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Rapid prototyping for Martian space systems

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Rapid prototyping for Martian space systems

Giuseppe Governale, Jasmine Rimani, Giuseppe Narducci, Nicole Viola, Roberta Fusaro

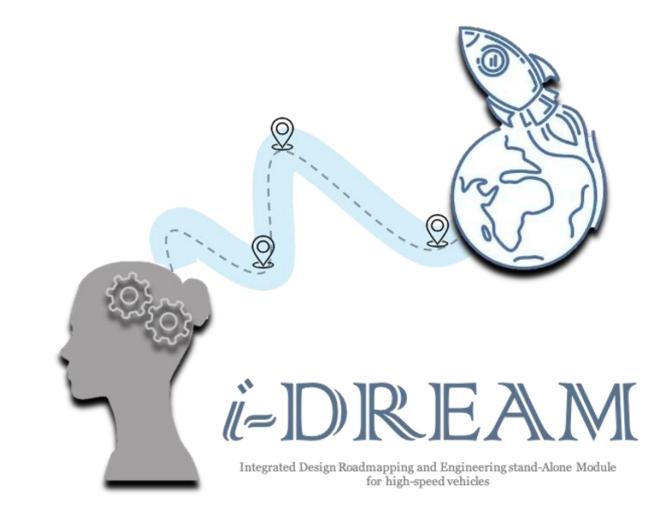
Moving To Mars (M2M) 2022 Workshop Montreal, Canada

Overview

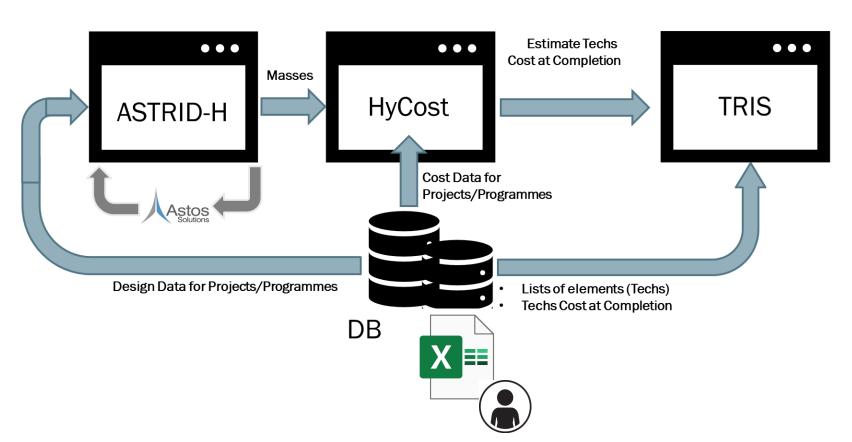
1. iDREAM overview and its capabilities

for microlaunchers and lunar vehicle

- Database HyDAT
- Design iASTRID-H
- Cost HyCost
- Technology Roadmap TRIS
- 2. iDREAM Mars application



iDREAM Integrated Framework



1. iastrid-h

Design and Mission Analysis

 Mission Analysis in ASTOS

2. HyCost

Cost estimation - LCC assessment

3. TRIS

Technology Roadmap

Database - HyDat

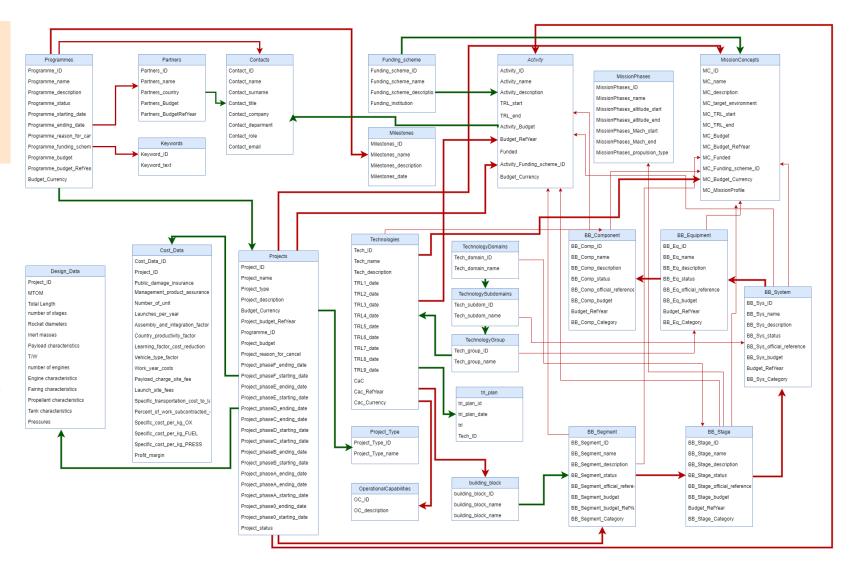
Heritage of POLITO technology roadmapping database for

- √ Hypersonic transportation systems
- √ Reusable access to space vehicles

A **MySQL database** supporting the whole iDRFAM framework:

- Design & mission analysis
- Cost Estimation
- Technology Roadmap

Equipped with unified connection by an ad-hoc developed **Database**Management Library for the operations of data input/output from/to the database throughout the tool modules.



iDREAM Microlaunchers





Design Routine - ASTRID H ML

Design Philosophy

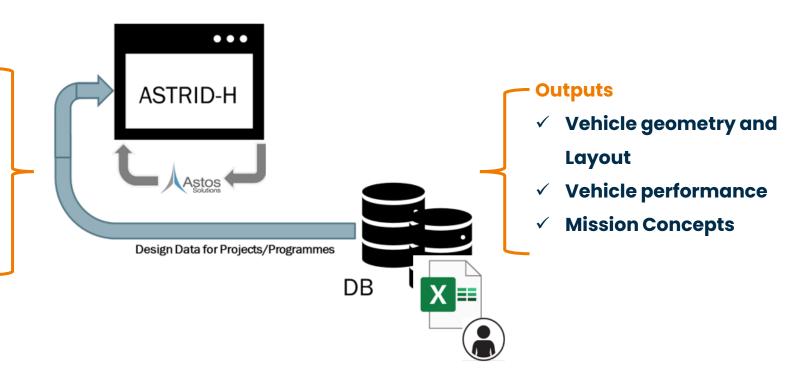
The microlaunchers design methodology follows a top-down approach.

From high-level requirements to subsystems design through the vehicle main parameters.

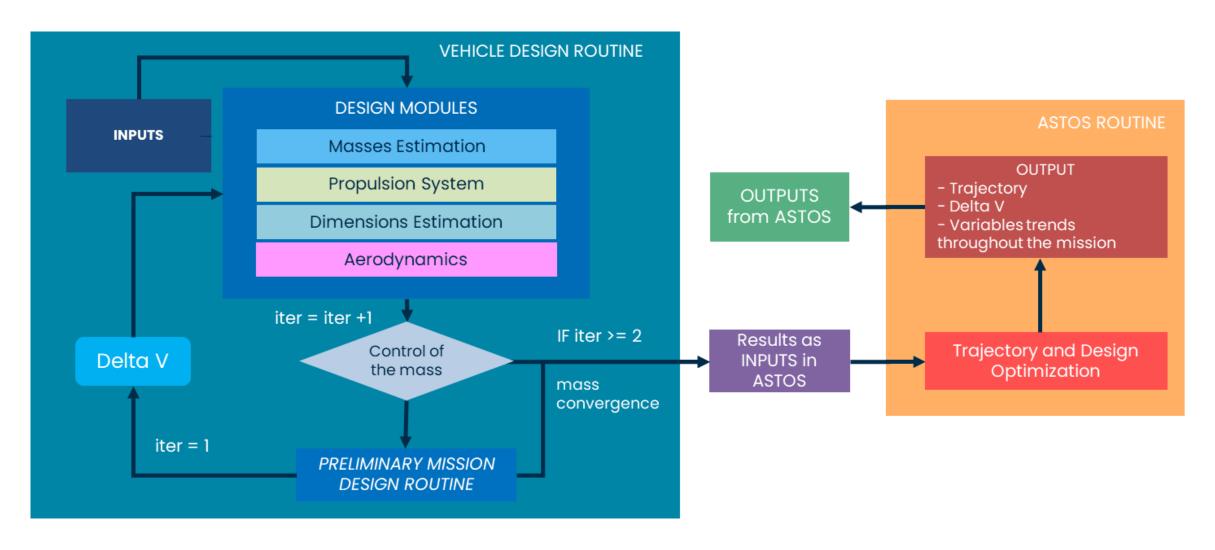
Design Routine Logic

Inputs from DATABASE (or User)

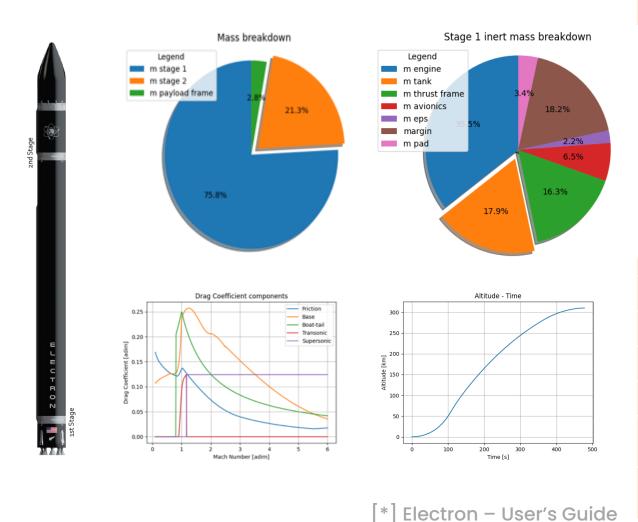
- Mission data (target orbit, launch site, inclination and launch azimuth)
- Nominal Payload Mass
- Propellants' characteristics (specific impulse, mixture ratio and densities)



