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Evaluation of the groundwater resources in the Geba basin, Ethiopia

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Abstract

This paper presents an assessment of the groundwater resources in the Geba basin, Ethiopia. Hydrogeological characteristics are derived from a combination of GIS and field survey data. MODFLOW groundwater model in PMWIN environment is used to simulate the movement and distribution of groundwater in the basin. Despite the limited data available, by simplifying the model as a single layered semi-confined groundwater system and by optimising the transmissivity of the different lithological units, a realistic description of the groundwater flow is obtained. It is concluded that 30,000 m³/d of groundwater can be abstracted in the Geba basin for irrigation in a sustainable way, in locations characterised by shallow groundwater in combination with aquitard type lithological units.

Keywords: Groundwater modelling, Transmissivity, Geba basin, Ethiopia

Introduction

Rainfall in Ethiopia is varying highly and erratic in time and space (Yazew 2005). As a consequence, precipitation is generally insufficient to sustain the agriculture needed to alleviate food insecurity, and it becomes very important to develop and manage all other available water resources. Groundwater is one of the renewable water resources that can be exploited in a sustainable way to help rural communities in terms of clean domestic water and irrigation.

This paper discusses the groundwater potential of the Geba basin (Fig. 1), Tigray region, northern Ethiopia. The Geba river basin is about 5,150 km², and forms part of the Tekeze-Atbara river basin, a tributary of the Blue Nile. The main economy of the area is agriculture, which accounts for more than 40% of the GDP and 80% of the labour force. Water is most crucial to support and sustain crop growth, and irrigation is often required (Leul 1994; Gemechu 2006). Hence, assessing the location and potential of additional resources as groundwater is essential. However, lack of long-term meteorological, hydrological, and hydraulic data in the basin makes accurate assessment of groundwater resources a difficult challenge.

Some groundwater investigations have been undertaken in the Geba basin by federal and regional authorities, local NGOs, or university departments. Chernet and Eshete (1982) performed some hydrogeological mapping around Mekelle (Fig. 1), the regional capital of Tigray. DEVECON (1992) investigated the water resources potential of the Mekelle area as part of the Five Towns Water Supply and Sanitation project of the Ministry of Water Resources of Ethiopia. Studies undertaken by local NGOs and the regional government for irrigation purposes have been conducted by REST (1996) and COSAERT (2001). NEDECO (1997) investigated the Tekeze river basin and described the water resources potential by borehole drilling of up to 300 m deep at several places in the Mekelle area. Hussein (2000) investigated the hydrogeology of the Aynalem well field, which supplies Mekelle with potable water. Gebregziabher (2003) used geophysical techniques as seismic refraction and magnetic and electrical profiling to investigate the hydrogeology of the Aynalem basin. WWDSE (2006) performed some hydro-meteorological, geological, and hydrogeological investigations around Mekelle, supplemented by a quasi-three dimensional groundwater flow

model. All of these studies only provide local and fragmental information, while a comprehensive insight in the groundwater resources of the Geba basin remains largely unknown. In this study the groundwater resources of the Geba basin are investigated using groundwater flow modelling integrated with GIS derived basin characteristics.

Methods

Development of Hydrogeological Data

The Geba basin is characterized by rugged terrain, with topography ranging from 960 to 3280 m. A digital elevation map (DEM), shown in Fig. 2, was derived from NASA SRTM data with 3 arc-second or a resolution of 90 m by 90 m. SRTM tiles of N12E038, N12E039, N13E38, N13E39, N14E038 and N14E039 were considered for bounding the area and subsequently preparing the DEM. For regional groundwater characterization, considerable test borings and water well-log data are required to determine the sequence and type of geological deposits. However, for the Geba basin such knowledge is lacking, except for some well-logs of the Aynalem well field, 3 km east of Mekelle city (DEVECON, 1992). Instead, hydrogeological characteristics were derived from a digital map, indicating 20 major lithological units in the basin. The map, shown in Fig. 3, was prepared in ArcView grid format (90 m pixel size) from a geologic map (Arkin et al. 1971), previous geological studies (Beyth 1972; Merla et al. 1979; Tesfaye and Gebretsadik 1982; Getaneh and Valera 2002; Sifeta, Roser, and Kimura 2005), field surveys, and satellite images.

