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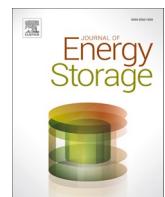
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Research papers

Influence of organics and gas mixing on hydrogen/brine and methane/brine wettability using Jordanian oil shale rocks: Implications for hydrogen geological storage



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ABSTRACT

The substitution of fossil fuel with clean hydrogen (H_2) has been identified as a promising route to achieve net zero carbon emissions by this century. However, enough H_2 must be stored underground at an industrial scale to achieve this objective due to the low volumetric energy density of H_2 . In underground H_2 storage, cushion gases, such as methane (CH_4), are required to maintain a safe operational formation pressure during the withdrawal or injection of H_2 . The wetting characteristics of geological formations in the presence of H_2 , cushion gas, and the resultant gas mixture in the mixing zone between them are essential for determining storage capacities. Therefore, the present work measured the contact angles of four Jordanian oil shale rocks with H_2 , CH_4 , and H_2 - CH_4 /brine mixture systems and their interfacial tension (IFT) in geological storage (geo-storage) conditions (pressures of 0.1 to 1600 psi and temperature at 323 K) to evaluate the residual and structural trapping potential and efficiency of CH_4 as a cushion gas. Various analytical methods were employed to comprehend the bulk mineralogy, elemental composition, topographic characterization, functional groups, and surface properties of the Jordanian oil shale rocks. The total organic carbon (TOC) effect on wettability was demonstrated and compared with previous studies. The Jordanian oil shale samples with high to ultrahigh TOC of 13 % to 18 % exhibited high brine advancing/receding contact angles. The rock samples became hydrophobic at the highest experimental pressure and temperature conditions (1600 psi and 323 K). The rock/ CH_4 /brine contact angles were higher than the rock/ H_2 /brine contact angles, and the H_2 - CH_4 /brine mixture contact angles remained in between those for pure gases. Moreover, the IFT displayed the inverse trend, where the H_2 /brine IFT measured higher than the CH_4 /brine IFT. The results suggest that the H_2 geo-storage in the tested organic-rich source rocks could be favorable when CH_4 is used as a cushion gas, consistent with previous studies using synthetically acidaged shale samples. For the first time, the present work used organic-rich rocks from Jordanian oil shale to present a more realistic situation and evaluate the influence of missing organic material and gas on the H_2 /brine/rock wettability during H_2 geo-storage.

1. Introduction

The global energy demand could increase by >27 % within the next three decades as the world population attains the 10 billion mark, increased from 7.98 billion [1–3]. The world has relied on fossil fuels as the primary energy source for centuries [4,5]. Burning fossil fuels remains the primary source of anthropogenic carbon dioxide (CO_2) emissions, a principal greenhouse gas contributing to global warming

and increasing the earth's temperature [3,6,7]. With the increasing global ambition to achieve net zero carbon emissions by midcentury [8,9], reducing the continual reliance on fossil fuels while maintaining a balance between energy supply and increasing energy demand is essential [10–13].

Renewable energy, such as solar, hydropower, and wind energy, is more sustainable and eco-friendlier than fossil fuels. However, their sources are intermittent and constrained to the earth's seasonal and

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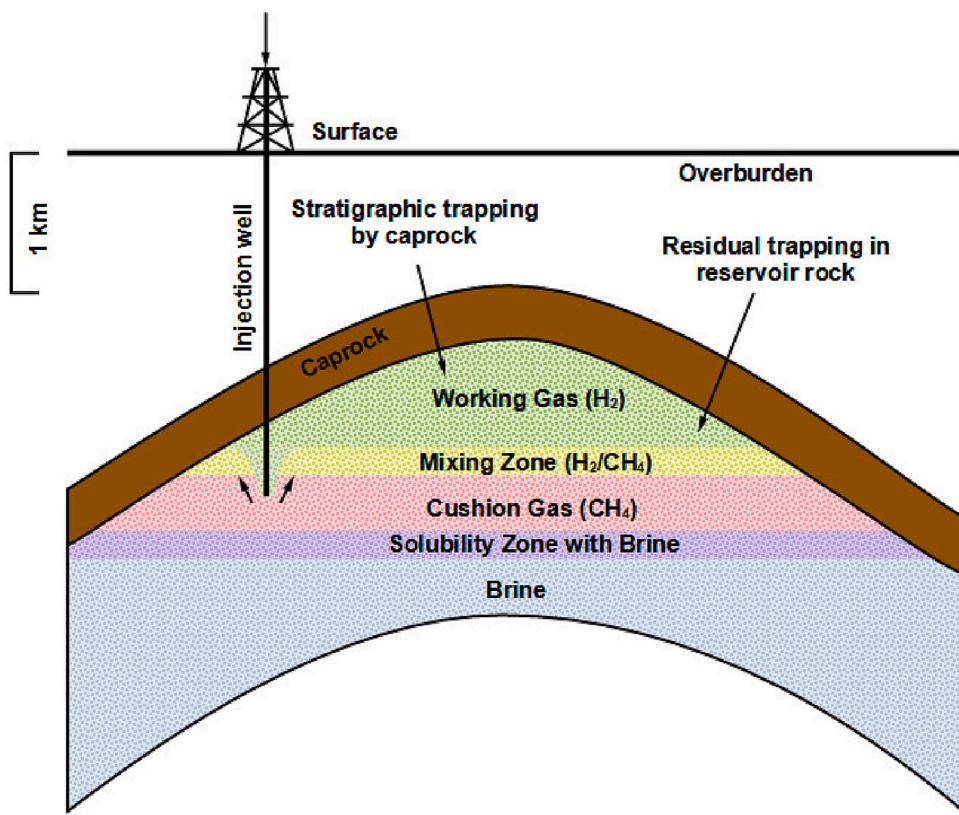


Fig. 1. Illustration of underground hydrogen storage and mixing zone between working gas (H_2) and cushion gas (CH_4).

quotidian cycles [14,15]. Recently, global attention has been focused on decarbonizing the industrial sectors via the hydrogen (H_2) economy [16–20] because it does not produce CO_2 when it burns and has low environmental and societal effects (a CO_2 -free global economy) [17,21,22].

In contrast, H_2 has low volumetric energy content due to its low density. Consequently, substantial volumes of H_2 must be stored at an industrial scale to back up the H_2 supply when needed [23]. Underground H_2 storage (UHS) is perceived as an economical and safer option than surface storage facilities [20,24], which are challenging and costly to construct and maintain [25].

Currently, the only used UHS media are salt caverns, which are more straightforward than porous formations and do not cause the microbial consumption of H_2 [16,26–28]. Despite the complexity of porous formations, deep saline aquifers and depleted hydrocarbon reservoirs provide more spacious storage options. Their features are well known from the experience acquired from subsurface storage of natural gas and CO_2 for decades [29–33]. Similarly, the subsurface facilities previously used for the transportation and storage of hydrocarbons could be upgraded for H_2 storage and production [19,34].

Currently, the only known information on the possibility of UHS is deduced from experience with CO_2 and methane (CH_4) subsurface storage [33,35–37]. However, the characteristics of pure H_2 differ from those of CO_2 and CH_4 [38]. Hydrogen is the lightest known molecule in nature and has a considerably lower density than other gases [17,39]. Moreover, CO_2 is intended to be stored permanently in geological storage (geo-storage) formations, whereas H_2 is stored temporarily to be withdrawn during acute energy demands [11,16]. Formation pressure should be sustained using cushion gases to maintain the integrity of the reservoir during H_2 withdrawal [40–42]. Both CO_2 and CH_4 are possible cushion gases for H_2 withdrawal. However, these gases create a mixing zone between the stored gas (H_2) and cushion gases (CO_2 or CH_4) [33,43], as illustrated in Fig. 1.

Previously, a few studies have reported insight into the rock-brine- H_2

interaction and rock-fluid interfacial tension (IFT) [33,44–50]. The influences of subsurface temperature, pressure, salinity, and organic-acid contamination inherent in geo-storage/caprock formations have been investigated concerning their wetting characteristics and IFT interactions in the presence of H_2 , CH_4 , and CO_2 [33,35,42,51,52]. From these results, we inferred that the residual/capillary trapping of H_2 in storage rocks, such as sandstone/quartz and carbonate/calcite, and adsorption trapping in coal and high total organic carbon (TOC) shale could be lower at high temperatures and low pressures. Likewise, the structural trapping potential of caprock was surmised to be favorable at high temperatures and low pressures and in the absence of organic acids in an overlying seal [53–57].

Recently, Hashemi et al. [33] measured the static contact angles of H_2 - CH_4 /brine/Bentheimer sandstone systems to assess the mixed-zone, cushion, and working gas wettability and IFT. They found that the contact angles varied from 25° to 45° at geo-storage temperatures ($30^\circ C$ and $50^\circ C$) and pressures (20–100 bar). Their results further demonstrated that the wetting behavior of Bentheimer rock was similar in the presence of H_2 , CH_4 , and the H_2 - CH_4 mixture regardless of the varying H_2 composition, geo-storage conditions, and sodium chloride (NaCl) concentrations.

Similarly, Mirchi et al. [43] computed the IFT values (via the pendant drop technique) and static contact angles for H_2 - CH_4 /brine on limestone and oil-wet sandstone at 1000 psi and $22^\circ C$ – $60^\circ C$ using captive/rising bubble methods. The results revealed that the IFT decreased with rising temperatures and reducing H_2 fractions in the H_2 - CH_4 mixture. The mixed system of H_2 and potential cushion gas (CH_4) demonstrated similar weakly water-wet characteristics on limestone and oil-wet sandstone rocks. Moreover, the contact angles varied from 52.42° to 71.1° . In addition, the contact angles of the H_2 /brine systems on the rock surfaces were lower than those of the CH_4 /brine systems, suggesting that CH_4 could be a feasible (promising) cushion gas for H_2 storage and withdrawal.

Van Rooijen et al. [58] confirmed that the storage media could

Table 1Summary of selected previous research reporting the contact angles of rock/H₂/brine systems.

Samples	Methodology	Temperature	Pressure	References	Remarks
Quartz	Captive bubble,	298 K	0.69–1.72 MPa & 6.89–20.68 MPa	Higgs et al. [69]	Effective contact angles of H ₂ /2000 ppm NaCl varied 31°–29° within a pressure range of 0.69–1.72 MPa, those of H ₂ /5000 ppm NaCl varied 35°–33° at 0.69–1.72 MPa, and the contact angle of H ₂ /water was 27° at 0.77 and 0.86 MPa
Bituminous coal	Tilted drop method	25 °C, 50 °C, and 70 °C	20–100 bar	Sedev et al. [70]	1. The coal surface was weakly water-wet in geo-storage 2. Brine contact angles increased with H ₂ pressure at 25 °C, with no significant pressure effect on contact angles at 50 °C or 70 °C
Saudi basaltic rocks	Modified sessile drop method	323 K	3–28 MPa	Alanazi et al. [71]	1. Saudi basalt with –OH bonds and a higher Si-O-Si group had superior sealing potential for H ₂ storage 2. Basaltic rocks with smaller pore sizes have higher storage potential
Sandstone (oil-wet) and limestone	Rising/captive bubble method	22 °C–60 °C	100 psi	Mirchi et al. [43]	Contact angle values ranged from 52.42°–71.1°, suggesting that oil-wet sandstone and limestone remained weakly water-wet in the presence of an H ₂ /CH ₄ mixture
Quartz	Experimental (tilted plate)	296 K–343 K	0.1–25 MPa	Iglauer et al. [50]	Contact angle values increased with pressure, temperature, and increased concentrations of organic acid
Mica	Experimental (tilted plate)	323 K	0.1–25 MPa	Ali et al. [59]	Advancing and receding contact angle values reached 106.2° and 97.3° when mica was aged in 10 ⁻² mol/L of organic-acid/n-decane solution at 323 K and 25 MPa
Clay minerals	Empirical correlations	333 K	5–20 MPa	Al-Yaseri et al. [72]	1. Contact angles were generally <40° 2. Montmorillonite was the most water-wet, whereas kaolinite was the least water-wet
Basalt	Empirical correlations	323 K	5–20 MPa	Al-Yaseri and Jha [47]	Contact angle values were generally < 20°
Sandstones (Berea and Bentheimer)	Experimental (captive bubble)	20 °C–50 °C	20–100 bar	Hashemi et al. [48]	Contact angle values vary between 25° and 45°
Quartz	Experimental (tilted plate)	323 K	0.1–25 MPa	Ali et al. [29]	Contact angle values were >90° when the effects of organic contamination (10 ⁻² mol/L lignoceric acid) were considered
Shale	Tilted plate	298 K–353 K	0.1–20 MPa	Hosseini et al. [56]	Caprock became less water-wet at low temperatures, high pressures, higher TOC values, and increasing concentrations of organic acid
Shale (0.081–23.4 wt%)	Semi-empirical correlations	343 K	5–20 MPa	Al-Yaseri et al. [73]	Capillary entry pressure reduced, whereas contact angles increased with increasing pressure (depth) and the TOC of the shale
Berea sandstone (length = 17 cm; diameter = 3.8)	Combination of MICP data and capillary pressure	18 °C	100 bar	Boon and Hajibeygi [74]	1. The receding contact angle of the H ₂ /water system on a Berea sandstone rock core was estimated as 45° 2. Displacement patterns during UHS can result from the interplay between the capillarity and viscous and gravitational forces
Glass	Microfluidic chip	20 °C	10 bar	van Rooijen et al. [75]	1. The porous medium stayed strongly water-wet in H ₂ ; dynamic advancing contact angles ranged from 13°–39°, whereas dynamic receding contact angles ranged from 6°–23° 2. Contact angle datasets of H ₂ , nitrogen, and gaseous CO ₂ were comparable, and higher channel widths produced smaller contact angles
Quartz	Geochemical modeling	296 K, 323 K, 343 K	0.1–25 MPa	Zeng et al. [76]	1. Concentrations of quartz surface species (> SiO ⁻ and > SiOCa ⁺) decreased with increased temperatures 2. No significant effect of increasing pressure and temperature was found on the disjoining pressure and H ₂ wettability of pure quartz, but increasing pressure and concentrations of organic acid molecules increased the rock hydrophobicity and H ₂ -wettability of aged quartz

