples of the wave-function and acoustic velocity at evenly-spaced points i along the z direction:

$$a_i \psi_{i-1} + b_i \psi_i + c_i \psi_{i+1} = \omega^2 \psi_i \quad (4)$$

where

$$a_i = -\frac{v_{i-1}^2 + v_i^2}{2\delta z^2} \quad (5)$$

$$b_i = \frac{v_{i-1}^2 + 2v_i^2 + v_{i+1}^2}{2\delta z^2} \quad (6)$$

$$c_i = -\frac{v_{i+1}^2 + v_i^2}{2\delta z^2} \quad (7)$$

The half-integer samples of squared velocity that typically arise in central finite differences [32], are taken as

the spatial-average of neighbouring points. It may now be solved by rewriting as a tridiagonal matrix equation:

$$\mathbf{H}\psi = \omega^2\psi \quad (8)$$

where

$$\mathbf{H} = \begin{pmatrix} b_1 & c_1 & 0 & \cdots & 0 \\ a_1 & b_2 & c_2 & \cdots & 0 \\ 0 & \ddots & \ddots & \ddots & 0 \\ \vdots & \cdots & a_{N-2} & b_{N-1} & c_{N-1} \\ 0 & \cdots & 0 & a_{N-1} & b_N \end{pmatrix} \quad (9)$$

The eigenvectors of the \mathbf{H} matrix give the envelopes of the acoustic wave $\psi(z)$ for each mode, and the corresponding eigenvalues give the square of the angular frequency ω .

This solution approach provides several advantages over commonly applied layer-by-layer transfer matrix methods [8]. All eigenvalues are computed simultaneously to machine precision, rather requiring a separate root-finding process for each mode. The numerical precision of the obtained eigenvalues can therefore be increased in a straightforward way by increasing the spatial mesh density. The most significant advantage, though, is that *arbitrary* heterostructure profiles may be considered, including diffuse structures, in which layers are not separated by abrupt interfaces, without any increase in computational expense.

Our model can thus be applied directly to complex periodic heterostructures such as GaAs/Al_xGa_{1-x}As THz QCL gain media (where typically $x = 0.1-0.3$). Although the acoustic velocity varies only by $\lesssim 5\%$ between the layers in typical structures, this represents a potentially very large margin of error for the design of high-precision radio-frequency modulators and transducers. As such, it is instructive to compare the numerical results of our model to analytical solutions for a bulk medium of identical length.

An improvement to the homogeneous-material model can be obtained by taking a reciprocal average of the ratios between the total length d_l and acoustic velocity v_l in each layer l of the structure [8]:

$$\omega_{\text{avg},n} = \frac{n\pi}{\sum_l \frac{d_l}{v_l}} \text{ or } \frac{1}{\omega_{\text{avg},n}} = \sum_l \frac{1}{\omega_l}, \quad \omega_l = \frac{n\pi v_l}{d_l} \quad (10)$$

$$\omega_{\text{avg},n} = n\pi \left(\frac{d_{\text{well}}}{v_{\text{well}}} + \frac{d_{\text{barrier}}}{v_{\text{barrier}}} \right)^{-1}$$

Here, ω_l can be interpreted as the resonant frequency of each isolated layer. The latter simplified expression denotes the most common case, in which the superlattice contains only two materials (i.e., alternating well and barrier layers). In this work, we have used $v_{\text{bulk}} = 4710 \text{ ms}^{-1}$, $v_{\text{AlAs}} = 5650 \text{ ms}^{-1}$, while the acoustic velocity in an arbitrary Al_xGa_{1-x}As barrier alloy was evaluated through linear interpolation as $v_{\text{barrier}} = v_{\text{bulk}} + x \cdot (v_{\text{AlAs}} - v_{\text{bulk}}) \text{ ms}^{-1}$.

Equations (3) and (10) provide simple approximations to the exact solution of Equation (2), in which the spatial variation of acoustic velocity is ignored. We define the frequency deviations of these approximate solutions from the exact numerical values f_n as:

$$\Delta f_{\text{bulk},n} = f_n - \frac{nv_{\text{bulk}}}{2d_{\text{sl}}} \quad (11)$$

$$\Delta f_{\text{avg},n} = f_n - \frac{n}{2\sum_l \frac{d_l}{v_l}}$$

These deviations allow us to determine the extent to which the detailed superlattice layer structure affects the phonon modes, and investigate the prospect of phononic bandstructure engineering. It is important to note that the model in Eq. (2) implicitly assumes linear dispersion of the acoustic phonon branch, which may not be valid for modes with high index n , unless a frequency dependent correction is introduced in v_s . Experimental work [10] typically reports modes up to 1 THz, with higher modes lost to dispersion. For this reason, we will limit analysis to the first 100 modes since this accounts for frequencies up to 1 THz for most cases of interest in the following sections.

III. PUMP-PROBE CHARACTERIZATION OF 2.8-THZ QCL GAIN MEDIA

To validate our arbitrary-heterostructure model, we compare its predictions with experimental measurements of phonon modes in a complex THz QCL heterostructure we have previously used for time-domain acoustic modulation studies [28]. This QCL comprises 88 periods of a GaAs/Al_{0.14}Ga_{0.86}As nine-well ‘hybrid’ bandstructure design and lasers around 2.8 THz [33]. The 13.9- μm -thick QCL active region was grown using molecular-beam epitaxy on a 150- μm -thick semi-insulating GaAs substrate, as described in [28].

Here, we present experimental measurements of the phonon modes in the QCL gain media using asynchronous optical sampling (ASOPS) femtosecond optical pump-probe techniques. An unprocessed sample of the same epitaxially-grown wafer as in [28] was used in this study (i.e., without a ridge-waveguide or electrical contact deposition). A 50-nm-thick aluminium film was deposited on the bottom surface of a section of semiconductor wafer (the substrate), to act as an acoustic transducer.

Two ASOPS measurement schemes, shown in Figure 1, were used. In each of these, a femtosecond pump laser is used to generate acoustic waves within the semiconductor sample. A delayed probe-laser pulse is then used to measure small changes over time in the reflectivity of the sample surface, $\Delta R/R$, resulting from the strain wave propagating through the sample. The Fourier transform of the resulting temporal trace then gives the spectrum of phonon modes.

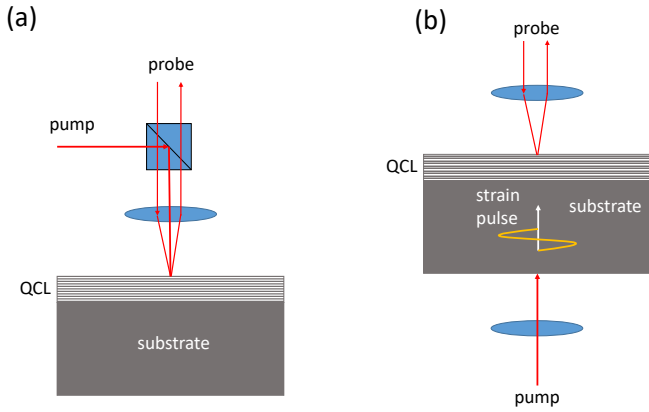


FIG. 1. Schematic illustrations of ASOPS experimental configurations, showing (a) reflection mode, and (b) transmission mode geometries.

