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2 **EFFECT OF ULTRA-LOW TEMPERATURE ON SOME MECHANICAL**
3 **PROPERTIES OF PAINTED AND FILM-COATED PLYWOOD**
4

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16 **ABSTRACT**

17 Plywood is used for insulation systems in liquid natural gas cargo ships because of its good
18 thermal properties. However, there are only a few research investigating the mechanical properties
19 of plywood exposed to ultra-low temperatures. This study aims to determine how plywood reacts
20 when exposed to ultra-low temperatures, such as - 196 °C. To achieve this purpose, the present
21 study investigated the bending strength, modulus of elasticity, and tensile-shear strength of painted
22 and film-coated plywood under ultra-low temperatures. The mechanical properties of plywood
23 were discovered to be significantly impacted by the ultra-low temperature as a result of this
24 research.. Moreover, not only the bending strength of the painted and film-coated plywood
25 increased with decreasing temperature, but also the modules of elasticity of the painted and film-
26 coated plywood increased. At decreasing temperature, the tensile shear strength of the painted and
27 film-coated oven-dried plywood increased, but the ensile-shear strength of painted and film-coated
28 air-dried plywood decreased. The tensile shear strength of air-dried plywood was determined to be
29 more sensitive to the temperature change. Therefore, attention should be paid to plywood used in
30 liquefied natural gas cargo ships with high humidity.

31
32 **Keywords:** Bending, Birch, modulus of elasticity, plywood, tensile shear strength.

33 INTRODUCTION

34 The plywood is a large-surface engineered wood product which has uniform strength
35 properties, lower shrinking and swelling and could be defect-free. Phenol formaldehyde (PF) resin
36 is frequently used as an adhesive for outdoor plywood to improve water resistance, however,
37 melamine-urea formaldehyde (MUF) adhesives are preferred for plywood production due to their
38 low cost. However, it has been noticed that plywood bonded with MUF resin is less durable than
39 plywood bonded with PF resin in outdoor conditions (Öncel *et al.* 2019).

40 Mechanical properties such as bending strength (Kim *et al.* 2015, Kim *et al.* 2018), modulus
41 of elasticity (Kim *et al.* 2015, Kim *et al.* 2018), tensile strength (Kim *et al.* 2015) and compression
42 strength (Cha *et al.* 2020) have been found to increase during freezing in plywood made of the
43 MUF and PF resins. Similarly, it has been discovered that compression strength and bending
44 strength values increased in wood composites with decreasing temperatures (Ayrilmis *et al.* 2010,
45 Bekhta and Marutzky 2007). However, mechanical properties of plywood such as the bending
46 strength (BS), modulus of elasticity (MOE), and tensile-shear strength (TSS) decreased by low
47 thermal cyclic shock (Kim *et al.* 2015, Kim *et al.* 2018).

48 As the strength of the ice increases as the temperature decreases, it is thought to contribute
49 to the increase of the mechanical properties of the wood. On the other hand, the increase in
50 mechanical properties caused by the freezing of oven-dried wood can be explained by factors other
51 than water. These can be shown as the hardening of wood cell walls due to low-level freezing (Zhao
52 *et al.* 2015). In addition, at low temperatures, the intermolecular distance of the material decreases,
53 so the intermolecular strength increases, and more energy is necessary for the breaking down of
54 the sample (Zhao *et al.* 2015, Zhao *et al.* 2016). Ultra-low temperature applications stabilize the
55 crystalline structure and reduce residual stress, making materials (such as metals, alloys, plastics,

56 and composites) stronger and more durable. (Kalia 2010). For example, it was found that the BS
57 of a wooden baseball bat increased by 26 % when it was cryogenically treated to a temperature of
58 -190 °C for 24 h (Kendra and Cortez 2010).