*MICP: mercury injection capillary pressure.

remain at water-wet conditions by measuring the contact angles of H₂/water on a microfluidic chip (with microchannel widths ranging from 50 to 130 μm) at 20 °C and 10 bar. The microfluidic chip was completely saturated with water before H₂ injection for the drainage tests, whereas in the imbibition experiments, the microfluidic chip was entirely saturated with H₂ before water injection. The results revealed that the wetting state remained at strong water-wet conditions and that the H₂/water advancing contact angles varied between 13° and 39°, whereas the receding contact angles varied between 6° and 23°. These results confirmed that a fully H₂-wet state is difficult to attain during UHS.

In contrast, Ali et al. found that containment safety of H₂ in storage and caprock is overpredicted when the influence of organic impurities (contaminations), which are characteristic of natural geo-storage formations, is neglected and that fully H₂-wet conditions (contact angles > 90°) can be attained in the presence of organic acids. Ali et al. [59] found that the caprock representative mineral (mica) demonstrated entirely H₂-wet behavior at 383 K and 25 MPa ($\theta_a = 106.2^\circ$, $\theta_r = 97.3^\circ$) in the presence of 10⁻² mol/L of lignoceric acid. The rock hydrophobicity

increased with an increased organic-acid concentration and alkyl chain length, as follows: hexanoic acid < lauric acid < lignoceric acid from C₆ to C₂₄ [29,53,59,60]. The high values of standard adsorption energy promoted the interactions between rock surfaces and H₂ molecules, which increased with the increasing alkyl chain length of the organic acids. Generally, organic contamination and salinity reduce the storage rock potential and containment security of H₂.

Pan et al. [61] and Arif et al. [62] demonstrated that the contact angle increases when the TOC of shale samples increases from 2% to 20% at a temperature of 323 K. A summary of previous studies on rock/H₂/brine systems of storage/caprock is presented in Table 1. Only a few of these studies have provided insight into the rock-wetting phenomenon and rock-fluid IFT of the mixing zone between the stored gas and cushion gas during UHS in organic-rich shale source rocks [33,43]. Moreover, in most previous studies, the clean rock substrates were aged in organic acids, such as stearic and lignoceric acid, to assess the effects of organic contamination inherent in geo-storage formations. None of the previous studies have used the original source rock with inherent

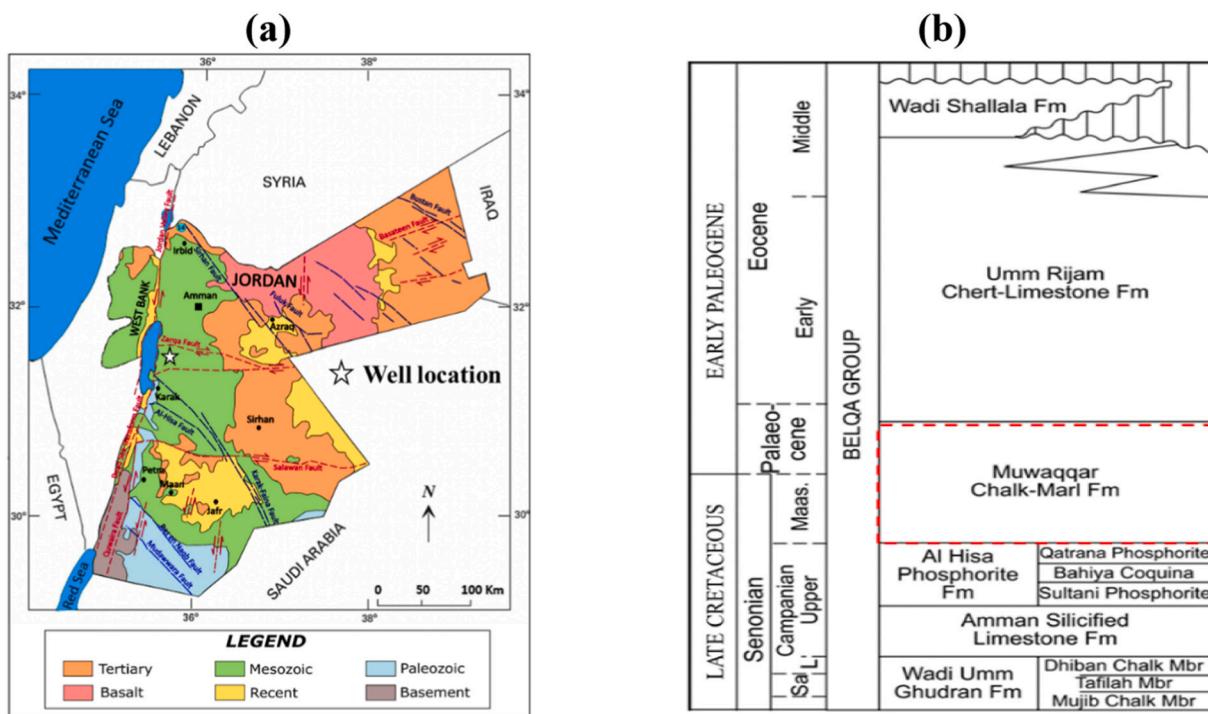


Fig. 2. (a) Geological map of Jordan marking the drilled well location and (b) generalized stratigraphic column with significant occurrences of Jordan shale source rocks from the Late Cretaceous to Early Paleogene (adapted from [79,80]).

organic-acid content to assess the effects of organic-acid contamination on the H₂-CH₄/brine/rock wettability and H₂-CH₄/brine IFT at geo-storage temperatures and pressures.

Thus, the present work evaluated the wettability and IFT of the H₂, CH₄, and H₂-CH₄ mixture (50 %/50 %) at 323 K at various pressures (0.1–1600 psi). A source rock, which is a good candidate for H₂ storage and inherently contains organic acids, was used as the rock substrate for the wettability measurement. Natural organic-rich shale source rocks (high TOC) from Jordan were used as rock substrates to evaluate the effects of natural organics on H₂, CH₄, and H₂-CH₄ mixture wettability. This work provides an understanding of the mixing-zone wettability and gas/brine IFT during UHS in organic-rich shale source rocks (Fig. 1). Several researchers have identified TOC to be a critical influencing parameter on the adsorption-desorption capacity and the storability of gas in calcareous and argillaceous source rocks [63–68]. Thus, this study also demonstrates the influence of organic material on the wettability and storability of H₂, CH₄, and the H₂-CH₄ mixture in these formations. The work provides a fundamental concept for UHS concerning organic matter and aids in implementing a large-scale H₂ economy for Jordanian oil shale rocks.

2. Materials and methods

2.1. Materials

The tested organic-rich shale source rocks, known as Jordanian oil shale, were collected from Jordan. The Jordanian oil shale rocks

correspond to the Muwaqqar Chalk-Marl formation, deposited during the Late Cretaceous to Early Paleocene period [77]. The Jordanian oil shale source rocks are among the richest globally [78,79], with a TOC value as high as 30 %. However, these source rocks are thermally immature and have not been reported to produce hydrocarbons on an economic scale.

Four samples of Jordanian shale source rocks were selected at various depths from a well drilled in northwest Jordan (Fig. 2(a)). The organic-rich interval, corresponding to these litho-stratigraphic units, was deposited in reducing conditions with restricted water circulation and was characterized as Type II-IIS kerogen (Abed and Amireh, 1983; Hakimi et al., 2016; Powell and Moh'D, 2011) (Fig. 2b). The CH₄, H₂, and H₂-CH₄ mixture used for the experiments were of high purity (99.99 mol%, supplied from Coregas, Australia). The brine salinity of 2 wt% of NaCl with 1 wt% of potassium chloride (KCl) was used throughout the experiments. The NaCl and KCl were reagent grade (99.9 % pure, supplied by Chemlab, Australia).

2.2. Total organic carbon determination of Jordanian oil shale samples

The selected rock samples were powdered, and about 50 mg of each sample was analyzed using RockEval 7S (©Vinci Technologies) for TOC measurements. The methodological and assessment criteria have been described in previous research (Behar et al., 2001; Carvajal-Ortiz et al., 2021). The parameters obtained from this analysis include S1, S2, S3, T_{max}, and sulfur content. The S1 (mgHC/gRock) indicates the volume of free hydrocarbons present without thermal cracking of the kerogen at

Table 2

RockEval parameters of the selected samples from Jordanian oil shale.

Sample Name	T _{max} (°C)	HI	OI	PI	S1 (mg/g)	S2 (mg/g)	S3 (mg/g)	Total Sulfur (%)	TOC (%)
Jordan-1	420	822	8	0.03	4.96	147.52	1.35	3.68	17.94
Jordan-2	419	847	9	0.03	4.17	136.69	1.5	2.94	16.15
Jordan-3	420	858	8	0.03	4.01	127.78	1.22	3.09	14.89
Jordan-4	418	861	9	0.04	4.41	111.37	1.14	3.06	12.93

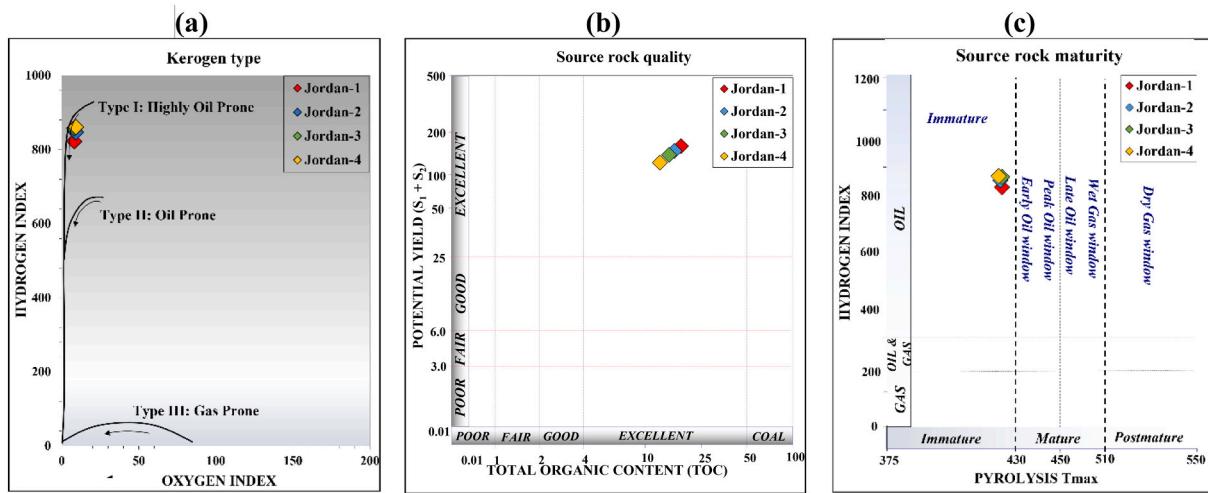


Fig. 3. Analyzed Jordanian oil shale rock parameters derived from RockEval pyrolysis: a) kerogen type, b) source rock quality, and c) source rock maturity.

