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A probabilistic approach for acoustic emission based monitoring techniques: with application to structural health monitoring

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Abstract

It has been demonstrated that acoustic-emission (AE), inspection of structures can offer advantages over other types of monitoring techniques in the detection of damage; namely, an increased sensitivity to damage, as well as an ability to localise its source. There are, however, numerous challenges associated with the analysis of AE data. One issue is the high sampling frequencies required to capture AE activity. In just a few seconds, a recording can generate very high volumes of data, of which a significant portion may be of little interest for analysis. Identifying the individual AE events in a recorded time-series is therefore a necessary procedure to reduce the size of the dataset. Another challenge that is also generally encountered in practice, is determining the sources of AE, which is an important exercise if one wishes to enhance the quality of the diagnostic scheme. In this paper, a state-of-the-art technique is presented that can automatically identify AE events, and simultaneously help in their characterisation from a probabilistic perspective. A nonparametric Bayesian approach, based on the *Dirichlet process* (DP), is employed to overcome some of the challenges associated with these tasks. Two main sets of AE data are considered in this work: (1) from a journal bearing in operation, and (2) from an Airbus A320 main landing gear subjected to fatigue testing.

1. Introduction

A research topic of increasing popularity in *Structural Health Monitoring* (SHM), is the use of *Acoustic Emission* (AE)-based techniques for damage detection. Although AE was first defined by Kaiser in 1950 [1], it was only with the development of high sampling-frequency instrumentation and highly-sensitive transducers that the detection of AEs was possible, and an extensive amount of research has since been carried out to better understand the underlying correlation between the physics of AEs and the mechanisms that produce them in mechanical systems [2–7]. Additionally, in a more practical context, several promising results have been demonstrated when implementing AE-based monitoring techniques for damage detection in structures and rotating machines. Some examples of this exercise include rolling element bearings [8, 9], gears [10], journal bearings [11, 12], self-compacting concrete specimens [13], and aerospace structures [14, 15].

Compared to other forms of monitoring techniques, AE measurements can provide a more sensitive means of detecting the onset of damage, facilitating the earlier diagnosis of an unhealthy structure. This attractive attribute can be of great value for the development of an optimised maintenance schedule. For example,

considering an offshore wind turbine, it is more convenient to determine remotely whether maintenance is required, given the associated high cost of having the wind turbine put out of service for a potentially unnecessary repair. Conversely, if the detected damage in the wind turbine suggests that it will fail prior to its next scheduled maintenance, then action can be taken to prevent a potentially-catastrophic outcome. The acquisition of a more sensitive damage-detection system therefore means having more time to plan a suitable course of action.

Despite its promising advantages in the early detection of damage, there are some added complications associated with AE analysis that need careful attention [16]. One of these limitations relates to the high sampling frequencies required to record AE signals. In a matter of a few seconds, a recording can generate millions of data-points, making them tedious to store and manipulate. One is therefore likely to rely on feature-extraction methods in order to reduce the overall size of the measured data. The features of interest are those that define the AE, and a few examples of these features can be seen in Figure 1, for a typical AE waveform.

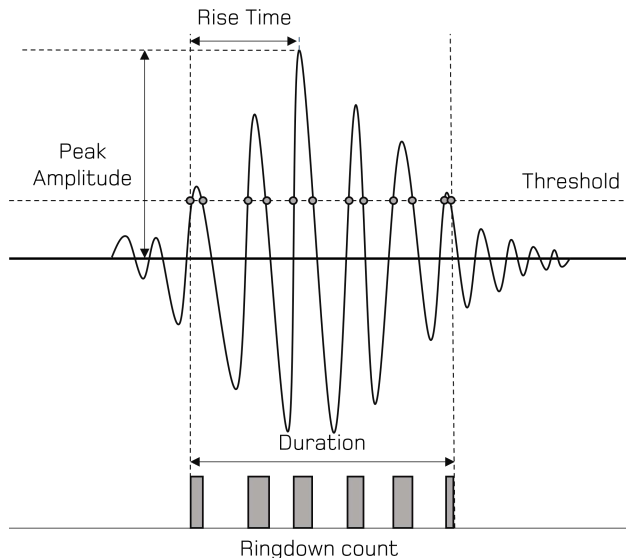


Figure 1: Features of a typical AE. Reproduced from [17].

Various means of feature extraction exist [18]; a common approach is to first identify and isolate the individual AE events/bursts that emerge throughout the recorded signal. The challenge here, however, is to have an algorithm to reliably identify the relevant AE events for analysis, and distinguish them from background noise.

One of the first steps in an AE-based monitoring scheme is to define a threshold from which any voltage crossings are assumed to indicate the presence of some form of AE burst activity. Unfortunately, deciding on the threshold is not as trivial as it may seem. In practice, the threshold may be established from experience, and judging a suitable threshold value will depend on the properties and geometrical constraints of the propagating medium. This approach is limited in that it is specific to the application at hand; the operator

must carefully select an optimal threshold to capture the AE events of interest.

Nevertheless, this exercise is not only meaningful for reducing the overall size of the dataset, but also for retaining AE events carrying information of the health-state of the structure. The underlying features that characterise the isolated AE events are somewhat influenced by their source, and some correlation will exist based on the type of damage or physical mechanism that generates them.

For example, several attempts have been pursued to correlate AE features - particularly the *ringdown count* (Figure 1) - with fracture-mechanical parameters, such as the stress-intensity factor of structures subjected to cyclic loading [19–22]. These studies are based on Paris-Erdogan-type laws [23], to make estimates of the remaining fatigue life of structures, and demonstrate that count-rates can in fact be used to estimate the growth-rate of cracks. The caveat for the unwary is that one must only use events generated by the *primary* crack extension. Even if all potential AE events are correctly identified and isolated for analysis, this condition is another challenge commonly encountered in practice, requiring the sources of AE events to be carefully characterised for analysis. This complication is even more of an inconvenience in applications dominated by a rich collection of AE sources and/or excessive amounts of background noise.

Some methods to characterise AE events have been proposed to isolate those deriving from crack extension. In the work of [19] and [22], the AE events of interest were those emitted within 10% and 30% of the peak amplitude of the applied load, respectively. Although good results were obtained from this choice, there is an associated risk of ignoring the AE events generated during the remainder of the fatigue cycle, and it is often necessary to obtain information from all possible sources [24]. This consideration inevitably implies the need for a more elaborate characterisation strategy.

In [25], for example, a pattern recognition approach was adopted to automatically classify AE signals obtained from a box girder of a bridge. The developed methods were able to identify three distinct classes that could distinguish crack-related signals from those generated by frictional processes. Another promising pre-processing technique that builds on this idea can be found in [26], where the proposed method outputs the best combination of AE-features that can provide the greatest separation of classes; therefore, yielding a dataset that is most sensitive to the various sources of AE. Bo et al. [27], argue that the complex nature of the AE signals must be accounted for when attempting to identify their sources, and proposed a novel deconvolution approach to separate the distinct sources emerging in a fatigue test of a wind-turbine blade. Although pattern-recognition techniques work well for this purpose, some form of validation is still required to link the identified classes with their corresponding generating mechanisms. An alternative approach employed in [14, 28], exploits the localisation capabilities of AE-based techniques to directly characterise AE activity emerging near the developing crack. Damage localisation is one important application of AE monitoring, but it can be difficult to implement, especially in structures with complex geometries [29, 30].

Overall, it becomes evident that two emerging challenges limit the extent to which AE techniques can generalise across SHM applications: the first, on the correct identification of individual AE events in a recording, and the second, on identifying their respective source. In this paper, a state-of-the-art means of

addressing these problems is proposed; a probabilistic framework is developed by treating the generation of AE events as a random process. Adopting this perspective allows one to quantify the probability of finding an AE event in any arbitrary section of a raw time-series. This implementation is fundamentally employed with a *Poisson* distribution, a *Probability Mass Function* (PMF) that will be used here as the building-block for modelling counts extracted from AE signals. Ultimately, a powerful nonparametric Bayesian approach is introduced and implemented, both to identify the AE events, and to group them based on their features in an online scheme.

The proposed strategies are described in the following sections, and then demonstrated with a rich AE dataset collected from a journal bearing in operation, and from an Airbus A320 main landing gear subjected to fatigue testing.

2. A probabilistic perspective for AE-based monitoring techniques

As highlighted above, determining the threshold for AE events can be an assiduous task that may depend highly on the expertise of the operator. Alternatively, a potentially more robust approach could be employed to have the threshold defined statistically. One may assume the background noise in the signal to be the result of a generating process in which the observations are samples drawn from a Gaussian distribution, and the threshold could then be determined numerically using a Monte Carlo method [17]. Although this approach offers a threshold determined directly from the recorded signal, the resulting selection of AE events may still be heavily corrupted by background noise. For example, if a 99th-percentile threshold is chosen on the recorded time-series, it means (at the risk of redundancy), having 1% of the data points estimated to lie above that threshold. This deceptively-small percentage could be a problem in scenarios where the sampling frequency is high, such as an AE reading. In the span of a few seconds, millions of data points are recorded, and thus thousands of “events” would consequently be taken into consideration for further analysis. This issue means mistakenly identifying a vast number of events deriving from the background noise, when it is likely that only a fraction of them will actually originate from damage.

An attempt to overcome these limitations is explored in this work by introducing a probabilistic framework; the idea is to quantify how certainly a threshold crossing is believed to derive from an AE event. Concretely, by counting the number of times a signal exceeds the threshold in a given time-frame, one can evaluate the probability of an AE event existing in that time-frame. In the following sections, it will be demonstrated how the Poisson distribution can be conveniently used for this purpose.

2.1. The Poisson distribution

The Poisson distribution is a discrete probability distribution used to model the number of events occurring in a given time or space interval. The Poisson PMF is defined as,

$$p(x|\lambda) = \frac{e^{-\lambda} \lambda^x}{x!} \quad (1)$$

where x is a positive integer corresponding to the number of observed events and λ is the rate or expected number of events happening in the time/space interval. The value of the parameter λ may be unknown, and a Bayesian framework is adopted here to infer the distribution over λ . The count-rate is therefore modelled according to some prior probability distribution, $p(\lambda)$, that quantifies a prior belief over all possible values of λ . Bayes' rule can then be applied for inference to recover the posterior $p(\lambda|x)$.

Fortunately, a conjugate prior of the Poisson distribution exists, allowing for a closed-form solution for $p(\lambda|x)$ [31]. In order to meet this condition, the chosen conjugate prior must be a Gamma distribution, resulting in another Gamma distribution when combined with the Poisson likelihood [31]. The predictive distribution, given a new observation x_{new} , can then be calculated by taking the expectation of the Poisson likelihood with respect to the posterior distribution,

$$p(x_{new}|x) = \mathbb{E}_{p(\lambda|x)}[p(x_{new}|\lambda)] = \int p(x_{new}|\lambda)p(\lambda|x) d\lambda \quad (2)$$

Conveniently, equation (2) reduces to a negative-binomial distribution. In particular,

$$x_{new}|x \sim \text{NB}(a^*, b^*) \quad (3)$$

$$a^* = N\bar{x} + a, \quad b^* = \frac{N + b}{N + b + 1}$$

where N is the number of training samples, \bar{x} is the sample mean of the number of already observed x , and the parameters a and b correspond to the shape and rate of the Gamma prior distribution, respectively. The probability of observing a certain number of events in a given time interval can be easily calculated from (3), and a meaningful representation of the uncertainty over λ is given in the process.

An AE event may be found in the time-series by treating the *ringdown-count* - or *count* for short - as the random variable x . Therefore, the strategy that follows assumes that the extracted counts are distributed according to a Poisson distribution. In order to demonstrate how this reasoning can be implemented in practice, the considered AE time-series will be limited to unprocessed recordings in which distinct transient events can be observed occurring sporadically in a continuous stream of background noise. This type of AE signal is often referred to as a *burst signal* [18], and an example of a typical AE recording of this type can be seen in Figure 2. Under this consideration, it is worth noting that a relatively-higher count-rate can be expected in sections encompassing an AE event.