In the scheme in Fig. 1(a), the top of the epitaxial QCL active region stack was pumped directly with $\lambda = 810$ nm pulses with a fluence of 0.6 mJ cm^{-2} , and with the sample at room temperature. It was probed on the same surface with $\lambda = 810$ nm pulses with a fluence of $20 \mu\text{J cm}^{-2}$. In this configuration, absorption of the pump light excites coherent phonons with wave vectors corresponding to the periodicity of the QCL structure (*i.e.*, the $q = 0$ modes in the folded dispersion). These modes do not strictly satisfy the selection rules for detection by the probe laser (*i.e.* $q = 2k_L$, where k_L is the photon wave vector of the optical probe). However, due to the finite absorption length of the probe light in the structure and the bandwidth of the laser pulses, the excited $q = 0$ modes become observable in this scheme [34].

The top panel in Fig. 2 shows the experimental reflectivity spectrum obtained, using an offset of 800 Hz between the pump and probe laser repetition rates. This provided measurements of the wafer reflectivity at intervals of 640 fs, over a total 1282 ns sampling window, giving a spectral resolution of 780 MHz. Phonon modes are observed in the resulting spectrum at 35 GHz, 42 GHz, and 69 GHz.

For comparison, the bottom panel shows the approximate folded dispersion relation, which was calculated using the BZC and BZE modes obtained by solving Eq. (2) for a single period of the QCL structure. The calculated modes (to 3 s.f. precision) were 17.4, **34.7**, 52.1, **69.5**, 86.8, **104**, 121, **139**, 156, **174** and 191 GHz, where only the BZC modes (highlighted in bold) are detectable in this scheme. The pink arrows in Fig. 2 are therefore identifiable (to within 1 GHz) as the first two BZC modes of the heterostructure. The orange arrow in Fig. 2 indicates a mode at 42 GHz, which does not correspond to any calculated BZE/BZC modes of the heterostructure. Instead, this is identifiable as a result of Brillouin scattering, *i.e.* interference between reflections of the probe pulse from the surface and from a strain pulse within the sample, with a frequency given by $2nv_s/\lambda = 42$ GHz,

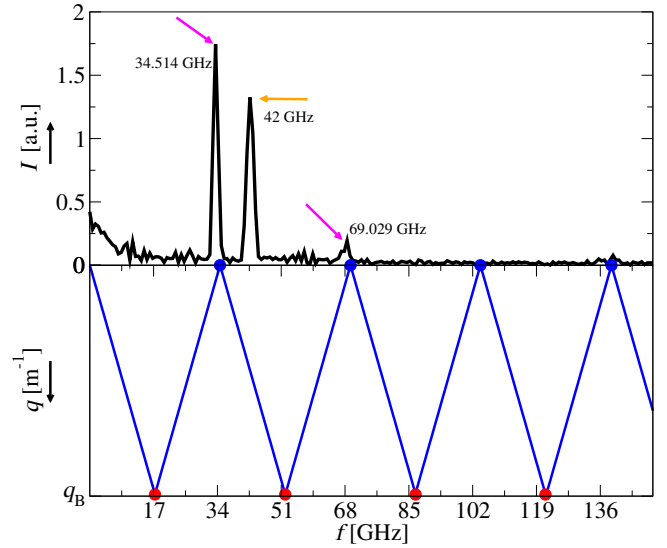


FIG. 2. Experimental probe reflectivity spectrum (top), obtained using a reflection-mode ASOPS geometry, and folded dispersion of the first Brillouin zone (bottom), obtained by solving Eq. (2) for a single period of the QCL. Blue and red circles indicate BZC and BZE modes respectively.

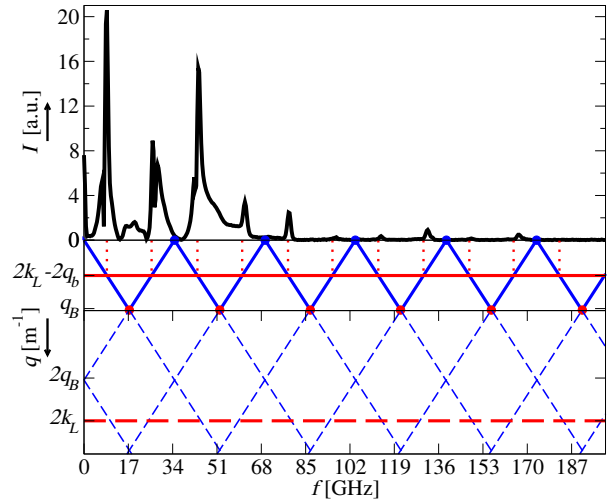


FIG. 3. Experimental probe reflectivity spectrum (top), using the configuration in Fig. 1(b), and acoustic dispersion resulting from model in Equation (2). Solid blue lines represent the phonon dispersion, folded into the first Brillouin zone, while dashed lines represent the extended dispersion at higher phonon wave vectors. The red dashed line corresponds to $q = 2k_L$, and the red solid line shows this folded into the first phonon Brillouin zone.

where $n = 3.68$ is the refractive index of the medium.

In the second scheme, shown in Fig. 1(b), the QCL structure was pumped indirectly, using broadband picosecond-duration acoustic strain pulses. These were generated by absorbing a $\lambda = 800$ nm pulse in a ~ 50 -nm-thick Al film on the opposite side of the GaAs substrate to which the QCL structure was grown. The sample was

cooled in a helium cryostat to 10K, so that the substrate was transparent to the high-frequency phonons in the pulse. The strain pulses are bipolar in form with approximately 20 ps duration, and the corresponding broad-bandwidth phonon spectrum is peaked at about 50 GHz [35]. When the strain pulse enters the QCL structure, it is able to excite *any* phonon mode within the bandwidth of the pulse (*i.e.*, not only the $q = 0$ modes).

As in the first scheme, the phonons in the QCL structure were detected through changes in the reflected probe intensity. In this case, however, phonon modes that satisfy the selection rule, $q = 2k_L = 4\pi n/\lambda$, are detected by the probe, and are the most prominent in the measured spectrum. For this reason, the probe wavelength $\lambda = 810$ nm influences the detected mode frequencies. Since the probe wavevector lies outside the first acoustic Brillouin zone ($2k_L > q_B$), the selection rule may be folded into the zone such that $q = 2k_L - 2q_B$, which is graphically illustrated by horizontal red lines in Fig. 3. The modes that are detected by this scheme thus correspond to intersections between the acoustic dispersion $q(f)$ and the red line at $2k_L - 2q_B$. As our model detects the BZC/BZE modes of the superlattice, the simplest approximation for the dispersion relation is $q(f) = 2\pi|f - f_{2n}|/v_{\text{bulk}}$ where f_{2n} correspond to the BZC modes, depicted by blue circles in Fig. 3.

$$f = f_{2n} \pm \left(\frac{v_{\text{bulk}} n_{\text{ref}}}{\lambda} - \frac{v_{\text{bulk}}}{d_{\text{sl}}} \right) \quad (12)$$

For the measurement in Fig. 3, the intersection points corresponding to Eq. (12) are $f = f_{2n} \pm 8.79$ [GHz]. This yields predicted spectral peaks at 8.79, 25.9, 43.5, 60.7, 78.2, 95.3, 113 etc. The experimental data peaks in Fig. 3 are found at 9, 26, 44, 62, 79, 97, 114 etc, in good agreement with the theoretical predictions. The accurate prediction of acoustic eigenmodes in this structure gives confidence in the use of the model to analyze and predict such effects a wider range of heterostructures in the following sections.