Microlauncher Design Routine



MicroLauncher Design Routine- Outputs



Global Input Variable Name	iDREAM – Preliminary Design	Electron [*]	Percentage differences [%]
Payload Mass [kg]	268.59	280.00	-4.08
Payload Diameter [m]	1.07	1.08	-0.93
MTOM [t]	12.49	12.5	-0.08
1st Stage Inert Mass [t]	0.89	0.90	-1.11
2 nd Stage Inert Mass [t]	0.19	0.20	-5.00
Fairing mass [kg]	44.04	44.00	0.09
Fairing Length [m]	2.57	2.40	7.08
Total Length [m]	18.00	18.00	0.00
1st Stage Thrust [kN]	244.97	224.30	9.22
2 nd Stage Thrust [kN]	27.79	25.8	7.71
1st Stage engine mass [kg]	35.58	35.00	1.66
2 nd Stage engine mass [kg]	38.15	35.00	9.00



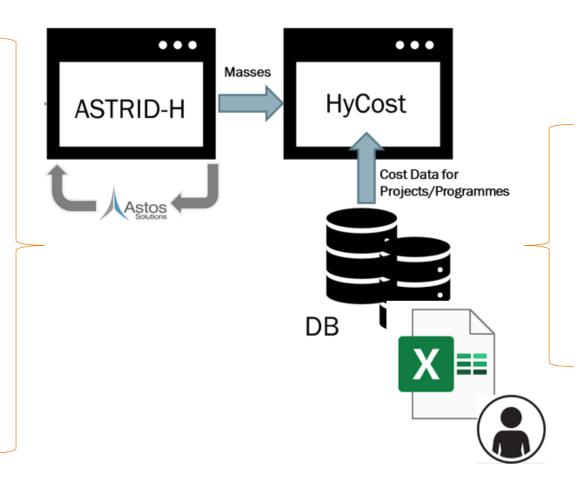
Cost Estimation routine – HyCost ML

Inputs from **DATABASE** (or User)

✓ Cost parameters

Inputs from **DESIGN routine** (or User)

- ✓ Pressurizant Tank mass
- ✓ Fuel Tank mass
- ✓ Oxidizer Tank mass
- √ Stage structure mass
- ✓ Engine(s) mass
- ✓ Thrust Vector Control mass.
- ✓ Pipes mass
- √ Valves mass
- ✓ Stage Harness mass
- ✓ Payload mass
- Avionics mass
- ✓ Attitude mass
- ✓ Interstage mass



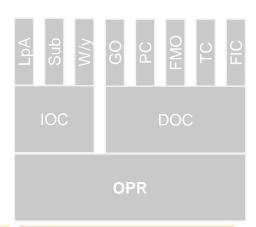
Outputs

- ✓ LCC assesment
 - **Development** cost
 - Operating cost
 - Manufacturing cost
 - · Cost per flight
 - Price per flight
- ✓ Technologies Cost at Completion

Cost Estimation Methodology ML

Based on T1 equivalent units
Applicable at subsystem and
equipment level





Launch Vehicle
Breakdown

Parts masses for FU costs

CER using FU for DEV costs (NRC)

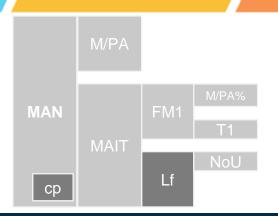
(RC, learning)
FU for MAN costs

(not from BDS)
CER for OPR costs

 $T1 = a * Mass^b$ a, b, regression coeff. [historical subsystem]

data]

based on Drenthe, 2016



Commercial factor ML

Scaling factor (cp) considering commercial applications: less subcontractors, more profit retain.

Considered in both development and manufacturing costs.

	Scale Factor S_m	2.85
	Original Cost Contributions	Scaled Commercial Cost Contributions
Management (M)	10%	3.5%
Product Assurance (PA)	5%	1.8%
Integration & Test (I&T)	9%	3.2%
Total Development Cost Contribution	26%	8.6%
Cost Reduction		-13.7%

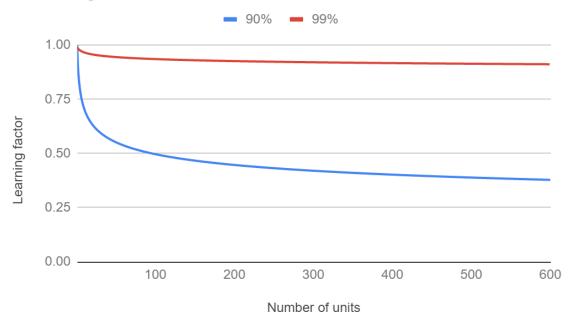
Learning factor ML

Mainly in the manufacturing costs, different learning curves wrt to the process

- 3D printing (99%)
- Traditional manufacturing (90%)

Azul Costs	[k€]	[k€]
MAN (t) 3D print.	501,823	23,186
MAN (t) BaU	478,637	
MAN (u) 3D print.	10,036	464
MAN (u) BaU	9,573	
3D printing	delta	+4.8%

Learning curves



PROs	CONs
lower unit cost for new components	not decreasing with production volume
less parts, easier integration	lower Stress/Number of Cycles curve
faster and less workers	high raw material cost

3D printing feature



Technology Roadmap routine - TRIS

Technology Roadmap Philosophy

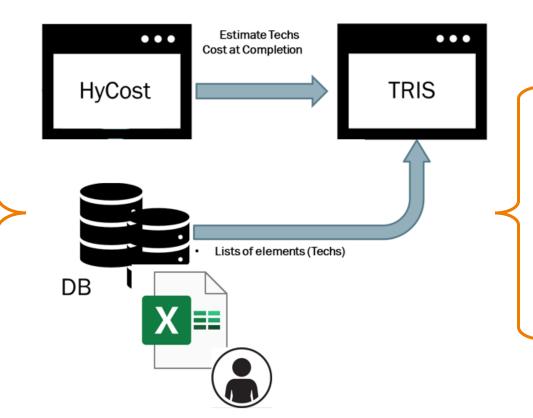
To generate technology roadmaps in support of strategic decisions, highlighting possible incremental paths towards the end-goal thanks to the exploitation of common System Engineering tools and processes.

Technology Roadmapping Routine Logic

Inputs from DATABASE (or User) and '

COST ROUTINE

- Stakeholder lists and characterization
- ✓ Elements lists:
 - Building blocks
 - Mission Concepts
 - Operational Capabilities
 - Technologies
- ✓ Elements characterization
 - Links between elements
 - o TRL
 - Costs
 - O ...



Outputs

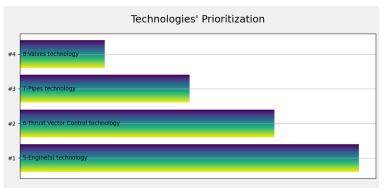
- Technology roadmap
 - Techs prioritization
 - Mission conceptsprioritization
 - Techs planning
 - Mission conceptsplanning

13

Technology Roadmap methodology

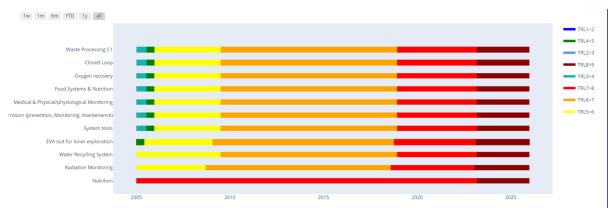
Prioritization Studies





The list of technology and activities are ordered as for the Stakeholders needs.

Planning definition





iDREAM Human Landing System





Design Routine - ASTRID H HLS

Design Philosophy

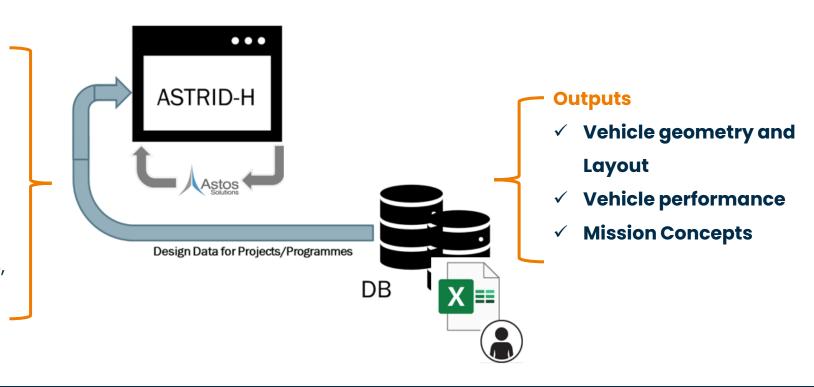
The human landing system **design** methodology follows a **bottom-up approach**.

From subsystems to the whole vehicle design.