In addition, 358 surface and ground water levels were recorded during the field surveys. The observation points included water levels in wells, boreholes, springs, reservoirs, and perennial river courses during base flow conditions (Fig. 4). The geographical location and elevation of these observation points were recorded by GPS. However, as the recorded elevations are liable to error, only horizontal coordinates from the GPS readings were considered accurate, while the water levels were adjusted by subtracting the water depth measured from the soil surface from the DEM values. Another problem with these observations is the erratic nature of the rainfall that causes large variations in water levels in hand dug wells, reservoirs, and streams in the region. Moreover, water levels usually are seasonal

(REST 2005). To simplify the model, these effects were ignored on this study, and all observations were considered as steady state.

Alene (2006) applied the WetSpass model (Batelaan and De Smedt 2001) to estimate seasonal and annual groundwater recharge in the Geba basin. He found that annual recharge ranges from zero to 215 mm per year and varies from location to location depending on slope, soil type, land-use, and climate. On average the total annual recharge was found to be 22 mm per year with a standard deviation of 33 mm, which accounts for 4% of the average annual rainfall in the area. This small amount of recharge is due to the high evapotranspiration in the region (Getnet 2005). The spatial distribution of the recharge obtained from WetSpass model was converted to a 90 m grid digital map as an input for the groundwater model.

Groundwater Modelling

The behaviour of the groundwater system was simulated using MODFLOW groundwater model (Harbaugh et al. 2000) in PMWIN Pro 7 environment (Chiang and Kinzelbach 2005). PMWIN Pro 7 has a capacity of a million computational cells. However, all GIS grid data available for the study are raster data with a 90 m × 90 m pixel size, which results in a larger number of cells than the model capacity. As a consequence, the grid was modified to a cell size of 180 m × 180 m. The number of cells in the x and y directions becomes 696 and 587 respectively, resulting in a modelled area of 125.28 km Easting and 105.66 km Northing. Active and inactive cells were defined to delineate the exact shape of the basin, and the boundary of the basin was considered as a no flow boundary condition.

The groundwater system was conceptualized as a single layered semi-confined aquifer. Hence, the following groundwater flow equation applies in a steady state

$$\frac{\partial}{\partial x} \left(T \frac{\partial h}{\partial x} \right) + \frac{\partial}{\partial y} \left(T \frac{\partial h}{\partial y} \right) + R - Q = 0, \quad (1)$$

where h is groundwater head or elevation (m), R is groundwater recharge (m/d), Q is groundwater discharge (m/d), x and y are horizontal dimensions (m), and T is transmissivity (m²/d), which is assumed to vary spatially depending on the

geological conditions. Equation 1 enables to set-up a groundwater model without specifying any vertical dimensions of the ground layers. Nevertheless, this simple model concept can produce realistic results for the regionally complex groundwater flow system if transmissivity values are optimised by calibrating the model such that a good fit is obtained between simulated and observed groundwater heads.

Groundwater discharge is modelled with the drain package of MODFLOW

$$Q = C \times \max [h - h_d, 0], \quad (2)$$

where h_d is drain level (m), and C is drain conductance (d^{-1}). Following a procedure proposed by Batelaan and De Smedt (2004), drain levels equal to topography minus 1 m are imposed over the whole basin and a large value is specified for the drain conductance, so that any groundwater level reaching the ground surface within one meter results in groundwater drainage to the surface. As such, the model is able to locate automatically all drainage and discharge areas as perennial rivers, and springs, and to quantify the corresponding discharge flux with Eq. 2.

In order for the model to provide accurate results, it is necessary to calibrate uncertain parameters until observations are reproduced with confidence. Hence, the transmissivity values of the geological formations, which are believed to be the most uncertain parameters, were optimized with PEST, a parameter estimation tool embedded in PMWIN Pro. 7. The optimization process was based on comparing simulated groundwater heads with the measured water levels inventory (Fig. 4) using three error criteria: mean error (ME), mean absolute error (MAE), and root mean squared error (RMSE). The mean error is the mean difference between computed heads h_c and observed heads h_o

$$ME = \frac{1}{n} \sum_{i=1}^n (h_c - h_o)_i, \quad (3)$$

The mean absolute error is the mean of the absolute value of the differences in measured and simulated heads

$$\text{MAE} = \frac{1}{n} \sum_{i=1}^n |h_c - h_o|_i, \quad (4)$$

and the root mean squared error is the average of the squared differences in measured and simulated heads

$$\text{RMSE} = \sqrt{\frac{1}{n} \sum_{i=1}^n (h_c - h_o)_i^2}, \quad (5)$$

where n is the number of observations.