Given that the count extracted from any arbitrary windowed section cannot be determined with absolute certainty, counts are interpreted as realisations of a random process. Now, one can let the Poisson distribution model the background noise. The idea here is to construct a dataset comprised of uni-dimensional variables representing the counts observed in a windowed section that correspond uniquely to background noise, or sections where no obvious AE activity exists. It is easy to imagine that the counts in each of these sections will be low, and one would hence end-up with an array comprised of a combination of zeros and/or random positive integers near zero. This approach may seem counter-intuitive at first, since the background noise is

being modelled rather than the actual AE events, but the results may be easier to interpret when evaluating the *Negative Log-Likelihood* (NLL), of new observations with respect to the already inferred distribution in (2),

$$NLL(x_{new}) = -\log(p(x_{new}|x)) \quad (4)$$

This strategy treats AE events as anomalies in the time-series, and evaluating (4) for new observations should therefore return higher-than-normal values whenever encountering sections in the time-series with AE events. In order to demonstrate this procedure in practice, a simple lead-break case-study test is now considered.

2.2. AE event identification in a time-series signal recorded from a lead-break test

A common and convenient way to simulate AE events is by breaking pencil-leads on an elastic surface. This type of source was simulated here with a Hsu-Nielson device [32], and then recorded with a 40dB WB Mistras AE sensor attached to the same surface. Figure 2 shows the AE signal recorded during the test. The time-series clearly displays at least two distinct bursts, indicating the instances when the pencil-leads snapped. The challenge is to have an algorithm identify and isolate these AE events. If one were to establish some threshold, then voltage crossings can be assumed to be indications of AE activity. Intuitively, this approach could easily detect the bursts observed here, to then have them isolated from the rest of the signal.

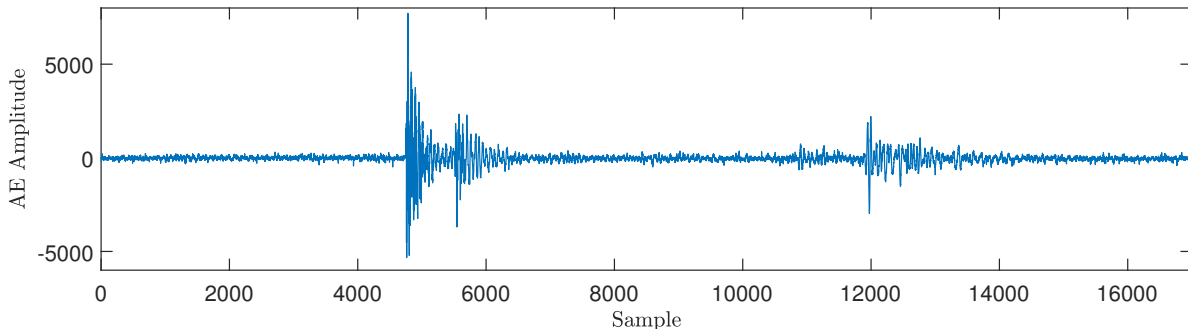


Figure 2: Acoustic emission waveforms from lead break test.

The problem, however, is that a vast number of “events” deriving from the background noise would also be taken into consideration, when only the main events caused by the pencil-lead breaks are of actual interest. Some progress can be achieved by adopting the Bayesian approach described above. Being explicit, the count-rate λ , associated with the background noise was therefore assumed to be distributed according to a Gamma distribution, and the corresponding parameters were set to units ($a = b = 1$) under the assumption that λ will be expected to be zero or some other value near zero. The reasoning behind this assumption is again based on treating the generated AE-waves as rare events.

After windowing the entire time-series with a non-overlapping square function, 20 samples were extracted and used to infer the posterior distribution. It is reiterated here that these samples are counts from sections known to lack any form of meaningful AE activity. The probability of observing x number of threshold

crossings in a given section was calculated using equation (3). In order to quantify the confidence of an AE event existing within a section, equation (4) was evaluated on each of the remaining sections. The results can be seen in Figure 3, where colour-bars representing the NLL were included. By looking at Figure 3a, the sudden increases in the NLL can be interpreted as an anomaly being detected, which in turn happen to correspond to the AE events of interest.

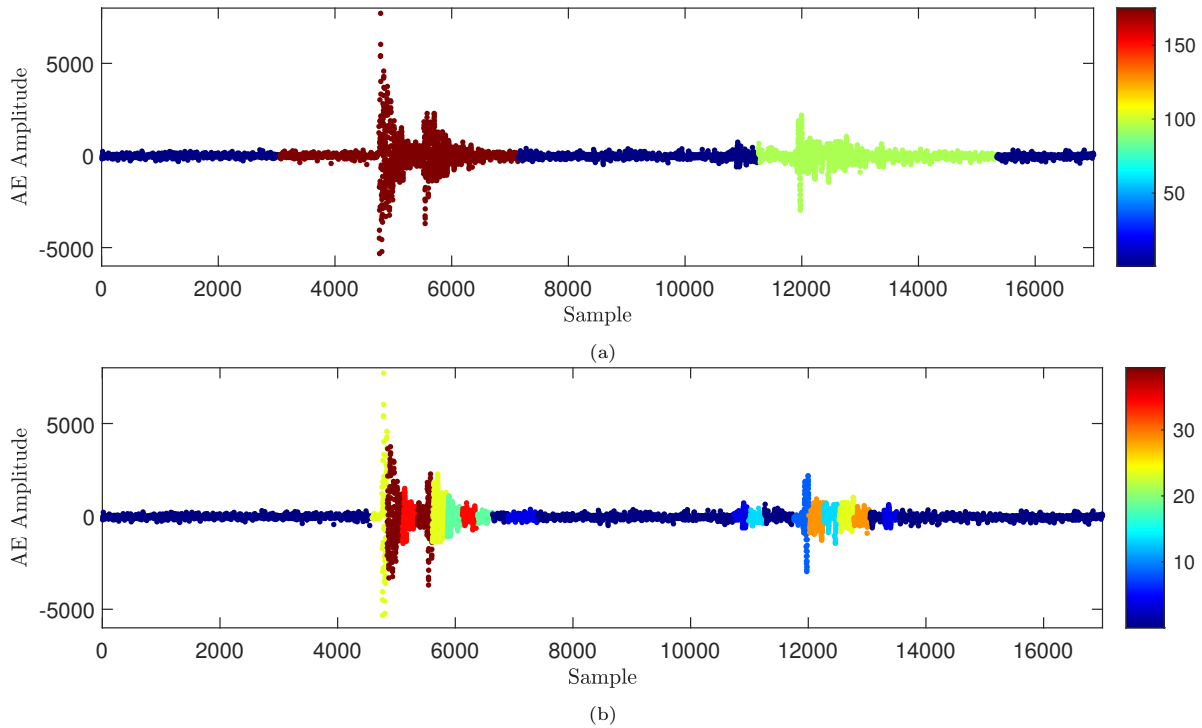


Figure 3: Negative log-likelihood results on lead-break dataset. The colour bar represents the likelihood of an event existing in a given time interval. Window lengths were (a) $n = 4096$ and (b) $n = 256$ data points.

An important point worth discussing is the immediate limitation that becomes evident when assessing the sensitivity of the model to the window-length. The results presented in Figure 3a seem more promising because a window-length comprised of 4096 sample-points was chosen beforehand to match the length of the main AE event. Unfortunately, knowing in advance the length of all potential AE events is unlikely to be case, specially when dealing with more complex applications. The effectiveness of this method clearly depends on the length of the sliding window, as demonstrated in Figure 3b, where a window length of 256 sample-points was chosen. By having a window-length shorter than the duration of the AE event, the model interprets several components in what should be a single event. The upside of establishing a shorter window-length is that the onset of the events are captured more precisely. It is clear that a validating step would become essential to determine the optimal window-length. In both cases, nonetheless, the background is mostly identified as noise.

3. Nonparametric clustering approach for AE event identification and feature extraction

An interesting development can be made by extending the model into a mixture of Poisson distributions. The idea is to have the events of interest modelled by a set of independent distributions, each characterised by a different mechanism responsible for the generation of the observable AE events. In doing so, the approach now aims to infer the parameters of the various components comprising the mixture model.

This idea inevitably leads to the problem of identifying AE events in *burst-type* signals, requiring the determination of a suitable window-length (Section 2.2). Before dwelling on ways in which the robustness of the model can be improved, some background on mixture models will be covered so that this paper is as self-contained as possible. The interested readers can refer to [31] or [33] if wishing to learn more on the machine-learning methods covered in this work.

3.1. Finite Poisson Mixture Model

Recalling the pre-processing steps followed so far, a feature vector X can be constructed by extracting the number of threshold crossings observed in subsections of a raw AE time-series, encapsulated by a sliding step-window of length n . As the window slides through the signal, the number of threshold crossings should vary with changes in the AE activity. The distribution of X will be such that a single Poisson distribution may poorly represent the observations. Therefore, a sensible choice may be to instead model the observations as draws from a combination of several independent Poisson distributions.

First, a multinomial distribution is proposed over a vector of mixing proportions $\boldsymbol{\pi}$, in which each element π_k , is a mixing coefficient defining the probability that an observation belongs to the k^{th} group. The total number of groups K , is predefined, and $\sum_K \pi_k = 1$. It should be noted that the collection of data-points assigned to a distribution in the mixture model will be referred to as a “group”. In the literature, the term group is also used interchangeably with “cluster”.

Part of the inference procedure is to derive a latent variable \mathbf{z} , representing the assignment of a data-point to one of the groups in the mixture model (i.e. its labels). If each group is defined by a unique Poisson distribution with count-rate λ_k , then each observation x_n can be modelled in the following form,

$$\begin{aligned} x_n | z_n &\sim \text{Poi}(\lambda_k) \\ z_n &\sim \text{Mult}(\boldsymbol{\pi}) \end{aligned} \tag{5}$$

All the model parameters can be then determined efficiently via *Expectation-Maximisation* [33], resulting in a maximum-likelihood solution, given the data that have been observed so far. Although this model may be a better representation of the observations, it can still be limited in practice. If only a few data points were available, having the local parameters estimated empirically could result in the model not generalising well in the presence of new observations.

Another consideration is in deciding automatically on the number of groups the mixture model should have. A possible solution here is to assume that the observations can be represented by two unique groups; that is, one characterised by the relatively low count-rate corresponding to background noise, and another

that accounts for all the possible higher count-rates that may correspond to AE events. The sequence of sections in the time-series should then be grouped into one in which some form of AE activity exists, and another in which minimal or no events are found. By discarding the latter, one is left with a series of AE events ready to be processed for feature extraction, as required by the application at hand.

However, it might be more convenient to take a step further and split the detected AE events into several groups, in order to get a better insight into their respective sources. For example, it might be better to know whether an AE event corresponds to a specific damaged component, rather than plainly categorising it together with all the rest. The problem, however, is on deciding *a-priori* the number of groups, since one would need to consider every possible condition that a structure or machine might encounter during its lifespan. One way to circumvent this problem is by having the model autonomously create new groups whenever it may be deemed necessary. This approach will require yet another modification, to provide the mixture model the flexibility to account for a possibly *infinite* number of groups.

3.2. Dirichlet Process Poisson Mixture Model

Dirichlet Processes (DPs) [34], are powerful stochastic processes with the ability to assign random probability measures to a finite partition $\{A_1, \dots, A_m\}$ of a continuous measurable space Θ . A DP can be defined by letting Θ be distributed according to some *base* distribution, G_o . A random measure over G_o can be represented by the vector $G = \{G(A_1), \dots, G(A_m)\}$, which can be said to be drawn from a DP if G is distributed as a finite-dimensional Dirichlet distribution with parameters $\{\alpha G_o(A_1), \dots, \alpha G_o(A_m)\}$. That is, $G \sim DP(\alpha, G_o)$ if,

$$\{G(A_1), \dots, G(A_m)\} \sim Dir(\alpha G_o(A_1), \dots, \alpha G_o(A_m)) \quad (6)$$

where α is a positive scaling parameter. A powerful application of the DP is when it is used as a prior on the parameters of a mixture model. In particular, the observations x_n are assumed to arise from the following generative process,

$$\begin{aligned} G | \alpha, G_o &\sim DP(\alpha, G_o) \\ \theta_n | G &\sim G \\ x_n | \theta_n &\sim p(x_n | \theta_n) \end{aligned}$$

where θ_n can now be interpreted as the parameters of the components in the mixture model. A graphical representation of the infinite Poisson mixture model is shown in Figure 4. By establishing a DP-prior on the mixture model, a distribution over K can also be inferred from the observations directly as part of the learning procedure, making DPs an attractive solution in SHM/CM when faced with a dataset comprised of a collection of unknown conditions. A detailed introduction to the infinite mixture model can be found in [35], and examples of its use in SHM can be found in [36, 37].