59 The variations between the adhesives and thermal properties of wood will cause performance
60 concerns when the structure is subjected to significant changes in temperature. The design must
61 account for differential part movement while maintaining structural integrity. The efficiency of
62 glue lines is well established at elevated temperatures. There is little information on the stability of
63 glue lines at low temperatures, particularly extremely cold temperatures, although there have been
64 some studies of timber bridges in cold climates. Work on adhesive films at cold temperatures
65 combined with the effect of moisture content should also be studied. Specimens are required for
66 further research on the effect of temperature changes on the integrity of the bond surface (Wang *et*
67 *al.* 2015).

68 Plywood has recently, become popular in ultra-cold conditions, such as liquid natural gas
69 (LNG) cargo ships (Cha *et al.* 2020, Kim *et al.* 2015, Kim *et al.* 2018). Even though previous
70 studies have focused on the effects of ultra-low temperature on BS, MOE and compressive strength
71 on plywood, there is no study on tensile shear strength at ultra-low temperature for plywood.
72 Therefore, the aim of this study was to determine how plywood react when exposed to ultra-low
73 temperatures, such as -196 °C. In this paper, the mechanical properties such as modulus of rupture,
74 modulus of elasticity, and tensile shear strength of plywood were tested at the ultra-low
75 temperature.

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77

78 MATERIALS AND METHODS

79 Materials

80 The birch plywood samples coated with film and paint were obtained from EKOL Plywood
81 Company (Kastamonu, Turkey). Painting and coating were applied to only one side of 9-layer
82 plywood that were unprotected exterior types and produced using phenol formaldehyde resin from
83 rotary cut veneers. In the production of plywood, a single surface of the veneer was glued by using
84 an amount of 150 g/m² phenol formaldehyde resin. The pressure was set to 0,7 N/mm², the
85 temperature 110 °C, and the pressing time was 17 minutes. All plywood test samples were obtained
86 from commercially produced boards and cut in the longitudinal direction of the boards. The
87 moisture content of the film-coated and painted plywood boards were 8,33 % and 9,77 %,
88 respectively. Ten samples were prepared for the bending strength tests with the dimensions of 280
89 mm × 50 mm × 12 mm (L x W x T). Ten samples for the tensile-shear tests were prepared with
90 dimensions of 150 mm × 25 mm × 12 mm (L x W x T).

91 Determination of density

92 The densities of air-dried and oven-dried plywood materials were determined according to
93 TS EN 323 (TSE 1999). Ten samples with dimensions of 50 mm × 50 mm × 12 mm (L x W x T)
94 were prepared to determine density of the materials. To determine the oven-dried density of
95 samples, the samples were dried up to 103 °C ± 2 °C until they were in constant weight and were
96 weighed with a precision of 0,001 g on an analytical balance. To determine the air-dried density of
97 samples, the samples were kept in the climatized room adjusted to a temperature of 20 °C and
98 relative humidity of 65 % until they reached consistent weight. Subsequently, the wood material
99 dimensions were measured with a digital caliper with precisions of 1 % sensitivity, and volumes
100 were determined by a stereo-metric method.

101 **Freeze treatment**

102 The oven-dried conditioned samples were dried up to $103\text{ }^{\circ}\text{C} \pm 2\text{ }^{\circ}\text{C}$ until they reached
103 constant weight. After drying, each sample was placed into a container filled with liquid nitrogen
104 (LN_2) for 10 minutes (Fig. 1, a). Samples were taken out from the container just before testing. Air-
105 dried samples were conditioned for four weeks at $20\text{ }^{\circ}\text{C} \pm 2\text{ }^{\circ}\text{C}$ and relative humidity of $65\% \pm 5$
106 $\%$. After conditioning, each sample was placed into a container filled with LN_2 for 10 minutes. The
107 samples were taken out from the container just before testing.

108



109

110 **Figure 1:** Freezing treatment of plywood samples (a), bending test (b), tensile-shear test (c).