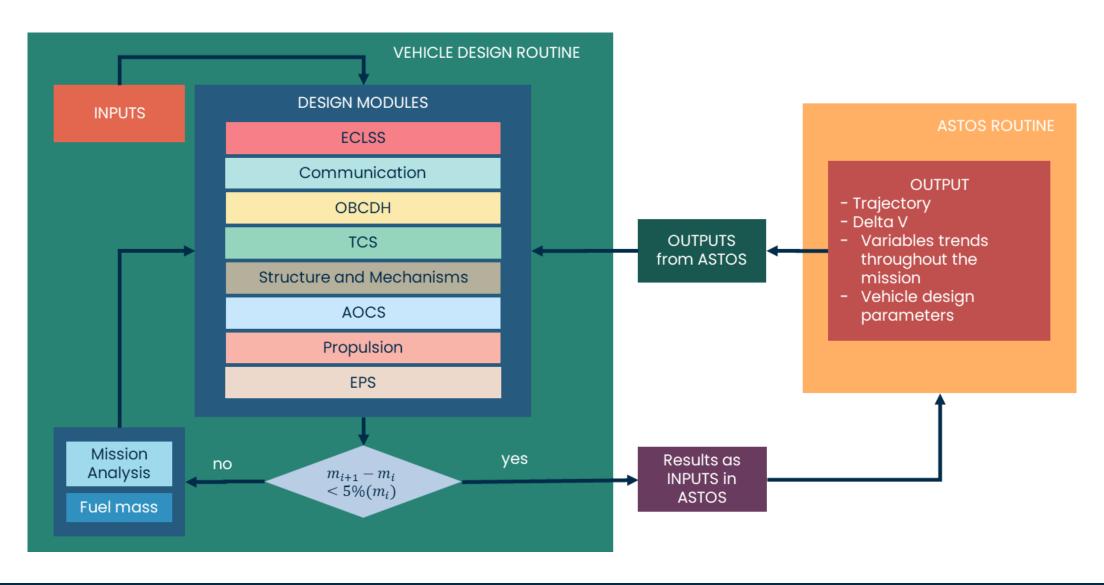
Design Routine Logic

Inputs from DATABASE (or User)

- Mission data: estimated deltaVs, mission phases time
- ✓ Nominal payload mass
- ✓ Number of crew
- ✓ Total mission time
- ✓ Subsystems data: PROPULSION, ECLSS, COMM, CDH, AOCS, TCS, STR, EPS)



Human Landing System Design Routine



Cost Estimation routine – HyCost HLS

Cost Philosophy

The human landing system **cost** methodology is based on the Advanced Mission Cost Model (AMCM)

Additionally, a cost estimation based on the analogy method was developed.

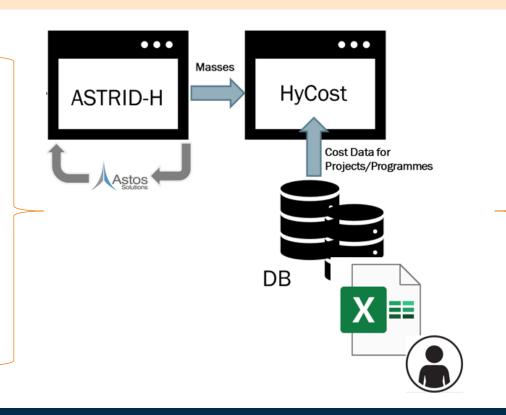
Cost Routine Logic

Inputs from **DATABASE** (or User)

- Number of units
- ✓ Initial Operating Capability year
- ✓ Inheritance
- ✓ Difficulty
- √ Mission Type

Inputs from **DESIGN routine** (or User)

✓ Dry mass



Outputs

- ✓ LCC assesment
 - **Development** cost
 - Operating cost
 - Manufacturing cost

Human Landing System - Cost Estimation - Validation

The budget allocated for the HLS in the Artemis program is

21,300

\$FY2020M

The result of the cost estimation by analogy for the HLS is

18,619

\$FY2020M

The result of the AMCM cost estimation is equal to

17,618

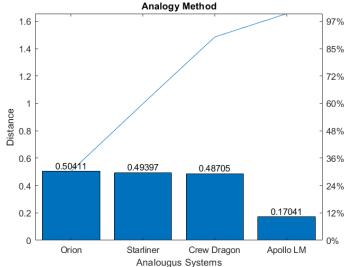
\$FY2020M

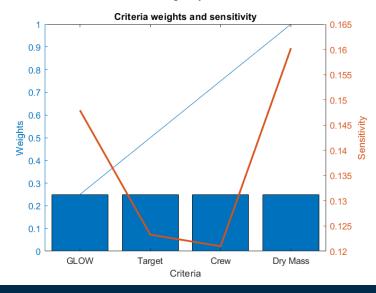
-14%

from the allocated budget

+5%

from the AMCM model

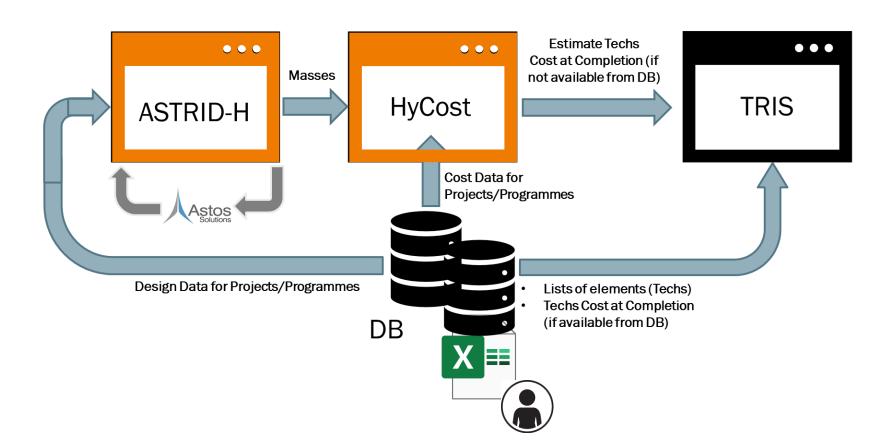




iDREAM Mars



iDREAM for Mars



DESIGN

- 1. Propulsion
 - i. Nuclear or others
- 2. ECLSS
 - i. Lower in %mass
 - ii. Artificial gravity

COST

- 1. AMCM
- 2. Analogy method

Conclusions

iDREAM is an integrated vehicle design routine with the capabilities of:

- ✓ providing a preliminary design of the studied system
- ✓ estimating the overall life-cycle cost of the designed system
- ✓ supporting the evaluation of technology roadmaps

The three modules of iDREAM can be used as standalone software

✓ iDREAM has been validated for microlaunchers and lunar applications.

iDREAM will be extended to provide design, life-cost assessment and technology roadmapping analysis for other space systems, such as Mars missions, for both orbital and surface systems

- ✓ The HyDat database is continuously updated
- ✓ An overview of the main affecting changes to the iDREAM routines has been presented for the Mars case



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Thanks for your attention

Any questions?



polito.it

bit.ly/SEEDSMaster22

Validation Study





MicroLauncher Design Routine-Inputs



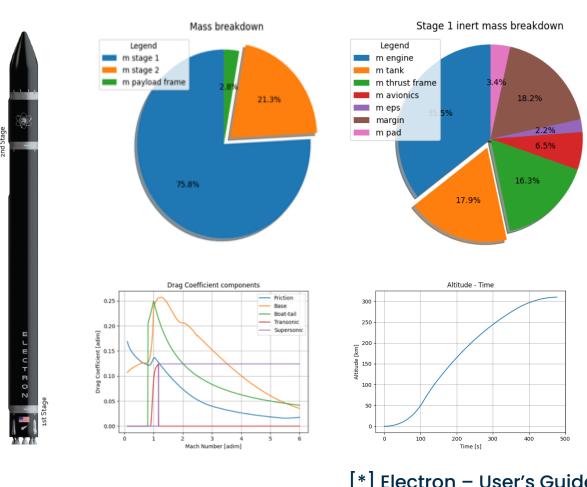
The Electron launch vehicle is fully designed and manufactured by Rocket Lab. It combines the latest manufacturing technologies with the capability of multiple launch ranges in a domestic launch site (Mahia Launch Complex or Rocket Lab Launch Complex).

Electron exists both as a 2-stage and as a 3-stage configuration. In this case, the 2-stage architecture is analysed

Vehicle design inputs

Global Input Variable Name	Value
Target Orbit [km]	300.00
Orbital Inclination [deg]	45
Launch site selection	Mahia, New Zealand
Number of stages	2
Nominal payload mass [kg]	200.0
Rocket diameters [m]	1.2
Thrust over weigth stage 1	2.0
Thrust over weigth stage 2	0.95
Maximum Take Off Mass [t]	12.5
Total Length [m]	18.0
Stage 1 Propellant	LOX/RP1
Stage 2 Propellant	LOX/RP1
Number of engine first stage	9.0
Number of engine second stage	1.0

MicroLauncher Design Routine- Outputs



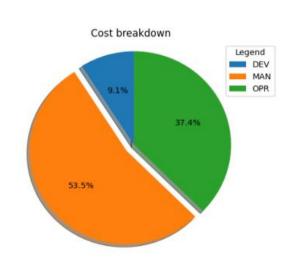
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1 st Stage engine mass [kg]	35.58	35.00	1.66
2 nd Stage engine mass [kg]	38.15	35.00	9.00

[*] Electron – User's Guide



MicroLauncher Cost Estimation Routine - Outputs





	Price per Flight [M€]	Specific price [k€/kg]
Electron	16	54
idream	17	52
Percentage differences [%]	7%	-4%



ML Backup





Microlaunchers design methodology

Main Requirements

- ✓ i-DREAM shall support the conceptual and preliminary design of Microlaunchers (MLs) and related reference missions.
- ✓ For the Mission Analysis, iDREAM shall make benefit of the commercial software ASTOS.
- ✓ The ML design methodology shall enable two different types of analysis:
 - o Assessment and verification of an already existing ML design (Existing routine) supported by the HyDat Database
 - o Definition of a new ML design and reference mission starting from a set of high-level requirements (New routine)