We note that further improvement between predicted and measured peaks could be made in Eq. (12). The acoustic velocity for each even eigenmode can be evaluated better by using the eigenvector solutions of Eq. (2) as the orthonormal basis, in order to calculate the probable acoustic velocity of each mode as the expectation value $v_n = \langle \psi_n | v(z) | \psi_n \rangle$. Similarly, the refractive index of $n_{\text{ref}} = 3.68$ corresponds to the bulk value of GaAs, if weighted average is taken, depending on the content of AlAs in the period, $n_{\text{ref}} = 3.64$ which changes Eq. (12) to predict sidebands around even modes as $f = f_{2n} \pm 8.33$ [GHz], we could also calculate refractive index expectation value for each stopband as $n_{\text{ref}} = \langle \psi_n | n_{\text{ref}}(z) | \psi_n \rangle$. In [10] the authors accounted for the mismatch between measurement and theory by assuming fitting nominal layer thickness growth variation of $\sim 3\%$, however we note that numerical solutions of Eq. (2) provide significant precision improvement than the bulk approximation for

BZE and BZC modes. Detected data in Fig. 3 has finite bandwidth around each detected modes, where signal even has contributions around $q = q_B$ (the odd stopbands) which occur due to complex phonon-photon interactions and material fluctuations that are not considered in our model.

IV. ACOUSTIC BANDSTRUCTURE ENGINEERING

As the acoustic velocity mismatch is relatively small in practical GaAs/AlGaAs heterostructures, the BZE/BZC modes are approximately evenly spaced, as expected from Eq. (3). However, the heterostructure layer composition introduces some deviation from these approximate solutions, which could potentially allow more precise design of acoustic bandstructure. We predict that this deviation would be enhanced in heterostructures with greater variation of acoustic velocity between layers, for example, in superlattices with a greater Al content in the barrier alloy. In this section, we explore this deviation for a range of superlattice structures, and discuss the prospects for bandstructure engineering.

A. THz QCL gain media

The resonant acoustic modes are approximately equidistant both numerically and experimentally for the ‘hybrid’ THz QCL structure we considered in the previous section. QCL design schemes can, however, differ considerably in terms of period length, and barrier alloy composition, which are key parameters in Eq. (10). We will therefore consider four exemplar THz QCL structures with considerable variation in their layer composition, which are detailed in the Appendix:

- Device A: the hybrid QCL design discussed in the previous section, which employs a nine-well GaAs/Al_{0.14}Ga_{0.86}As heterostructure, of total 1362 Å period length [28].
- Device B: an LO-phonon depopulated design [10], which employs a three-well GaAs/Al_{0.15}Ga_{0.85}As design, of total 643 Å period length.
- Device C: a bound-to-continuum (BTC) design [30], which employs an eight well GaAs/Al_{0.1}Ga_{0.9}As heterostructure, of total 1150 Å period length.
- Device D: an LO-phonon depopulated design with very high Al content in the barrier alloy [36], which employs a two-well, GaAs/Al_{0.3}Ga_{0.7}As design, of total 269.3 Å period length.

The inset in Fig. 4 shows the deviation between consecutive modes in each of these structures, as obtained from

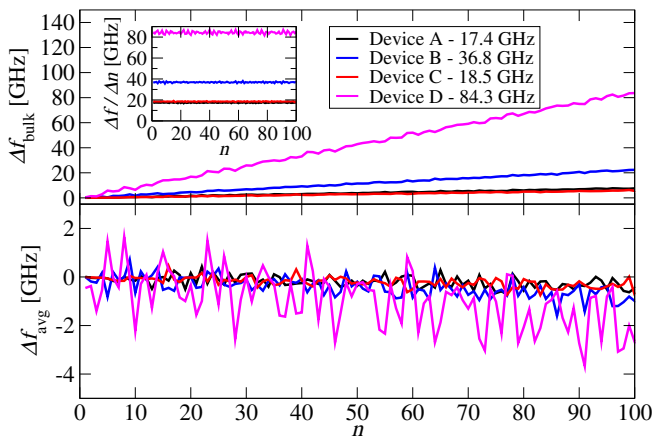


FIG. 4. Frequency offset from the bulk (top) and average (bottom) approximation calculated by Eq. (11) for QCL devices A–D. Inset: the frequency difference between consecutive resonant acoustic modes for the corresponding structures.

solving Eq. (2) numerically. The results for Devices A and B are in good agreement with the mode spacing seen experimentally in Section III and in Ref. [10] respectively.

The top and bottom panels of the figure show the deviation between the exact numerical solution of Eq. (2) and the approximations for homogeneous media, as given in Eq. (11). The deviation from the homogeneous model is greatest for Device D, and smallest for Device C, owing to the large acoustic-velocity mismatch between layers in the heterostructure. Device D also exhibits a periodic ($\Delta n \approx 10$) variation in the deviation from the analytical solutions, which we will separately examine later. In each case, the deviation from Eq. (3) increases approximately linearly with respect to mode index, and is largest for Device D. However, the deviation from Eq. (10) remains approximately centred around zero for all mode indices. We can conclude that the bulk approximation in Eq. (3) underestimates the effective velocity of acoustic modes in a realistic heterostructure, and creates significantly larger offsets than the average-velocity approximation in Eq. (10) whose estimation provides < 2 GHz mismatch from numerical values even for structures with high barriers.

B. Superlattices with non-uniform layer profiles

One of the main advantages of the model in Eq. (2) is its ability to model arbitrary heterostructure profiles, such as those with poorly-defined interfaces arising from interdiffusion or surface-segregation of alloy components during epitaxial growth. We therefore consider three exemplar superlattice structures with non-uniform layer compositions, and analyse their mode structure:

- Device E: A step-barrier LO-phonon depopulated THz QCL [37], that employs a three-well design with two different barrier heights in its period ($x =$

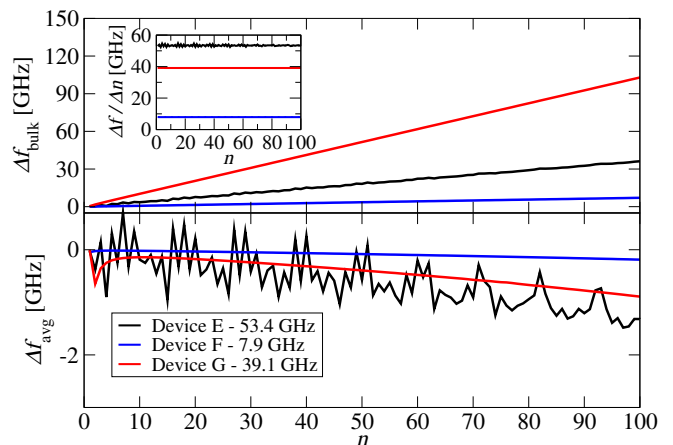


FIG. 5. Frequency offset from the bulk (top) and average (bottom) approximation calculated by Eq. (11) for variable barrier height LO phonon THz QCL structure [37] (Device E), a parabolic quantum well superlattice (Device F) that quadratically varies Al content $x = 0 - 0.14$ across 3000 Å period length and a parabolic quantum well (Device G) with varying Al content $x = 0 - 0.42$ across 620 Å well length. We used a mono-layer step of 2.825 Å for generating the parabolic profiles. Inset: the frequency difference between consecutive resonant acoustic modes for the corresponding structures.