111

112 **Mechanical test**

113 The bending strength and tensile-shear strength tests of plywood samples were performed at
114 2.5 mm/min speed on Shimadzu™ AG-IC 20/50 KN STD Universal Testing machine (Fig. 1, b).
115 The experiment time between removing wood samples from LN_2 and performing mechanical tests
116 was calculated as one minute. The bending strength was conducted according to TS EN 310 (TSE
117 1999). Painted and film-coated plywood surfaces were tested in the tensile zone in the bending
118 strength test. Calculation of BS of the $280\text{ mm} \times 50\text{ mm} \times 12\text{ mm}$ (L x W x T) specimens was
119 made according to Eq. 1:

120

$$BS = \frac{3 \times F_{max} \times L}{2 \times b \times h^2} \left(\frac{N}{\text{mm}^2} \right) \quad (1)$$

121 where F_{max} : max. load (N), L : span (mm); b : width of cross-section (mm); h : dept of cross-section
122 (mm)

123 According to TS EN 310 (TSE 1999) standard, modulus of elasticity was carried out.
124 Calculation of MOE of the prepared specimens was made according to Eq. 2:

$$125 \quad MOE = \frac{(F_2 - F_1) \times L^3}{4 \times b \times h^3 \times (d_2 - d_1)} \left(\frac{N}{mm^2} \right) \quad (2)$$

126 where $F_2 - F_1$: increment of load on the straight-line portion of the deformation curve (N), L : span
127 (mm), b : width of cross-section (mm), h : dept of cross-section (mm), $d_2 - d_1$: increment of
128 deformation corresponding to $F_2 - F_1$ (mm).

129 The tensile-shear strength was performed according to TS 3969 EN 314-1 (TSE 1998)
130 standards (Fig. 1, c). Calculation of tensile-shear strength of the prepared specimens was made
131 according to Eq. 3:

$$132 \quad \sigma = \frac{F}{A} = \frac{F}{(L \times b)} \left(\frac{N}{mm^2} \right) \quad (3)$$

133 where σ : Tensile shear strength (N/mm²), F : maximum load (N), L : shear plate length (mm), b :
134 shear plate width (mm).

135 **Data analysis**

136 The statistical parameters like an analysis of variance (ANOVA) were calculated with SPSS
137 23 (IBM 2020).

138

139

140

141 **RESULTS AND DISCUSSION**

142 **Density**

143 The oven-dried painted plywood samples of 0,728 g/cm³ were kept at 20 °C ± 2 °C for 2
 144 weeks at 60 % ± 5 % and brought to 9,77 % balance humidity and the air-dried density value was
 145 0,763 g/cm³. The film-coated plywood samples with the oven-dried density of 0,703 g/cm³ were
 146 kept at 20 °C ± 2 °C for 2 weeks at 60 % ± 5 % and brought to 8,33 % balance humidity, and the
 147 air-dried density value was 0,738 g/cm³.