Expected Tool Developments

- ✓ Upgraded version of ASTRID-H (Aircraft on-board Systems sizing and TRade-off analysis in Initial Design)
 - ASTRID-H is a proprietary tool of the research group of Politecnico di Torino, developed for almost a decade through different research activities.
 - ASTRID-H has been validated for the conceptual and preliminary design of a wide-range of transportation system from civil aviation to access to Space and beyond.
- ✓ Exploitation of ASTOS commercial software to support the design of MLs with reliable and accurate Mission Analysis.
- ✓ Upgraded version of HyDat , a database developed by Politecnico di Torino to support technology roadmapping activities of ESA for hypersonic transportation systems and Reuseble Access to Space Vehicles

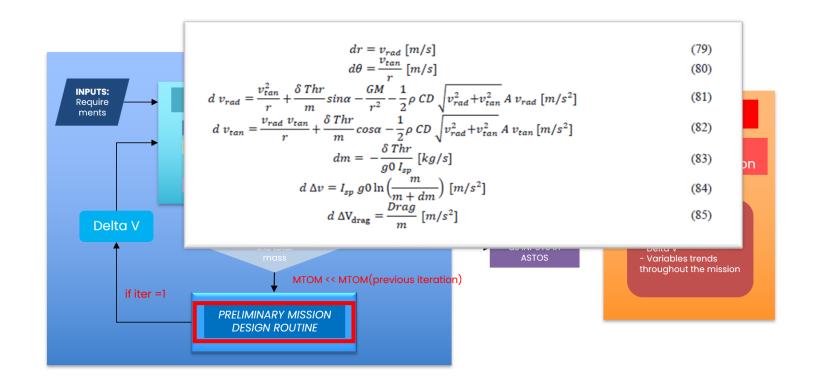


Micro-Launcher Design Routine (III)

Preliminary Mission Module ->

- First trajectory estimation;
- Variable trends throughout the mission;
- 3) Delta V and Gravity and Drag Losses.

Starting point for new iterations!



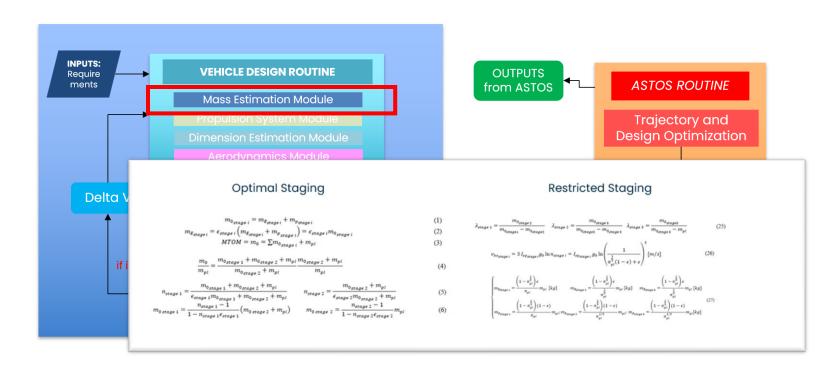


- [5] O. Sutton and G. Biblarz, Rocket Propulsion Elements.
- [6] F. Castellini, Multidisciplinary Design Optimization for expendable launch vehicles, 2012.
- 7] R. Ernst, Liquid Rocket Analysis (LiRA). Development of a Liquid Bi-Propellant Rocket Engine.
- [8] S. Contant, Design and Optimization of a Small Reusable Launch Vehicle Using Vertical Landing Techniques.
- [9] F. Miranda, Design Optimization of Ground and Air-Launched Hybrid Rockets.
- [10] R. V. Fernando de Souza Costa, "Preliminary Analysis of Hybrid Rockets for Launching Nanosats into LEO".

Mass Estimation Module -> estimate the different masses of the Launcher

Two Staging algorithms implemented.

- **Optimal Staging**
- 2. Restricted Staging: simplified method (only for existing ML) -> MTOM is requested as input.





- [2] H. Curtis, Orbital Mechanics for Engineering Students, Elsevier Aerospace Engineering Series, Elsevier, 2004.
 [3] K. Suresh and B. Sivan, Integrated Design for Space Transportation Systems, Springer, 2015.
- [4] D. M. Gaspar, "A Tool for Preliminary Design of Rockets".

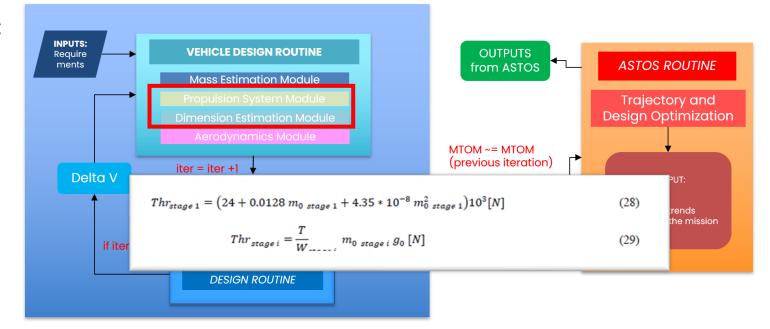
Propulsion System Module -> **Thrust** and **Geometrical characteristics** of the Engines.

Preloaded or **New propellant** in terms of:

- 1) Specific impulse;
- 2) Density;
- Mixture Ratio (bi-propellant).

Dimensions Estimation Module -> **Geometrical characteristics** of the Launcher.

- 1) Tanks length;
- 2) Stages length;
- 3) Fairing length.





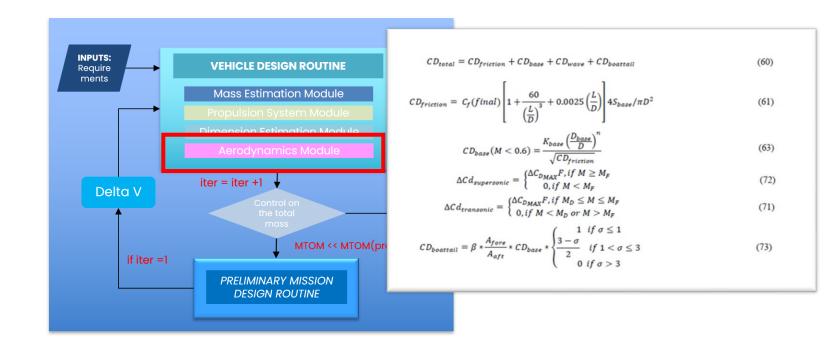
- 5] O. Sutton and G. Biblarz, Rocket Propulsion Elements.
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Aerodynamics Module ->
Drag coefficient = f (Mach, AoA).

Components considered:

- **1)** Base Drag;
- 2) Friction Drag;
- 3) Boattail Drag;
- 4) Supersonic and Transonic Drag.





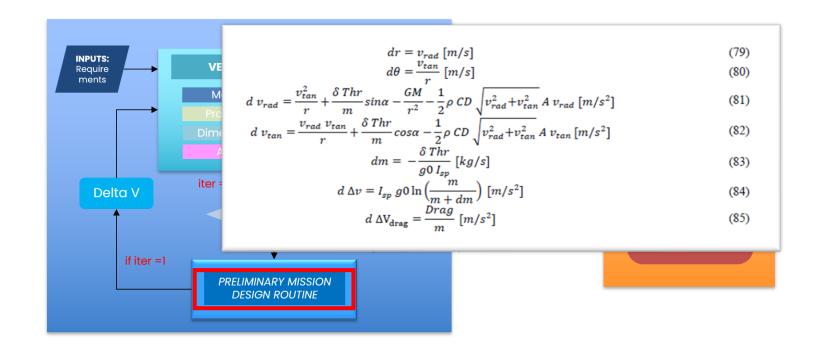
[11] P. Sharma, "Drag Coefficient Prediction".

[12] W. Stoney, "Collection of zero lift drag data on bodies of revolution from free flight investigation".

Preliminary Mission Module ->

- First trajectory estimation;
- Variable trends throughout the mission;
- 3) Delta V and Gravity and Drag Losses.

Starting point for new iterations!





- [5] O. Sutton and G. Biblarz, Rocket Propulsion Elements.
- [6] F. Castellini, Multidisciplinary Design Optimization for expendable launch vehicles, 2012.
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- [9] F. Miranda, Design Optimization of Ground and Air-Launched Hybrid Rockets.
- [10] R. V. Fernando de Souza Costa, "Preliminary Analysis of Hybrid Rockets for Launching Nanosats into LEO".

MicroLauncher Cost Estimation

Main Requirements

- ✓ i-DREAM shall support the conceptual and preliminary design of Microlaunchers (MLs) with the Life-cycle costing (LCC) assessment of MLs.
- ✓ This capability shall be exploitable:
 - o inside the integrated framework (thus using inputs coming from design)
 - in standalone mode

Expected Tool Developments

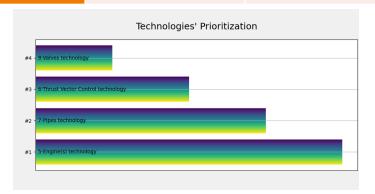
- ✓ Upgraded version of HyCost
 - HyCost is a proprietary tool of the research group of Politecnico di Torino, developed with ESA, to support a wide range of high-speed vehicles
 - TRIS has been validated for in different fields, from space exploration, to reusable access to space and re-entry vehicles.
- ✓ The cost estimation uses the heritage and know-how developed for previous contracts with ESA on the Microlaunchers design and evaluation capabilities.
- ✓ The routine uses the collected data from previous contracts as available input for the "Existing" case.