0.15 and $x = 0.075$) and has 444 Å period length.

- Device F: A wide parabolic quantum well GaAs/Al_cGa_{1-x}As superlattice [38] that varies $x = 0 - 0.14$ across 3000 Å period length.
- Device G: A narrow parabolic quantum well GaAs/Al_xGa_{1-x}As superlattice [39] that varies $x = 0 - 0.42$ across 620 Å period length.

Layer composition and functions that generate parabolic profiles can be found in the Appendix.

In Fig. 5 we present the results of our calculations on these structures. Device E is structurally similar to the THz QCL structures analysed in Fig. 4, however it displays a more pronounced noise-like variation between consecutive modes in Fig. 5, even though its highest barrier is $x = 0.15$ and we expected similar behaviour to Device B. It is likely that the additional perturbation in the heterostructure profile generates different resonance effects. By contrast, the parabolic quantum well potentials in Fig. 5 are very well described by the average frequency formula in Eq. (10). This indicates that the fine structure of the acoustic dispersion is a result of interface mismatch within the heterostructure, and this is effectively damped by the use of diffuse interface geometry. The deviation is also larger in structures where there is a larger mismatch in barrier height. This may be of significant importance in material systems where there is a large mismatch between acoustic velocities in well and barrier material, or where the acoustic velocities are larger than in GaAs, which can also apply in mid-infrared QCL designs.

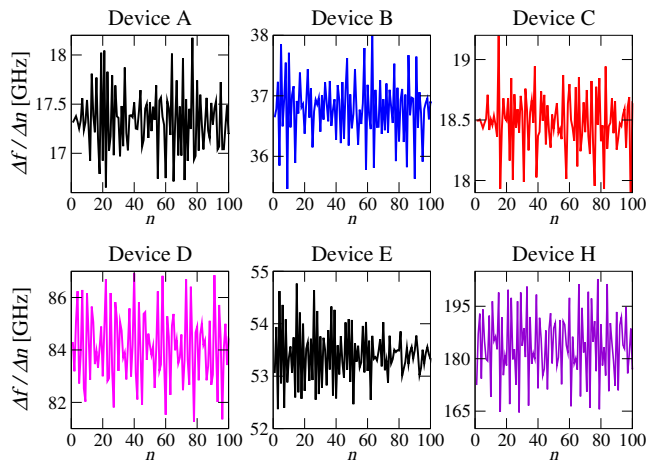


FIG. 6. The frequency difference between consecutive resonant acoustic modes for the corresponding structures analysed in this section.

C. High precision frequency control

Our experimental and theoretical analysis in the previous sections has shown that the spacings between consecutive BZE and BZC modes in arbitrary superlattices are determined by two factors. First, the *average* spacing between modes is given to a reasonable level of accuracy by Eq. (10). This is determined solely by the length of the heterostructure period, and its average alloy composition. In other words, this “coarse” tuning of the acoustic dispersion results from the periodicity of the superlattice. The second, fine-tuning component results from the detailed layer structure of the superlattice, and is most prominent in systems with a large, and abrupt mismatch between the acoustic velocity in each layer. To confirm that this effect is not caused by numerical error, we used 20,000 spatial points for solving the eigenvalue problem in Eq. (2), and performed an error convergence check. In some cases, this fine-tuning component exhibits a periodicity, which we investigate further in this section, through simulation of the previous QCL devices (A–E). We have included an additional two-well GaAs/AlAs superlattice structure [8], denoted ‘Device H’ here, for which TA phonon spectra have previously been analysed experimentally. For this TA-branch dispersion, $v_{\text{GaAs}} = 3329 \text{ ms}^{-1}$ and $v_{\text{AlAs}} = 3957 \text{ ms}^{-1}$ were assumed.

Fig. 6 shows the calculated BZE/BZC modes for each of these devices. We observe that Devices B, C and H do not exhibit a well-defined periodicity, Device D has a clear periodic envelope every 18 modes, Device E has an attenuating envelope every ~ 11 modes and Device A has a weakly-defined envelope every ~ 44 modes. We hypothesise that the observed periodicity is a consequence of an intra-period resonance of the acoustic wave with a layer within the superlattice. This is most likely to occur within an AlGaAs barrier layer, as the acoustic velocity is higher than in the well layers, meaning the modes

are more likely to be confined in the barriers. For an observed period Δn in Fig. 6, we can estimate the suspected barrier layer width by assuming modes are equidistant through average approximation in Eq. (10) and apply the bulk-confinement approximation for that layer:

$$L_n \approx \frac{\Delta n \pi v_{\text{barrier}}}{\omega_{\text{avg}}} \quad (13)$$

Interestingly, Eq. (13) is in good agreement with observations made in Fig. 6 as it provides layer width equal to one of the dominant barriers in the corresponding designs.

- Device D has a very clear $\Delta n \approx 18$ envelope and $L_{18} = 16.44 \text{ \AA}$, which is close to the 17.5 \AA barrier width within this structure.
- Device E has an attenuating envelope with $\Delta n \approx 11$ envelope, and $L_{18} = 41.21 \text{ \AA}$, which is related to one of the three barriers of this structure ($41, 43$ and 46 \AA).
- Device H exhibits a Fourier Transform peak at $\Delta n \approx 6$, and $L_6 = 18.65 \text{ \AA}$, which corresponds to the only two 17 \AA barriers within the structure.
- Device A has a weak $\Delta n \approx 44$ period, and $L_{44} = 31.66 \text{ \AA}$, which corresponds to multiple 31 \AA , barriers within the structure.

The amplitude of variations in Fig. 6 can directly be affected by increasing barrier height and therefore the acoustic velocity in the barriers. In order to confirm our estimate in Eq. (13), we alter the layer structure of studied devices as follows (layer composition is presented in the Appendix):

- Device D₁: we double the thickness of the 17.5 \AA barrier in Device D to confirm that the period of oscillations halves.
- Device C₁: we make the 24 \AA barrier the largest in Device C by replacing its material with pure AlAs ($x = 1$).
- Device C₂: we set two very tall $x = 1$ barriers in Device C, a 24 \AA layer as in C₁ and a 30 \AA layer to study the effect of having two dominant barriers in the design.
- Device I: we consider a GaAs/AlAs heterostructure with three 150 \AA wells separated by barriers of $20, 40$ and 80 \AA . If the periodicity of the confinement is caused by the barrier layers, this will create an ideal periodicity matching condition.
- Device J: we consider a heterostructure with two sets of identical wells and fixed barrier width as shown in the Appendix. This should create a perfectly periodic structure that is independent of the barrier height. To confirm this, we use $x = 0.1$ in the barrier material.

