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Citation for published version (APA):

Zhang, S., Erckens, R. J., Jongsma, F. H. M., De Brabander, J., Webers, C. A. B., & Berendschot, T. T. J. M. (2020). Dark-field illumination in conjunction with confocal Raman spectroscopy for real-time noninvasive aqueous humor investigation. *Optical Engineering*, *59*(9), Article 092002. https://doi.org/10.1117/1.OE.59.9.092002

Document status and date: Published: 01/09/2020

DOI: 10.1117/1.OE.59.9.092002

Document Version: Publisher's PDF, also known as Version of record

Document license: Taverne

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Dark-field illumination in conjunction with confocal Raman spectroscopy for real-time noninvasive aqueous humor investigation

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Abstract To obtain a real-time noninvasive analysis of the content of the aqueous humor (AH) in the eye, a confocal dark-field ophthalmic probe was designed and optimized by ray-tracing software. The confocal technique allows Raman spectrometric sampling of the AH with suppressing signals from the surrounding tissues. Dark-field illumination prevents the excitation light to reach the vulnerable retinal tissue directly. In order to evaluate the optical performance and safety of this method, a functional prototyped eye contact probe has been designed and tested on *ex vivo* rabbit eyes. © *2020 Society of Photo-Optical Instrumentation Engineers (SPIE)* [DOI: 10.1117/1.OE.59.9.092002]

Keywords: Raman spectroscopy; eye; aqueous humor; confocal microscopy; dark-field illumination.

Paper 191724SS received Dec. 13, 2019; accepted for publication Mar. 27, 2020; published online May 4, 2020.

1 Introduction

The anterior chamber (AC) (Fig. 1) contains an ocular fluid called aqueous humor (AH), the functions of which are maintaining eye pressure and providing nutrition to the cornea and lens. If these proteins, nucleotides, and metabolites in the AH could be detected, they could be helpful in understanding ocular diseases.^{1–3} Glucose levels in AH correlate with those in blood plasma and may be used as an indicator of diabetes complications in the eye.^{4–6} Inflammatory cytokine profiles in the AH could reveal associations with glaucoma, the leading irreversible cause of blindness.⁷ Further, recently it was shown that three ocular proteins in the AH can be used as a diagnostic aid for several retinal disease diagnoses.⁸ The current standard in clinical practice to analyze AH is invasive biopsy. However, this approach has several drawbacks: first, breaking the integrity of the eye raises the risk of inflammation. Second, it is a burden to the patients, which impairs its frequent use. Third, the procedure requires multiple devices and a clinical environment. Fourth, it also bears the risk of changing the composition of the AH during the process.

To understand the mechanism of eye diseases, it is preferable to investigate the physiological and pathological changes in real time of the eye with noninvasive methods. Since the eye is transparent in the electromagnetic spectrum of 350 to 2000 nm, several optical diagnostic techniques have been developed for anterior eye section examinations, such as biomicroscopy (slit lamp) and optical coherence tomography (OCT).⁹ However, these morphological examinations are lacking the ability of revealing the biochemical information of ocular tissues. Raman spectroscopy can do this in a noninvasive way.¹⁰ The Raman effect is associated with inelastic scattering from vibrations or rotations of chemical bonds, and therefore the spectra have a specific fingerprint for each biomedical molecule due to their unique atomic composition and structure. As such, Raman spectroscopy is capable of identifying targeted tissues both qualitatively and quantitatively and is therefore widely used for molecular identification in biomedical and preclinical applications.^{2,11–14} To evaluate the feasibility of our Raman spectroscopy system for ocular research, the first Raman spectroscopy experiments of our research group to measure

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Fig. 1 OCT image of anterior segment of a rabbit eye, acquired with a Heidelberg Engineering BD900 SL-OCT.

a rabbit eye were performed in 1990s at the UTMB in Galveston, Texas.¹⁵ With a setup using an 514.5-nm wavelength argon ion laser as excitation source and a liquid nitrogen-cooled spectrometer, good isolated Raman spectra of the AH of an *ex vivo* rabbit eye were obtained as a proof of principle experiments.¹⁶