Results and Discussion

Because of the wide spatial coverage of the basin and the large number of observations, it was not possible to optimize all transmissivity values automatically at the same time. Therefore, optimization was achieved by using 3 or 4 parameters at a time whilst other parameters were kept constant. For calibration, PEST uses RMSE as calibration criterion. Ideally, this value should be as small as zero, but for the Geba basin with complex geological conditions the RMSE target was set at 10 m. Figure 5 shows the comparison between observed and final simulated groundwater heads. The maximum error, minimum error, mean error, mean absolute error, and the root mean squared error values obtained were 19.0 m, -19.1 m, .2.0 m, 5.7 m and 7.1 m respectively, which can be considered fair in view of the regional scale and large variation in topography. The optimised transmissivity values are given in Table 1 for each geological formation and for the river beds, which were considered as a separate unit. All transmissivity values are rather small, except for the river beds, so that none of the formations can be considered as aquifers. Largest values are obtained for alluvium, Enticho sandstone, fine intrusive, granite (obviously this refers to the weathered crust), meta-sediment, trap basalt, and upper sandstone. These formations can be considered as semi-pervious aquitards, hence, able to transmit groundwater and could be possible sources for abstracting groundwater for irrigation. The other formations have very small transmissivities and can be classified as rather impervious and are not suited for abstracting groundwater.

Figure 6 shows the final simulated regional groundwater head distribution. The groundwater head varies from a minimum of 960 m around the outlet of the Geba River to maximum 3,235 m at the northern extreme. The map indicates that groundwater levels closely follow topography. Finally, the depth to the groundwater was estimated from the difference between topography and simulated groundwater levels, as depicted in Fig. 7. This map shows that while there are places where the groundwater is near the surface such that hand dug wells or shallow drilled wells could abstract groundwater for irrigation, in other localities groundwater is situated at depths of up to 200 m from the soil surface. The groundwater balance can be calculated by aggregating all groundwater flows as predicted by the model. There is only one input, recharge, which amounts in total to about 3.0×10^5 m³/d on average, and there is also only one output, groundwater drainage, which also amounts to 3.0×10^5 m³/d, yielding an average river base flow of about 3.5 m³/s at the outlet of the Geba River. This latter value corresponds well with field observations (MoWR 2002). A fraction of the groundwater transmitted between recharge and discharge can be abstracted safely without causing adverse effects (Miles and Chambet 1995). This fraction can cautiously be estimated as 10%, which amounts to 30,000 m³/d of groundwater that can be abstracted and used for irrigation in the Geba basin in a sustainable way. The possible sites where this can be achieved are locations with shallow groundwater, for instance less than 5 m below soil surface, in combination with aquitard type lithological units, which can be identified by combining Figs. 3 and 7.

Conclusions

In this study, the main objective was to investigate the distribution of groundwater in the Geba basin in Northern Ethiopia. Because of lack of detailed hydrogeological information, the groundwater system of the Geba basin was conceptualized in a simplified numerical model. However, all local variations and actual conditions were incorporated in the model by calibration of the transmissivity values for each geological unit. A steady state groundwater flow model was applied using MODFLOW model in PMWIN package. Observations of water levels collected from wells, boreholes, springs, reservoirs, and perennial

river courses were used for calibration of the groundwater model, by optimizing the transmissivity values for each lithological unit.

The comparison of observed and predicted groundwater levels shows a good agreement, with a mean error of about 2 m and a root mean squared error of 7.1 m. These results are acceptable in view of the size of the study area and lack of detailed information regarding hydrogeological conditions. From the results obtained, it can be concluded some geological formations can be considered as aquitards and could be used for groundwater abstraction, but this should be supported by local geophysical explorations. Moreover, model results also show that in many areas depth to groundwater is shallow, which would allow domestic wells to be dug for irrigation. A first and crude estimation indicates that possibly 30,000 m³/d of groundwater can be abstracted in the Geba basin in a sustainable way.

