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Risk-based maintenance strategy for deteriorating bridges using a hybrid computational intelligence technique: a case study

The current bridge inspection and maintenance protocol that is used in most countries focuses primarily on the visible aspects of bridge fitness and undervalues the invisible aspects such as resistance to scouring and earthquake. To help transportation authorities better consider both aspects, the present study developed a new computational intelligence system called the Risk-Based Evaluation Model for Bridge Life-Cycle Maintenance Strategy (REMBMS). This model considers the three main risk factors of component deterioration, scouring, and earthquakes in order to minimise the expected life-cycle cost of bridge maintenance. Monte Carlo simulation is used to estimate the probability of bridge maintenance. The Evolutionary Support Vector Machine Inference Model (ESIM) was applied to estimate the risk-related maintenance cost using historical data from the Taiwan Bridge Maintenance System (TBMS) database. The timeinfluenced expected costs were obtained by multiplying each maintenance probability with its associated cost. Finally, the Symbiotic Organisms Search (SOS) algorithm is used to identify the bridge maintenance schedule that optimises the life-cycle maintenance cost. The present study provides to bridge management authorities an effective approach for determining the optimal timing and budget for maintaining transportation bridges.

Keywords: bridge maintenance strategy; artificial intelligence; optimisation; bridge risk evaluation; evolutionary support vector machine inference model; symbiotic organisms search

1. Introduction

Frequent earthquakes, typhoons, and heavy rains regularly challenge the structural integrity of bridges and seriously deteriorate bridge components in Taiwan and the many other countries with similar climatic and tectonic conditions. In Taiwan, flooding and mudflows are particularly serious threats to bridges during the typhoon season, which typically lasts from summer through early autumn. Additionally, Taiwan's location in a complex tectonic area makes earthquakes fairly common. A particularly serious 7.3 magnitude earthquake that hit Taiwan in 1999 collapsed over 20 bridges. Furthermore, age-related deterioration is an issue that affects all bridges. Taiwan currently lists more than 4,000 bridges that are over 30 years old, with 2,500

of these dating from the 1970s, a period of heavy government investment in the national infrastructure (Liao and Yau 2011).

The number of bridges that have deteriorated beyond their designed safety thresholds continues to increase worldwide. Furthermore, the expenditures that will be necessary to maintain, repair, and rehabilitate these bridges greatly exceed the budgetary allocations for these purposes (Goyal, Whelan, and Cavalline 2017). As daily traffic loads and natural stresses continue to deteriorate the conditions of bridges, proper bridge maintenance has become an increasingly crucial task for bridge-management agencies. Therefore, an updated approach to the management of bridges that optimises the available resources under conditions of uncertainty and of multiple, conflicting objectives is necessary to enhance bridge lifespans (Hu, Daganzo, and Madanat 2015; Frangopol, Kong, and Gharaibeh 2001).

Bridges may face serious multihazard risks such as natural ageing, scouring, and earthquakes (seismic events) during the long-time operation. Researchers have studied the behaviour of bridges in dealing with the inevitable deterioration or natural hazards. Simon, Bracci, and Gardoni (2010) investigated the impact of corrosion on the seismic fragility and response of deteriorated bridges. Gardoni and Rosowsky (2011) proposed seismic fragility increment functions to estimate the deformation-shear fragility of deteriorating bridges that is not requiring a traditional reliability analysis. Zanini et al. (2013) studied the effect of degradation phenomena on the seismic vulnerability of bridges. The seismic degradation of highway bridges was investigated by Kumar and Gardoni (2014) by using the nonlinear time history analysis. It was presented that the degradation in reinforced concrete columns may give a significant impact on the seismic vulnerability of the bridges. Similar to earthquakes, scouring can induce serious damage or even collapse to many bridges as reported by Zampieri et al. (2017) in their failure analysis of mansonry arch bridges. Therefore, there is a need on effective and efficient maintenance strategy to reduce such dangerous risks.

Significant research time and energy has invested in developing effective maintenance and restoration strategies for bridges (Furuta et al. 2006; Frangopol and Bocchini 2012; Zanini, Faleschini, and Pellegrino 2016; Yadollahi, Abd Majid, and Mohamad Zin 2015). Roberts and Shepard developed the bridge health index (BHI), which relates to the ratio of the current element value and the proposed total element value (Roberts and Shepard 2001; Frangopol, Kong, and Gharaibeh 2001). Huang used neural networks to model the deterioration of concrete bridge decks and came to conclusions that differed significantly from Roberts and Shepard using the Markov process in the bridge management system (Huang 2003). Huang's study demonstrated that deterioration does not relate exclusively to the age of a bridge but also to its maintenance and history overlay. Huang used single-component deterioration to estimate the life-cycle cost of a bridge (Huang and Mao 2010). However, his estimates focused exclusively on the bridge deck slab. Tserng utilised Huang's approach in combination with the new performance index (NPI) to assess when preventive maintenance should be executed (Tserng and Chung 2007). However, Tserng's approach did not consider maintenance costs. Meanwhile, Bucher and Frangopol have developed lifetime maintenance strategies that covers time-based maintenance and performance-based maintenance (Bucher and Frangopol 2006). However, some invisible risks such as scour and earthquake were still not taken into account. Finally, the several studies that have analysed the effectiveness of various strategies in guiding bridge maintenance revealed that little offers a methodology to account for the maintenance costs over the life cycle of a bridge and that most of the visible and invisible risks related to this life cycle are not addressed.

The Taiwan Bridge Management System (TBMS) is a national bridge-management system that the transportation-related agencies of the Taiwan government use to direct visual inspections of more than a thousand bridges annually. TBMS provides the methodology to inspect the visible risk that is attributable to component deterioration using the bridge condition

index (CI). Bridge CI values are calculated based on the visual inspection results, with these index values providing an indication of the overall condition of individual bridges, which is used to specify the relevant maintenance-service level of each bridge. Thus, the CI value helps decision makers in these agencies execute proper bridge maintenance. After a bridge is inspected, maintenance is scheduled only if the CI value falls below a specific threshold.

However, using CI as a solely indicator for determining the maintenance decision may be misleading, as CI considers only component deterioration that is visible and detected during the inspection process (Liao and Yau 2011). The invisible risks associated with natural hazards such as floods and earthquakes may also significantly deteriorate the bridge. Because the invisible risks attributable to scouring and earthquakes are not taken into consideration in the TBMS or in previous studies, the present research proposes an alternative bridge maintenance strategy: Risk-Based Evaluation Model for Bridge Life-Cycle Maintenance (REMBMS). This strategy addresses both the visible and invisible risks in a more advanced bridge management system. In the first stage, REMBMS uses Monte Carlo to simulate the probability of bridge maintenance using historical data. In the second stage, a hybrid artificial intelligence model called the Evolutionary Support Vector Machine Inference Model (ESIM) is used to estimate the impact of the various risk factors on costs. Next, the bridge maintenance probability is multiplied with the associated costs to calculate the expected cost. Finally, REMBMS utilises the Symbiotic Organisms Search (SOS) algorithm to obtain an estimate of minimum cost. This advanced strategy is expected to yield a bridge maintenance strategy that generates optimal timing and budget estimates that bridge-maintenance planners may use to minimise life-cycle maintenance costs.

2. Literature Review

2.1. Bridge Inspection in Taiwan

Visual inspection is one of the common method used to investigate the bridge condition (Yeum and Dyke 2015; Quirk et al. 2017). In Taiwan, the Taiwan Bridge Management System (TMBS) is used to manage the inventory and inspection data for thousands of domestic bridges. The TBMS, first developed in 2000 (Liao and Yau 2011), is used by transportation-related government agencies to guide ongoing bridge inspection and maintenance efforts. Current regulations mandate that all bridges in the TMBS database be inspected visually at least once every two years and that special inspections be performed after extremely heavy rains and severe earthquakes. Special inspections are quick and simple inspections for obvious damage and regular inspections investigate a checklist of 20 bridge components. Trained inspectors perform the regular inspections using their eyes and portable tools only. These inspectors approach the target bridges on foot, by boat, or in special vehicles.