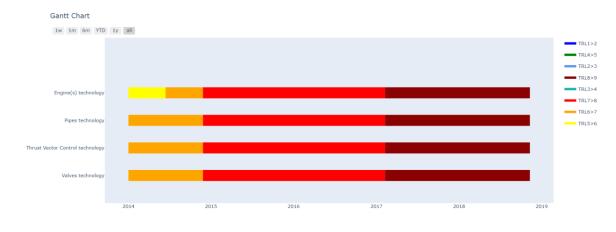
MicroLauncher Technology Roadmapping – Outputs



Ranking	Name	Current TRL
1	Engine(s) technology	5
2	Pipes technology	6
3	Thrust Vector Control technology	6
4	Valves technology	6



Tech Name	TRL 5	TRL 6	TRL 7	TRL 8	TRL 9
Engine(s) tech	01/01/2014	14/06/2014	26/11/2014	08/02/2017	10/11/2018
Pipes tech		01/01/2014	01/07/2014	05/12/2016	10/11/2018
TVC tech		01/01/2014	01/07/2014	05/12/2016	10/11/2018
Valves tech		01/01/2014	01/07/2014	05/12/2016	10/11/2018



MicroLauncher Technology Roadmapping – Inputs



• **Start Date**: 01-01-2014 (Electron launch vehicle)

• **End Date:** 11-11-2018 (first

Electron Mission – IT'S

BUSINESS TIME)

Target TRL: 9

Stakeholder	Role	Impact	Criterion	Prioriti zation Order
Rocket Lab	OP	KE	Current TRL	ASC
Rocket Lab	OP	KE	Cost at Completion	DESC
Rocket Lab	OP	KE	Number of Missions linked	ASC
Rocket Lab	ОР	KE	Number of Activities linked	ASC
Rocket Lab	OP	KE	Number of BBs linked	ASC
Rocket Lab	OP	KE	Number of Ocs linked	ASC
PoliTo	E-U	MON	Current TRL	ASC
PoliTo	E-U	MON	Cost at Completion	DESC
NASA	С	KE	Cost at Completion	DESC
NASA	С	KE	Number of Missions linked	ASC
U.S. Government	SP	KS	Number of Missions linked	ASC
DARPA	S SP	KI	Cost at Completion	DESC
DARPA	SP	KI	Number of Missions linked	ASC
ESA	OP	KI	Cost at Completion	DESC
ESA	OP	KI	Current TRL	ASC

HLS Backup





HLS Design and mission analysis methodology

Objective:

i-DREAM shall support the conceptual and preliminary design of HLSs and related nominal mission, while exploiting some routines of the commercial software **ASTOS**.

Tool:

- Upgraded version of ASTRID-H (Aircraft on-board Systems sizing and TRade-off analysis in Initial Design)
 - Proprietary tool of the research group of Politecnico di Torino
 - · Developed for almost a decade through research activities.
 - ASTRID-H supports the conceptual and preliminary design of a wide-range of high-speed transportation system from supersonic/hypersonic civil aircraft to Reusable Access to Space.

Expected Outputs:

iASTRID-H for HLS shall enable two different types of analysis:

- Assessment and verification of an already existing HLS design (Existing routine) supported by TREX DB (ESA proprietary DB)
- Definition of a new HLS design and reference mission starting from a set of high-level requirements (New routine)

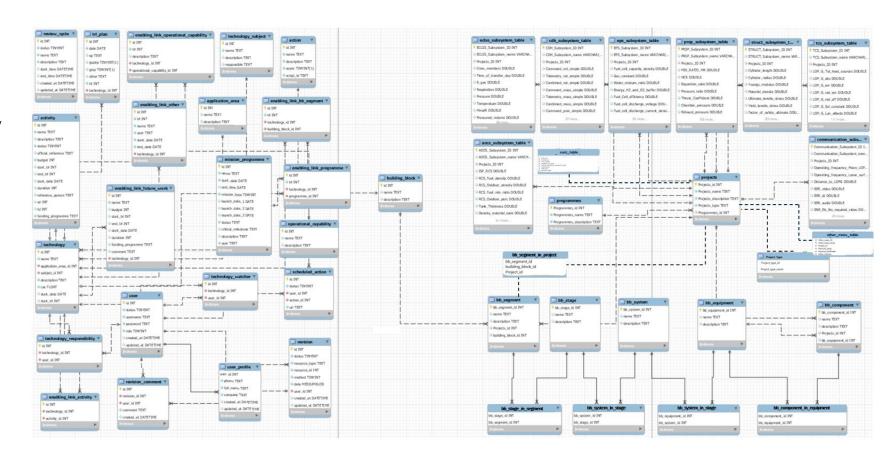


TREX Database

To support the multidisciplinary design of HLS, Politecnico di Torino upgraded TREX, a database initially developed by ESA to support internal technology roadmapping activities.

The MySQL version of TREx backend has been properly modified to store data of existing HLS projects and to support:

- Design & mission analysis
- Cost Estimation
- Technology Roadmap





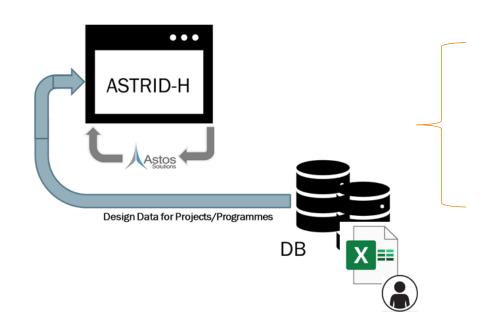
iDREAM (iASTRID-H) - HLS - Overview

Bottom-up approach:

From subsystem to vehicle design

Inputs from **TREX** (or **User**):

- Mission data (estimated Delta Vs, mission phases time)
- Nominal Payload Mass
- Number of crew
- Total mission time
- Details on the vehicle
 Configuration (subsystems data: PROPULSION, ECLSS, COMM, CDH, AOCS, TCS, STR, ___
 EPS etc...)

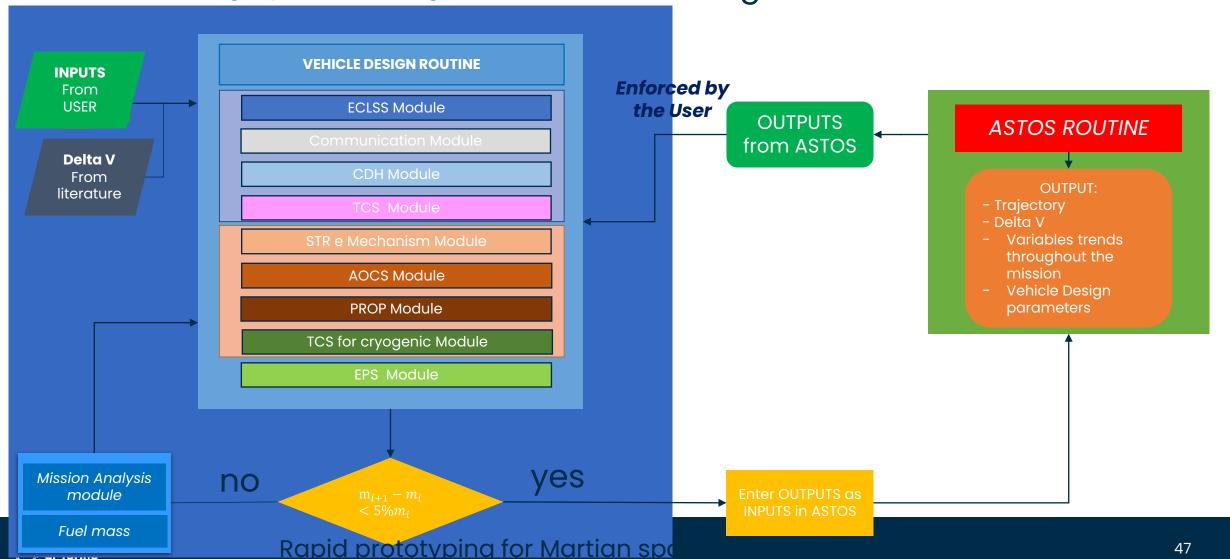


Outputs:

- Vehicle geometry and Layout
- Vehicle performance (propellant mass, final DeltaV, mass budgets, power budgets)
- Mission Concepts

iDREAM (iASTRID-H) - HLS - Design Steps

Human Landing System Design Routine -> Elestingsease



iDREAM (iASTRID-H) - HLS - Subsystems

ECLSS Module

Environment Control Life Support Subsystem (ECLSS) shall be able to sustain life for 4 astronauts during the mission.

Communication Module

Communication shall be able to sustain communication between astronauts and LOPG orbit during the whole mission.

CDH Module

Command and Data Handling(CDH) subsystem allows to interface human with other subsystems.

TCS Module

Thermal Control Subsystem (TCS) shall be able to control temperature for human habitat ,and other subsystems' component. (MLI, louvres, heat pipes, coldplates, heaters)

STR e Mechanism Module

Structure and Mechanism module estimates the mass, power and volume budgets of total structure, landing gear, docking mechanism and thermal protection system.

PROP Module

Propulsion Subsystem shall be able to sustain the descent manoeuvre during the mission. (fuel tanks, engine, pressurant and turbopumps)

AOCS Module

Attitude and Orbit Control Subsystem (AOCS) shall be able to sustain HLS asset along manoeuvres duration during the mission (AOCS fuel, tanks, AOCS engines, sun sensors, star trackers, etc...).

TCS for cryogenic Module

Thermal Control Subsystem (TCS) for cryogenic shall be able to control temperature for cryogenic fuel tanks.(MLI for fuel tanks)

EPS Module

Electrical Power Subsystem(EPS) shall be able to produce power required from the LSAM subsystems (batteries, solar arrays and fuel cells).