To begin, it will be necessary to make the inference over the parameters Bayesian. This step will lead nicely into the incorporation of a DP-prior over K . Firstly, the priors over λ_k are considered. As already

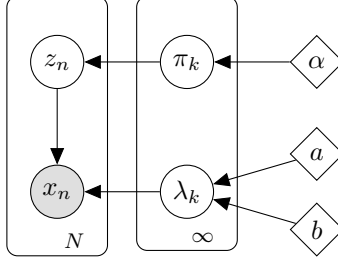


Figure 4: Graphical model of the infinite Poisson mixture model.

reviewed in Section 2.1, the Gamma distribution is chosen once again to represent the prior belief on λ . Assuming that the rate values, λ_k , of each group are independent, allows the specification of the joint density,

$$p(\lambda_1, \dots, \lambda_K | a, b) = \prod_{k=1}^K p(\lambda_k | a, b) \quad (7)$$

Now, the vector \mathbf{z}_n is characterised according to a multinomial distribution parameterised by $\boldsymbol{\pi}$,

$$p(\mathbf{z}_n | \boldsymbol{\pi}) = \prod_k \pi_k^{z_{nk}} \quad (8)$$

where the normalising constant simplifies to unity, and the expression is reduced to the probability of assigning a group. A Dirichlet distribution is chosen as a suitable prior on $\boldsymbol{\pi}$, and is also conjugate to the multinomial distribution. The probability density function of the Dirichlet distribution is given by,

$$p(\boldsymbol{\pi} | \boldsymbol{\alpha}) = \frac{\Gamma(\sum_k \alpha_k)!}{\prod_k \Gamma(\alpha_k)} \prod_k \pi_k^{\alpha_k} \quad (9)$$

which is parameterised by $\boldsymbol{\alpha} = \{\alpha_1, \dots, \alpha_k\}$. Having defined the densities on the parameters, the joint posterior likelihood is given by,

$$p(\mathbf{Z}, \boldsymbol{\pi}, \lambda_1, \dots, \lambda_k | X, \boldsymbol{\alpha}, a, b) \propto \left[\prod_n \prod_k (\pi_k p(x_n | \lambda_k))^{z_{nk}} \right] \left[\prod_k p(\lambda_k | a, b) \right] p(\boldsymbol{\pi} | \boldsymbol{\alpha}) \quad (10)$$

The conditional distributions for each parameter are proportional to the joint distribution, and can be derived analytically to give a Gibbs sampler [33], to solve equation (10). However, it will be worth marginalising out $\boldsymbol{\pi}$ and $\boldsymbol{\lambda}$ from the joint posterior to instead implement a collapsed Gibbs sampler [38]. This last step will not only improve the robustness of the sampler, but it will be a necessary one to have the model extend to an infinite number of components. The collapsed distribution is finally expressed as,

$$p(z_{nk} = 1 | \mathbf{Z}^{-n}, X^{-n}, \boldsymbol{\alpha}, a, b) \propto \frac{c_k^{-n} + \alpha_k}{\sum_j^K c_j^{-n} + \alpha_j} p(x_n | \mathbf{Z}^{-n}, X^{-n}, a, b) \quad (11)$$

where,

$$p(x_n | \mathbf{Z}^{-n}, X^{-n}, a, b) = \text{NB}(\mathbf{r}, \mathbf{p}) \quad (12)$$

and,

$$\mathbf{r} = a + \sum_{m \neq n} z_{mk} x_m, \quad \mathbf{p} = \frac{\sum_{m \neq n} z_{mk} + b}{\sum_{m \neq n} z_{mk} + b + 1}$$

The new notation c_k^{-n} corresponds to the count of all but the n^{th} element in the k^{th} group, \mathbf{Z}^{-n} to the set of all assignments except for the n^{th} one, and X^{-n} to the set of all the other observations; the superscript $-n$ does not represent a power here. The expression in (11) is also simplified by considering the value where the k^{th} element of \mathbf{z}_n is equal to unity, while all others are zero. A full derivation is provided in Appendix A. In this form, \mathbf{z}_n can now be resampled directly from equation (11). The two parts of this expression can be interpreted as comprising a new prior,

$$p(z_{nk} = 1 | \boldsymbol{\alpha}, \mathbf{Z}^{-n}) = \frac{c_k^{-n} + \alpha_k}{\sum_{j=1}^K c_j^{-n} + \alpha_j} \quad (13)$$

and a likelihood defined by the negative binomial density with parameters \mathbf{r} and \mathbf{p} . In this form, an infinite number of components can be managed, if the parameters α_k in (9) are all set to the same value. The Dirichlet prior can then be expressed as,

$$p(\boldsymbol{\pi} | \boldsymbol{\alpha}) = Dir(\boldsymbol{\alpha}/K, \dots, \boldsymbol{\alpha}/K) \quad (14)$$

and the sampling prior for $z_{nk} = 1$ becomes,

$$p(z_{nk} = 1 | \boldsymbol{\alpha}, \mathbf{Z}^{-n}) = \frac{c_k^{-n} + \alpha/K}{\alpha + N - 1} \quad (15)$$

where the fact that $\sum_{j=1}^K \alpha/K = \alpha$ and $\sum_{j=1}^K c_j^{-n} = N - 1$ were used. Now, by letting $K \rightarrow \infty$, equation (15) reduces to,

$$p(z_{nk} = 1 | \boldsymbol{\alpha}, \mathbf{Z}^{-n}) = \frac{c_k^{-n}}{\alpha + N - 1} \quad (16)$$

This new expression defines the prior probability of the n^{th} data point going into the k^{th} group, and it is proportional to the number of members that currently exist in that group. So far, the new prior only accounts for groups in which members exist, but in this framework, there is always a non-zero probability for a data-point to be assigned to a new ‘‘empty’’ component that is yet to be created. The probability of a new member finding its place in one of these empty groups can be easily derived by computing 1 minus the total probability of it going into any of the non-empty components. Hence,

$$p(z_{nk_*} = 1 | \boldsymbol{\alpha}, \mathbf{Z}^{-n}) = 1 - \sum_{k=1}^K \frac{c_k^{-n}}{\alpha + N - 1} = \frac{\alpha}{\alpha + N - 1} \quad (17)$$

where the subscript $*$ in k_* denotes an empty component. One can notice that the prior defines a probability of a new member either going to a non-empty component proportional to the number of its members, or to one of an infinite number of empty components proportional to α . Implementing this reasoning may begin by assigning all observations to the same component, and then resampling the assignments of each observation with probability,

$$p(z_{nk} = 1 | \boldsymbol{\alpha}, \mathbf{Z}^{-n}) = \begin{cases} \frac{c_k^{-n}}{\alpha + N - 1} & \text{for } c_k^{-n} > 0 \\ \frac{\alpha}{\alpha + N - 1} & \text{for } c_k^{-n} = 0 \end{cases} \quad (18)$$

After incorporating the data, an observation is assigned by sampling from $p(z_{nk} = 1 | \dots)$.

When accounting for an infinite number of components ($K \rightarrow \infty$), one can move from having a prior that determines how the observations group together among a fixed number of components, to one that can partition the data in any possible number of them. It should be noted at this point that the term “component” has been introduced to refer to the collection of all groups that are “empty” and “non-empty”. The former corresponds to groups that are yet to have data-points assigned to them, and the latter to those that already exist in the model.

Finally, the result yields an infinite Gibbs sampling procedure that involves resampling each z_n according to the probabilities,

$$p(z_{nk} = 1 | \dots) \propto \begin{cases} c_k^{-n} p(x_n | \mathbf{Z}^{-n}, X^{-n}, a, b) & \text{for non-empty components} \\ \alpha p(x_n | a, b) & \text{empty components} \end{cases} \quad (19)$$

where $p(x_n | \mathbf{Z}^{-n}, X^{-n}, a, b)$ is given by equation (12), and $p(x_n | a, b)$ by the expectation of the likelihood, $p(x_n | \boldsymbol{\lambda})$, with respect to the prior $p(\boldsymbol{\lambda} | a, b)$,

$$p(x_n | a, b) = \int p(x_n | \boldsymbol{\lambda}) p(\boldsymbol{\lambda} | a, b) d\boldsymbol{\lambda} \quad (20)$$

which, in this instance, is possible to evaluate because $p(x_n | \boldsymbol{\lambda})$ is a Poisson distribution parameterised by $\boldsymbol{\lambda}$, and $p(\boldsymbol{\lambda} | a, b)$ is its conjugate Gamma prior.

The resampling procedure can now be dictated as follows:

1. All elements are assigned to a non-empty component ($K = 1$).
2. One element is removed from its component and its likelihood evaluated with equation (19). The component is eliminated if the element was unique in that component.
3. If the unassigned element is more likely to belong to an empty component, then a new component is created, and the data point is assigned to that component.
4. One sweep is completed when each data point has been evaluated. The whole process is then repeated from Step Two, until the posterior converges to a solution.

It must be noted that inferring (19) is not limited to a collapsed Gibbs sampler, and variational methods have been developed for inference of Dirichlet process mixture models [39]. The sampling method here was preferred for its simpler implementation and intuition. The DP-PMM will be now demonstrated to model the AE events in a time-series signal.

4. AE event identification in time-series signals

Recovering AE events from a raw time-series can be a challenging task, particularly as the behavior of an event will differ from one to the next, and also because consecutive events may also overlap. As mentioned earlier, identifying and extracting these events may be an assiduous task, but a meaningful one, as it should reveal information on the health-state of the machine being monitored.

By introducing a DP prior, the mixture model can now adapt to the complex nature of the AE analysis. Compared to the methods already described, an infinite mixture model may be better suited for the detection of individual AE events in the time-series. Even without knowing the exact nature of the generated AEs, this approach should assign the various events into groups based on their features. Given that the feature of interest here is the count of an event, these groups are therefore modelled by a set of independent Poisson distributions. Extracting counts from individual events is a challenge in itself, since it is this feature that one needs to identify them in the first place.

A sliding window approach is again considered. As demonstrated in Section 2.2, the immediate challenge of this approach is finding a suitable window-length; if too long, it will be less likely to discern individual events and their counts. Conversely, if too short, a single event could mistakenly be interpreted as a collection of them. Under these considerations, the window-length should at least match the duration of the shortest event in the signal. However, it may be impossible to know this information beforehand, and some form of validation would be needed to find the best parameters. If the geometry and materials of the propagating medium are simple enough, some insight can be gained by simulating the potential events. For now, an initial guess will be made, and some robustness will be provided by: (1), overlapping the windows along the signal and, (2) the nonparametric mixture model.

The AE waveform shown in Figure 5 will be considered for this demonstration. This waveform corresponds to an AE time-series recorded from a journal bearing operating at $150rpm$ and under constant axial load of $5kN$. A step function with a length of $n = 1000$ sample points ($\Delta t = 0.001s$) was used for the windowing procedure. In each windowed section, the count was extracted by taking the number of times the signal was found to go over a pre-defined threshold. In this case, a 99^{th} percentile threshold was defined over the entire waveform. It is worth noting that, although a hard-threshold is established here, the probabilistic approach should alleviate the aforementioned shortcomings. A threshold crossing will no longer be assumed to be from an AE event; instead, a probability will quantify the (un)certainty of there being an AE event.

Having constructed the dataset, the DP-PMM was implemented to find a suitable partition of the extracted counts. A window overlap of 87.5% was used for this first demonstration. It will be shown how overlapping the window is an important step to improve the robustness of this method.

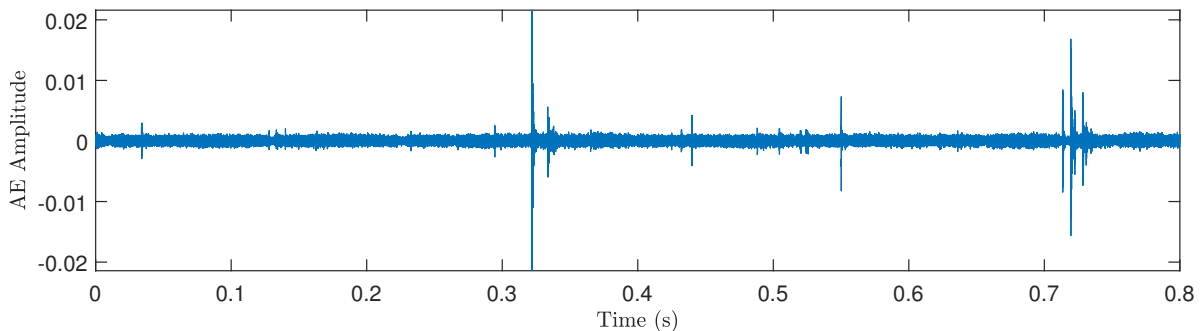


Figure 5: AE readings from a plain journal bearing operating under hydrodynamic lubrication at a rotational speed of $150rpm$ and applied static load of $5kN$.