In Taiwan, the methodology used to conduct these regular bridge inspections and evaluations is known as DER&U. DER&U mandates the inspection of 20 unique bridge components (Tserng and Chung 2007), with 4 indices used to evaluate the conditions of these components: "D" represents degree of deterioration; "E" represents extent of the deterioration; "R" represents the relationship between the deterioration and the safety of the bridge; and "U" represents the urgency of repair. All of these indexes are numerically rated on an integer scale from 0 to 4. An index value of 0 means either that the component does not exist or that the inspector was unable to make the inspection. Index values ranging from 1 to 4 correlate positively with deterioration status, with a 1 indicating good condition (no/minimal deterioration) and a 4 indicating extremely poor condition (serious deterioration).

The DER&U ratings are obtained for calculating the CI of a bridge. First, a component condition index Icij is calculated based on the evaluated integers of D, E, and R for each component. The calculation is based on a point-deduction mechanism, i.e., deficiencies in a component deduct points from a perfect score of 100. Equation (1) shows the formula for calculating an Icij value for the "j" item of component "i". Notably, the value of "a", an integer in this equation usually set as 1, may be set by the user.

After the inspection is completed, the sub-item condition index (Icij) for each sub-item of the 20 main items is calculated as follows:

$$Ic_{ij} = 100 - 100 \times \frac{(D+E) \times R^a}{(4+4) \times 4^a}$$
 (1)

where $I = 1 \sim 20$, $j = 1 \sim n$ (number of sub-items), and parameter "a" relate to the importance of the bridge, with a = 1 for a highway bridge, a = 2 for a freeway bridge. Next, the condition index for each of the 20 main items is calculated as follows:

$$Ic_{i} = \frac{\sum_{j=1}^{n} Ic_{ij}}{n}$$
(2)

Finally, the CI of the bridge is calculated using Ici and its corresponding weighting wi, as follows:

$$CI = \frac{\sum_{i=1}^{20} \operatorname{Ic}_{i} \times w_{i}}{\sum_{i=1}^{20} w_{i}}$$
(3)

The values of w_i are adopted from Tserng and Chung (2007) as reported in Table 1. The level of component deterioration of a bridge may be measured by its CI, which is calculated based on the DER&U inspection results.

<Insert Table 1 here>

The Scouring Stability Index (SSI) may be used to measure the scouring stability of a bridge. The SSI of a bridge is calculated in a manner that is similar to CI, but uses only the several components in the DER&U inspection that are normally affected by scouring. These components include: Waterway (3), Abutment foundations (5), Abutments (6), Scouring protection of piers (12), Pier foundations (13), and Piers and columns (14). Equation (6) shows the formula used to calculate SSI.

$$SSI = \frac{Ic_3 \times w_3 + Ic_5 \times w_5 + Ic_6 \times w_6 + Ic_{12} \times w_{12} + Ic_{13} \times w_{13} + Ic_{14} \times w_{14}}{w_3 + w_5 + w_6 + w_{12} + w_{13} + w_{14}}$$
(4)

As for the earthquake risk, the pushover method is employed to carry out the assessment to obtain the yield acceleration (Ay) and collapse acceleration (Ac). To measure the damage state of bridges, this study adopts the seismic damage index from Chiu, Lyu, and Jean (2014).

Due to the uncertainty in predicting the time at which an earthquake will occur, Monte Carlo Simulation is applied to simulate these two ground accelerations with seismic damage index to estimate the earthquake maintenance probability.

2.2. Evolutionary Support Vector Machine Inference Model (ESIM)

Over the past years, many studies reveals that artificial intelligence (AI) techniques have surpassed the traditional methods in terms of performance and accuracy as a result of their excellent learning features (Cheng and Prayogo 2014; Cheng et al. 2015; Cheng, Prayogo, and

Wu 2014; Cheng et al. 2016). The evolutionary support vector machine inference model (ESIM) is a hybrid AI method developed by Cheng and Wu (Cheng and Wu 2009) that fuses two different AI techniques, namely support vector machines (SVMs) and fast messy genetic algorithm (fmGA). In this complementary system, SVM acts as a supervised learning tool to handle input-output mapping and fmGA works to optimise SVM parameters.

SVM is a recent AI paradigm developed by Vapnik (Vapnik 1995) that has been used in a wide range of applications. This paradigm is a supervised learning tool that was designed to solve classification and regression problems. SVM works by mapping input vectors into a higher dimensional feature space. The optimal hyperplane is identified within this feature space with the help of a kernel function. This inner product in the feature space attempts to make training data linearly separable. Several admissible kernel functions that are used today include the polynomial kernel, the radial basis function (RBF) kernel, and the sigmoid kernel. However, the RBF kernel has been recommended for general users as a first choice due to its ability to analyse higher-dimension data, its ability to conduct searches using only one hyper parameter, and its relatively few numerical difficulties (Chang and Lin 2011). Therefore, the generalisation ability and predictive accuracy of SVM are determined in the present study using the optimal penalty and kernel parameters (C and γ parameters).

Determining the SVM parameters C and γ is a complicated and problem-oriented process. Improper parameter settings lead to poor accuracy in the resultant prediction/classification model. fmGA has previously been employed to simplify and increase the effectiveness of the SVM parameter-setting process. The fmGA proposed by Goldberg, Deb, Kargupta, and Harik (Goldberg et al. 1993) is a relatively recently developed machine-learning and optimisation tool that is based on a genetic algorithm approach. The fmGA represents an improvement over the messy genetic algorithm (mGA), which was initially

developed to overcome the simple genetic algorithm (sGA) linkage problem resulting from a parameter-coding problem that generated suboptimal solutions.

2.3. The Symbiotic Organisms Search (SOS) Algorithm

The SOS algorithm is a new metaheuristic algorithm that was developed by Cheng and Prayogo (Cheng and Prayogo 2014). It was inspired by the biological dependency-based interaction or symbiosis seen among organisms in nature. Similar to most population-based metaheuristic algorithms, SOS uses a population of organisms which contains candidate solutions to seek the global solution within a search space; has special operators that use the candidate solutions to guide the search process; uses a selection mechanism to preserve the better solutions; requires proper setting of common control parameters such as population size and maximum number of evaluations. Furthermore, SOS has been proven to successfully solve various problems in different fields of research (Cheng et al. 2014; Tran, Cheng, and Prayogo 2016; Kamankesh, Agelidis, and Kayousi-Fard 2016; Panda and Pani 2016; Secui 2016; Vincent et al. 2017).

In the initial stage, a random ecosystem (population) matrix is created, with each row representing a candidate solution to the corresponding problem. The user predetermines the number of organisms in the ecosystem, which is the size of the ecosystem. As with other metaheuristic algorithms, the rows in the matrix are called organisms. Each virtual organism represents a candidate solution to the corresponding problem/objective. The search begins after the initial ecosystem has been generated. During the search process, each organism benefits from continuous interaction with others in three different ways:

1. Mutualism Phase: In this phase, an organism develops a mutually beneficial relationship with another organism. The relationship between bees and flowers is a classic example of mutualism.

- 2. Commensalism Phase: In this phase, an organism develops a relationship with another organism that benefits itself but does not impact upon the other organism. An example of commensalism is the relationship between remora fish and sharks.
- 3. Parasitism Phase: In this phase, an organism develops a relationship with another organism that benefits itself and harms the other organism. An example of parasitism is the plasmodium parasite, which uses its relationship with the anopheles mosquito to transfer between human hosts.

These three phases reflect the most common symbioses used by organisms to increase their fitness and survival advantage over the long term. During an interaction event, the one that receives a benefit will evolve into a fitter organism, while the one that is harmed will perish. The mechanisms for updating the best organism are conducted after an organism has completed its three phases. The phases are repeated until the stop criterion is achieved.