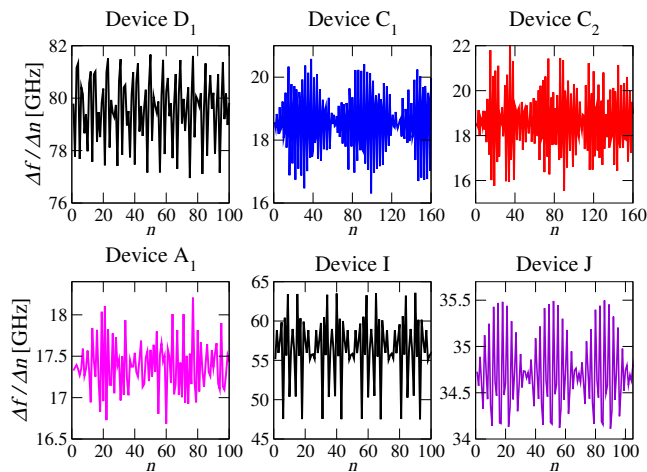


FIG. 7. The frequency difference between consecutive resonant acoustic modes for altered structures that test validity of approximation created by Eq. (13)

The results, shown in in Fig. 7, agree with our approximation in Eq. (13). Doubling the barrier width of Device D reduced the periodicity to $\Delta n \approx 9$ in Device D₁, which corresponds to $L_9^{D_1} = 34.82$ Å. Setting the 24 Å barrier in Device C to $x = 1$ has fully confined consecutive mode dependence for Device C₁, yielding $L_{60}^{C_1} = 24.65$ Å. However, setting two very high barriers in C₂ results in a more complex mode structure, and the Fourier transform of the data reveals peaks that correspond to $L_{60}^{C_2} = 24.65$ Å and $L_{46}^{C_2} = 32.15$ Å, in excellent agreement with the barriers whose heights were increased. This result provides us with a fundamental understanding that the complex mode structure in Fig. 6 is consequence of mixed contribution to the period due to different barrier widths. We have observed clear periodicity in Fig. 6 for Device D because it has two barriers in approximately 1:2 ratio, Device E had several layers of ~ 42 Å width and similarly, Device A has multiple 31 Å barrier layers. We also note that a high barrier is not required to generate periodicity; any barrier that is purposely dominant would impose its effect. In Device A₁, we purposely set the injection 41 Å barrier to $x = 0.3$ and this has generated the confinement in Fig. 7 that corresponds to $L_{34}^{A_1} = 42.03$ Å. The Fourier transformation of data corresponding to Device A₁ also shows a peak that corresponds to $L_{43}^{A_1} = 33.23$ Å, which is understandable as this device has five 31 Å barriers in its layer sequence (more information can be found in the Appendix).

If wells have equal width, and all barriers widths are in 1:2 ratio as in Device I, we expect to obtain perfect periodicity. This can be observed in in Fig. 7 where the periodicity corresponds to the layer width $L_{24}^I = 20.68$ Å, and the Fourier transform shows peaks also with 12 and 6 mode period due to the symmetry of the device. If all barriers have equal width, perfect periodicity is attainable even when there is no significant difference in acous-

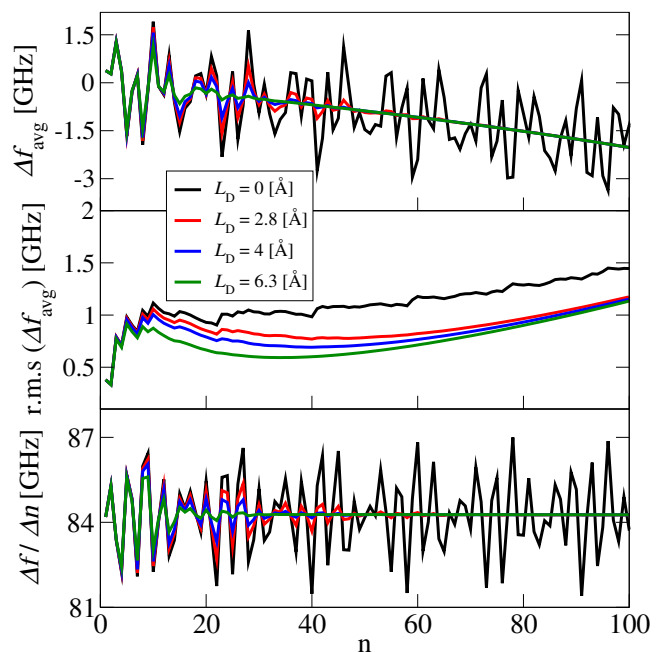


FIG. 8. We analyse Structure D for several values of diffusion length using the annealing model in [40]. Top and middle: Frequency offset from the average approximation [Eq. (11)] and its cumulative root mean square average, respectively. Bottom: The frequency difference between consecutive resonant modes.

tic velocity in wells and barriers as is the case in Device J. The two well widths affect the phase of the observed oscillation, while the 20 Å barrier causes confinement every 34 modes, which corresponds to $L_{34}^J = 20.35$ Å when applying the approximation in Eq. (13).

We note that the lack of periodicity in the parabolic superlattices in Devices F and G can be understood by Eq. (13) as well. The parabolic profiles of these devices were generated on a spatial resolution of monolayer thickness in GaAs, 2.825 Å, and thus, regardless of the acoustic velocity that would correspond to each spatial segment, the resulting period in consecutive mode profile would be too large to be observed. There is also no dominant barrier layer, as these devices have a diffuse distribution of Al content in their layer sequence. This also raises an interesting effect with imperfect growth and tolerance. The rectangular heterostructure profiles in superlattice material systems may in reality undergo interdiffusion process that result in diffuse profiles for the superlattice interfaces. These effects are estimated to have up to 15 Å diffusion lengths [40–44]. In Fig. 8 we model growth tolerances in structure D using an annealing approach [40] by assuming constant diffusion profile across the superlattice. We find that observed periodicity in Fig. 7 vanishes for modes with higher index and larger diffusion lengths. This also results in smoother dependence of the frequency offset from the average approximation (Eq. (11)) resulting in smaller r.m.s average.

The effect in Fig. 7 can be controlled and manipu-

lated through superlattice design, and this observation opens multiple engineering opportunities. Furthermore, the observed periodicity cannot be seen in the approximate approaches in Eqs. (3) and (10) and only the numerical consideration of Eq. (2) can explain the effect. The fine-tuning control of frequency is a fundamental trait in optical devices, thus the ability to perform analogous control of different acoustic resonant frequencies through superlattice design could find an important use in phononic applications. Conversely, our analysis shows that the thickness of layers within a superlattice could be inferred through precise measurements of the acoustic mode spacing, in analogy with X -ray diffraction measurements of crystalline solids.

V. TRANSPORT EFFECTS

In our previous work [28], we showed that optically-generated picosecond acoustic (strain) pulses propagating along the growth direction of a QCL, alter the band-structure potential sequentially and perturb the resonant tunneling between adjacent QCL periods. Here, we will examine the potential THz QCL transport effects that could be induced by *resonant* (non-propagating) acoustic phonon modes.

The transport in THz QCLs requires the use of models that include coherent effects, such as Non-Equilibrium Green Function (NEGF) [45–47], or density matrix (DM) approaches [30, 31, 48–50] or the Wigner function formalism [51]. The NEGF approaches provide highly detailed results at a high numerical cost, whereas the DM approaches offer comparable outputs [48] with high numerical efficiency. The DM models deviate from NEGF simulations when high electric field bias is applied, making them less suitable for modelling mid-infrared QCLs, however they are ideal for device optimisation of THz QCL structures [29].