To obtain a high signal-to-noise ratio in Raman spectroscopy, a laser is indispensable as an excitation source. However, radiation limitations for light damage of retinal tissue are strict when employing laser light.^{16,17} There are two kinds of light hazard in the eye. Wavelengths below 550 nm might cause photochemical light damage on the retinal tissue.¹⁷ Here, exposure time is limited due to its cumulative effect on living tissue. Longer wavelengths do not induce photochemical light damage and have the benefit of suppressing the disturbing background fluorescence. However, with longer wavelengths the danger of thermal damage increases while Raman responses decrease. For this reason, we chose excitation wavelengths at the end of the visual spectrum—that is patient friendly—of 671 and 785 nm at relative low intensities of 10 to 25 mW with prolonged exposure times of 60 to 90 s. Note that even this power excitation is unsafe when direct laser radiation reaches the retinal tissue. To prevent the latter and guarantee an eye safe usage, we designed and constructed a circular symmetric Raman eye probe for clinical use with the principle of "dark-field" illumination in which only scattered light can reach the patients retina. The optical performance of this probe will be presented in this paper using simulation diagrams. In addition, we will show results of ex vivo test in rabbit eyes using a prototype of the probe.

2 Design

To evaluate its optical principles, the basic structure of the probe was first designed and developed by ray-tracing software Zemax (version 16.5 Sp3, Zemax LLC, Kirkland, Washington). After performance optimization and validation of the design, the three-dimensional (3-D) model for manufacturing was generated by Autodesk inventor (professional version 2016, Autodesk Corp., San Rafael, California). In the end, the 3-D model was imported into Zemax again for final check (such as tolerance influence) before fabricating the prototype.

The spectrometer provides an excitation beam with a waist of about 18 μ m. For simplicity, we assumed a point light source in ray-tracing for the optical setup. To optimize our dark-field design with Zemax, a Liou-Brennan eye model was used.¹⁸ All ray-tracings were done at 785 nm.

2.1 Optical Design

To prevent light damage on retinal tissue, direct excitation of the posterior part of the eye should be avoided. We have opted for the approach to apply dark-field illumination principle for patients, with the incident laser light passing through the periphery of the cornea and focusing on the AC. This way it ends up in iris tissue instead of directly reaching the retina and only the scattered light can reach the posterior parts of the eye through the crystalline lens. It offers an integration length of about 0.5 mm (calculated for a 25- μ m pinhole) perpendicular to the optical axis of the eye and the numerical aperture (NA) of the probe could be designed to match that of the Raman spectrometer (NA = 0.05).

The probe was designed and developed based on a former patent [Fig. 2(a)].¹⁹ Unfortunately, alignment of this model proved to be so difficult, that no reproducible results could be obtained. In particular, the distance between the focusing lens and the probe proved to be critical. In the redesigned probe, a central mirror focuses the collimated incoming light that is further guided by two conical mirrors into the eye. This design eliminates the degree of freedom for the distance between separated focusing lens and the probe formerly patented [region 1, Fig. 2(a)]. A collimated beam is sufficient as an incident beam for the redesigned probe [region 1, Fig. 2(b)]. Applying a mirror-only system, chromatic aberration induced by the focusing lenses is also no longer present.

Figure 2(b) shows a schematic representation of the newly designed probe.²⁰ It is formed by three mirrors (2, 3, and 4), where surface 2 is an aspherical concave aluminum mirror to provide focusing power. The rotationally symmetric aspheric concave mirror can be described as



Fig. 2 Design of the ophthalmic probe. (a) In former patented design, (1) a focusing lens with (2) an entry surface and (3) an exit surface is used to provide focusing power and (4) a spherical surface adapted to the converging beam without adding further focusing power is also used to acting as a contact probe guides the light into (11) the eye. (5) An internal conical mirror reflects the light to a further (6) conical mirror which further directs the light into the anterior eye chamber through (7) an interface and (8) cornea surface. The excitation light will end on (9) the iris, only scattering light reaches the posterior part of the eye through (10) the crystalline lens. (b) In the newly designed probe, (1) the collimated incident light directly reached (2) an aspherical concave mirror which provides focusing power of the probe. The reflected light is guided by (3) a rotationally symmetric flat mirror to feed into the main body of (8) the probe and direct to (10) the eye by (4) surface through (6) an interface on (7) the corneal interface surface. The excitation light will end on (7) the iris tissue, only scattering could reach the posterior part of the eye through (9) the crystalline lens.