3. Proposed Risk-Based Evaluation Model for Bridge Life-Cycle Maintenance (REMBMS) Strategy

This section describes the newly proposed Risk-Based Evaluation Model for Bridge Life-Cycle Maintenance (REMBMS) in detail. Risk-based approach presents an applicable strategy to determine the optimal design involving such uncertainties (Zhu and Frangopol 2012; Beaurepaire et al. 2013; Barone and Frangopol 2014; Beconcini et al. 2016; Frangopol and Bocchini 2012). There are four main stages in the proposed model. The objective of the REMBMS is to minimise the total cost of maintenance related to both visible and invisible risk factors. Three main AI techniques are involved in the last three stages. After completing the risk evaluation model in the first stage, a Monte Carlo Simulation is employed in the second stage to estimate the bridge maintenance and rebuilding probabilities, which will be used to calculate the expected future maintenance and rebuilding costs. In the third stage, ESIM is used

to establish accurate bridge maintenance cost models that are based on historical data. In the final stage, SOS is used as the core optimiser in the REMBMS model to identify the lowest total-expected maintenance cost for the bridges. Fig. 1 describes the overall operational architecture of the proposed algorithm.

The first stage of the proposed REMBMS identifies and categorised the risk involved in a bridge and to establish a bridge risk evaluation model by determining the bridge synthesised capacity index that will be used for further analysis in the subsequent stages. The present study adopted Expectancy Value Theory (EVT) to address all of the three risk factors that were identified and evaluated in the previous stage (component deterioration, scour, and earthquake). The objective was to estimate the total expected cost of maintenance by synthesizing all of the risk factors involved in each bridge (see Fig. 2). The expected cost considers the bridge maintenance and/or rebuilding strategy. In the maintenance strategy, all three risks are considered to influence the expected maintenance cost. Alternatively, decision makers who do not perform necessary maintenance on bridges face much higher risks of bridge collapse due to scouring and earthquake damage and thus should consider the expected costs of rebuilding in their strategy. The following equations were used to represent the relationship between the expected cost and the risks factors.

$$E(Cost) = E(MC) + E(RC)$$
(5)

$$E(MC) = \left(\sum_{i=1}^{100} P_{MD_i} \times C_{MD_i} + \sum_{i=1}^{100} P_{MS_i} \times C_{MS_i} + \sum_{i=1}^{100} P_{ME_i} \times C_{ME_i}\right)$$
(6)

$$E(RC) = \left(\sum_{i=1}^{100} P_{S_i} \times C_{RS_i} + \sum_{i=1}^{100} P_{E_i} \times C_{RE_i}\right)$$
(7)

where:

- E(Cost) is expected cost, E(MC) is expected maintenance cost, and E(RC) is expected rebuilding cost.
- ullet P_{MD} is the probability of deterioration-related maintenance, P_{MS} is the probability of scour-related maintenance, and P_{ME} is the probability of earthquake-related maintenance.
- C_{MD} is the maintenance cost attributable to deterioration, C_{MS} is the maintenance cost attributable to scouring, and C_{ME} is the maintenance cost attributable to earthquake damage.
- P_S is the bridge collapse probability attributable to scouring, P_E is the bridge collapse
 probability attributable to earthquake, C_{RS} is the rebuilding cost attributable to
 scouring, and C_{RE} is the rebuilding cost attributable to earthquake damage.

The following sections calculate the probabilities of bridge maintenance and rebuilding.

4. Estimating the Bridge Maintenance Probability

This section describes the stepwise procedures that were used in the present study to calculate the bridge maintenance probability for all three identified risk factors. The bridge is composed of many different members, with each member having a distinct function. Conducting a risk assessment of an entire bridge structure is very difficult and prone to wide margins of error. However, using the previous identification and evaluation model, the risk factors that affect bridges may be distinguished into visible deterioration and invisible hazards. Visible

deterioration is represented by component deterioration, while invisible hazards are distinguished into two categories: scouring damage and earthquake damage. Thus, the aim of this stage is to obtain the bridge maintenance probability for each of the involved factors. The

following subsection describes the steps used to achieve the goal.

4.1. Component Deterioration (CI)

Step 1: Bridge classification

Bridges of the same type (design approach), similar traffic loading status, and similar

distance from the sea are presumed to share similar deterioration conditions. The more than

40,000 bridges in Taiwan have been categorised into 10 types, summarised below in Table 2.

<Insert Table 2 here>

Step 2: Statistical analysis.

In this step, the CI for each bridge was collected from the TBMS. The relationship

between the age of a bridge and its CI was then plotted based on the historical data. Fig. 3 shows

an example plot, with the CI declining over time. Further, regression analysis was conducted to

assess the relationship between bridge age and the CI. By obtaining the linear formula, the

declining slope of the bridge CI may be determined for use in the next step. Fig. 3 shows the

slope of the bridge as -0.3813. Furthermore, applying regression analysis to all of the bridges

of each type allowed the average and variance of the related slopes to be calculated. Table 3

shows the average and variance of the slope for the bridges of the beam/girder type.

<Insert Fig. 3 here>

<Insert Table 3 here>

Step 3: Determine CI threshold.

The goal of this step was to identify the CI maintenance threshold. CI values below this threshold indicate that a bridge requires maintenance. After a review of relevant documents, interviews, and historical information, the threshold was identified as varying between 75 and 85.

Step 4: Monte Carlo Simulation

After obtaining the average and variance for each CI slope in step 3, statistical declining CI curves for each were established using the Monte Carlo Simulation. The maintenance probability was calculated by counting the number of times that the CI fell below the threshold during the simulation.

Step 5: Obtain maintenance probability attributable to component deterioration (P_{MD})

The annual probability of maintenance attributable to component deterioration (P_{MD}) may be calculated after completing the Monte Carlo Simulation. To illustrate the example of the proposed methodology, five bridges were included in this study. The information for each bridge is shown in Table 4. The photographic documentation for each bridge, which is obtained from TBMS database, is shown in Fig. 4. Table 5 lists the annualised probability of maintenance for several of the bridges. For example, in bridge number B04-0030-217A, the P_{MD} value after 10 years is equal to 1.7%. It means the 10-year CI fell below the threshold about 170 times out of every 10,000 simulations.

<Insert Table 4 here>

<Insert Fig. 4 here>

<Insert Table 5 here>

4.2. Scouring (SSI)

Step 1: Bridge classification.

This step is similar to the approach used to classify bridges in the Component Deterioration section (see Section 4.1, step 1). However, the bridges in the current section are classified by the river that they cross rather than by distance from the sea, traffic loading conditions, and structural type.

Step 2: Statistical analysis.

<Insert Table 6 here>

Table 6 aligns the Scouring Stability Index (SSI) slope index with the average flood return period for various main rivers in Taiwan. Statistical analysis may thus be used to obtain declining curve values for CI. As shown in Table 6, bridges that cross the Tamsui River have an expected average annual SSI decline of: 1*-1+0.5*-1+0.2*-2+0.1*-2+0.05*-3+0.02*-3+0.01*-3+0.005*-4=-2.36.

Step 3: Determine SSI threshold.

The default SSI threshold value for maintenance was determined to be 75.

Step 4: Monte Carlo Simulation

Based on the flood return period and the SSI slope index information obtained in Table 6, the Monte Carlo Simulation may be used to establish the statistically declining SSI curves for each bridge. Further, probability of maintenance values may be calculated by counting the number of times that the SSI fell below the threshold during the simulation. This step is similar to the Monte Carlo Simulation previously described in the Component Deterioration section (see Section 4.1, step 4).

Step 5: Obtain the probability of scour-related maintenance (P_{MS})

An annualised estimate of P_{MS} may be obtained after completing the Monte Carlo Simulation. Table 7 illustrates several examples of bridge maintenance probability over time.

<Insert Table 7 here>

Step 6: Obtain the probability of rebuilding due to scouring (P_{Rs})

An annualised estimate of the probability of rebuilding due to scouring (P_{Rs}) may be obtained after completing the Monte Carlo Simulation. This probability is calculated by counting the number of 100-year floods that occurred during the simulation period. The P_{Rs} should equal 1%, which is the equivalent of a 100-year probability.

4.3. Earthquake

Step 1 – Step 3: Conduct the potential earthquake analysis model, the ground vibration analysis model, and the bridge seismic hazard assessment.

These three steps were adopted from Das, Gupta, and Srimahavishnu (2007) and Chiu, Lyu, and Jean (2014). The goal of these steps is to apply a ground vibrations analysis model in order to calculate two ground acceleration values for each bridge location: the yield acceleration (Ay) value and collapse acceleration (Ac) value.