Table 3

Mineralogy from x-ray powder diffraction (XRD) analysis and total organic carbon.

Sample No.	Mineral composition from XRD		
	Mineral phase	Chemical formula	Abundance %
Jordan-1	Calcite	CaCO_3	85
	Quartz	SiO_2	14
	Berlinite	$\text{Al}(\text{PO}_4)$	1
Jordan-2	Calcite	CaCO_3	92
	Quartz	SiO_2	4
	Apatite	$\text{Ca}_5[\text{PO}_4]_3(\text{OH},\text{F},\text{Cl})$	4
Jordan-3	Calcite	CaCO_3	73
	Quartz	SiO_2	14
	Apatite	$\text{Ca}_5[\text{PO}_4]_3(\text{OH},\text{F},\text{Cl})$	12
Jordan-4	Langite	$\text{Cu}_4(\text{SO}_4)(\text{OH})_6 \cdot 2\text{H}_2\text{O}$	1
	Calcite	CaCO_3	44
	Quartz	SiO_2	54
	Apatite	$\text{Ca}_5[\text{PO}_4]_3(\text{OH},\text{F},\text{Cl})$	1.4
	Berlinite	$\text{Al}(\text{PO}_4)$	0.5

approximately 300 °C. In addition, S2 (mgHC/gRock) is the quantity of hydrocarbons produced due to thermal cracking from 300 °C to 600 °C, whereas S3 (mgCO₂/gRock) indicates the amount of CO₂ produced during the programmed pyrolysis. Finally, T_{max} (°C) is the temperature for the maximum peak of S2 and denotes the source sample maturity. Sulfur content is measured during pyrolysis and oxidation with temperatures up to 1200 °C.

The TOC percentage of the rock is determined by the oxidation in the air in a second oven from the residual organic carbon after pyrolysis. Other functional parameters are also calculated from the parameters, including the oxygen index (OI = S3/TOC), hydrogen index (HI = S2/TOC), production index (PI = S1/(S1 + S2)), and hydrocarbon potential (S1 + S2). All results are checked and calibrated using the Institut Français du Pétrole Energies Nouvelles standards.

The Jordan source rock samples displayed varying TOC ranging from 13 % to 18 %. The parameters from RockEval 7S are presented in Table 2. The samples are numbered descending from the highest (Jordan-1) to the lowest (Jordan-4) TOC, whereas the HI indicates a slight increase with the decrease in TOC. A modified Van Krevelen diagram is plotted against the HI and OI of the analyzed samples, suggesting a Type II kerogen with high sulfur content (Fig. 3(a)). This type of kerogen represents the deposition of organic matter in marine environments under euxinic conditions. A cross-plot between the TOC and hydrocarbon potential yield (S1 + S2) characterized the studied source rocks samples as having excellent quality (Fig. 3(b)). However, the

corresponding T_{max} values for these samples are low (about an average of 419 °C). The low T_{max} values suggest that the studied source rock has not reached the optimum thermal maturity window to generate hydrocarbons and is therefore characterized as an immature source rock interval (Fig. 3(c)). The complex pyrolysis plots for each sample are displayed in the appendix (Figs. A.2 to A.4).

2.3. Bulk mineralogy determination of Jordanian oil shale samples

The mineralogical composition of the tested Jordanian oil shale samples was determined through an x-ray powder diffraction (XRD) analysis (RAYONS x-ray instrument) [81]. The equipment applied a cobalt K α radiation source at 40 mA and 40 kV. A Rietveld x-ray diffractometer was used for achieving the XRD patterns and Rietveld refinement. High Score Plus software was used to identify the size of each phase.

The mineralogy presented in Table 3 indicated that a significant composition of the samples is calcite and quartz with very few traces of phosphate minerals (i.e., berlinitic and apatite). Nevertheless, some variation exists in the mineral abundance between the analyzed samples, as illustrated in Table 3. The highest calcite abundance was found in Jordan-2 at 92 wt%, and the lowest was in Jordan-4 at 44 wt%. Jordan-1 and 3 demonstrated a high calcite abundance of 85 % and 73 %, respectively. While Jordan-1, 2, and 3 have a low quantity of quartz (between 4 and 14 wt%), Jordan-4 contains 54 wt%. Overall, the XRD findings suggest that the samples contain minerals ordinarily present in shale rocks.

2.4. Surface characterization and pore-size determination of Jordanian oil shale samples

Scanning electron microscopy (SEM) was conducted using the Quattro SEM instrument. The SEM images in Fig. 4 demonstrated that the samples were fine-grained and moderately to poorly sorted, ranging from packstone (Jordan-1, 2, and 3) to wackestone (Jordan-4). The images display inter-particle porosities with small moldic porosities filled with bio-micritized clasts of peloids, plankton foraminifers, bryozoans, and echinoderms that indicate the heterogeneity of the packed shale source rock.

A Tristar II (3020) instrument was used to conduct low-pressure nitrogen (N₂, 99.99 vol%) adsorption-desorption isotherm measurements at 77 K to measure the pore volume, specific Brunauer–Emmett–Teller (BET) surface area, and average pore size of the rocks. The pore system among all samples is primarily reduced by syntaxial calcite cement and the bio-micrite volume. The packing influence

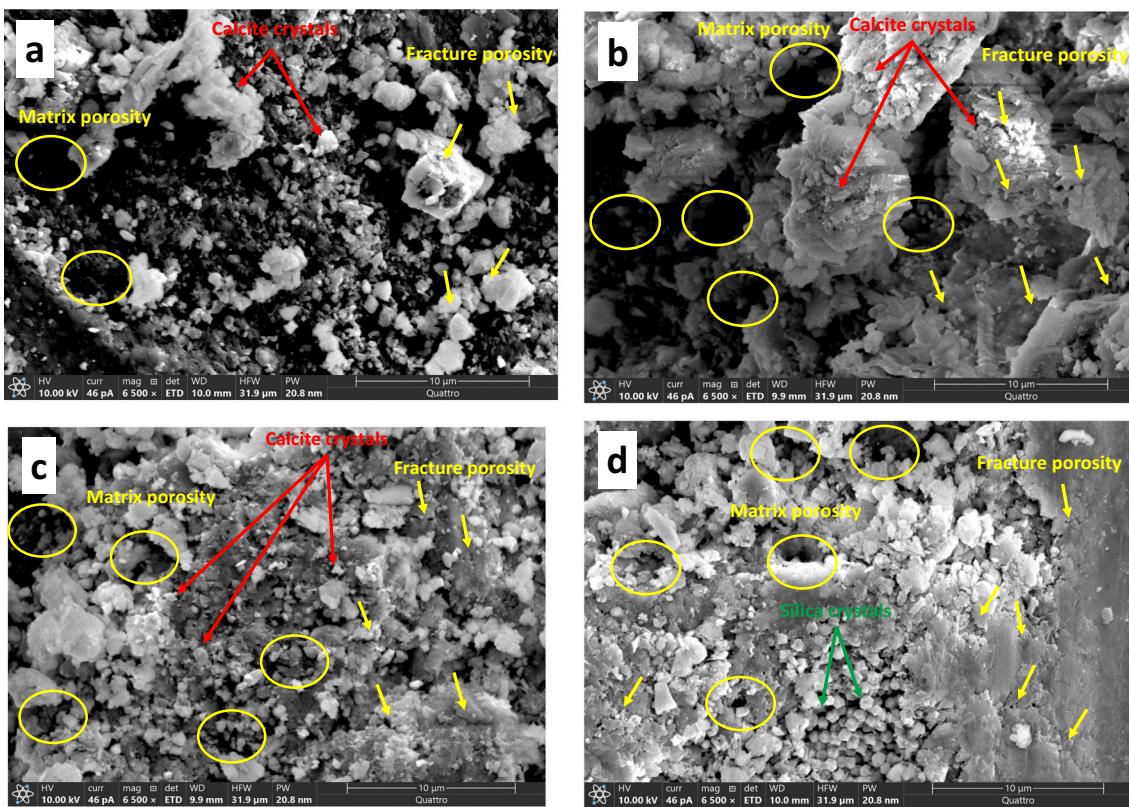


Fig. 4. Scanning electron micrographs of Jordanian oil shale samples: a) Jordan-1, b) Jordan-2, c) Jordan-3, and d) Jordan-4.

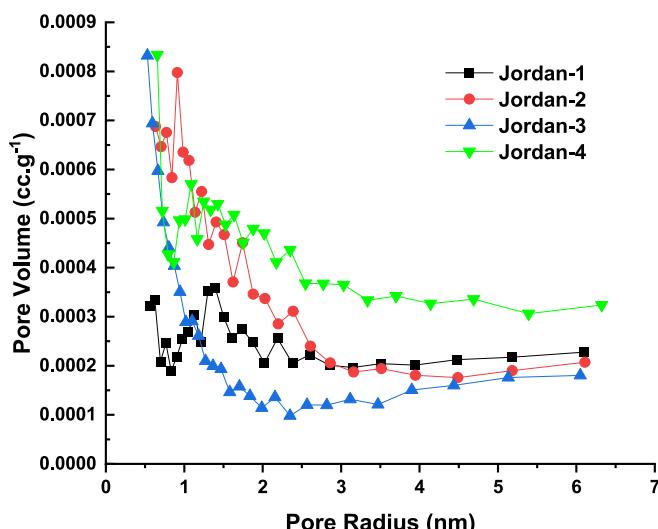


Fig. 5. Associated pore-size distribution of the analyzed Jordanian oil shale samples.

Table 4

Textural properties of the examined samples (summary of N₂ Brunauer–Emmett–Teller (BET) surface area).

Sample Name	Jordan-1	Jordan-2	Jordan-3	Jordan-4
Specific surface area, m ² /g	3.08	3.68	3.53	3.19
Pore volume, cm ³ /g	0.032	0.031	0.024	0.011
Average pore throat radius, nm	20.7	17.3	13.62	7.365
Type of pores (2–50 nm)	Mesopores	Mesopores	Mesopores	Mesopores

of various calcified components on the pore system presented by the SEM images (Fig. 4) is reflected in the pore distribution from the N₂ adsorption/desorption isotherms in Fig. 5.

The average pore-size distribution measured from the N₂ adsorption-desorption isotherms of all analyzed samples ranges from 15 to 42 nm (Table 4), indicating a mesoporous system (below 50 nm) with a negligible presence of micropores according to IUPAC nomenclature (Rouquerol et al., 1994). Furthermore, the total volume was measured at relatively low pressures approaching 1, based on the N₂ adsorption-desorption isotherms (Table 4).

2.5. Surface functional groups and topography of Jordanian oil shale samples

The chemical active functional groups on the surface of the rock were characterized (within a wavenumber of 650–4000 cm⁻¹) through Fourier transform infrared (FTIR) spectroscopy analysis using a PerkinElmer spectrometer (100-FTIR instrument). The FTIR spectra of the Jordanian shale samples are presented in Fig. 6, which demonstrates a series of peak patterns with diversified functional groups (Table 5). The spectra primarily characterize band series of vibrations of calcium carbonate (CO₃²⁻) ions at the band from 690 to 874 cm⁻¹ and at peaks of 2853 and 2927 cm⁻¹ (Andersen and Brečević, 1991; Rodriguez-Blanco et al., 2011).