Zhang et al.: Dark-field illumination in conjunction with confocal Raman spectroscopy...

$$z = \frac{cr^2}{1 + \sqrt{1 - (1+k)c^2r^2}} + \beta_1 r^1 + \beta_2 r^2 + \dots$$
(1)

Here *c* is the curvature (the reciprocal of the radius) and *r* is the radial coordinate. To have a focusing effect, it implies that a parabola curve is needed for the two-dimensional cross-section curvature. Hence, the conic constant k = -1 and the equation can be written as

$$z = \beta_1 r^1 + \left(\frac{1}{2}c + \beta_2\right) \times r^2 \tag{2}$$

where β_1 and β_2 were both optimized and obtained by Zemax simulations, respectively. Surface 3 is a rotationally symmetric flat aluminum mirror that guides the laser beam to surface 4 properly. The mirror is tilted toward the curved mirror with 6.7 deg and 7.5 mm long measured in cross section. The distance between surface 2 and surface 3 is also optimized by Zemax to ensure a focus in the central part of the AC. Surface 4 is an interface of poly(methyl methacrylate) (PMMA) and air, which functions as a mirror by total internal reflection.

The eye fitting part was carefully designed to fit the cornea. As shown in Fig. 2(b), the direction of the light beam guided by mirror 3 and surface 4 was designed such that it reaches the eye fitting surface perpendicularly, this to avoid extra refraction and minimize power loss. The diameter of the eye fitting component was 26.3 mm for the outer diameter of the probe and 15 mm for the eye fitting part. Its length was 7.5 mm in total. Surface 4 was tilted 51 deg from the horizontal surface to obtain total internal reflection in the PMMA body of the design. Through a special designed interfacial surface [6 in Fig. 2(b)] with a radius of 8 mm and a chord length of 0.6 mm, astigmatism caused by the corneal surface. Hereafter, the light will be absorbed in the region between cornea and iris. We assumed an 8-mm pupil, the edge of which also being the edge of the incident beam as shown in surface 7 in Fig. 2(b). Finally, the eye fitting surface was designed with a radius of 7.9 mm to match the curvature of the cornea. For patient comfort, all corners are rounded with varies of radius, respectively.

2.2 Prototype Manufacture

Based on the optimization by ray-tracing, the optical design as explained above was used to produce a prototype of the probe (Fig. 3). The central focusing mirror [surface 2 in Fig. 2(b)] and the conical-shaped mirror [surface 3 in Fig. 2(b)] were made by polished aluminum to obtain a high reflectivity and quartz coating to prevent oxidation. The PMMA body of the probe with a refractive index of 1.487 at 671 nm and 1.485 at 785 nm²¹ ensures total internal reflection at surface 4 and transmission at interface 6. All parts of the probe were produced using a high-precision lathe.



Fig. 3 Assembled prototype probe.

3 Measurement

3.1 Confocal Raman Spectroscopy

To bring Raman spectroscopy into the clinic, a compact and easy to transport spectrometer was used. Figure 4 shows the schematic representation of the confocal Raman spectroscopy (CRS) setup. It consists of a Raman spectrometer with two integrated excitation sources, one for the fingerprint region and one for the longer wavelength shift, a dark-field eye probe, and a sample stage. The confocal setup with 25-µm pinhole minimizes possible contributions of out of focus signals that are generated in tissues along the pathway.²²

As excitation sources a 15-mW diode laser with a wavelength of 785 nm (Innovative Photonic Solutions SM 785 nm, Monmouth Junction) and a 20-mW diode laser with a wavelength of 671 nm (Laser Quantum Ignis 671 and SMD 6000, Konstanz, Germany) were utilized. A high-performance Raman spectrometer (Module Model 2500, River Diagnostics[®], Rotterdam, The Netherlands) was employed with a charge-coupled device camera to record the Raman spectra at a working temperature of -65° C. The module receives the laser excitation light through two single-mode diamond optical fibers. A 25- μ m pinhole was placed in the spectrometer to allow the laser beams—that have a waist of about 18 μ m—pass into the measurement area. An 80-mm focal length doublet lens was placed after the spectrometer aperture to change the diverging beam (NA = 0.05) into an 8-mm-diameter parallel beam. Alignment of the 80-mm collimating lens was achieved with a shearing interferometer to obtain a perfect parallel excitation beam that is coupled into the eye probe.