To obtain Ay and Ac, the pushover method is employed. The purpose of the pushover analysis is to evaluate the expected performance of a structural system by estimating its strength and deformation demands in design earthquakes by means of a static-inelastic analysis, and comparing these demands to available capacities at the performance levels of interest. The 1999 Chi-Chi Earthquake and other ground motions are used to obtain the structural performance under peak ground acceleration (PGA). Furthermore, the seismic damage index is adopted from

Chiu, Lyu, and Jean (2014) to measure the damage state of bridges. The seismic damage index corresponding to each earthquake event can be estimated while considering the occurrence time and PGAs of earthquakes for a bridge within a specific period. The Monte Carlo Simulation will then be used to specify the exceedance probability of a specified damage state.

Step 4: Conduct the Monte Carlo Simulation

In this step, we simulate the earthquake events that were obtained from local historical data using the Monte Carlo Simulation. The goal of these simulations is to estimate the earthquake maintenance probability (P_{ME}). P_{ME} may be calculated by counting the number of occurrences of earthquakes larger than the threshold values for Ay and Ac during the simulation period. The threshold values for Ay and Ac were set to 0.2g and 0.24g, respectively.

Step 5: Obtain the probability of earthquake-related maintenance (PME)

An annualised estimate of P_{ME} may be obtained after completing the Monte Carlo Simulation. Table 8 illustrates several examples of bridge maintenance probability over time.

<Insert Table 8 here>

Step 6: Obtain the probability of rebuilding due to earthquake damage (P_{RE})

The annual probability of rebuilding due to earthquake damage (P_{RE}) may be found using the results of the Monte Carlo Simulation by counting the number of earthquake incidents of magnitude > 0.24g.

5. Estimating the Maintenance and Rebuilding Cost

After acquiring all of the probability factors required for each risk factor in Section 4, this section explains the stepwise procedures that were used to calculate the maintenance and

rebuilding costs for the three risk factors. The artificial intelligence (AI) inference model ESIM is employed to build the prediction model to accurately estimate the costs. The datasets were obtained from the TBMS and the data were collected by the Directorate General of Highways (MOTC). The following subsection describes the stepwise procedures that were used.

5.1. Component Deterioration

Step 1: Determine the factors that influence component deterioration.

The factors that influence component deterioration include 9 inputs: CI, the Construction Cost Index, year of last maintenance, bridge area, bridge height, structural type, distance from sea, and location. The output factor is bridge maintenance cost.

Step 2: Establish historical cases.

A total of 160 cases were used to establish the dataset that was subsequently used to build the prediction model. Table 9 displays the statistical description of historical data that was used in the present study to estimate the cost of maintenance that is attributable to component deterioration. Additionally, Fig. 5 illustrates the distribution of each influencing factor.

<Insert Table 9 here>

<Insert Fig. 5 here>

Step 3: Develop AI-based prediction model for maintenance cost.

ESIM was used to develop the prediction model. The iteration was set to 100 and the range for C and γ were set to 0-200 and 0.0001-1, respectively. Ten-fold cross validation was used in data partitioning in order to minimise the bias associated with the random sampling of training and testing data cases. Table 10 displays the training and testing results obtained using ESIM. Root Mean Square Error (RMSE) was used to measure the performance. The data

were normalised to range: 0 - 1. The graph shows that the average RMSE training and testing errors were minimal: 0.10198 and 0.10167, respectively. These errors were small enough to justify the model as good for predicting the new cases.

<Insert Table 10 here>

Step 4: Predict the maintenance cost attributable to component deterioration (C_{MD}).

The maintenance cost attributable to component deterioration (C_{MD}) was predicted after all runs of the ESIM had been completed. Table 11 shows the final results of several examples of bridge maintenance costs over time.

<Insert Table 11 here>

5.2. Scouring

Step 1: Determine the factors that influence scouring.

The factors that influence scouring include 9 inputs: SSI, the Construction Cost Index, year of last maintenance, bridge area, bridge height, structural type, distance from sea, and location. The output factor is the cost of bridge maintenance attributable to scouring.

Step 2: Establish historical cases.

A total of 228 cases were used to establish the dataset that was used to build the prediction model. Table 12 displays the historical data used in the present study to estimate the maintenance cost that is attributable to scouring.

<Insert Table 12 here>

Step 3: Develop AI-based prediction model for maintenance cost.

This step is similar with the Section 5.1, step 3 above. Table 13 shows the training and testing results obtained by ESIM. The graphic shows that the average RMSE training and testing errors were minimal: 0.09697 and 0.09737, respectively. These errors were small enough to justify the model as good for predicting the new cases.

<Insert Table 13 here>

Step 4: Predict the maintenance cost attributable to scouring (C_{MS}).

The maintenance cost attributable to scouring (C_{MS}) was predicted after all runs of the ESIM had been completed. Table 14 shows the final results of several examples of bridge maintenance costs over time.

<Insert Table 14 here>

Step 4: Rebuilding cost attributable to scouring (C_{RS}).

In the absence of regular maintenance, bridges that are subject to scouring damage face a higher risk of bridge failure/collapse than those bridges that are not affected by scouring. Thus, the anticipated cost of rebuilding these bridges should be considered in long-term bridge budget strategies. The cost of rebuilding a bridge is the same regardless of the cause of failure (e.g., scouring, earthquake). Table 15 lists the estimated rebuilding costs for several bridges.

<Insert Table 15 here>

5.3. Earthquake

Step 1: Estimate the Earthquake Damage Ratio

This research applies an estimation concept that utilises the damage ratio to estimate the probabilities of various maintenance costs. Fig. 6 illustrates the methodology that was used to

obtain the C_{ME}, as suggested in reference (Chiu, Lyu, and Jean 2014). Each bridge has its own future damage probability, which is calculated during the earthquake events simulation.

<Insert Fig. 6 here>

Step 2: Earthquake maintenance cost (C_{ME})

Table 16 shows the final result of several examples of bridge maintenance costs for each damage ratio.

<Insert Table 16 here>

Step 3: Earthquake rebuilding cost (CRE)

Not performing regular maintenance on a bridge elevates the risk of bridge collapse during an earthquake. The cost of rebuilding is the same whether damage is attributable to an earthquake or to scouring. Thus, as described previously, the values of C_{RE} and C_{RS} are the same in the context of the same bridge (See Table 15).

6. Establishing the Bridge Maintenance Cost Optimisation model

This section integrates the maintenance probabilities, the rebuilding probabilities, and the associated costs in order to obtain the total expected cost E(Cost). Further, the SOS algorithm is used to identify the optimal E(Cost). The bridge maintenance and rebuilding probabilities (P_{MD}, P_{MS}, P_{RS}, P_{ME}, P_{RE}) were previously obtained using the Monte Carlo simulation in Section 4 and the bridge maintenance and rebuilding costs (C_{MD}, C_{MS}, C_{RS}, C_{ME}, C_{RE}) were previously estimated using ESIM in Section 5. The formula described in Section 3 is used to synthesise the obtained probabilities and costs in order to obtain the E(Cost).

Step 1: Optimal search with SOS algorithm method

The SOS algorithm was used to simulate different maintenance strategies and to iteratively improve the best strategy using its unique searching mechanisms. After creating an initial group of random maintenance strategies, the so-called "population", this population underwent three search phases: mutualism, commensalism, and parasitism. Each of the three operators stochastically updated the strategy by improving and preserving the best strategy in population.

<Insert Fig. 7 here>

Fig. 7 is an example of a typical maintenance strategy. In this example, the maintenance strategy implements maintenance activities at years 30 and 70. The chronological events of the strategy shown in Fig. 7 are explained as follows.

- The CI curve begins at the maximum value of 100 and declines along a path dictated by the corresponding CI slope. Maintenance should be conducted before the CI value drops below the CI threshold value.
- The first maintenance was performed at year 30, after which the CI value rises to a higher level (90). In this event, maintenance cost [E(MC)₃₀] and rebuilding cost [E(RC)₃₀] are added into the total expected cost calculation. After year 30, the CI begins declining from 90.
- 3. The second maintenance was performed at year 70, after which the CI value again rises to 90. In this event, maintenance cost [E(MC)₄₀] and rebuilding cost [E(RC)₄₀] are added to the total expected cost calculation.
- 4. At year 100 (the end of bridge life cycle), no maintenance is performed because the CI value remains above the CI threshold. Thus, only rebuilding cost [E(RC)₄₀] was added into the total expected cost calculation.