4.1. Results and discussion

The assignments inferred by the proposed strategy are those as shown in Figure 6. Visually, it seems as if the main acoustic events were almost undoubtedly detected in all cases. These events were also detected with minimal intervention, since the number of groups changes as demanded by the observations.

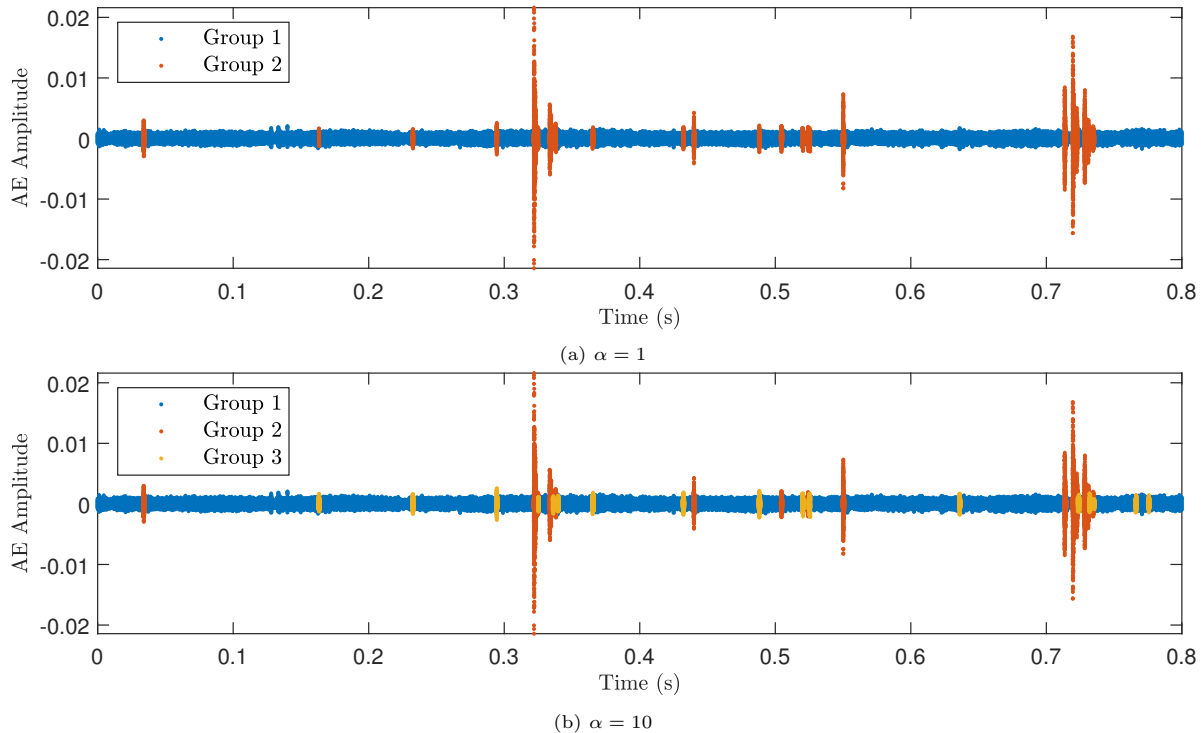


Figure 6: Arbitrary section from time-series after the model has categorised the AE events.

In this example, two different values of α were used. In the first case (6a), two distinct groups were identified by the model to differentiate the identified AE events. The first group, displayed in blue, is associated with the background noise. One can therefore discard all samples that belong to this group, as they may be of little interest for the health-state analysis. The remaining group, displayed in red, appears to distinguish the events of interest. The second case (6b), demonstrates the effect of increasing α to promote the formation of new groups. The results are shown Figure 6b, where now an additional group was generated to include the AE events characterised by lower amplitudes.

Having the AE events grouped in this way provides an organised benchmark from which one can proceed with the analysis. For example, only events from “Group 2” can be considered for extracting their individual features, such as amplitude, rise-time and energy (among others). This approach significantly reduces the dimensionality of the original dataset and encodes most of the information needed to diagnose the state of the structure or machine being monitored [17]. An emerging defect should affect these features to some extent, giving an anomaly detector an indication that the system has deviated from normal conditions. Alternatively, a new group could develop as damage becomes more prevalent, and one could then query

this new component and decide whether it arises from further damage. The nature of the DP-PPM in this context could allow for an online monitoring without having to initiate a new training period.

In the case of not overlapping the sliding window, some sections may indicate a high likelihood of there being an event, even when no clear excitation exists (or vice-versa). This effect can be observed in Figure 7a, where an arbitrary event from Figure 6 was singled out for this demonstration. In this scenario, a window length of $n = 200$ with an overlap of 87.5% was used. The results show that the section preceding the actual event is assigned to “Group 1”. Most of this section is in fact attributed to noise, but an initial portion of the event is captured at the end-edge of the window. On average, the number of counts decreases because of this window “offset”, misleading the model into assigning this section incorrectly. It would have been better for the model to assign this section to “Group 2”, so that no information of the actual event was lost.

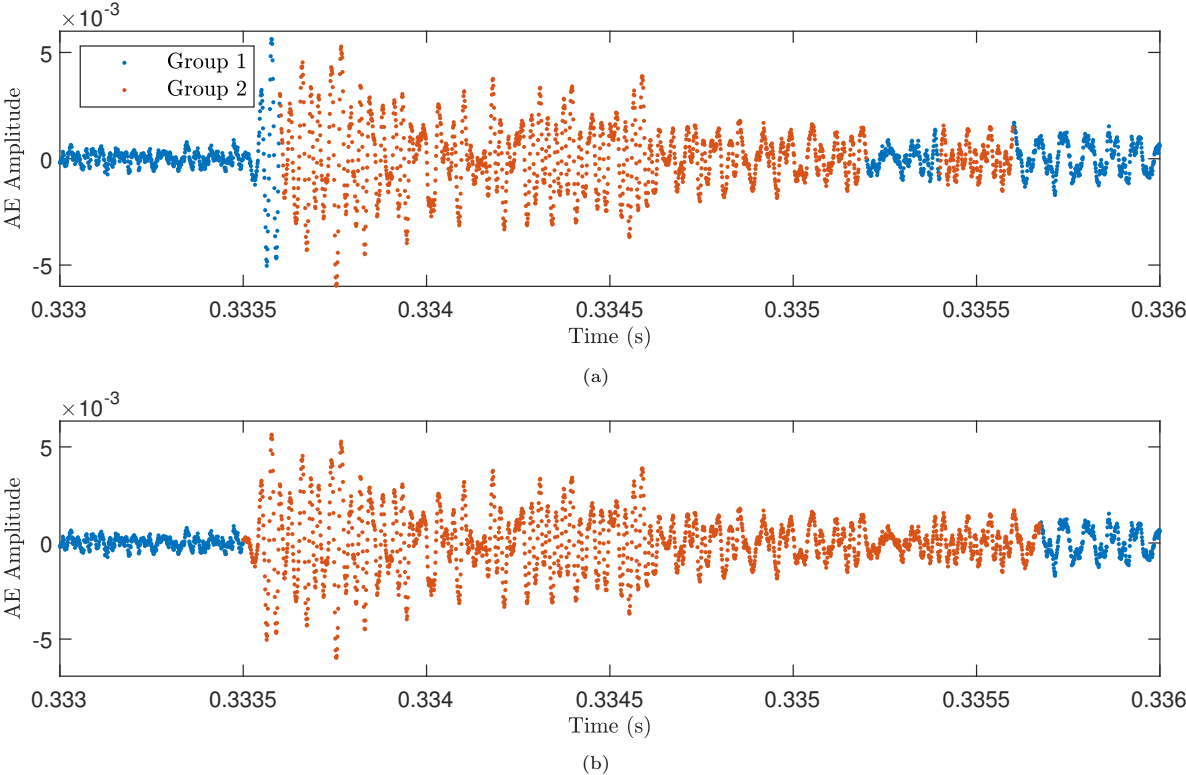


Figure 7: Arbitrary AE event from waveform shown in Figure 6. The results demonstrate the robustness of the model when: (a) no overlapping is used, and (b) a 87.5% overlap is used for the sliding step-window.

This undesired effect is a consequence of using a fixed window size moving through the signal without overlapping. Iterating the model by varying the offset of the sliding window allows for all existing events to be, at least once, somewhat aligned to the window. By overlapping the sliding window, the assignment likelihood can be evaluated for each constructed dataset and then averaged to decide upon the component associated with each section.

The results of averaging the likelihoods after overlapping the sliding window for count extraction can be seen in Figure 7b. Following this approach makes the model more robust to the window length, provided

that the overlapped portion, N_w , is large enough, and that the window slides in steps of length $(1 - N_w)$.

An interesting consequence of averaging the assignment likelihood can be observed in Figure 8. The colour-bar represents the probability of a section being assigned to “Group 2”. After normalising the averaged likelihoods, an arbitrary AE event from the example shown in Figure 6b was singled-out for this additional demonstration. The assignment-probability experiences gradual changes as the AE event develops and decays. So far, the presented results have only displayed the labels of the assigned sections, and are hence limited to visualising the group to which each data point is most likely to belong. Some progress in validating the effectiveness of this method can be achieved by instead considering the individual cluster-assignment probabilities. One can now determine the points where the AE event may begin and end by considering the region in which the probabilities are above a given minimum. Additionally, this model provides a quantifiable measure of confidence in assigning the windowed sections. Therefore, one also has the flexibility to evaluate the risk of choosing the necessary events based on their assignment-probabilities.

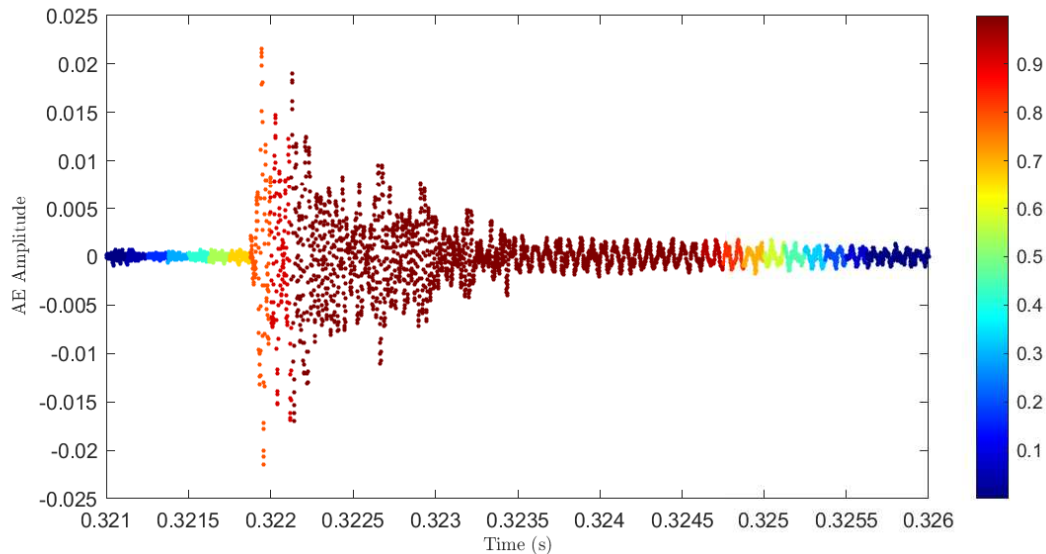


Figure 8: Arbitrary AE event displaying the probability of being assigned to Group Two.

5. Application to landing gear

Identifying AE events in a signal is an important pre-processing step when performing this type of AE-based monitoring. As demonstrated in the previous section, a probabilistic approach may offer several advantages over traditional methods in the identification and extraction of AE events, and with the added flexibility of the mixture model, the DP-PMM may be an effective alternative for managing what can be an overwhelming dataset.