As such, we employ a density-matrix model [30, 31] for calculation of electron transport in arbitrary THz QCLs. This model uses a tight-binding approximation for electronic structure calculation, which is then extended to an infinite period consideration of the QCL within the first-neighbor approximation. In the transport model, we treat various non-radiative interactions of electrons with alloy disorder (AD), longitudinal optical (LO) phonons, acoustic (AC) phonons, ionised impurities (II), interface roughness (IFR) and other electrons (EE).

To model the resonant acoustic effect, we add a static deformation potential $V_{S_n}(z)$ to the Hamiltonian for an electron in the QCL, which we assume to be directly proportional to the envelope of the local acoustic strain, $p_n(z)$. The BZE and BZC solutions of Eq. (2) provide standing-wave-like resonant modes with envelopes $p_n(z)$, giving:

$$V_{S_n}(z) = M \cdot p_n(z) \quad (14)$$

where M is a modulation strength constant. For the

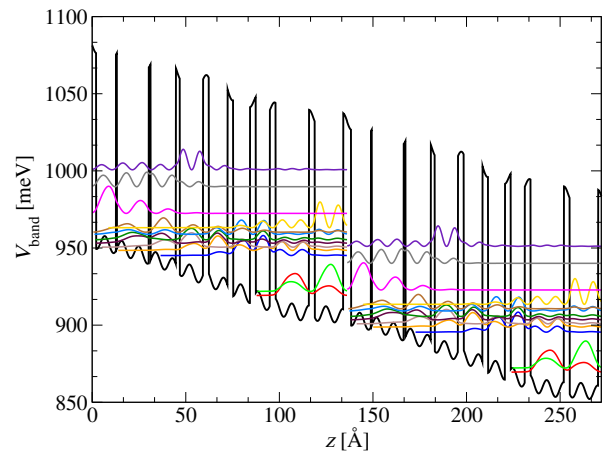


FIG. 9. Conduction band potential of a hybrid QCL design [28] with the addition of the 30th acoustic mode with modulation $M = 5$ meV. Two periods are shown at the resonance bias $K = 3.63$ kV cm⁻¹ along with the corresponding wavefunction moduli squared.

acoustic signal generated in [28], we estimated that the strain amplitude perturbed the conduction band potential by ~ 2 meV. With this assumption in Eq. (14), we can explore which acoustic modes affect electron transport, how the effects scale with modulation strength M , and which type of QCL designs are affected most significantly. We will dedicate special focus either to modes with frequencies ~ 100 GHz as these have been reported experimentally in the modulation of superlattice band-structures [11, 13, 15], or to 500–700 GHz modes, as a coherent phononic source has been reported in this range [52].

It is important to note that the strain standing wave, and hence deformation potential, oscillates in the time-domain around the zero point. The acoustic frequencies considered in this work are on the scale of a few hundred GHz, and the deformation, therefore, oscillates on a similar timescale to the electron dynamics within intersubband devices. As such, the deformation cannot be “averaged out” as a fast background effect, and a computationally demanding time-dependent model would be required for an accurate analysis of the acoustic effect on electron transport. In this work, however, we use a simplified time-independent approximation. Here, we consider the strain wave at its zero-phase point in the time domain, i.e., with the local deformation “frozen” at its maximum value. This allows us to gain insight rapidly into the effect of the spatial component of the acoustic deformation upon carrier dynamics.

In Fig. 9, we present the conduction band potential of Device A, as described in Section III, and Ref. [28], where the 30th acoustic mode is added as strain to the original potential with modulation strength $M = 5$ meV to illustrate the effect of Eq. (14) on the bandstructure potential. The potential itself is the main input for our Schrödinger–Poisson solver, from which we obtain the

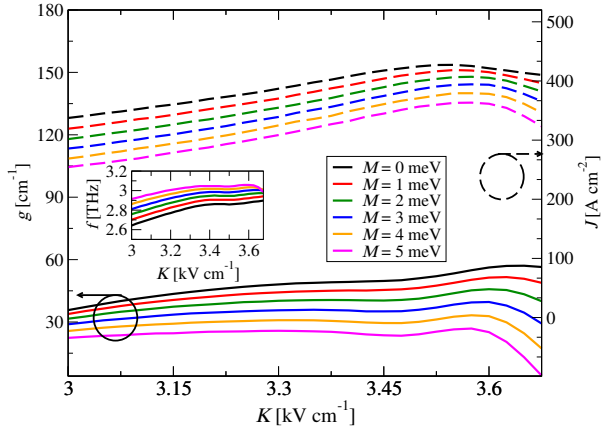


FIG. 10. Material gain and current density dependence on electric field when the first acoustic mode $n = 1$ is added with a range of modulation strengths to the conduction band potential of Device A.

quasi-bound state energies and the corresponding wavefunctions. This algorithm is coupled with a density matrix transport model and we can obtain the dependence of the QCL emission frequency, f , current density J and material gain g as a function of the applied electric field K . The K and J values directly correspond to the voltage and current in experimental device characterization, while the material gain offers insight into whether the structure lases or not, as well as providing information on the dynamic range. If a double-metal plasmonic waveguide is assumed, typical losses are $\sim 20 \text{ cm}^{-1}$. Our simulations are reliable up to the peak of current density $J(K)$. Beyond this, the device enters a negative-differential-resistance (NDR) regime, and becomes electrically bistable.

Our approach to understanding the effect of acoustic resonances on QCL performance is to analyse key QCL performance parameters derived from $g(K)$, $J(K)$ and $f(K)$, when (a) the modulation strength of a given mode is varied, and when (b) the mode index is varied, with a constant modulation strength.

In Fig. 10, we show the contribution of the first acoustic phonon mode with resonant frequency 17.4 GHz and modulation strengths M up to 5 meV in Device A. The traces corresponding to $M = 0$ represent the unperturbed simulation outputs of our model. We observe a monotonically rising current density profile, material gain that surpasses the losses and in the inset, we note that this structure operates around 2.5–2.75 THz, which agrees very well with the experimental results [28]. There is a significant change in performance as the modulation strength M increases, where the most important effect is a shift of the current density peak, causing a reduction to the dynamic range.

To quantify the acoustic strain effect, we have extracted key performance parameters for the QCL—the dynamic range, peak gain, peak (NDR) current density and the frequency of emission at the start of the NDR

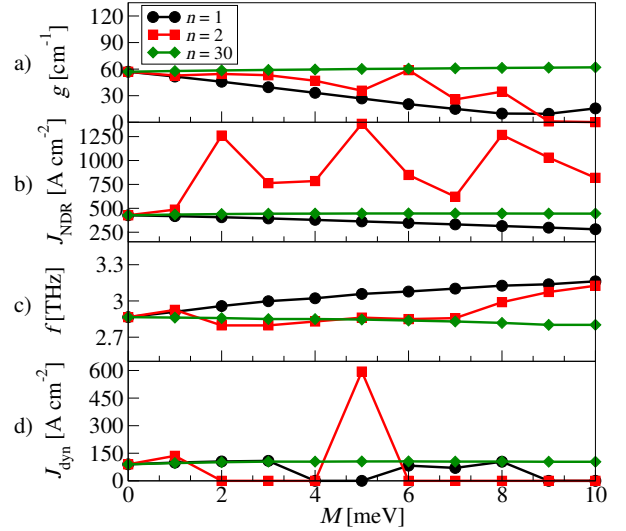


FIG. 11. Dependence of performance parameters for Device A, as a function of modulation strength using acoustic modes $p_n(z)$ with indices $n = 1, 2, 30$. Results are shown for (a) peak gain, (b) current density at the NDR point, (c) emission frequency (at NDR point) and (d) dynamic range.

region—as a function of modulation strength, with results presented in Fig. 11 for the $n = 1, 2$ and 30 modes.