Each E(MC) and E(RC) was calculated using Eqs. (5) and (6). The full E(Cost) calculation of this maintenance strategy is:

$$E(Cost) = [E(MC)_{30} + E(MC)_{40}] + [E(RC)_{30} + E(RC)_{40} + E(RC)_{30}].$$

Step 2: Optimal life-cycle maintenance cost

The SOS optimising procedure is repeated for different levels of the CI threshold. In the present study, the CI threshold is set between 75 and 85. The SOS preserves the best strategy until the end of the optimisation procedure.

7. Experimental Results

The study uses the 3961 entries of historical bridge data that are included in the Taiwan Bridge Management System (TBMS). Most of the bridges included in the TBMS are reinforced concrete bridges and managed by Directorate General of Highways (MOTC). The life cycle of all of these bridges is assumed to be 100 years. REMBMS was performed in all four of the proposed stages.

After completing the third stage, all expected maintenance and rebuilding costs may be obtained by multiplying each probability with its associated cost. Tables 17 and 18 show the expected maintenance and rebuilding costs that are attributable to component deterioration, scour, and earthquake, respectively.

<Insert Table 17 here>

<Insert Table 18 here>

In the last stage, SOS used the corresponding maintenance and rebuilding costs to optimise the best strategy. The experiment was repeated using several threshold levels in the

range of 75 to 85 to further elicit the relationship between CI threshold and expected cost. Table 19 displays the best result of the REMBMS strategy after the completion of the optimisation process in detail and Fig. 8 depicts the CI declining curve for each period. Using a CI threshold of 85, maintenance on one of the bridges should be implemented during years 35, 45, 55, 65, 75, 85, and 100, with a total expected cost of NTD 135.764 million.

<Insert Table. 19 here>

<Insert Fig. 8 here>

Fig. 9 illustrates the relationship between CI threshold and expected cost. It is thus apparent that lower CI threshold values are associated with lower expected maintenance costs. However, it is important to remember that the model introduced in the present study does not consider traffic loading conditions or social costs. Therefore, the bridge management authority must consider these two factors in its ultimate determination of appropriate maintenance schedules and budgets. The REMBMS is designed to assist bridge management authorities by providing various strategic plan options for optimising the timing and budget for bridge maintenance.

<Insert Fig. 9 here>

8. Conclusions

The present research introduces a novel, integrated model called REMBMS. The solutions obtained using REMBMS provide significantly better maintenance timing and cost estimates than the bridge maintenance approach that is currently used by the transportation authorities in Taiwan. Reasons for the superiority of the REMBMS include: risk-factor identification considers scouring and earthquake damage as well as component deterioration as main risk factors; Monte Carlo simulation is used to determine risk probability; and ESIM is used to

extrapolate estimates of bridge maintenance cost from historical data. The total maintenance cost (E(Cost)) is calculated by multiplying each maintenance probability with its associated cost. Furthermore, the SOS optimises the given objective function to obtain the minimum E(Cost) for each bridge. The present study provides to bridge management authorities an effective approach for determining the optimal timing and budget for maintaining transportation bridges.

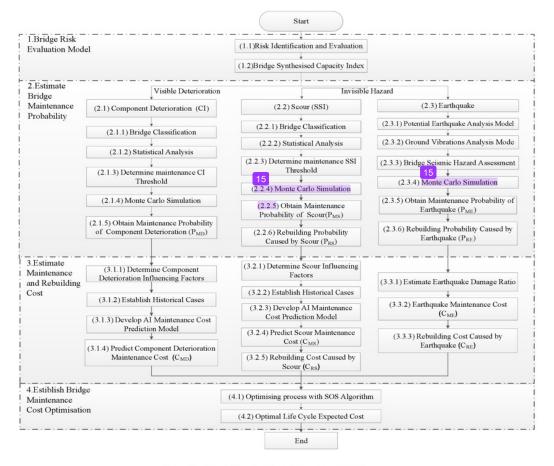


Fig. 1. Flowchart of main research steps

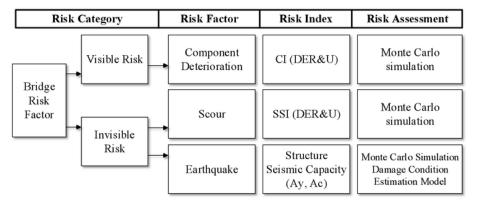


Fig. 2. Bridge risk evaluation diagram

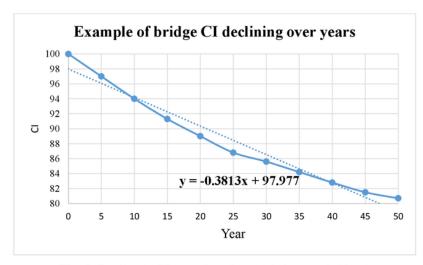


Fig. 3. Decline in CI over time (beam/girder type bridges)



Fig. 4. Photographic documentation for each bridge obtained from TBMS database

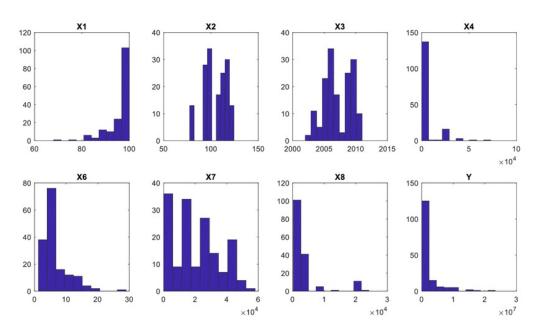


Fig. 5. Distribution of influencing factors

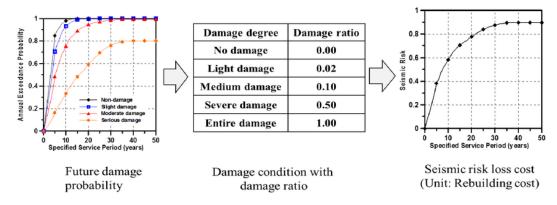


Fig. 6. Method used to obtain the earthquake maintenance cost (C_{ME})

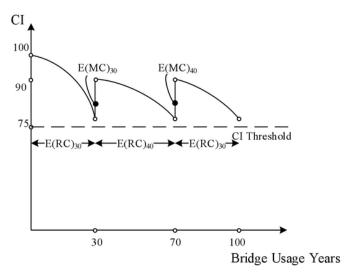


Fig. 7. Example of maintenance strategy (30th and 70th)

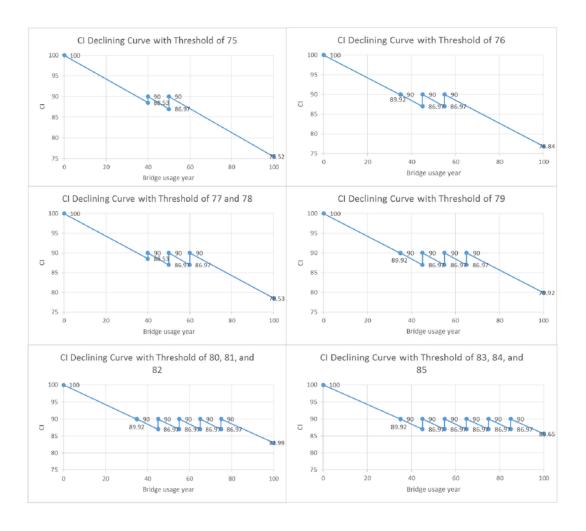


Fig. 8. CI declining curves for CI threshold values ranging from 75 to 85

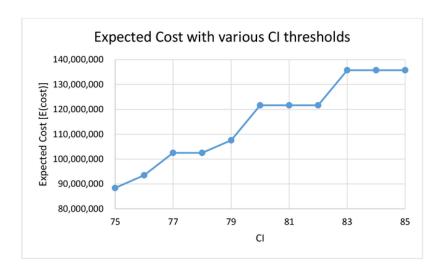


Fig. 9. Expected costs at various CI thresholds.