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Table 1. Calibrated transmissivity values for the lithological units.

Geological Formations	Transmissivity (m ² /d)
Adigrat Sandstone	0.13
Alluvium	0.5 - 5
Dolerite sill	0.017
Enticho Sandstone	5
Fine Intrusive	4
Granite	2.35
Limestone-Marl	0.2
Marl-Limestone	0.0016
Meta-conglomerate	0.1
Meta-greywack	0.01
Meta-limestone	1
Meta-sediment	2
Meta-volcanic	0.015
River Beds	200 - 500
Shale	0.054
Shale-Marl-Limestone	0.0015
Tillite	0.1
Transition	0.1
Trap Basalt	13.8
Upper Sandstone	16

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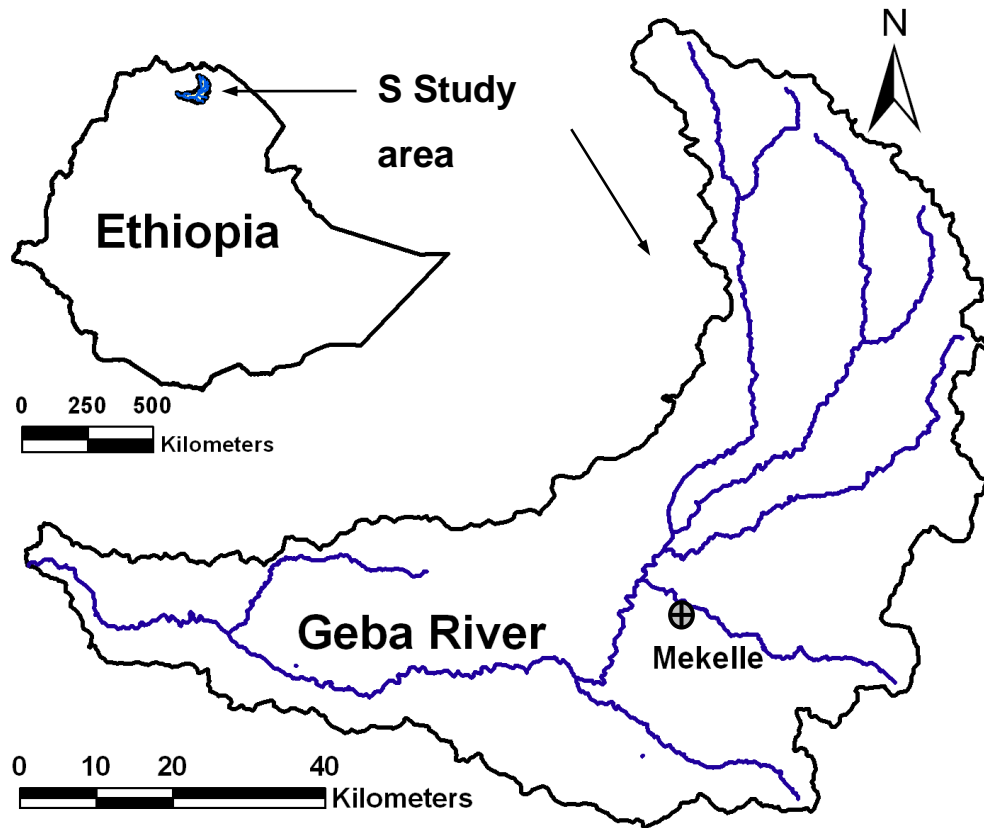


Figure 1. Location map of the Geba basin.