The eye probe was mounted in a gimbal mirror mounts (BHAN-50M, OptoSigma[®], Les Ulis, France), with fine adjustment in horizontal and vertical directions. Maximum adjustment range is ± 4 deg, resolution of rotation is 0.31 deg and 0.48 deg in x and y axes separately. Alignment in the sample was performed by translation and rotation adjustments of the gimbal until the maximum signal appeared.

All Raman spectra were processed by a self-developed MATLAB program (Version 2017b, The Mathworks Inc., Natick).²³

3.2 Sample Preparation

Enucleated eyes from sacrificed New Zealand white rabbits were stored in -80° C freezers before use. The eyes were thawed at room temperature then submerged in phosphate-buffered saline



Fig. 4 Schematic of the optical setup. The circle symmetric probe, the diode lasers (671 and 785 nm) are coupled on one optical axis by a (1) mirror and (2) and (3) dichroic mirror within the spectrometer. The excitation light leaves the spectrometer through (4) an integrated 25- μ m pinhole. (6) An *f* = 80-mm achromat collimates the excitation beam before it enters (7) the gimbal-mounted probe. (9) The eye is optically coupled to the probe with (8) an ophthalmic gel. The back-scattered Raman radiation that fits into the NA = 0.05 optical system is transported back into the spectrometer and recorded by (5) a CCD. Due to this coincidence setup, the spectrometer facilitates a confocal isolation of the AH from the about 100× stronger Raman signal from the corneal tissue.

(pH 7.4) to prepare for use. 150- μ l volume AH was removed from the rabbit eye by a syringe with 30G needle. Subsequentially, the same volume of phenylephrine HCl 10% (Bausch & Lomb UK Limited, Surrey, United Kingdom) was injected by another 30G needle syringe into the AC. All animal sample procedures were conducted under the Guidelines of the Central Laboratory Animal Facility of Maastricht University and complied with the ARVO Statement for the Use of Animals in Ophthalmic and Visual Research. All protocols were approved by the Central Committee for Animal research and were in accordance with the European Guidelines (2010/63/EU).

For the prototype probe as shown in Fig. 3, topically applied Methocel[®] 2% (OmniVision, Santa Clara, California) was used as an ophthalmic gel. It functions both to moister the cornea and to remove air between the probe and the eye. The gel has a refractive index of 1.469, which also bridges the refraction index difference of the probe (1.487) and cornea (1.376).

4 Results and Discussions

4.1 Ray-Trace Simulation

In Fig. 5(a), the spot diagram shows that the root-mean-square (RMS) radius of the excitation light (785 nm) focus in the AC is 6.684 μ m and the geometric (GEO) radius is 18.577 μ m. The RMS radius gives a rough idea of the spread of the focus spot while the GEO radius indicates the distance of farthest illuminated boundary from the center. Due to the small aperture and the long wavelength, this is an about diffraction limited spot. Figure 5(b) shows the cumulative normalized energy as function of the encircled radius. When properly aligned, nearly all energy was collected within a 12- μ m radius (triangle-labeled line). In case of a severe (3.5 mm) lateral misalignment with the probe, the ray-traced focus showed a scattered power distribution in a broad area outside the focal area (dots labeled line). However, with already a slight rotation misalignment of 0.3 deg in one direction, no energy at all is collected within a 12- μ m radius (square-labeled line). A recognizable signal can only be obtained with a 100- μ m radius, implying that the widths of the pinhole of the spectrometer need to be 200 μ m to collect a considerable amount of the Raman backscattered light. However, a 200- μ m pinhole destroys the confocal effect necessary to limit the integration length in the AH.