Table 1. Bridge elements and their weighting values $\left(w_{i}\right)$

Index	Element	Weighting value wi
1	Approach embankments	3
2	Approach quardrails	3 6 2
3	Waterway	4
4	Approach embankments protection works	3
5	Abutment foundation	7
6	Abutment	6
7	Wing/retaining wall	5
8	Surface/wearing coat	5 6 3
9	Superstructure drainage	4
10	Curb/sidewalk	2
11	Parapet	3
12	Pier protection work	6
13	Pier foundation	8
14	Pier and column	7
15	Bearing	5
16	Earthquake stopper/restrainer	5
17	Expansion joint	6
18	Girder	8
19	Diaphragm	6
20	Deck slab	7

Table 2. Bridge classifications in Taiwan

Type	Quantity
Truss bridge	63
Box bridge	1388
Cable-stayed bridge	62
Beam/Girder bridge	31778
Simple supported beam	130
Strut-frame bridge	115
Slab beam	8319
Arch bridge	289
Frame bridge	243

Table 3. The statistical analysis of the slope of beam/girder bridge

	-	-	-	-
Туре	Distance from the sea	Traffic loading	Average of	Variance of
1,700	(m)	(car/day)	slope	the slope
	<300	<6000	-0.230	0.047
	<300	6000~12000	-0.056	0.001
	<300	>12000	-0.405	0.000
	300~1000	<6000	-0.229	0.094
	300~1000	6000~12000	-0.060	0.001
Beam/girder	300~1000	>12000	-0.405	0.000
Beam/girder	1000~3000	<6000	-0.201	0.096
	1000~3000	6000~12000	-0.048	0.001
	1000~3000	>12000	-0.405	0.000
	>3000	< 6000	-0.275	0.552
	>3000	6000~12000	-0.242	0.053
	>3000	>12000	-0.284	0.048

Table 4. Bridge information

Bridge Number	Bridge Name	Design year	Length (m)	Width (m)	Number of spans
B04-0030-217A	Jiaxin bridge	1973	15.6	18	2
B04-0030-217B	Maoluo river bridge	1995	950	17.25	23
B04-0030-217C	Xinjia bridge	1956	6.3	22.4	1
B04-0030-217D	Xinjie bridge	2002	90	22	3
B04-0030-220A	Huzaikeng bridge	1955	40.2	22.6	2

Table 5. Annualised bridge maintenance probability attributable to component deterioration ($P_{\rm MD}$), Bridges B04-0030-217A to B04-0030-220A (%)

Bridge Number -										Υe	ears									
Bridge Number -	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
B04-0030-217A	0	0	0	0	0	0	0	0	0	1.7	36.8	97	100	100	100	100	100	100	100	100
B04-0030-217B	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O	0	0	O	0
B04-0030-217C	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
B04-0030-217D	0	0	0	0	0	0	0	0	0	2.3	39.1	97.1	100	100	100	100	100	100	100	100
B04-0030-220A	0	0	0	0	0	0	0	O	0	1.7	37.4	97.1	100	100	100	100	100	100	100	100

Table 6. Flood return period for Taiwan's main rivers, corresponding to the SSI slope index

Main since				Flood Ret	urn Period	1		
Main river	1-year	2-year	5-year	10-year	20-year	50-year	100-year	200-year
Tamsui	-1	-1	-2	-2	-3	-3	-3	-4
Fengshan	-1	-1	-7	-9	-11	-14	-17	-19
Touqian	-1	-1	-2	-3	-4	-5	-6	-7
Zhonggang	-2	-3	-4	-5	-6	-8	-9	-9
Houlong	-1	-1	-2	-2	-3	-3	-4	-5
Da-an	-1	-3	-5	-7	-10	-13	-16	-20
Dajia	-1	-3	-5	-7	-8	-10	-12	-13
Wu	-1	-1	-2	-2	-3	-3	-4	-5
Zhuoshui	-1	-7	-12	-15	-18	-22	-27	-30
Beigang	-1	-4	- 6	-7	- 9	-11	-12	-12
Puzi	-1	-2	-4	-5	- 6	-7	-8	- 9
Bazhang	-1	-2	-3	-4	-4	-5	-5	-6
Jishui	-1	-1	-2	-2	-3	-4	-5	-5
Cengwen	-1	-1	-2	-2	-2	-3	-3	-3
Yanshui	-1	-2	-4	-4	-5	-6	- 6	- 6
Erren	-1	-1	-1	-2	-3	-2	-2	-4
Gaoping	-1	-1	-2	-2	-3	-3	-3	-3
Donggang	-1	-3	-4	-5	-5	-6	-7	-8
Sicong	-1	-3	-4	-5	-6	-7	-7	-8
Beinan	-1	-1	-1	-2	-2	-2	-3	-3
Xiuguluan	-1	-2	-3	-4	-4	-5	-5	-6
Hualien	-1	-3	-4	-5	-5	-6	-7	-7
Heping	-1	-1	-2	-3	-3	-4	-5	-5
Lanyang	-1	-2	-2	-3	-3	-4	-5	-6

Table 7. Probability of scour-related maintenance over time (P_{MS}), Bridges B04-0030-217A to B04-0030-220A (%)

Bridge Number																				
Bridge Number	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
B04-0030-217A	0	0	0	0	0	0	0	0	0.2	0.6	0.8	0.7	0.4	0.5	0.7	0.7	3	1.5	1.8	1.6
B04-0030-217B	0	0	0	0	0	0	0	0	0.4	0.4	0.6	0.3	0.4	0.7	0.3	1	1.8	1.6	1.6	2
B04-0030-217C	0	0	0	0	0	0	0	0	0.3	0.8	0.6	0.5	0.5	0.4	0.4	0.6	1.9	2.2	1.9	1.6
B04-0030-217D	6.3	5.7	5.7	5.5	5.6	5	18.5	16.8	19.6	20.5	20.4	20.4	18.5	19.6	20.5	21.1	20.2	22.6	19.4	21.5
B04-0030-220A	0	0	0	0	0	0	0	0	0.7	0.2	0.8	0.7	0.8	0.6	0.2	0.4	2.1	2.8	1.5	1.5

Table 8. Probability of earthquake-related bridge maintenance over time (P_{ME}), Bridges B04-0030-217A to B04-0030-220A (%)

Duidee Namber										Ye	ars									
Bridge Number	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
B04-0030-217A	1	6.5	13	16.5	18.5	19.5	20	23.5	24.5	27.8	28.8	28.8	30.5	31.3	32	32.8	34.8	35.5	35.5	37.8
B04-0030-217B	1	1.25	2.25	2.75	3.75	4	5.25	6	6.5	7.5	8	9	9.75	11.3	11.8	13	14	14.5	15.5	18.8
B04-0030-217C	0.5	1.75	2	2.5	3.5	4.25	5.75	7	8.5	9.5	10.3	10.8	11.3	12.8	13	14	14.5	15	15.5	16.3
B04-0030-217D	9.5	16	28	32.8	34	35.5	39	40.5	44.5	49.3	50.5	50.8	53.3	55.8	59.3	62	63.3	65.8	67.8	71.5
B04-0030-220A	1.75	9.5	14.3	16.8	20.5	23.8	24.5	25.5	26.5	27.8	28.8	29.8	33.3	34.5	34.5	36.3	36.3	36.3	36.3	36.3

Table 9. Statistical description of historical data used to estimate the maintenance cost attributable to component deterioration (C_{MD})

Influencing Factors	Minimum	Maximum	Average	Standard Deviation
X1: CI	68	100	95.92	5.21
X2: Construction Cost Index	77.52	124.25	105.16	11.86
X3: Last maintenance (year)	2002	2011	2007.21	2.41
X4: Bridge area (m²)	40	72682	5008.28	11312.25
X5: Bridge height (m)	1.2	29	6.32	4.30
X6: Structural type	beam	, arch, cantileve	r, box girder,	truss
X7: Distance from sea (m)	7.70	57979.15	20447.31	15136.13
X8: Average Daily Traffic (ADT)	207.75	24142.25	4001.61	5289.56
X9: Location (mountain or not mountain?)	0	= not mountain	, 1 = mountair	ı
$Y \colon Bridge \ Maintenance \ Cost \ (C_{MD}) \ (in \ NTD)$	2,590	23,289,363	1,845,238	3,541,901