The highest sharp stretching characteristics of hydrocarbons were demonstrated at 1420 cm⁻¹, which most likely represents C—H bonding and refers to the presence of hydrocarbon film on the surface of the rock samples. Additionally, other peaks of H functional groups might be observed at 2853 and 2927 cm⁻¹. There is a broad mountain centered at about 3622 and 3699 cm⁻¹, a characteristic of the hydroxyl O—H stretching mode of alcohols. The breadth of this signal is a consequence of H₂ bonding between molecules. Furthermore, bands of free-electron functional groups are recognized: a weak carbonyl peak C = O at

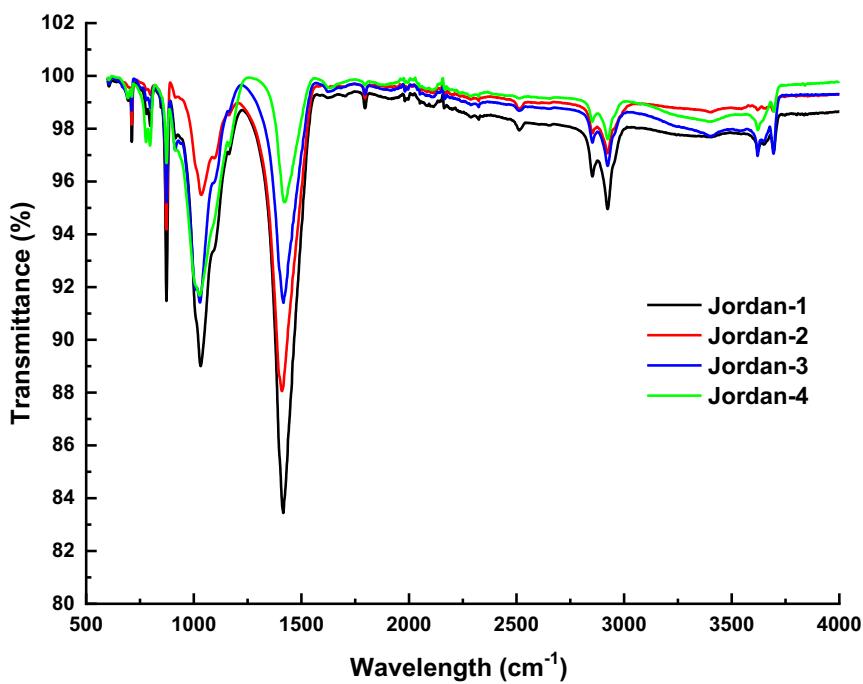


Fig. 6. Fourier transform infrared spectra of Jordanian oil shale samples at different depths.

Table 5

Fourier transform infrared spectra signals in Jordanian shale source rock samples based on guidelines provided by Coates (2006).

Peak wave number [cm ⁻¹]	Proposed assignment	Mineral/compound	Reference
778–875	In-plane bending mode of CO ₃ ²⁻	Calcite or vaterite	Rodriguez-Blanco et al. [82]; Andersen and Brecevic [83]
695–712		Calcite	Kiefer et al. [84]; Ji et al. [85]; Chakrabarty and Mahapatra [86]
871	Out-of-plane bending vibration of CO ₃ ²⁻	Calcite	Kiefer et al. [54]; Wang et al. [87]
1030	S=O stretching	In sulfoxide	Coates [88]
1083	Symmetric CO ₃ ²⁻ stretching vibration		Wang et al. [87]
1420	C-H stretching vibrations	Hydrocarbon film	Nandyanto et al. [89]
1626	C=C in stretching	In alkene	Nandyanto et al. [89]
1798	COOH functional group in aromatic compounds	Combination of a broad -OH stretch and a C=O stretching peak in ester (arachidyl dodecanoate)	George et al. [90]
2853	In-plane bending mode of CO ₃ ²⁻ and CH groups	In alkane compounds	Ji et al. [85]
2927	In-plane bending mode of CO ₃ ²⁻ and CH groups	In alkane compounds	Ji et al. [85]
3622	Primary O—H group	In organic compounds	Coates [88]
3699	Secondary O—H group	In organic compounds	Coates [88]

Table 6

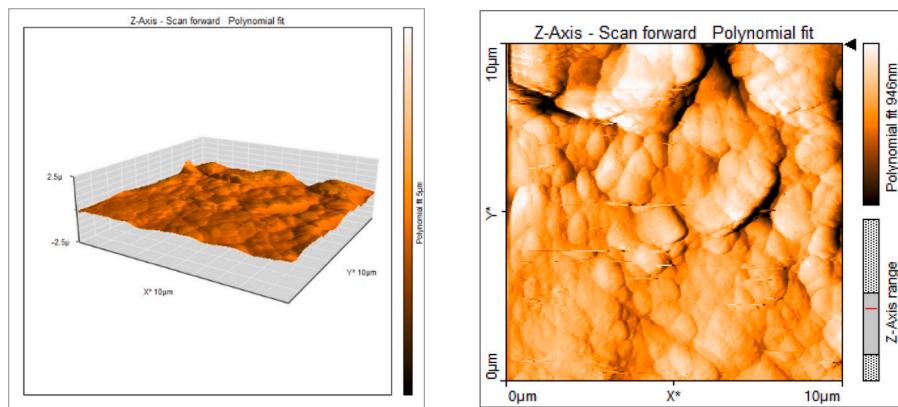
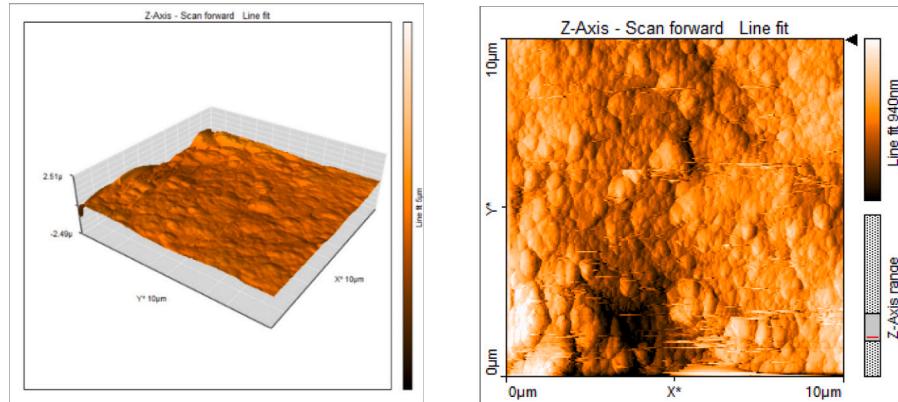
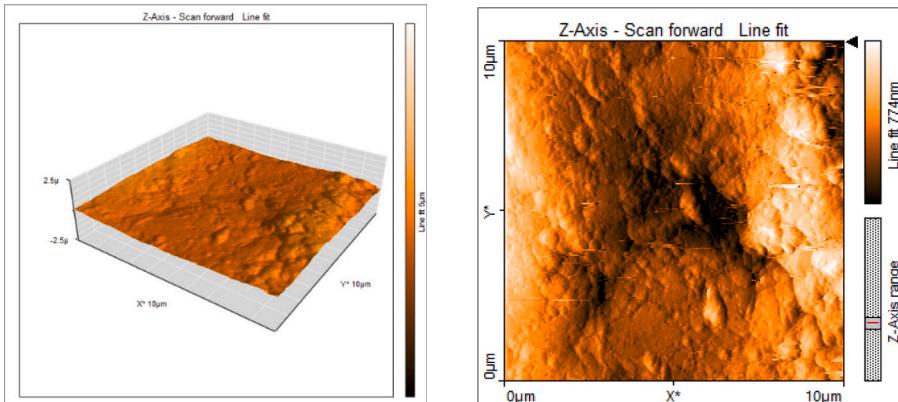
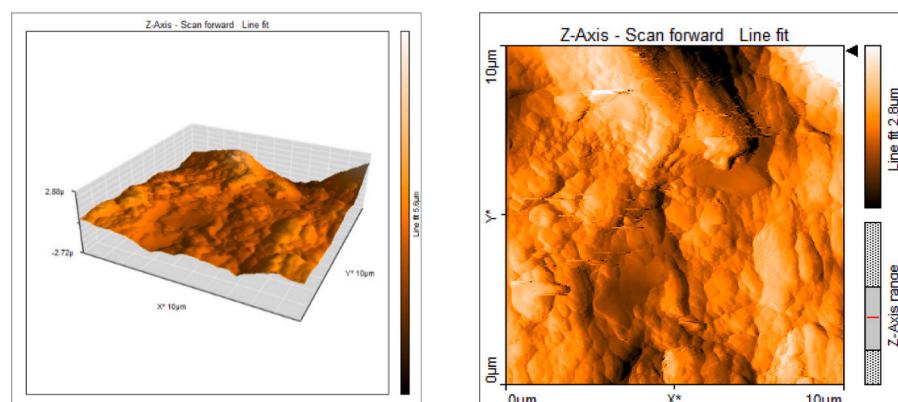
Root mean square surface roughness obtained from atomic force microscopy.

Surface roughness (nm)			
Jordan-1	Jordan-2	Jordan-3	Jordan-4
136	89	142	399

1798 cm⁻¹ and a middle peak of sulfonyl groups S = O at 1030 cm⁻¹.

The distribution of the peaks varies among the analyzed samples. The carbonate ion (CO₃²⁻) signals descend from the highest peak in Jordan-1, followed by Jordan-2 and 3, to the lowest in Jordan-4. Similarly, the C—H bond stretching at 1420 and 2853 cm⁻¹ and bond bending at 2927 cm⁻¹ follow the same trend, corresponding to the variation in TOC from the highest (Jordan-1) to the lowest (Jordan-4). In addition, the carboxyl group (COOH) stretching vibrations observed at 1798 cm⁻¹ demonstrated a similar signal trend between samples. Only the stretching frequencies of sulfonyl functional groups at 1030 cm⁻¹ and the hydroxyl functional groups at 3622 and 3699 cm⁻¹ displayed some variation. The S = O bond is more firmly in Jordan-1 (the highest TOC) than Jordan-4, where Jordan-1 > Jordan-4 > Jordan-3 > Jordan-2. While the peaks of the O—H bond stretching were observed as follows: Jordan-3 > Jordan-1 > Jordan-4 > Jordan-2. A detailed explanation of the major signals in the FTIR spectrum of the source rock samples is presented in Table 5.

The surface roughness of the Jordanian oil shale samples was determined using atomic force microscopy (AFM; Flex-Axiom, Nanosurf with a C3000i controller). The AFM results of the studied samples are presented in Table 6 and Fig. 7. The order of increasing surface roughness based on the AFM results is Jordan-4 > Jordan-3 > Jordan-1 > Jordan-2. Previous studies have revealed that the contact angles of CO₂/brine and H₂/brine systems on storage rocks decreased with increasing surface roughness and that the brine advancing/receding angles measured on smooth surfaces are higher than those on rough surfaces because the brine droplet diffuses quickly into the grooves on uneven surfaces [91–93]. However, the variations in surface roughness among the Jordanian oil shale samples used for this study should have no significant effect on the contact angle values because the changes in surface roughness between each sample were <1 μm (1000 nm) [93].

a) Jordan-1**b) Jordan-2****c) Jordan-3****d) Jordan-4****Fig. 7.** Two- and three-dimensional topography of the four Jordanian source rock samples.

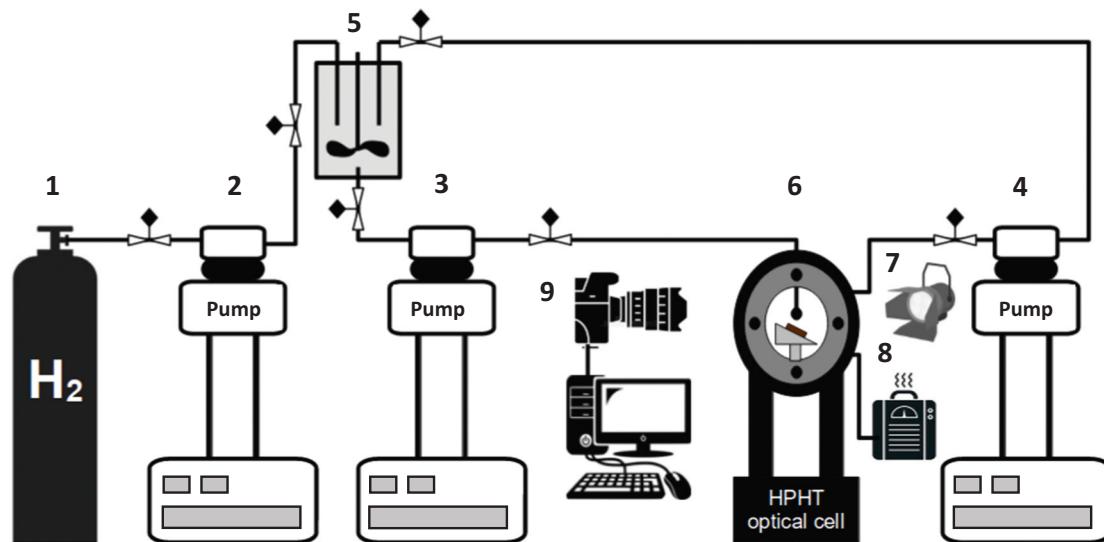


Fig. 8. Schematic of high-pressure, high-temperature (HPHT) contact angle system: (1) Gas bottle, (2) ISCO syringe pump for gas, (3) HPHT Hastelloy cell with tilted plate housing, front view, (4) ISCO syringe pump for live brine, (5) brine feed source, and (6) high-resolution video camera with acquisition and interpretation system.