148 **Effect of freezing on the mechanical properties of plywood**

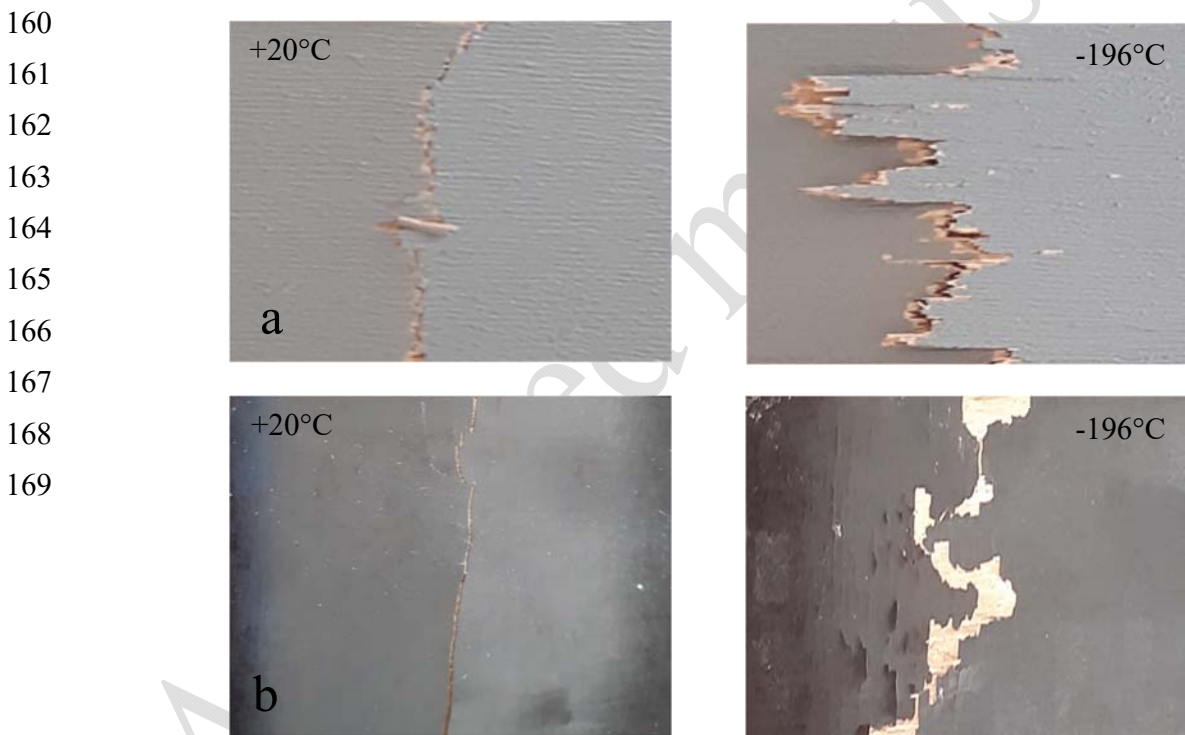
149 Table 1 shows the effect of ultra-low temperature on the BS, MOE, and tensile-shear strength
 150 (TSS) of the plywood.

151 **Table 1:** Mechanical properties of plywood at ultra-low temperature.

Plywood type	Temperature (°C)	Bending strength BS (N/mm ²)		Modules of elasticity MOE (N/mm ²)		Tensile shear strength (N/mm ²)	
		Oven dried	Air dried	Oven dried	Air dried	Oven dried	Air dried
Painted	+20 (Control)	97,34 ^{CD}	86,99 ^{DE}	12170,61 ^D	9943,59 ^F	1,929 ^C	3,012 ^{A*}
	-196	121,87 ^B	146,27 ^A	14744,47 ^B	15647,96 ^A	2,319 ^B	2,262 ^B
	Percent Change (%)	+25,20	+68,10	+21,10	+57,40	+20,20	-24,90
Film-coated	+20 (Control)	81,32 ^E	84,71 ^E	10810,84 ^E	10101,60 ^F	1,487 ^D	2,488 ^B
	-196	112,09 ^B	101,05 ^C	12848,16 ^C	14682,15 ^B	1,984 ^C	1,980 ^C
	Percent Change (%)	+37,80	+19,30	+18,80	+45,40	+33,40	-20,40

*Groups with the same letters in the column indicate that there was no statistical difference (p≤0,05) between the specimens according to Duncan's multiply range test.

152 Fig. 2 (a) and (b) show the fracture characteristics of the outer layer during the room and ultra-low
153 temperature in the bending test. At room temperature, the outermost layer of the plywood fractured
154 flat, while at ultra-low temperature a more fragmented fracture occurred. Temperature affects the
155 type of failure mechanism. The bonding force between the layers and the resin is not very strong
156 at room temperature. As a result, the ambient samples fail relatively easily at the resin-layer
157 interface, explaining the low MOE and MOR values. On the other hand, the resin is hardened and
158 the bonding force is relatively strong at cryogenic temperatures compared to ambient temperatures
159 (Kim *et al.* 2015).