Table 10. ESIM Training and Testing Results

	Normalised	l RMSE	ESIM Parameters			
Fold	Training	Testing	C	γ		
1	0.0857	0.0976	192	0.6673		
2	0.0712	0.1582	198	0.8821		
3	0.1210	0.0934	66	0.1177		
4	0.1220	0.0465	7	0.5356		
5	0.1157	0.0630	50	0.2501		
6	0.1404	0.1068	28	0.0358		
7	0.1093	0.1728	24	0.2761		
8	0.0845	0.0745	126	0.9991		
9	0.0902	0.0827	140	0.5713		
10	0.0798	0.1212	200	0.9501		
Average	0.10198	0.10167				

Table 11. Bridge maintenance cost attributable to component deterioration (C_{MD}) by year, Bridges B04-0030-217A to B04-0030-220A (in New Taiwan Dollars/NTD)

Bridge Number		Years											
Bridge Number	1	2	3	4	5	6	7	8	9	10			
B04-0030-217A	769,327	769,327	769,327	769,327	769,327	769,327	769,327	769,327	769,327	769,327			
B04-0030-217B	518,158	426,196	320,167	200,228	66,307	81,353	242,970	418,419	607,865	810,986			
B04-0030-217C	751,985	652,901	539,671	412,192	270,438	114,565	55,610	239,671	437,862	649,824			
B04-0030-217D	69,327	769,327	769,327	769,327	769,327	769,327	769,327	769,327	769,327	769,327			
B04-0030-220A	47,688	286,148	568,542	889,987	1,268,394	1,690,465	2,155,155	2,684,238	3,231,054	3,815,305			
Deides Number	Years												
Bridge Number	11	12	13	14	15	16	17	18	19	20			
B04-0030-217A	769,327	769,327	769,327	769,327	769,327	769,327	769,327	769,327	769,327	769,327			
B04-0030-217B	1,027,954	1,258,565	1,502,612	1,760,181	2,031,273	2,315,774	2,613,132	2,923,737	3,246,854	3,583,088			
B04-0030-217C	876,045	1,116,318	1,370,070	1,637,835	1,919,359	2,214,250	2,522,517	2,843,734	3,178,572	3,526,268			
B04-0030-217D	769,327	769,327	769,327	769,327	769,327	769,327	769,327	769,327	769,327	769,327			
B04-0030-220A	4,448,906	5,128,277	5,854,979	6,621,112	7,429,297	8,267,156	9,135,507	10,022,185	10,964,802	11,912,463			

Table 12. Historical data used to estimate the maintenance cost attributable to scouring (C_{MS})

No	SSI	Construction Cost Index	Year of last maintenance	Bridge area (m²)	Bridge height (m)	Structural type	Location (mountain or not mountain)	Bridge Maintenance Cost (C _{MS})
1	99	93.24	2005	9956	11.3	Beam	0	1502
2	99	116.86	2010	1200	4.2	Beam	0	1711
3	99	100.00	2006	1500	3.5	Beam	0	3000
4	99	100.00	2006	1500	3.5	Beam	0	3000
5	99	81.14	2003	6900	5.5	Beam	0	3697
6	98	113.24	2009	3979	8	Beam	0	3974
7	99	113.24	2009	3979	8	Beam	0	3974
222	50	93.24	2005	1188	6.5	Beam	0	9750107
223	81	124.25	2008	2530	25	Box Girder	0	10068410
224	77	92.60	2004	846	5.7	Beam	0	10893683
225	80	113.24	2009	11400	20	Beam	0	11406937
226	80	113.24	2009	11400	20	Beam	0	11406937
227	80	113.24	2009	39627	4.6	Beam	0	11710030
228	80	93.24	2005	34452	10.33	Beam	0	12947501

Table 13. ESIM Training and Testing Results

F-14	Normalis	ed RMSE	ESIM Pa	arameters
Fold	Training	Testing	C	γ
1	0.0943	0.0989	200	0.4001
2	0.0955	0.0542	185	0.8705
3	0.0917	0.1013	120	0.6001
4	0.0875	0.1160	126	0.8881
5	0.0938	0.0819	192	0.5221
6	0.0993	0.0909	16	0.9592
7	0.1083	0.1434	0	0.7057
8	0.1158	0.1214	0	0.4705
9	0.0937	0.0675	189	0.8141
10	0.0898	0.0982	192	0.9571
Average	0.09697	0.09737		

Table 14. Bridge maintenance cost attributable to scouring (C_{MS}) by year, Bridges B04-0030-217A to B04-0030-220A (in NTD)

Bridge Number	Years									
Bridge Number	1	2	3	4	5	6	7	8	9	10
B04-0030-217A	1,588,471	1,588,471	1,588,471	1,588,471	1,588,471	1,588,471	1,588,471	1,588,471	1,588,471	1,588,471
B04-0030-217B	223,618	115,391	43,521	40,759	153,388	259,237	357,112	444,700	594,138	700,062
B04-0030-217C	529,977	438,355	382,116	307,305	233,041	136,315	71,107	13,532	102,462	217,098
B04-0030-217D	1,588,471	1,588,471	1,588,471	1,588,471	1,588,471	1,588,471	1,588,471	1,588,471	1,588,471	1,588,471
B04-0030-220A	2,728	152,986	259,548	425,425	568,759	729,117	889,111	1,006,588	1,181,400	1,372,786
Bridge Number					Ye	ars				
	11	12	13	14	15	16	17	18	19	20
B04-0030-217A	1,588,471	1,588,471	1,588,471	1,588,471	1,588,471	1,588,471	1,588,471	1,588,471	1,588,471	1,588,471
B04-0030-217B	806,704	916,970	1,043,477	1,200,898	1,295,841	1,436,030	1,516,496	1,671,207	1,798,494	1,920,305
B04-0030-217C	280,433	370,874	501,534	618,916	696,968	819,749	939,350	1,062,485	1,143,094	1,241,048
B04-0030-217D	1,588,471	1,588,471	1,588,471	1,588,471	1,588,471	1,588,471	1,588,471	1,588,471	1,588,471	1,588,471
B04-0030-220A	1,538,706	1,672,951	1,877,533	2,068,785	2,203,953	2,391,232	2,597,531	2,846,115	2,967,085	3,131,235

Table 15. Bridge rebuilding cost attributable to scouring damage (C_{RS}), Bridges B04-0030-217A to B04-0030-220A (in NTD)

Bridge Number	C_{RS}
B04-0030-217A	9,547,000
B04-0030-217B	737,438,000
B04-0030-217C	4,195,000
B04-0030-217D	67,320,000
B04-0030-220A	36,341,000

Table 16. Earthquake maintenance cost (C_{ME}) for each damage ratio, Bridges B04-0030-217A to B04-0030-220A (in NTD)

				C_{ME}		
Bridges	Rebuilding Cost	No	Light Damage	Medium	Severe	Entire Damage
		Damage	Light Damage	Damage	Damage	Entire Damage
B04-0030-217A	9,547,000	0	190,940	954,700	4,773,500	9,547,000
B04-0030-217B	737,438,000	0	14,748,760	73,743,800	368,719,000	737,438,000
B04-0030-217C	4,195,000	0	83,900	419,500	2,097,500	4,195,000
B04-0030-217D	67,320,000	0	1,346,400	6,732,000	33,660,000	67,320,000
B04-0030-220A	36,341,000	0	726,820	3,634,100	18,170,500	36,341,000

Table 17. Expected maintenance costs attributable to component deterioration, scour, and earthquake, Bridges B04-0030-217A to B04-0030-220A (in NTD)