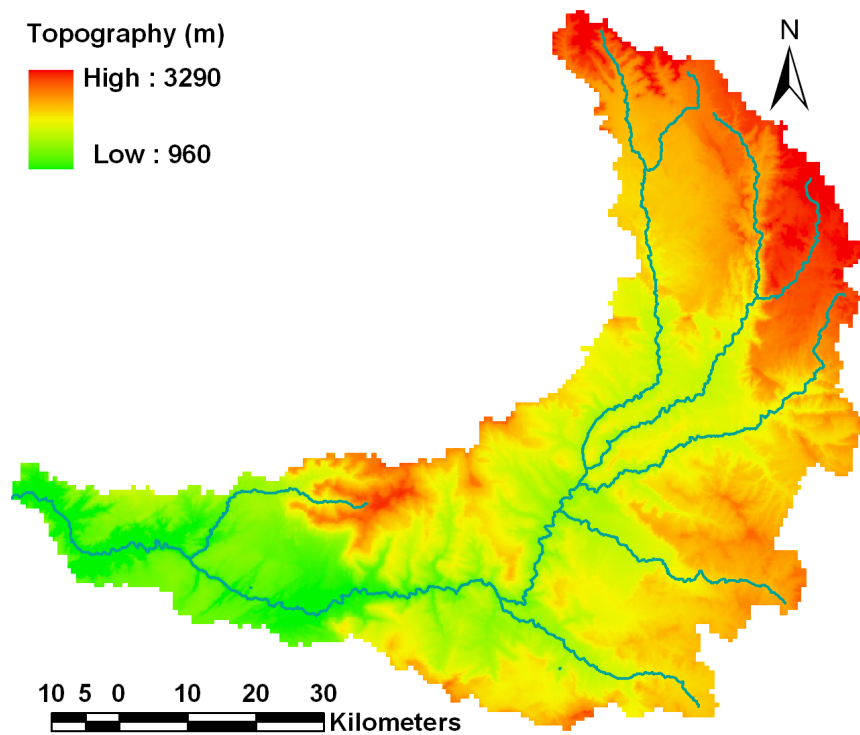


Figure 2. Topographic elevation map of the Geba basin.

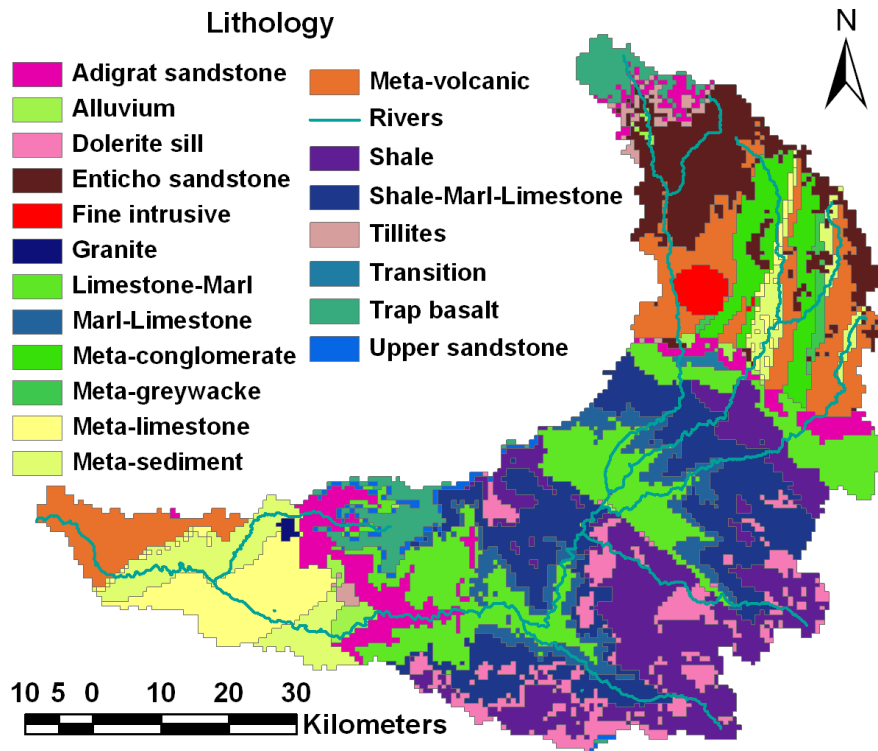


Figure 3. Map showing lithological units in the Geba basin.