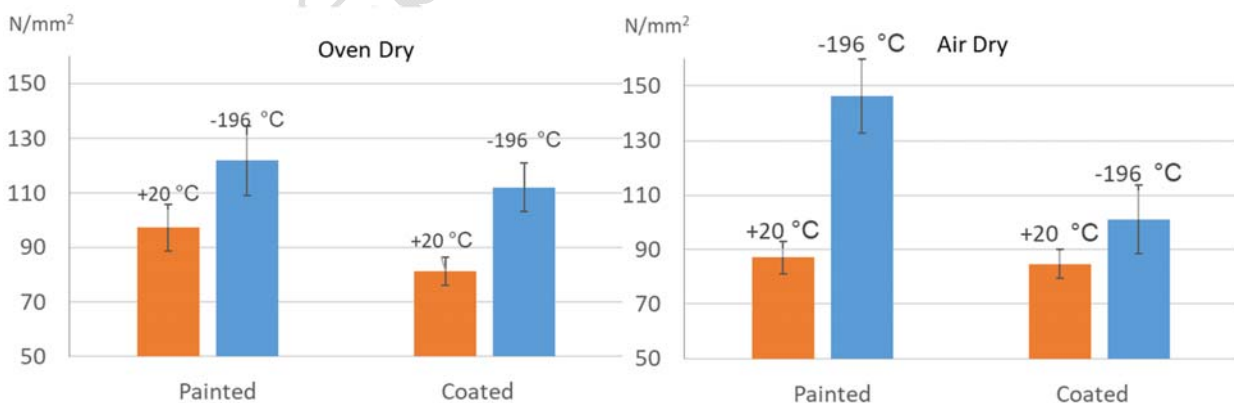


170
171 **Figure 2:** Fracture characteristics of painted (a) and film-coated (b) plywood between room
172 temperature (+20 °C) and ultra-low temperature (-196 °C).

173
174 Fig. 3 shows the effect of the ultra-low temperature on the bending strength. The BS of the
175 painted and film-coated plywood increased with decreasing temperature. For oven-dried and air-

176 dried painted plywood samples, with decreasing temperatures from +20 to -196 °C, the average BS
 177 was increased by 25,2 % and 68,1 %, respectively. For oven-dried and air-dried film-coated
 178 plywood samples, with decreasing temperatures from +20 °C to -196 °C, the average BS was
 179 increased by 37,8 % and 19,3 %, respectively. There was a statistically significant difference in the
 180 BS changes between +20 °C and -196 °C painted and film-coated plywood for oven-dried and air-
 181 dried humidity. However, the BS values did not significantly differ between oven-dried and air-
 182 dried film-coated at the temperature of 20 °C.

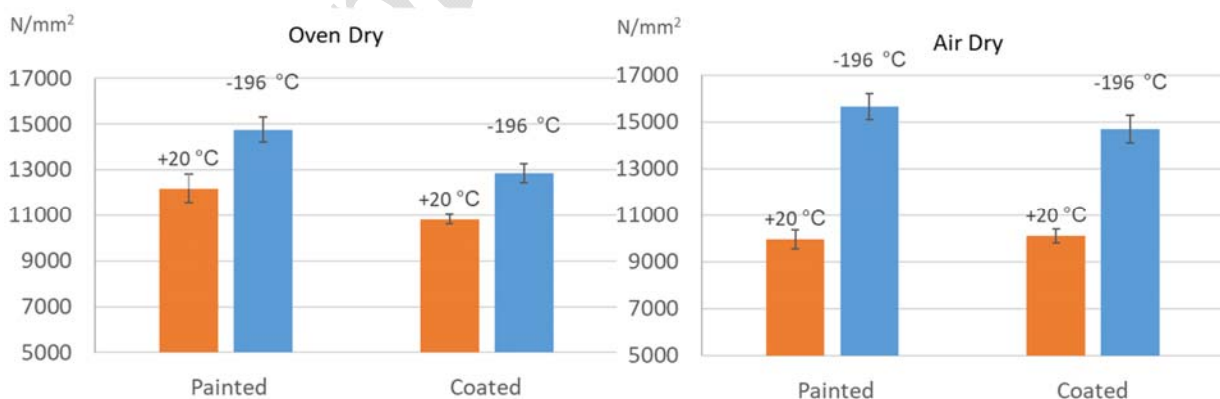
183 A previous study by Ayrilmis *et al.* (2010) reported that the BS values in plywood increased
 184 by 21,9 % when the temperature decreased from +20 °C to -30 °C. Similar trends were followed for
 185 MDF and OSB specimens because of increase in stiffness of the specimens at colder temperatures
 186 which may be attributed to ice crystals being formed on wood cell walls (Ayrilmis *et al.* 2010).
 187 Also, several researchers reported similar increases of BS and MOE with decreasing temperature
 188 in particleboard (Bekhta and Marutzky 2007), in solid beech wood (Özkan 2021). Drake *et al.*
 189 (2015) investigated the shear behavior of glulam beams with the four-point bending test between -
 190 40 and +20 °C. As a result of cooling from +20 to -40 °C, the strength and stiffness of the beams
 191 increased with decreasing temperature.