An additional application of the DP-PMM in SHM is explored in this section. The experimental study under consideration is the fatigue testing of a 300M steel lug welded on an *Airbus A320* main fitting. This

study corresponds to one of a series of projects conducted by *The University of Cardiff* in collaboration with *The University of Sheffield*, and under the support of *Messier-Dowty Ltd*. The series of experiments carried out investigated the use of AE techniques for the detection and localisation of fractures in certified landing gears under fatigue testing.

5.1. Experimental method

The dataset explored here is an extensive collection of AE waveforms recorded throughout the fatigue test. A loading arm attached to the lug was used to transmit a cyclic load at a rate of $1Hz$ and with a peak amplitude of $5.5kN$. The load was later increased to $6kN$, $6.5kN$ and $7kN$ after 90,000 cycles, 110,000 cycles and 138,500 cycles, respectively. Gradually increasing the load was necessary to promote crack-growth, eventually leading to rupture after 160,000 cycles (200,000s). The test was made more “realistic” by also exciting the sliding tube of the main fitting, periodically at a rate of $0.4Hz$. The added contribution of the sliding tube was included to promote the generation of benign AE events, as would be expected outside laboratory conditions.

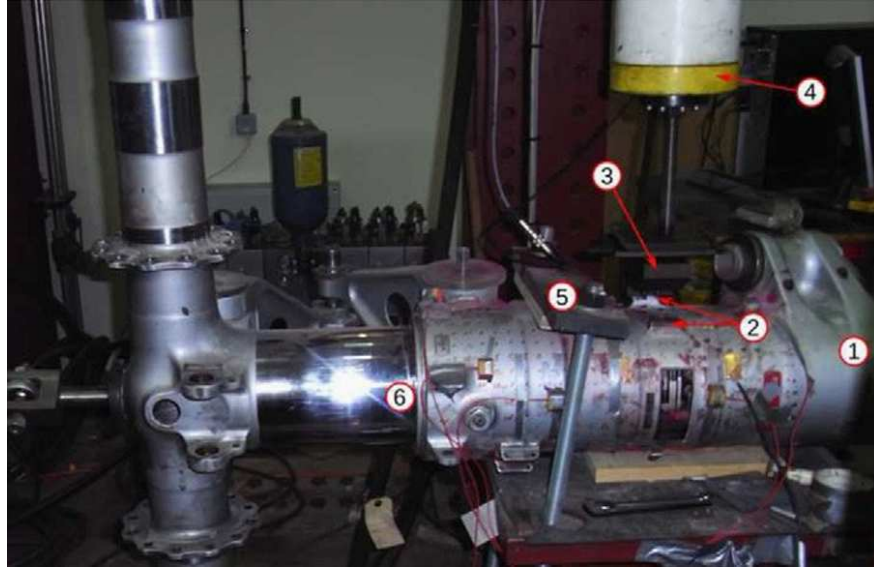
This dataset has been analysed before in [15], where spatial-scanning statistics were used to detect and localise the source of damage in the landing gear. In the following, the analysis will be limited to the early identification of damage, and how the implementation of nonparametric probabilistic techniques can aid in this task.

The main fitting was mounted with eight *Physical Acoustics Limited (PAL) Nano 30* sensors around the cylindrical part of the landing gear (Figure 9a). All sensors were attached to the structure with magnetic-clamps, and brown-grease was used as an acoustic-couplant. Using a *PALPCI – 2* acquisition system, the measured data were recorded at a sampling rate of $2MHz$. Fixed-size windows of 2048 samples were recorded upon the signal crossing a pre-established threshold of $43dB$. A memory buffer remained active to include 500 sample-points before the trigger event of each waveform.

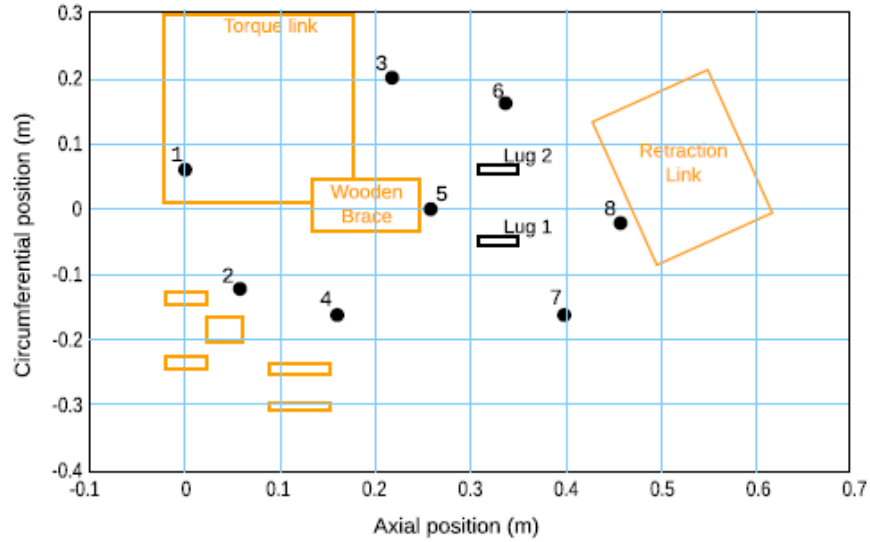
5.2. Feature selection

From the sensor-arrangement presented in Figure 9b, only the waveforms recorded from Channel Five were used in this analysis, given that the corresponding sensor was the one placed nearest to the lug subjected to the fatigue load. For the duration of the fatigue test, this sensor accounted for a total of 755,193 recorded waveforms. Handling this amount of data quickly became a complication, and it was necessary to extract features from the recorded waves in order to proceed with the analysis.

Following the same reasoning as in the previous case study, the counts of each waveform were extracted and used as features for the analysis. In particular, a feature-vector $X = \{x_1, \dots, x_N\}$ representing the N extracted counts was constructed for the development of the damage-detection algorithm. Figure 10a shows the evolution of the counts as the waveforms were recorded during the fatigue test. The dataset is rich in information, and it is not all that clear whether an obvious pattern exists that could indicate a form of fracture emerging and evolving until failure. This is also the case when observing the energy of the recorded



(a)



(b)

Figure 9: (a) Experimental set-up and (b) sensor arrangement (red dots) (from [15]). The main landing-gear fitting (1), can be seen to be comprised of the lugs (2), loading arm (3), load actuator (4), restraining wooden brace (5), and a sliding tube (6).

waveforms, as shown in Figure 10b. Nevertheless, some peaks are observed more frequently towards the end of the test, suggesting that a more elaborate monitoring mechanism could anticipate failure and warn an operator of the urgency for an inspection of the affected part.

An important step worth mentioning here is on dye-penetrant visual inspections that were carried out periodically throughout the experiment. The outcome of each visual inspection is represented by the colour of the dashed vertical lines included in the figures, where: (1) blue is for no evident fracture, (2) yellow is for possible fracture, and (3) red is for a confirmed surface fracture. Carrying out this simple step adds special value to this dataset, since it gives one means to validate the performance of a novelty detector.

That is, the monitoring system should be expected to flag an abnormal operation prior to the first “possible fracture” given by the visual inspection. The green lines here indicate the instances when the applied load was increased.

In an ideal scenario, where background AE activity is almost non-existent, a sudden up-turn in energy should indicate anomalous activity, likely to have been caused by crack nucleation or growth. However, as demonstrated in this case, it is in fact difficult to discern any clear patterns in the dataset that can reliably indicate the presence of damage. The small load contribution administered by the sliding tube proves to have a substantial effect on the overall AE activity. Figures 10a and 10b are clear examples on how overwhelming AE datasets can get in practice.

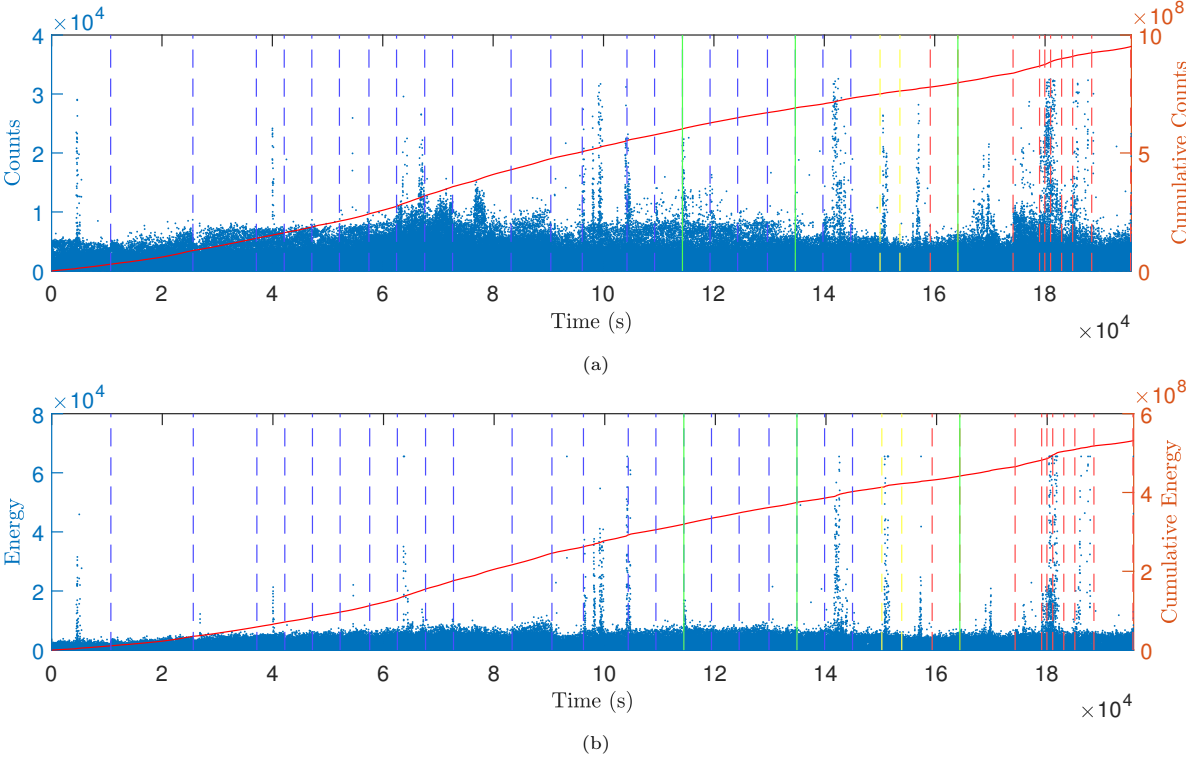


Figure 10: Experimental results: (a) AE counts and (b) AE energy.

The idea here is to have the DP-PMM cluster the waveforms by their counts. It is assumed that count-rates corresponding to anomalous AE events will somewhat deviate from those corresponding to benign events. By clustering the AE events, closer attention can be paid to the inferred clusters that are characterised by the growth and development of fracture. Other features from these clusters, such as energy, can then be monitored to determine the health-state of the lug.

5.3. Online monitoring strategy

Using a collapsed Gibbs sampler to infer the cluster assignment has the advantage of evaluating each sample-point marginally. The implication of this advantage is that the model can adapt in real time as new sample-points are introduced, allowing for an online monitoring approach. However, as the dataset grows

with the addition of new sample-points, inference becomes increasingly slower, to the point where inferring the posterior likelihood takes longer than the rate at which new observations are introduced. This drawback comes from having to reassess the assignment of every sample-point on each iteration of the Gibbs sampler. For now, to circumvent this problem, the proposed solutions were to: (1) reduce the dataset to a manageable size, and (2) to resample the assignments of all current observations only in instances where the model appears to be the most uncertain on the assignment of a new observation.

The former solution involved reducing the dataset to 10% of its size by approximately retaining one waveform recorded every 2.6 seconds. An associated risk exists from potentially neglecting waveforms derived from structural damage, making this an important parameter to manage for this type of application. In this case, a reasonable balance between time of computation and quality of results was achieved.