Maintenance	Daidas Number		Years											
Costs	Bridge Number	1	2	3	4	5	6	7	8	9	10			
	B04-0030-217A	2,434	2,434	2,434	2,434	2,434	2,434	2,434	2,434	2,434	2,43			
	B04-0030-217B	148,200	148,200	148,200	148,200	148,200	148,200	148,200	148,200	148,200	148,20			
Рмр*Смр	B04-0030-217C	983	983	983	983	983	983	983	983	983	98			
	B04-0030-217D	14,040	14,040	14,040	14,040	14,040	14,040	14,040	14,040	14,040	14,04			
	B04-0030-220A	6,271	6,271	6,271	6,271	6,271	6,271	6,271	6,271	6,271	6,27			
	B04-0030-217A	0	0	0	0	0	0	0	0	3,177	9,53			
	B04-0030-217B	0	0	0	0	0	0	0	0	2,377	2,80			
$P_{MS} * C_{MS}$	B04-0030-217C	0	0	0	0	0	0	0	0	307	1,73			
	B04-0030-217D	100,074	90,543	90,543	87,366	88,954	79,424	293,867	266,863	311,340	325,63			
	B04-0030-220A	0	0	0	0	0	0	0	0	8,270	2,74			
	B04-0030-217A	95,470	620,555	1,241,110	1,575,255	1,766,195	1,861,665	1,909,400	2,243,545	2,339,015	2,649,29			
	B04-0030-217B	7,374,380	9,217,975	16,592,355	20,279,545	27,653,925	29,497,520	38,715,495	44,246,280	47,933,470	55,307,85			
$P_{ME} {}^{*}\!C_{ME}$	B04-0030-217C	20,975	73,413	83,900	104,875	146,825	178,288	241,213	293,650	356,575	398,52			
	B04-0030-217D	6,395,400	10,771,200	18,849,600	22,047,300	22,888,800	23,898,600	26,254,800	27,264,600	29,957,400	33,155,10			
	B04-0030-220A	635,968	3,452,395	5,178,593	6,087,118	7,449,905	8,630,988	8,903,545	9,266,955	9,630,365	10,084,62			
Maintenance							Years							
Costs	Bridge Number	11	12	13	14	15	16	17	18	19	20			
	B04-0030-217A	285,546	748,681	771,761	771,761	771,761	771,761	771,761	771,761	771,761	771,76			
	B04-0030-217B	148,200	148,200	148,200	148,200	148,200	148,200	148,200	148,200	148,200	148,20			
$P_{MD} * C_{MD}$	B04-0030-217C	983	983	983	983	983	983	983	983	983	98			
	B04-0030-217D	314,847	761,057	783,367	783,367	783,367	783,367	783,367	783,367	783,367	783,36			
	B04-0030-220A	1,670,162	4,985,829	5,861,251	6,627,383	7,435,568	8,273,427	9,141,778	10,028,456	10,971,074	11,918,73			
	B04-0030-217A	12,708	11,119	6,354	7,942	11,119	11,119	47,654	23,827	28,592	25,41			
	B04-0030-217B	4,840	2,751	4,174	8,406	3,888	14,360	27,297	26,739	28,776	38,40			
Pms*Cms	B04-0030-217C	1,683	1,854	2,508	2,476	2,788	4,918	17,848	23,375	21,719	19,85			
	B04-0030-217D	324,048	324,048	293,867	311,340	325,637	335,167	320,871	358,994	308,163	341,52			
	B04-0030-220A	12,310	11,711	15,020	12,413	4,408	9,565	54,548	79,691	44,506	46,96			
	B04-0030-217A	2,744,763	2,744,763	2,911,835	2,983,438	3,055,040	3,126,643	3,317,583	3,389,185	3,389,185	3,603,99			
	B04-0030-217B	58,995,040	66,369,420	71,900,205	82,961,775	86,648,965	95,866,940	103,241,320	106,928,510	114,302,890	138,269,62			
Рме*Сме	B04-0030-217C	429,988	450,963	471,938	534,863	545,350	587,300	608,275	629,250	650,225	681,68			
	B04-0030-217D	33,996,600	34,164,900	35,847,900	37,530,900	39,887,100	41,738,400	42,579,900	44,262,900	45,609,300	48,133,80			
	B04-0030-220A													

Table 18. Expected rebuilding costs attributable to component deterioration, scour, and earthquake, Bridges B04-0030-217A to B04-0030-220A (in NTD)

Rebuilding	Daides anabes					Ye	ars					
costs	Bridge number	1	2	3	4	5	6	7	8	9	10	
	B04-0030-217A	0	0	0	0	0	0	0	0	571	1,904	
	B04-0030-217B	0	0	0	0	0	0	0	0	1,142	1,269	
Ps*Crs	B04-0030-217C	0	0	0	0	0	0	0	0	857	2,539	
	B04-0030-217D	1,999	3,618	5,426	6,981	8,885	9,520	41,095	42,650	55,978	65,053	
	B04-0030-220A	0	0	0	0	0	0	0	0	1,999	635	
	B04-0030-217A	119,000	119,000	119,000	119,000	238,000	238,000	476,000	476,000	476,000	476,000	
	B04-0030-217B	0	0	0	0	0	0	0	0	0	(
$P_E * C_{RE}$	B04-0030-217C	0	0	0	0	0	0	0	0	0	(
	B04-0030-217D	0	0	119,000	119,000	119,000	119,000	238,000	357,000	476,000	476,000	
	B04-0030-220A	0	0	0	0	0	0	0	0	0	119,000	
Rebuilding	D.:I	Years										
Costs	Bridge number	11	12	13	14	15	16	17	18	19	20	
	B04-0030-217A	2,793	2,666	1,650	2,221	3,332	3,554	16,184	8,568	10,853	10,155	
	B04-0030-217B	2,094	1,142	1,650	3,110	1,428	5,077	9,710	9,139	9,647	12,693	
P_S*C_{RS}	B04-0030-217C	2,094	1,904	2,063	1,777	1,904	3,046	10,250	12,566	11,456	10,155	
	B04-0030-217D	71,210	77,683	76,319	87,076	97,580	107,132	108,972	129,091	116,969	136,453	
	B04-0030-220A	2,793	2,666	3,300	2,666	952	2,031	11,329	15,994	9,044	9,520	
	B04-0030-217A	476,000	595,000	595,000	595,000	595,000	595,000	595,000	595,000	595,000	595,000	
	B04-0030-217B	0	0	0	0	0	0	0	0	0	(
$P_E * C_{RE}$	B04-0030-217C	0	0	0	0	0	0	0	0	0	(
	B04-0030-217D	595,000	833,000	833,000	952,000	1,190,000	1,309,000	1,428,000	1,785,000	2,023,000	2,261,000	
	B04-0030-220A	119,000	119,000	238,000	238,000	238,000	357,000	476,000	476,000	476,000	476,000	

Table 19. The best maintenance strategies for Bridge A02-0080-000B after SOS optimisation, using four CI threshold values between 75 and 85 (in NTD)

Maintenance	Thresh	nold: 75	Thresl	nold: 76	 Thresl	nold: 84	Thres	Threshold: 85	
Maintenance year	CI value	Expected cost	CI value	Expected cost	 CI value	Expected cost	CI value	Expected cost	
0	100	0	100	0	 100	0	100	0	
5	-	-	-	-	 -	-	-	-	
10	-	-	-	-	 -	-	-	-	
15	-	-	-	-	 -	-	-	-	
20	-	-	-	-	 -	-	-	-	
25	-	-	-	-	 -	-	-	-	
30	-	-	-	-	 -	-	-	-	
35	-	-	89.92	65.333	 89.92	65.333	89.92	65.333	
40	88.53	74.316	-	-	 -	-	-	-	
45	-	-	86.97	14.086	 86.97	14.086	86.97	14.086	
50	86.97	14.086	-	-	 -	-	-	-	
55	-	-	86.97	14.086	 86.97	14.086	86.97	14.086	
60	-	-	-	-	 -	-	-	-	
65	-	-	-	-	 86.97	14.086	86.97	14.086	
70	-	-	-	-	 -	-	-	-	
75	-	-	-	-	 86.97	14.086	86.97	14.086	
80	-	-	-	-	 -	-	-	-	
85	-	-	-	-	 86.97	14.086	86.97	14.086	
90	-	-	-	-	 -	-	-	-	
95	-	-	-	-	 -	-	-	-	
100	75.52	0	76.84	0	 85.65	0	85.65	0	
Total Expected Cost		88.402		93.505		135.764		135.764	

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