192 **Figure 3:** The effect of ultra-low temperature on the bending strength of the painted and film-
 193 coated plywood.

194 Fig. 4 shows the effect of the ultra-low temperature on the modules of elasticity. The MOE
 195 of the painted and film-coated plywood increased with decreasing temperature. For oven-dried and
 196 air-dried painted plywood samples , the average MOE was increased by 21,1 % and 57,4 %,
 197 respectively with decreasing temperatures from +20 to -196 °C whereas the average MOE was
 198 increased by 18,8 % and 45,4 %, respectively for oven-dried and air-dried film-coated plywood
 199 samples. There was a statistically significant difference in the MOE changes between +20 °C and
 200 -196 °C painted and film-coated plywood for oven-dried and air-dried humidity.

201 Bekhta and Marutzky (2007) examined BS and MOE values changes between -40 and +40
 202 °C in particleboards with 12 % humidity. As a result of cooling from +40 to -40 °C, the BS and
 203 MOE values increased by 34 % and 38 %, respectively. Cha *et al.* (2020) found that the MOE of
 204 plywood increased with decreasing temperature. Zhao *et al.* (2015) studied the MOE of water-
 205 saturated, fresh-cut, air-dried, and oven-dried birch (*Betula platyphylla*) wood under the
 206 temperatures at +20 °C and -196 °C. The results showed that the MOE of birch wood with different
 207 MCs increased with low-temperature treatment. Furthermore, the low-temperature application had
 208 more effect on specimens with higher MC than specimens with lower MC.

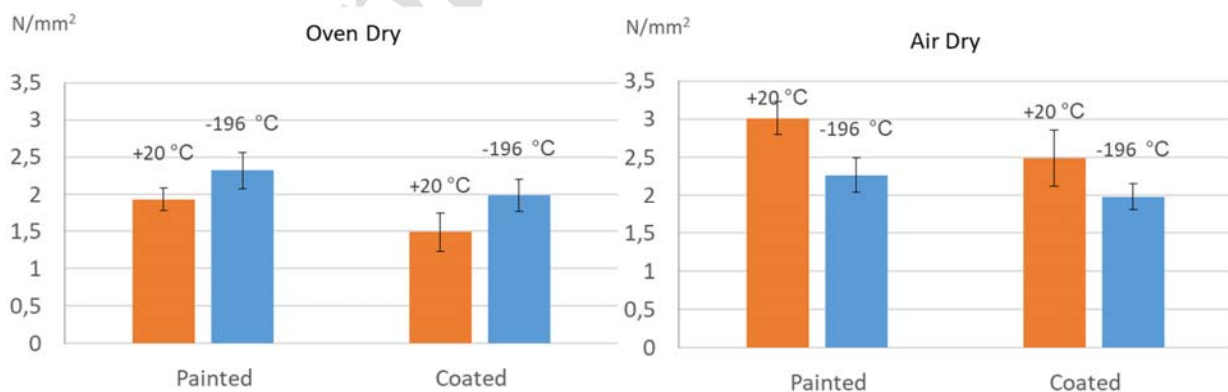


209 **Figure 4:** The effect of ultra-low temperature on the modules of elasticity of the painted and film-
 210 coated plywood.