Deciding on when to resample the assignment of all observations can be determined based on the entropy of the posterior distribution over the labels,

$$\mathbb{H}(p(z_n|X^{-n}, \mathbf{Z}^{-n})) = - \sum_{k=1}^{K+1} p(z_n|X^{-n}, \mathbf{Z}^{-n}) \log(p(z_n|X^{-n}, \mathbf{Z}^{-n})) \quad (21)$$

The result of computing the entropy of the posterior likelihood, when presented with a new observation, is a quantification of how “confused” the model is at deciding its assignment to any of the existing K non-empty components, characterised by previously-observed conditions; or to a $K + 1$ empty component for a condition that has not yet been observed. Introducing this step in the clustering algorithm helps reduce the number of iterations required by the Gibbs sampler to infer the posterior distribution; that is, it works on the assumption that if the model is certain of the assignment of an arbitrary observation, then it may not be necessary to resample all the previous assignments. In practice, it is more convenient to normalise the entropy by defining the information efficiency [40],

$$\eta(x_n) = \frac{\mathbb{H}(p(z_n|X^{-n}, \mathbf{Z}^{-n}))}{\log(K + 1)} \quad (22)$$

where (22) yields a value between zero and one, and can be viewed as an approximation of how likely an additional sweep of the Gibbs sampler will improve the model. In this way, a sample from a uniform distribution $a \sim U(0, 1)$ can be drawn and compared against $\eta(x_n)$; if a is less than $\eta(x_n)$, then the whole dataset is reassessed, otherwise the new sample-point x_n is assigned to the component returning the highest likelihood. This approach is based on that followed in [41], where a constrained DP-based model is constructed in a semi-supervised monitoring scheme, and the information efficiency is used to determine when to inspect the condition of a given measurement. Here, the configuration is unsupervised, and class labels are not required for the assignment of a sample-point to a cluster; this is a convenient property, since one is not required to know *a-priori* all the sources of AE that may exist in the system. However, it may be required to query the formed clusters to identify those that are characterised by events deriving from damage.

5.4. Damage-detection strategy

There are different ways in which this method can be used for novelty detection. A simple mechanism could involve having the DP-based model trigger an alarm upon the formation of a new cluster. This approach would require having the model learn from a training set in which it is known that the structure is operating normally. During the training process, several clusters would form to account for the normal operation of the structure subjected to Environmental and/or operational Variations (EoVs), and any new clusters forming after the training phase would suggest an anomalous behaviour that has not yet been observed.

One immediate complication of this approach is that the formation of new clusters may not necessarily be a direct consequence of some change occurring to the physical system, and it may instead be attributed to the stochastic nature of the sampler when inferring the number of non-empty components [42]. At each iteration, when the assignment of a sample-point is resampled, a finite probability of forming a new cluster exists, and the number of non-empty components may briefly grow as a result. These sporadic components may attract one or two members, but chances are that they will collapse again after a few iterations of the sampler. In practice, the new formation of clusters may only be an indicator of anomalous behaviour if the clusters survive to account for future observations. A possibly sensible alternative could be to instead monitor the rate at which the number of members from each component grows over time.

Cluster growth-rate can be a more robust indicator of damage, by working on the assumption that the generation of benign AE events will be steady. This assumption may hold since the cyclic load applied by the sliding tube remained unchanged for the duration of the experiment, and no additional inputs were introduced. Unless subjected to unforeseen variations, any clusters formed to characterise the benign AE events should therefore sustain a somewhat constant growth-rate. In contrast, a sudden release of energy caused by fracture will not only result in the additional formation of clusters, but also in a more inconsistent growth-rate of these, since AE events of this type will likely occur sporadically with the progression of the original fracture, or from the generation of new fractures in the structure.

5.5. Results and discussion

Following the strategy described above, the DP-based model clustered the recorded AE waveforms as shown in Figure 11. The dashed vertical lines indicate the moment when a new cluster was created. A different colour was used to represent each cluster and their corresponding members. The dataset was eventually split into $K = 48$ different non-empty components, by setting $\alpha = 1$.

One of the first observations that can be made from the results presented in Figure 11, is on the rate at which new clusters appeared. At the beginning of the fatigue test, the model was exposed (for the first time), to a vast number of AE events defined by a variety of different features. It is therefore natural to expect most clusters being created at the start, when the model is learning to identify and group the AE events as they are being introduced. Most of the first-appearing clusters are likely to correspond to the benign generating mechanisms attributed to the friction introduced by the sliding tube. Some higher-energy events can also be observed occurring somewhat early in the test, also triggering the creation of new clusters.

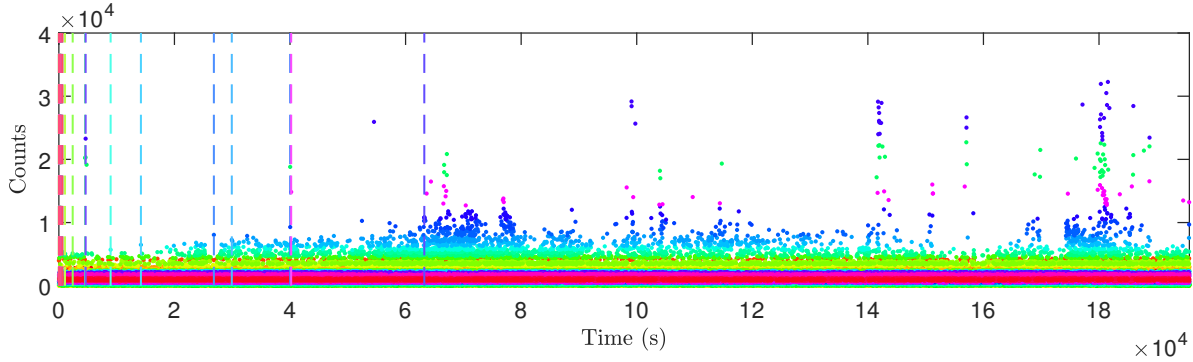


Figure 11: AE counts clusters inferred by the DP-PMM.

Although these high-energy clusters could relate to the first indications of crack initiation, they may also be a result of internal fractures already existing prior to the start of the fatigue test. A point not yet mentioned, is that the lug had previously been fractured from preceding fatigue tests, and then repaired by welding it back in its original place. The sudden release of the internal stresses induced by the weld could have justifiably been a source of AE events exhibiting high counts. It is, unfortunately, impossible to know for sure the sources of all the observed events, as they could have also been generated from a variety of other mechanisms, such as material plastification, crack closure and crack-face rubbing [43], among others.

Nonetheless, some consolation can be found by recalling that AE events deriving from crack nucleation and propagation will tend to exhibit a higher energy content (and counts), than those from any other potential mechanism in this setting. As reviewed in Section 1, the characterisation of AE events in fatigue tests is a subject that has been thoroughly examined in the literature, and on the basis of this consideration, one can therefore simplify the monitoring scheme by only looking at clusters that are characterised by the highest count-rates.

Something that may be worth noting from the results, is the very last cluster being created only after 60,000s. This was somewhat of a surprising outcome, since a steady increase in the count-rate was expected to occur with the integrity of the structure declining over time, leading to the creation of new clusters throughout the whole duration of the test. Contrary to this belief, it seems as if the count-rate converged early on to a maximum value of around 30,000. That is, no evident development of this feature was observed after the last cluster was created. A similar behaviour can also be observed in Figure 10b, where a somewhat unnatural maximum limit appears to prevent the energy of emitted AE events going above a value of 65,535.

Upon inspection, it was discovered that the extracted counts were limited by the fixed window-length (i.e. 2048 samples), chosen for recording the identified AE events. It was possible that the recording length was at times shorter than the actual duration of the emitted AE events, thus neglecting portions of the signal that could have accounted for the true count-rates characterising the progression of damage. This outcome is a clear demonstration of the challenges faced when deciding on the correct parameters in AE-based monitoring applications. A longer window length, or the implementation of the probabilistic approach presented in

Section 4.1, could have potentially avoided this problem, and might be solutions worth considering in future fatigue tests of this type.

The limitation imposed by establishing a short window-length makes it difficult to track the development of fracture in the lug. Consequently, the DP-PMM can no longer be used to determine instances when it might be necessary to inspect the landing gear, since new clusters cannot be expected to appear at later stages of its lifespan. Fortunately, this shortcoming can be alleviated by instead monitoring the growth-rate of the existing clusters.

Figure 12 shows the cumulative sum of events corresponding to each of the identified clusters. The number of events were accumulated in this way to help visualise the growth-rate of the clusters throughout the test. Figure 12 also shows the cumulative sum of counts. In both cases, a somewhat steady growth can be observed in almost all clusters, with a few exceptions exhibiting noticeable step increases. Since benign AE events are expected to emerge at a continuous rate, irrespective of the health-state of the lug, it may be reasonable to assume that clusters representing background activity are those that show a steady growth in Figure 12. Conversely, high-energy bursts manifesting from the growing crack are expected to be represented by the sudden step increases exhibited by some of these patterns.

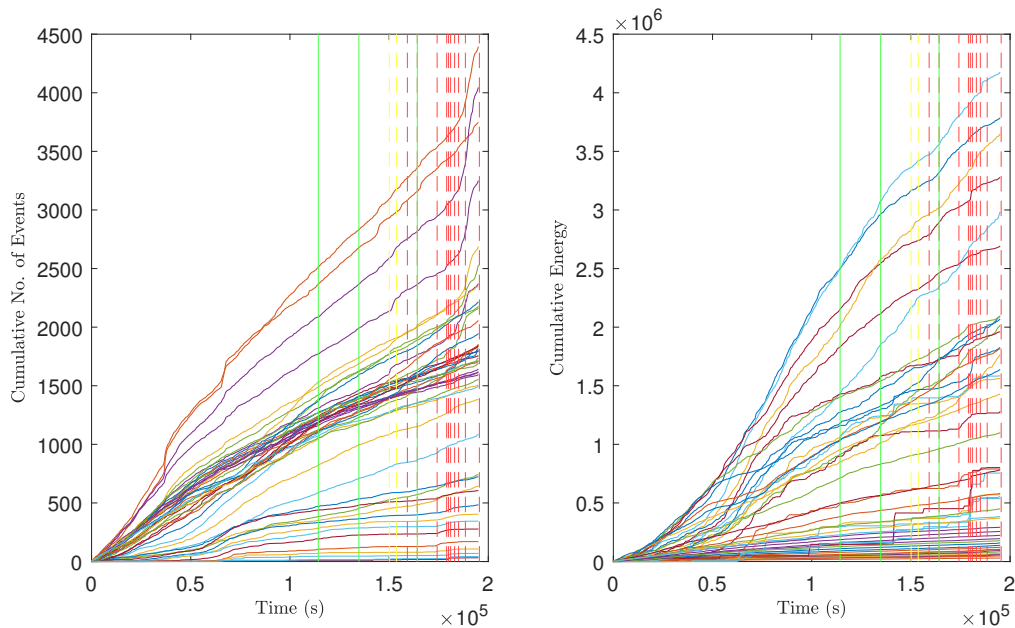


Figure 12: Cumulative number events (left) and cumulative energy (right) of all inferred groups.

The clusters exhibiting these sharp up-turns were therefore extracted and inspected in isolation. The energy rate of the 20th, 27th, 35th and 41st clusters can be observed in Figure 13. These four clusters are in fact characterised by the AE events with the highest count-rates, and their selection was based on this parameter. The results now clearly show energy peaks happening sporadically, with sharp up-turns manifesting throughout the duration of the experiment. By removing the background AE activity, the data

become clearer and easier to interpret. Additionally, the size of the dataset is drastically reduced, and only the AE-waves of interest are retained, making it suitable for the development of a robust monitoring system.

Visually, one can see peaks manifesting moments before the visual inspection indicated a possible presence of fracture, where a first warning is provided in advance at 60,000s, and the last by the prominent step increase occurring at approximately 140,000s into the experiment; specially when looking at the collection of waves corresponding to the 35th cluster. The observed peak in this scenario may be interpreted as an indication of fracture extending to a detrimental length, and this form of warning is provided early enough for an operator to intervene and have the landing-gear inspected for damage.

The advantage of this approach is that the early presence of damage could be detected without needing to resort to source-localisation techniques, which can be cumbersome to implement, and require at least three sensors to be placed within the propagating medium of the generated waves. Here, only a single sensor was needed, and although the collected data from this sensor alone were very rich, the processing strategies presented in this work appear to be enough to have the model successfully flag an abnormal event in both real time and without having to perform an invasive procedure. Unfortunately, there is no way to characterise the sources of AE in this configuration, but the assumptions made here appear to satisfy the identification of AE-waves that were more sensitive to damage.