2.6. Interfacial tension and contact angle measurement

Contact angles (advancing and receding) were measured in high-pressure, high-temperature (HPHT) cells using the tilted plate technique (17°) to assess the wetting behaviors of organic-rich carbonate rock in the presence of H_2 /brine, CH_4 /brine, and $\text{H}_2\text{-CH}_4$ /brine mixture systems [94]. Two Teledyne ISCO D-260 pumps were connected to the HPHT cell to introduce fluids into the viewing cell (the pressure precision is 0.01 %). Thermodynamic equilibration was conducted in a mixing reactor (500 mL Parr) affixed to the gas cylinder (H_2 and CH_4) and the brine ISCO pump to prevent mass transfer effects between the gases (H_2 and CH_4) and brine during contact angle experiments. The Jordanian sample thin section was positioned in the IFT cell, followed by gas injection (H_2 , CH_4 , or $\text{H}_2\text{-CH}_4$ mixture). The fluid temperature in the viewing cell and ISCO pumps was maintained using a heating tape and controller (HTC101-002) and a heating bath (900 °F, Julabo), respectively. Once the experimental pressure and temperature conditions were reached, a droplet ($5 \pm 0.75 \mu\text{L}$ drop size) of equilibrated brine (1 % KCl + 2 % NaCl) was dispersed. Initially, the IFT measurements were conducted at the point where the droplet was about to leave the needle; afterward, it was dispensed onto the rock surface. The contact angles were recorded at the droplet's leading (for advancing contact angles) and trailing edges (for receding contact angles). A high-performance camera was used to video-record the procedure, and contact angles were measured with ImageJ software for further analysis. We repeated the experiments thrice and computed the average standard deviation (± 3) based on repeated measurements. A schematic of the experimental setup for the contact angles and IFT measurements is presented in Fig. 8.

3. Results and discussion

Rock-fluid interaction and wetting characteristics are crucial parameters controlling gas spread through a geological formation [95–97]. They regulate the storage capacity [62,98,99], fluid dynamics, and flow throughout the porous media [98,100,101]. In addition, they control the gas injection rates [100,102], gas withdrawal rates [29,103–105], and gas entrapment safety [106–109]. In this context, the receding contact angle is for the condition where gas is injected and brine is displaced. When $\theta_r > 90^\circ$, it may affect the structural entrapment of gas [110]. Further, the advancing contact angle describes the situation in which brine imbibes again and entraps the gas in clusters, causing residual

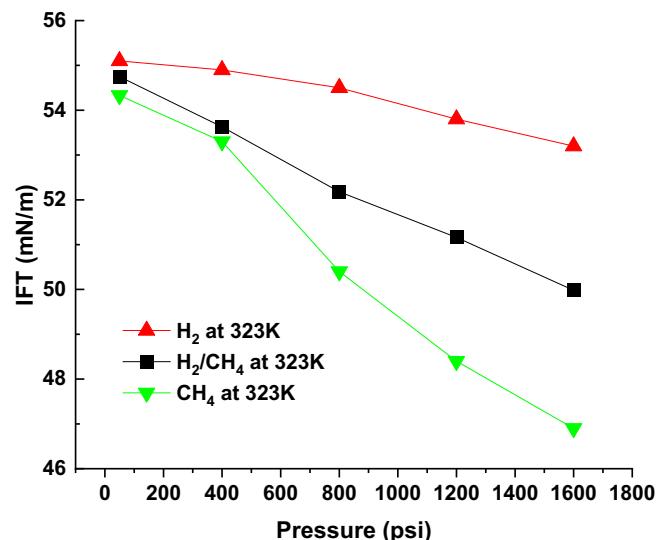


Fig. 9. Measured interfacial tension (IFT) between gas and liquid (10 wt% NaCl brine) for H_2 /brine, CH_4 /brine, and $\text{H}_2\text{-CH}_4$ /brine mixture (50 %/50 %) systems at varying pressures (50–1600 psi) and 323 K using a high-pressure high-temperature contact angle IFT system. The uncertainty based on repetitiveness is from ± 1.7 to ± 2.3 mN/m.

trapping. When $\theta_a > 50^\circ$, it may affect the primary drainage [104,111–113]. Natural geo-storage formations have an inherent organic presence, which may significantly affect the storage capacity [114–116]. Therefore, contact angles (θ_a and θ_r) were measured for four Jordanian oil shale samples with various TOC at various pressures and temperatures (0.1–1600 psi and 323 K) and compared further with other shale TOC geological formations. Moreover, IFT measurements were conducted for H_2 /brine, CH_4 /brine, and $\text{H}_2\text{-CH}_4$ /brine mixtures at similar HPHT conditions, which can further be used for gas column height calculations.

3.1. Interfacial tension of H_2 /brine, CH_4 /brine, and $\text{H}_2\text{-CH}_4$ /brine

The measured IFT values for H_2 /brine, CH_4 /brine, and $\text{H}_2\text{-CH}_4$ /brine

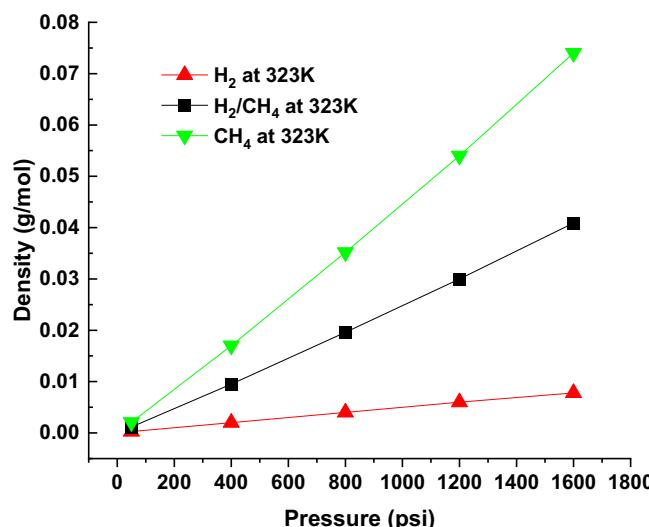


Fig. 10. Density of H₂/brine, CH₄/brine, and H₂-CH₄/brine mixture (50 %/50 %) systems at varying pressures (50–1600 psi) and 323 K [126].

systems are presented in Fig. 9. The IFT generally decreased with increasing pressure. However, the change in the CH₄/brine IFT with increasing pressure was more significant than that of the H₂/brine IFT. The steep drop beyond around 400 psi of the CH₄/brine IFT is attributed to reaching critical CH₄ conditions (i.e., 673 psi and 190.55 K). Moreover, the highest IFT values were measured in pure H₂, whereas the pure CH₄/brine IFT values were the lowest. For instance, at 323 K, the IFT value of pure H₂/brine slightly decreased from 55 to 53 mN/m, whereas the CH₄/brine IFT values decreased from 54.5 to 46.5 mN/m with increasing pressure from 200 to 1600 psi. As expected, the IFT values of H₂-CH₄/brine range between pure H₂ and pure CH₄. This trend agrees with IFT data previously reported for gas/brine IFT as a function of pressure in previous research. The trend can be attributed to increasing intermolecular cohesive interaction and decreasing the adhesive force between the brine and gas molecules due to rising gas densities with increasing pressure [6,18,36,117].

Similarly, the lower pure CH₄/brine IFT and H₂-CH₄/brine IFT compared to pure H₂/brine IFT can be attributed to higher densities of pure CH₄ and the CH₄-H₂ mixture compared to pure H₂ (Fig. 10), resulting in better interaction of pure CH₄ and CH₄-H₂ molecules at the interface in comparison to the H₂/brine system. Previous studies have also demonstrated that H₂ molecules have higher bond strength (cohesive action) and a lower relative brine solubility than CH₄ molecules [33,43].

Thus, it is likely that more pure CH₄ and H₂-CH₄ mixture molecules accumulated at the interface (due to their higher density) compared to pure H₂, which increased interfacial activity for CH₄/brine and H₂-CH₄/brine compared to pure H₂/brine systems. During UHS, the containment security of H₂ and the storage potential of the storage rocks (capillary/residual trapping capacities) and sealing integrity of the caprock (structural trapping capacities) are significantly influenced by the capillary pressure (P_c) presented in Eq. (1) [118,119]:

$$P_c = P_{H_2} - P_{water} = \frac{2\gamma \cos(\theta)}{r}, \quad (1)$$

where the H₂/brine IFT (γ) is in mN/m, and r is the capillary radius (average pore size of the rock) in nanometers (nm). The upward movement of the buoyant H₂ and leakages of the stored H₂ across the caprock are promoted when the capillary force is lower than the buoyancy pressure or buoyancy force of the H₂ plume [98,99,120]. The possibility of H₂ leakage across the caprock is high when the threshold capillary pressure is exceeded [23,53,121,122]. Lower contact angle values and higher H₂-brine IFT values are necessary for maintaining

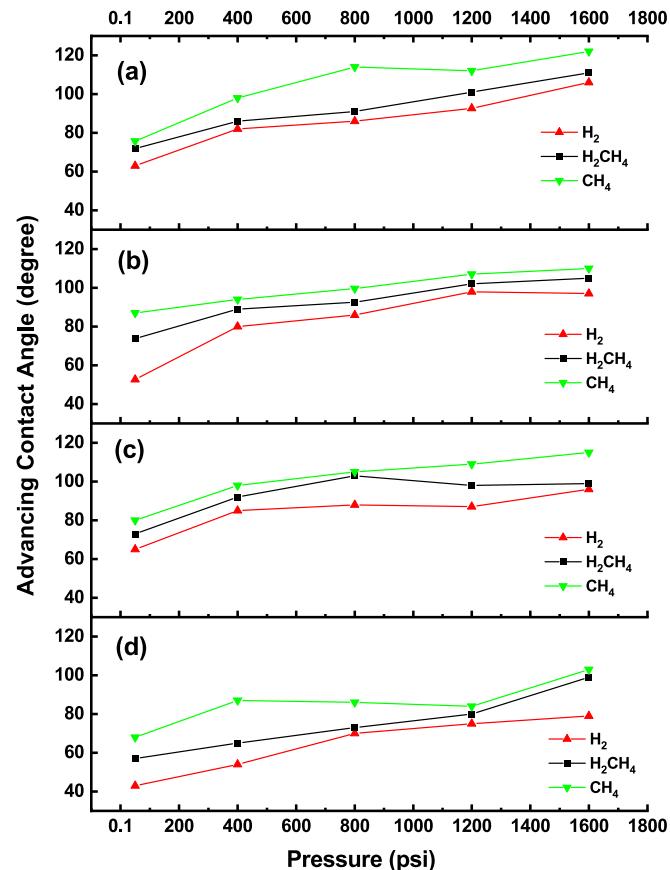


Fig. 11. Advancing contact angles of H₂/brine, CH₄/brine, and H₂-CH₄/brine mixture (50 %/50 %) systems on Jordanian oil shale samples at 323 K: a) Jordan-1, b) Jordan-2, c) Jordan-3, and d) Jordan-4. The average uncertainty obtained from repetitive measurement is $\pm 3^\circ$.

higher capillary pressure (high residual and structural trapping potential) [5,123–125].

We observed that the mixture of a potential cushion gas during UHS (CH₄) along with H₂ resulted in decreasing the IFT compared to the pure H₂/brine IFT, suggesting that the risk of stored H₂ diffusion across the caprock is high at the mixing zone between the stored gas and cushion gas (H₂-CH₄ mixture). Thus, we infer that the structural trapping of H₂ by the caprock reduces due to the H₂-CH₄ mixing zone and anticipated lower breakthrough pressure from decreasing the IFT. However, all studied Jordanian oil shale samples are high TOC shale and can only serve as the storage for H₂ through adsorption trapping mechanisms. The TOC values of the Jordanian oil shale samples as measured through RockEval pyrolysis are 13 %, 15 %, 16 %, and 18 %, corresponding for Jordan-4 to 1 in this study, arranged respectively based on the TOC. For such rocks, the increasing hydrophobicity of organic-rich rock promotes the adsorption trapping of H₂ in kerogen and the subsequent production (expulsion) of CH₄ from organic-rich rocks.