211 Fig. 5 shows the effect of the ultra-low temperature on the tensile shear strength. The TSS of
 212 the painted and film-coated oven-dried plywood increased with decreasing temperature. But, the

213 TSS of painted and film-coated air-dried plywood decreased with decreasing temperature. For
 214 oven-dried painted and film-coated plywood samples, with decreasing temperatures from +20 °C
 215 to -196 °C, the average TSS was increased by 20,2 % and 33,4 %, respectively. For painted and
 216 film-coated air-dried plywood samples, with decreasing temperatures from +20 °C to -196 °C, the
 217 average TSS declined by 24,9 % and 20,4 %, respectively. There was a statistically significant
 218 difference in the TSS changes between +20 °C and -196 °C painted and film-coated plywood for
 219 oven-dried and air-dried humidity. However, there was no a statistically significant difference in
 220 the TSS between oven-dried and air-dried plywood at -196 °C.

221 Wang *et al.* (2015) investigated the shear strength of Norway spruce (*Picea abies*) joints,
 222 which were glued with seven different commercially available adhesives and evaluated at six
 223 different temperatures: -60, -50, -40, -30, -20, and +20 °C. the temperature changes have a
 224 considerable impact on the shear strength of wood joints in general. For example, as temperature
 225 dropped, the shear strength of wood joints bonded with different adhesives also reduced. Using
 226 polyurethane adhesive gave the highest shear strength, while the adhesive with the lowest shear
 227 strength was melamine urea-formaldehyde.



228 **Figure 5:** The effect of ultra-low temperature on the tensile shear strength of the painted and film-
 229 coated plywood.

230
 231

232 **CONCLUSIONS**

233 In the present study, the mechanical and fracture characteristics of the painted and film-
234 coated plywood were investigated at ultra-low temperatures. The main conclusion is as follows:

- 235 • The mechanical and fracture characteristics of the PF resin plywood used in ultra-low
236 temperatures were determined in oven-dried and air-dried humidity.
- 237 • The painted air-dried plywood showed the highest bending strength, tested at -196 °C
238 temperature while film-coated air-dried showed the weakest bending strength tested at +20
239 °C temperature.
- 240 • The painted air-dried plywood had the highest MOE value when tested at -196 °C
241 temperature, while film-coated air-dried and painted air-dried panels had the lowest MOE
242 value tested at +20 °C temperature. As a result, the brittleness of the wood increases during
243 freezing as the bending strength increases,.
- 244 • The tensile-shear strength of plywood at temperatures of +20 and -196 °C was studied.
245 Generally, the tensile-shear strength of painted plywood resisted the effects of ultra-low
246 temperature better than that of film-coated plywood. It was also determined that there was
247 a decrease in the tensile-shear strength of air-dried samples due to the temperature decrease.
248 It shows that the water in the wood material harms the adhesion strength of the glue in cold
249 climates.

250 The findings of this study support the design of LNG containers using plywood for structural
251 safety at ultra-low temperatures. Also, this study gives an idea about the ultra-low temperature
252 resistance of PF resin plywood. As a result, PF resin plywood can be used in an ultra-low
253 temperature environment depending on the humidity.

254

255 **AUTHORSHIP CONTRIBUTIONS**

256 M. O.: Conceptualization, Formal analysis, Investigation, Methodology, Project administration,
257 Supervision, Writing-original draft. O. E. O.: Investigation, Resources, Writing-original draft.

258

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