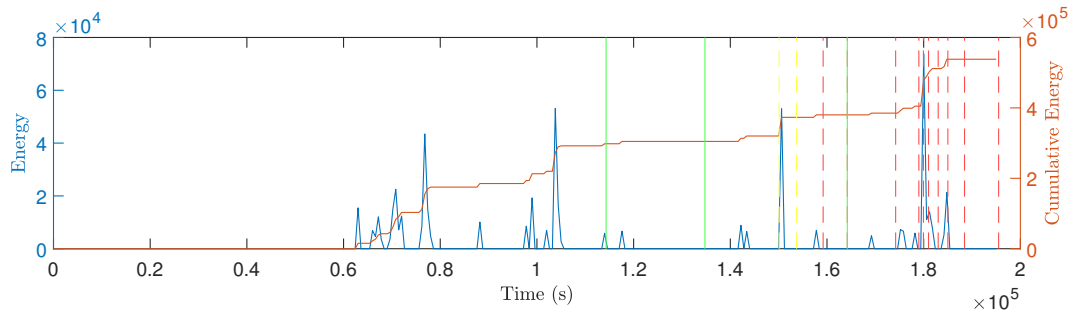
6. Conclusions and Future Work

The approach presented in this work demonstrated promising results in the probabilistic detection of AE events in time-series signals. Challenges associated with pre-defining an arbitrary hard-threshold were addressed. In the presented method, threshold-crossings in a given time window are no longer assumed to indicate, with absolute certainty, the existence of an AE event. Instead, the number of threshold-crossings given in a time window is treated as a random sample, which is then used to infer a probability of an event existing in that time window.

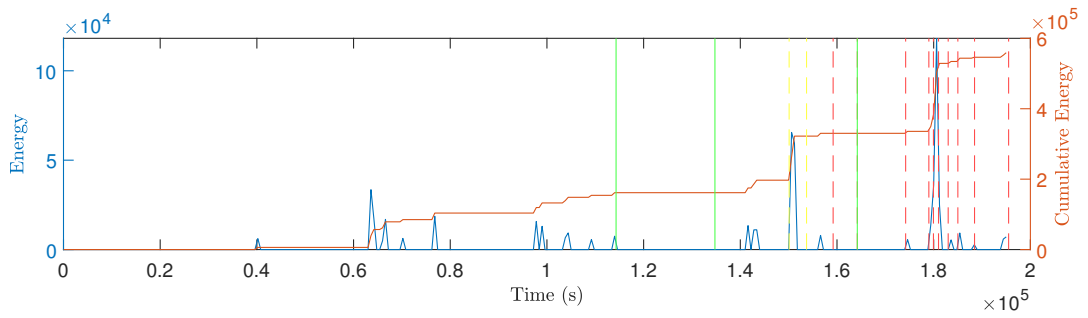
Secondly, the proposed methodology gives some insight into scenarios where the nature of the AE activity is unknown, by not only detecting but also categorising all the observable events. Some form of validation would still be required to ensure that the window length, overlapped portion and hyperparameters are optimal. However, a validation procedure may be achieved by using the inferred assignment-probabilities. This consideration may be pursued in the future.

Given the probabilistic framework of the model, when an event is identified, a degree of (un)certainly on its assignment is provided. An operator could therefore decide to retain those AE events categorised with high certainty, after establishing a minimum criterion that is suitable for the application at hand.

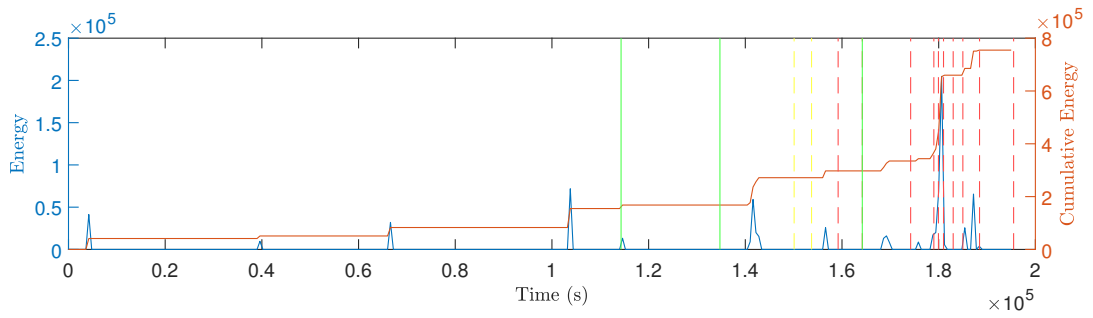
Finally, the promising capabilities of the DP-PMM in AE-based monitoring methods were explored further with experimental data gathered from a fatigue test of a landing gear. The implementation of the DP-PMM helped simplify the interpretation of an overwhelming dataset, allowing one to identify the groups of AE events that were more sensitive to damage, and therefore detect the early onset of fracture in the



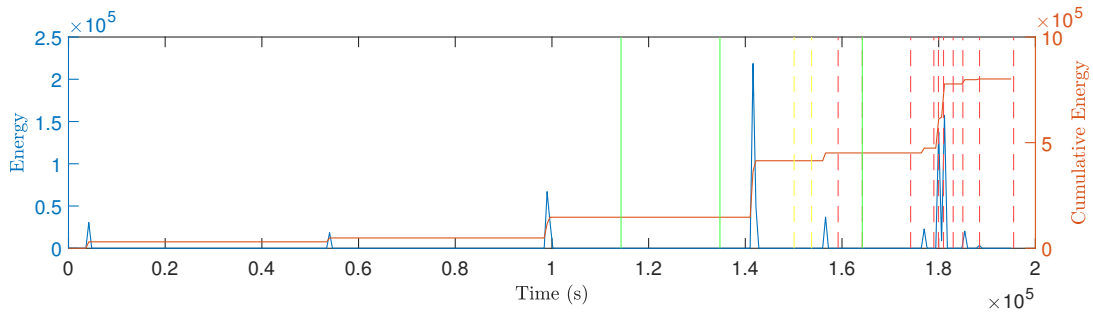
(a) Cluster No. 34



(b) Cluster No. 41



(c) Cluster No. 20



(d) Cluster No. 35

Figure 13: Energy rate corresponding to individual clusters 34, 41, 20 and 35, from top to bottom.

structure. Although this method yielded a successful outcome for this case study, exploring how well the DP-PMM generalises when faced in different applications is an exercise worth pursuing in the future.

Acknowledgements

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Appendix A. Derivation of $p(z_{nk} = 1 | \mathbf{Z}^{-n}, \mathbf{X}^{-n}, \boldsymbol{\alpha}, \mathbf{a}, \mathbf{b})$

Given the joint distribution defined by equation (10), it is possible to derive the conditional distributions over \mathbf{z}_n , $\boldsymbol{\pi}$ and $\boldsymbol{\lambda}$. A conventional Gibbs sampler could then be employed to infer the joint distribution over these parameters. However, in this case, the probability distribution of interest is that defined over \mathbf{z}_n , conditioned on all other parameters. The motivation to derive an expression for $p(\mathbf{z}_n | \dots)$ begins by marginalising $\boldsymbol{\pi}$ and $\boldsymbol{\lambda}$ out of equation (10). If $\boldsymbol{\pi}$ is first considered, then one can approach the marginalisation process in a two-step decomposition, where sampling from $p(\mathbf{z}_n, \boldsymbol{\pi})$ is said to be equivalent to drawing a sample of $\boldsymbol{\pi}$ first, and then using this sample to draw \mathbf{z}_n . That is,

$$\begin{aligned} p(\mathbf{z}_n, \boldsymbol{\pi} | \mathbf{Z}^{-n}, \boldsymbol{\lambda}, \boldsymbol{\alpha}, x_n) &\propto p(\mathbf{z}_n | \boldsymbol{\pi}, x_n, \boldsymbol{\lambda}) p(\boldsymbol{\pi} | \mathbf{Z}^{-n}, \boldsymbol{\alpha}) \\ &\propto \prod_{k=1}^K [\pi_k p(x_n | \lambda_k)]^{z_{nk}} p(\boldsymbol{\pi} | \mathbf{Z}^{-n}, \boldsymbol{\alpha}) \end{aligned}$$

Here, \mathbf{Z}^{-n} is the set of all assignments except the n^{th} one. The notation of this expression can then be simplified by instead considering the value where the k^{th} element of \mathbf{z}_n is equal to unity,

$$\begin{aligned} p(z_{nk} = 1, \boldsymbol{\pi} | \mathbf{Z}^{-n}, \boldsymbol{\lambda}, \boldsymbol{\alpha}, x_n) &\propto \pi_k p(x_n | \lambda_k) p(\boldsymbol{\pi} | \mathbf{Z}^{-n}, \boldsymbol{\alpha}) \\ &\propto p(z_{nk} = 1 | \boldsymbol{\pi}) p(x_n | \lambda_k) p(\boldsymbol{\pi} | \mathbf{Z}^{-n}, \boldsymbol{\alpha}) \end{aligned}$$

In this form, it becomes possible to marginalise $\boldsymbol{\pi}$ out,

$$\begin{aligned} p(z_{nk} = 1 | \mathbf{Z}^{-n}, \boldsymbol{\lambda}, \boldsymbol{\alpha}, x_n) &\propto \int p(z_{nk} = 1 | \boldsymbol{\pi}) p(x_n | \lambda_k) p(\boldsymbol{\pi} | \mathbf{Z}^{-n}, \boldsymbol{\alpha}) d\boldsymbol{\pi} \\ &\propto p(x_n | \lambda_k) \int p(z_{nk} = 1 | \boldsymbol{\pi}) p(\boldsymbol{\pi} | \mathbf{Z}^{-n}, \boldsymbol{\alpha}) d\boldsymbol{\pi} \\ &\propto p(x_n | \lambda_k) p(z_{nk} = 1 | \mathbf{Z}^{-n}, \boldsymbol{\alpha}) \end{aligned}$$

where,

$$p(z_{nk} = 1 | \mathbf{Z}^{-n}, \boldsymbol{\alpha}) = \int p(z_{nk} = 1 | \boldsymbol{\pi}) p(\boldsymbol{\pi} | \mathbf{Z}^{-n}, \boldsymbol{\alpha}) d\boldsymbol{\pi}$$

and the posterior, $p(\boldsymbol{\pi}|\mathbf{Z}^{-n}, \boldsymbol{\alpha})$, is the result of having a Dirichlet prior, $p(\boldsymbol{\pi}|\boldsymbol{\alpha})$, as the conjugate of the multinomial likelihood, $p(\mathbf{Z}^{-n}|\boldsymbol{\pi})$. Concretely,

$$p(\boldsymbol{\pi}|\mathbf{Z}^{-n}, \boldsymbol{\alpha}) \propto \prod_{k=1}^K \pi_k^{\beta_k-1}, \quad \beta_k = \alpha_k + c_k^{-n}$$

where c_k^{-n} is the number of objects assigned to the k^{th} group, excluding the assignment on x_n . Hence,

$$\begin{aligned} p(z_{nk} = 1|\mathbf{Z}^{-n}, \boldsymbol{\alpha}) &= \frac{\Gamma(\sum_{j=1}^K \beta_j)}{\prod_{j=1}^K \Gamma(\beta_j)} \int \pi_k \prod_{j=1}^K \pi_j^{\beta_j-1} d\boldsymbol{\pi} \\ &= \frac{\Gamma(\sum_{j=1}^K \beta_j)}{\prod_{j=1}^K \Gamma(\beta_j)} \int \prod_{j=1}^K \pi_j^{\beta_j+\delta_{jk}-1} d\boldsymbol{\pi} \\ &= \frac{\Gamma(\sum_{j=1}^K \beta_j)}{\prod_{j=1}^K \Gamma(\beta_j)} \frac{\prod_{j=1}^K \Gamma(\beta_j + \delta_{jk})}{\Gamma(\sum_{j=1}^K (\beta_j + \delta_{jk}))} \end{aligned}$$

where $\delta_{jk} = 1$ when $j = k$, and zero otherwise. Since $\sum_{j=1}^K \delta_{jk} = 1$,

$$\begin{aligned} p(z_{nk} = 1|\mathbf{Z}^{-n}, \boldsymbol{\alpha}) &= \frac{\Gamma(\sum_{j=1}^K \beta_j)}{\prod_{j=1}^K \Gamma(\beta_j)} \frac{\prod_{j=1}^K \Gamma(\beta_j + \delta_{jk})}{\Gamma(\sum_{j=1}^K \beta_j + 1)} \\ &= \frac{\beta_k}{\sum_{j=1}^K \beta_j} \end{aligned}$$