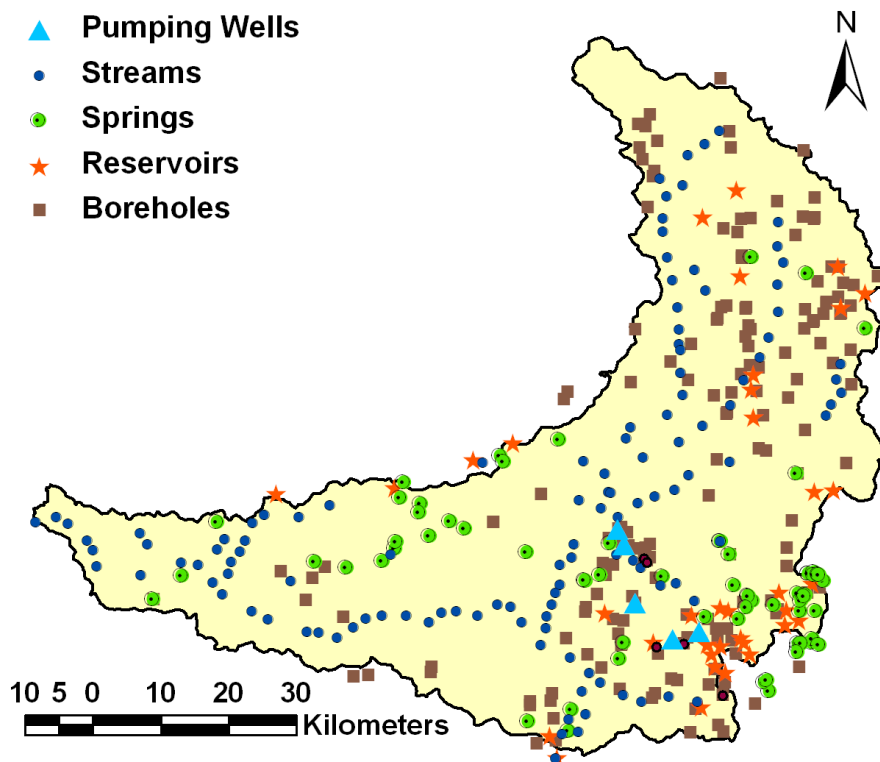


Figure 4. Locations of surface and groundwater levels observed during field campaigns.

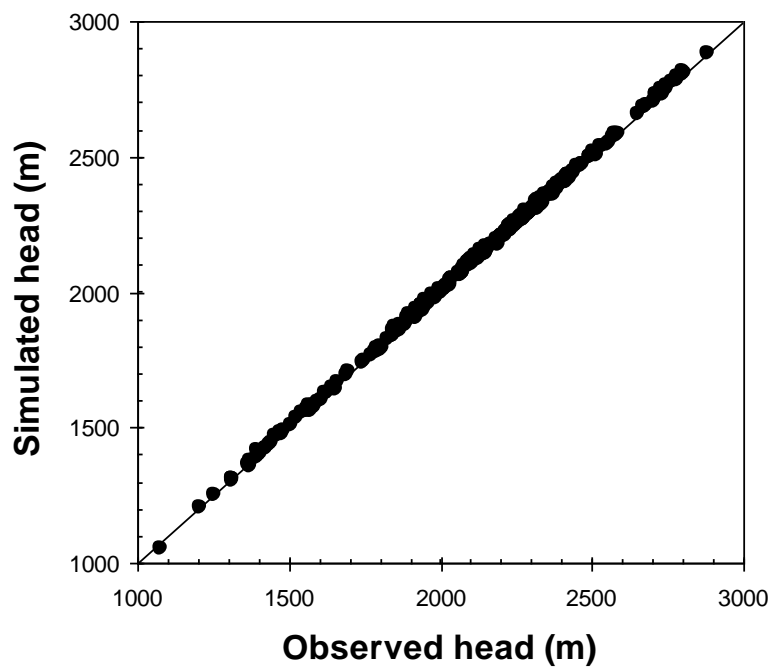


Figure 5. Scatter plot of calculated versus observed groundwater heads.