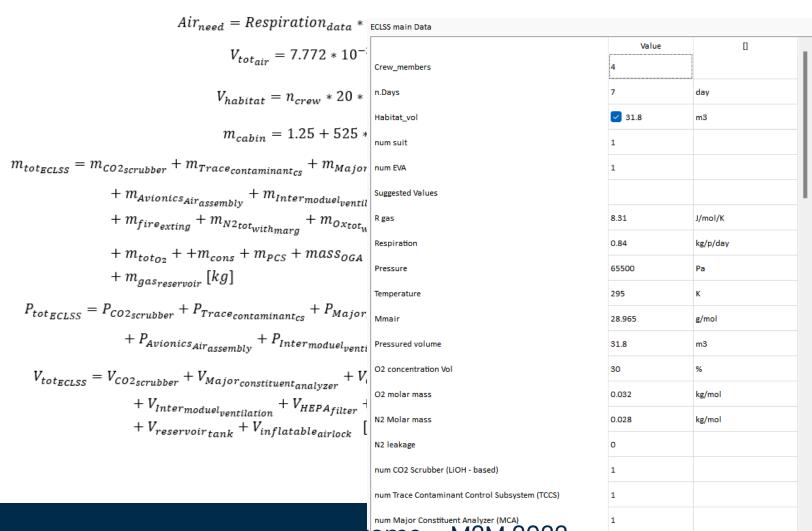


iDREAM (iASTRID-H) - HLS - Subsystems

$$m_{consumable} = 9.4 * n_{crew} * n_{days} + 2.3 * n_{days} + 4.5 * n_{evacycles}[kg]$$

Inputs:

- Number of Astronauts
- Mission Duration





iDREAM (ASTOS) - HLS

Missio

Human Landing System Design Routine -> ASTOS Routine

ASTOS routine can be launched directly from iDREAM GUI.

Connection allowed thanks:

- IT collaboration
 - Connection
 GUI
- homotopy.xml file

```
<?xml version="1.0" encoding="ISO-8859-1"?>
<Variables checksum="a725273773" xsl:schemaLocation="http://www.astos.de/schema/astos/9.17/scenario Scenario.xsd" xmlns:xsl="http://www.w3.org/2001/XMLSchema-instance"
xmlns="http://www.astos.de/schema/astos/9.17/scenario">
   <Variable type="Floating Point Value" name="DaysToAddForStartingDate">0.0</Variable>
   <Variable type="Floating Point Value" name="GS_Altitude">0.0</Variable>
   <Variable type="Floating Point Value" name="GS_Latitude">0.0</Variable>
   <Variable type="Floating Point Value" name="GS_Longitude">0.0</Variable>
   <Variable type="Floating Point Value" name="InclinationLLO">75.0</Variable>
   <Variable type="Floating Point Value" name="InitialArgOfPeriapsis">10.0</Variable>
   <Variable type="Floating Point Value" name="InitialRAAN">20.0</Variable>
   <Variable type="Floating Point Value" name="InitialTrueAnomaly">30.0</Variable>
   <Variable type="Floating Point Value" name="Initial_Apoapsis">101.0</Variable>
   <Variable type="Floating Point Value" name="Initial_Periapsis">100.0</Variable>
   <Variable type="Floating Point Value" name="Isp">453.0</Variable>
   <Variable type="Floating Point Value" name="Nozzle Ae">1.471
   <Variable type="Floating Point Value" name="Phase10 PitchConstant Time">5.0</Variable>
   <Variable type="Floating Point Value" name="Phase10_Throttle_PitchConstant">1.0</Variable>
   <Variable type="Floating Point Value" name="Phase11_BurnToLLOTime">120.0</Variable>
   <Variable type="Floating Point Value" name="Phase11 Throttle BurnToLLO">1.0</Variable>
   <Variable type="Floating Point Value" name="Phase12 CoastToLLOTime">200.0</variable>
   <Variable type="Floating Point Value" name="Phase12_TargetAltitude">100.0</Variable>
   <Variable type="Floating Point Value" name="Phase12_TargetInclination">70.0</Variable>
   <Variable type="Floating Point Value" name="Phase13_CircLLO_Time">1000.0</Variable>
   <Variable type="Floating Point Value" name="Phase1_LLOInitialTime">2910.0</Variable>
   <Variable type="Floating Point Value" name="Phase1_Pitch">0.0</Variable>
   <Variable type="Floating Point Value" name="Phase1_Yaw">-15.0</Variable>
   <Variable type="Floating Point Value" name="Phase2_BurnTime">35.0</Variable>
   <Variable type="Floating Point Value" name="Phase2 TargetPeriapsisToReduce">0.5</Variable>
   <Variable type="Floating Point Value" name="Phase2 Throttle DecreasingPeriapsis">1.0</Variable>
   <Variable type="Floating Point Value" name="Phase3_CoastToPeriapsisTime">2560.0</Variable>
   <Variable type="Floating Point Value" name="Phase3 FinalPitchToDecrApo">0.0</Variable>
   <Variable type="Floating Point Value" name="Phase3_FinalYawToDecrApo">207.0</Variable>
   <Variable type="Floating Point Value" name="Phase3_TargetAltitudeToDecreaseApoapsis">30.0/Variable>
   <Variable type="Floating Point Value" name="Phase4_DecreaseApoTime">200.0</Variable>
   <Variable type="Floating Point Value" name="Phase4_TargetApoapsis">40.0</Variable>
   <Variable type="Floating Point Value" name="Phase4 Throttle DecreaseApoapsis">1.0</Variable>
   <Variable type="Floating Point Value" name="Phase5_CoastToImpactTime">50.0</Variable>
   <Variable type="Floating Point Value" name="Phase5_FinalPitchToBrake">10.0</Variable>
   <Variable type="Floating Point Value" name="Phase5_FinalYawToBrake">205.0</Variable>
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   <Variable type="Floating Point Value" name="Phase6_BrakingTime">500.0</Variable>
   <Variable type="Floating Point Value" name="Phase6_TargetImpactAltitude">0.0</Variable>
   <Variable type="Floating Point Value" name="Phase6_Throttle_Braking">1.0</Variable>
   <Variable type="Floating Point Value" name="Phase7_DesiredYawForLaunch">27.0</Variable>
   <Variable type="Floating Point Value" name="Phase7 TimeOnMoon">1.0</Variable>
    Which has "Flating Brint Value" same "Bhases" Life (Friend's F. O. Mariables
```



iDREAM (iASTRID-H) - HLS

Human Landing System Design Routine -> Mission Analysis Routine

Mission Analysis

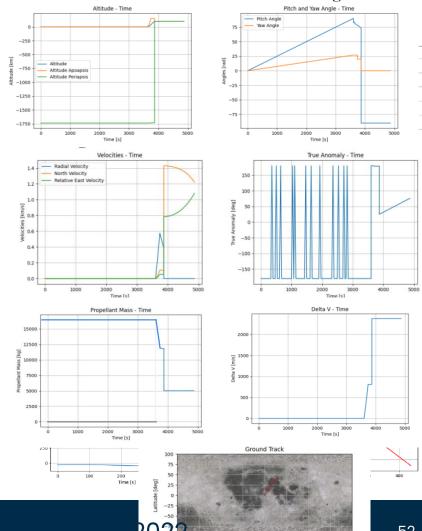
3 parts:

- **ASTOS: Descent** (with no Soft Landing Phase)
- Python environment: **Soft Landing Routine**
- **ASTOS: Ascent**

Spote beam distance utine:

- Phases 8-9-10: ascent phase: the sequence for hower timed different from the lift of Were the the the transfer of t
- orbit 15 km **Phases 11**: main burn during the ascent
- Phase: insertion of the vehicle in the transfer

 Phase 3500 450 the transfer the terreting the Gele ynth startifush enable the
- Phase end condition due to the new **Phase 12** coasting phase to reach the desired altitude previous burn
- Phase 13: Once the target altitude is reached,
- iPhase 4 the cetibel desilect artitude is theachied, a second burn is used to decrease the apoapsis of the orbit
- Phase 5: coasting phase to decrease the altitude of the Lunar Lander



Human Landing System - Cost Estimation

Objective:

The **second capability** of i-DREAM consists in supporting the conceptual and preliminary design of HLSs with the LCC assessment of HLSs.

Politecnico di Torino upgraded HyCost, a proprietary tool of the research group of Politecnico di Torino developed especially with ESA, to support a wide range of high-speed vehicles.

The AMCM model was implemented in the tool as cost routine for the HLS case. However, also a cost estimation methodology was developed based on analogy.