The material gain and the current density values in Fig. 11(a) and 11(b) are taken as the peak values of the corresponding traces in Fig. 10, whereas the frequency in Fig. 11(c) is taken at NDR point (peak of the current density in Fig. 10). The dynamic range in Fig. 11(d) is calculated as the current density difference between the NDR value and the value that corresponds to material gain threshold of $\sim 20 \text{ cm}^{-1}$, we note when the threshold bias is larger than the bias corresponding to the NDR value, the dynamic range is set to zero value, physically indicating a non-lasing structure. In Fig. 11(d), the second mode causes highly disruptive perturbation to the conduction band potential leading to a non-lasing structure. This occurs because the second mode has a sinusoidal shape across one period and when added to conduction band potential, similarly as in Fig. 9, it causes abrupt changes in the shape of the conduction band potential, drastically affecting QCL performance.

As expected, the perturbation to each of these values increases with respect to M . However, the effect of the higher order $M = 30$ mode ($\sim 522 \text{ GHz}$) is shown to be considerably weaker than that of the lower modes.

This is confirmed further in Fig. 12, which shows that the variation in the QCL performance parameters oscillates and then decays as a function of acoustic mode index in all cases. The first 20 modes all affect transport, are capable of perturbing the conduction band potential strongly, and even prevent the structure from lasing owing to a strong shift of the NDR point and reduction of dynamic range. This is in agreement with previous reports of heterostructures being modulated by $\sim 100 \text{ GHz}$

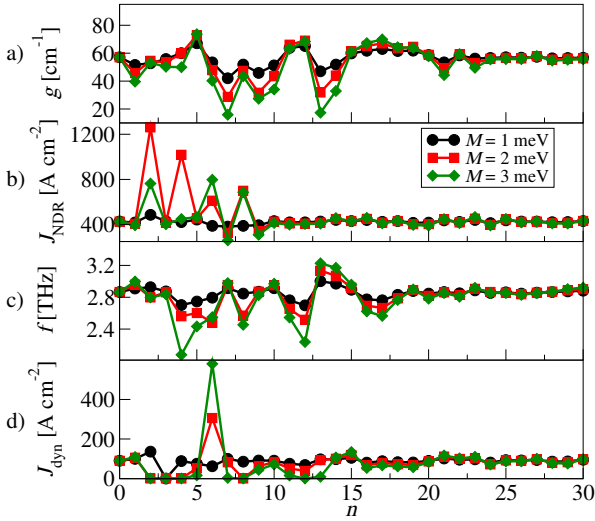


FIG. 12. Dependence of performance parameters for Device A (Hybrid QCL design), as a function of acoustic mode $p_n(z)$ index, using varying modulation strengths $M = 1, 2, 3$ meV. Results are shown for (a) peak gain, (b) current density at the NDR point, (c) emission frequency at NDR point and (d) dynamic range. Values corresponding to $n = 0$ represent non-perturbed values (ie $M = 0$).

acoustic pulses [11, 13, 15]. The lowest mode perturbs potential at its endpoints the most. In our simulations of transport we always define the QCL period as starting (and ending) from the midpoint of the injection barrier. Adding a modulated standing wave $M \cdot p_0(z)$ causes perturbation of the injection barrier so strongly affecting the tunnelling. We note that this effect is significant in Fig. 11 even for low modulation strengths. However, higher-order modes have negligible effect. This is explained by the periodicity of the high-order acoustic modes becoming much shorter than that of the QCL potential profile. As such, these act as a very high-frequency oscillation superimposed upon the QCL potential, which by analogy with the envelope-function model, will have only a weak effect on the eigenstates of the electrons.

In Fig. 13 and Fig. 14, we show comparable analyses of an LO-phonon depopulated QCL (Device B) [10] and a BTC QCL (Device C) [30] respectively. In both cases, we observe a similar general behaviour to that in Fig. 11, however Device B displays very high sensitivity to the second acoustic mode. This is understandable, as the LO-phonon-depopulated QCL design is more sensitive to perturbations in the injection barrier, because the coupling between adjacent periods is more selective than in BTC and Hybrid structures. Interestingly, the second mode causes very sudden deterioration of the material gain in Fig. 14, and this is likely due to the nature of the bandstructure potential for this particular structure.

We note that both Hybrid and LO-phonon-depopulated QCLs use similar resonant tunnelling injection between adjacent periods, while BTC structures employ closely spaced minibands of states to

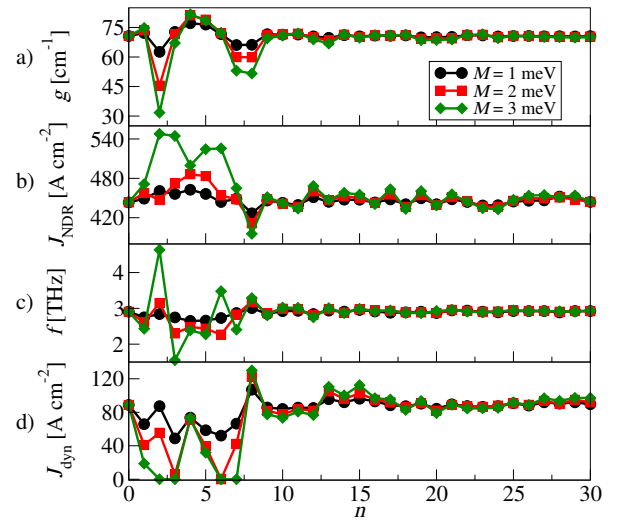


FIG. 13. Dependence of performance parameters for Device B (LO phonon design), as a function of acoustic mode $p_n(z)$ index, using varying modulation strengths $M = 1, 2, 3$ meV. Results are shown for (a) peak gain, (b) current density at the NDR point, (c) emission frequency (at NDR point) and (d) dynamic range.

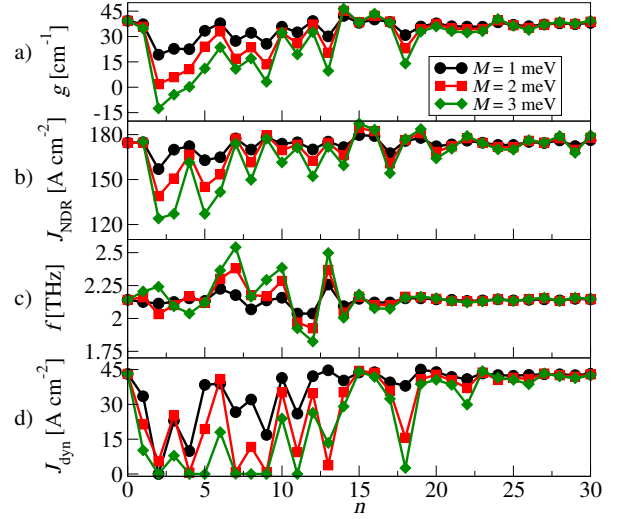


FIG. 14. Dependence of performance parameters for Device C (BTC design), as a function of acoustic mode $p_n(z)$ index, using varying modulation strengths $M = 1, 2, 3$ meV. Results are shown for (a) peak gain, (b) current density at the NDR point, (c) emission frequency (at NDR point) and (d) dynamic range.

depopulate the lower lasing level. For this reason, Device C is more sensitive to lower mode perturbation.