3.2. Pressure and gas mixing effect on H₂/brine, CH₄/brine, and H₂-CH₄/brine wettability

Previous research has addressed the influences of wetting behaviors on storage formation and caprock for the success of UHS in sandstone and carbonate formations [29,53,55,121,127]. However, the influence of H₂-cushion gas mixed-zone wettability on the containment security of H₂ in organic-rich shale source rocks has never been reported in the literature, to the best of the authors' knowledge. We measured contact angles at 323 K and varying pressures (0.1–1600 psi) to assess the effect of pressure and gas type (pure CH₄, pure H₂, and H₂-CH₄ mixtures) on

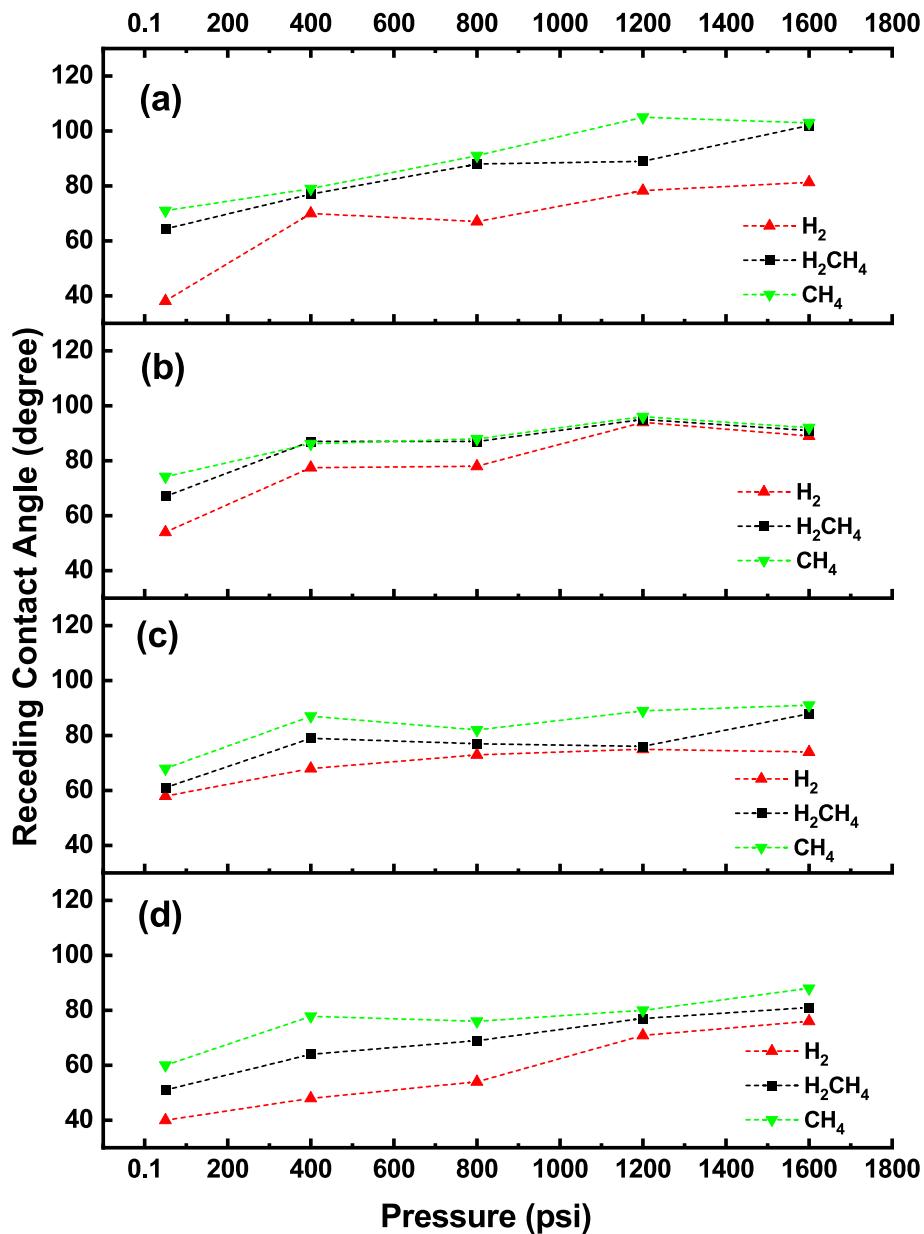


Fig. 12. Receding contact angles of H_2 /brine, CH_4 /brine, and H_2 - CH_4 /brine mixture (50 %/50 %) systems on Jordanian oil shale samples at 323 K: a) Jordan-1, b) Jordan-2, c) Jordan-3, and d) Jordan-4. The average uncertainty from repetitive measurement is $\pm 3^\circ$.

the wettability of organic-rich shale source rock.

The contact angles of H_2 , CH_4 , and H_2 - CH_4 mixtures on organic-rich shale rocks at various pressures are presented in Figs. 11 and 12 and Table A.1. The plotted contact angle datasets indicate that the gas type demonstrated varying characteristics on the studied Jordanian oil shale samples (Jordan-1 to 4) at various pressures. The contact angles generally increased with increasing pressure due to the increasing gas densities and intermolecular cohesive forces at higher pressures, promoting the interaction between the gas molecules and rock surfaces at higher pressures [30,128,129].

For instance, considering the Jordan-4 sample with the lowest TOC (13 wt%), the contact angles of H_2 /brine systems ranges between 43° and 79° (for θ_d) and 43° and 76° (for θ_r), suggesting a weakly water-wet condition as the pressure ranges between 50 and 1600 psi at 323 K. At the same pressure range and temperature conditions, the contact angles of CH_4 /brine systems range between 68° and 103° (for θ_d) and 60° and 88° (for θ_r), indicating weakly water-wet to intermediate-wet conditions. Similarly, at similar pressure ranges and temperature conditions,

the contact angles of H_2 - CH_4 /brine systems range between 73° and 99° (for θ_d) and 61° and 88° (for θ_r), suggesting weakly water-wet to intermediate-wet conditions (Figs. 11 and 12).

These results can be attributed to the density differences between H_2 , CH_4 , and the H_2 - CH_4 mixture, as depicted in Fig. 10. The interactions between the CH_4 molecules and the surface of the rock are higher than those for H_2 molecules and the rock surface. The results indicate that the contact angles of CH_4 are higher than those of the H_2 contact angle ($CH_4 > H_2$ - $CH_4 > H_2$). This outcome implies that the rock is less water-wet at the H_2 - CH_4 mixing zone than in the working zone. The increasing predisposition of the rock to become more hydrophobic at the H_2 - CH_4 mixing zone is beneficial for the adsorption trapping mechanism, which favors the adsorption of gas molecules in micropores [60,65]. This predisposition permits significant quantities of H_2 to be trapped on kerogen and the subsequent CH_4 expulsion (recovery) from the organic-rich Jordan shale formation [33,43].

In contrast, higher contact angles of H_2 - CH_4 mixtures on the Jordanian oil shale samples than those of pure H_2 also suggest that capillary

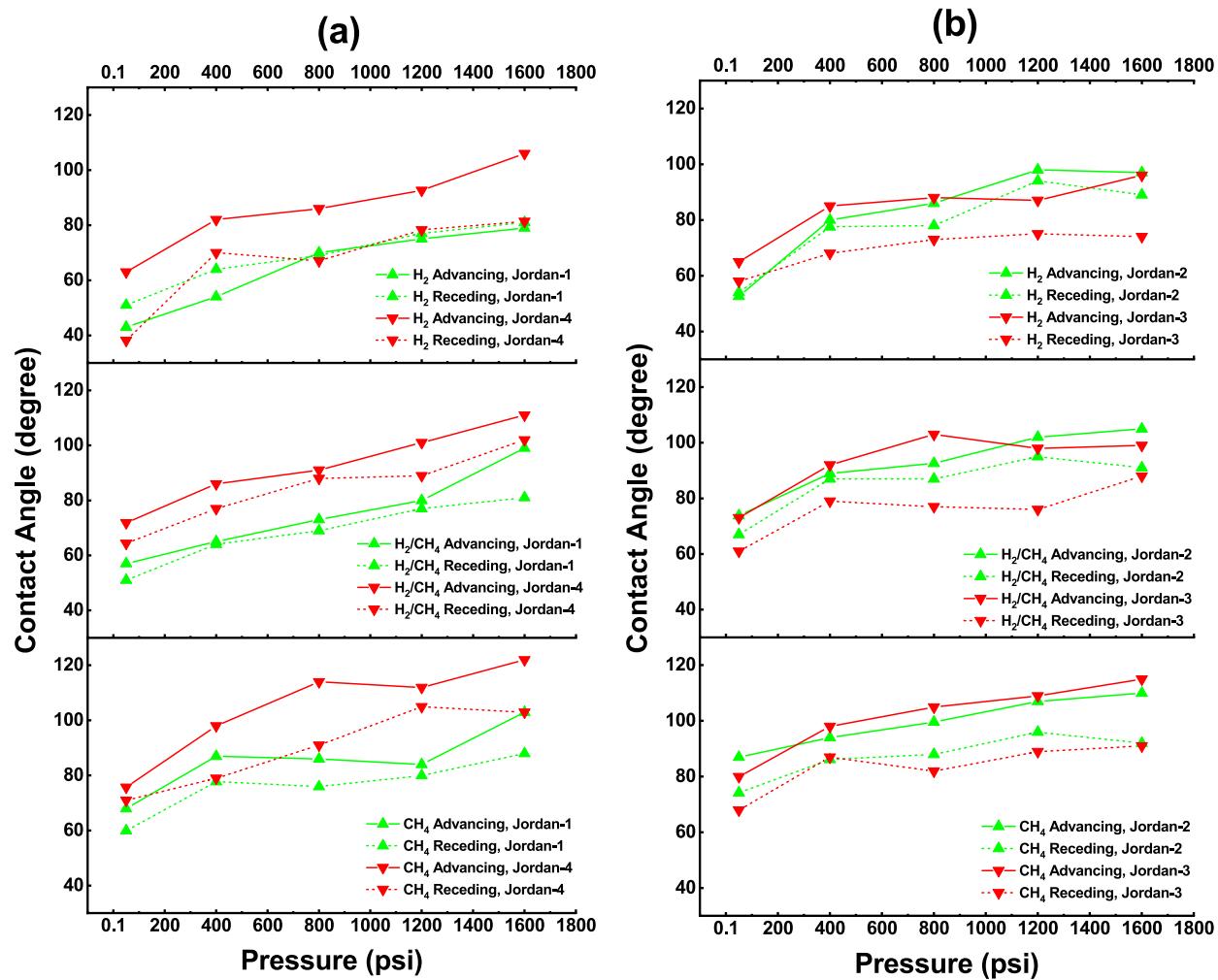


Fig. 13. Advancing and receding contact angles of H_2 /brine, CH_4 /brine, and $\text{H}_2\text{-CH}_4$ /brine mixture (50 %/50 %) systems as a function of pressure and total organic carbon (TOC) at 323 K – a) highest TOC (Jordan-1, TOC = 18 %) and lowest TOC (Jordan-4, TOC = 13 %) and b) intermediate TOC samples (Jordan-2, TOC = 16 %; Jordan-3, TOC = 15 %).

entry pressure is lower and that the associated structural integrity of caprock for H_2 entrapment is lower [98,102,130]. Generally, as the receding contact angles increase beyond 90° , an upwardly directed suction force (lower capillary pressure) initiates that significantly increases the capillary leakage (risk of H_2 leakage via the caprock), reduces H_2 column heights, and reduces containment security.

3.3. Effect of total organic carbon on H_2 /brine, CH_4 /brine, and $\text{H}_2\text{-CH}_4$ /brine wettability

Organic acids are inherently available in formation water due to reductive conditions where anoxic situations thrive [3,114–116]. The presence and quantity of organic materials depend on the formation type. However, a minimal existence is enough to significantly influence the petro-physical (i.e., pore system), petro-graphical (i.e., mineralogy and elemental composition), and wetting characteristics of any geological formation [131–133], affecting gas entrapment safety and storage quantity [6,117]. Moreover, the organic-rich shale formations have an abundance of organics (straight and branched chain), similar to the studied Jordanian oil shale rocks [61,62,134,135]. Recently, some studies have demonstrated the functional dependence of gas wettability on organics, source rock type, and TOC [62,136–138].

In this section, the influence of TOC on H_2 /brine, CH_4 /brine, and $\text{H}_2\text{-CH}_4$ /brine systems for the four Jordanian oil shale samples was investigated for a wide range of pressures (0.1–1600 psi) at 323 K. The

dynamic contact angles for the analyzed samples are illustrated in Fig. 13, indicating an increasing trend with TOC ranging from 13 to 18 wt% (high to ultrahigh) for all three gas systems. The results imply a shift in wettability status from intermediate-wet ($70^\circ < \theta < 110^\circ$) to weakly H_2 -wet ($110^\circ < \theta < 130^\circ$) [99,139]. For example, the advancing contact angle for the H_2 /brine system for Jordan-1 at 1600 psi and 323 K increased from 96° to 106° , whereas for CH_4 /brine and $\text{H}_2\text{-CH}_4$ /brine systems, it increased from 115° to 122° and 99° to 111° , respectively. Additionally, the receding contact angle at the same conditions rose from 76° to 81° , 88° to 103° , and 81° to 102° for H_2 /brine, CH_4 /brine, and $\text{H}_2\text{-CH}_4$ /brine systems, respectively.