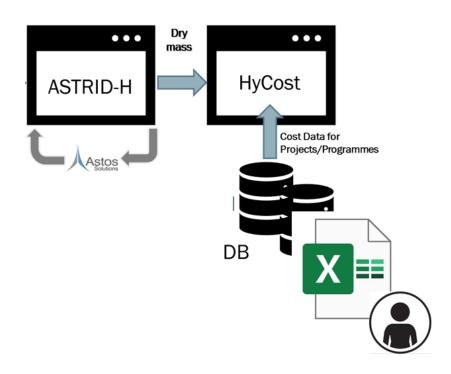
Human Landing System - Cost Estimation

Inputs from **TREX** (or **User**):

- Number of units
- Initial Operating Capability year
- Inheritance
- Difficulty
- Mission Type

Inputs from **iASTRID-H**:

Dry mass



Outputs:

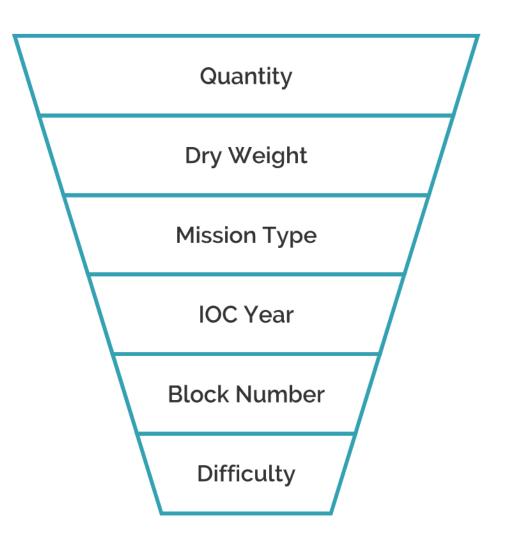
LCC assesment for HLSs



Human Landing System - Cost Estimation

Integration of the AMCM

- 1. Input from GUI
- 2. Run estimation
- 3. Graph and print of results





Human Landing System - Cost Estimation - Validation

Analogy method cost estimation

- For early design stages with no consistent data available
- Based on attributes available for analogue missions.
- Evaluating the closeness of one project to another based on distance metrics

Eulerian distance metric k is the number of attributes/characteristics used for	the
adjustment, weighted as for α , normalised to measure	the
distance between the i-th and i-th projects.	

_	Mission	\$FY2020M	Unit	Price	Crew	С	Target	Т	GLOW [kg]	G	dry mass [kg]	М	Σ
	Apollo LM	23,413	15	2,341*	2	0.40	Lunar Surface	0.0	16,374	0.07	4,920	0.21	0.17
	Orion	29,500	12	2,458*	4	0.00	Lunar Orbit	0.5	33,446	0.72	15,485	0.79	0.50
	Crew Dragon	3,153		55mln/seat	7	0.60	LEO	1.0	12,055	0.28	6,350	0.07	0.49
	Starliner	4,949		90mln/seat	7	0.60	LEO	1.0	13,000	0.23	5,591	0.14	0.49
	HLS	21,300	3	7100	4		Lunar Surface		17,975		7,150		

$$d_{i,j} = \sqrt{\frac{\sum_{k} \alpha_{k} \left[\frac{x_{k}^{i} - x_{k}^{j}}{\max_{i}(x_{k}^{i}) - \min_{i}(x_{k}^{i})}\right]^{2}}{\sum_{k} \alpha_{k}}}$$

Human Landing System - Cost Estimation -

Validation

The budget allocated for the HLS in the Artemis program is

21,300

\$FY2020M

The result of the cost estimation by analogy for the HLS is

18,619

\$FY2020M

The result of the AMCM cost estimation is equal to

17,618

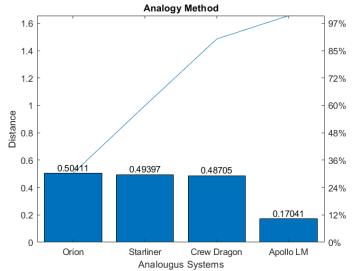
\$FY2020M

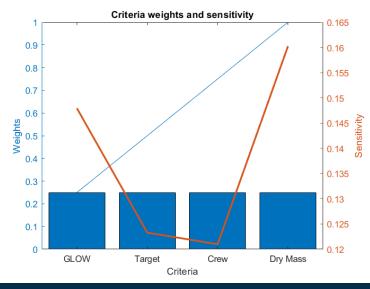
-14%

from the allocated budget

+5%

from the AMCM model





Mars Backup

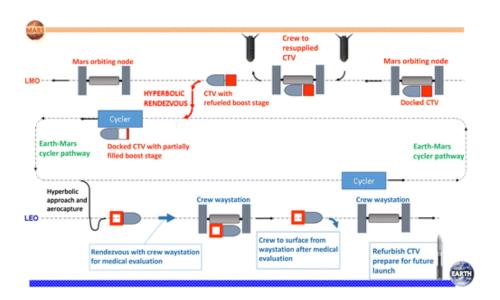


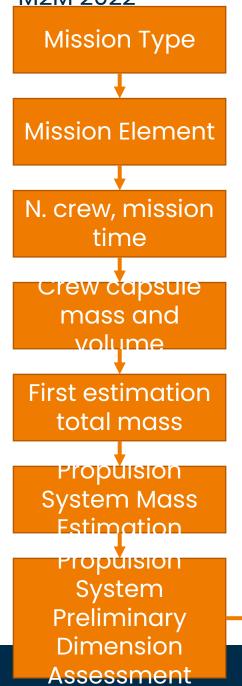


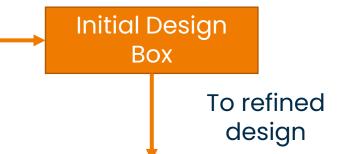
Rapid prototyping for Martian space systems - M2M 2022

 Let's say that the mission type is the one of a cycler. We would probably have:

- A cycler
- A crew transfer vehicle
- A payload transfer vehicle (maybe)









- If we have a cycler mission and we focus on the transfer vehicle between Earth orbit and the cycler, we can reuse a lot of the work performed for Idream Moon.
 - ECLSS definition without including ECLSS
 - All the part related to chemical propulsion



Rapid prototyping for Martian space systems – M2M 2022 ECLSS (i)

Inputs -> number crew, mission time

 $M_crew = n_crew(70 kg + 42 kg) [70 kg - astronaut weight [1], 42 kg - suits weight [2]]$

M_consumables [3] (modified because wrona) >

$$m_{\text{consumables}} = n_{\text{crew}} t_{\text{mission}} \left(2.9 \frac{\text{kg}}{\text{day}} \left(1 - 0.7 \right) + 1.83 \frac{\text{kg}}{\text{day}} + 0.82 \frac{\text{kg}}{\text{day}} + 1.22 \frac{\text{kg}}{\text{day}} \right)$$

Machado, Larissa Balestrero, and Markus Wilde. "Parametric design of a crew transfer vehicle for Earth-Mars cyclers." Journal of Spacecraft and



^[1] Hanford, A., "Advanced Life Support Baseline Values and Assumptions Document," NASA TP-2015-218570, 2015.

^{2]} McMann, K. S. T., and Harold, J., US Spacesuits, Springer Praxis, Chichester, England, U.K., 2005, Chap. 4.

Rapid prototyping for Martian space systems – M2M 2022 ECLSS (II)

Inputs \rightarrow number crew, mission time Habitable Volume

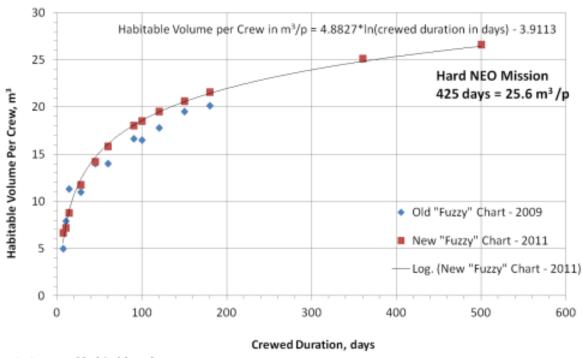


Figure 1: Averaged habitable volume curve.

[1] Simon, Matthew, et al. "Factors impacting habitable volume requirements: Results from the 2011 Habitable Volume Workshop." Center for Advanced Space Studies-Universities Space Research Association (2011).



Inputs -> number crew, mission time

Crew Habitat Mass = From G. Drake ed., Mars Architecture Steering Group, 2nd Addendum of the Human Exploration of Mars, Design Reference Architecture 5.0, NASA Johnson Space Center, 2014. Or you can use the formula of Human Spaceflight to have a first estimate of the mass of the crew habitat. It keeps into account the pressurized volume as well!

From the study of other transfer vehicles it looks like the Crew Habitat Mass is around:

8%-12% of the total mass for a nuclear propelled system (To be refined) Around 20% for transfer vehicles toward a cycler (short travels)

Table 3. Mass of the habitable module (kg) as a function of the crew size and number of days, according to NASA data (NASA Design Reference Architecture, annex 2, 2014, page 370 [8]).

Crew size \ duration (d)	600	800	1000
3	23505	26794	30139
4	27128	31144	35199

 $m_{bo} = 592 \times (number\ of\ crew \times mission\ duration\ [d] \times pressurized\ volume\ [m^3])^{0.346}$ (12-1)



6 34039 39694 45333

Rapid prototyping for Martian space systems – M2M 2022 ECLSS (IV)

Inputs -> number crew, mission time

From human spaceflight the power associated to the crew habitat can be estimated as:

average power required = $1000 \text{ W} + 500 \text{ W} \times \text{number of crew}$ peak power required = average power $\times 1.75$

 This value is around 5%-7% of the total required power for a transfer vehicle toward Mars (always from the book: Human Spaceflight)



Propulsion Systems - M2M 2022 Propulsion System Sizing - Chemical

Estimate thrust level from the initial calculate weight (T/W = 1.5/2

Estimate number of Thrusters given an engine thrust from database (same as IDREAM standard) or estimate mass Thruster from the IDREAM regression formulae (the one that Giuseppe Narducci built for different types of propulsion systems).

Estimate the tanks and engine length and diameter following what Giuseppe Narducci did.