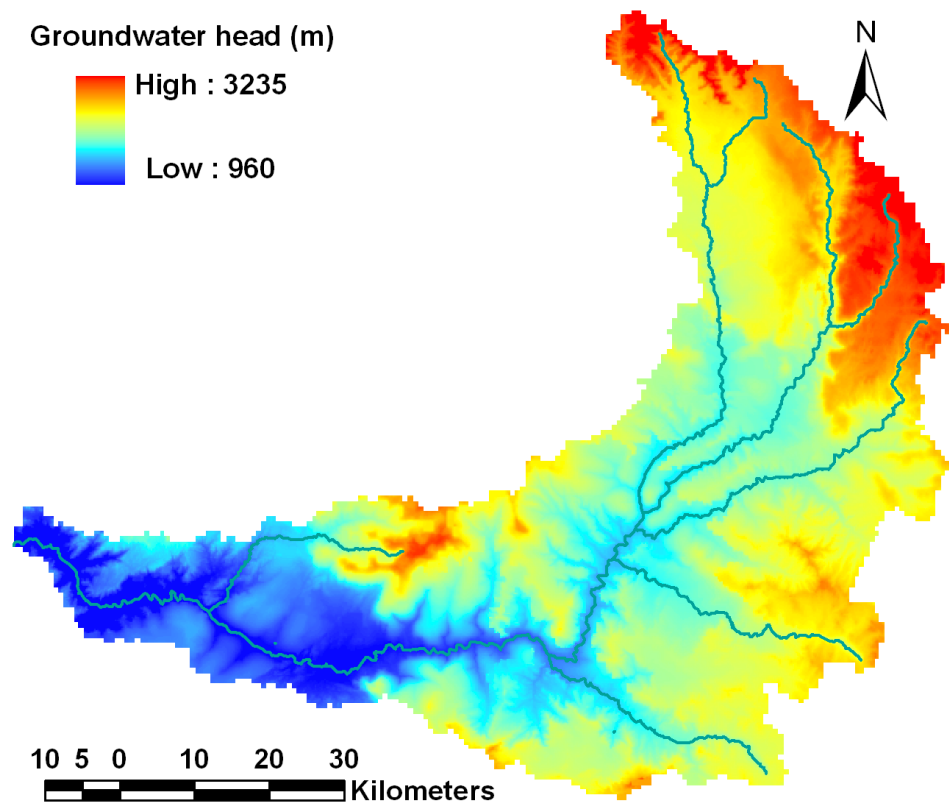


Figure 6. Simulated groundwater heads in the Geba basin.

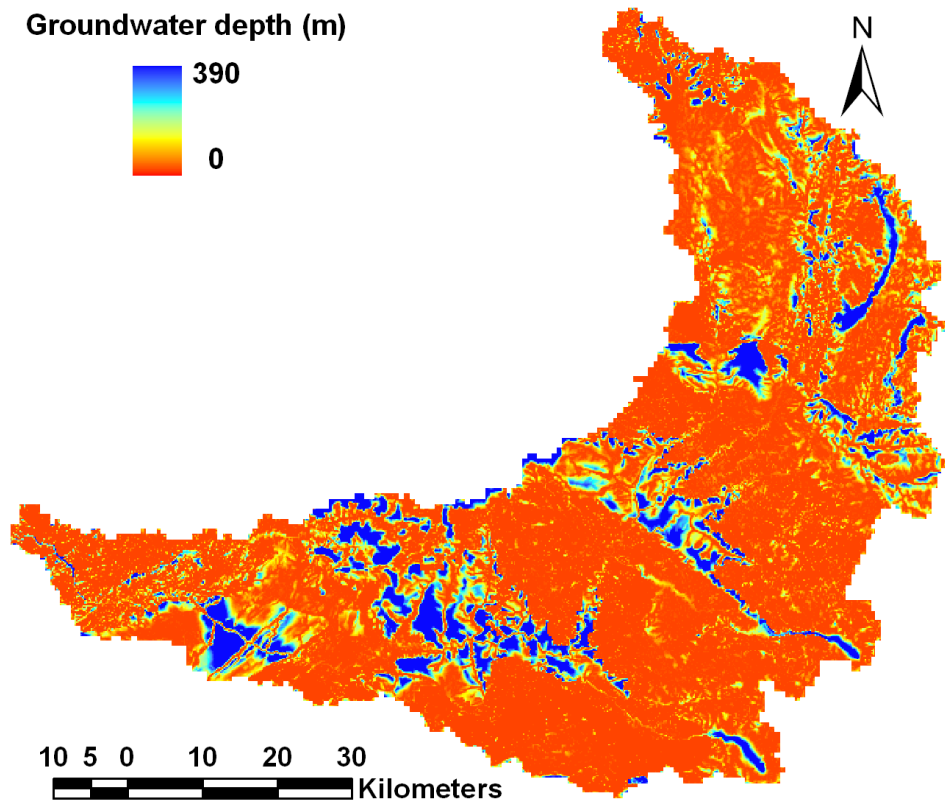


Figure 7. Depth to groundwater map of the Geba basin.