Comparing the highest (Jordan-1) and lowest TOC (Jordan-4), Fig. 13(a) indicated that the contact angle increase is also a function of pressure. As the pressure increased, the higher TOC sample exhibited higher contact angles, and the lowest TOC sample displayed the lowest contact angles. This outcome indicates a higher shift toward H_2 -wet conditions for higher TOC samples. Jordan-2 and 3 displayed close behavior regarding the difference in TOC for both samples at only 1 wt %. Hence, no significant discrepancy was identified in Fig. 13(b) because both samples have similar mineral compositions, as presented in Table 3, particularly in calcite and quartz content.

The average increments in contact angles due to the increase in TOC from 13 to 18 wt% are approximately 10° in advancing and 15° in receding angles, implying that TOC has a more pronounced influence on the receding contact angle. In the context of H_2 geo-storage, the receding

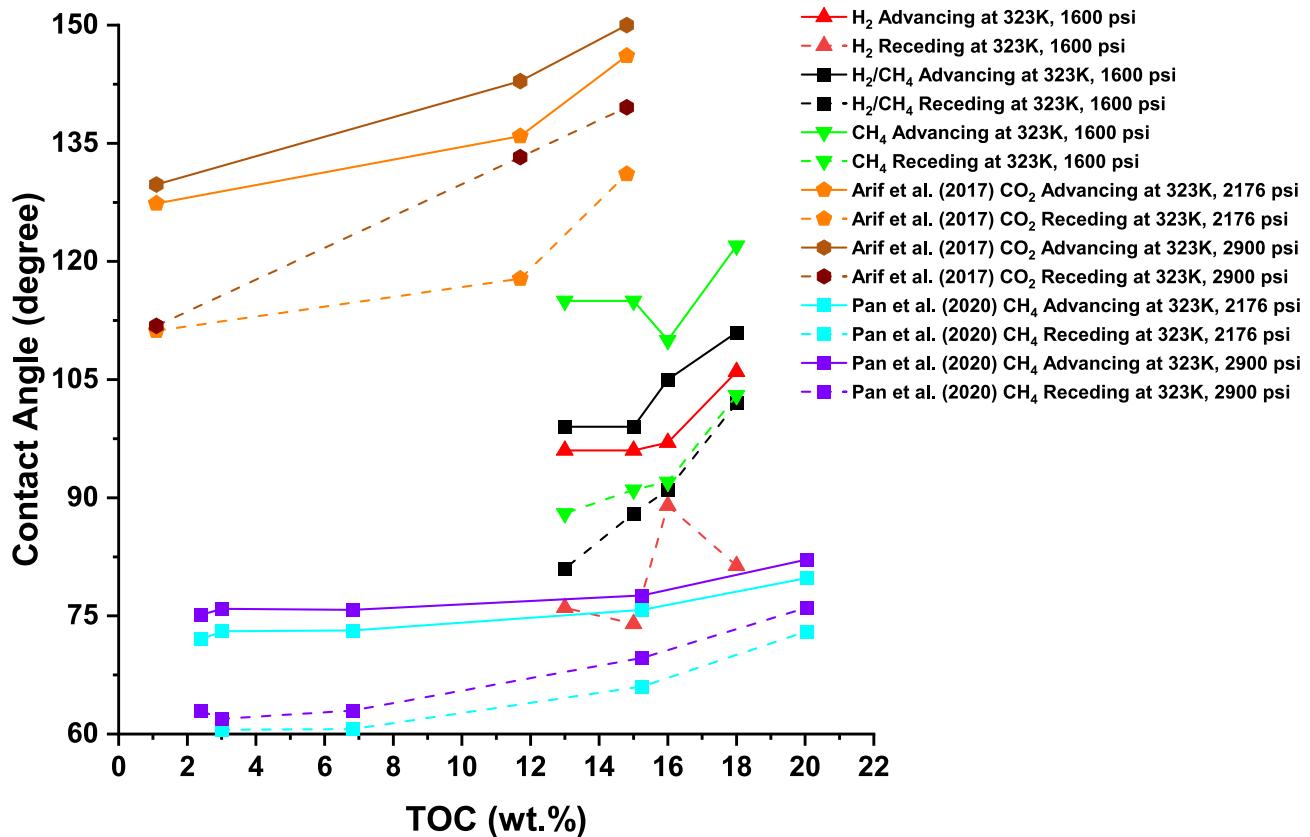


Fig. 14. Advancing and receding contact angles of H₂/brine, CH₄/brine, and H₂-CH₄/brine mixture (50 %/50 %) systems as a function of total organic content (TOC) for Jordanian oil shale samples, including CO₂/brine contact angles of high TOC shale from Arif et al. (2017) [62] and CH₄/brine from Pan et al. (2020) [61]. The average uncertainty from repetitive measurement is $\pm 3^\circ$.

contact angle typically represents the structural trapping mechanism, a significant H₂ trapping mechanism in geological formations [39,121,140]. Moreover, the effect of TOC is consistent with previous studies (Fig. 14) [61,62].

The function of shale TOC for CO₂/brine and CH₄/brine systems has behaved similarly in previously reported studies for wettability measurements at various geo-storage conditions in terms of pressure and temperature [61,62]. The brine contact angles increased for CO₂ and CH₄ gases as TOC increased. The current study reported a similar increase, which implies that inherent organic materials in shale formations have a strong affinity with the rock matrix, making it hydrophobic [3,61]. However, CO₂/brine contact angles were higher than other gases and mixtures at all tested HPHT conditions due to the difference in gas densities and intermolecular attraction of gas molecules to the rock surface [128]. Comparative studies have provided a wide range of shale TOC from 0.1 to 20 wt% compared to this study (13 to 18 wt%). Although the current study does not focus on varying temperature, one major similarity between the study by Pan et al. (2020) [61] and this study is the CH₄/brine contact angles. The brine contact angles reported in this study for CH₄ gas are higher than those reported for CH₄ by Pan et al. [61] due to the difference in the formation type and salinity (5 wt% NaCl for Pan et al. [61] and 2 wt% NaCl + 1 wt% KCl for this study). Organics profoundly influence the wetting characteristics and associated storage capacities compared to other influencing parameters. Therefore, it is pertinent to gauge the effect of organics in simulation studies for correct estimations, and ramifications should be considered before the injection of gases for geo-storage purposes.

This research evaluated a natural organic-rich shale source rock, which is a promising candidate for H₂ storage and inherently contains organic acids, to assess the influence of organic materials on the wettability of H₂-CH₄/brine/rock systems and the H₂-CH₄/brine IFT.

The study further evaluated the suitability of CH₄ as a cushion gas for UHS and highlighted the contributions of organic contamination to the H₂ containment security of natural organic-rich shale source rocks. However, the H₂-CH₄/brine reactions with the host rocks, which also significantly affect the storage potential of the source rock, were not studied.

4. Conclusions

Underground storage of H₂ in geological formations has been suggested as an effective technique of ensuring energy security by storing a large volume of H₂ in geo-storage formations until critical energy demand is reached [11,16–19,24,36,141–143]. Before H₂ injection into the subsurface, cushion gas injection is required to maintain the pressure in the formation and enable facile retrieval of the stored H₂ when needed [42,72,144]. Thus, a working gas zone (H₂, in this case), mixing zone (H₂-CH₄, in this case), and cushion gas zone (CH₄, in this case) must exist at the geo-storage formations [17,39,42]. There is a lack of information on the wetting characteristics and gas/brine IFT for organic-rich rock samples. This research was conducted to provide insight into the rock-wetting behaviors and gas/brine IFT during UHS in Jordanian oil shale samples. The following conclusions were reached.

- Advancing contact angles of H₂-CH₄/brine systems on four studied samples ranged between 57° and 111°, whereas the receding contact angles ranged between 51° and 102° when pressure increased from 50 to 1600 psi at 323 K. This result indicates that the organic-rich shale source rocks demonstrated weakly water-wet to weakly H₂-wet conditions at the mixing zone.
- The pure CH₄/brine system demonstrated a higher rock-wetting tendency (higher contact angles) and the lowest gas/brine IFT

- compared to H₂/brine systems under all studied pressure and temperature conditions, suggesting a higher interaction between the CH₄ molecules and rock compared to H₂. Thus, CH₄ may be used as a favorable cushion gas during H₂ storage to maintain the formation pressure.
3. The effects of pressure and temperature on the wettability and IFT of pure H₂/brine, pure CH₄/brine, and H₂-CH₄/brine systems displayed similar behavior, where higher contact angles and lower gas/brine IFT were measured at higher pressures, which is consistent with the literature [61,62].
 4. When cushion gas is injected into a geo-storage formation before H₂, the H₂-CH₄ mixture could result in decreased capillary pressure (due to reducing the IFT and increasing the contact angles), suggesting that the risk of stored H₂ diffusion across the caprock could be high at the mixing zone between the stored gas and cushion gas (H₂-CH₄ mixture). However, the increasing rock hydrophobicity could increase the adsorbed H₂ molecules on rock micropores. Thus, more H₂ could be trapped on the kerogen of rock through adsorption trapping, resulting in CH₄ production and a balance between enhanced CH₄ recovery and reduced/decreased capillary trap/structural entrapment.
 5. Although higher contact angles and lower IFT for the H₂-CH₄/brine system suggest that the trapping capacity of H₂ could be reduced at the H₂-CH₄ mixing zone due to the anticipated lower breakthrough pressure, the increasing affinity of these rocks to the CH₄ instead of H₂ could decrease the likelihood of H₂ diffusion into the pore space, promoting easier separation during H₂ injection and withdrawal cycles.
 6. The influence of TOC on H₂/brine, CH₄/brine, and H₂-CH₄/brine systems was also investigated for a wide range of pressures (0.1–1600 psi) at 323 K. The results indicated a significant shift in wettability from intermediate-wet ($70^\circ < \theta < 110^\circ$) to weakly gas-wet ($110^\circ < \theta < 130^\circ$) as the TOC increased, which is consistent with previous studies using synthetically acid-aged shale samples.
 7. The present work demonstrated a similarity in the H₂/brine and CH₄/brine wettability behavior by comparing the current study using the actual high TOC shale (13 to 18 wt%) to other studies providing a wide range of shale TOC from 0.1 to 20 wt%.

Appendix A

The N₂ adsorption-desorption isotherms indicate a Type V isotherm following the work by Sing et al. (1985), attributed to the existence of mesopores with a weak interaction of N₂ on the pore surface (Garcia-Diego and Cuellar, 2005). The hysteresis in the N₂ adsorption-desorption isotherms for the four analyzed samples is relatively marginal at lower pressures (Fig. A.1). The hysteresis primarily depends on the mesoporous content and pore size. Specifically, N₂ molecules are first adsorbed on the walls of mesopores. Then, a film of the condensed adsorbed N₂ is made in the mesopores due to the depression effect of the saturated vapor pressure of confined N₂ (Andersson et al., 2018; Sing et al., 1985). Among all analyzed samples, Jordan-4 displayed the most significant hysteresis because of the diameter of the mesopores, which are near the critical diameter of N₂ at 77 K (around 4 nm; Abid et al., 2021). The pyrolysis profiles in the appendix (Figs. A.2 to A.5) indicate intermediate to high TOC values, ranging from 13 (Jordan-4) to 18 wt% (Jordan-1).

CRediT authorship contribution statement

Amer Alanazi: Conceptualization, Methodology, Investigation, Data curation, Software, Writing – original draft. **Nurudeen Yekeen:** Conceptualization, Formal analysis, Writing – review & editing. **Mujahid Ali:** Methodology, Investigation, Data curation, Validation, Software. **Muhammad Ali:** Methodology, Investigation, Data curation, Validation, Software. **Israa S. Abu-Mahfouz:** Visualization, Validation. **Alireza Keshavarz:** Validation, Resources, Project administration. **Stefan Iglauer:** Conceptualization, Visualization, Supervision. **Hussein Hoteit:** Conceptualization, Validation, Resources, Writing – review & editing, Supervision.

Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

Data availability

Data will be made available on request.