<u>Vou can have chemical propulsion if you use a cycler \rightarrow you just</u>



Rapid prototyping for Martian space systems - M2M 2022

IDREAM Regression Propulsion - Chemical

$$m_{engine} \ (Turbo-pump) \\ = \begin{cases} 7.54354 \ e - 3 \ Thr^{0.885635} + 20.2881 \ for \ cryo \ propellant \ (Thr \leq 200e3) \\ 1.9101 \ e - 3 \ Thr \ for \ cryo \ propellant \ (Thr > 200e3) \\ 3.75407e3 \ Thr^{0.0705627} - 8.8479e3 \ for \ cryo \ storable \ propellant \ (Thr \geq 450e3) \\ -0.0003 \left(\frac{Thr}{1000}\right)^2 + 1.3807 \left(\frac{Thr}{1000}\right) for \ cryo \ storable \ propellant \ (Thr < 450e3) \ [kg] \\ 6.37913Thr^{0.353665} - 148.832 \ for \ storable \ propellant \ (Thr \geq 200e3) \\ -0.0021 \left(\frac{Thr}{1000}\right)^2 + 2.0264 \left(\frac{Thr}{1000}\right) for \ storable \ propellant \ (Thr < 200e3) \end{cases} \\ m_{engine} \ (Pressure - Fed) \\ = \begin{cases} -2.13325e - 9 \ Thr^2 + 1.7087e - 3 \ Thr + 6.38629 \ for \ cryo \ storable \ propellant \ (Thr \leq 300e3) \\ -0.0005 \left(\frac{Thr}{1000}\right)^2 + 1.244 \left(\frac{Thr}{1000}\right) + 18.336 \ for \ cryo \ storable \ propellant \ (Thr < 300e3) \\ -3.36532e - 8 \ Thr^2 + 4.74402e - 3 \ Thr - 19.3920 \ for \ storable \ propellant \ (Thr < 55e3) \end{cases}$$
 [kg]
$$25.56 \log \left(\frac{Thr}{1000}\right) + 29.824 \ for \ storable \ propellant \ (Thr \geq 55e3) \end{cases}$$

The total mass of the engine can be evaluated as in [6] using eq. (36):

$$m_{engine\ TOT} = n_{engine} m_{engine} [kg]$$
 (36)

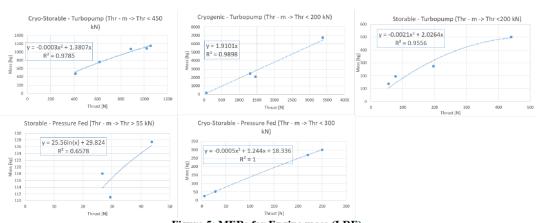


Figure 5: MERs for Engine mass (LRE).



Rapid prototyping for Martian space systems – M2M 2022 IDREAM Regression Propulsion – Chemical

$$\begin{cases} m_{press} = 1.1 \frac{p_{tank} \cdot 10^5 (V_F + V_{ox})}{R \, T_{press}} \cdot \frac{\gamma}{1 - p_{tank}/p_{press}} \, [kg] \\ \\ m_{press_{tank}} = 4 \, \pi \big(D_{press} \big)^2 \tau_{press} \rho_{tank} \, [kg] \end{cases}$$

$$m_{press_{sys}} = m_{pressurant} + m_{press_{tank}} \, [kg]$$

$$L_{tank} = \begin{cases} \left(\frac{m_{ox}}{\rho_{ox}} + \frac{m_F}{\rho_F} + \frac{\pi}{6}\right) \frac{(1 + V_{ullage})4}{\pi D_{tank}^2} & \text{if bi-prop} \\ \frac{m_{mono}}{\rho_{mono}} \frac{(1 + V_{ullage})4}{\pi D_{tank}^2} & \text{if mono} \end{cases}$$

$$[m] \qquad m_{intertank} = \begin{cases} 5.4015 \cdot 2\pi r_{rocket} L_{intertank} (3.2808(2 \, r_{rocket}))^{0.5169} \rightarrow lower \, stage} \\ 3.8664 \cdot 2\pi r_{rocket} L_{intertank} (3.2808(2 \, r_{rocket}))^{0.6025} \rightarrow upper \, stages} \end{cases}$$

$$[kg]$$

$$\begin{cases} m_{tank}(bi-prop) = m_{tank_{ox}} + m_{tank_{f}} \\ m_{tank}(bi-prop) = m_{tank_{ox}} + m_{tank_{f}} \end{cases} \\ = 1.2 \cdot \frac{\rho_{tank_{ox}}\pi}{6} \left(D_{rocket}^{3} - (D_{rocket} - 2\tau_{tank})^{3}\right) \\ + 1.5 \left(\left(\frac{D_{rocket}}{2}\right)^{2} - \left(\frac{D_{rocket}}{2} - \tau_{tank}\right)^{2}\right) L_{tank_{ox_{cyl}}} \\ m_{tank_{fuel}} = 1.2 \cdot \frac{\rho_{tank_{f}}\pi}{6} \left(D_{rocket}^{3} - (D_{rocket} - 2\tau_{tank})^{3}\right) \\ m_{tank_{fuel}} = 1.2 \cdot \frac{\rho_{tank_{f}}\pi}{2} \left(\frac{D_{rocket}}{2} - \tau_{tank}\right)^{2}\right) L_{tank_{fcyl}} \end{cases}$$

$$m_{tank}(mono) = m_{tank} = 1.2 \cdot \frac{\rho_{tank}\pi}{6} \left(D_{rocket}^{3} - (D_{rocket} - 2\tau_{tank})^{2}\right) L_{tank_{fcyl}}$$

$$+1.5 \left(\left(\frac{D_{rocket}}{2}\right)^{2} - \left(\frac{D_{rocket}}{2} - \tau_{tank}\right)^{2}\right) L_{tank_{cyl}}$$

$$+1.5 \left(\left(\frac{D_{rocket}}{2}\right)^{2} - \left(\frac{D_{rocket}}{2} - \tau_{tank}\right)^{2}\right) L_{tank_{cyl}}$$

$$m_{intertank} = 0.3 \cdot r_{rocket} \ [m]$$

$$m_{intertank} = \begin{cases} 5.4015 \cdot 2\pi r_{rocket} L_{intertank} \big(3.2808 (2 \ r_{rocket}) \big)^{0.5169} \rightarrow lower \ stage \\ 3.8664 \cdot 2\pi r_{rocket} L_{intertank} \big(3.2808 (2 \ r_{rocket}) \big)^{0.6025} \rightarrow upper \ stages \end{cases}$$
 [kg]

Take at home lesson: for most of the propulsion subsystem we can use what is already in



Repid prototyping for Martian space systems – M2M 2022 IDREAM Regression Propulsion – Chemical

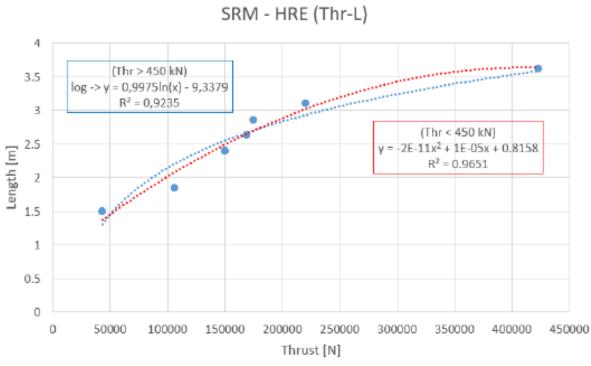


Figure 9: SRM - HRE Regression law Thrust [N]-Length [m]

Take at home lesson: for most of the propulsion subsystem we can use what is already in



Propulsion Systems - M2M 2022 Propulsion System Sizing Beyond Idream - Chemical

Propulsion system mass of valves, lines structure from [1]

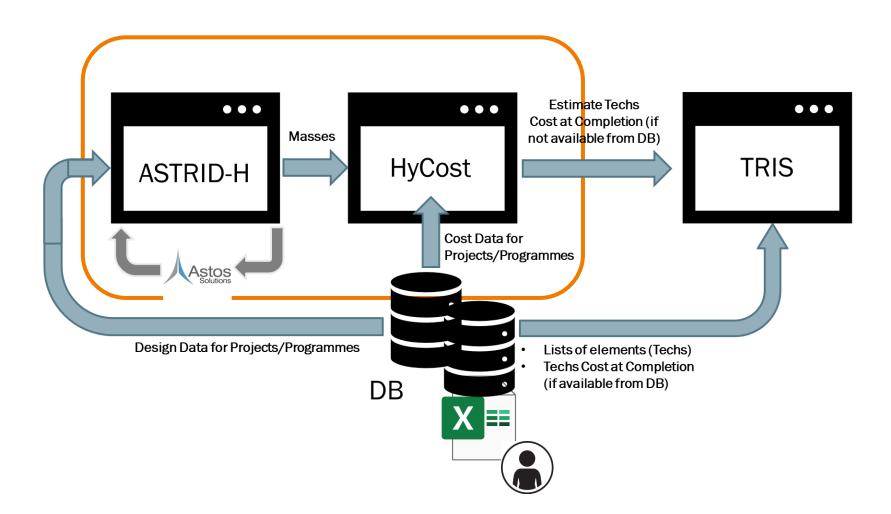
$$m_{valves,lines,structure} = \left(\frac{27}{73}\right) * \left(m_{engine} + m_{tanks} + m_{intertank}\right)$$

You have an itertank if your tank is not spherical

[1] Machado, Larissa Balestrero, and Markus Wilde. "Parametric design of a crew transfer vehicle for Earth-Mars cyclers." Journal of Spacecraft and Rockets 57.3 (2020): 565-579.



iDREAM for Mars



DESIGN

- 1. Propulsion
 - i. Nuclear
- 2. ECLSS
 - i. Lower in %mass
 - ii. Artificial gravity

COST

- 1. AMCM
- 2. Analogy method