As with Device A, the acoustic perturbation effect oscillates and then decays at higher mode indices. In each case, the periodicity of the acoustic deformation potential becomes short compared with that of the QCL layer structure. LO phonon QCLs employ fewer quantum wells per period than BTC or Hybrid designs, and are therefore

much shorter. As such, in Fig. 14 and Fig. 12, the added strain perturbs transport up to 20–24th mode, while in Fig. 13, the transport features saturate around the 10th mode. Interestingly however, the frequency of the saturation point is comparable for all three designs (~ 400 GHz), as the LO phonon design has a wider separation between modes.

Modulation of the QCL emission frequency (on the scale of a few hundred GHz) is shown also to be possible for each of the three devices. This reaffirms our conclusion that acoustic modulation of QCL performance is caused by perturbing the conduction band potential in the injection barrier. Thus, tunnelling current and injection will be affected most strongly, though optical transitions, which typically happen in the first two wells of QCL period, are also likely to suffer some detuning due to applied strain. In all cases, we observe an oscillation in emission frequency (and current and gain) as the acoustic mode index increases. This occurs as lower modes have a spatial distribution that locally perturbs the potential profile in wells where the optical transition take place.

VI. CONCLUSION

We have presented analysis of acoustic resonances in arbitrary superlattice heterostructures, focusing on THz QCL devices. The model presented in Section II provides a flexible method to determine the resonant frequencies with high precision in arbitrary superlattice profiles. In Section IV, we discussed the precision of quasi-analytical approaches and calculated the deviation from bulk and average approximations given in Eq. (11). We showed that a coarse approximation to the acoustic mode frequencies may be determined analytically from the period length and average acoustic velocity in the superlattice. However, approximately 2 GHz detuning of the acoustic mode spacing arises from the precise layer composition in the structure, and this may only be computed using numerical methods.

We show that this detuning effect is greatest in superlattices with high variation of acoustic velocity between layers. This is in some cases periodic, and its period is determined by resonances of the acoustic wave within barrier layers in the structure. As such, this effect can be manipulated through superlattice layer design and offers another degree of freedom for fine-tuning frequency control of phononic devices.

In Section V we examined the effect of acoustic modes on electron transport in THz QCLs, using a deformation-potential approach. We found that the gain, threshold current and emission frequency are all perturbed significantly for acoustic modes up to ~ 200 GHz, in line with previous experimental investigations. These affect bandstructure potential in its most sensitive location — the injection barrier, thus directly affecting resonant tunnelling that couples carriers between adjacent periods, while slightly higher modes may also perturb bandstructure

potential in wells in which key optical transitions take place. For high-frequency modes, however, the acoustic deformation potential oscillates on a length-scale much smaller than the QCL layer structure, and hence has negligible effect on transport. We also observed that overall, designs with longer period length display slightly higher sensitivity to acoustic perturbations.

This investigation demonstrates the potential for the design of THz QCLs for high speed modulation, or higher temperature operation, through the engineering of phonon interactions.

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DATA AVAILABILITY

The data associated with this paper are openly available from the University of Leeds Data Repository. <https://doi.org/10.5518/1301>.

AUTHOR DECLARATIONS

Conflict of interest

The authors have no conflicts to disclose.

Author contributions

Aleksandar Demić: writing — original draft preparation (lead); investigation (lead); methodology (equal); software; visualization; data curation. **Alexander Valavanis:** writing — reviewing & editing (lead); investigation (supporting); conceptualization (equal); methodology (equal); supervision (equal); funding acquisition (supporting). **James Bailey:** investigation (supporting); **Andrey Akimov:** investigation (supporting); **Paul Dean:** funding acquisition (supporting). **Lianhe Li:** investigation (supporting). **A. Giles Davies:** funding acquisition (supporting); conceptualization (supporting). **Edmund H. Linfield:** funding acquisition (supporting); conceptualization (supporting). **Paul Harri-**

TABLE I. Layer composition of considered structures in section IV. Layer widths in bold text represent the barriers, each structure ends with the injection barrier layer.

Structure.	Layer thicknesses [\AA]	Al composition in $\text{Al}_x\text{Ga}_{1-x}\text{As}$ layers
Device A	106/ 5 /170/ 10 /135/ 21 /124/ 31 /100/ 31 /90/ 31 /75/ 31 /178/ 31 /152/ 41	$x = 0.14$
Device B	110/ 18 /115/ 35 /94/ 39 /184/ 48	$x = 0.15$
Device C	144/ 10 /118/ 10 /144/ 24 /144/ 24 /132/ 30 /124/ 32 /120/ 44 /126/ 50	$x = 0.1$
Device D	76.4/ 17.5 /154.7/ 33.7	$x = 0.3$
Device E	82/ 46 /72/ 41 /160/ 43	$x = 0.15, x = 0.075$
Device F	$x(z) = \frac{4x_0}{d_{sl}^2} \left(z - \frac{d_{sl}}{2} \right)^2$	$d_{sl} = 3000 \text{ \AA}, dz = 2.825 \text{ \AA}, x_0 = 0.14$
Device G	$x(z) = \frac{4x_0}{d_{sl}^2} \left(z - \frac{d_{sl}}{2} \right)^2 \left[1 + 0.18 \cdot \frac{4x_0}{d_{sl}^2} \left(z - \frac{d_{sl}}{2} \right)^2 \right]$	$d_{sl} = 620 \text{ \AA}, dz = 2.825 \text{ \AA}, x_0 = 0.42$
Device H	42/ 17 /20/ 17	$x = 1$
Device D ₁	76.4/ 35 /154.7/ 33.7	$x = 0.3$
Device C ₁	144/ 10 /118/ 10 /144/ 24 /144/ 24 /132/ 30 /124/ 32 /120/ 44 /126/ 50	$x = 0.1, x = 1$
Device C ₂	144/ 10 /118/ 10 /144/ 24 /144/ 24 /132/ 30 /124/ 32 /120/ 44 /126/ 50	$x = 0.1, x = 1$
Device A ₁	106/ 5 /170/ 10 /135/ 21 /124/ 31 /100/ 31 /90/ 31 /75/ 31 /178/ 31 /152/ 41	$x = 0.14, x = 0.3$
Device I	150/ 20 /150/ 40 /150/ 80	$x = 1$
Device J	100/ 20 /100/ 20 /200/ 20 /200/ 20	$x = 0.1$

son: conceptualization (equal) **Anthony Kent:** conceptualization (equal); supervision (equal); funding acquisition (equal). **John Cunningham:** conceptualization (equal); project administration (lead); supervision (equal); writing — reviewing & editing (equal); funding acquisition (equal).

erate parabolic profiles of Devices F and G.

APPENDIX: LAYER COMPOSITION OF DEVICES

The layer composition of structures used in Section IV are shown in Table I, along with functions used to gen-

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