Now, because $\beta_k = c_k^{-n} + \alpha_k$,

$$p(z_{nk} = 1|\mathbf{Z}^{-n}, \boldsymbol{\alpha}) = \frac{c_k^{-n} + \alpha_k}{\sum_{j=1}^K c_j^{-n} + \alpha_j}$$

Following the same reasoning, it is also possible to collapse λ_k from the sampler. The joint density over $z_{nk} = 1$ and λ_k is derived by carrying out an equivalent two-step decomposition,

$$p(z_{nk} = 1, \lambda_k|\mathbf{Z}^{-n}, X^{-n}, \boldsymbol{\alpha}, a, b) \propto p(z_{nk} = 1|\mathbf{Z}^{-n}, \boldsymbol{\alpha})p(x_n|\lambda_k)p(\lambda_k|\mathbf{Z}^{-n}, X^{-n}, a, b)$$

where X^{-n} corresponds to all objects except for x_n . Marginalising λ_k out from this expression gives,

$$\begin{aligned} p(z_{nk} = 1|\mathbf{Z}^{-n}, X^{-n}, \boldsymbol{\alpha}, a, b) &\propto \int p(z_{nk} = 1|\mathbf{Z}^{-n}, \boldsymbol{\alpha})p(x_n|\lambda_k)p(\lambda_k|\mathbf{Z}^{-n}, X^{-n}, a, b) d\lambda_k \\ &\propto p(z_{nk} = 1|\mathbf{Z}^{-n}, \boldsymbol{\alpha}) \int p(x_n|\lambda_k)p(\lambda_k|\mathbf{Z}^{-n}, X^{-n}, a, b) d\lambda_k \\ &\propto p(z_{nk} = 1|\mathbf{Z}^{-n}, \boldsymbol{\alpha})p(x_n|\mathbf{Z}^{-n}, X^{-n}, a, b) \end{aligned}$$

where,

$$p(x_n|\mathbf{Z}^{-n}, X^{-n}, a, b) = \int p(x_n|\lambda_k)p(\lambda_k|\mathbf{Z}^{-n}, X^{-n}, a, b) d\lambda_k$$

and, like in the previous case, the posterior, $p(\lambda|\mathbf{Z}^{-n}, X^{-n}, a, b)$, is the result of having a Gamma prior $p(\lambda_k|a, b)$, as conjugate of the Poisson likelihood, $p(X^{-n}|\lambda_k, \mathbf{Z}^{-n})$. Concretely,

$$p(\lambda_k|\mathbf{Z}^{-n}, X^{-n}, a, b) \propto \lambda_k^{\delta-1} e^{-\gamma\lambda_k},$$

$$\delta = a + \sum_{m \neq n} z_{mk} x_m, \quad \gamma = \sum_{m \neq n} z_{mk} + b$$

Hence,

$$\begin{aligned} p(x_n | \mathbf{Z}^{-n}, X^{-n}, a, b) &= \frac{\gamma^\delta}{x_n! \Gamma(\delta)} \int \lambda_k^{(x_n + \delta) - 1} e^{-(\gamma + 1)\lambda_k} d\lambda_k \\ &= \frac{\gamma^\delta}{x_n! \Gamma(\delta)} \frac{\Gamma(x_n + \delta)}{(1 + \gamma)^{(x_n + \delta)}} \end{aligned}$$

Re-arranging and having $r = \delta$ and $p = \gamma / (\gamma + 1)$,

$$\begin{aligned} p(x_n | \mathbf{Z}^{-n}, X^{-n}, a, b) &= \frac{\Gamma(x_n + r)}{x_n! \Gamma(r)} \frac{\left(\frac{p}{1-p}\right)^r}{\left(1 + \frac{p}{1-p}\right)^{(x_n + r)}} \\ &= \frac{\Gamma(x_n + r)}{x_n! \Gamma(r)} p^r (1-p)^r \\ &= NB(r, p) \end{aligned}$$

Finally,

$$p(z_{nk} = 1 | \mathbf{Z}^{-n}, X^{-n}, \boldsymbol{\alpha}, a, b) \propto \frac{c_k^{-n} + \alpha_k}{\sum_j^K c_j^{-n} + \alpha_j} p(x_n | \mathbf{Z}^{-n}, X^{-n}, a, b)$$

References

- [1] J. Kaiser. *An investigation on the occurrence of noises in tensile tests or a study of acoustic phenomena in tensile tests*. PhD thesis, Tech Hochsch, 1950.
- [2] J. Hanchi and B.E. Klamecki. Acoustic emission monitoring of the wear process. *Wear*, 145(1):1–27, 1991.
- [3] Y. Fan, F. Gu, and A. Ball. Modelling acoustic emissions generated by sliding friction. *Wear*, 268:811–815, 02 2010.
- [4] A. Hase, H. Mishina, and M. Wada. Correlation between features of acoustic emission signals and mechanical wear mechanisms. *Wear*, 292-293:144–150, 2012.
- [5] C.J. Hellier. *Handbook of Nondestructive Evaluation*. McGraw-Hill Education, 2013.
- [6] P. Feng, P. Borghesani, W.A Smith, R.B. Randall, and Z. Peng. A review on the relationships between acoustic emission, friction and wear in mechanical systems. *Applied Mechanics Reviews*, 72(2), 10 2019.
- [7] J. Ma, H. Zhang, Z. Shi, F. Chu, F. Gu, and A.D. Ball. Modelling acoustic emissions induced by dynamic fluid-asperity shearing in hydrodynamic lubrication regime. *Tribology International*, 153:106590, 2021.
- [8] A. Choudhury and N. Tandon. Application of acoustic emission technique for the detection of defects in rolling element bearings. *Tribology International*, 33(1):39–45, 2000.

- [9] Y. He, X. Zhang, and M. Friswell. Defect diagnosis for rolling element bearings using acoustic emission. *Journal of Vibration and Acoustics*, 131, 12 2009.
- [10] P. Feng, P. Borghesani, H. Chang, W.A. Smith, R.B. Randall, and Z. Peng. Monitoring gear surface degradation using cyclostationarity of acoustic emission. *Mechanical Systems and Signal Processing*, 131:199–221, 2019.
- [11] S. Poddar and N. Tandon. Detection of journal bearing vapour cavitation using vibration and acoustic emission techniques with the aid of oil film photography. *Tribology International*, 103:95–101, 2016.
- [12] S. Poddar and N. Tandon. Detection of particle contamination in journal bearing using acoustic emission and vibration monitoring techniques. *Tribology International*, 134:154–164, 2019.
- [13] C. Chen, X. Chen, and S. Guo. Experimental study on acoustic emission characteristic of fatigue crack growth of self-compacting concrete. *Structural Control and Health Monitoring*, 26(4):e2332, 2019.
- [14] K.M Holford, R. Pullin, S. Evans, M. Eaton, J. Hensman, and K. Worden. Acoustic emission for monitoring aircraft structures. *Proceedings of the Institution of Mechanical Engineers Part G Journal of Aerospace Engineering*, 223, 08 2009.
- [15] J. Hensman, K. Worden, M. Eaton, R. Pullin, K. Holford, and S. Evans. Spatial scanning for anomaly detection in acoustic emission testing of an aerospace structure. *Mechanical Systems and Signal Processing*, 25(7):2462–2474, 2011.
- [16] J.Z. Sikorska and D. Mba. Challenges and obstacles in the application of acoustic emission to process machinery. *Journal of Process Mechanical Engineering*, 222(1):1–19, 2008.
- [17] C.R. Farrar and K. Worden. *Structural Health Monitoring : a Machine Learning Perspective*. Wiley, 2013.
- [18] A. Terchi and Y.H.J. Au. Acoustic emission signal processing. *Measurement and Control*, 34(8):240–244, 2001.
- [19] T.M. Morton, R.M. Harrington, and J.G. Bjeletich. Acoustic emissions of fatigue crack growth. *Engineering Fracture Mechanics*, 5(3):691–697, 1973.
- [20] M.N. Bassim, S.St. Lawrence, and C.D. Liu. Detection of the onset of fatigue crack growth in rail steels using acoustic emission. *Engineering Fracture Mechanics*, 47(2):207–214, 1994.
- [21] A. Berkovits and D. Fang. Study of fatigue crack characteristics by acoustic emission. *Engineering Fracture Mechanics*, 51(3):401–416, 1995.
- [22] M. Rabiei, M. Modarres, and P. Hoffman. Structural integrity assessment using in-situ acoustic emission monitoring. *Proceedings of the Annual Conference of the Prognostics and Health Management Society*, 2014.

- [23] P. Paris and F. Erdogan. A critical analysis of crack propagation laws. *Journal of Basic Engineering*, 85(4):528–533, 12 1963.
- [24] V. Moorthy, T. Jayakumar, and Baldev Raj. Acoustic emission behaviour during stage II fatigue crack growth in an AISI type 316 austenitic stainless steel. *Bulletin of Materials Science*, 17(6):699–715, 1994.
- [25] S. Rippengill, K. Worden, K.M Holford, and R. Pullin. Automatic classification of acoustic emission patterns. *Strain*, 39(1):31–41, 2003.
- [26] M.G.R. Sause, A. Gribov, A.R. Unwin, and S. Horn. Pattern recognition approach to identify natural clusters of acoustic emission signals. *Pattern Recognition Letters*, 33(1):17–23, 2012.
- [27] Z. Bo, Z. Yanan, and C. Changzheng. Acoustic emission detection of fatigue cracks in wind turbine blades based on blind deconvolution separation. *Fatigue & Fracture of Engineering Materials & Structures*, 40(6):959–970, 2017.
- [28] J. Hensman, R. Pullin, M. Eaton, K. Worden, K.M Holford, and S.L. Evans. Detecting and identifying artificial acoustic emission signals in an industrial fatigue environment. *Measurement Science and Technology*, 20(4):045101, 2009.
- [29] J. Hensman, R. Mills, S.G. Pierce, K. Worden, and M. Eaton. Locating acoustic emission sources in complex structures using Gaussian processes. *Mechanical Systems and Signal Processing*, 24(1):211–223, 2010.
- [30] M.R. Jones, T.J. Rogers, K. Worden, and E.J. Cross. A Bayesian methodology for localising acoustic emission sources in complex structures. *Mechanical Systems and Signal Processing*, 163:108143, 2022.
- [31] K.P. Murphy. *Machine Learning: a Probabilistic Perspective*. MIT Press, 2013.
- [32] N.N. Hsu. Acoustic emission simulator, 1977. US Patent 4,018,084.
- [33] C.M. Bishop. *Pattern Recognition and Machine Learning*. Information Science and Statistics. Springer, 2006.
- [34] T.S. Ferguson. A Bayesian analysis of some nonparametric problems. *The Annals of Statistics*, 1(2):209 – 230, 1973.
- [35] C. Rasmussen. The infinite Gaussian mixture model. In *Advances in Neural Information Processing Systems*, volume 12, pages 554–560. MIT Press, 1999.
- [36] T.J. Rogers, K. Worden, R. Fuentes, N. Dervilis, U.T. Tygesen, and E.J. Cross. A Bayesian non-parametric clustering approach for semi-supervised structural health monitoring. *Mechanical Systems and Signal Processing*, 119:100–119, 2019.

- [37] C.T. Wickramarachchi, T.J. Rogers, T.E. McLeay, W. Leahy, and E.J. Cross. Online damage detection of cutting tools using Dirichlet process mixture models. *Mechanical Systems and Signal Processing*, 2022.
- [38] S. MacEachern. Estimating normal means with a conjugate style Dirichlet process prior. *Communications in Statistics - Simulation and Computation*, 23(3):727–741, 1994.
- [39] D.M. Blei and M.I. Jordan. Variational inference for Dirichlet process mixtures. *Bayesian Analysis*, 1(1):121 – 143, 2006.
- [40] D.J.C. MacKay. *Information Theory, Inference and Learning Algorithms*. Cambridge University Press, Cambridge, 2003.
- [41] L.A. Bull, N. Dervilis, K. Worden, E.J. Cross, and T.J. Rogers. A sampling-based approach for information-theoretic inspection management. *Proceedings of the Royal Society. A, Mathematical, Physical, and Engineering Sciences*, pages 20210790–20210790, 2022.
- [42] S. Rogers and M. Girolami. *A First Course in Machine Learning*. Chapman & Hall CRC, 2nd edition, 2016.
- [43] T.M. Roberts and M. Talebzadeh. Acoustic emission monitoring of fatigue crack propagation. *Journal of Constructional Steel Research*, pages 695–712, 2003.