The simulation indicates the extreme sensitivity for rotation misalignment. Under such a misalignment, the focus of the excitation light is displaced and disrupted into scattered elements. Hence, the collected Raman signal obtained from such an element will be strongly decreased and



Fig. 5 Simulation result of the newly designed probe. In Fig. 5(a), the spot diagram shows that the RMS radius of the focus is 6.684 μ m and the GEO radius is 18.577 μ m. In Fig. 5(b), the encircled radius of cumulative normalized energy diagram shows that aligned probe (triangle-labeled line) could collect nearly all energy within a 12- μ m radius (square-labeled line). A recognizable signal can only be obtained with a 100- μ m radius; 3.5-mm lateral misalignment (dots labeled line) could collect nearly all energy within a 30- μ m radius; a rotation misalignment of 0.3 deg leads to a recognizable signal with around 100 μ m radius.



Fig. 6 Raman spectrum obtained by the prototype probe with (a) 10% phenylephrine in 90-s integration time and (b) water OH bending mode in 60-s integration time.

will not be a guidance to proper focusing. The decreased maximum intensity after the focus and the disrupted intensity distribution will minimize the light damage of the tissue accordingly.

4.2 Raman Spectrum

The design of prototyped probe for measuring the Raman spectrum of the AH in a "dark-field" modality was tested on *ex vivo* rabbit eyes. To avoid the 100 times stronger signals of the surrounding tissues, a confocal setup was applied using a spectrometer of which the excitation light as well as the Raman signal was passing the same 25- μ m pinhole. In Fig. 6(a), a peak at the wavenumber of 1002 cm⁻¹ is observed with an exposure time of 90 s from the AH of a rabbit eye with phenylephrine injection. The peak position is the same as the ocular drug phenylephrine which formerly reported by Elshout et al.²⁴ In Fig. 6(b), the AH showed a spectral response from the OH bending mode of water at an exposure time of 60 s.

Although the prototyped probe showed a recognizable Raman signal, it was by far not the signal that could be easily obtained due to the alignment difficulties which is also revealed by the simulation results. More effort was needed to achieve this alignment, which is an unsurmountable obstacle for ophthalmologists during clinical practice.

4.3 Data Processing

AH contains variant compounds including inorganic ions and organic anion, carbohydrates, glutathione and urea, proteins, growth-modulatory factors, oxygen, and carbon dioxide.¹ Not all of them are Raman active since the Raman scattering mainly related to the vibrational, rotational, and other low-frequency modes of intramolecular bonds. These compounds in AH are dynamically interchanging with many tissues inside the eye, but AH is in a closure environment with stable exchange rate of 2 to 3 μ l/min in a health human eyes¹ and exchange rate of 2.6 to 3.6 μ l/min in rabbit eyes,²⁵ which can be considered as static comparing with the Raman measurement time. In a multiple chemical mixture environment such as AH, substance identification only by single peak might lead to a biased conclusion because some composition might share some chemical bonds in common. However, there is not a well-accepted data processing procedure available yet.²⁶ In a previous study, we proposed and validated a MATLAB program for data processing of Raman detection of ocular drug topically delivered to the animal eyes *in vitro* and *in vivo*.²³ It demonstrated that with proper data processing techniques, Raman spectroscopy could be used in ocular tissue investigation with an ophthalmic probe.

5 Conclusion

In this study, simulation analysis and *in vitro* tests indicated that the dark-field probe as prototyped is suitable for applying on human eyes. Recognizable Raman signals were acquired from the *ex vivo* rabbit eyes as proof of principle. This design demonstrated the potential for real-time, noninvasive Raman AH measurements. However, difficulties to achieve alignment hinder its clinical application and further improvement is needed. Development of a probe with a less critical rotational alignment and of which the signal during the alignment guides the operator to a proper alignment will be the next step in our research.

Acknowledgments

We would like to thank Sumipro B.V. for their advice while manufacturing the prototype and Theresa Kocanda for her help while evaluating the performance of probe prototype. We also would like to thank Christian J.F. Bertens for his help while obtaining the OCT image of the rabbit eye in Fig. 1. Shuo Zhang acknowledges the China Scholarship Council for the support by State Scholarship Fund No. 201309110103. The authors declare that there are no conflicts of interest to disclose.

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John De Brabander received his PhD in medical and technologic advancements in contact lenses from Maastricht University. He also, with a master on education sciences, acted as an educational coordinator for ophthalmology at Maastricht University. Although being retired, he still focuses on the development of measurement and imaging techniques for the diagnosis and treatment of the eye.

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