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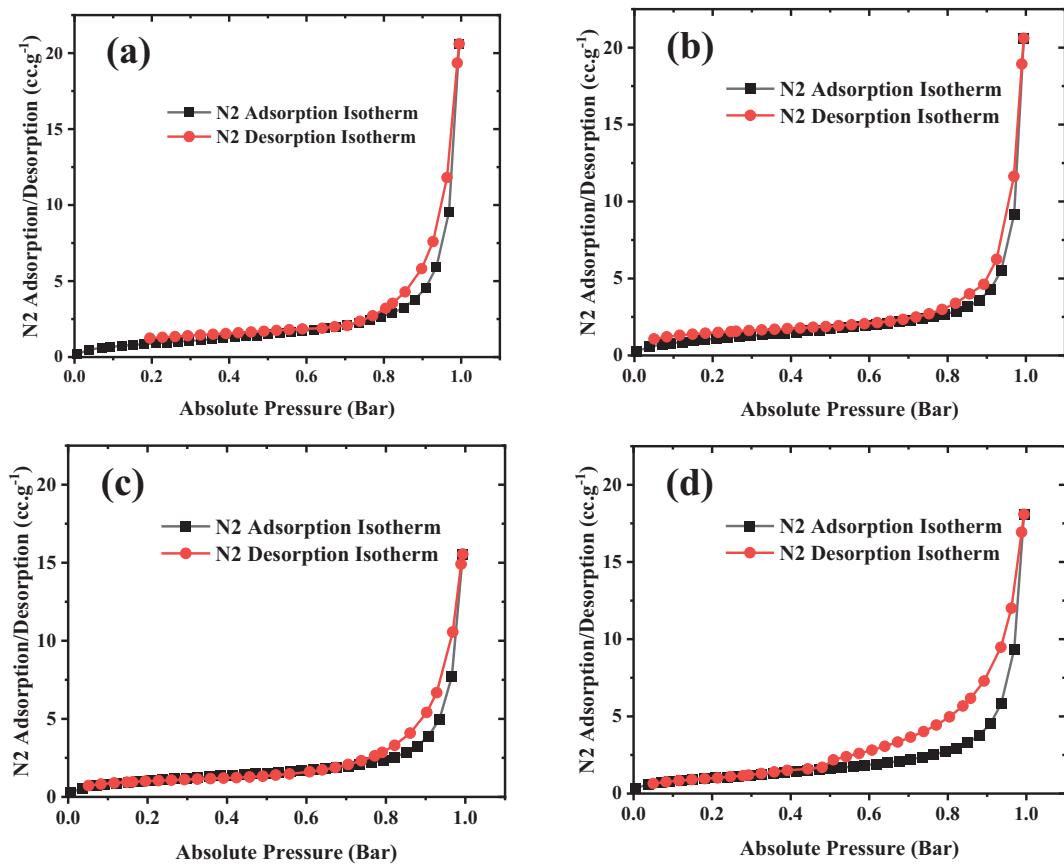


Fig. A.1. Nitrogen adsorption-desorption isotherm curves: a) Jordan-1, b) Jordan-2, c) Jordan-3, and d) Jordan-4.

The RockEval hydrocarbon pyrolysis indicates the TOC of the studied Jordanian oil shale samples depicted in Figs. A.2 to A.5.

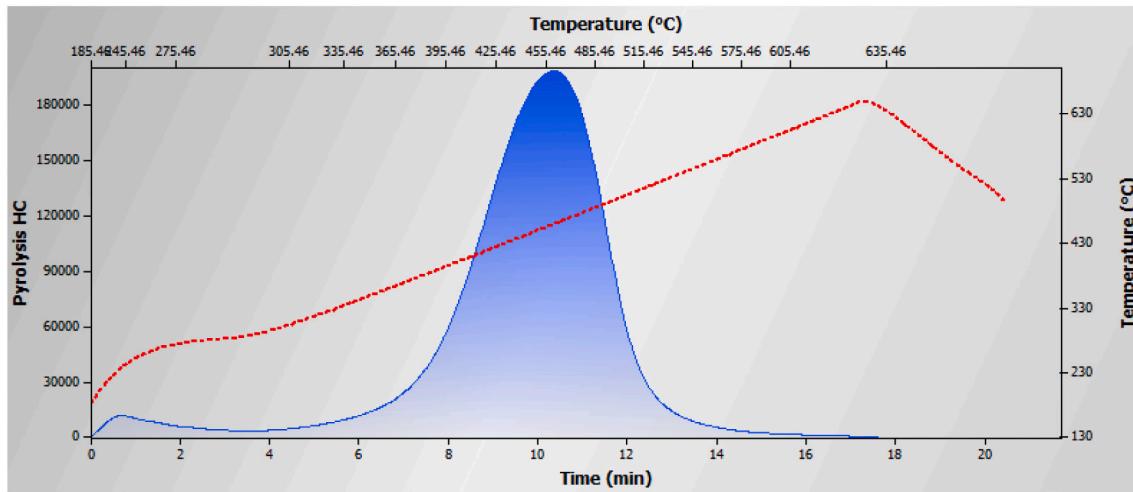


Fig. A.2. Hydrocarbon pyrolysis profile of Jordan-1 obtained from RockEval.

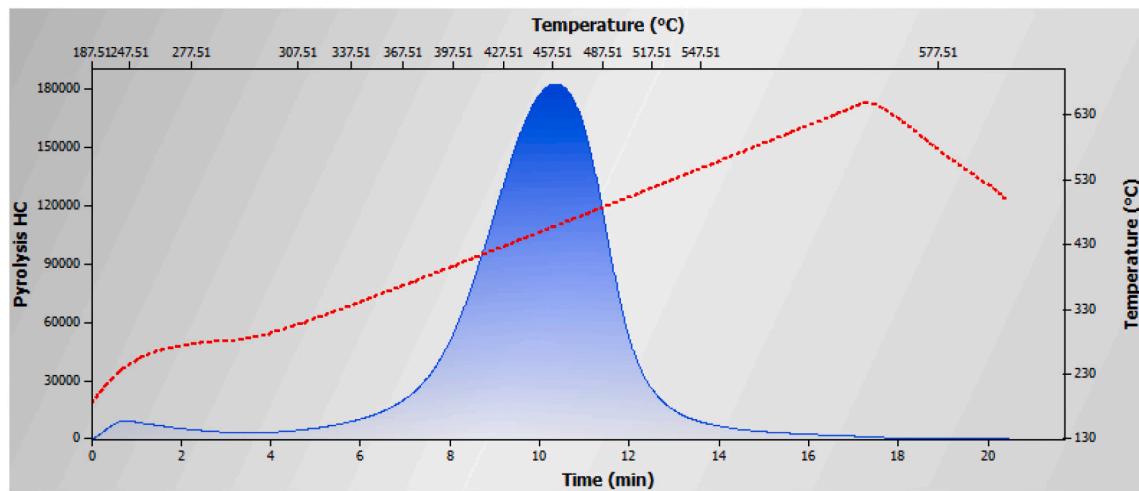


Fig. A.3. Hydrocarbon pyrolysis profile of Jordan-2 obtained from RockEval.

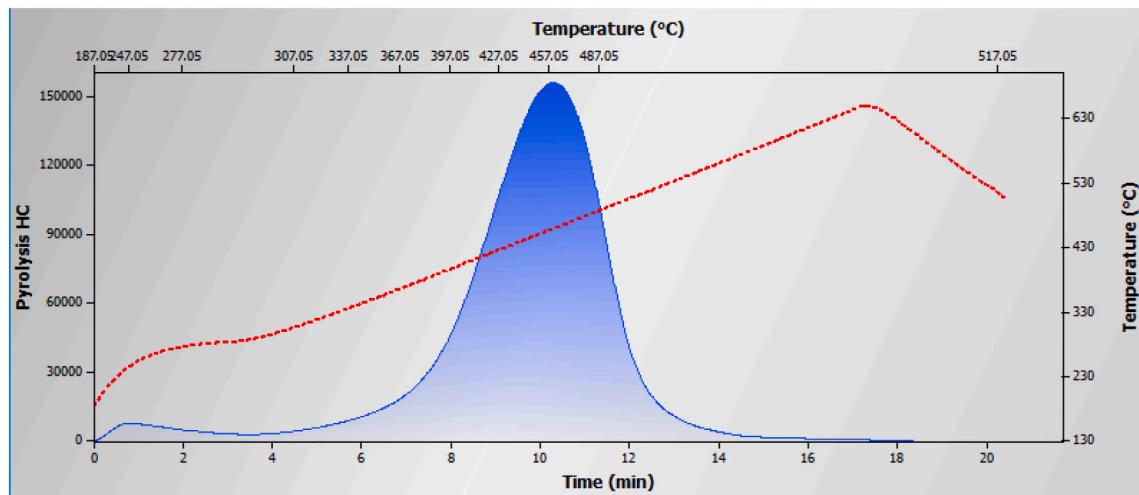


Fig. A.4. Hydrocarbon pyrolysis profile of Jordan-3 obtained from RockEval.

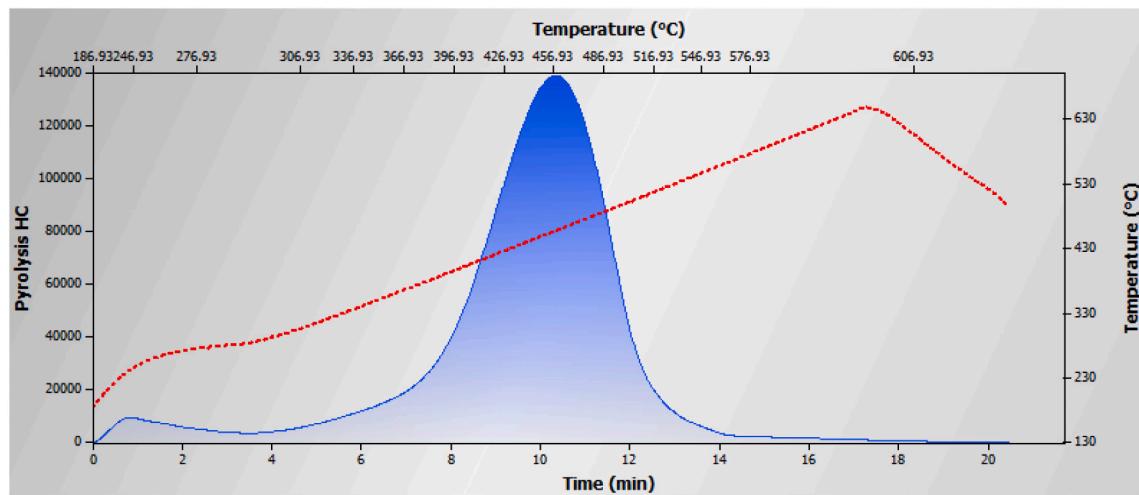


Fig. A.5. Hydrocarbon pyrolysis profile of Jordan-4 obtained from RockEval.

Table A.1Contact angles of H₂, CH₄, and H₂-CH₄ mixtures on organic-rich shale source rocks at various pressures.

Rock sample	Gas type	Pressure, psi	Contact angle, degree	
			Advancing	Receding
Jordan-1	H ₂	50	43	51
		400	54	64
		800	70	69
		1200	75	77
		1600	79	81
	CH ₄	50	68	60
		400	87	77.8
		800	86	76
		1200	84	80
		1600	103	88
Jordan-2	H ₂ /CH ₄	50	57	51
		400	65	64
		800	73	69
		1200	80	77
		1600	99	81
	H ₂	50	52.7	54
		400	80	77.5
		800	86	78
		1200	98	94
		1600	97	89
Jordan-3	CH ₄	50	87	74.2
		400	94	86.2
		800	99.6	88
		1200	107	96
		1600	110	92
	H ₂ /CH ₄	50	73.8	67
		400	89	87
		800	92.6	87
		1200	102	95
		1600	105	91
Jordan-4	H ₂	50	65	58
		400	85	68
		800	88	73
		1200	87	75
		1600	96	74
	CH ₄	50	80	68
		400	98	87
		800	105	82
		1200	109	89
		1600	115	91
	H ₂ /CH ₄	50	73	61
		400	92	79
		800	103	77
		1200	98	76
		1600	99	88
	CH ₄	50	63	38.2
		400	82	70
		800	86	67
		1200	92.6	78.3
		1600	106	81.4
	H ₂	50	75.7	71
		400	98	79
		800	114	91
		1200	112	105
		1600	122	103
	H ₂ /CH ₄	50	71.9	64.4
		400	86	77
		800	91	88
		1200	101	89
		1600	111	102

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